

INDUSTRIAL ROBOTICS

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3 - KINEMATIK

Objectives of the chapter

- We want:
 - Calculate where a robot moves when we set certain joint angles (forward transformation, forward kinematics)
 - Calculate how we need to adjust joint angles to reach a certain position (backward transformation, inverse kinematics)

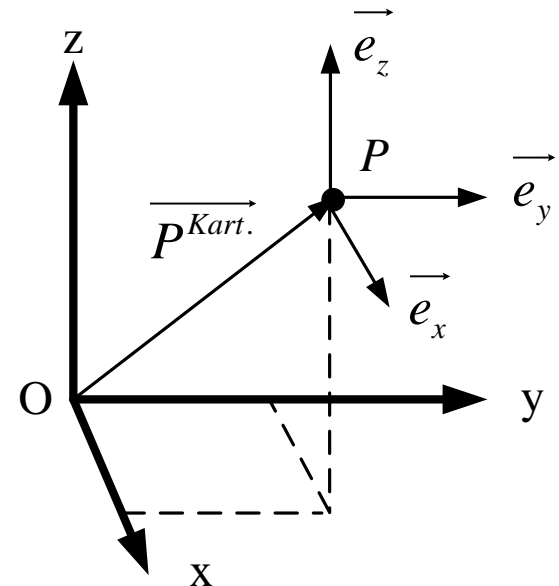


Contents of the lecture

- Structure
 - Coordinate systems
 - Reference systems
 - Transformations between reference systems
 - The Denavit-Hartenberg process
 - Inverse Kinematics / Backward Transformation
 -

Coordinate systems

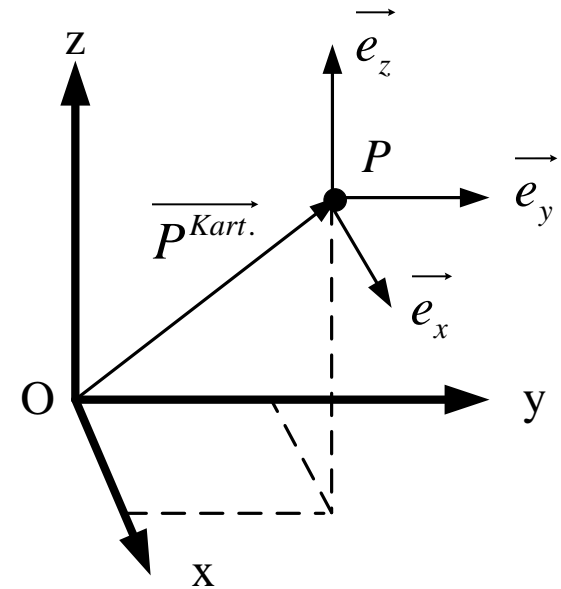
- Origin
 - Reference point to which the coordinates refer
 - Coordinates there take the value 0
- Unit vectors
 - Vectors of length 1 tangential to the coordinate axes
 - n vectors for n-dimensional KS
- Vectors
 - Linear combination of unit vectors



$$\overrightarrow{P^{Kart.}} = \begin{pmatrix} x \\ y \\ z \end{pmatrix} = x\overrightarrow{e_x} + y\overrightarrow{e_y} + z\overrightarrow{e_z}$$

Koordinatensysteme

- Cartesian coordinate system

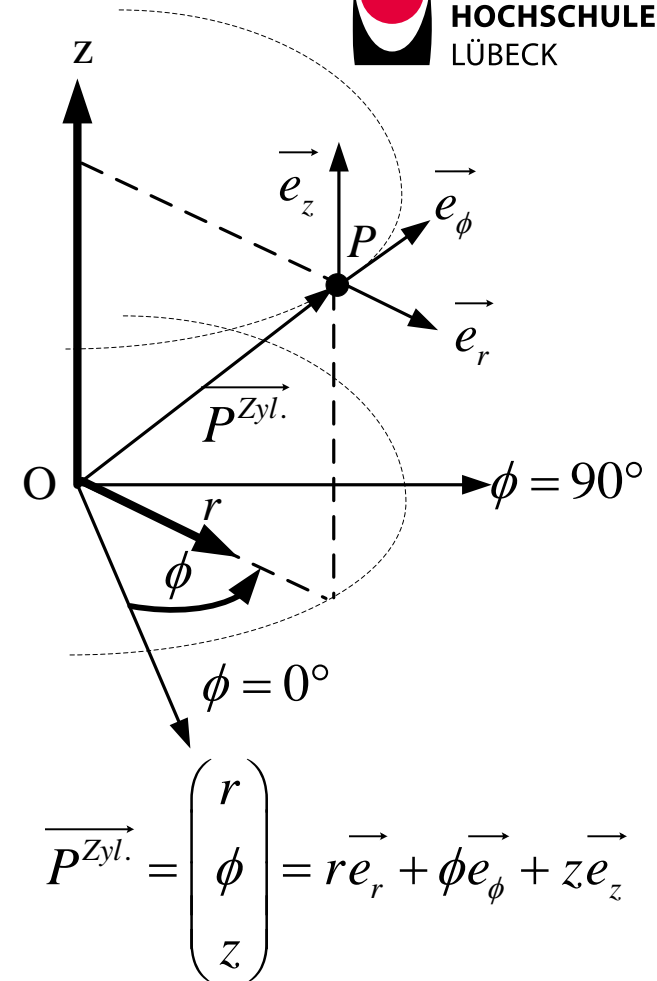
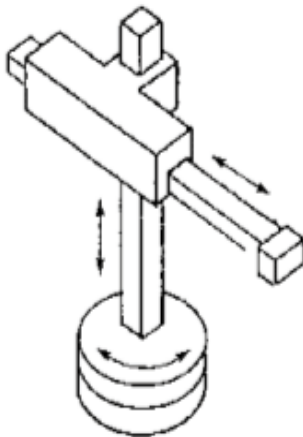


$$\overrightarrow{P^{Kart.}} = \begin{pmatrix} x \\ y \\ z \end{pmatrix} = x\overrightarrow{e_x} + y\overrightarrow{e_y} + z\overrightarrow{e_z}$$

CS	Dist.	Angles	Unit vectors	coord.
Cartesian	3	0	$\overrightarrow{e_x}, \overrightarrow{e_y}, \overrightarrow{e_z}$	x, y, z

Coordinate systems

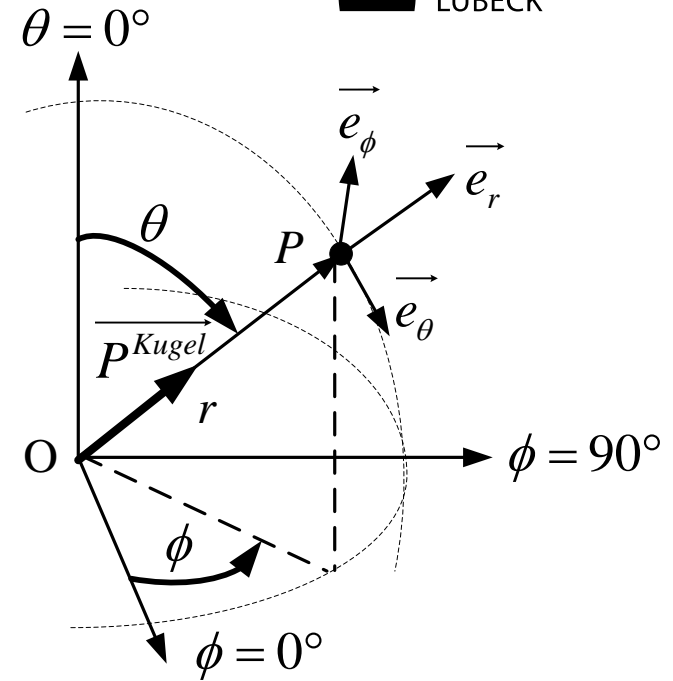
- Cylinder coordinate system



CS	Dist.	Angles	Unit vectors	coord.
Cylinder	2	1	$\overrightarrow{e_r}, \overrightarrow{e_\phi}, \overrightarrow{e_z}$	r, Φ, z

Coordinate systems

- Spherical Coordinate System



$$\vec{P}^{Kugel} = \begin{pmatrix} r \\ \phi \\ \theta \end{pmatrix} = r\vec{e}_r + \phi\vec{e}_\phi + \theta\vec{e}_\theta$$

CS	Dist.	Angles	Unit vectors	coord.
spheric al	1	2	$\vec{e}_r, \vec{e}_\phi, \vec{e}_\theta$	r, Φ, θ

Reference systems

- Common reference coordinates in robotics

- World coordinates**

- Firmly connected to the surroundings

- Base coordinates of the robot**

- Hand flange coordinates**

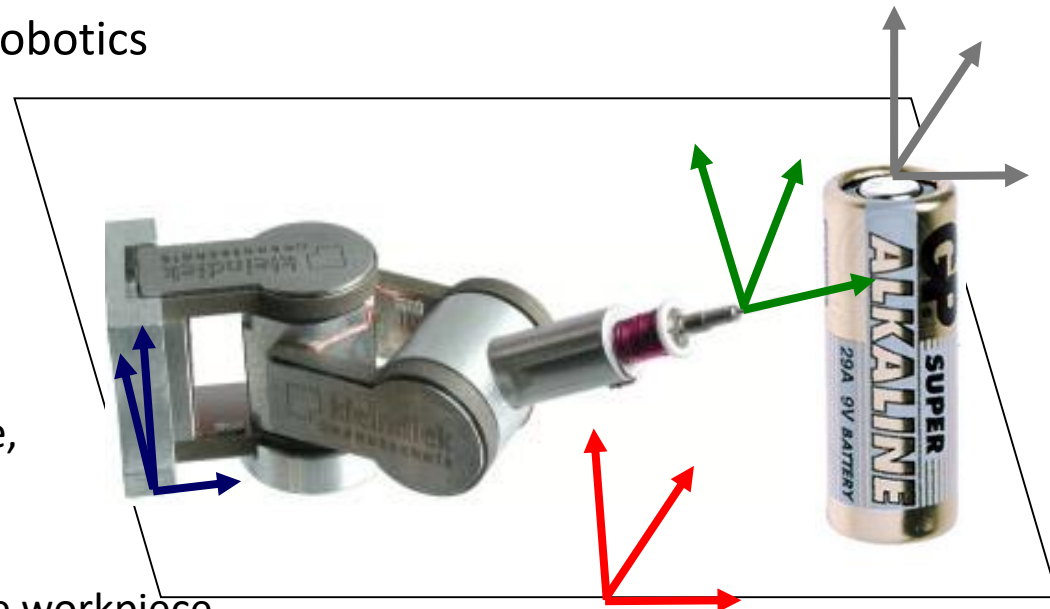
(Tool Connector Point, TCP)

- connected to the hand flange,
 - are also moved

- Workpiece coordinates**

- Coordinates connected to the workpiece
 - Workpiece and thus also its CS can be movable!

- Convention: When working with coordinates and systems, always specify the reference system, e.g.:



$$\overrightarrow{P^{TCP}}, \overrightarrow{P^{Welt}}, \overrightarrow{P^{WST}}$$

Transformations between reference systems

- Transformations between reference Coordinate systems

- How can a location in the workpiece KS be converted into base coordinates?

- Transformation consists of:

- Translation:

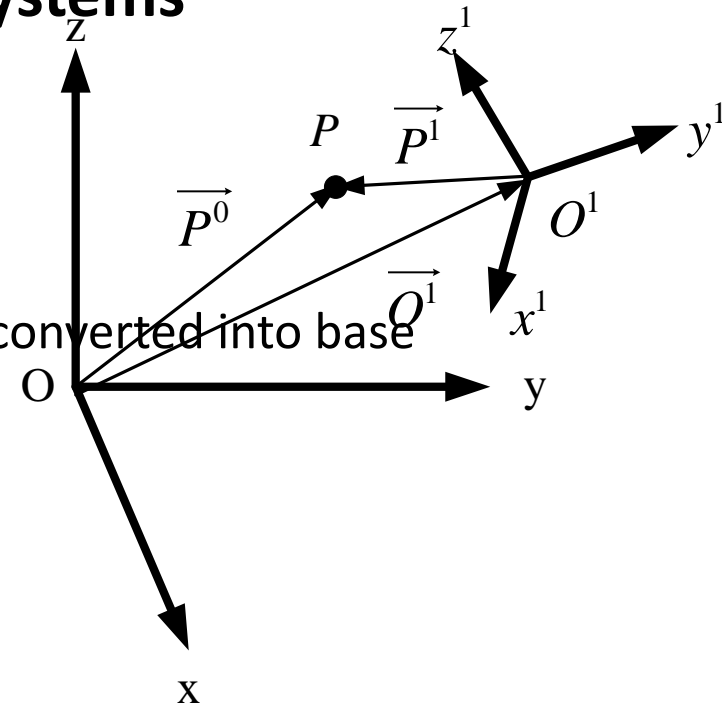
- Shift of KS 1 compared to KS 0
- Description by a vector

- Rotation

- Rotation of the CS 1 compared to the CS 0
- Description by a rotation matrix

- Goal:

Development of a transformation matrix that combines translation and rotation.



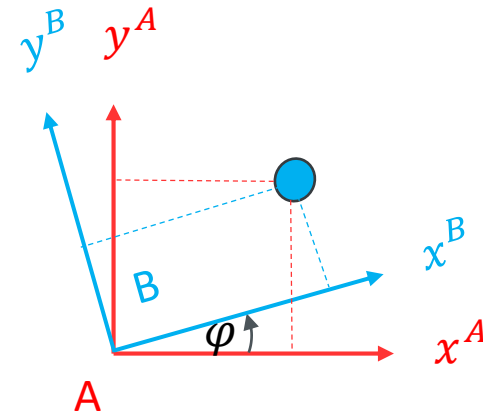
$$\overrightarrow{P^0} = \overrightarrow{O^1} + \mathbf{R}_1^0 \overrightarrow{P^1}$$

Transformations between reference systems

- 2D rotation
 - The transformation of a CS rotated by the angle ϕ can be represented by a simple 2 x 2 rotation matrix:
 - This allows a point P^B to be transferred to CS A:

$$T_B^A = R(\varphi) = \begin{pmatrix} \cos \varphi & -\sin \varphi \\ \sin \varphi & \cos \varphi \end{pmatrix}$$

$$p^A = T_B^A p^B = \begin{pmatrix} \cos \varphi & -\sin \varphi \\ \sin \varphi & \cos \varphi \end{pmatrix} \begin{pmatrix} x_P^B \\ y_P^B \end{pmatrix}$$



Transformations between reference systems

- 2D rotation
 - Reverse transformation from CS A to CS B:

$$T_A^B = R(\varphi)^T = \begin{pmatrix} \cos \varphi & \sin \varphi \\ -\sin \varphi & \cos \varphi \end{pmatrix} \quad p^B = T_A^B p^A = \begin{pmatrix} \cos \varphi & \sin \varphi \\ -\sin \varphi & \cos \varphi \end{pmatrix} \begin{pmatrix} x_P^A \\ y_P^A \end{pmatrix}$$

- The rotation matrices $R(\varphi)^T$ and $R(\varphi)$ are orthonormal to each other, thus:

$$R(\varphi)^T R(\varphi) = I = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}$$

- The determinant is 1.

Transformations between reference systems

- 3D rotation around an elementary axis
 - Similar to 2D rotation, the 3D rotation matrices result in simple rotations (elementary rotations)
 - Rotation around the x-axis:

$$T_B^A = R(x, \alpha) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \alpha & -\sin \alpha \\ 0 & \sin \alpha & \cos \alpha \end{pmatrix}$$

-

- Rotation around the y-axis:

$$T_B^A = R(y, \beta) = \begin{pmatrix} \cos \beta & 0 & \sin \beta \\ 0 & 1 & 0 \\ -\sin \beta & 0 & \cos \beta \end{pmatrix}$$

-

- Rotation around the z-axis:

-

$$T_B^A = R(z, \theta) = \begin{pmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Transformations between reference systems

- 3D rotation around any axis

- Rotation matrix

-

$$T_B^A = R(x, \alpha) = \begin{pmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{pmatrix}$$

- Coordinate transformation of a point p from KS B to KS A:

-

$$p^A = T_B^A p^B = \begin{pmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{pmatrix} \begin{pmatrix} x_P^B \\ y_P^B \\ z_P^B \end{pmatrix}$$

- Back transformation:

-

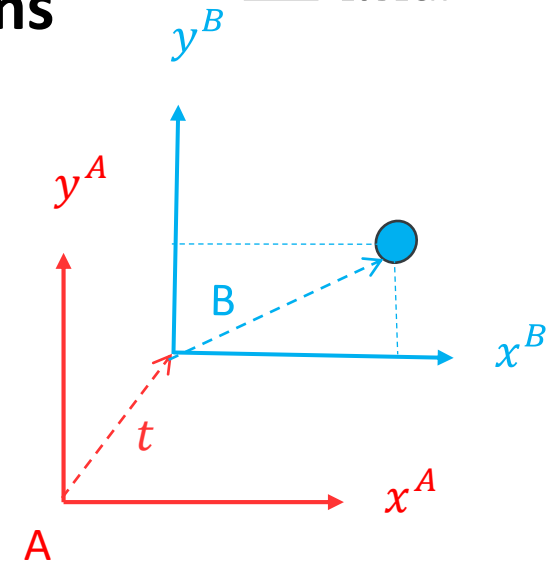
$$p^B = T_B^{A^T} p^A = T_A^B p^A$$

Transformations between reference systems

- Translation of coordinate systems
 - The translation corresponds to a simple addition of the displacement vector t :

$$p^A = p^B + t$$

-
- Problem:
 - Rotation transformation is achieved by matrix multiplication
 - Translation transformation is achieved by vector addition
 - requires several arithmetic operations
 - Reverse transformation is time-consuming to calculate
- Solution: Use of homogeneous coordinates for the closed calculation of transformations
-



Transformations between reference systems

- Homogeneous 3D translation
 - Approach: Another "virtual" coordinate is added to the matrices
 - Example: 2D Translation

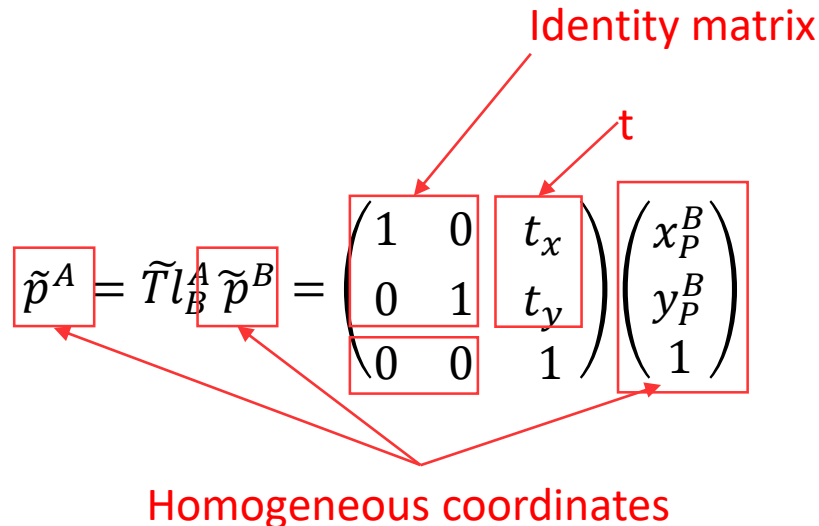
$$\dot{p}^A = p^B + t = \begin{pmatrix} x_P^B \\ y_P^B \end{pmatrix} + \begin{pmatrix} t_x \\ t_y \end{pmatrix} \longrightarrow \tilde{p}^A = \tilde{T}l_B^A \tilde{p}^B = \begin{pmatrix} 1 & 0 & t_x \\ 0 & 1 & t_y \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_P^B \\ y_P^B \\ 1 \end{pmatrix}$$

Identity matrix

t

$$\tilde{p}^A = \tilde{T}l_B^A \tilde{p}^B = \begin{pmatrix} 1 & 0 & t_x \\ 0 & 1 & t_y \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} x_P^B \\ y_P^B \\ 1 \end{pmatrix}$$

Homogeneous coordinates



The diagram illustrates the components of the homogeneous transformation matrix. Red arrows point from the text labels to specific parts of the matrix equation: 'Identity matrix' points to the top-left 2x2 submatrix, 't' points to the translation vector in the third column, and 'Homogeneous coordinates' points to the bottom row of the matrix and the homogeneous coordinate '1' in the vector.

Transformations between reference systems

- Homogeneous 3D translation

- General wording for translation (3D)
- $$\begin{pmatrix} p^A \\ 1 \end{pmatrix} = \begin{pmatrix} I_{3 \times 3} & t \\ 0_{1 \times 3} & 1 \end{pmatrix} \begin{pmatrix} p^B \\ 1 \end{pmatrix}$$

- Homogeneous coordinates
-

$$\tilde{p}^A = \begin{pmatrix} I_{3 \times 3} & t \\ 0_{1 \times 3} & 1 \end{pmatrix} \tilde{p}^B$$

- Translation matrix with the translation vector in homogeneous coordinates:
-

$$\tilde{T}l(t) = \begin{pmatrix} I_{3 \times 3} & t \\ 0_{1 \times 3} & 1 \end{pmatrix}$$

Transformations between reference systems

- Homogeneous 3D rotation
 - Approach: the translation vector is zero, the unit matrix is replaced by the rotation matrix.

$$\tilde{R} = \begin{pmatrix} R & 0_{3 \times 1} \\ 0_{1 \times 3} & 1 \end{pmatrix}$$

-
- Rotation with homogeneous coordinates:
-

$$\begin{pmatrix} p^A \\ 1 \end{pmatrix} = \begin{pmatrix} R & 0_{3 \times 1} \\ 0_{1 \times 3} & 1 \end{pmatrix} \begin{pmatrix} p^B \\ 1 \end{pmatrix} = \begin{pmatrix} R p^B \\ 1 \end{pmatrix}$$

$$\tilde{p}^A = \begin{pmatrix} R & 0_{3 \times 1} \\ 0_{1 \times 3} & 1 \end{pmatrix} \tilde{p}^B = \tilde{R} \tilde{p}^B$$

Transformations between reference systems

- Homogeneous 3D transformation
 - Concatenation of transformations – translation and rotation
 - Intermediate coordinate system KS* is created by shifting KS A around the vector t :

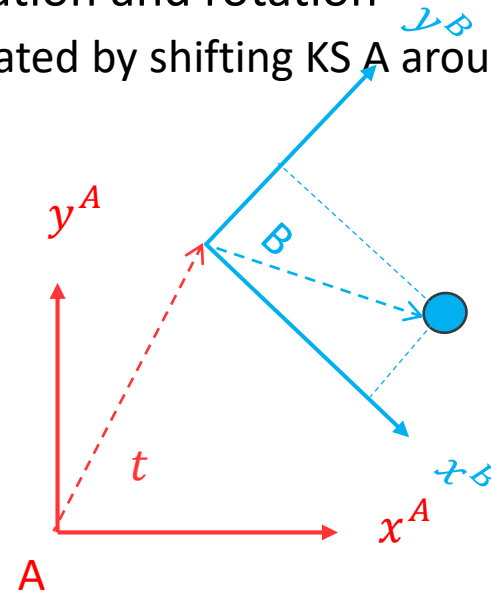
$$T_*^A = \tilde{T}l(t)$$

-
- By rotating the intermediate coordinate system KS* is created by KS B:

$$T_B^* = \tilde{R}$$

- This can be summarized to:

$$T_B^A = T_*^A T_B^* = \tilde{T}l(t)\tilde{R} = \begin{pmatrix} I_{3 \times 3} & t \\ 0_{1 \times 3} & 1 \end{pmatrix} \begin{pmatrix} R & 0_{3 \times 1} \\ 0_{1 \times 3} & 1 \end{pmatrix} = \begin{pmatrix} R & t \\ 0_{1 \times 3} & 1 \end{pmatrix}$$



Transformations between reference systems

- Homogeneous 3D Transformation Summary
 - Homogeneous transformation matrices have the form:

$$T = \begin{pmatrix} R & t \\ 0_{1 \times 3} & 1 \end{pmatrix}$$

- Inverse transformation matrix:

$$T^{-1} = \begin{pmatrix} R^T & -R^T t \\ 0_{1 \times 3} & 1 \end{pmatrix}$$

$$T T^{-1} = \begin{pmatrix} R & t \\ 0_{1 \times 3} & 1 \end{pmatrix} \begin{pmatrix} R^T & -R^T t \\ 0_{1 \times 3} & 1 \end{pmatrix} = \begin{pmatrix} I_{3 \times 3} & 0_{3 \times 1} \\ 0_{1 \times 3} & 1 \end{pmatrix} = I_{4 \times 4}$$

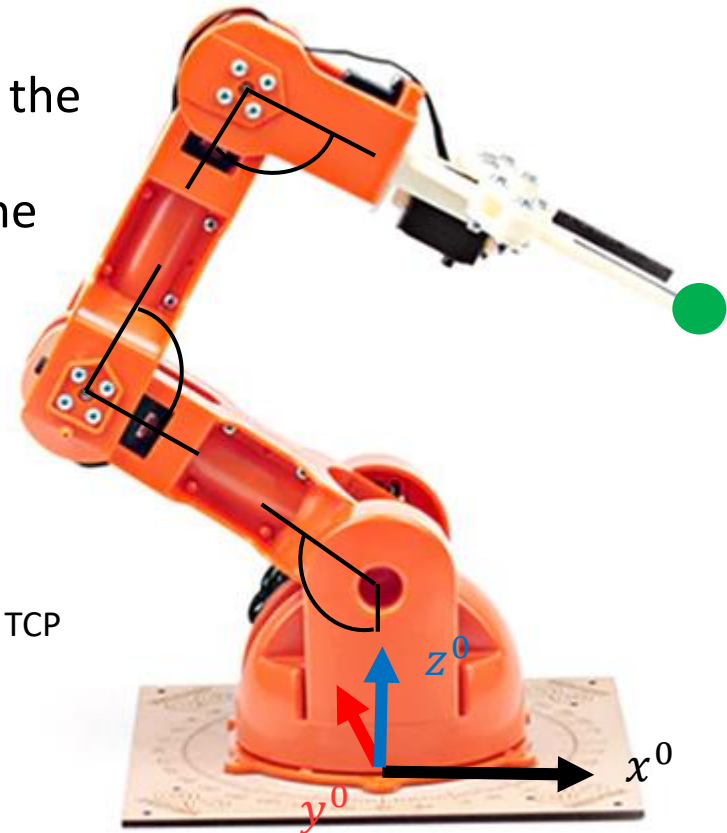
- Several transformations can be combined by multiplying the homogeneous transformation matrices.

This saves computing time in the robot controller!

- $$T_C^A = T_B^A T_A^B$$

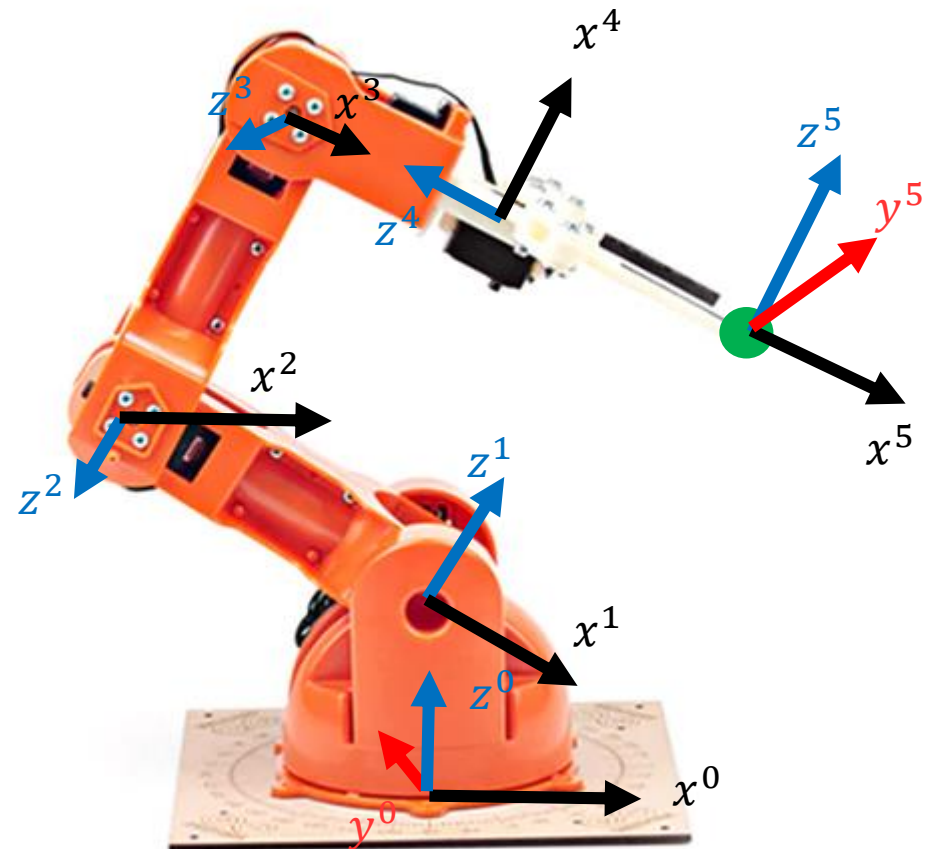
The Denavit-Hardenberg-Transformation

- Problem formulation:
We are looking for a method with which the position of the TCP in the base or world coordinate system can be calculated if the joint angles of the robot are known.
- This is called the so-called forward transformation or forward kinematics.
-
- Notes:
 - In the picture, the gripper tip is used instead of the TCP
 - The axes bear the CS number in the superscriptum
 -



The Denavit-Hartenberg-Transformation

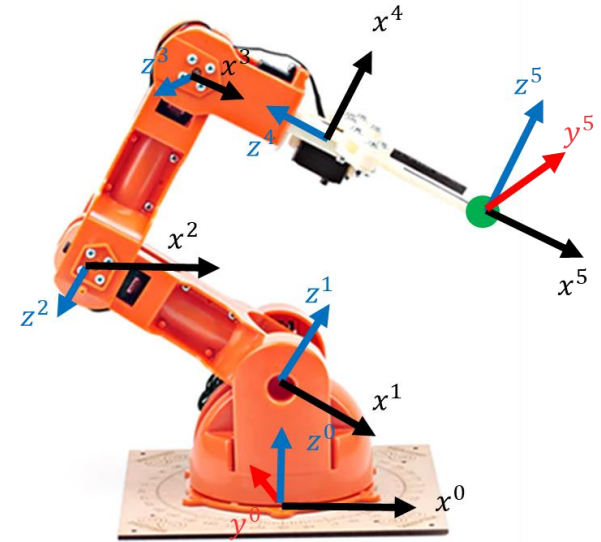
- Approach (I):
- Each joint is provided with its own coordinate system
 - Thus, each member has 2 coordinate systems
- Hint:
 - the basic coordinate system and the tcp coordinate system are usually predefined



The Denavit-Hartenberg-Transformation

- Approach (II):
 - For each member, the DH Transformation parameters are determined to transform from the i-th to the i-1-th joint:
 - Translation along the z-axis: d
 - Rotation around the z-axis: δ
 - Translation along the x-axis: a
 - Rotation around the x-axis: α
 - This gives the DH transformation matrix for one member:
 -

$$T_i^{i-1} = \tilde{T}l(z, d) * \tilde{R}(z, \delta) * \tilde{T}l(x, a) * \tilde{R}(x, \alpha)$$



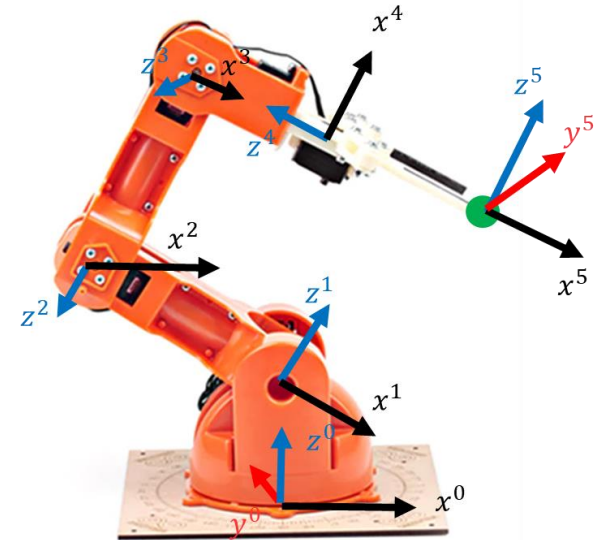
The Denavit-Hardenberg-Transformation

- Approach (III):
 - The DH Transformation Matrix:

$$T_i^{i-1} = \tilde{T}l(z, d) * \tilde{R}(z, \delta) * \tilde{T}l(x, a) * \tilde{R}(x, \alpha)$$

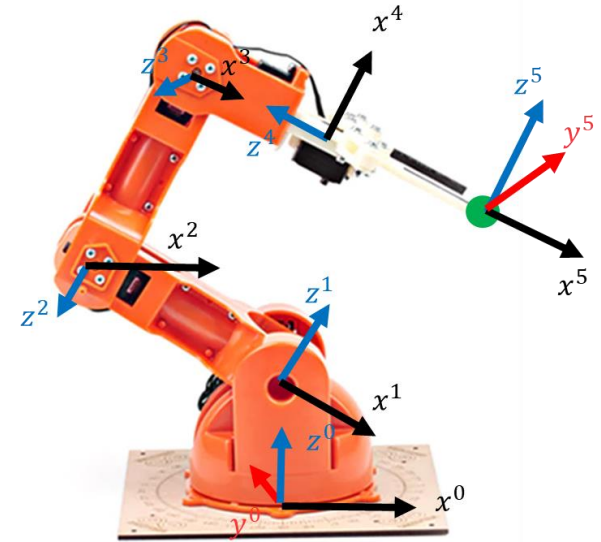
- Can be easily converted into the following form:

$$T_i^{i-1} = \begin{pmatrix} \cos \delta_i & -\sin \delta_i \cos \alpha_i & \sin \delta_i \sin \alpha_i & a_i \cos \delta_i \\ \sin \delta_i & \cos \delta_i \cos \alpha_i & -\cos \delta_i \sin \alpha_i & a_i \sin \delta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{pmatrix}$$



The Denavit-Hartenberg-Transformation

- Approach (IV):
 - In total, there are four DH parameters per CS: a_i , α_i , d_i und δ_i
 - Two of the four DH parameters are always constants: a_i , α_i
 - Only one of the other parameters d_i and δ_i is a variable, this depends on the type of movement at the joint i:
 - Translation: d_i variable and δ_i constant
 - Rotation: d_i constant und δ_i variable
- This is the result of the DH analysis:
List of individual parameters in a table:



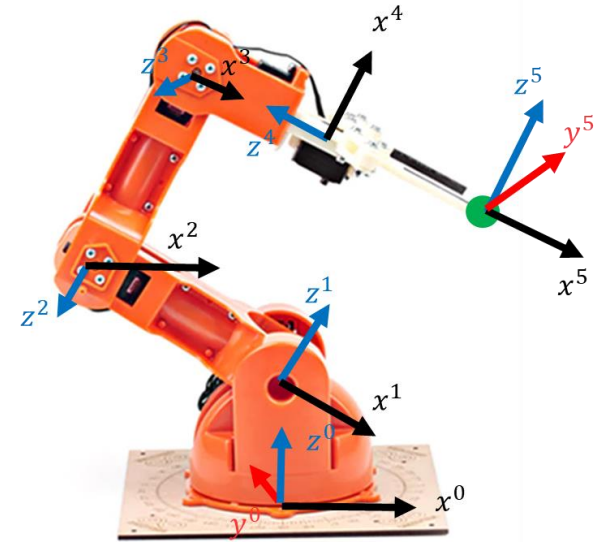
Glied	d_i	δ_i	a_i	α_i
1
2
3
4
5

The Denavit-Hartenberg-Transformation

- Approach (V):
 - The multiplication of the transformation matrices results in the overall transformation rule:

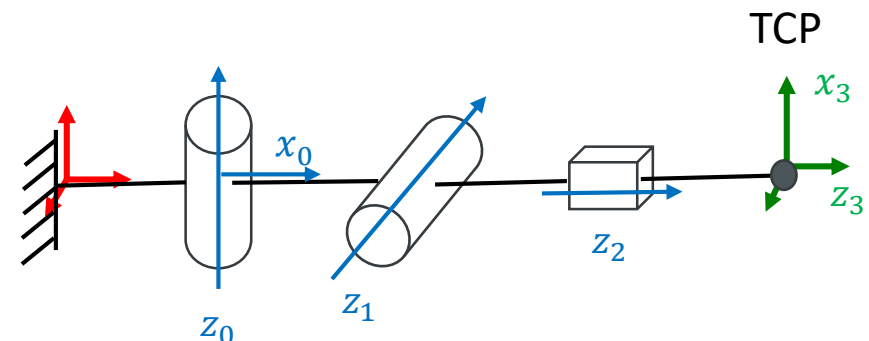
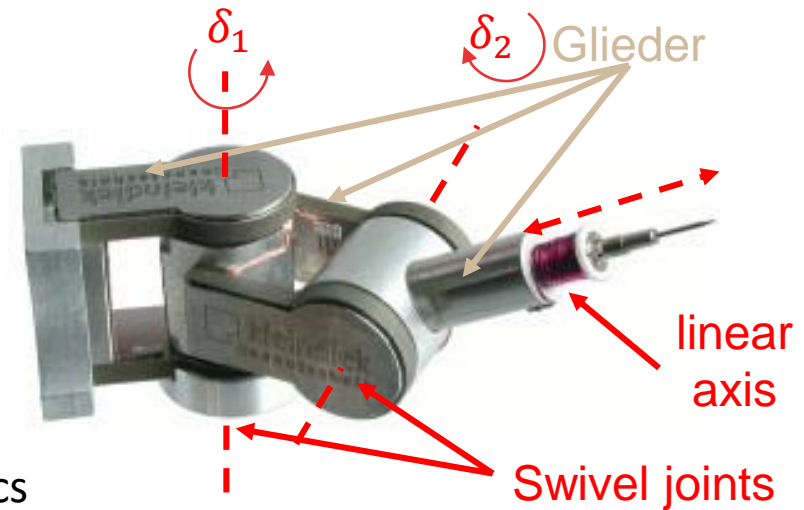
$$\begin{pmatrix} x^0 \\ y^0 \\ z^0 \\ 1 \end{pmatrix} = T_1^0 * T_2^1 * ... * T_n^{n-1} * \begin{pmatrix} x^n \\ y^n \\ z^n \\ 1 \end{pmatrix}$$

- Dies ist die:
 - Forward transformation or
 - Forward kinematics
 - The DH parameters are also required for backward transformation / inverse kinematics.



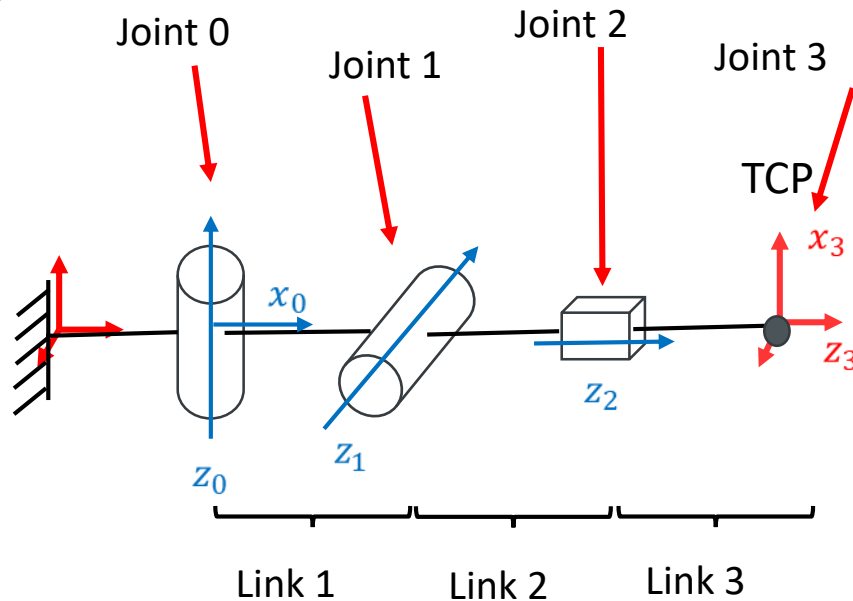
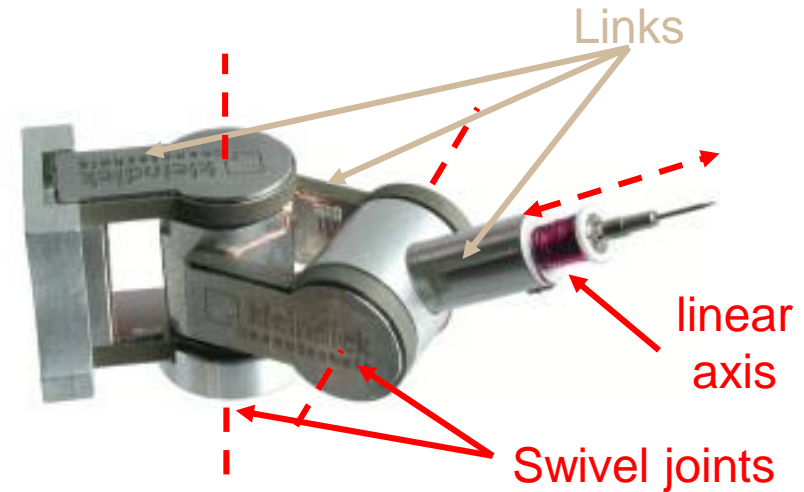
The Denavit-Hartenberg-Transformation

- The DH Process – Step 1
- Analysis of the kinematic chain
 - Links are represented by strokes and by joints (T/R) together connected.
 - If necessary, "straighten" the kinematics
 -
- Each joint has its own coordinate system
 - Z-axis points in the direction of positive movement/rotation
 - X-axis will be set later (if not specified)
 - Y-axis can be omitted!



The Denavit-Hartenberg-Transformation

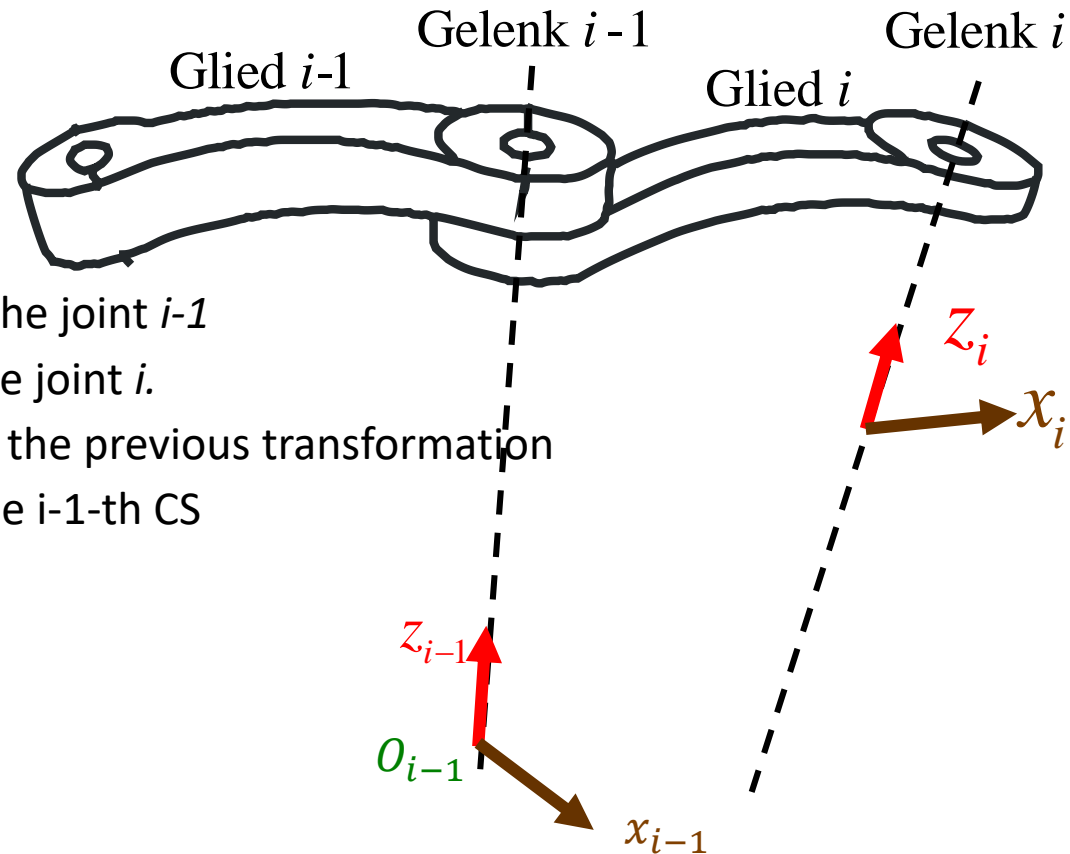
- The DH Process – Step 1
 - Benennung der Gelenke und Glieder
 - Red World KS is not taken into account here
 - Enter angles and distances if necessary



The Denavit-Hartenberg-Transformation

• The DH Process – Step 2

- Naming of the links and joints:
- On the link i are the joints $i-1$ and i
-
- The axis \mathbf{z}_{i-1} lies on the axis of the joint $i-1$
- The axis \mathbf{z}_i lies on the axis of the joint i .
- The axis \mathbf{x}_{i-1} is determined by the previous transformation
- Thus also the origin \mathbf{O}_{i-1} of the $i-1$ -th CS
-
- The position of the axis \mathbf{x}_i is determined in the next step.

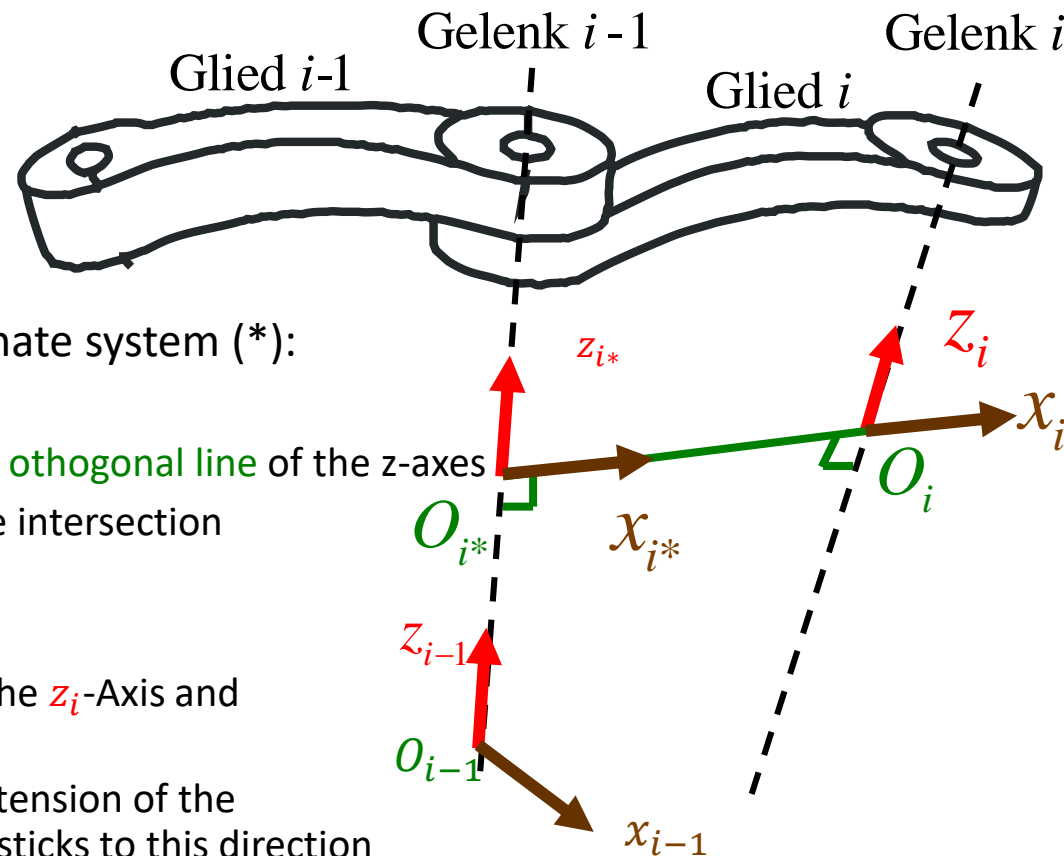


The Denavit-Hartenberg-Transformation

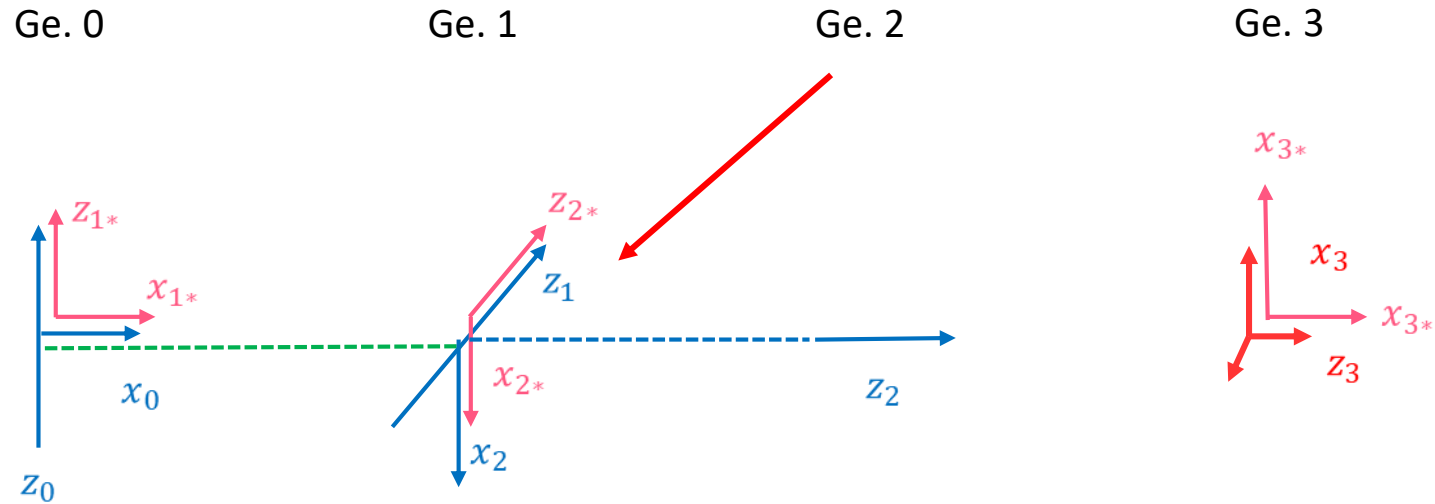
• The DH Process – Step 2

Definition of coordinate systems:

- The axes \mathbf{x}_i and \mathbf{x}_{i*} lie on the **common orthogonal line** of axes \mathbf{z}_{i-1} and \mathbf{z}_i .
- Specifying the auxiliary coordinate system (*):
 - \mathbf{z}_{i*} is located on the \mathbf{z}_{i-1} -axis
 - \mathbf{x}_{i*} is located on the **common orthogonal line** of the z-axes
 - The origin of KS \mathbf{O}_{i*} lies at the intersection of \mathbf{z}_{i*} and \mathbf{x}_{i*}
- Definition of the i-th CS:
 - \mathbf{O}_i lies at the intersection of the \mathbf{z}_i -Axis and the **common orthogonal line**
 - The axis \mathbf{x}_i is based on the extension of the **common orthogonal line** and sticks to this direction



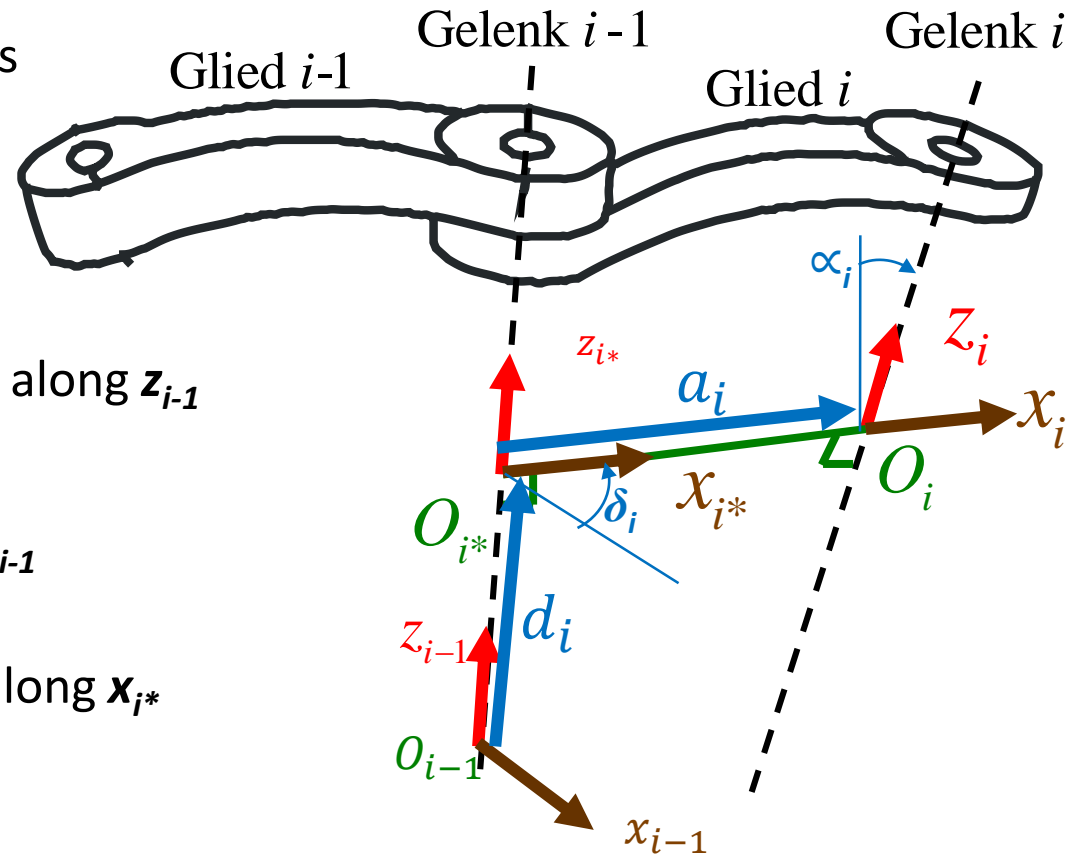
The Denavit-Hartenberg-Transformation



- The DH Process – Step 2
Definition of coordinate systems:
 - Origin of joint 2 migrates to the origin of joint 1 (special case)
 -

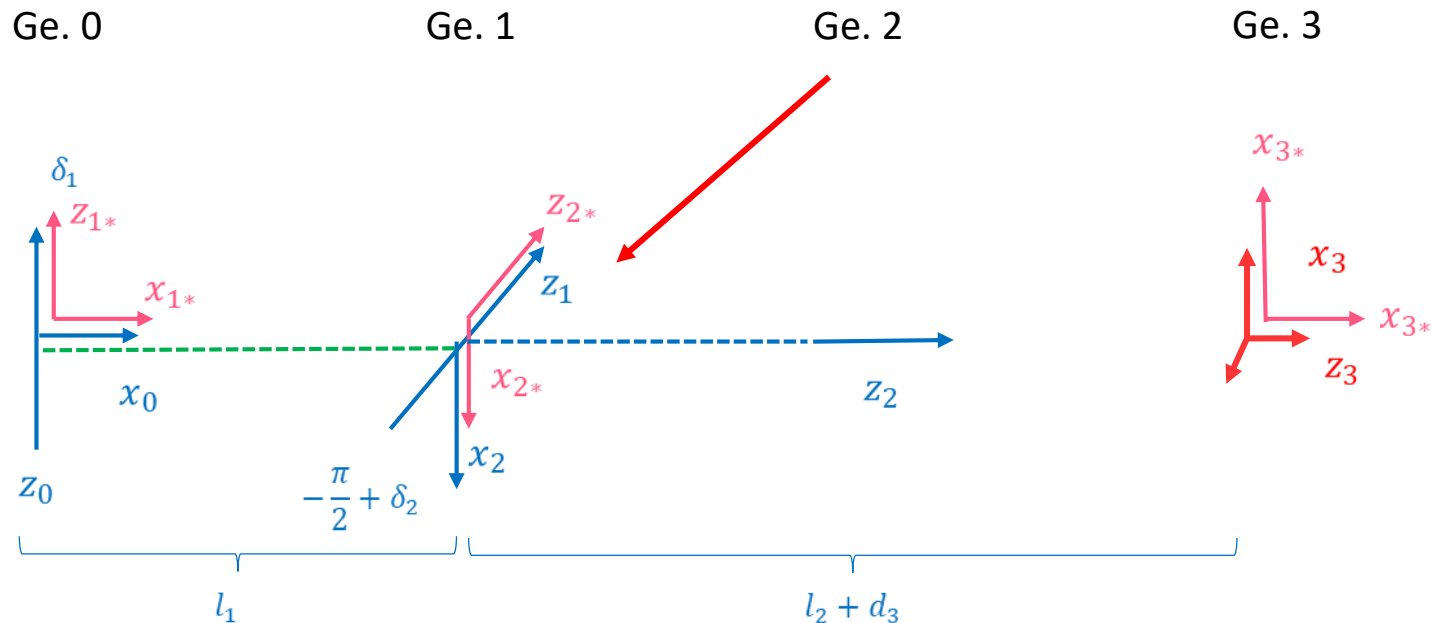
The Denavit-Hartenberg-Transformation

- The DH Process – Step 3
Determination of DH parameters



- d_i : Distance from O_{i-1} to O_{i*} along z_{i-1}
- δ_i : Angle of x_{i-1} to x_{i*} over z_{i-1}
- a_i : Distance from O_{i*} to O_i along x_{i*}
- α_i : Angle of z_{i*} to z_i over x_i

The Denavit-Hartenberg-Transformation



- The DH Process – Step 3
Determination of DH parameters:

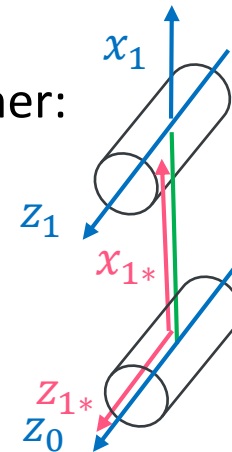
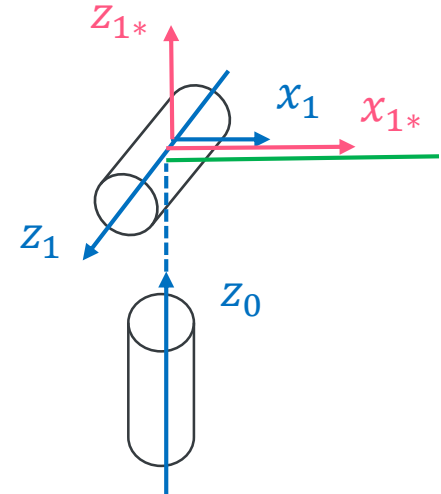
Glied	d_i	δ_i	a_i	α_i
1	0	δ_1	l_1	$-\pi/2$
2	0	$+\pi/2 + \delta_2$	0	$+\pi/2$
3	$l_2 + d_3$	0	0	0

The Denavit-Hartenberg-Transformation

- The DH Process – Step 2

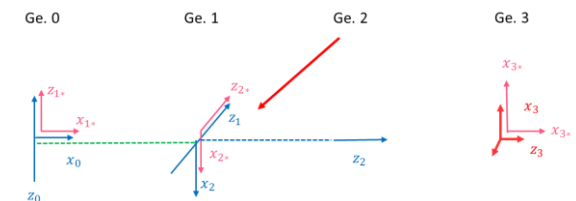
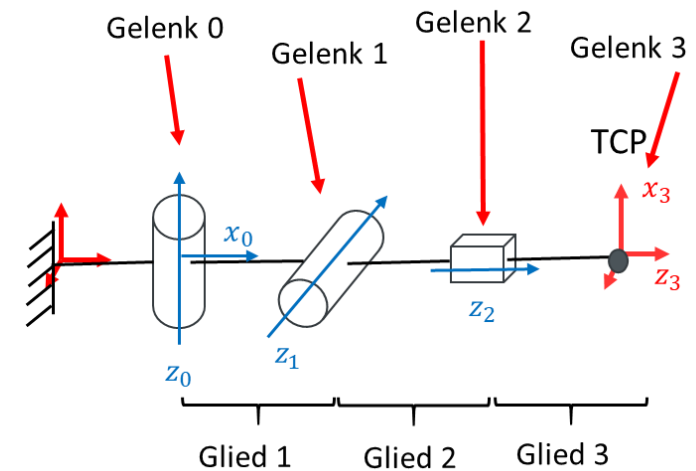
Definition of coordinate systems: special cases

- orthogonal z-axes
-
- Parallel z-axes
- Extreme case: parallel z-axes lying on top of each other:
 - O_1 Suitably chosen
 - O_{1*} ins neue Koordinatensystem O_1



The Denavit-Hartenberg-Transformation

- Summary:
 - Step 1: Sketch with links, joints and z-axes
 - Step 2: Definition of the (help) coordinate systems in another sketch
 - Step 3: Determination of DH parameters, summary in a table
 - Now the transformation matrix can be set up.



$$T_3^0 = T_1^0(\delta_1) * T_2^1(\delta_2) * T_3^2(d_3)$$

Glied	d_i	δ_i	a_i	α_i
1	0	δ_1	l_1	$-\pi/2$
2	0	$+\pi/2 + \delta_2$	0	$+\pi/2$
3	$l_2 + d_3$	0	0	0

The Denavit-Hartenberg-Transformation

Direct kinematics / forward kinematics:

- clearly defined (for open chains)
- to calculate analytically with the help of matrices

$$\begin{pmatrix} x \\ y \\ z \\ 1 \end{pmatrix}^{Welt} = T_0^{Welt} \cdot T_3^0(\delta_1, \delta_2, d_3) \cdot T_{Wzg}^3 \cdot \begin{pmatrix} x \\ y \\ z \\ 1 \end{pmatrix}^{TCP}$$

Indirect kinematics / backward kinematics:

- non-linear system of equations → closed solutions are not always possible
- Multiple solutions may be possible
- There can be an infinite number of solutions (e.g. redundant kinematics)
- There can be no acceptable solutions
- therefore:
 - Introduction of boundary conditions
 - possibly numerical solutions

Inverse Kinematics / Backward Transformation

- Initial problem: Inverse kinematics explained using the example:



- Mathematically speaking:
 - We are looking for the "Tool Configuration Vector" w in base coordinates, which is composed of the desired position p and the orientation R of the TCP.
 - The transfer function f depends on the joint variables q of the robot.

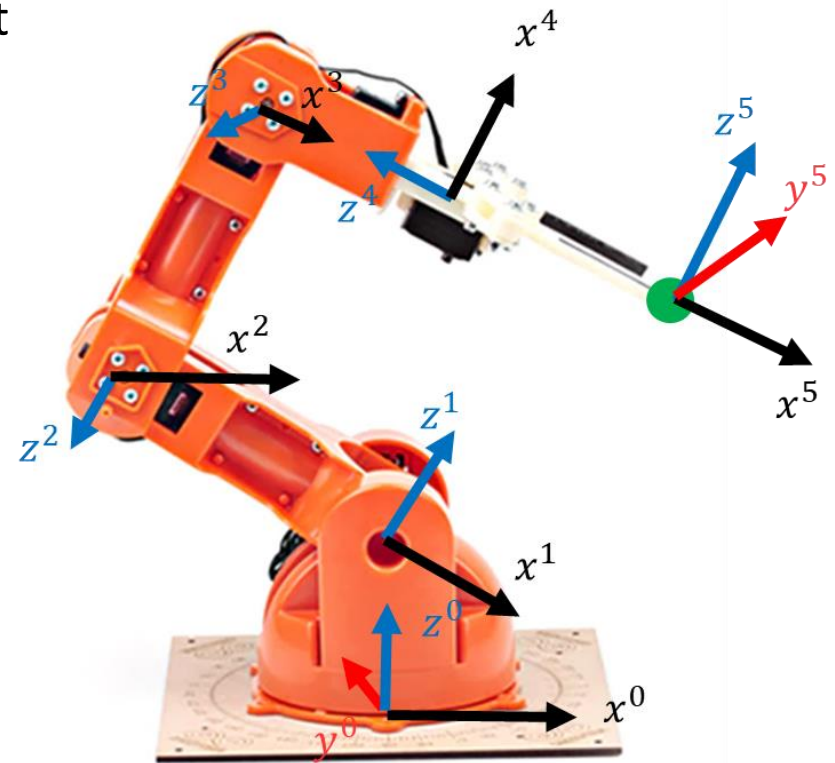
$$w(q) = f(q_1, q_2, \dots, q_n) = f(\theta_1, \theta_2, \dots, \theta_n) = \begin{pmatrix} p \\ R \end{pmatrix}$$

Inverse Kinematics / Backward Transformation

- General approach backward transformation
- If there is a spherical wrist, then the wrist orientation R and the target position p can be calculated back to wrist position:

$$p^{wrist} = p - d * r^3$$

- d is the length of the tool
- r^3 is the approach vector
-



Inverse Kinematics / Backward Transformation

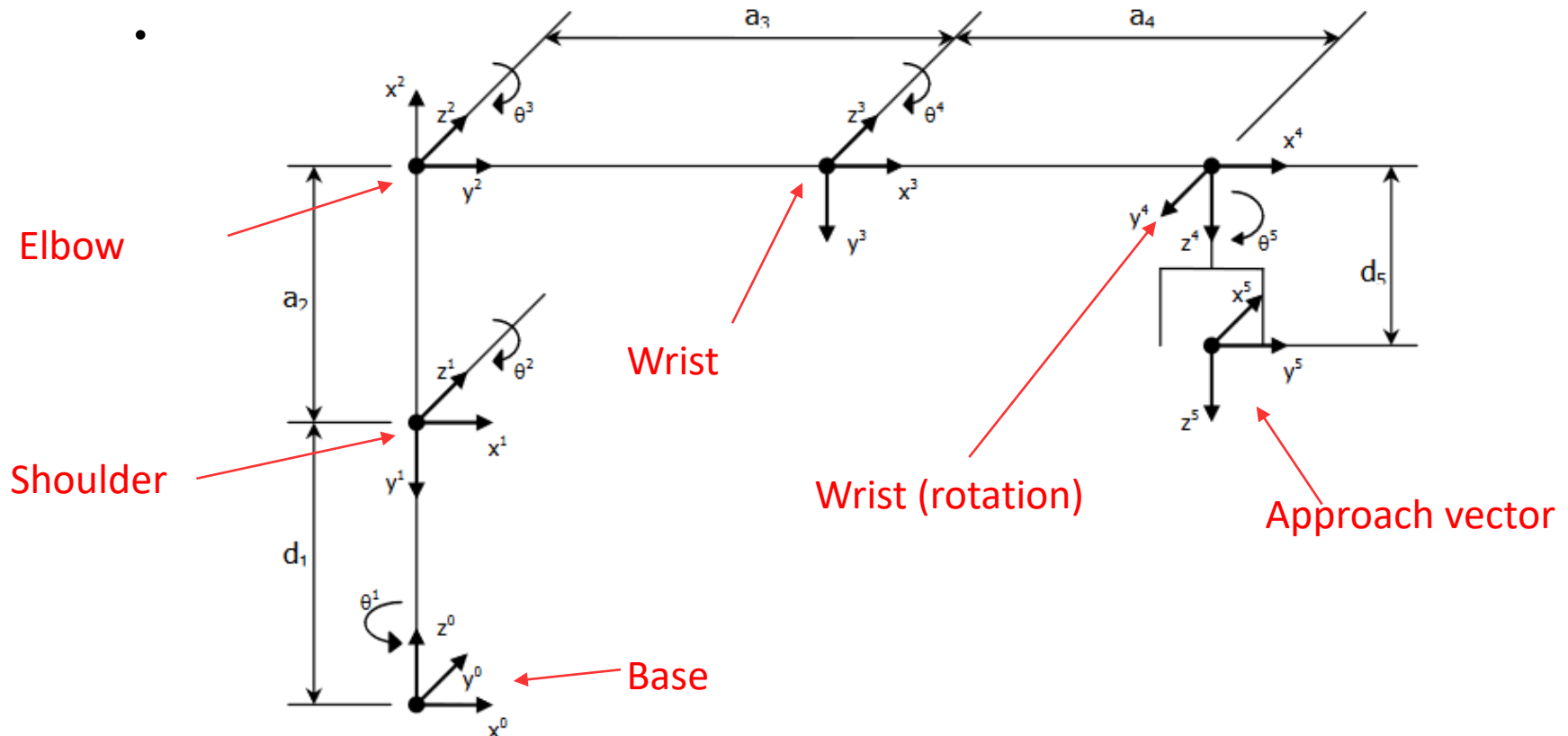
- Numerical approach backward transformation
 - Determination of the zeros of the expression:

$$f(\theta_1, \theta_2, \dots, \theta_n) - \begin{pmatrix} p \\ R \end{pmatrix} = 0$$

- Approach, e.g. by Newton method
-
- Contains the partial derivatives of the TCP coordinates according to the individual joint angles (Jakobi matrix)
-

Inverse Kinematics / Backward Transformation

- Reverse transformation 5-axis articulated arm (Schilling – Fundamentals of Robotics)
 - Kinematic model
 -



Inverse Kinematics / Backward Transformation

- Reverse transformation 5-axis articulated arm
- "Tool configuration vector" w :

$$w(q) = \begin{pmatrix} x \\ y \\ z \\ \text{Rot. around } x_0 \\ \text{Rot. around } y_0 \\ \text{Rot. around } z_0 \end{pmatrix}$$

Position of the gripper (here origin of KS 5)
related to KS 0

Approach vector

- Vector of joint variable q :

$$q = \begin{pmatrix} q_1 \\ q_2 \\ q_3 \\ q_4 \\ q_5 \end{pmatrix} = \begin{pmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \\ \theta_4 \\ \theta_5 \end{pmatrix}$$

Inverse Kinematics / Backward Transformation

- Reverse transformation 5-axis articulated arm (Schilling – Fundamentals of Robotics)
 - Determine the bases' rotation angle

$$q_1 = \text{atan2}(w_2, w_1)$$

- $\text{atan2}(y, x)$ function is the 4-quadrant variant for the arcus-tangent function (available in most programming languages, based on the sequence of x, y)

x-value	Quadrant	$\text{atan2}(y, x)$
$x > 0$	1, 4	$\text{atan}(y/x)$
$x = 0$	1, 4	$[\text{sgn}(y)] * \pi/2$
$x < 0$	2, 3	$\text{atan}(y/x) + [\text{sgn}(y)] * \pi$

Inverse Kinematics / Backward Transformation

- Reverse transformation 5-axis articulated arm (Schilling – Fundamentals of Robotics)
 - Calculation of elbow joint angle q_3
 - The total tool pitch angle corresponds to the given angle w_4

$$q_{234} = q_2 + q_3 + q_4 = w_4$$

$$q_{234} = \text{atan2}(-w_4 \cos q_1 - w_5 \sin q_1, -w_6)$$

- 2 intermediate variables are introduced:

$$b_1 = w_1 \cos q_1 + w_2 \sin q_1 - a_4 \cos q_{234} + d_5 \sin q_{234}$$

$$b_2 = d_1 - a_4 \sin q_{234} - d_5 \cos q_{234} - w_3$$

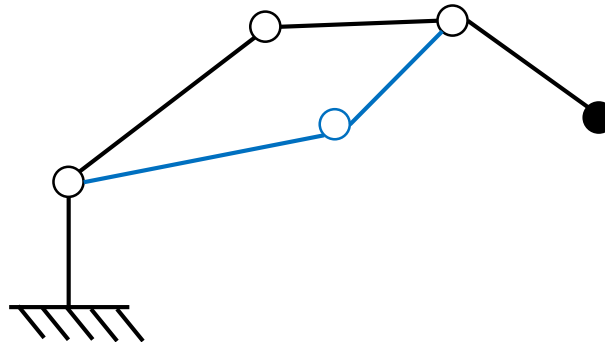
- From this, b^2 is calculated: $b^2 = b_1^2 + b_2^2$

Inverse Kinematics / Backward Transformation

- Reverse transformation 5-axis articulated arm (nach Schilling – Fundamentals of Robotics)
 - Calculation of elbow joint angle q_3
 - and from this the joint angle q_3 :

$$q_3 = \pm \arccos \frac{b^2 - a_2^2 - a_3^2}{2a_2 a_3}$$

- +/- takes into account the „elbow up“- and the „**elbow down**“-variant, respectively



Inverse Kinematics / Backward Transformation

- Reverse transformation 5-axis articulated arm (Schilling – Fundamentals of Robotics)
 - Calculation of the shoulder-joint angle q_2

$$q_2 = \text{atan}((a_2 + a_3 \cos q_3)b_2 - a_3 b_1 \sin q_3, (a_2 + a_3 \cos q_3)b_1 + a_3 b_2 \sin q_3)$$

- Tool pitch angle:

$$q_4 = q_{234} - q_2 - q_3$$

-

- Tool roll angle q_5 :

$$q_5 = \pi \ln(\sqrt{w_4^2 + w_5^2 + w_6^2})$$

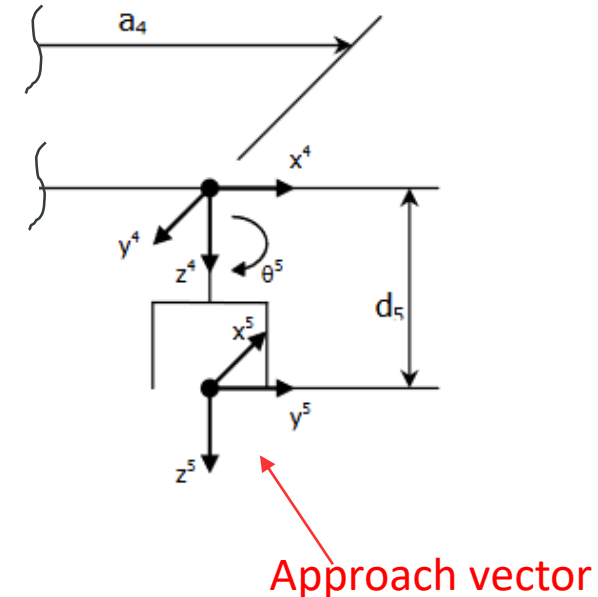
Inverse Kinematics / Backward Transformation

- for the 5-axis articulated robot, the approach vector has to be given in the form:

$$w = \begin{pmatrix} w_p \\ w_o \end{pmatrix} \begin{pmatrix} p \\ \exp\left(\frac{q_n}{\pi}\right) r_3 \end{pmatrix}$$

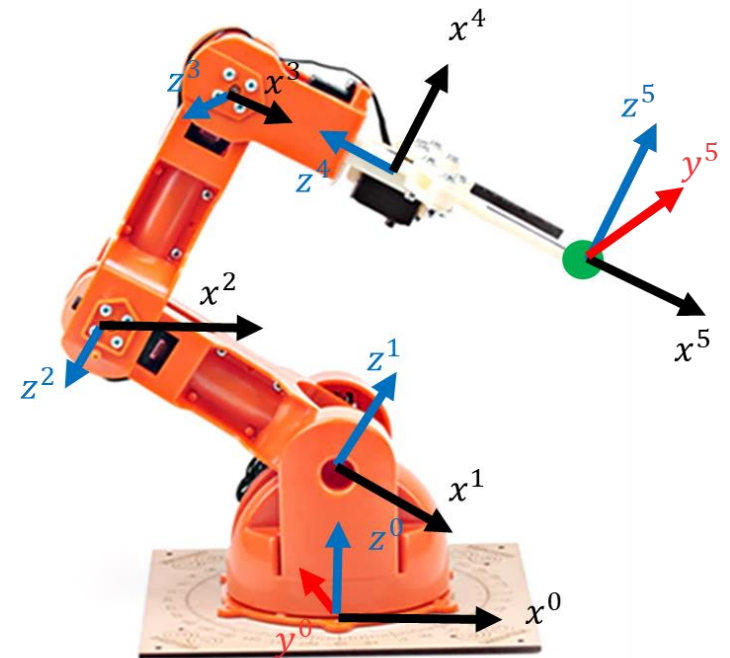
- where w_p is the position vector and w_o describes the orientation.
- the function $f(q_n) = \exp\left(\frac{q_n}{\pi}\right) r_3$:
 - describes the roll angle based on the length of w_o
 - r_3 is the unit vector
 - is always positive
 - its inverse function is well defined:

$$f^{-1}(w) = \pi \ln(\sqrt{w_4^2 + w_5^2 + w_6^2})$$



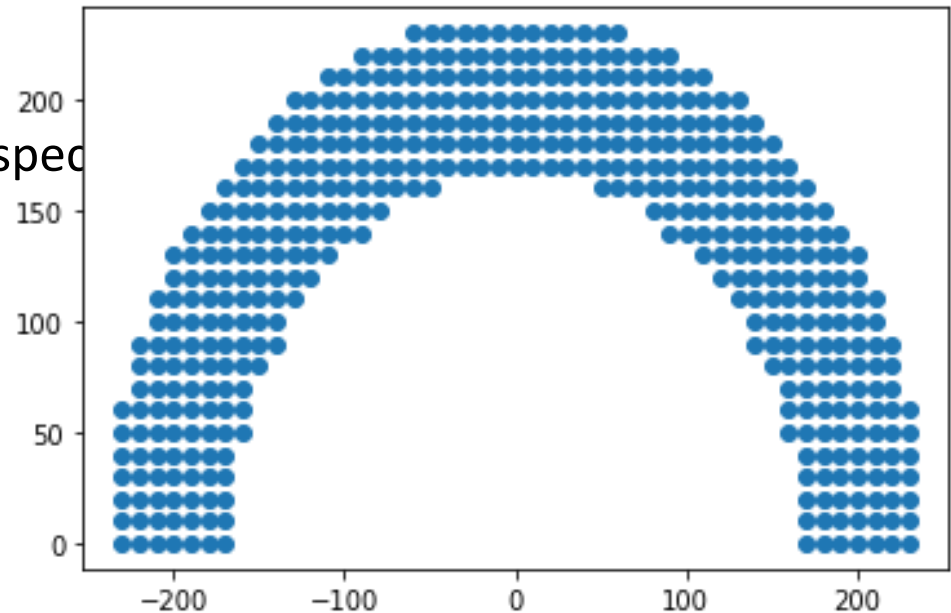
Inverse Kinematics / Backward Transformation

- Reverse transformation 5-axis articulated arm (Schilling – Fundamentals of Robotics)
 - Model considers general configuration as shown
 - To adapt the model to the Tinkerbot Braccio
 - Comparison of DH parameters (sign)
 - Adaptation of coordinate systems:
 - Consider different direction of rotation
 - Consider offset, especially with the tool pitch angle!



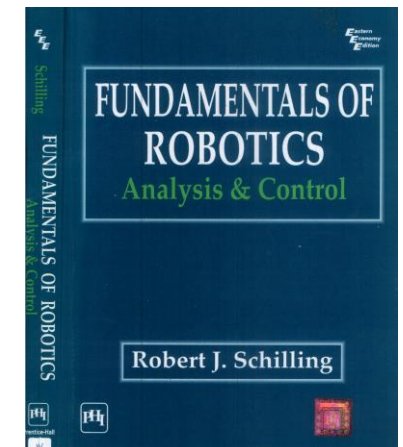
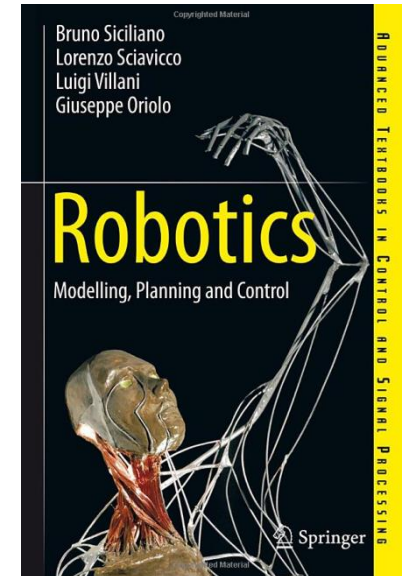
Inverse Kinematics / Backward Transformation

- Working area of the Tinkerbot Braccio (5-axis articulated arm)
- Boundary conditions:
 - Orientation of the gripper:
 - tilted by $11,25^\circ$ ($=\pi/16$) with respect to the z-axis of the base KS
 - Rotation of the hand
 - Joint axis of rotation always 90°
 - Position of the gripper tip 3 mm above X-Y plane
- Result:
 - 5-axis articulated arm has a very limited working area
 - Gripper can hardly be aligned parallel to the z-axis of the base KS



Inverse Kinematics / Backward Transformation

- Analytical solutions exist e.g. for the following kinematics:
 - 5-axis articulated arm
 - Scara
 - 6-axis articulated arm
- The following references:
 - B.Siciliano, L. Sciavicco, L. Villani, G. Oriolo
"Robotics: Modelling, Planning and Control ,
Springer 2009
Attention: different approach to DH transformation!
 - Schilling, R.J.
"Fundamentals of Robotics", Prentice Hall 2003



Summary

- DH method forms the basis for calculating TCP position based on the joint variables
- Inverse kinematics is necessary in practical application to determine the joint variables for a TCP pose.
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