

Model-based analysis of granulation and drying in continuous manufacturing

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PSE Advanced Process Modelling Forum





Outline

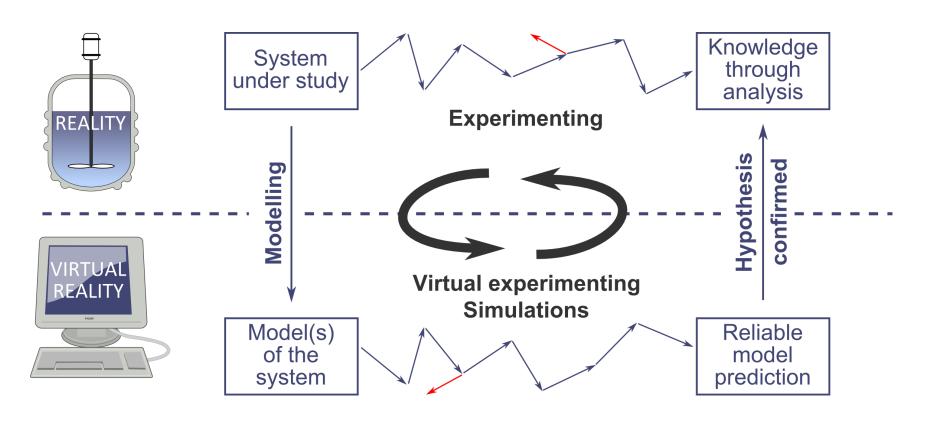
- Introduction
- Tools for model-based analysis
- Examples of ConSigma
 - Twin screw wet granulation
 - Fluid bed drying
- Another promising tool





Why modelling?

Model-based ANALYSIS → build knowledge

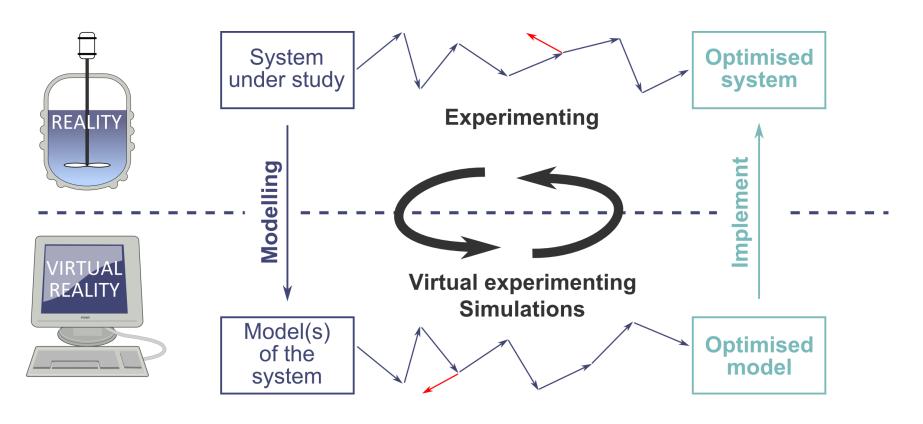






Why modelling?

Model-based OPTIMISATION → optimise



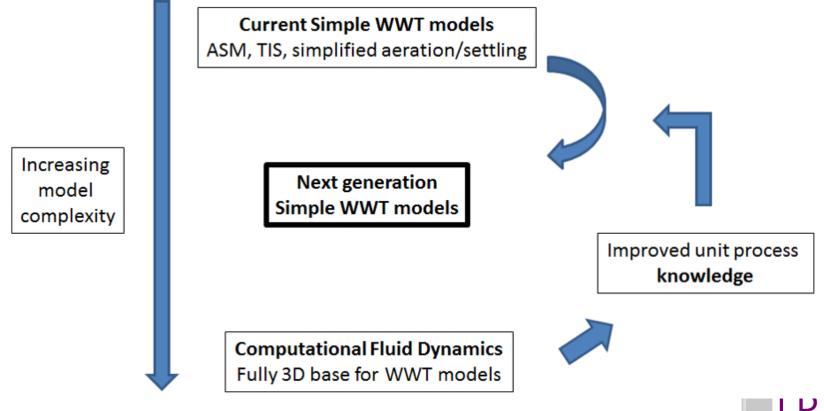




One or more models?

Different objectives require different models

One single model to meet all objectives for a unit process or flow sheet does not exist!

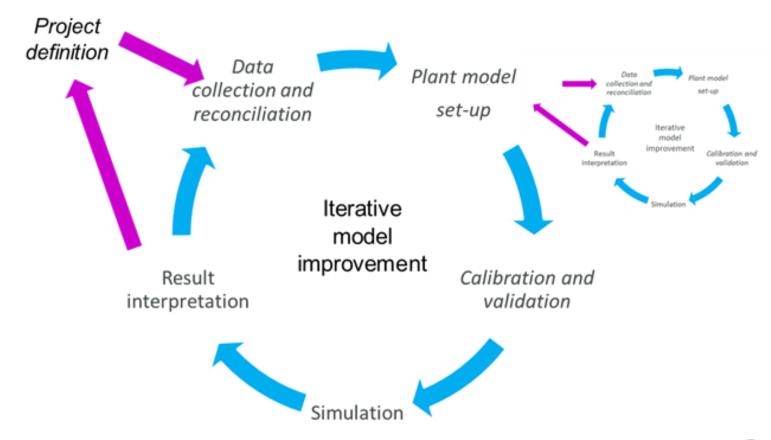


BI@MATH



One or more models?

Models have a life cycle

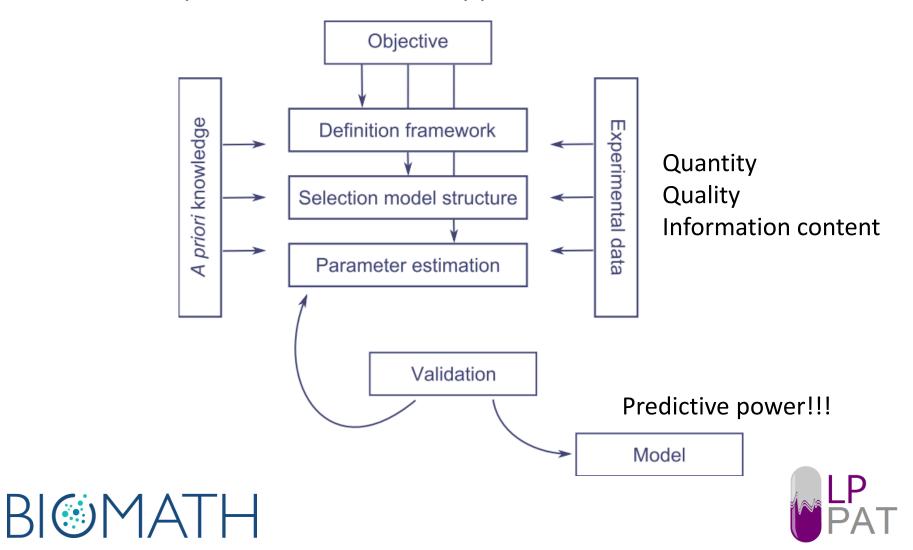






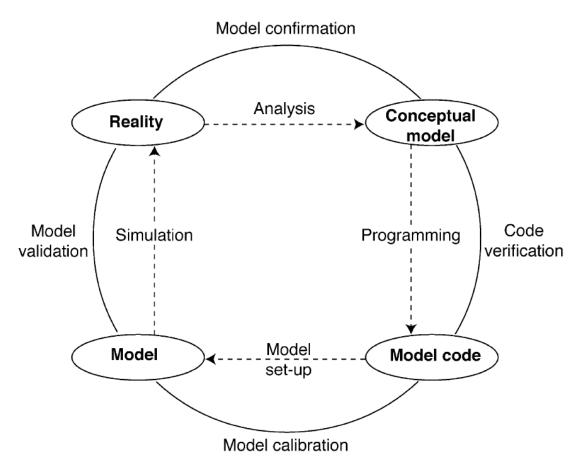
Model building process

Tedious step-wise and iterative approach



Terminology

Calibration – verification - validation







Sensitivity analysis

- Select parameters for parameter estimation
- Model reduction
- Reducing model uncertainty
- Propose informative experiments
 - Model selection
 - Parameter estimation





Sensitivity analysis

- Local
 - 1 point in parameter space
 - Fast computation
- Global
 - "average" sensitivity in bounded parameter space
 - Computationally expensive



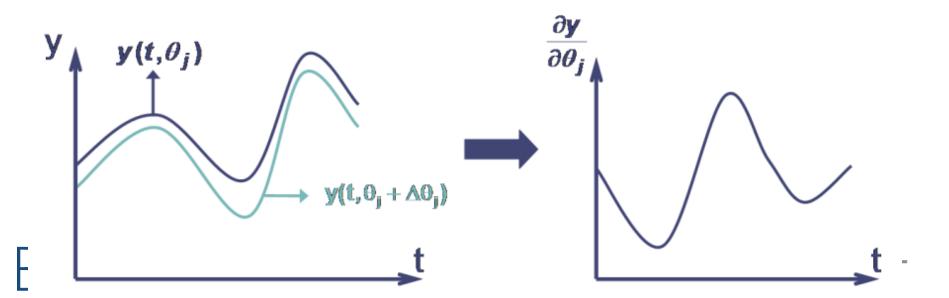


Local Sensitivity analysis

$$\frac{\partial y}{\partial \theta}$$

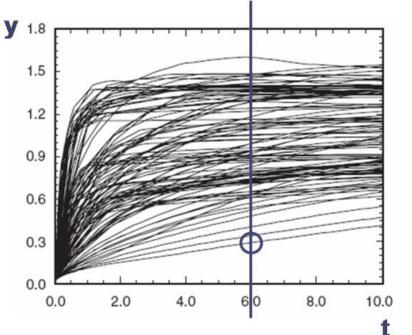
Finite difference approximation

$$\frac{\partial y(t)}{\partial \theta_j} = \lim_{\Delta \theta_j \to 0} \frac{y(t, \theta_j + \Delta \theta_j) - y(t, \theta_j)}{\Delta \theta_j}$$



Global Sensitivity analysis

- Standardised regression coefficients
- → Linear regression of Monte Carlo analysis



$$Y = \Theta \cdot B + E$$

$$\begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_n \end{bmatrix} = \begin{bmatrix} 1 & \theta_{11} & \theta_{12} & \cdots & \theta_{1p} \\ 1 & \theta_{21} & \theta_{22} & \cdots & \theta_{2p} \\ \vdots & \vdots & \vdots & & \vdots \\ 1 & \theta_{n1} & \theta_{n2} & \cdots & \theta_{np} \end{bmatrix} \begin{bmatrix} b_0 \\ b_1 \\ \vdots \\ b_p \end{bmatrix} + \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \vdots \\ \epsilon_n \end{bmatrix}$$

$$SRC_{\theta_i} = b_i \cdot \frac{\sigma_{\theta_i}}{\sigma_y}$$

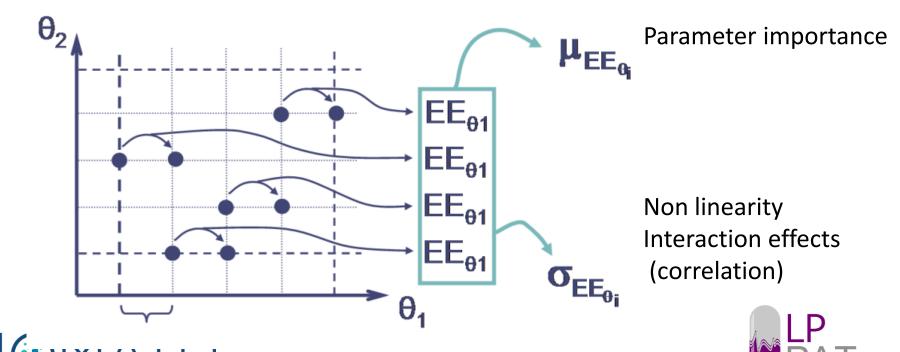




Global Sensitivity analysis

Morris screening – Elementary effects

$$EE_{\theta_i} = \frac{y(\theta_i + \Delta) - y(\theta)}{\Delta}$$



Global Sensitivity analysis

Variance decomposition

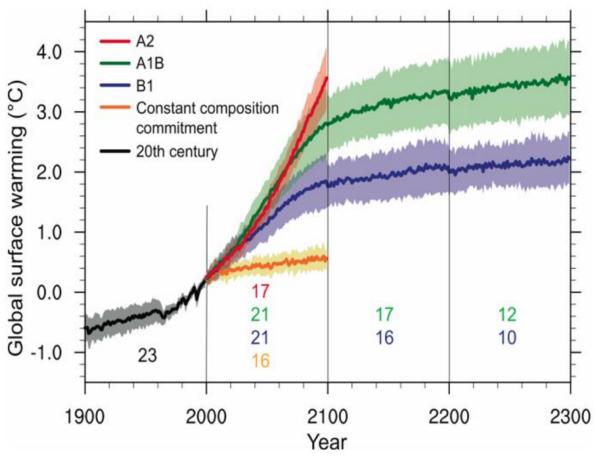
$$\sigma_y^2 = \sigma_1^2 + \sigma_2^2 + \sigma_3^2 + \sigma_{12}^2 + \sigma_{13}^2 + \sigma_{23}^2 + \sigma_{123}^2$$
$$1 = S_1 + S_2 + S_3 + S_{12} + S_{13} + S_{23} + S_{123}$$

- FAST (Fourier Amplitude Sensitivity Test)
- Sobol indices
- Computationally expensive
 - Valid for non-linear models





Uncertainty analysis







Uncertainty analysis

Uncertainties in

- Model structure
- Model implementation
- Measurement error (calibration)
- Model input (predictive)
- Model parameters (uncertainty in estimation)





Uncertainty analysis

Linear approximation: differential analysis

$$y = f(x_1, x_2, \dots, x_n)$$
 \rightarrow $\sigma_y^2(t) = \sum_n \sigma_{x_i}^2 \left(\frac{\partial y(t)}{\partial x_i}\right)^2$

Output Cl

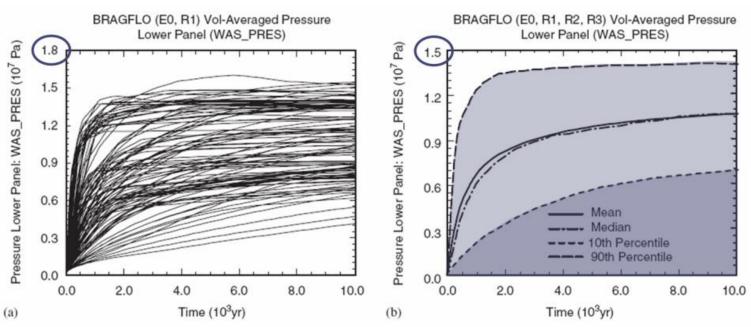
$$\delta_{y} = \pm t_{N-p}^{\alpha} \sigma_{y}$$





Uncertainty analysis

Statistics of Monte Carlo analysis







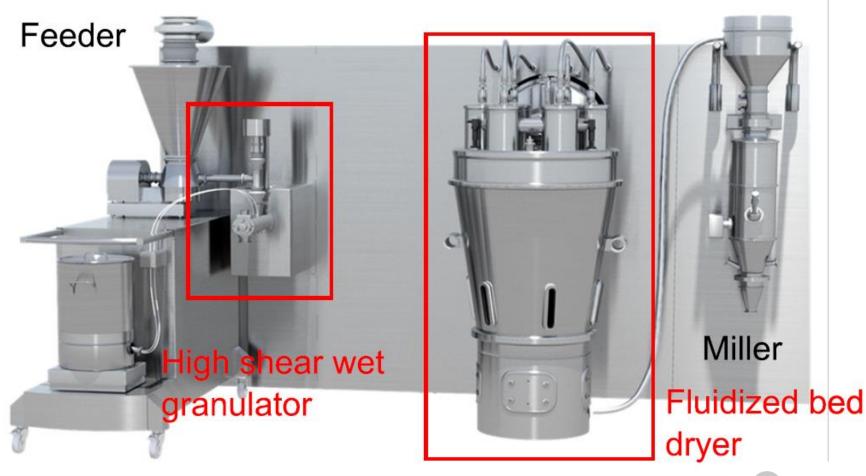
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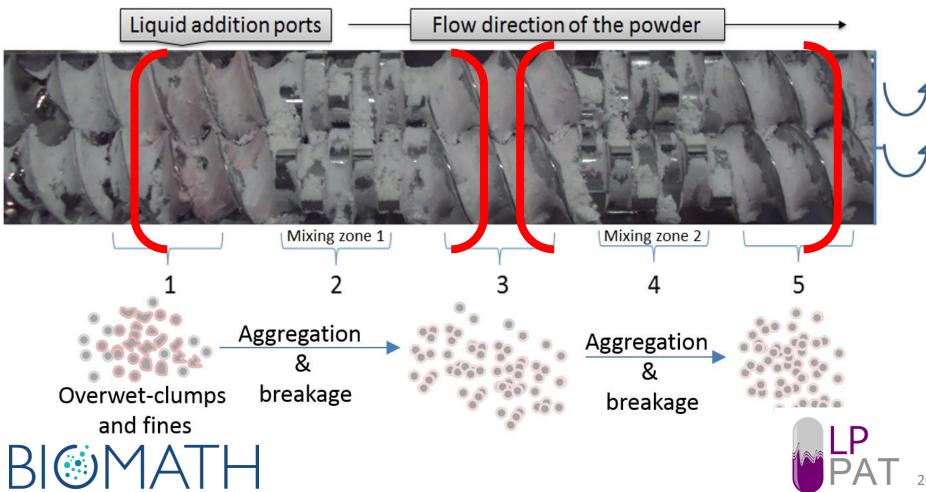
The process under study: ConsiGmaTM-25







The system and its mechanisms:



Slide with breakdown in PBMs



Combination of aggregation and breakage

- → Kernel choice
- → parameters unknown

Tough optimisation problem





Local optimisation likely fails

Calibration requires global search algorithms:

Global Sensitivity Analysis

Which parameter in the PBM-kernels (breakage or aggregation) is sensitive

> Parameters to be calibrated

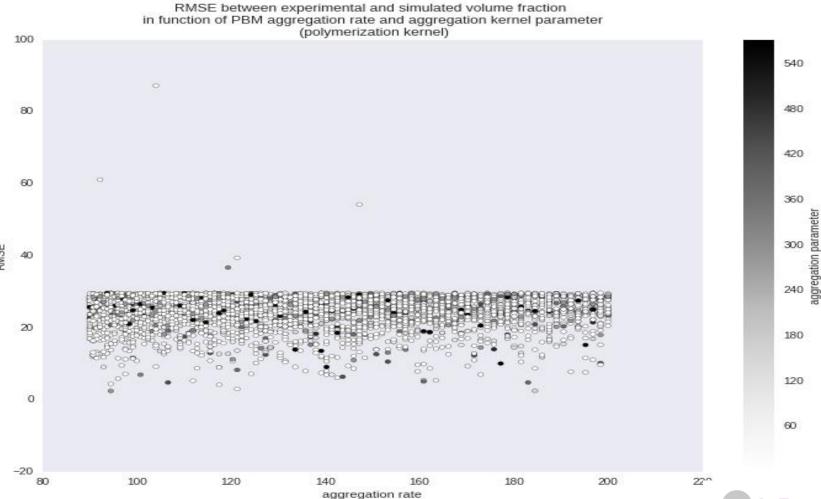
Global Optimisation Algorithms

Exploring the whole parameter space

Thousands of simulations

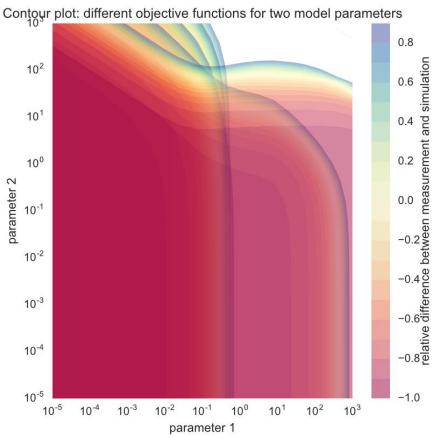








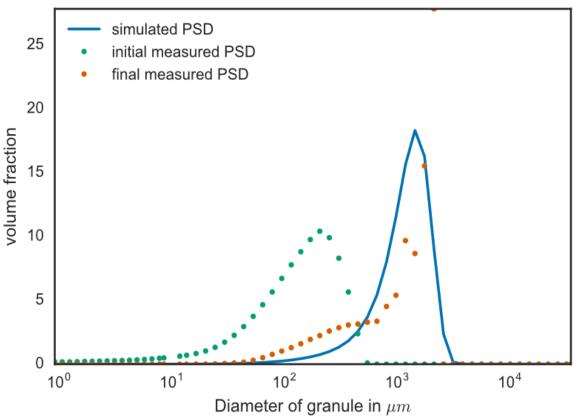
Impact of choice of objective function (RMSE, SSE, D43,...)







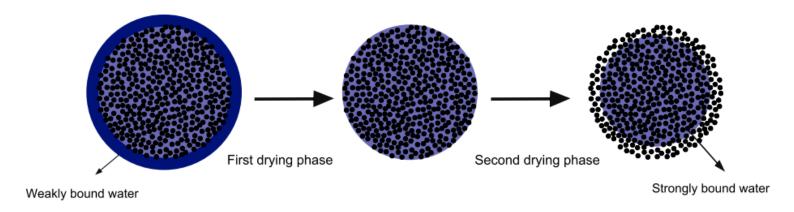
Simulation results with calibrated model parameters







Conceptualisation of reality:



1. Fast drying phase

$$\dot{m}_{v} = h_{D}(\rho_{v,s} - \rho_{v,\infty})A_{d}$$

2. Slow drying phase

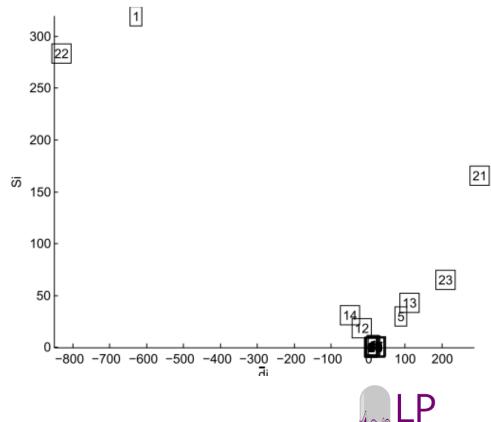
$$\dot{m}_{v} = -\frac{8\pi\epsilon^{\beta_{1}e^{-\beta_{2}T_{g}}}D_{v,cr}M_{w}p_{g}}{\Re(T_{cr,s} + T_{wc,s})}In[\frac{p_{g} - p_{v,i}}{p_{g} - (\frac{\Re}{4\pi M_{w}h_{D}R_{p}^{2}}\dot{m}_{v} + \frac{p_{v,\infty}}{T_{g}})T_{p,s}}]$$





Global Sensitivity Analysis

| Nr. | Factor | Nominal value |
|------------|---------------------------|---|
| 1 | $\mathrm{T_{g}}$ | 55 °C |
| 2 | V_g | $200 \text{ m}^3/\text{h}$ |
| 3 | $\mathbf{p_g}$ | 101000 Pa |
| 4 | $\mathbf{R}_{\mathbf{p}}$ | $0.6\mathrm{mm}$ |
| 5 | Humidity | 9% |
| 6 | $T_{p,0}$ | 25 °C |
| 7 | ϵ | 0.05 |
| 8 | μ_{gas} | $0.00002\mathrm{kg/m/s}$ |
| 9 | $ ho_{gas}$ | $1.2\mathrm{kg/m^3}$ |
| 10 | k_{gas} | $0.0285\mathrm{W/m/K}$ |
| 11 | $c_{p,gas}$ | $1009\mathrm{kg/m^3}$ |
| ${\bf 12}$ | $\mathbf{M}\mathbf{w}$ | $18.015\mathrm{e}	ext{-}3\mathrm{kg/mol}$ |
| 13 | $ ho_{	ext{liquid}}$ | $1000\mathrm{kg/m^3}$ |
| $\bf 14$ | $\rho_{\mathbf{solid}}$ | $1525\mathrm{kg/m^3}$ |
| 15 | $k_{droplet}$ | $0.07\mathrm{W/m/K}$ |
| 16 | k_{liquid} | $0.63\mathrm{W/m/K}$ |
| 17 | k_{solid} | $0.75\mathrm{W/m/K}$ |
| 18 | $c_{p,s}$ | $1252\mathrm{kg/m^3}$ |
| 19 | TWC | $647.13\mathrm{K}$ |
| 20 | ϵ_{rs} | 0.8 |
| 21 | $eta_{f 1}$ | 4912.4 |
| 22 | β_{2} | -0.024282 |
| 23 | $R_{w,0,fac}$ | 1.025 |





Global Sensitivity Analysis

| Technique | k | N | Most sensitive factors |
|----------------------|----|------|--|
| Morris screening | 23 | 240 | β_2 - T_g - β_1 - $R_{w,0,fac}$ |
| CSM plot | 10 | 400 | β_2 - T_g |
| SRC | 10 | 1000 | - |
| SRRC | 10 | 1000 | β_2 - $R_{w,0,fac}$ - T_g - ρ_{solid} |
| S_i | 10 | 1000 | β_2 - T_g - β_1 -Mw |
| S_{Ti} | 10 | 1000 | eta_2 - T_g - eta_1 - $ ho_{liquid}$ |

Choose parameters to estimate
Check model robustness (uncertainty)





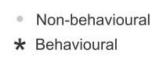
Uncertainty Analysis

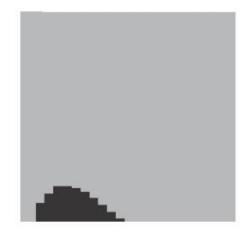
| Case | Parameter | Calibrated value | Range in uncertainty |
|------|-----------------|--------------------------------|------------------------------|
| 1 | ϵ | 0.05 | 50% |
| 1 | $V_{ m g}$ | 200 m ³ /h | 50% |
| 1 | R_p | $0.6 \times 10^{-3} \text{ m}$ | 50% |
| 2 | β_1 | 4.91×10^{3} | 20% |
| 2 | β_2 | 2.43×10^{-2} | 20% |
| 3 | ϵ | 0.05 | [0.03-0.06] |
| 3 | $V_{ m g}$ | 200 m ³ /h | 20% |
| 3 | R_p | $0.6 \times 10^{-3} \text{ m}$ | $[0.30-0.65 \times 10^{-3}]$ |
| 3 | $\dot{\beta_1}$ | 4.91×10^{3} | 20% |
| 3 | β_2 | 2.43×10^{-2} | [0.022-0.026] |



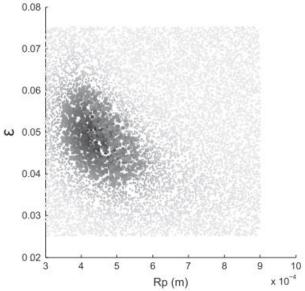


Uncertainty Analysis



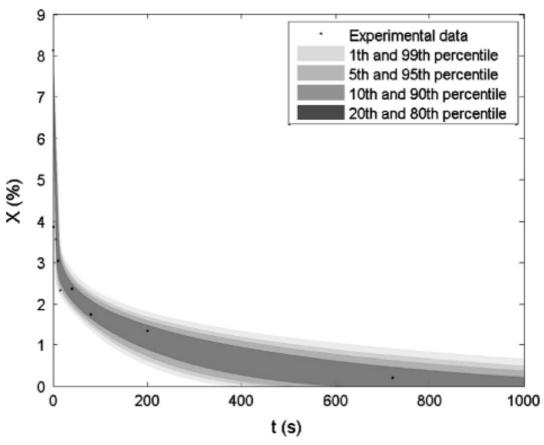








Uncertainty Analysis: model predictive power







Outline

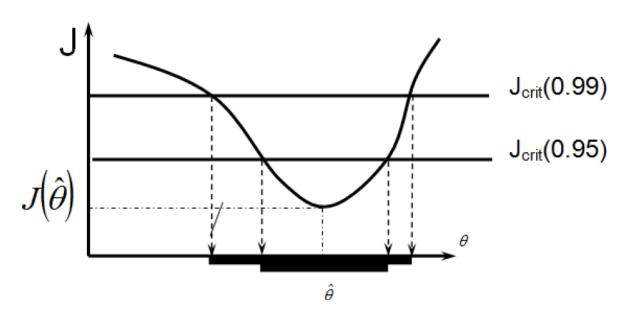
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Optimal experimental design (OED)

Quality of parameter estimate



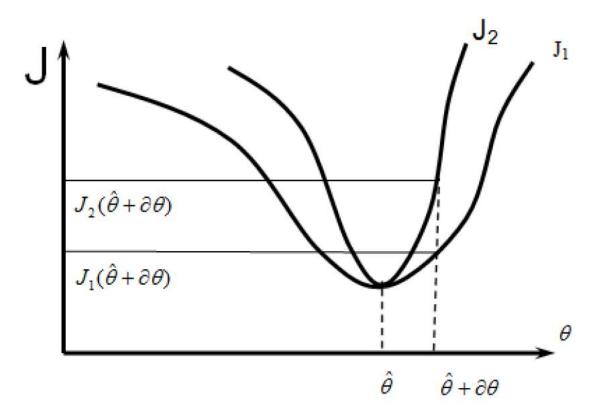
$$\left\{\boldsymbol{\theta} : J(\boldsymbol{\theta}) \leq c \times J(\hat{\boldsymbol{\theta}})\right\}$$





Optimal experimental design (OED)

How to improve quality of parameter estimate?







Optimal experimental design (OED)

How to improve quality of parameter estimate?

$$E\left[J\left(\hat{\theta} + \delta\theta\right)\right] = J\left(\hat{\theta}\right) + \delta\theta^{T} \left[\sum_{i=1}^{N_{data}} \left(\frac{\partial y}{\partial \theta}\right)_{i}^{T} Q_{i} \left(\frac{\partial y}{\partial \theta}\right)_{i}\right] \delta\theta$$

Fisher Information Matrix (FIM)

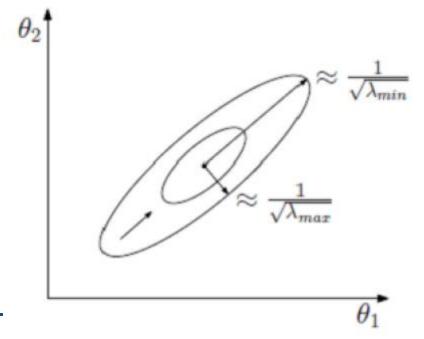
- Iterative procedure
 - Conduct exp, calibrate, propose new exp, etc
 - Reduction of # exp (vs. DOE)





Optimal experimental design (OED)

- How to improve quality of parameter estimate?
- Maximise FIM
 - D-optimal max [det(FIM)]







Conclusions

- Good modelling practice is important
- Use appropriate modelling tools to make choices
- E.g. calibration of complex models → use global methods
 - Computationally expensive
 - But yield a lot of information on the model and can assist in experimental data collection (Optimal Experimental Design)
- Techniques exist, we need to use them





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