# APM 2013



The Advanced Process Modelling Forum

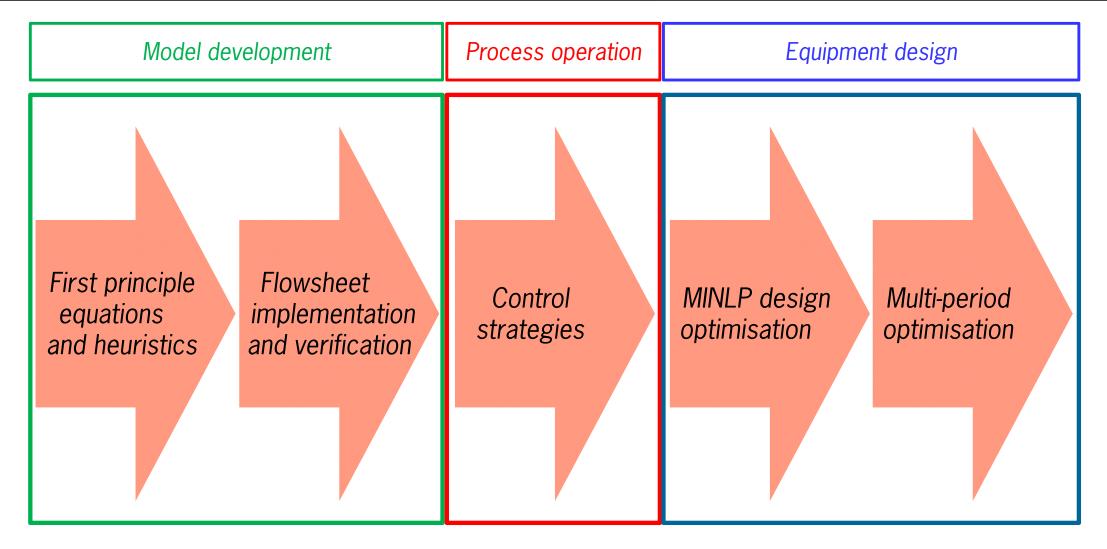
17-18 April 2013, London

Optimising compression train design and operation for flexible design

Mario Calado – Consultant, Power & CCS

#### Overview

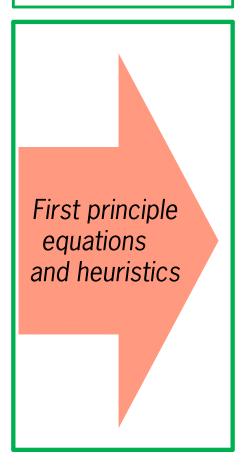




# Overview



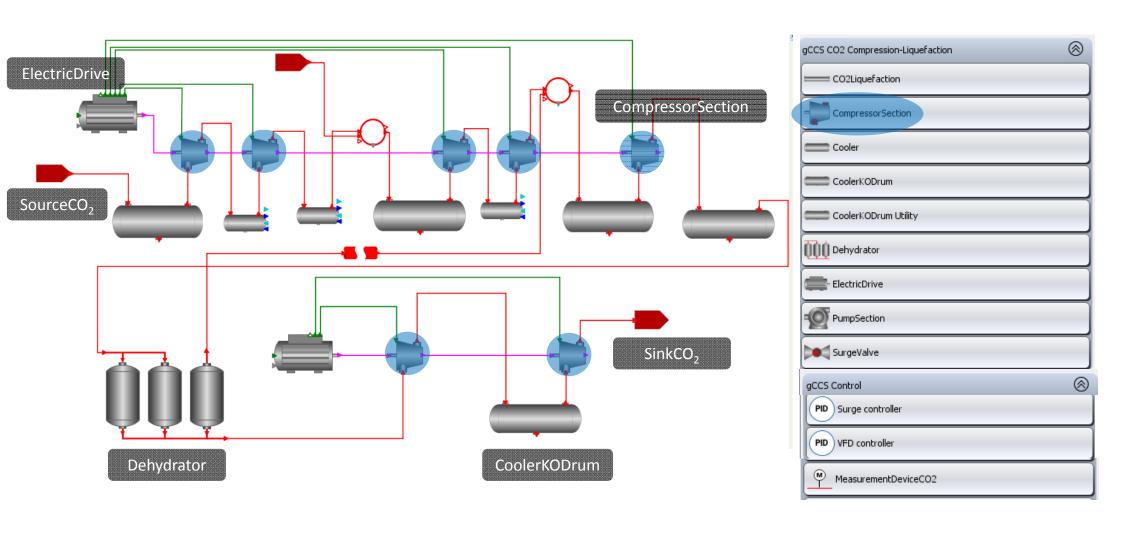
#### Model development



# gCCS Compression-Liquefacion

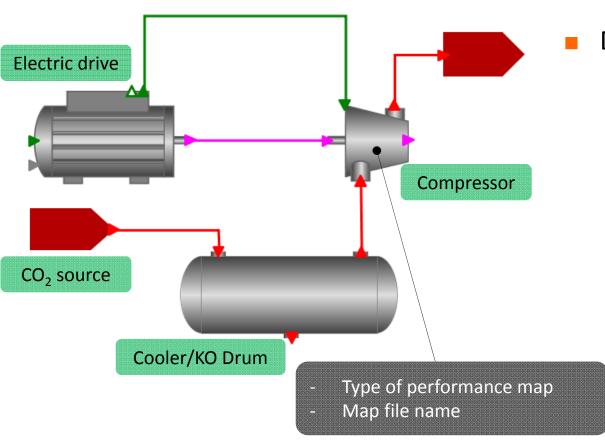
Component models





Main specifications





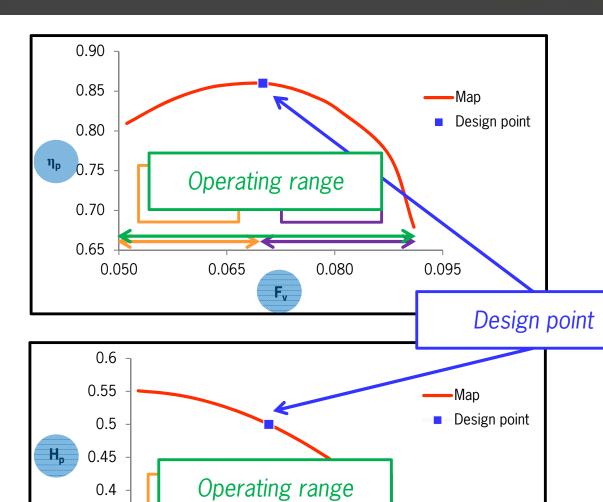
- Detailed compressor modelling
  - know-how & expertise supplied by Rolls-Royce
- Different types of performance map

Specification preview: CompressorSection						
		-				
Mode	Performance only ▼					
Performance specification	Compressor maps  ▼					
Map type	1-D ( H_p(Q) and η(Q) )   ▼					
Specify  Map	1-D (H_p(Q) and η(Q)) 1-D dimensionless (Ψ(Φ) and η(Φ)) 2-D (H_p(Q,ω) and η(Q,ω))					
<ul><li>✓ Gear speed multip</li><li>✓ Design speed</li></ul>	lier 1.0	Hz				
OK Cancel Reset All Help						

0.065

Performance maps





0.08

Fv

0.095

- Performance map based on flow/head and flow/efficiency curves
- Design point corresponds to the maximum efficiency
- Compressor has a flow operating range

**Surge**: distance from minimum flow

Choke: distance from maximum flow

Both need to be controlled in order to maintain operability

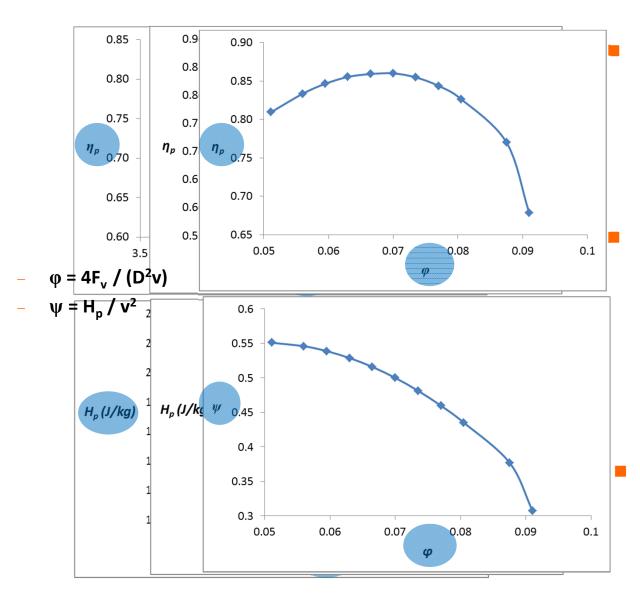
0.35

0.3

0.05

#### Performance maps





#### 1D maps

- Efficiency/flow curve
- Head/Flow curve
- Uses affinity laws to extrapolate for different speeds

#### 2D maps

- Same type of curve as 1D map
- Multiple curves corresponding to different speeds
- Interpolates between curves to determine operation for different speeds

#### **Dimensionless maps**

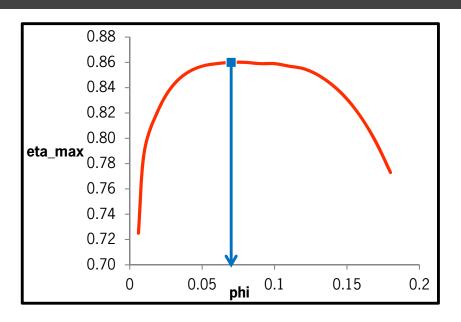
- Curve based on dimensionless flow  $(\phi)$  and head  $(\psi)$
- Contains same information as 2D maps

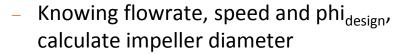
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# Compressor design

Design heuristics





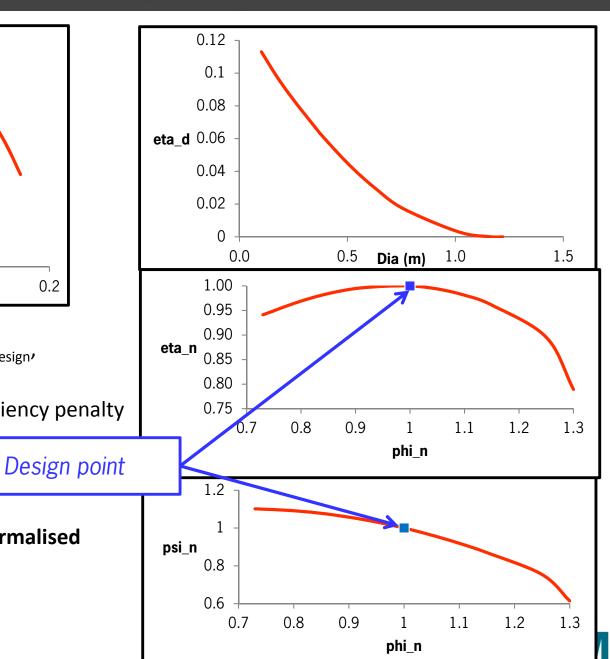


With the diameter, calculate efficiency penalty (eta<sub>d</sub>)

Calculate design eta

Calculate design psi

Using the design point and the normalised map, establish performance map



Performance vs Design mode

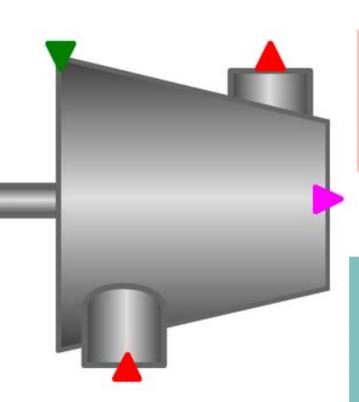


#### Design

- Inlet conditions
- Speed
- Design discharge pressure

#### Performance

- Inlet conditions
- Speed
- Design parameters
- Performance maps (1D or 2D)



#### Design

- Outlet conditions
- Power requirement
- Design parameters
- Performance maps

#### Performance

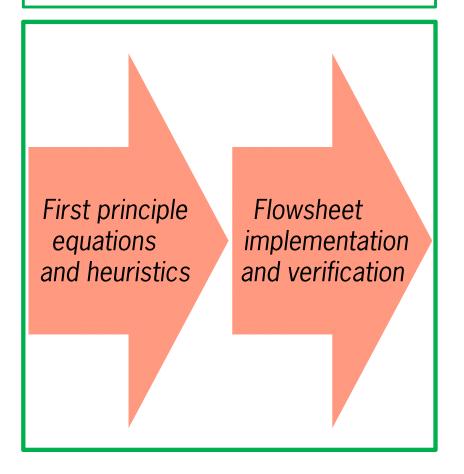
- Outlet conditions
- Power requirement



#### Overview



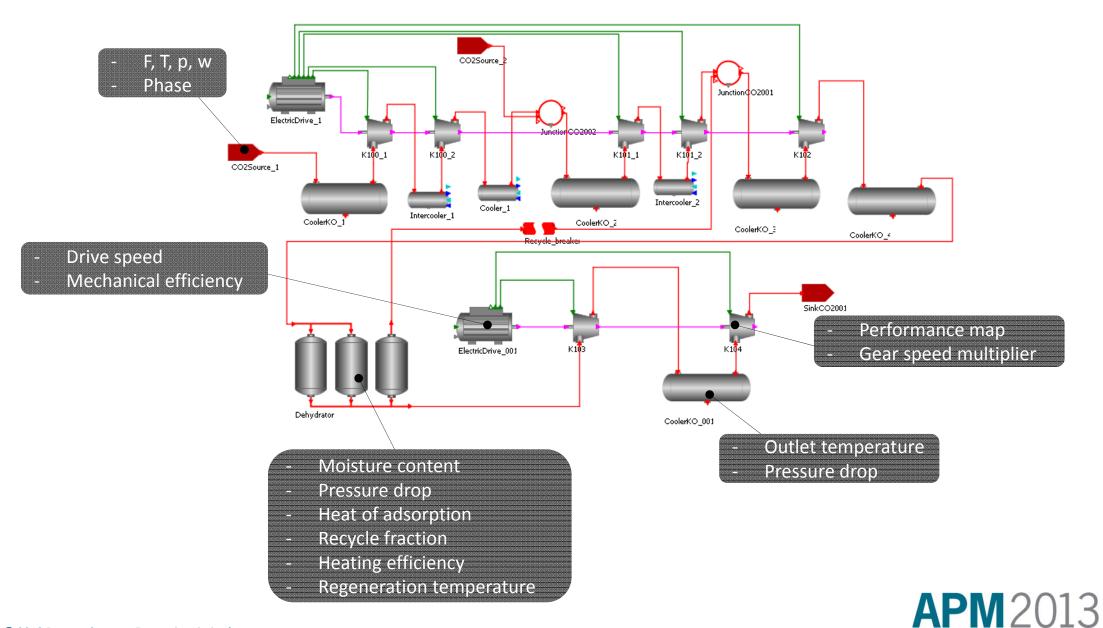
#### Model development



#### Model verification

**IEAGHG Case A0** 





#### Model verification





Ref: "International Energy Agency Greenhouse Gas" (IEA GHG) report (August, 2010)

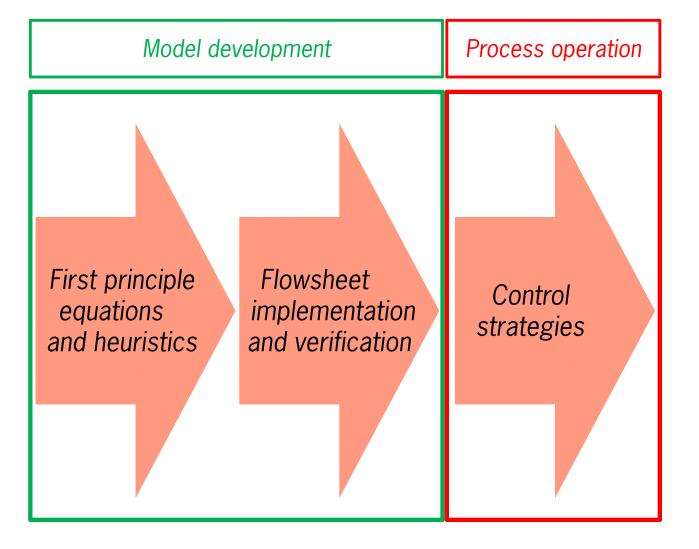
Сотопиологи	Discharge temperature (°C)				Discharge pressure (bar)				
Compressor	Report	gCCS	Deviation (%)		Report	gCCS	Deviation (%)		
K100 <sub>1</sub>	83.6	83.7		0.05		3.65	3.64		0.3
K100 <sub>2</sub>	45.7	45.7		0.1		5.00	4.98		0.4
K101 <sub>1</sub>	69.1	70.1		1.5		10.5	10.4		1.1
K101 <sub>2</sub>	68.3	68.5		0.4		18.8	18.5		1.4
K102	69.1	69.5		0.6		34.0	33.3		1.9
K103	90.1	88.4		1.9		70.0	69.9		0.2
K104	79.2	79.4		0.3		111.2	110.7		0.4

- Deviation between simulation results and data is lower than 2%.
- Good accuracy from all the compression system models.
- Accuracy condition needed for optimisation is satisfied.



# Overview

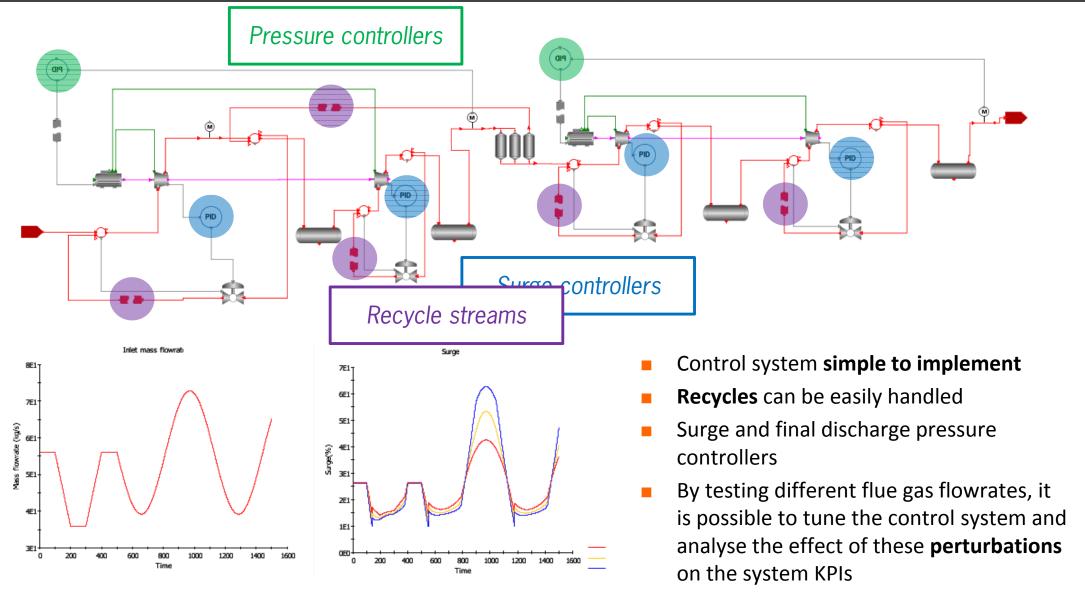




## Compressor train – control strategies

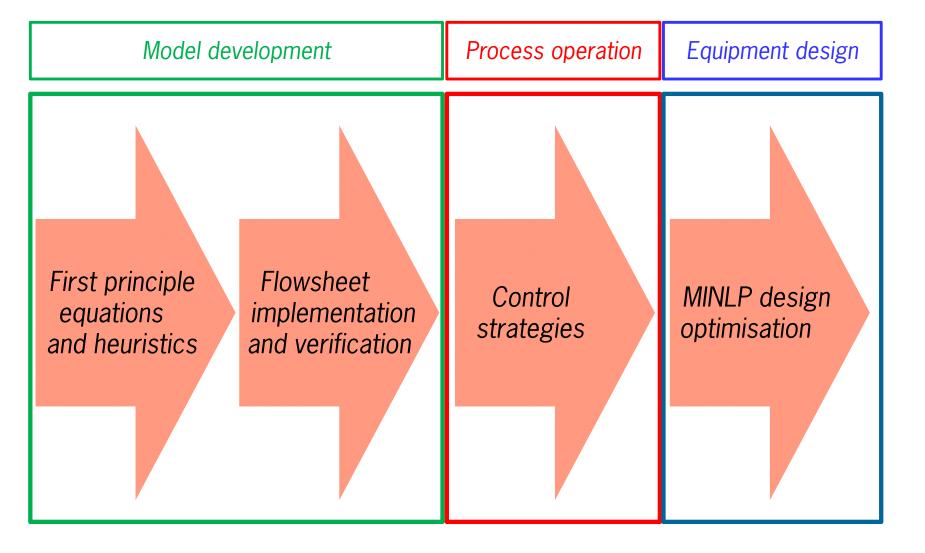
**IEAGHG Case B0** 





#### Overview





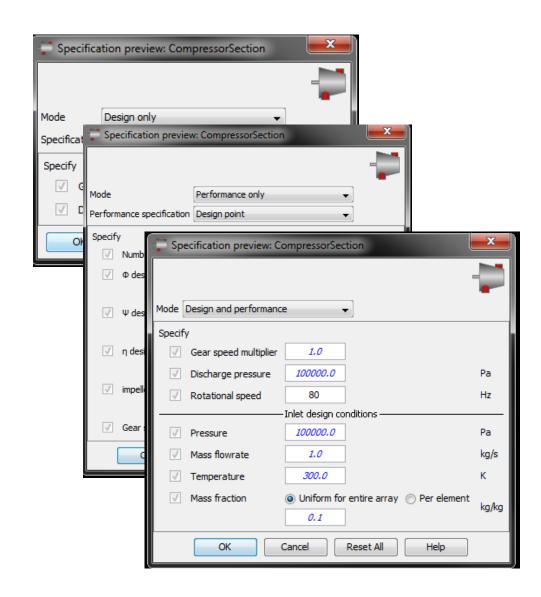
# Compressor train design - conventional

Design methodology



For a given train configuration,

- First, design the compressor for a specified discharge pressure, where the inlet conditions come from upstream equipment.
- Then, run a simulation in performance mode introducing the diameter and design point calculated in the previous design.
- The user can skip the first step by using design/performance mode by giving the design conditions while operating at off-design.





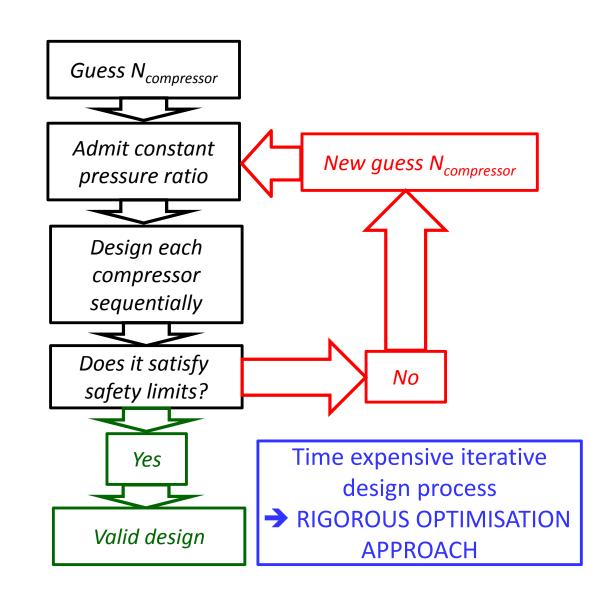
# Compressor train design - conventional

Design methodology



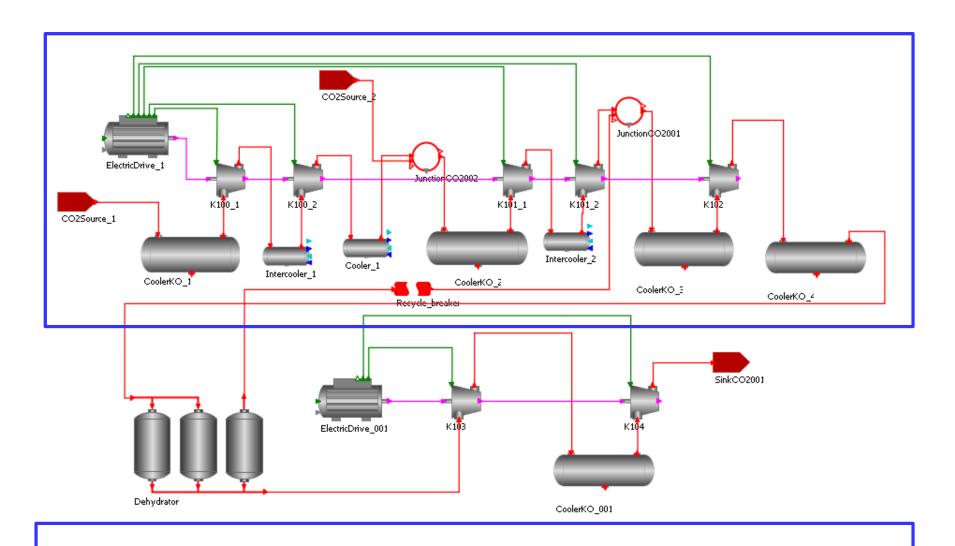
For a given train configuration,

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Concept





Here focus on optimising the "first half" of the train (before dehydration)

Problem description (Based on Case A0 from the IEA GHG report)



#### **Objective: Minimize total cost**

- CAPEX (Peters & Timmerhaus)
  - Compressors
  - Coolers
  - Electric Drive
  - Instrumentation and control
  - Project
  - Spare parts
- OPEX
  - Electricity
  - Cooling water
  - Maintenance
  - Interest

#### Degrees of freedom

- Number of compressor sections
- Pressure ratio of each compressor

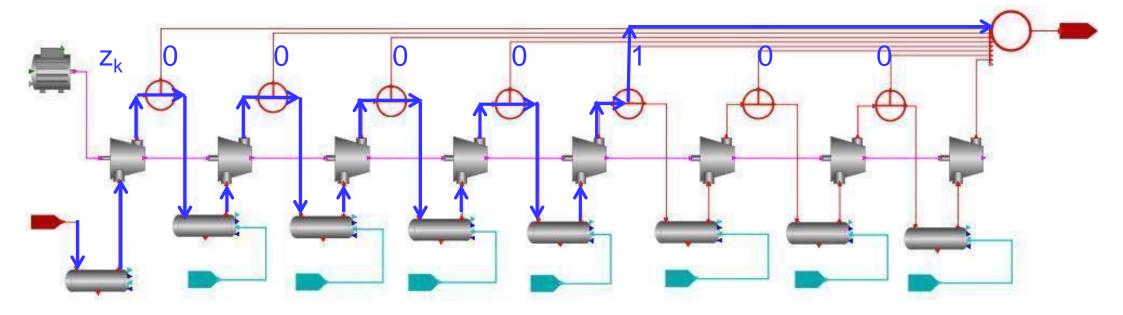
#### Constraints

 Final discharge pressure specification



Superstructure



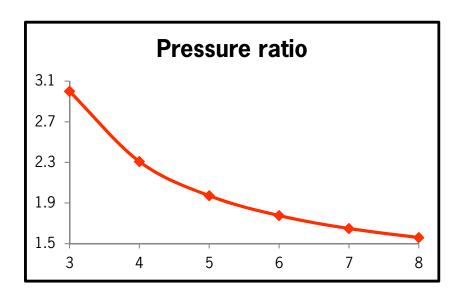


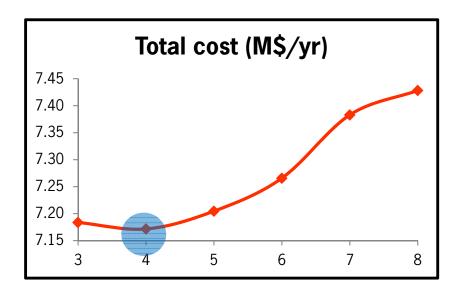
- Binary "flip variables" Z<sub>k</sub>
  - $Z_k$  determines whether compressor k is included or bypassed
  - e.g.  $Z_5 = 1 \rightarrow 5$  compressors in train
- Number of coolers = Number of compressors
- By-passed compressors and coolers have zero cost

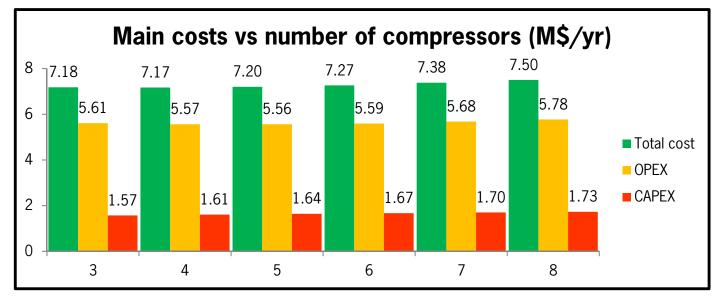


Total cost, CAPEX and OPEX





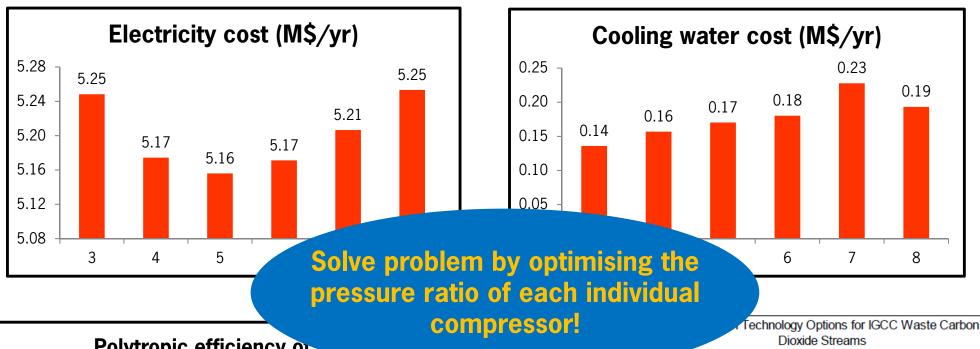


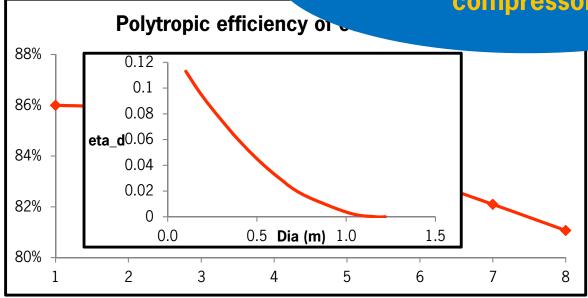


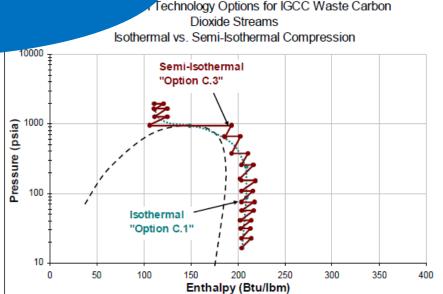


Operating cost, efficiency



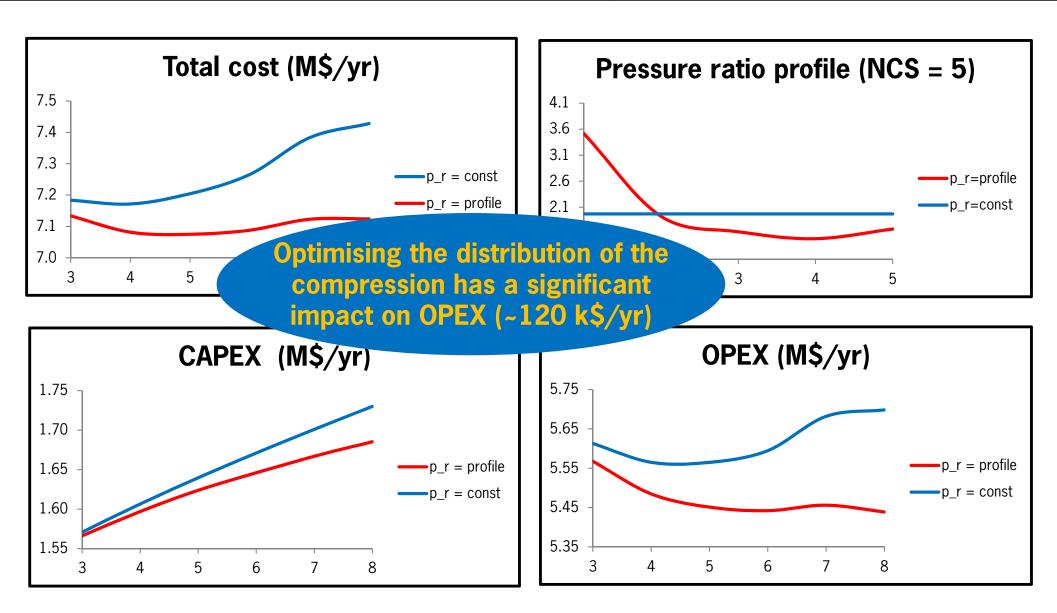






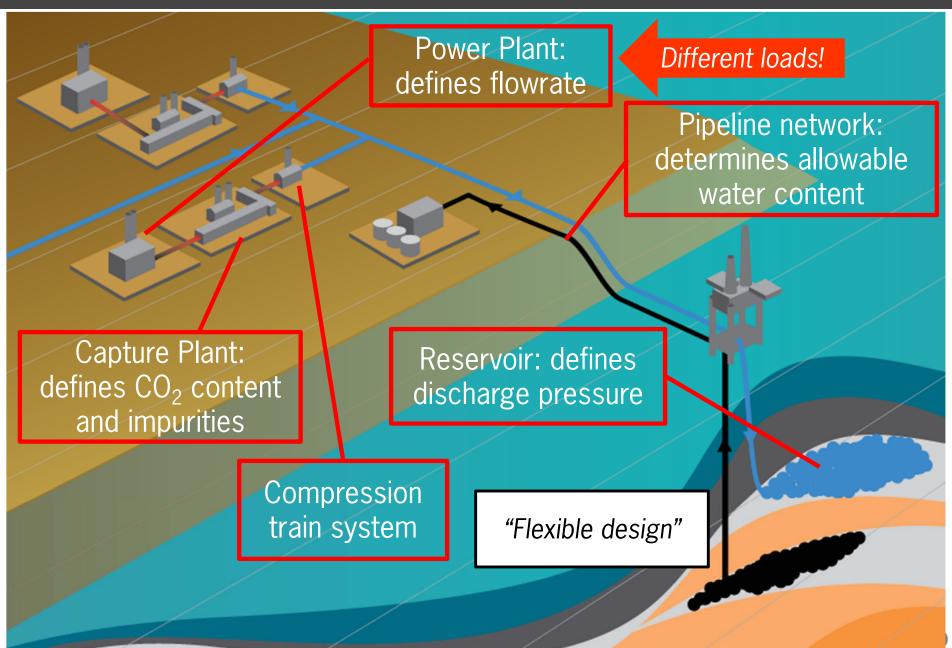
New formulation





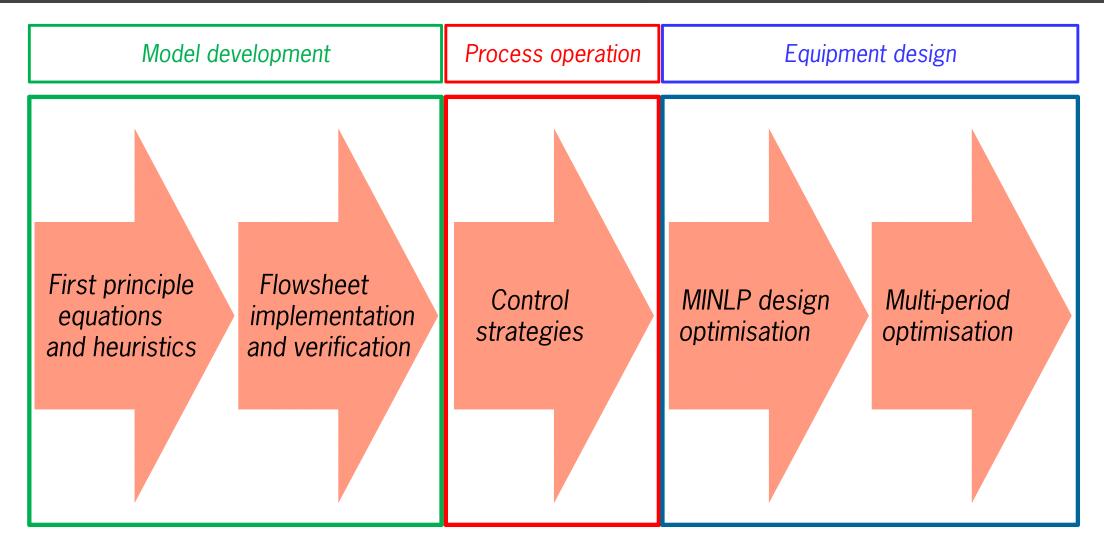
CCS chain





#### Overview





Design flexibility



#### OPEX stability

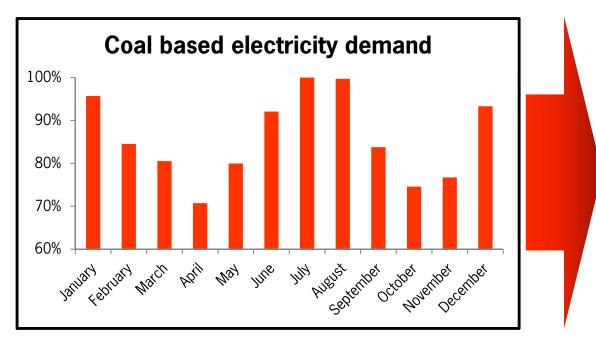
- Compressor efficiency greatly decreases when operating in "off-design" conditions
- Major increment of OPEX
- Important if the compression train operates in "off-design" conditions for a significant amount of time

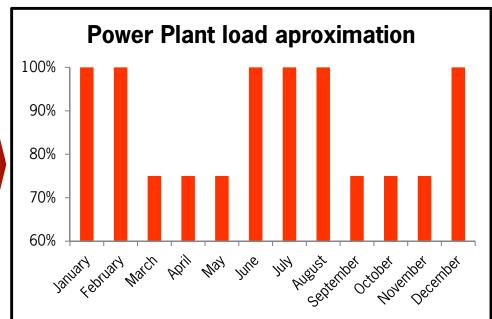
#### Safety limits

- Discharge temperature limit determined by materials of construction
- Electric drive can only operate within a certain range of speeds
  - range may not be sufficient to maintain desired discharge pressure
- Above issues are already known at the design stage
  - → Avoid relying on control system or safety procedures for resolving them
- Design system to operate over set of anticipated scenarios
  - Scenario probabilities taken into account in determining expected value of OPEX in objective function

Scenarios







\*U.S. Energy Information Administration (EIA)

Total cost =  $CAPEX_{100\%} + 0.5*OPEX_{100\%} + 0.5*OPEX_{75\%}$ 

- Power plant load changes during the year
  - Electricity demand fluctuations
  - Optimising design for only 100% load might not be the best approach
- Two scenarios (100% load and 75% load) with equal probability were taken into account in the multi-period design optimisation



**Formulation** 



#### Decision variables

- Number of compressors
- Pressure ratio of each individual compressor
- Speed of drive in "off-design" scenario

# Safety limits (for both scenarios)

- Maximum discharge temperature
- Minimum surge margin
- Final discharge pressure specification



Results



	Previous train	New train	△ (%)
Load	100%	75%	-
N <sub>compressor</sub>	5	5	-
Nu <sub>100%</sub> (Hz)	80	80	-
Nu <sub>75%</sub> (Hz)	76.6	76.2	-0.5%
C <sub>cap</sub> (M\$/yr)	0.85	0.86	0.5%
C <sub>ope</sub> (M\$/yr)	1.78	1.80	1.3%
C <sub>tot</sub> (M\$/yr)	2.63	2.66	1.0%

	Pressure ratio				
Compressor	1	2	3	4	5
Previous train	3.33	1.88	1.56	1.53	1.87
New train	4.05	1.89	1.61	1.33	1.75

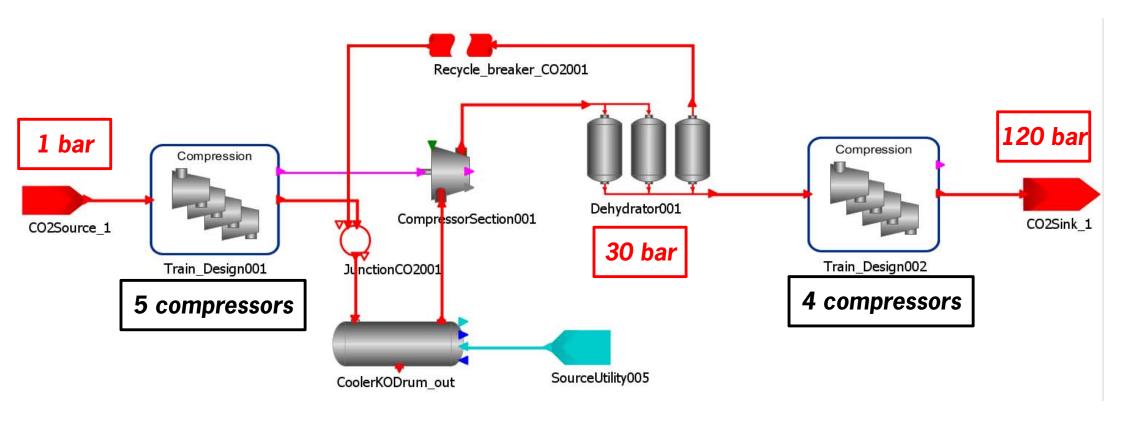
	Surge (%)					
Compressor	1	2	3	4	5	
Previous traip	8.1	8.3	8.4	8.3	8.4	
New train	10	10.3	10.7	11.4	12	

- New train design is 1% more expensive than previous design
  - due to the surge lower limit constraint (10% minimum)
- HOWEVER, previous train design doesn't satisfy all operational constraints for the "off-design" scenario
- The train work balance changed, compressing more in the first 3 compressor due to the efficiency penalty in the "off-design" scenario
- Significantly increase in processflexibility with a small cost penalty

# Full train optimisation

Results – IEA GHG Case AO





9 compressors

$$C_{cap} = 16.4 \text{ M}$$
\$

#### Conclusions

#### Summary



- Rigorous compressor model
  - Performance maps (1D, 2D and dimensionless)
  - Design heuristics
- Compression train simulation
  - Model verification (steady state)
  - Control system implementation
- Rigorous multi-period mixed-integer optimisation
  - Design the train considering a set of anticipated scenarios
  - Minimises total cost (CAPEX + OPEX)
  - Ensures all operational constraints are met under all scenarios
- Techno-economical decisions based on a rigorous design modelling tool
- Applicable to any range of conditions and gases (CO<sub>2</sub>, LNG, etc.)



# Acknowledgements



This work was carried out as part of a £3m project led by PSE and commissioned and cofunded by the Energy Technologies Institute (ETI) and project participants E.ON, EDF, Rolls-Royce, Petrofac (via subsidiary CO2DeepStore), PSE and E4tech.













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Thank you!



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