

# JACKAL's Model Predictive Control Model

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## 1 State Parameters and Control Vectors

### 1.1 State Parameter Vector

$$\mathbf{x}_t = \begin{bmatrix} x_t \\ y_t \\ \theta_t \\ v_t \\ cte_t \\ e\theta_t \end{bmatrix}$$

where:

- $x_t$  and  $y_t$  represent the vehicle's position coordinates.
- $\theta_t$  is the vehicle's orientation or heading angle.
- $v_t$  is the vehicle's velocity.
- $cte_t$  (Cross Track Error) measures the lateral distance between the vehicle and the reference trajectory.
- $e\theta_t$  (Error in Theta) represents the orientation error relative to the trajectory's tangent at the vehicle's current position.

### 1.2 Control Vector

$$\mathbf{u}_t = \begin{bmatrix} \omega_t \\ a_t \end{bmatrix}$$

where:

- $\omega_t$  is the angular velocity, which affects the vehicle's heading.
- $a_t$  is the acceleration, controlling the speed increase or decrease.

These control inputs are used to predict and optimize the vehicle's trajectory over the prediction horizon, ensuring adherence to the desired path while maintaining dynamic stability and safety.

## 2 Total Cost Function

The total cost function  $J$  is defined as:

$$\begin{aligned}
 J = & \sum_{i=0}^{N-1} (w_{cte}(cte_i - ref_{cte})^2 + w_{\theta}(e\theta_i - ref_{\theta})^2 + w_v(v_i - ref_v)^2) \\
 & + \sum_{i=0}^{N-2} (w_{angvel}angvel_i^2 + w_{accel}accel_i^2) \\
 & + \sum_{i=0}^{N-3} (w_{angvel\_d}(angvel_{i+1} - angvel_i)^2 + w_{accel\_d}(accel_{i+1} - accel_i)^2)
 \end{aligned}$$

where:

- $cte_i$ ,  $e\theta_i$ , and  $v_i$  represent the cross-track error, heading error, and velocity at step  $i$ .
- $ref_{cte}$ ,  $ref_{\theta}$ , and  $ref_v$  are the target values for these states.
- $w_{cte}$ ,  $w_{\theta}$ ,  $w_v$ ,  $w_{angvel}$ ,  $w_{accel}$ ,  $w_{angvel\_d}$ , and  $w_{accel\_d}$  are weights indicating the importance of each component.
- $angvel_i$  and  $accel_i$  are the control inputs at each step for angular velocity and acceleration.

## 3 Constraint Formulations

### 3.1 Initial State Constraints

$$\begin{aligned}
 x[1] &= x_{start}, \\
 y[1] &= y_{start}, \\
 \theta[1] &= \theta_{start}, \\
 v[1] &= v_{start}, \\
 cte[1] &= cte_{start}, \\
 e\theta[1] &= e\theta_{start}.
 \end{aligned}$$

### 3.2 Vehicle Dynamics and Control Constraints

$$\begin{aligned}
 x_{t+1} &= x_t + v_t \cos(\theta_t) \cdot dt, \\
 y_{t+1} &= y_t + v_t \sin(\theta_t) \cdot dt, \\
 \theta_{t+1} &= \theta_t + \omega_t \cdot dt, \\
 v_{t+1} &= v_t + a_t \cdot dt, \\
 cte_{t+1} &= cte_t + (v_t \sin(e\theta_t) \cdot dt), \\
 e\theta_{t+1} &= e\theta_t - (\theta_t - \text{atan}(f'(x_t))) + \omega_t \cdot dt.
 \end{aligned}$$

where  $f'(x_t)$  represents the derivative of the polynomial trajectory fit evaluated at  $x_t$ .

### 3.3 Actuator Limitations

To ensure smooth control actions and avoid abrupt vehicle behavior, actuator limitations are imposed:

$$\begin{aligned} |\omega_t| &\leq \omega_{max}, \\ |a_t| &\leq a_{max}. \end{aligned}$$

### 3.4 Actuator Change Constraints

Minimizing the change in control inputs to promote smoother transitions:

$$\begin{aligned} |\Delta\omega_t| &\leq \Delta\omega_{max}, \\ |\Delta a_t| &\leq \Delta a_{max}. \end{aligned}$$