

# Parametric Models

- Models for Dynamic Systems
- Plant Parametric Models

# Contents

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- Plant Parametric Models

# State-Space Models for Dynamic Systems

State-Space Models:

$$\dot{x}(t) = f(x(t), u(t), t), \quad x(t_0) = x_0 \in \mathbb{R}^n$$

$$y(t) = g(x(t), u(t), t)$$

where

- $t$  is the time variable
- $x(t)$  is an  $n$ -dimensional vector with real elements that denotes the state of the system
- $u(t)$  is an  $r$ -dimensional vector with real elements that denotes the input variable or control input of the system

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- $y(t)$  is an  $l$ -dimensional vector with real elements that denotes the output variables that can be measured
- $f, g$  are real vector valued functions
- $x(t_0)$  denotes the value of  $x(t)$  at the initial time  $t = t_0 \geq 0$

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# State-Space Models for Dynamic Systems

LTV system: when  $f, g$  are linear functions of  $x$  and  $u$

$$\dot{x} = A(t)x + B(t)u, \quad x(t_0) = x_0$$

$$y = C^\top(t)x + D(t)u$$

where  $A(t) \in \mathcal{R}^{n \times n}$ ,  $B(t) \in \mathcal{R}^{n \times r}$ ,  $C(t) \in \mathcal{R}^{n \times l}$ ,  $D(t) \in \mathcal{R}^{l \times r}$ . If in addition to being linear,  $f, g$  do not depend on time  $t$ , we have

$$\dot{x} = Ax + Bu, \quad x(t_0) = x_0$$

$$y = C^\top x + Du$$

where  $A, B, C$ , and  $D$  are matrices of the same dimension as above but with constant elements.

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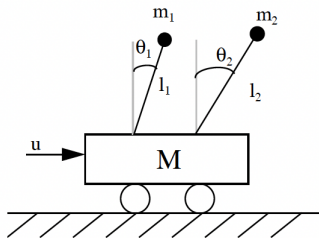
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**Figure 2.1** Cart with two inverted pendulums

Example: Let us consider the cart with the two inverted pendulums shown in Figure 2.1, where  $M$  is the mass of the cart,  $m_1$  and  $m_2$  are the masses of the bobs, and  $l_1$  and  $l_2$  are the lengths of the pendulums, respectively.

Example: Using Newton's law and assuming small angular deviations of  $|\theta_1|, |\theta_2|$ , the equations of motions are given by

$$M\dot{v} = -m_1g\theta_1 - m_2g\theta_2 + u$$

$$m_1 \left( \dot{v} + l_1 \ddot{\theta}_1 \right) = m_1 g \theta_1$$

$$m_2 \left( \dot{v} + l_2 \ddot{\theta}_2 \right) = m_2 g \theta_2$$

where  $v$  is the velocity of the cart,  $u$  is an external force, and  $g$  is the acceleration due to gravity. Assume that  $m_1 = m_2 = 1$  kg and  $M = 10m_1$ . If we now let  $x_1 = \theta_1$ ,  $x_2 = \dot{\theta}_1$ ,  $x_3 = \theta_1 - \theta_2$ ,  $x_4 = \dot{\theta}_1 - \dot{\theta}_2$  be the state variables, write the dynamic of the system into the following form:

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Let  $x = [x_1, x_2, x_3, x_4]^\top$ , we have the 4th order system is described by

$$\dot{x} = Ax + Bu$$

with

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 1.2\alpha_1 & 0 & -0.1\alpha_1 & 0 \\ 0 & 0 & 0 & 1 \\ 1.2(\alpha_1 - \alpha_2) & 0 & \alpha_2 - 0.1(\alpha_1 - \alpha_2) & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ \beta_1 \\ 0 \\ \beta_1 - \beta_2 \end{bmatrix}$$

and  $\alpha_1 = \frac{g}{l_1}$ ,  $\alpha_2 = \frac{g}{l_2}$ ,  $\beta_1 = -\frac{0.1}{l_1}$ , and  $\beta_2 = -\frac{0.1}{l_2}$ .

## Solutions

For LTV system:

$$x(t) = \Phi(t, t_0)x(t_0) + \int_{t_0}^t \Phi(t, \tau)B(\tau)u(\tau)d\tau$$

with  $\Phi(t, t_0)$  is transition matrix, satisfies

$$\frac{\partial \Phi(t, t_0)}{\partial t} = A(t)\Phi(t, t_0), \quad \Phi(t_0, t_0) = I$$

For LTI system, it holds  $\Phi(t, t_0) = e^{A(t-t_0)}$  and the solution

$x(t), y(t)$  are given by

$$x(t) = e^{A(t-t_0)}x_0 + \int_{t_0}^t e^{A(t-\tau)}Bu(\tau)d\tau$$

$$y(t) = C^T x(t) + Du(t)$$

Note: In this course, we usually assume  $D$  matrix is zero.

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# Input-Output Model

Consider a system described by the  $n$ th-order differential equation

$$y^{(n)}(t) + a_{n-1}y^{(n-1)}(t) + \cdots + a_0y(t) = b_mu^{(m)}(t) + \cdots + b_0u(t)$$

where

$$y^{(i)}(t) \triangleq \frac{d^i}{dt^i}y(t), \text{ and } u^{(i)}(t) \triangleq \frac{d^i}{dt^i}u(t);$$

$u(t)$  is the input variable, and  $y(t)$  is the output variable;

the coefficients  $a_i, b_j, i = 0, 1, \dots, n-1, j = 0, 1, \dots, m$  are

constants, and  $n$  and  $m$  are constant integers.

*Note, above equation can only describe single-input-single-output (SISO) system.*

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To obtain the transfer function, we take the Laplace transform on both sides of the equation and assume zero initial conditions

$$G(s) \triangleq \frac{Y(s)}{U(s)} = \frac{b_m s^m + b_{m-1} s^{m-1} + \cdots + b_0}{s^n + a_{n-1} s^{n-1} + \cdots + a_0}$$

*Definitions:*

1. We say that  $G(s)$  is proper, if  $n \geq m$ ; strictly proper if  $n > m$ ; and biproper if  $n = m$ .
2. The relative degree  $n^*$  of  $G(s)$  is defined as  $n^* = n - m$ .
3. Coprime

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1. Characteristic equation  $P(s) = 0$
2. Roots of  $P(s) = 0$  are poles of system =  $\text{eig}[A]$
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## Relation between SS and TF

SS representation

$$\dot{x} = Ax + Bu, \quad x(t_0) = x_0$$

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Transfer function

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From a SS representation to a transfer function:

$$G(s) = C^\top (sI - A)^{-1} B + D$$

From a transfer function description to a SS representation, is not as straightforward and not *Unique*.

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## Relation between SS and TF

For instance, consider a 4th order system

$$G(s) = \frac{Y(s)}{U(s)} = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{s^4 + a_3 s^3 + a_2 s^2 + a_1 s + a_0} \frac{Z(s)}{Z(s)}.$$

Notice that, by multiplying by  $Z(s)/Z(s)$ , we do not change the transfer function,  $G(s)$ . Equating the numerator and denominator polynomials yields

$$Y(s) = [b_3 s^3 + b_2 s^2 + b_1 s + b_0] Z(s)$$

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Define the four state variables as follows:

$$x_1(t) = z(t)$$

$$x_2(t) = \dot{x}_1(t) = \dot{z}(t)$$

$$x_3(t) = \dot{x}_2(t) = \ddot{z}(t)$$

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*Exercise:* Consider a fourth order dynamics

$$y^{(4)} - 1.1(\alpha_1 + \alpha_2)y^{(2)} + 1.2\alpha_1\alpha_2y = \beta_1u^{(2)} - \alpha_1\beta_2u$$

find its transfer function and ss presentation.

## Canonical form

For transfer function

$$G(s) \triangleq \frac{Y(s)}{U(s)} = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_0}{s^n + a_{n-1} s^{n-1} + \dots + a_0}$$

controllable canonical form

$$\dot{x}_c = \begin{bmatrix} 0 & 1 & \dots & 0 & 0 \\ 0 & 0 & \ddots & \dots & 0 \\ \vdots & \vdots & & \ddots & \vdots \\ 0 & 0 & \dots & 0 & 1 \\ -a_0 & -a_1 & \dots & -a_{n-2} & -a_{n-1} \end{bmatrix} x_c + \begin{bmatrix} 0 \\ 0 \\ 0 \\ \vdots \\ 1 \end{bmatrix} u$$
$$y = \begin{bmatrix} b_0 & b_1 & \dots & b_m & 0 & \dots & 0 \end{bmatrix} x_c$$

## Canonical form

or in the observer form

$$\dot{x} = \begin{bmatrix} -a_{n-1} & 1 & 0 & \cdots & 0 \\ -a_{n-2} & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & & \ddots & \vdots \\ -a_1 & 0 & 0 & \cdots & 1 \\ -a_0 & 0 & 0 & \cdots & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ \vdots \\ b_m \\ \vdots \\ b_0 \end{bmatrix} u$$
$$y = [1, 0, \dots, 0]x$$

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## Linear Parametric Model

Consider an  $n$ -th order differential equation given by

$$y^{(n)} + a_{n-1}y^{(n-1)} + \cdots + a_0y = b_{n-1}u^{(n-1)} + b_{n-2}u^{(n-2)} + \cdots + b_0u$$

where  $a_i$  and  $b_i$  are unknown parameters characterizing the plant.

IF the system can be written in the compact form of

$$z = \theta^\top \phi \tag{1}$$

where  $\theta$  is a vector contains all the unknown parameter,  $z$  and  $\phi$  are signal available for measurement, then we refer (1) as *Linear Static Parametric Model* (SPM)

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IF the system can be written in the compact form of

$$z = W(s)(\theta^\top \phi) \quad (2)$$

where  $\theta$  is a vector contains all the unknown parameter,  $z$  and  $\phi$  are signal available for measurement,  $W(s)$  **is a known stable proper transfer function** then we refer (2) as *Linear Dynamic Parametric Model* (DPM)

## Linear Parametric Model

For SPM and DPM, given the measurements  $z(t), \phi(t)$ , we can design on-line estimation algorithm that estimates  $\theta$  with  $\hat{\theta}(t)$  at each time.

The linearity is important for accurate estimation!

Example: Consider a first-order system

$$\dot{x} = -x + ax + bu$$

where  $a, b$  are unknown parameters.

How about  $\dot{x} = ax + bu$ ? What if  $\dot{x}$  is not available?

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## Bilinear Parametric Model

A special case of nonlinear in the parameters models for which convergence results exist is

$$z = \rho(\theta^\top \phi + z_1) \quad (3)$$

and

$$z = W(s)\rho(\theta^\top \phi + z_1) \quad (4)$$

where  $\theta, \rho$  are unknown parameters,  $z, z_1$  and  $\phi$  are signals available for measurement,  $W(s)$  is a known stable proper transfer function then we refer (3) and (4) as *Bilinear Static Parametric Model* (B-SPM) and *Bilinear Dynamic Parametric Model* (B-DPM), respectively.

## Bilinear Parametric Model

Example: Consider the mass-spring-dashpot system shown in Figure 2.1. Using Newton's law, we obtain the differential equation that describes the dynamics of the system as

$$M\ddot{x} = u - kx - f\dot{x}$$

Let us assume that the mass  $M$ , damping coefficient  $f$  and spring-coefficient  $k$  are the constant unknown parameters that we want to estimate online, write the parametric model of the system.

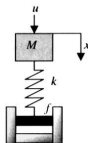


Figure 2.1. Mass-spring-dashpot system.

## Bilinear Parametric Model

Example: Consider the second ARMA model

$$y(k+4) = -a_1y(k+3) - a_2y(k+2) + b_1u(k+1) + b_2u(k)$$

where  $y(k)$  and  $u(k)$  are available signals. Express the model into a form of SPM.

What if  $a_1 \neq 0$  but is very small, and the rest of unknown parameters are extremely large, can you write the model into a B-SPM form so that the parameter estimation will be in similar range?

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## Bilinear Parametric Model

Generalization: Consider a general SISO LTI system with transfer function equals to

$$G(s) \triangleq \frac{Y(s)}{U(s)} = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_0}{s^n + a_{n-1} s^{n-1} + \dots + a_0}$$

Given  $m \leq n$  and only  $y(t)$  and  $u(t)$  are available for measurements. Express the model into a form of SPM.

$$z = \frac{1}{\Lambda(s)} y^{(n)} = \frac{s^n}{\Lambda(s)} y$$

$$\theta^* = [b_m, \dots, b_0, a_{n-1}, \dots, a_0]^T \in \mathcal{R}^{n+m+1}$$

$$\phi = \left[ \frac{s^m}{\Lambda(s)} u, \dots, \frac{1}{\Lambda(s)} u, -\frac{s^{n-1}}{\Lambda(s)} y, \dots, -\frac{1}{\Lambda(s)} y \right]^T$$

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## Summary:

- System Modeling: SS and Transfer function
- Four parametric models