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Technical Report

3rd Generation Partnership Project; Technical Specification Group Radio Access Network; Solutions for NR to support non-terrestrial networks (NTN) (Release 16)



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Foreword

This Technical Report has been produced by the 3rd Generation Partnership Project (3GPP).

The contents of the present document are subject to continuing work within the TSG and may change following formal TSG approval. Should the TSG modify the contents of the present document, it will be re-released by the TSG with an identifying change of release date and an increase in version number as follows:

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z the third digit is incremented when editorial only changes have been incorporated in the document.

In the present document, modal verbs have the following meanings:

shall indicates a mandatory requirement to do something

shall not indicates an interdiction (prohibition) to do something

The constructions "shall" and "shall not" are confined to the context of normative provisions, and do not appear in Technical Reports.

The constructions "must" and "must not" are not used as substitutes for "shall" and "shall not". Their use is avoided insofar as possible, and they are not used in a normative context except in a direct citation from an external, referenced, non-3GPP document, or so as to maintain continuity of style when extending or modifying the provisions of such a referenced document.

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The construction "may not" is ambiguous and is not used in normative elements. The unambiguous constructions "might not" or "shall not" are used instead, depending upon the meaning intended.

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will indicates that something is certain or expected to happen as a result of action taken by an agency the behaviour of which is outside the scope of the present document

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might indicates a likelihood that something will happen as a result of action taken by some agency the behaviour of which is outside the scope of the present document

might not indicates a likelihood that something will not happen as a result of action taken by some agency the behaviour of which is outside the scope of the present document

In addition:

is (or any other verb in the indicative mood) indicates a statement of fact

is not (or any other negative verb in the indicative mood) indicates a statement of fact

The constructions "is" and "is not" do not indicate requirements.

1 Scope

The objectives for this document are, based on the outcomes of the TR 38.811 [2], to study a set of necessary features/adaptations enabling the operation of the New Radio (NR) protocol in non-terrestrial networks for 3GPP Release 16 with a priority on satellite access. Access network based on Unmanned Aerial System (UAS) including High Altitude Platform Station (HAPS) could be considered as a special case of non-terrestrial access with lower delay/Doppler value and variation rate.

The objectives for the study are the following

- Consolidation of potential impacts on the physical layer and definition of related solutions if needed
- Performance assessment of NR in selected deployment scenarios (LEO based satellite access, GEO based satellite access) through link level (Radio link) and system level (cell) simulations
- Study and define related solutions if needed on NR related Layer 2 and 3
- Study and define related solutions if needed on RAN architecture and related interface protocols

NOTE: As far as architecture issues are concerned, this TR supersedes TR 38.811 [2]

2 References

The following documents contain provisions, which, through reference in this text, constitute provisions of the present document.

- References are either specific (identified by date of publication, edition number, version number, etc.) or non-specific.
- For a specific reference, subsequent revisions do not apply.
- For a non-specific reference, the latest version applies. In the case of a reference to a 3GPP document (including a GSM document), a non-specific reference implicitly refers to the latest version of that document *in the same Release as the present document*.

- [1] 3GPP TR 21.905: "Vocabulary for 3GPP Specifications"
- [2] 3GPP TR 38.811 v15.2.0: "Study on New Radio (NR) to support non-terrestrial networks (Release 15)"
- [3] 3GPP TS 38.401: "NG-RAN; Architecture description (Release 15)"
- [4] 3GPP TR 38.874: "NR-Study on IAB (Integrated Access and Backhaul)"
- [5] 3GPP TS 37.340: "NR; Multi-connectivity; Overall description"
- [6] RP-181370: "Study on solutions evaluation for NR to support Non Terrestrial Network"
- [7] 3GPP TS 23.501 V15.0.0: "System Architecture for the 5G System"
- [8] R3-184403, NR-NTN: "Paging in NGSO Satellite Systems"
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- [10] AIAA 2006-6753: "Revisiting Spacetrack Report #3 , Models for Propagation of NORAD Element Sets", David A. Vallado, Paul Crawford, Richard Hujšák, T. S. Kelso, presented at the AIAA/AAS Astrodynamics Specialist Conference, Keystone, CO, 2006 August 21–24, 2006

- [11] 3GPP TS 38.420: "NG-RAN; Xn general aspects and principles"
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- [27] R1-1912610 "System simulation results and link budget for NTN", ZTE, submitted to RAN1#99
- [28] R1-1909693 "Simulation Assumptions for Multi Satellite Evaluation", Nokia, Nokia Shanghai Bell, submitted to RAN1#98
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3 Definitions of terms, symbols and abbreviations

3.1 Terms

For the purposes of the present document, the terms and definitions given in TR 21.905 [1] and the following apply. A term defined in the present document takes precedence over the definition of the same term, if any, in TR 21.905 [1].

Availability: % of time during which the RAN is available for the targeted communication. Unavailable communication for shorter period than [Y] ms shall not be counted. The RAN may contain several access network components among which an NTN to achieve multi-connectivity or link aggregation.

Feeder link: Wireless link between NTN Gateway and satellite

Geostationary Earth orbit: Circular orbit at 35,786 km above the Earth's equator and following the direction of the Earth's rotation. An object in such an orbit has an orbital period equal to the Earth's rotational period and thus appears motionless, at a fixed position in the sky, to ground observers.

Low Earth Orbit: Orbit around the Earth with an altitude between 300 km, and 1500 km.

Medium Earth Orbit: region of space around the Earth above low Earth orbit and below geostationary Earth Orbit.

Minimum Elevation angle: minimum angle under which the satellite or UAS platform can be seen by a terminal.

Mobile Services: a radio-communication service between mobile and land stations, or between mobile stations

Mobile Satellite Services: A radio-communication service between mobile earth stations and one or more space stations, or between space stations used by this service; or between mobile earth stations by means of one or more space stations

Non-Geostationary Satellites: Satellites (LEO and MEO) orbiting around the Earth with a period that varies approximately between 1.5 hour and 10 hours. It is necessary to have a constellation of several Non-Geostationary satellites associated with handover mechanisms to ensure a service continuity.

Non-terrestrial networks: Networks, or segments of networks, using an airborne or space-borne vehicle to embark a transmission equipment relay node or base station.

NTN-gateway: an earth station or gateway is located at the surface of Earth, and providing sufficient RF power and RF sensitivity for accessing to the satellite (resp. HAPS). NTN Gateway is a transport network layer (TNL) node.

On Board processing: digital processing carried out on uplink RF signals aboard a satellite or an aerial.

On board NTN gNB: gNB implemented in the regenerative payload on board a satellite (respectively HAPS).

On ground NTN gNB: gNB of a transparent satellite (respectively HAPS) payload implemented on ground.

One-way latency: time required to propagate through a telecommunication system from a terminal to the public data network or from the public data network to the terminal. This is especially used for voice and video conference applications.

Regenerative payload: payload that transforms and amplifies an uplink RF signal before transmitting it on the downlink. The transformation of the signal refers to digital processing that may include demodulation, decoding, re-encoding, re-modulation and/or filtering.

Round Trip Delay: time required for a signal to travel from a terminal to the sat-gateway or from the sat-gateway to the terminal and back. This is especially used for web-based applications.

Satellite: a space-borne vehicle embarking a bent pipe payload or a regenerative payload telecommunication transmitter, placed into Low-Earth Orbit (LEO), Medium-Earth Orbit (MEO), or Geostationary Earth Orbit (GEO).

Satellite beam: A beam generated by an antenna on-board a satellite

Service link: Radio link between satellite and UE

Transparent payload: payload that changes the frequency carrier of the uplink RF signal, filters and amplifies it before transmitting it on the downlink

Unmanned Aircraft Systems: Systems encompassing Tethered UAS (TUA), Lighter Than Air UAS (LTA), Heavier Than Air UAS (HTA), all operating in altitudes typically between 8 and 50 km including High Altitude Platforms (HAPs)

User Connectivity: capability to establish and maintain data / voice / video transfer between networks and Terminals

User Throughput: data rate provided to a terminal

3.2 Symbols

Void

3.3 Abbreviations

For the purposes of the present document, the abbreviations given in TR 21.905 [1] and the following apply. An abbreviation defined in the present document takes precedence over the definition of the same abbreviation, if any, in TR 21.905 [1].

ECEF	Earth-Centered, Earth-Fixed
EIRP	Equivalent Isotropic Radiated Power
FAR	False Alarm Rate

FRF	Frequency Reuse Factor
FSS	Fixed Satellite Services
GEO	Geostationary Earth Orbiting
gNB	next Generation Node B
GW	Gateway
HAPS	High Altitude Platform Station
HEO	Highly Elliptical Orbiting
ISL	Inter-Satellite Links
LEO	Low Earth Orbiting
Mbps	Mega bit per second
MEO	Medium Earth Orbiting
MS	Mobile Services
MSS	Mobile Satellite Services
NAS-MM	Non-Access Stratum Mobility Management
NAS-SM	Non-Access Stratum Session Management
NGEO	Non-Geostationary Earth Orbiting
NTN	Non-Terrestrial Network
RAN	Radio Access Network
RTD	Round Trip Delay
SNR	Signal-to-Noise Ratio
SRI	Satellite Radio Interface
TLE	Two-Line Element
Rx	Receiver
UAS	Unmanned Aircraft System
UE	User Equipment

4 Non-Terrestrial Networks overview and scenarios

4.1 Non-Terrestrial Networks overview

A non-terrestrial network refers to a network, or segment of networks using RF resources on board a satellite (or UAS platform).

The typical scenario of a non-terrestrial network providing access to user equipment is depicted below:

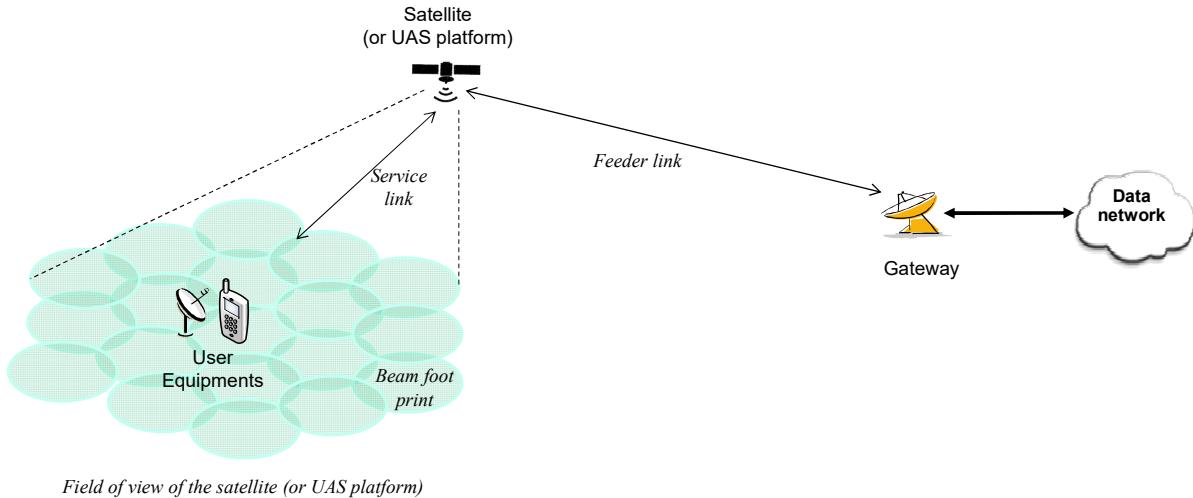


Figure 4.1-1: Non-terrestrial network typical scenario based on transparent payload

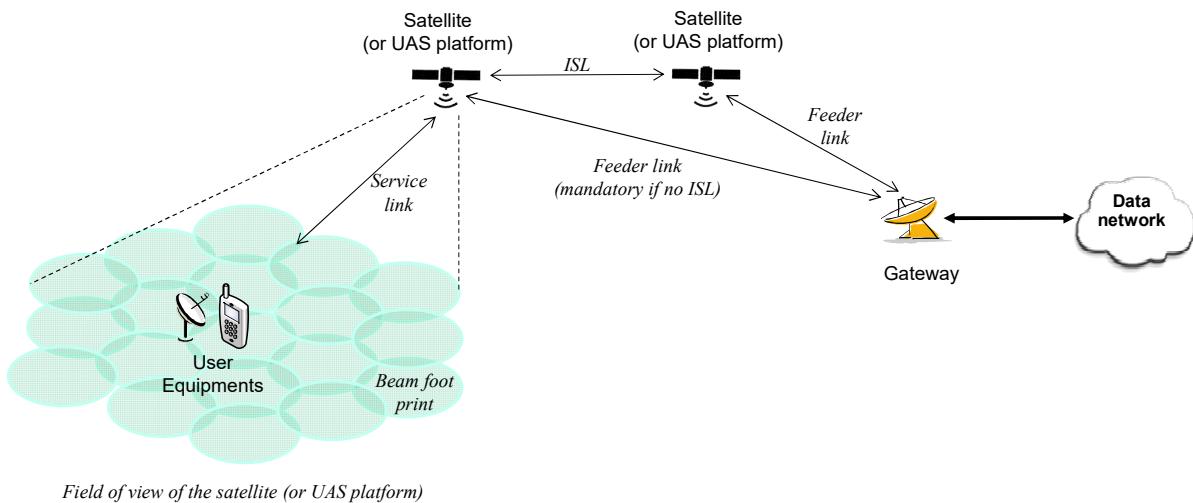


Figure 4.1-2: Non-terrestrial network typical scenario based on regenerative payload

Non-Terrestrial Network typically features the following elements:

- One or several sat-gateways that connect the Non-Terrestrial Network to a public data network

- a GEO satellite is fed by one or several sat-gateways which are deployed across the satellite targeted coverage (e.g. regional or even continental coverage). We assume that UE in a cell are served by only one sat-gateway
- A Non-GEO satellite served successively by one or several sat-gateways at a time. The system ensures service and feeder link continuity between the successive serving sat-gateways with sufficient time duration to proceed with mobility anchoring and hand-over
- A Feeder link or radio link between a sat-gateway and the satellite (or UAS platform)
- A service link or radio link between the user equipment and the satellite (or UAS platform).
- A satellite (or UAS platform) which may implement either a transparent or a regenerative (with on board processing) payload. The satellite (or UAS platform) generate beams typically generate several beams over a given service area bounded by its field of view. The footprints of the beams are typically of elliptic shape. The field of view of a satellites (or UAS platforms) depends on the on board antenna diagram and min elevation angle.
 - A transparent payload: Radio Frequency filtering, Frequency conversion and amplification. Hence, the waveform signal repeated by the payload is un-changed;
 - A regenerative payload: Radio Frequency filtering, Frequency conversion and amplification as well as demodulation/decoding, switch and/or routing, coding/modulation. This is effectively equivalent to having all or part of base station functions (e.g. gNB) on board the satellite (or UAS platform).
- Inter-satellite links (ISL) optionally in case of a constellation of satellites. This will require regenerative payloads on board the satellites. ISL may operate in RF frequency or optical bands.
- User Equipment are served by the satellite (or UAS platform) within the targeted service area.

There may be different types of satellites (or UAS platforms) listed here under:

Table 4.1-1: Types of NTN platforms

Platforms	Altitude range	Orbit	Typical beam footprint size
Low-Earth Orbit (LEO) satellite	300 – 1500 km	Circular around the earth	100 – 1000 km
Medium-Earth Orbit (MEO) satellite	7000 – 25000 km		100 – 1000 km
Geostationary Earth Orbit (GEO) satellite	35 786 km	notional station keeping position fixed in terms of elevation/azimuth with respect to a given earth point	200 – 3500 km
UAS platform (including HAPS)	8 – 50 km (20 km for HAPS)		5 - 200 km
High Elliptical Orbit (HEO) satellite	400 – 50000 km	Elliptical around the earth	200 – 3500 km

Typically

- GEO satellite and UAS are used to provide continental, regional or local service.
- a constellation of LEO and MEO is used to provide services in both Northern and Southern hemispheres. In some case, the constellation can even provide global coverage including polar regions. For the later, this requires appropriate orbit inclination, sufficient beams generated and inter-satellite links.

HEO satellite systems are not considered in this document.

4.2 Non-Terrestrial Networks reference scenarios

We shall consider in this document non-terrestrial networks providing access to user equipment in six reference scenarios including

- Circular orbiting and notional station keeping platforms.
- Highest RTD constraint
- Highest Doppler constraint
- A transparent and a regenerative payload
- One ISL case and one without ISL. Regenerative payload is mandatory in the case of inter-satellite links.
- Fixed or steerable beams resulting respectively in moving or fixed beam foot print on the ground

Six scenarios are considered as depicted in Table 4.2-1 and are detailed in Table 4.2-2.

Table 4.2-1: Reference scenarios

	Transparent satellite	Regenerative satellite
GEO based non-terrestrial access network	Scenario A	Scenario B
LEO based non-terrestrial access network: steerable beams	Scenario C1	Scenario D1
LEO based non-terrestrial access network: the beams move with the satellite	Scenario C2	Scenario D2

Table 4.2-2: Reference scenario parameters

Scenarios	GEO based non-terrestrial access network (Scenario A and B)	LEO based non-terrestrial access network (Scenario C & D)
Orbit type	notional station keeping position fixed in terms of elevation/azimuth with respect to a given earth point	circular orbiting around the earth
Altitude	35,786 km	600 km 1,200 km
Spectrum (service link)	<6 GHz (e.g. 2 GHz) >6 GHz (e.g. DL 20 GHz, UL 30 GHz)	
Max channel bandwidth capability (service link)	30 MHz for band < 6 GHz 1 GHz for band > 6 GHz	
Payload	Scenario A: Transparent (including radio frequency function only) Scenario B: regenerative (including all or part of RAN functions)	Scenario C: Transparent (including radio frequency function only) Scenario D: Regenerative (including all or part of RAN functions)
Inter-Satellite link	No	Scenario C: No Scenario D: Yes/No (Both cases are possible.)
Earth-fixed beams	Yes	Scenario C1: Yes (steerable beams), see note 1 Scenario C2: No (the beams move with the satellite) Scenario D 1: Yes (steerable beams), see note 1 Scenario D 2: No (the beams move with the satellite)
Max beam foot print size (edge to edge) regardless of the elevation angle	3500 km (Note 5)	1000 km
Min Elevation angle for both sat-gateway and user equipment	10° for service link and 10° for feeder link	10° for service link and 10° for feeder link
Max distance between satellite and user equipment at min elevation angle	40,581 km	1,932 km (600 km altitude) 3,131 km (1,200 km altitude)
Max Round Trip Delay (propagation delay only)	Scenario A: 541.46 ms (service and feeder links) Scenario B: 270.73 ms (service link only)	Scenario C: (transparent payload: service and feeder links) 25.77 ms (600km) 41.77 ms (1200km) Scenario D: (regenerative payload: service link only) 12.89 ms (600km) 20.89 ms (1200km)
Max differential delay within a cell (Note 6)	10.3 ms	3.12 ms and 3.18 ms for respectively 600km and 1200km
Max Doppler shift (earth fixed user equipment)	0.93 ppm	24 ppm (600km) 21ppm(1200km)
Max Doppler shift variation (earth fixed user equipment)	0.000 045 ppm/s	0.27ppm/s (600km) 0.13ppm/s(1200km)
User equipment motion on the earth	1200 km/h (e.g. aircraft)	500 km/h (e.g. high speed train) Possibly 1200 km/h (e.g. aircraft)
User equipment antenna types	Omnidirectional antenna (linear polarisation), assuming 0 dBi Directive antenna (up to 60 cm equivalent aperture diameter in circular polarisation)	
User equipment Tx power	Omnidirectional antenna: UE power class 3 with up to 200 mW Directive antenna: up to 20 W	
User equipment Noise figure	Omnidirectional antenna: 7 dB Directive antenna: 1.2 dB	
Service link	3GPP defined New Radio	
Feeder link	3GPP or non-3GPP defined Radio interface	3GPP or non-3GPP defined Radio interface

- NOTE 1: Each satellite has the capability to steer beams towards fixed points on earth using beamforming techniques. This is applicable for a period of time corresponding to the visibility time of the satellite
- NOTE 2: Max delay variation within a beam (earth fixed user equipment) is calculated based on Min Elevation angle for both gateway and user equipment
- NOTE 3: Max differential delay within a beam is calculated based on Max beam foot print diameter at nadir
- NOTE 4: Speed of light used for delay calculation is 299792458 m/s.
- NOTE 5: The Maximum beam foot print size for GEO is based on current state of the art GEO High Throughput systems, assuming either spot beams at the edge of coverage (low elevation).
- NOTE 6: The maximum differential delay at cell level has been computed considering the one at beam level for largest beam size. It does not preclude that cell may include more than one beam when beam size are small or medium size. However the cumulated differential delay of all beams within a cell will not exceed the maximum differential delay at cell level in the table above.

The NTN study results apply to GEO scenarios as well as all NGSO scenarios with circular orbit at altitude greater than or equal to 600 km.

5 NTN-based NG-RAN Architectures

The study has been carried out minimizing the need for new interfaces and protocols in the NG-RAN to support non-terrestrial networks.

5.1 Transparent satellite based NG-RAN architecture

5.1.1 Overview

The satellite payload implements frequency conversion and a Radio Frequency amplifier in both up link and down link direction. It corresponds to an analogue RF repeater.

Hence the satellite repeats the NR-Uu radio interface from the feeder link (between the NTN gateway and the satellite) to the service link (between the satellite and the UE) and vice versa.

The Satellite Radio Interface (SRI) on the feeder link is the NR-Uu. In other words, the satellite does not terminate NR-Uu.

The NTN GW supports all necessary functions to forward the signal of NR-Uu interface.

Different transparent satellites may be connected to the same gNB on the ground.

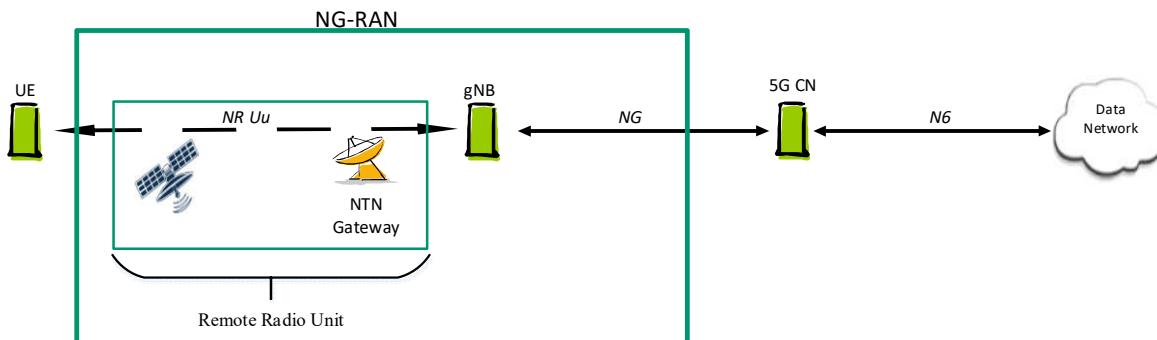


Figure 5.1-1: Networking-RAN architecture with transparent satellite

Note: Whilst several gNBs may access a single satellite payload, the description has been simplified to a unique gNB accessing the satellite payload, without loss of generality.

5.1.2 Detailed description of the architecture

The architecture of a transparent-satellite based NG-RAN is depicted in the following figure. The mapping to QoS flows is also highlighted.

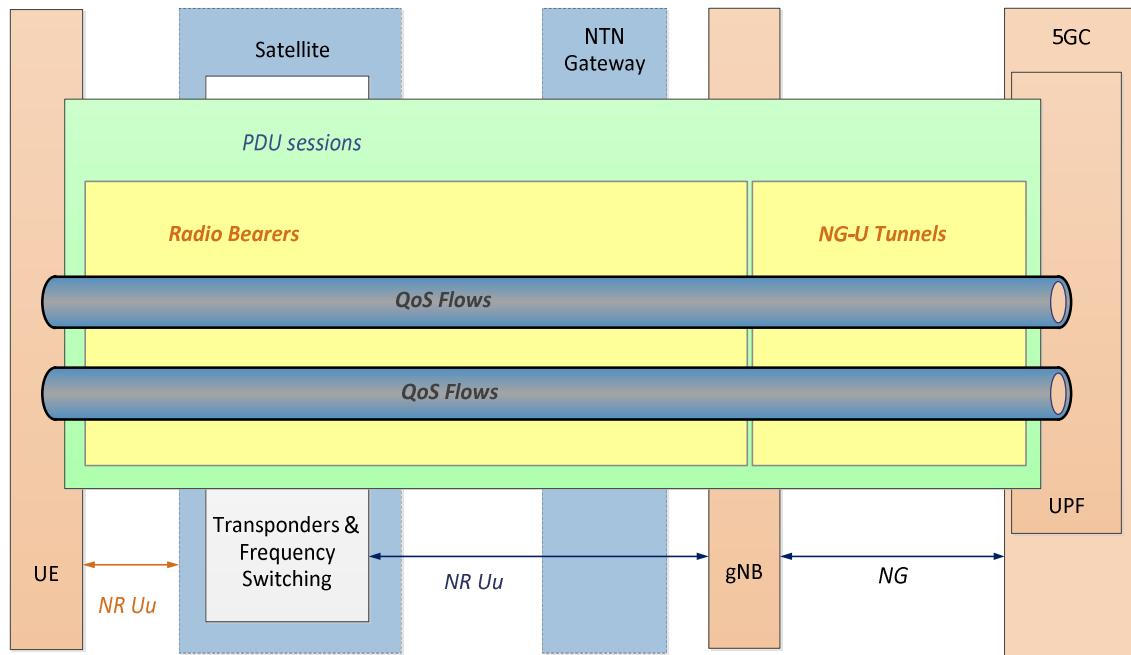


Figure 5.1-2: Transparent-satellite based NG-RAN with mapping to QoS flows

UE has access to the 5G system via a 3GPP NR based radio interface.

The user plane protocol stack is described hereafter.

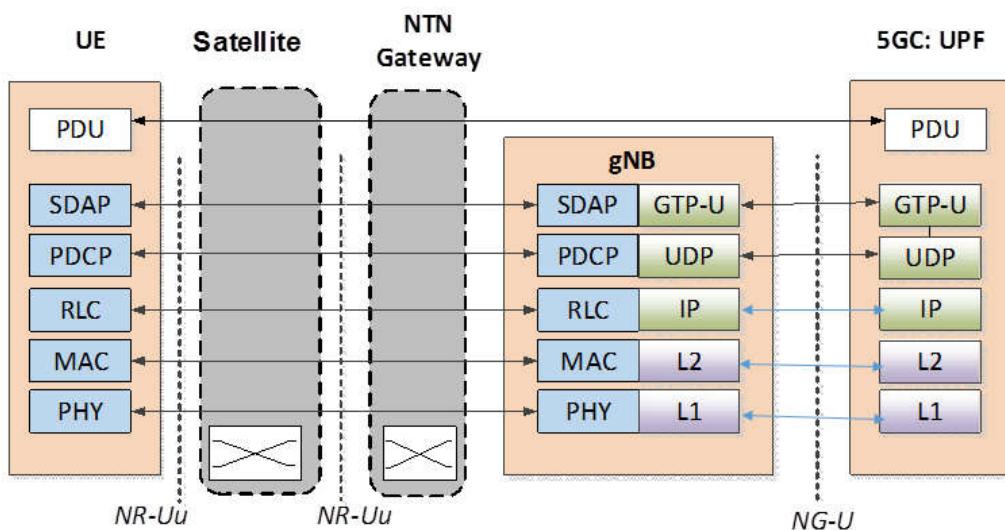


Figure 5.1-3: User plane Protocol stack (Transparent satellite)



RF processing & Frequency Switching

The user data is transported between the UE and the 5GC, as usual, but via the NTN Gateway.

The control plane protocol stack is described hereafter.

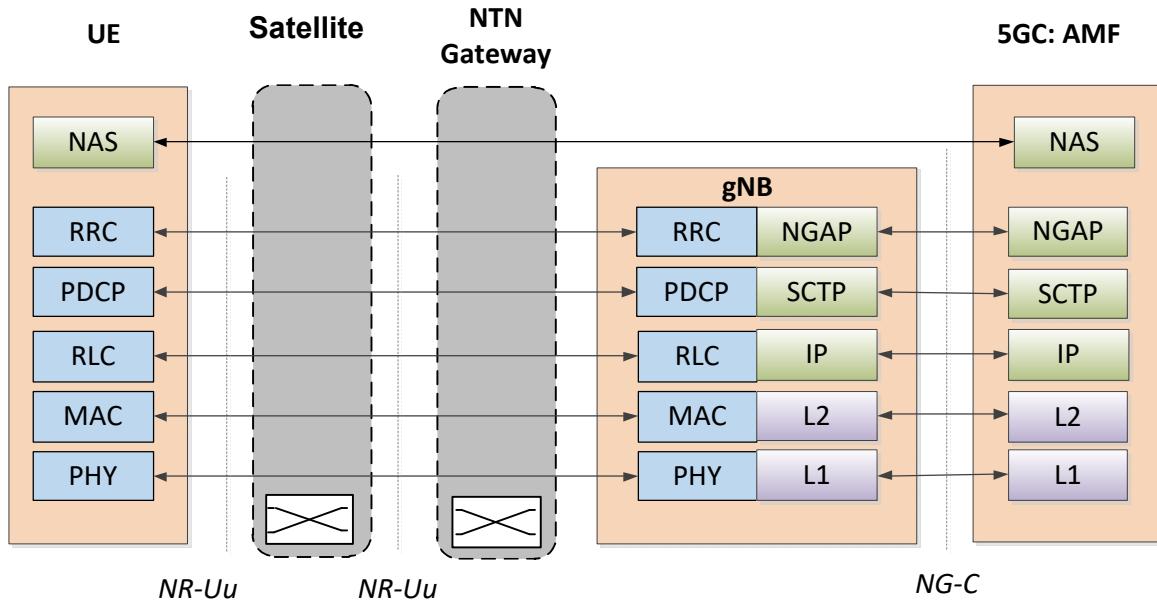


Figure 5.1-4: Control plane Protocol stack (Transparent satellite)



RF processing & Frequency Switching

The NAS (NAS-SM and NAS-MM) signalling from the UE and the NG-AP signalling from the gNB are transported toward the 5GC and vice versa.

5.1.3 NG-RAN impacts

There is no need to modify the NG-RAN architecture to support transparent satellite access.

NR-Uu timers may have to be extended to cope with the long delay of the feeder link and service link.

In the context of a LEO scenario with ISL, the delay to be considered shall encompass at least the feeder link (SRI) and one or several ISLs.

Both CP and UP protocol are terminated on the ground.

- With respect to CP, this scenario does not pose any particular issues but the need to adapt to the much longer roundtrip times of the Uu. This can be addressed by implementation
- Concerning UP, apart from issues arising from the longer roundtrip time for UP packets, the UP protocol itself is unaffected. The longer delay on the Uu interface will however require more buffering for the UP packets into the gNB.

5.2 Regenerative satellite based NG-RAN architectures

5.2.1 gNB processed payload

5.2.1.1 Overview

The NG-RAN logical architecture as described in TS 38.401 is used as baseline for NTN scenarios.

The satellite payload implements regeneration of the signals received from Earth.

- NR-Uu radio interface on the service link between the UE and the satellite
- Satellite Radio Interface (SRI) on the feeder link between the NTN gateway and the satellite.

SRI (Satellite Radio Interface) is a transport link between NTN GW and satellite.

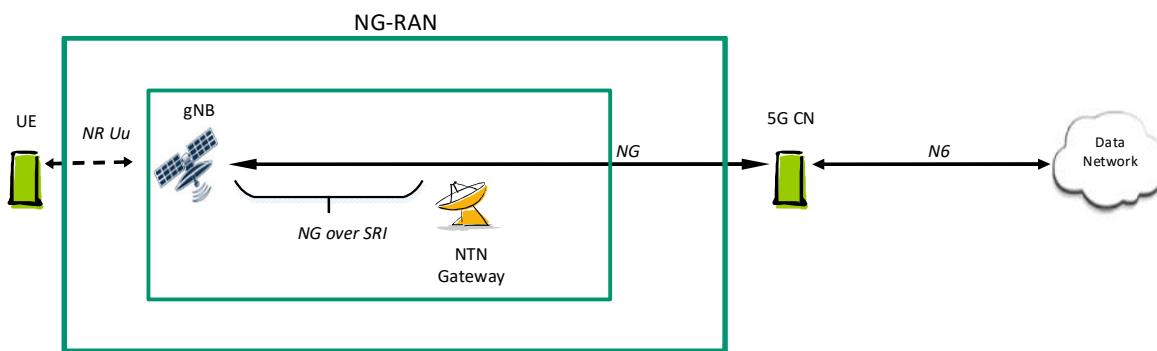


Figure 5.2.1-1: Regenerative satellite without ISL, gNB processed payload

NOTE: The satellite may embark additional traffic routing functions that are out of RAN scope.

The satellite payload also provides Inter-Satellite Links (ISL) between satellites

ISL (Inter-Satellite Links) is a transport link between satellites. ISL may be a radio interface or an optical interface that may be 3GPP or non 3GPP defined but this is out of the study item scope.

The NTN GW is a Transport Network Layer node, and supports all necessary transport protocols.

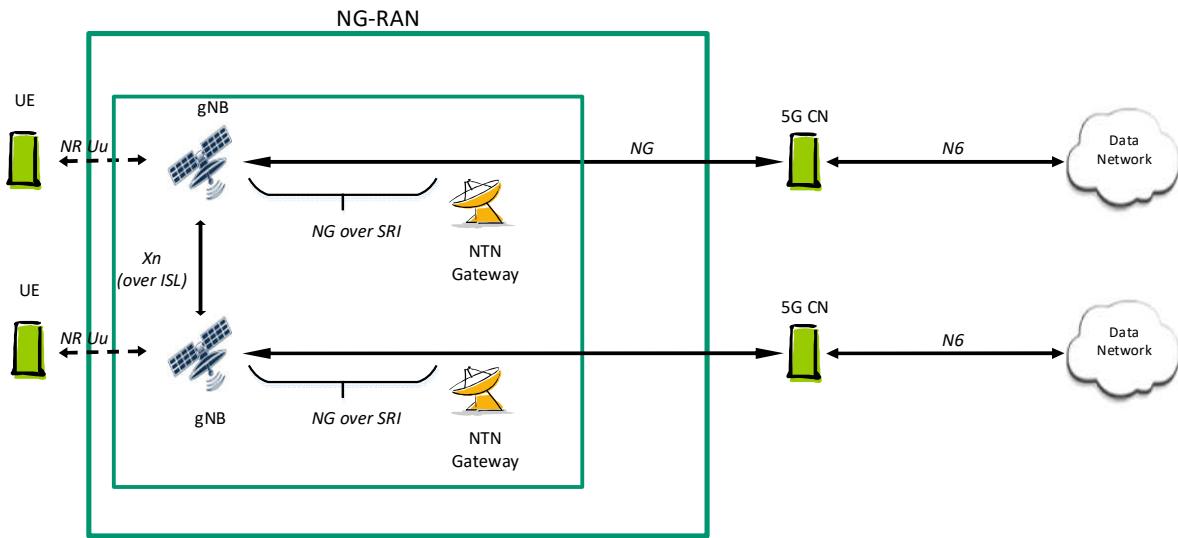


Figure 5.2.1-2: Regenerative satellite with ISL, gNB processed payload

The figure above illustrates that UE served by a gNB on board a satellite could access the 5GCN via ISL.

The gNB on board different satellites may be connected to the same 5GCN on the ground.

If the satellite hosts more than one gNB, the same SRI will transport all the corresponding NG interface instances.

5.2.1.2 Detailed description of the architecture

The architecture of a regenerative-satellite based NG-RAN is depicted on the following figure. The mapping to QoS flows is also highlighted.

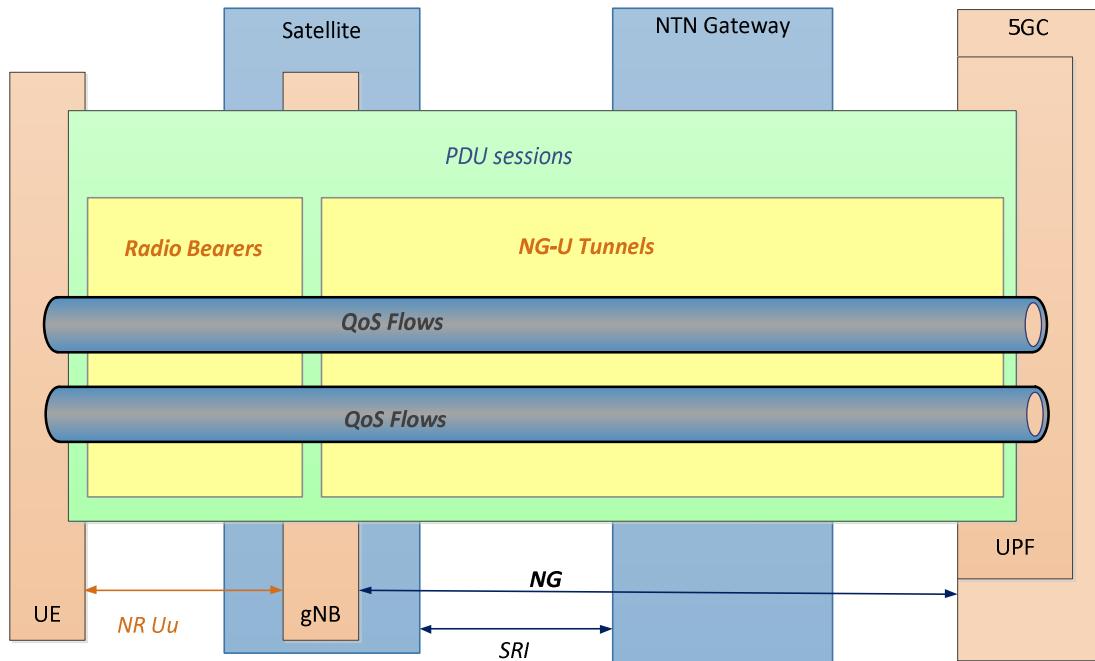


Figure 5.2.1-3: Regenerative satellite based NG-RAN architecture (gNB on board) with QoS flows

The UE user plane protocol stack for a PDU session is described hereafter.

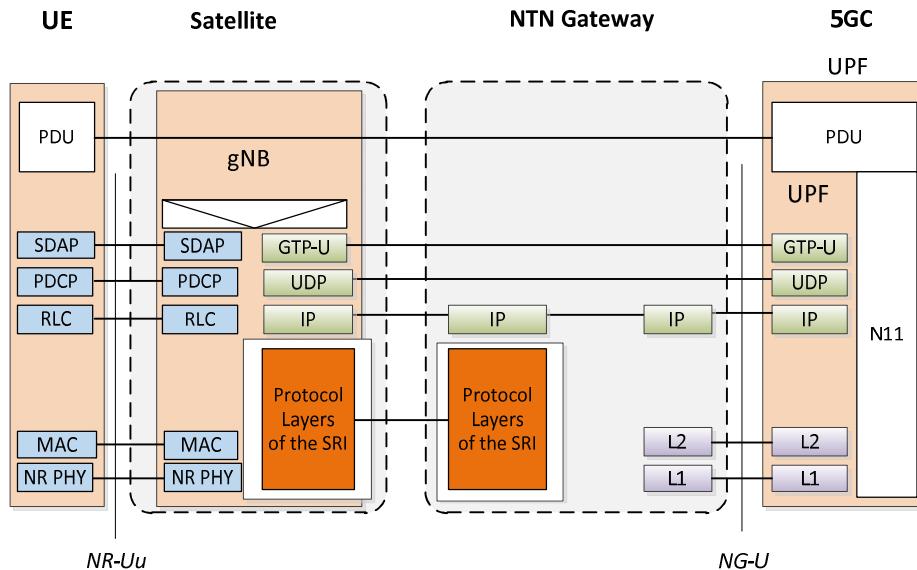


Figure 5.2.1-4: NG-RAN protocol architecture for regenerative satellite (gNB on board): User Plane

The Protocol stack of the Satellite Radio Interface (SRI) is used to transport the UE user plane between satellite and NTN-Gateway.

The User PDUs are transported over GTP-U tunnels, as usual, between the 5GC and the on-board gNB, but via the NTN Gateway.

The UE control plane protocol stack for a PDU session is described hereafter.

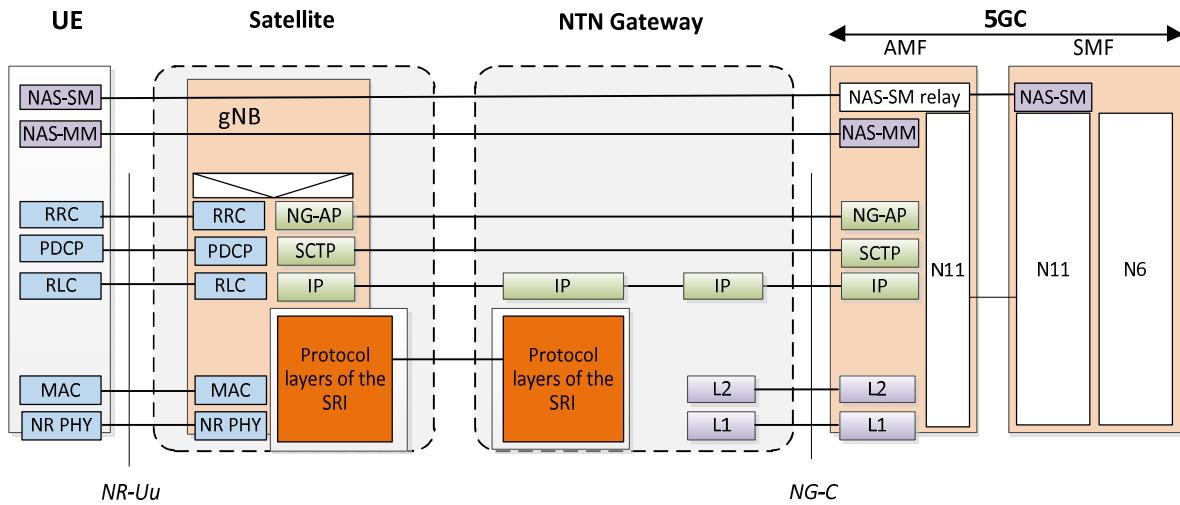


Figure 5.2.1-5: NG-RAN protocol architecture for regenerative satellite (gNB on board): Control Plane

The NG-AP is transported over SCTP, between the 5GC and the on board gNB, as usual, but via the NTN Gateway.

The NAS protocol is also transported by the NG-AP protocol, between the 5GC and the on board gNB, via the NTN Gateway.

5.2.1.3 NG-RAN impacts

NG Application Protocol timers may have to be extended to cope with the long delay of the feeder link.

NG can experience longer latency (up to several hundreds of ms in case of a GEO satellite) than in terrestrial networks, and this will affect both CP and UP; this can be addressed by implementation.

In the context of a LEO scenario with ISL, the delay to be considered shall encompass at least the feeder link (SRI) and one or several ISLs.

5.2.2 gNB-DU processed payload

5.2.2.1 Overview

The NG-RAN logical architecture with CU/DU split as described in TS 38.401 is used as baseline for NTN scenarios.

The satellite payload implements regeneration of the signals received from Earth.

- NR-Uu radio interface on the service link between the satellite and the UE
- Satellite Radio Interface (SRI) on the feeder link between the NTN gateway and the satellite. The SRI transports the F1 protocol.

The satellite payload may provide inter-satellite links between satellites.

SRI (Satellite Radio Interface) are transport links; the logical interface F1 that they transport are 3GPP-specified.

The NTN GW is a Transport Network Layer node, and supports all necessary transport protocols.

DU on board different satellites may be connected to the same CU on ground.

If the satellite hosts more than one DU, the same SRI will transport all the corresponding F1 interface instances.

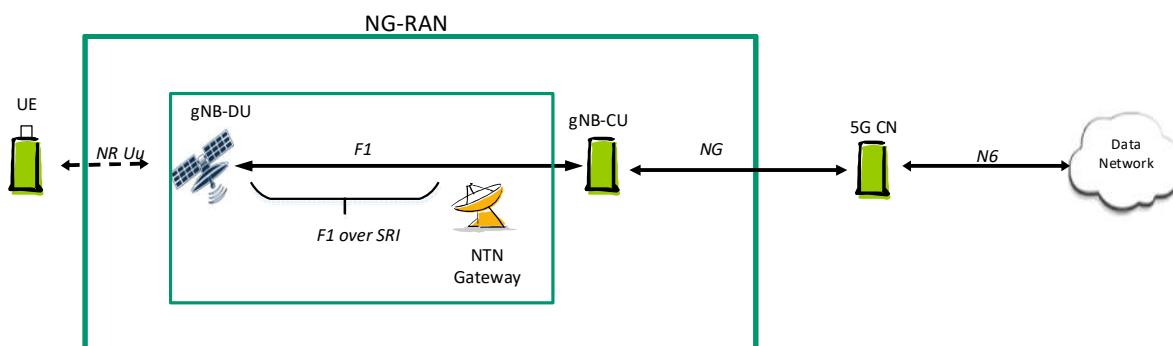


Figure 5.2.2-1: NG-RAN with a regenerative satellite based on gNB-DU

5.2.2.2 Detailed description of the architecture

The architecture of a regenerative-satellite based NG-RAN is depicted on the following figures. The mapping to QoS flows is also highlighted.

The PDCP PDUs (Protocol Data Units) are transported by the SRI protocols stack.

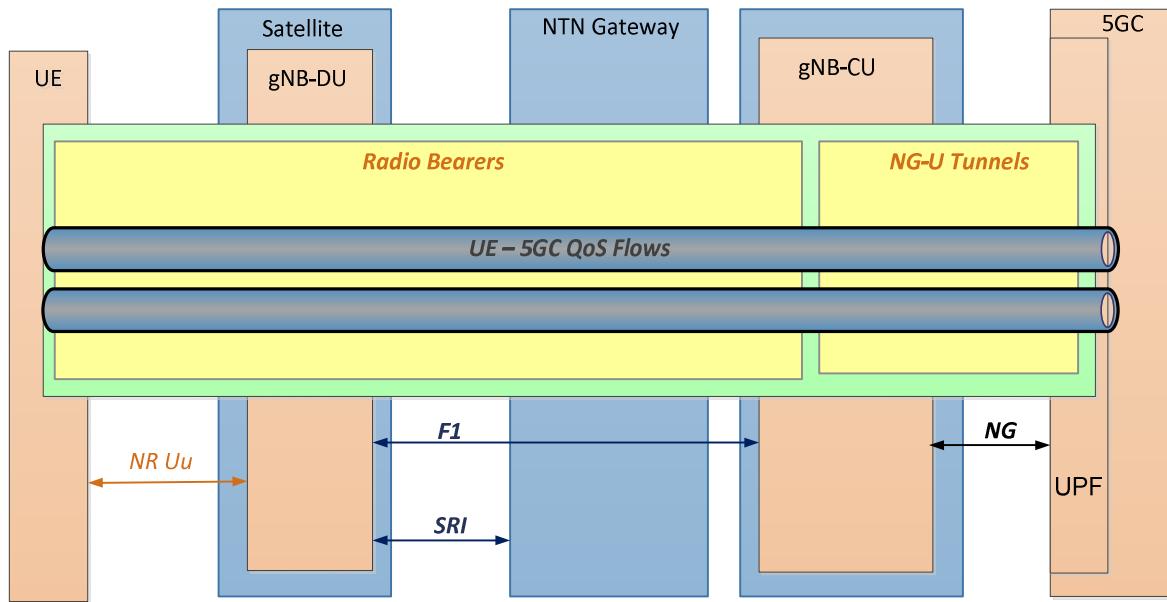


Figure 5.2.2-2: Regenerative satellite based NG-RAN architecture (gNB-DU on board) with QoS flows

The UE user plane protocol stack for a PDU session is described hereafter.

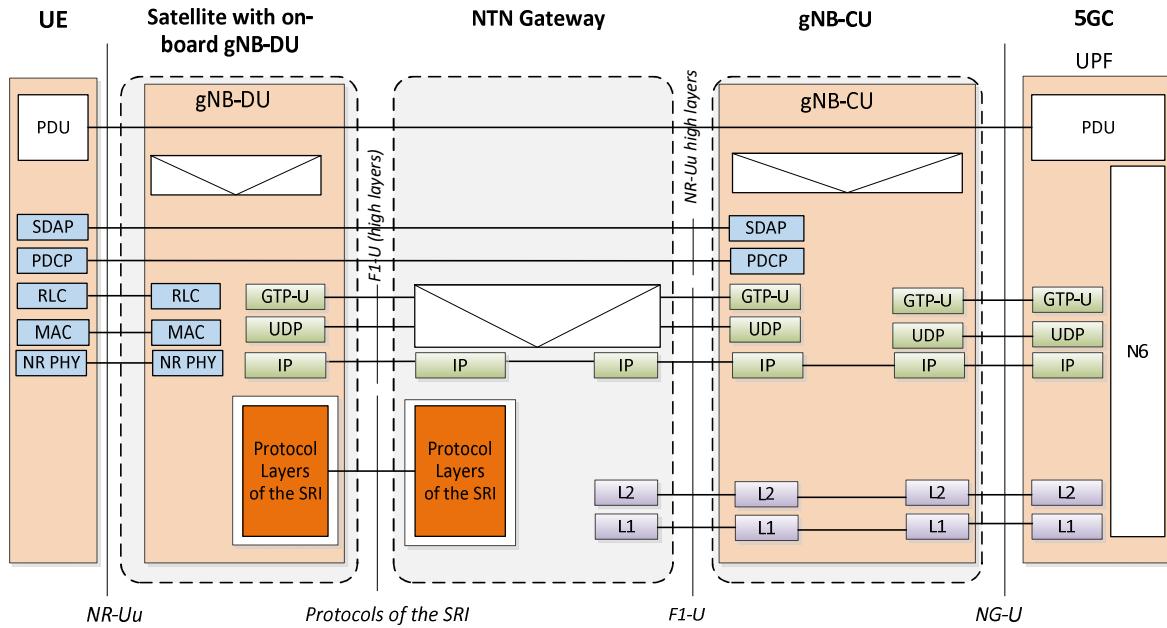


Figure 5.2.2-3: NG-RAN protocol architecture for regenerative satellite (gNB-DU on board): User Plane

The Protocol stack of the Satellite Radio Interface (SRI) is used to transport the UE user plane between satellite and NTN-Gateway.

The User PDUs are transported over GTP-U tunnels between the 5GC and the gNB-CU.

The User PDUs are transported over GTP-U tunnels between the gNB-CU and the on board gNB-DU via the NTN Gateway.

The UE control plane protocol stack for a PDU session is described hereafter

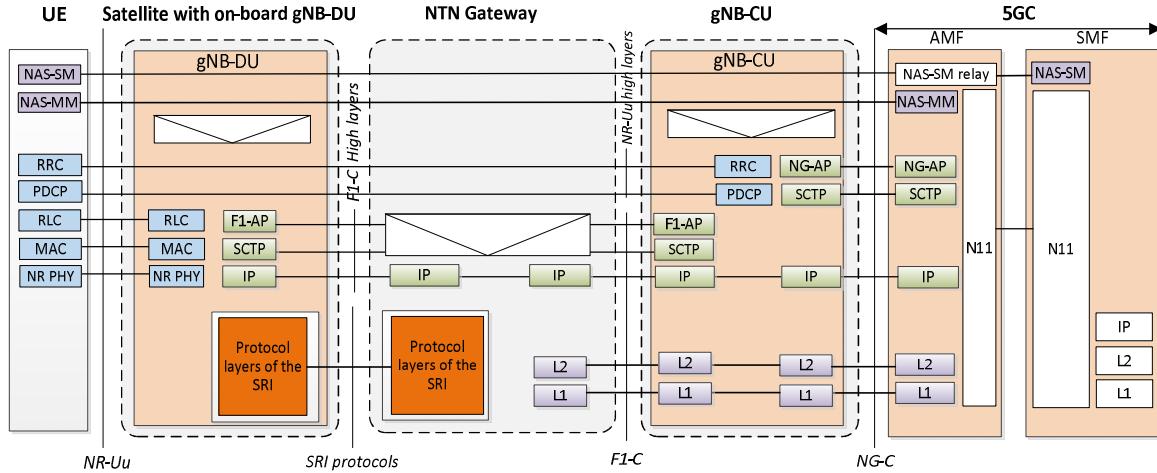


Figure 5.2.2-4: NG-RAN protocol architecture for regenerative satellite (gNB-DU on board): Control Plane

The NG-AP PDUs are transported over SCTP between the 5GC and the gNB-CU.

The RRC PDUs are transported over PDCP over the F1-C protocols stack between the gNB-CU and the on board gNB-DU, via the NTN Gateway. The F1-C PDUs are transported over SCTP over IP. IP packets are transported over SRI protocols stack, at the SRI and over any L2/L1 layers at gNB-CU – NTN Gateway interface.

The NAS protocols (NAS-MM, NAS-SM) are also transported by the NG-AP protocol, between the 5GC, gNB-CU and the on board gNB-DU, via the NTN Gateway.

5.2.2.3 NG-RAN impacts

RRC and other Layer3 processing are terminated in the gNB-CU on ground, and are subject to stricter timing constraints.

The use of this architecture option for LEO (Low Earth Orbit) systems or even for GEO (Geostationary Earth Orbit) may impact current F1 implementation (e.g. timer extensions). Such impact for LEO will be much less significant than for GEO.

In this architecture, all CP interfaces toward terrestrial NG-RAN nodes are terminated on the ground.

- With respect to CP, this scenario does not pose any particular issues apart from the fact that F1AP will need to adapt to the much longer roundtrip times of the SRI.
- Concerning UP, the instance running over Xn is unaffected by the presence of the NTN, while the instance running over F1 (transported over the SRI) will need to adapt to the much longer roundtrip times of the SRI. This, in turn, will require more buffering for the UP packets into the gNB-CU.

5.2.3 gNB processed payload based on relay-like architectures (Optional)

How to apply the Integrated Access and Backhaul (IAB) proposed architecture configuration resulting from the IAB SI reflected in the TR 38.874 document [4] is for further study.

5.3 Multi connectivity involving NTN-based NG-RAN

5.3.1 Overview

This clause discusses multi connectivity [5], either for transparent or regenerative NTN-based NG-RAN, and in combination or not with terrestrial-based NG-RAN (NR or EUTRA). The focus is on dual connectivity with simultaneous use of two radio access.

This may apply to transparent satellites as well as regenerative satellites with gNB or gNB-DU function on board.

A number of service scenarios as described in TS 22.261 (e.g. user in residential homes, in vehicles, in high speed trains or on board airplanes), would benefit from the combination of terrestrial and non-terrestrial access to meet the targeted service performances in terms of data rate and/or reliability.

In underserved areas, the bandwidth provided by a terrestrial based access (e.g. LTE) may be limited at cell edge. Adding a NTN based NG-RAN will be an enable to achieve the targeted experience data rate.

Under some scenarios such as high speed trains, the service area may not be fully homogeneous along the rail track and multi connectivity involving NTN-based NG-RAN would enable to provide the targeted reliability.

Hence a UE may be connected and served simultaneously by at least:

- One NTN-based NG-RAN and one terrestrial-based access (NR or EUTRA)
- One NTN-based NG-RAN and another NTN-based NG-RAN

As for terrestrial access, connectivity combining can occur for either the uplink or the downlink or both.

The same gNB could serve NR cells via the terrestrial access network and via the satellite access network (e.g. with transparent payload on board the satellite).

5.3.2 Architecture aspects

Multi connectivity involving transparent NTN-based NG-RAN

A User Equipment is connected to a 5GCN via simultaneously a transparent NTN-based NG-RAN and a cellular NG-RAN. We assume that the NTN Gateway is located in the PLMN area of the cellular access network.

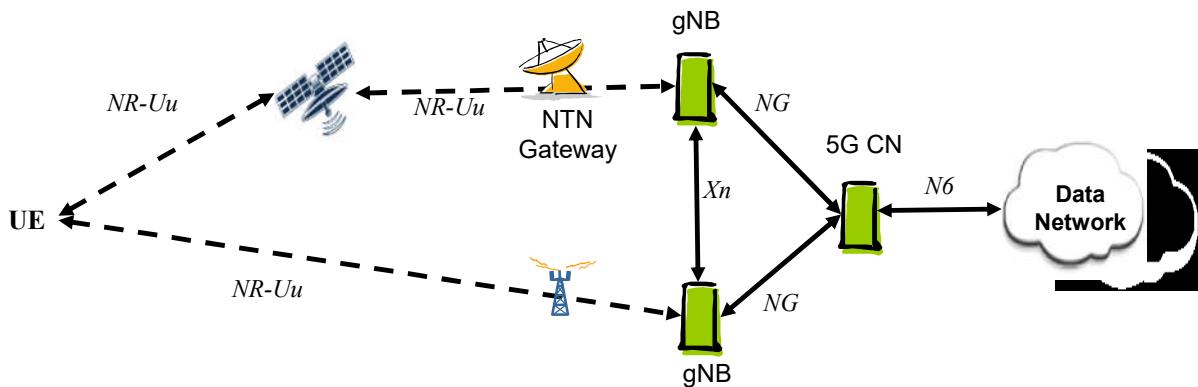


Figure 5.3.2-1: Multi connectivity involving transparent NTN-based NG-RAN and cellular NG-RAN

Both gNB of the NTN-based NG-RAN or the gNB of the cellular NG-RAN could be elected as master node.

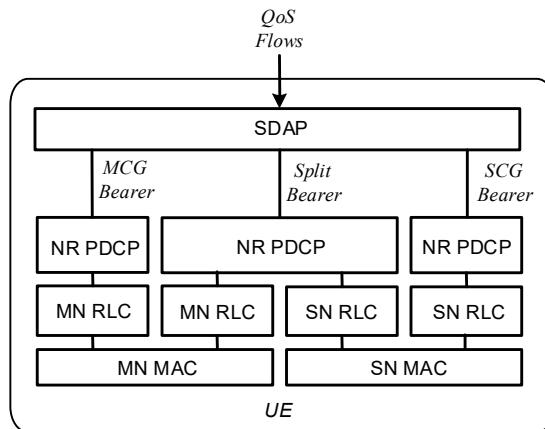


Figure 5.3.2-2: Radio Protocol Architecture for MCG, SCG and split bearers from a UE perspective in MR-DC with 5GC

Another case to be considered, refers to the combination of two Transparent NTN-based NG-RANs either GEO or LEO based or a combination of both. This is of interest to provide service to UEs in unserved areas. The LEO NTN-based NG-RAN featuring relatively low latency can be used to support the delay sensitive traffic while the GEO NTN-based NG-RAN would provide additional bandwidth to meet the targeted throughput requirements. This is depicted in the figure below.

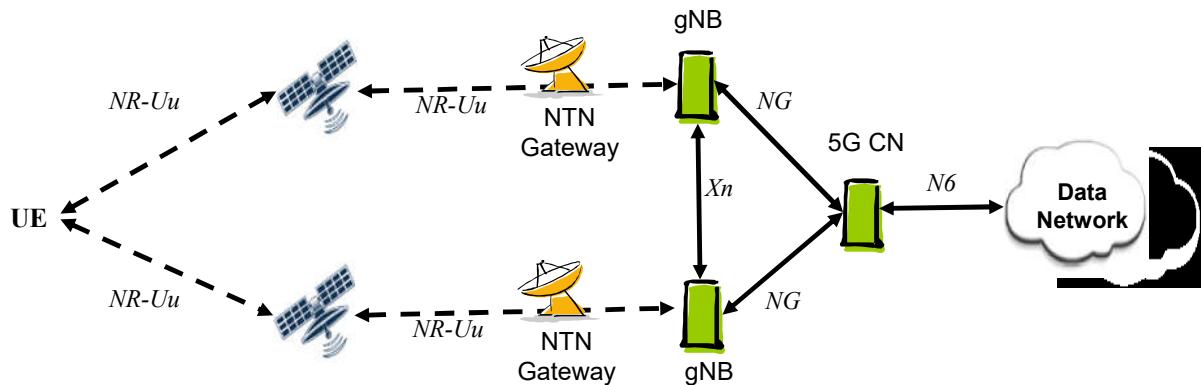


Figure 5.3.2-3: Multi connectivity between two transparent NTN-based NG-RAN

Multi connectivity involving regenerative NTN-based NG-RAN (gNB-DU on board)

Another case to be considered, refers to the combination of a regenerative NTN-based NG-RAN (gNB-DU on board) and a cellular NG-RAN. This is of interest to provide service to UEs in underserved areas. This is depicted in the figure below.

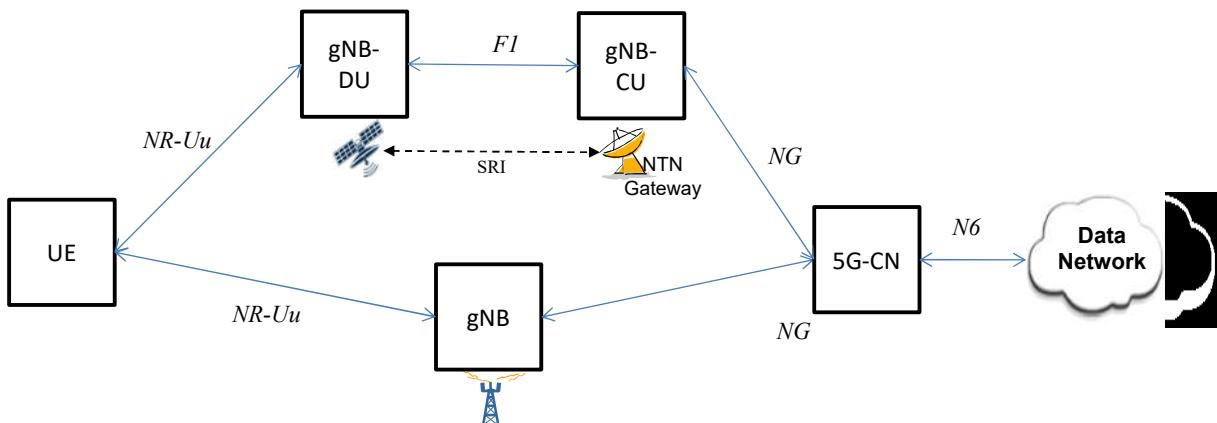


Figure 5.3.2-4: Multi connectivity involving regenerative NTN-based NG-RAN (gNB-DU) and cellular NG-RAN

Note that the multi connectivity may also involve two regenerative NTN-based NG-RAN (gNB-DU on board)

Multi connectivity involving regenerative NTN-based NG-RAN (gNB on board)

The combination of two regenerative NTN-based NG-RAN (gNB on board) either GEO or LEO based or a combination of both with Inter Satellite Links in between is also worth to consider to provide service to UEs in unserved areas. This is depicted in the figure below.

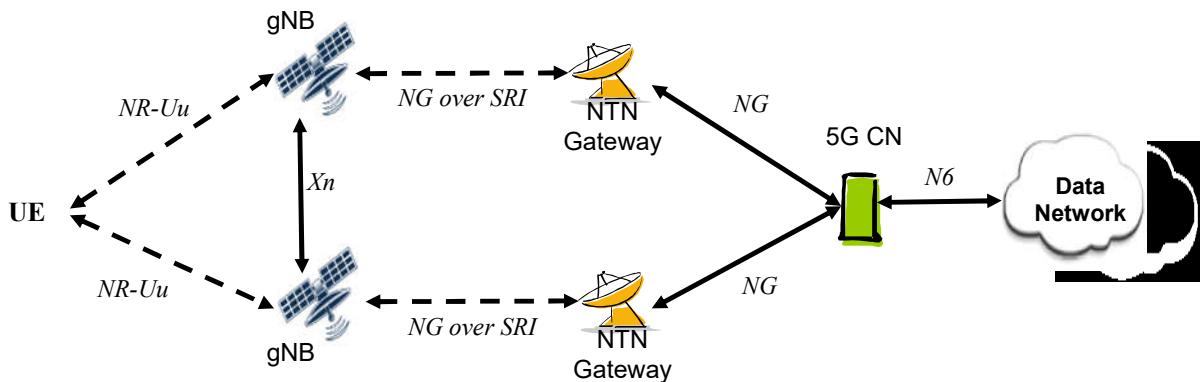


Figure 5.3.2-5: Multi connectivity between two regenerative NTN-based NG-RAN (gNB on board)

Note that multi connectivity between regenerative NTN-based NG-RAN (gNB on board) and cellular NG-RAN (NR or LTE based) is not addressed because the transport of Xn protocol over the Feeder link (based on Satellite Radio interface) is For Further Study.

5.3.3 NG-RAN impacts

In case of multi-connectivity involving transparent NTN-based NG-RAN (i.e. gNB on the ground), all CP and UP interfaces toward terrestrial NG-RAN nodes are terminated on the ground.

In case of multi-connectivity involving regenerative NTN-based NG-RAN with gNB-CU on the ground and gNB-DU on board, all CP interfaces toward terrestrial NG-RAN nodes are terminated on the ground.

- With respect to CP, this scenario does not pose any particular issues apart from the fact that F1AP will need to adapt to the much longer roundtrip times of the SRI.
- Concerning UP, the leg running over Xn is unaffected by the presence of the NTN, while the leg running over F1 (transported over the SRI) will need to adapt to the much longer roundtrip times of the SRI. Overall, UP buffering in the node hosting PDCP will need to compensate for the difference between the two interfaces. Therefore, there will be an impact on the terrestrial NG-RAN node involved in DC if such NG-RAN node hosts the PDCP.

In case of multi Connectivity involving regenerative NTN-based NG-RAN with on board gNB, setting up and maintaining Xn interfaces toward terrestrial gNBs over the feeder link would require all the corresponding traffic (CP and UP) to be transported over the SRI relevant to the satellite-hosted gNB. This may be a challenge.

Prerequisites for NR-NR DC where both MN and SN are NTN-based are to have at least a partial coverage area overlap, and to have Xn up and running through the ISL between them. The Xn connection between the satellites will add to the delay. NR-NR DC involving satellites whose orbital positions are close to one is feasible.

The multi connectivity procedure as defined in [5] may require some adaptations to support:

- Radio access technology featuring extended latency
- Radio access technology possibly suffering from variable latency within the backhaul network (e.g. a Xn interface crossing multiple satellite located on different orbital plane)
- Differentiated delay between both radio access technology involved

NG-RAN should allow the necessary flexibility to elect as master node either the gNB of the NTN-based NG-RAN or the gNB of the cellular NG-RAN.

5.4 Service continuity between NTN and Terrestrial Networks

In TS 22.261 (Clause 6.2.3 Service continuity requirements), for a 5G system with satellite access, the following requirements apply:

- The 5G system shall support service continuity between 5G terrestrial access network and 5G satellite access networks owned by the same operator or owned by 2 different operators having an agreement.

Mobility between TN and NTN

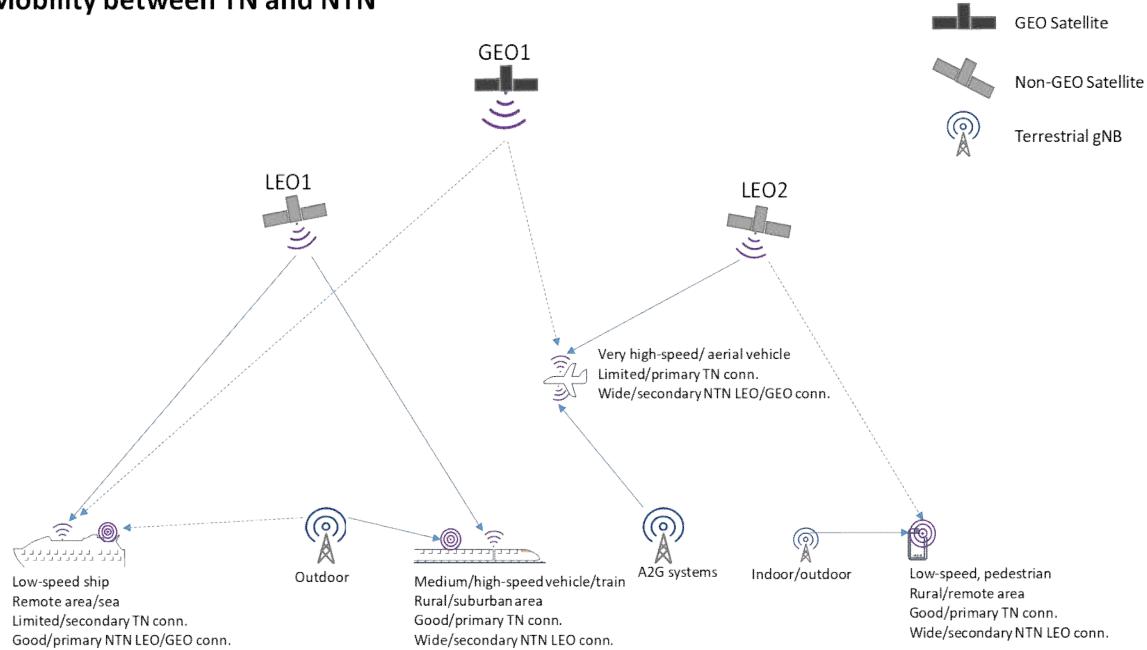


Figure 5.4-1: Typical example of NTN-TN interworking

The NTN and TN could either operate in two different frequency bands (e.g. FR1 vs FR2), or in same frequency band (e.g. FR1 or FR2).

The NTN reference scenarios as listed in chapter 4.2 considers two types of NTN UEs, a) UE with Omni directional antenna, b) UE with directive antenna. For the support of NTN-TN service continuity use cases, assumptions on UE characteristics considering NTN use cases are listed in the below table:

Table 5.4-1: NTN use cases mapped to TN-NTN service continuity use cases and assumptions for frequency band and UE characteristics

NTN Use case	NTN-TN service continuity use case	Assumptions for UE characteristics
Stationary UE (eMBB) Pedestrian UE (eMBB) Machine UE (mMTC)	Medium/high throughput – TN or NTN (LEO) Low to medium throughput NTN (GEO)	The UE is assumed to have TN and NTN connectivity capabilities. The UE has omni-directional antenna type applicable to both TN and NTN connectivity. The NTN access may operate in frequency bands below or above 6 GHz
Stationary/Vehicular relay UE (eMBB) [Relay UE on vehicles or ships Relay UE on high speed trains Relay UE on board airplanes]	Medium/high throughput – TN or NTN (LEO) Medium/high throughput NTN (GEO)	The relay UE is assumed to have TN and NTN connectivity capabilities and provides service to the TN only capable UEs outdoor or inside buildings, vehicle or train/airplane, respectively. The vehicular relay UE can have different antenna types for TN and NTN connectivity. The NTN access may operate in frequency bands below or above 6 GHz

5.4.1 Scope

The focus of the NTN-TN service continuity and mobility studies should be on mechanisms to minimize specification impact for cases where UE's connectivity changes from the NTN to TN ('hand-in') and where UE's connectivity changes from the TN to NTN ('hand-out'). Coverage mechanisms, including inter-frequency and intra-frequency service

continuity and mobility mechanisms are to be considered as baseline solutions. The NR Release 15-16 service continuity and mobility mechanisms shall be considered also for the NTN-TN service continuity and mobility studies.

5.4.2 Reference scenario

It is recommended to use a reference scenario for NTN-TN service continuity and mobility studies, defined as follows:

- A multi-cell TN network-border coverage is available according to an outdoor rural NR scenario (e.g. Table 6.1.3-1 in TR 38.913)
- One NTN LEO satellite provides multi-cell coverage with moving cells on Earth (the satellite NR cells are modelled according to NTN assumptions, Table 6.1.1-1 & 4 in TR38.821)
- Outdoor handheld (pedestrian) UEs or VSAT (vehicular relay) UEs are capable of TN and NTN connectivity (for NTN UE use Table 6.1.1-3 in TR 38.821)

5.4.3 Assumptions

The NTN-TN service continuity and mobility mechanisms targeted to minimizing UE power consumption, e.g. DRX enhancement solutions are only a secondary priority.

The study of dual-connectivity mechanisms between NTN and TN, in the baseline NTN-TN service continuity and mobility solutions is a secondary priority.

6 Radio Layer 1 issues and related solutions

6.1 Link-Level and System-Level Evaluations

Both multi-satellite and single satellite simulations should be considered for calibration and performance evaluation.

6.1.1 System level simulations

6.1.1.1 Simulation assumptions

The following tables representing two sets of satellite parameters are considered as the baseline for system level simulator calibration:

Table 6.1.1.1-1: Set-1 satellite parameters for system level simulator calibration

Satellite orbit	GEO	LEO-1200	LEO-600
Satellite altitude	35786 km	1200 km	600 km
Satellite antenna pattern	Section 6.4.1 in [2]	Section 6.4.1 in [2]	Section 6.4.1 in [2]
Payload characteristics for DL transmissions			
Equivalent satellite antenna aperture (Note 1)	S-band (i.e. 2 GHz)	22 m	2 m
Satellite EIRP density		59 dBW/MHz	40 dBW/MHz
Satellite Tx max Gain		51 dBi	30 dBi
3dB beamwidth		0.4011 deg	4.4127 deg
Satellite beam diameter (Note 2)		250 km	90 km
Equivalent satellite antenna aperture (Note 1)	Ka-band (i.e. 20 GHz for DL)	5 m	0.5 m
Satellite EIRP density		40 dBW/MHz	10 dBW/MHz
Satellite Tx max Gain		58.5 dBi	38.5 dBi
3dB beamwidth		0.1765 deg	1.7647 deg
Satellite beam diameter (Note 2)		110 km	40 km
Payload characteristics for UL transmissions			
Equivalent satellite antenna aperture (Note1)	S-band (i.e. 2 GHz)	22 m	2 m
G/T		19 dB K ⁻¹	1.1 dB K ⁻¹
Satellite Rx max Gain		51 dBi	30 dBi
Equivalent satellite antenna aperture (Note1)	Ka-band (i.e. 30 GHz for UL)	3.33 m	0.33 m
G/T		28 dB K ⁻¹	13 dB K ⁻¹
Satellite RX max Gain		58.5 dBi	38.5 dBi

NOTE 1: This value is equivalent to the antenna diameter in Sec. 6.4.1 of [2].
 NOTE 2: This beam size refers to the Nadir pointing of the satellite.
 NOTE 3: All these satellite parameters are applied per beam.
 NOTE 4: The EIRP density values are considered identical for all frequency re-use factor options.
 NOTE 5: The EIRP density values are provided assuming the satellite HPA is operated with a back-off of [5] dB.

Table 6.1.1.1-2: Set-2 satellite parameters for system level simulator calibration

Satellite orbit	GEO	LEO-1200	LEO-600
Satellite altitude	35786 km	1200 km	600 km
Satellite antenna pattern	Section 6.4.1 in [2]	Section 6.4.1 in [2]	Section 6.4.1 in [2]
Payload characteristics for DL transmissions			
Equivalent satellite antenna aperture (Note 1)	S-band (i.e. 2 GHz)	12 m	1 m
Satellite EIRP density		53.5 dBW/MHz	34 dBW/MHz
Satellite Tx max Gain		45.5 dBi	24 dBi
3dB beamwidth		0.7353 deg	8.8320 deg
Satellite beam diameter (Note 2)		450 km	190 km
Equivalent satellite antenna aperture (Note 1)	Ka-band (i.e. 20 GHz for DL)	2 m	0.2 m
Satellite EIRP density		32 dBW/MHz	2 dBW/MHz
Satellite Tx max Gain		50.5 dBi	30.5 dBi
3dB beamwidth		0.4412 deg	4.4127 deg
Satellite beam diameter (Note 2)		280 km	90 km
Payload characteristics for UL transmissions			
Equivalent satellite antenna aperture (Note1)	S-band (i.e. 2 GHz)	12 m	1 m
G/T		14 dB K ⁻¹	-4.9 dB K ⁻¹
Satellite Rx max Gain		45.5 dBi	24 dBi
Equivalent satellite antenna aperture (Note1)	Ka-band (i.e. 30 GHz for UL)	1.33 m	0.13 m
G/T		20 dB K ⁻¹	5 dB K ⁻¹
Satellite Rx max Gain		50.5 dBi	30.5 dBi
NOTE 1: This value is equivalent to the antenna diameter in Sec. 6.4.1 of [2].			
NOTE 2: This beam size refers to the Nadir pointing of the satellite			
NOTE 3: All these satellite parameters are applied per beam.			
NOTE 4: The EIRP density values are considered identical for all frequency re-use factor options.			

The following table is agreed for UE characteristics for System Level Simulations

Table 6.1.1.1-3: UE characteristics for system level simulations

Characteristics	VSAT (Note 2)	Handheld	Other (Note 1)
Frequency band	Ka band(i.e. 30 GHz UL and 20 GHz DL)	S band (i.e. 2 GHz)	Ka band(i.e. 30 GHz UL and 20 GHz DL)
Antenna type and configuration	Directional Section 6.4.1 of [2] with 60 cm equivalent aperture diameter	(1, 1, 2) with omni-directional antenna element	Directional (M,N,P,Mg,Ng) = (TBD,TBD,2,1,1); (dV,dH) = (TBD, TBD) λ with directional antenna element (HPBW=65 deg)
Polarisation	circular	Linear: +/-45°X-pol	Linear: +/-45°X-pol
Rx Antenna gain	39.7 dBi	0 dBi per element	TBD dBi per element
Antenna temperature	150 K	290 K	TBD K
Noise figure	1.2 dB	7 dB	TBD dB
Tx transmit power	2 W (33 dBm)	200 mW (23 dBm)	[TBD W (TBD dBm)]
Tx antenna gain	43.2 dBi	0 dBi per element	TBD dBi per element
NOTE 1: Moving platforms (e.g., aircrafts, vessels), building mounted devices. These values are provided for information.			
NOTE 2: VSAT terminal characteristics could be implemented with phased array antenna			

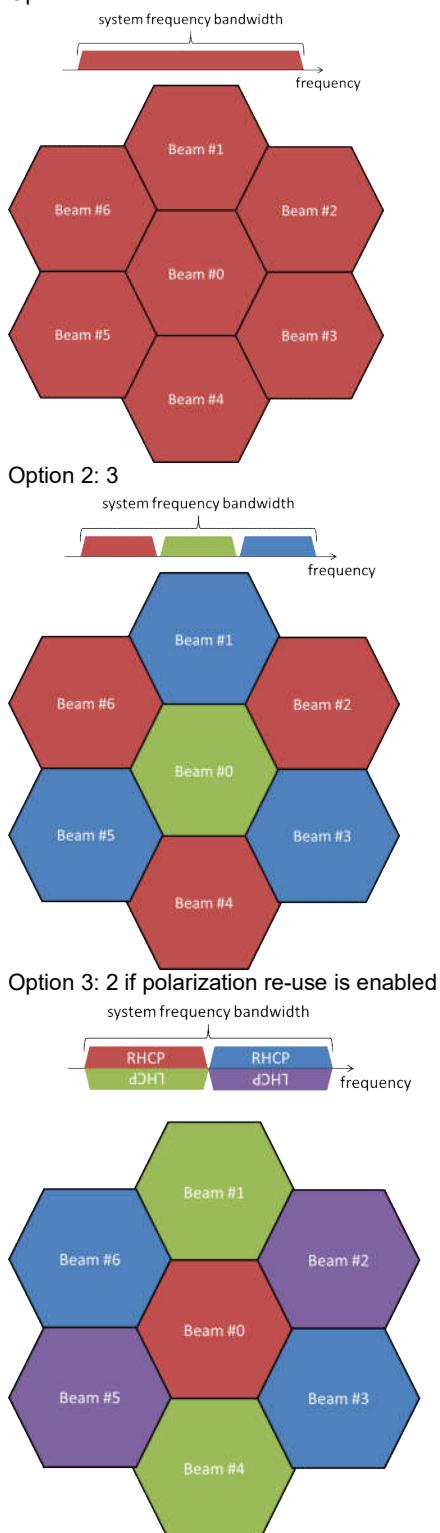
The following table is agreed for the beam layout definition for a single satellite simulation

Table 6.1.1.1-4: Beam layout definition for single satellite simulation

Scenario	Scenario A, C2 and D2
Beam layout definition	<p>Baseline: Hexagonal mapping of the beam bore sight directions on UV plane defined in the satellite reference frame.</p> <p>Only the 3dB beam width parameters should be used. The beam diameter and beam spacing values can be computed directly from the 3 dB beam width assumptions and should be considered as informative.</p>
Number of beams	Baseline: 19-beam layout considering wrap-around mechanism (i.e. 18 beams surrounding the central beam and allocated on 2 distinct "tiers")
UV plane illustration (extracted from [19])	<p>Spherical Coordinate System</p> <p>Projection of Coordinate System On the X-Y Plane (view from above Z-axis)</p> <p>Unit Circle</p> <p>Direction Cosines</p> $\begin{cases} u = \sin \theta \cos \phi \\ v = \sin \theta \sin \phi \end{cases}$
UV plane convention	<p>U axis is defined as the perpendicular line to the satellite-earth line on the orbital plane as illustrated here after:</p> <p>The straight line being orthogonal to UV plane is pointing towards the Earth centre. UV coordinates of the nadir of the reference satellite is (0,0)</p>
Adjacent beam spacing on UV plane	Baseline: Adjacent beam spacing computation based on 3dB beam width of the satellite antenna pattern: $ABS = \sqrt{3} \times \sin(HPBW/2 \text{ [rad]})$
Central beam bore sight direction definition	Baseline: Case 1: Central beam center is considered at nadir point Case 2: Central beam boresight direction computed based on elevation angle target

Table 6.1.1.1-5: System Level Simulation assumptions for calibration

Configuration scenario	A, C2 and D2
Frequency band	S-band (i.e. 2 GHz) / Ka-band (i.e. 20 GHz DL, 30 GHz UL)
Maximum Bandwidth per beam (DL + UL)	S-band: DL 30 MHz and UL 30 MHz Ka-band: DL 400 MHz and UL 400 MHz The bandwidth per beam must be adapted based on the frequency factor and the polarization re-use option considered.
Satellite characteristics (G/T, EIRP density, antenna diameter)	See Table 6.1.1.1-1 and Table 6.1.1.1-2 Note: Same satellite characteristics should be considered for both single and multi-satellite simulations
Satellite antenna pattern	See section 6.4.1 in [2]: Bessel function
Satellite polarization configuration	Circular
Beam layout definition	For singles satellite simulation: See Table 6.1.1.1-4 For multi satellites simulation: FFS

<p>Frequency re-use factor</p>	 <p>Option 1: 1</p> <p>system frequency bandwidth</p> <p>frequency</p> <p>Option 2: 3</p> <p>system frequency bandwidth</p> <p>frequency</p> <p>Option 3: 2 if polarization re-use is enabled</p> <p>system frequency bandwidth</p> <p>frequency</p>
<p>Polarization re-use</p>	<p>Option 1: Disable Option 2: Enable Note: Polarization re-use should apply only if circular polarization for terminal antenna is considered</p>
<p>Channel model</p>	<p>Large scale model of [2] (Note 2)</p>
<p>Deployment scenarios</p>	<p>Base-line: Rural Additional deployment scenario results can be provided</p>

Propagation conditions	Base-line: Clear Sky Line of sight
UEs outdoor/indoor distribution	100% outdoor distribution for UEs
UE distribution	Base-line for calibration: at least X=10 UEs per beam with uniform distribution in all the Voronoi cell area associated to each beam. The cell area associated to a given beam is defined as the Voronoi cell associated with the corresponding beam centers.
UE configuration	S-band: Handheld (optional for scenario A) Ka-band: VSAT Others (optional for scenario A) See Table 6.1.1.1-3
UE orientation	VSAT and Others: Ideal Tracking serving beam; Handheld: Random
Handover Margin	0 dB
UE attachment	RSRP
Metrics for calibration	Base-line: Coupling loss, Geometry Note: Coupling loss is defined as the signal loss from the antenna port to the antenna port
NOTE 1: Typical impairment values (additional frequency error, SNR loss) due to the feeder link except for delay can be considered to be negligible. When available, specific values can be considered in the evaluation and should be reported.	
NOTE 2: For the calibration purpose, the ionospheric scintillation loss shall be considered equal to zero (i.e., the UEs are located between 20 and 60 degrees of latitude). The atmospheric absorptions loss shall be considered.	

Traditionally, the wrap around mechanism used in system level simulations refers to a mirroring effect of the surrounding cells/beams so that the computational load of the simulations can be reduced. However, these types of schemes are not applicable in NTN context except in the specific case of central beam at nadir (90° elevation). Therefore, for the evaluation, all the additional surrounding beams should be simulated independently.

As a consequence, a new wrap around mechanism is introduced in case of single satellite simulation for intra-satellite interference modelling based on additional bore-sight beam directions which should be computed based on the methodology captured in Table 6.1.1.1-4.

In particular, the following wrap-around mechanism should be adopted for calibration:

- For FRF = 1, two additional tiers of beams are considered in the simulation surrounding the 19-beam layout (cf. Figure 6.1.1.1-1 – FRF=1).
- For FRF > 1, four additional tiers of beams are considered in the simulation surrounding the 19-beam layout (cf. Figure 6.1.1.1-1 – FRF=3).
- Considering a UE attached to a beam, in the DL/UL all remaining beams are treated as interference as long as these beams are sharing the same frequency band/polarization (cf. Figure 6.1.1.1-2).

For the metrics statistic (e.g. coupling loss, geometry), only the UEs placed in the inner-19 beams are considered.

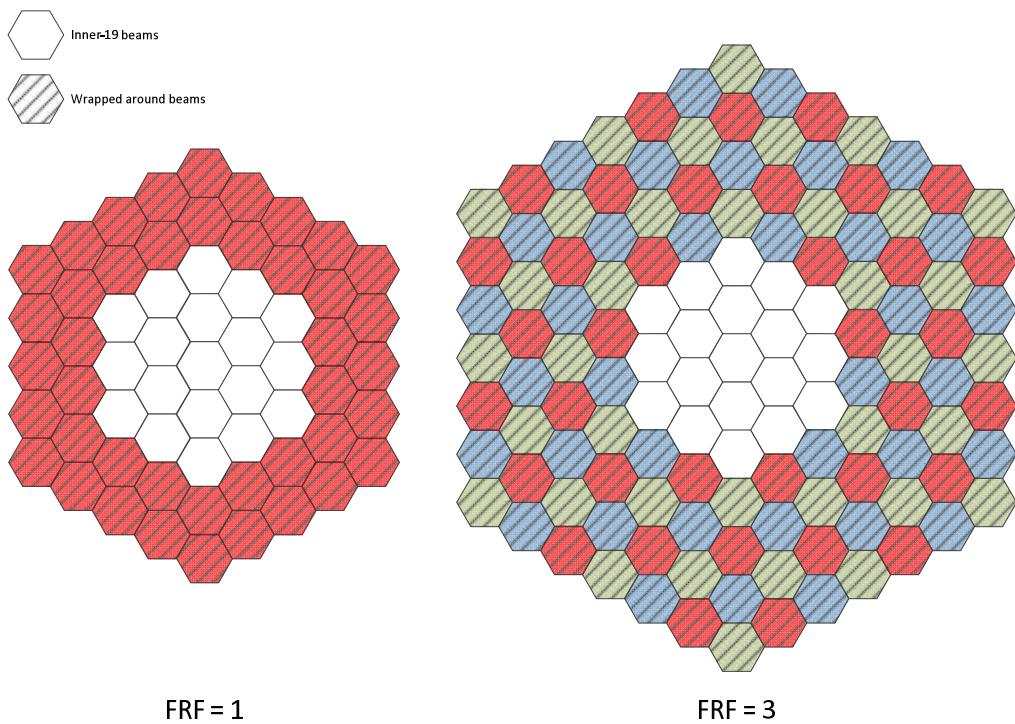


Figure 6.1.1.1-1: Illustrations of the additional tiers of beams to be wrapped around based on the FRF configurations

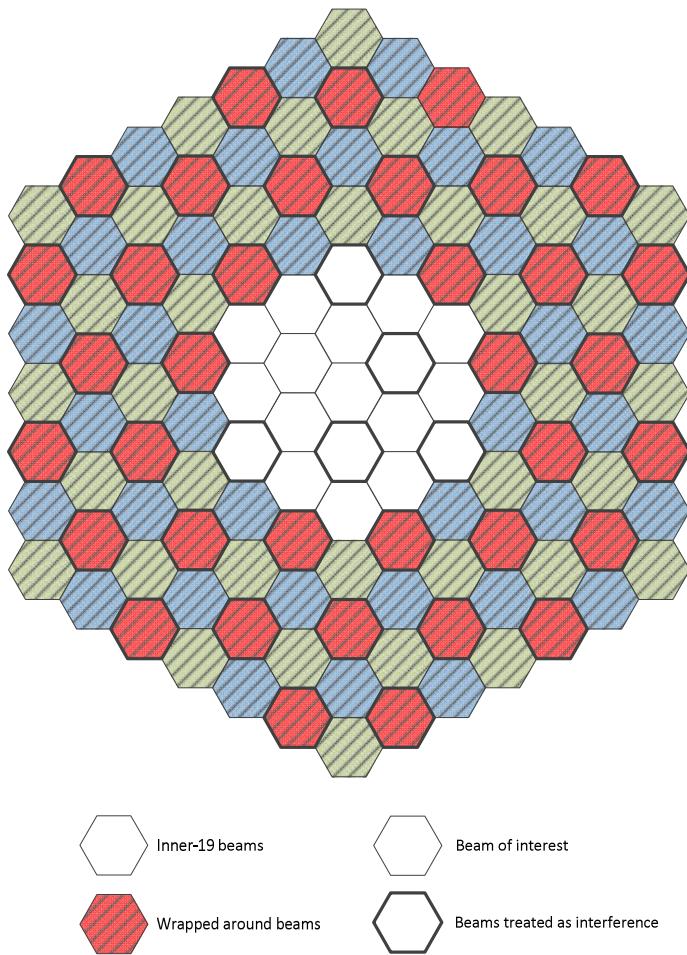


Figure 6.1.1.1-2: Definition of the interfering beams to be considered

The beam layout parameters captured in the following table are adopted as a starting point for single satellite simulations.

Table 6.1.1.1-6: Beam layout parameters for single satellite simulation

Scenario	Scenario A	Scenario C2/D2
Carrier frequency	S-band: 2 GHz Ka-band: 20 GHz for DL	S-band: 2 GHz Ka-band: 20 GHz for DL
Adjacent beam spacing (ABS) on UV plane	S-band: Set 1: ABS = 0.0061 Set 2: ABS = 0.0111 Ka-band: Set 1: ABS = 0.0027 Set 2: ABS = 0.0067	S-band: Set 1: ABS = 0.0668 Set 2: ABS = 0.1334 Ka-band: Set 1: ABS = 0.0267 Set 2: ABS = 0.0667
Satellite location	Any position on the geostationary orbit	Any position on the LEO orbit
Central beam center elevation angle target	Baseline: 45 deg	Baseline: 90 deg
Central beam bore sight direction coordinates in UV plane	Baseline: (0.107,0)	Baseline: (0,0)
Gateway direction coordinates in UV plane	Baseline: Same as central beam bore sight direction coordinates in UV plane Note: Not needed for calibration	

For handheld terminal, the following association between antenna port and antenna element is assumed for calibration, evaluations and link budgets calculation:

- 1 TX with one antenna element associated to one Tx branch.
- 2 RX with each antenna element associated to one Rx branch.

NOTE: Implementations without the above association can be evaluated in addition

As a consequence, the following considerations are assumed for handheld use cases:

- For downlink transmission, a combination of the two Rx branches allows to prevent depolarization loss. (cf. Figure 6.1.1.1-3)
- For uplink transmissions,
 - A 3dB depolarization loss should be taken into account assuming polarization reuse is applied and satellite reception implements circular polarization (e.g., when frequency reuse option 3 is considered) (cf. Figure 6.1.1.1-4 – configuration A)
 - A 0dB depolarization loss can be assumed when satellite reception implements dual polarization per beam (e.g., for the frequency reuse 1 and 3 cases) (cf. Figure 6.1.1.1-4 – configuration B)

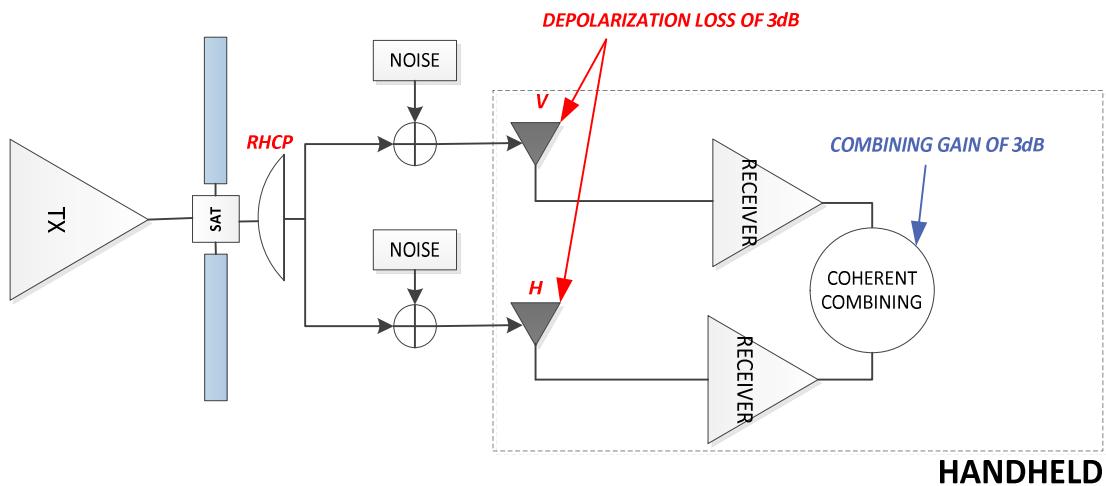


Figure 6.1.1.1-3: Example of DL RX/TX configuration for handheld use cases

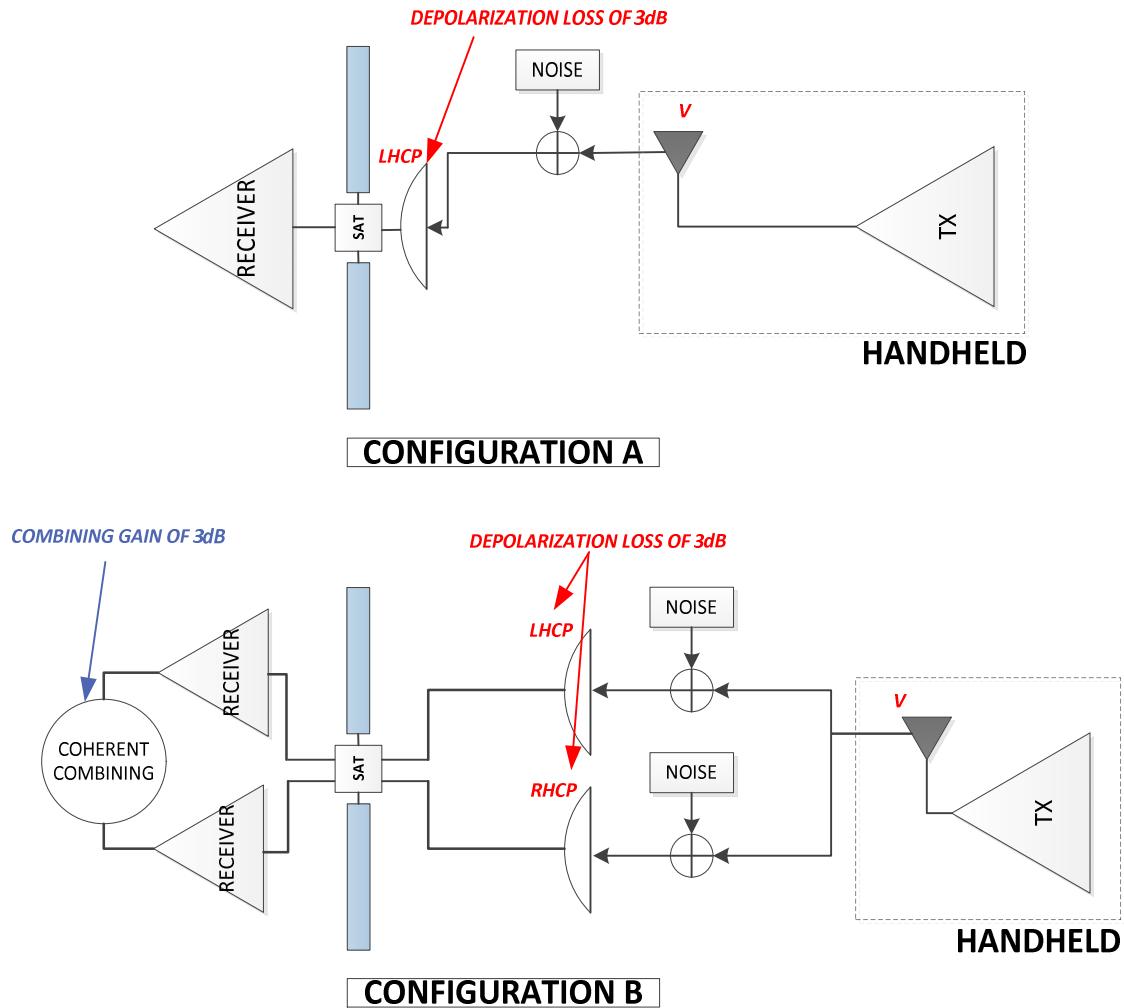


Figure 6.1.1.1-4: Example of UL RX/TX configurations for handheld use cases

For VSAT use cases, calibration results and link budgets should be computed assuming no depolarization loss.

Table 6.1.1.1-7: SLS parameters for performance evaluation

Configuration scenario	A, C2 and D2
Frequency band	Same as in Table 6.1.1.1-5
Maximum Bandwidth per beam (DL + UL)	Same as in Table 6.1.1.1-5
Satellite characteristics (G/T, EIRP density, antenna diameter)	Same as in Table 6.1.1.1-5
Satellite antenna pattern	Same as in Table 6.1.1.1-5
Satellite polarization configuration	Same as in Table 6.1.1.1-5
Beam layout	Same as in Table 6.1.1.1-5
Number of beams	Same as in Table 6.1.1.1-5
Frequency re-use factor	Same as in Table 6.1.1.1-5
Polarization re-use	Same as in Table 6.1.1.1-5
Deployment scenarios	Same as in Table 6.1.1.1-5
Fast fading model	Frequency selective channel model listed in [2]
Propagation conditions	Same as in Table 6.1.1.1-5
UEs outdoor/indoor distribution	Same as in Table 6.1.1.1-5
UEs coverage distribution	Same as in Table 6.1.1.1-5
UE configuration	Same as in Table 6.1.1.1-5
UE orientation	Same as in Table 6.1.1.1-5
Handover Margin	To be reported by the companies
UE attachment	RSRP
Receiver type	MMSE-IRC
Scheduler	To be reported by the companies
Traffic model	FTP 3 (see TR 38.802) packet size = 0.5 Mbyte
Channel estimation	Realistic
CSI feedback	Release 15 (Note 2)
Metrics for performance	Baseline: UE throughput (5%, 50%, 95%) at 20% and [50 or 60]% RU (Note 4)
NOTE 1:	Typical impairment values (additional frequency error, SNR loss) due to the feeder link except for delay can be considered to be negligible. When available, specific values can be considered in the evaluation and should be reported.
NOTE 2:	The impact of RTT should be considered for evaluation
NOTE 3:	The overhead due to control channel and RS can be reported by the companies [e.g. 4/14]
NOTE 4:	The bandwidth used for RU calculation is based on the allocated bandwidth for each beam

The following table captures the impairments introduced on the RF signal due to the satellite payload and movement for link level simulations.

Table 6.1.1.1-8: Impairments due to satellite payload and satellite movement

	S-band	Ka-band
Phase noise model (Note 2)	Optional	Phase noise profile according to TR38.803
On-board oscillator long-term drift (Note 3)	[0.5] ppm	[0.5] ppm
Max Doppler shift (Note 1)	Scenario A: 0.15 ppm Scenario C2/D2: <ul style="list-style-type: none">• 1200 km: 20 ppm• 600 km: 24 ppm	
Max Doppler shift if pre/post compensation mechanism is assumed at satellite payload side	Scenario A: n/a Scenario C2/D2: <ul style="list-style-type: none">• Satellite alt. = 1200 km<ul style="list-style-type: none">- beam diameter = 90 km (Set 1 - S-band): 0.91 ppm	

	<ul style="list-style-type: none"> - beam diameter = 40 km (Set 1 - Ka-band): 0.40 ppm - beam diameter = 190 km (Set 2 - S-band): 1.91 ppm - beam diameter = 90 km (Set 2 - Ka-band): 0.91 ppm - beam diameter = 1000 km (Max beam foot print size): 9.17 ppm ● Satellite alt. = 600 km - beam diameter = 50 km (Set 1 - S-band): 1.05 ppm - beam diameter = 20 km (Set 1 - Ka-band): 0.42 ppm - beam diameter = 90 km (Set 2 - S-band): 1.88 ppm - beam diameter = 50 km (Set 2 - Ka-band): 1.05 ppm - beam diameter = 1000 km (max beam foot print size): 15.82 ppm
Max Doppler rate	<p>Scenario A: n/a</p> <p>Scenario C2/D2:</p> <ul style="list-style-type: none"> ● 0.09 ppm/s for 1200 km satellite altitude ● 0.27 ppm/s for 600 km satellite altitude
<p>NOTE 1: Min. Elevation angle for both sat- user equipment is equal to 10 degree.</p> <p>NOTE 2: For regenerative scenario, this can be considered as the phase noise model for the gNB. For transparent scenarios, it should be considered as an additional phase noise w.r.t the phase noise generated by the gNB and the UE.</p> <p>NOTE 3: These values are provided for information only and have not been considered in Radio Layer 1 analysis for the following reasons: 1) In the cases where transparent satellite payload are considered, it is assumed that the gNB can detect the frequency shift due to on -board oscillator long-term drift and compensate for it. 2) In the cases where regenerative satellite payload are considered, it is assumed that the on -board oscillator drift is sufficiently decreased to become negligible.</p>	

Table 6.1.1.1-9: List of calibration study cases

Case	Satellite orbit	Satellite parameter set	Central beam elevation	Terminal	Frequency Band	Frequency/Polarization Reuse
1	GEO	Set 1	45 deg	VSAT	Ka-band	Option 1
2	GEO	Set 1	45 deg	VSAT	Ka-band	Option 2
3*	GEO	Set 1	45 deg	VSAT	Ka-band	Option 3
4*	GEO	Set 1	45 deg	Handheld	S-band	Option 1
5*	GEO	Set 1	45 deg	Handheld	S-band	Option 2
6	LEO-600	Set 1	90 deg	VSAT	Ka-band	Option 1
7	LEO-600	Set 1	90 deg	VSAT	Ka-band	Option 2
8*	LEO-600	Set 1	90 deg	VSAT	Ka-band	Option 3
9	LEO-600	Set 1	90 deg	Handheld	S-band	Option 1
10	LEO-600	Set 1	90 deg	Handheld	S-band	Option 2
11*	LEO-1200	Set 1	90 deg	VSAT	Ka-band	Option 1
12*	LEO-1200	Set 1	90 deg	VSAT	Ka-band	Option 2
13*	LEO-1200	Set 1	90 deg	VSAT	Ka-band	Option 3
14	LEO-1200	Set 1	90 deg	Handheld	S-band	Option 1
15	LEO-1200	Set 1	90 deg	Handheld	S-band	Option 2
16**	GEO	Set 2	45 deg	VSAT	Ka-band	Option 1
17**	GEO	Set 2	45 deg	VSAT	Ka-band	Option 2
18**	GEO	Set 2	45 deg	VSAT	Ka-band	Option 3
19**	GEO	Set 2	45 deg	Handheld	S-band	Option 1
20**	GEO	Set 2	45 deg	Handheld	S-band	Option 2
21**	LEO-600	Set 2	90 deg	VSAT	Ka-band	Option 1
22**	LEO-600	Set 2	90 deg	VSAT	Ka-band	Option 2
23**	LEO-600	Set 2	90 deg	VSAT	Ka-band	Option 3
24**	LEO-600	Set 2	90 deg	Handheld	S-band	Option 1
25**	LEO-600	Set 2	90 deg	Handheld	S-band	Option 2
26**	LEO-1200	Set 2	90 deg	VSAT	Ka-band	Option 1
27**	LEO-1200	Set 2	90 deg	VSAT	Ka-band	Option 2
28**	LEO-1200	Set 2	90 deg	VSAT	Ka-band	Option 3
29**	LEO-1200	Set 2	90 deg	Handheld	S-band	Option 1
30**	LEO-1200	Set 2	90 deg	Handheld	S-band	Option 2

NOTE 1: no star = 1st priority, * = second priority scenario, ** = third priority scenario
 NOTE 2: Only 1st priority cases will be considered for calibration phase 1

6.1.1.2 Calibration results

Based on System Level Simulation assumptions for calibration described in Table 6.1.1.1-5, the results of CL, Geometry SIR and Geometry SINR simulated on DL and UL transmissions are reported in Table 6.1.1.2-1 and Table 6.1.1.2-2. These results are representative of the average performance reported by the different companies in [20] [21].

Table 6.1.1.2-1: Calibration results on DL transmissions

	DL Coupling Loss			DL Geometry SIR			DL Geometry SINR		
	@5%	@50%	@95%	@5%	@50%	@95%	@5%	@50%	@95%
SC1	109.3	113.6	117.9	-3.0	-1.0	1.2	-3.2	-1.2	1.0
SC2	109.2	113.6	118.0	8.4	9.0	9.2	5.5	7.4	8.4
SC3	109.3	113.7	118.0	9.7	10.0	10.2	6.0	8.1	9.2
SC4	138.0	140.3	142.5	-3.1	-1.1	1.1	-4.0	-2.1	-0.1
SC5	138.0	140.3	142.5	8.0	8.9	9.2	1.5	3.3	4.9
SC6	96.2	97.5	98.9	-3.0	-1.1	1.1	-3.2	-1.2	0.8
SC7	96.2	97.5	98.9	8.3	9.0	9.2	6.6	7.6	7.8
SC8	96.2	97.5	98.9	9.7	9.9	10.1	7.5	8.1	8.5
SC9	123.7	125.3	127.0	-3.0	-1.1	1.1	-3.1	-1.1	1.0
SC10	123.7	125.3	127.0	8.3	9.0	9.2	7.3	8.2	8.5
SC11	102.2	103.5	105.0	-3.0	-1.1	1.1	-3.2	-1.2	0.8
SC12	102.2	103.5	105.0	8.3	9.0	9.2	6.6	7.6	7.8
SC13	102.2	103.5	105.0	9.7	9.9	10.1	7.5	8.1	8.5
SC14	129.8	131.3	133.0	-3.0	-1.1	1.1	-3.1	-1.1	1.0
SC15	129.8	131.4	133.0	8.3	9.0	9.2	7.3	8.2	8.5
SC16	117.3	121.7	126.0	-3.0	-1.0	1.2	-4.3	-2.2	0.0
SC17	117.3	121.7	126.0	8.3	9.0	9.2	-0.3	3.2	6.0
SC18	117.4	121.8	126.1	9.7	10.0	10.1	-0.2	3.4	6.4
SC19	143.4	145.8	148.1	-3.1	-1.1	1.0	-5.9	-4.0	-2.1
SC20	143.4	145.8	148.1	8.3	9.1	9.5	-3.3	-1.2	0.9
SC21	100.3	105.5	111.1	-3.0	-1.1	1.1	-4.5	-2.3	-0.1
SC22	100.3	105.5	111.1	8.3	9.0	9.2	-1.3	3.4	6.4
SC23	100.4	105.6	111.1	9.7	9.9	10.1	-1.2	3.5	6.9
SC24	129.8	131.5	133.3	-3.0	-1.0	1.2	-3.3	-1.4	0.7
SC25	129.8	131.5	133.3	8.3	8.9	9.3	5.0	6.2	6.9
SC26	106.1	111.6	117.3	-3.0	-1.1	1.1	-4.6	-2.3	0.0
SC27	106.1	111.6	117.2	8.3	9.0	9.2	-1.4	3.3	6.5
SC28	106.2	111.6	117.3	9.7	9.9	10.1	-1.4	3.5	7.0
SC29	135.8	137.6	139.4	-3.0	-1.0	1.2	-3.3	-1.4	0.7
SC30	135.8	137.6	139.4	8.3	8.9	9.3	5.0	6.2	6.9

NOTE: Geometry SINR = $-10\log_{10}(I/C + N/C)$, where C, I and N equals the carrier, interferer and noise power levels measured over the configured signal bandwidth.

Table 6.1.1.2-2: Calibration results on UL transmissions

	UL Coupling Loss			UL Geometry SIR			UL Geometry SINR		
	@5%	@50%	@95%	@5%	@50%	@95%	@5%	@50%	@95%
SC1	109.2	113.5	117.8	-6.9	-1.3	4.4	-7.0	-1.5	1.0
SC2	109.2	113.5	117.8	3.6	8.3	12.9	3.1	7.6	12.2
SC3	109.2	113.5	117.8	4.5	9.3	14.1	3.5	8.1	12.7
SC4	137.9	140.2	142.5	-4.6	-1.0	3.3	-9.8	-7.3	-5.0
SC5	138.0	140.3	142.5	8.0	8.9	9.2	1.5	3.3	4.9
SC6	96.1	97.4	98.8	-3.9	-1.1	2.6	-3.9	-1.1	2.6
SC7	96.1	97.4	98.8	6.1	8.3	10.4	6.1	8.3	10.4
SC8	96.1	97.4	98.8	6.9	9.3	11.6	6.9	9.3	11.5
SC9	123.7	125.3	127.1	-4.0	-0.8	3.2	-4.1	-1.1	2.7
SC10	123.7	125.4	127.1	6.9	9.0	11.1	5.2	7.1	9.0
SC11	102.2	103.4	104.8	-4.0	-1.1	2.6	-4.0	-1.2	2.5
SC12	102.2	103.4	104.8	5.9	8.2	10.4	5.9	8.2	10.3
SC13	102.2	103.4	104.8	6.7	9.2	11.6	6.7	9.2	11.5
SC14	129.7	131.4	133.1	-4.0	-0.8	3.2	-4.5	-1.7	1.5
SC15	129.7	131.4	133.1	6.9	9.0	11.1	2.3	4.1	5.8
SC16	117.2	121.5	125.8	-6.7	-1.2	4.5	-7.6	-2.6	2.5
SC17	117.2	121.5	125.8	3.7	8.3	12.9	0.9	5.3	9.6
SC18	117.2	121.5	125.8	4.5	9.3	14.1	0.3	4.7	9.0
SC19	143.4	145.7	148.1	-4.6	-0.9	3.5	-13.9	-11.6	-9.3
SC20	143.4	145.7	148.1	6.3	9.1	11.8	-13.6	-11.2	-8.9
SC21	100.1	105.4	111.0	-8.3	-1.6	4.9	-8.3	-1.6	4.9
SC22	100.1	105.4	111.0	2.2	8.0	13.7	2.1	7.9	13.7
SC23	100.1	105.4	111.0	3.0	9.0	14.9	3.0	8.9	14.8
SC24	129.8	131.5	133.4	-3.9	-0.7	3.5	-4.5	-1.6	1.7
SC25	129.8	131.6	133.4	7.1	9.3	11.6	2.1	4.0	5.9
SC26	106.0	111.4	117.1	-8.5	-1.6	5.0	-8.5	-1.7	4.9
SC27	106.0	111.4	117.1	2.0	8.0	13.9	1.9	7.9	13.8
SC28	106.0	111.4	117.1	2.9	9.0	15.1	2.7	8.7	14.8
SC29	135.8	137.6	139.5	-4.0	-0.7	3.5	-6.0	-3.6	-1.2
SC30	135.8	137.6	139.5	7.2	9.4	11.7	-2.8	-0.9	0.9

NOTE: Geometry SINR = $-10\log_{10}(I/C + N/C)$, where C, I and N equals the carrier, interferer and noise power levels measured over the configured signal bandwidth.

6.1.1.3 System Level Simulation Evaluation Results

Two companies have provided DL user throughput performance results based on single satellite SLS assumptions, see Section 6.1.1.1.

One source provided results for 8 different study cases for 20% and ~50% target resource utilization (RU), see Table 6.1.1.3-1. Additional assumptions are 10UEs per cell, proportional fair scheduling. LOS probability is according to Table 6.6.1-1 in TR 38.811. The used deployment scenario is rural. The number of HARQ processes is assumed to be RTT/T_slot.

Table 6.1.1.3-1: SLS UE throughput performance in Mbit/s [22]

Study case	GEO, Ka-band		LEO-600, Ka-band		LEO-600, S-band		LEO-1200, S-band	
	1	2	6	7	9	10	14	15
RU=20%	5%	0.96	0.48	2.04	1.02	0.11	0.03	0.11
	50%	2.7	2.05	4.08	2.78	0.31	0.15	0.3
	95%	4.93	3.9	6.43	4.7	0.52	0.34	0.52
RU~50%	5%	5.34	4.03	6.91	4.76	0.44	0.3	0.4
	50%	8.53	6.61	10.03	7.75	0.74	0.58	0.78
	95%	11.99	9.99	13.7	11.22	1.09	0.88	1.09

One source provided results for LEO-1200 S-Band with no frequency reuse (Study case 14) with 20% resource utilization, see Table 6.1.1.3-2. Additional assumptions are 10UEs per cell, proportional fair scheduling and 16 parallel HARQ processes. LOS probability is according to Table 6.6.1-1 in TR 38.811. The used deployment scenario is rural.

Table 6.1.1.3-2: SLS UE throughput performance in Mbit/s [23]

Study case	LEO-1200, S-band		
	14	5%	0.2
RU=20%	50%	0.31	
	95%	0.44	

6.1.2 Link level simulations

The following table provides the LLS parameters for DL synchronization performance evaluation

Table 6.1.2-1: LLS parameters for DL synchronization evaluation

	S-band	Ka-band
Carrier Frequency	2 GHz	20 GHz
Channel Model	For GEO (optional): Baseline TDL/CDL model in [2], with delay/angular scaling factors equals to the mean delay/angular spread and mean K factor for suburban LOS elevation angle 10 deg For LEO: Baseline TDL/CDL model in [2], with delay/angular scaling factors equals to the mean delay/angular spread and mean K factor for suburban LOS elevation angle [30] deg	
Subcarrier Spacing(s)	15kHz, 30kHz	120kHz, 240kHz
DL RS	SSB	
Antenna Configuration at the TRP (satellite)	1Tx	1Tx
Antenna Configuration at the UE	(1, 1, 2) with omni-directional antenna element	VSAT with 60 cm equivalent aperture diameter
UE speed	3 km/h	0 km/h, 1200 km/h
UE elevation angle	For GEO (optional): 10°, For LEO: 30°	
Frequency Offset	UE crystal accuracy: 10 ppm Satellite: oscillator accuracy values provided in Table 6.1.1.8 Doppler shift in channel due to satellite movement: max. Doppler shift values provided in Table 6.1.1.8 Doppler shift in channel due to UE movement: max. value to be computed based on the UE speed and the elevation angle Note 1: The final frequency offset is computed as follows $FO = (A_{UE} + DS_{sat} + DS_{UE}) \times 10^{-5} \times f_{service,DL}$ where: FO denotes the final frequency offset in Hz A _{UE} denotes the UE crystal accuracy in ppm DS _{sat} denotes Doppler shift due to satellite movement in ppm. Pre/post Doppler shift compensation can be assumed. DS _{UE} denotes the Doppler shift due to UE movement in ppm f _{service,DL} denotes the carrier frequency used on the service Down Link in Hz A uniform distribution in [- FO max value, + FO max value] shall be assumed. Note 2: Doppler spectrum on Rayleigh fading taps based on Jake model should be considered in addition to Doppler shift (see section 6.9.2 in [2]) Note 3: For a Rayleigh fading tap a minimum Doppler of 1 Hz should be considered.	
Frequency drift	[Doppler rate values provided in Table 6.1.1.8]	
Phase noise model	S-band phase noise modelling (optional) Ka-band phase noise modelling: phase noise profile according to TR38.803.	
Metrics	One-shot initial cell detection accuracy of PCID; CDF of timing and frequency residual offset at SNIR point corresponding to 90% likelihood for one-shot detection accuracy of cell ID. Note 4: FAR of PCID detection requirement = 1%	
NOTE: The SNR range to be evaluated should be based on the link budget analysis for each channel		

The following table provides the LLS parameters for PRACH performance evaluation.

Table 6.1.2-2: LLS parameters for PRACH performance evaluation

Configurations	S-band	Ka-band
Carrier Frequency	2 GHz	30 GHz
Channel Model	Baseline TDL/CDL-D model in [2], with delay/angular scaling factors equals to the mean delay/angular spread and mean K factor for suburban at corresponding elevation angle for each case	
Antenna Configuration at the TRP (satellite)	1 Rx 2 Rx optional	1 Rx 2 Rx optional
Antenna Configuration at the UE	Omni-directional antenna with single linearly polarized antenna element	VSAT with 60 cm equivalent aperture diameter
Frequency Offset	<p>Doppler shift in channel due to satellite movement; max. Doppler shift values provided in Table 6.1.1.1-8</p> <p>Doppler shift in channel due to UE movement; max. value to be computed based on the UE speed and the elevation angle</p> <p>Residual frequency offset after synchronization: [0.1] ppm</p> <p>Note 1: In case the network performs both pre and post common Doppler shift compensation, the final frequency offset is computed as follow:</p> $FO = (DS_{sat} \times 10^{-5} + DS_{UE} \times 10^{-5} + 1) \times (DS_{sat} \times 10^{-5} + DS_{UE} \times 10^{-5} + 1) \times (RO \times 10^{-5} + 1) \times f_{service,UL} - f_{service,LL}$ <p>where</p> <p>FO denotes the final frequency offset in Hz</p> <p>RO denotes the residual frequency offset after synchronization in ppm</p> <p>DS_{sat} denotes the residual Doppler shift due to satellite movement in ppm after common Doppler compensation</p> <p>DS_{UE} denotes the Doppler shift due to UE movement in ppm</p> <p>$f_{service,UL}$ denotes the central frequency used on the service Up Link in Hz</p> <p>A uniform distribution in [- FO max value, + FO max value] shall be assumed</p> <p>Note 2: Doppler spectrum on Rayleigh fading taps based on Jake model should be considered in addition to Doppler shift (see section 6.9.2 in [2])</p> <p>Note 3: For a Rayleigh fading tap a minimum Doppler of 1 Hz should be considered.</p>	
UE speed	3 km/h	0 km/h, 1000 km/h
Timing Offset	<p>A uniform distribution in [0 max differential delay] shall be assumed.</p> <p>Note 1: Ideal common delay compensation is assumed.</p> <p>Note 2: The maximal differential delay values that should be supported for NTN are provided in Table 4.2-2. The max differential delays expected for specific cases can be computed based on the half power beam width and the target elevation angle.</p>	
Phase noise model	S-band phase noise modelling (optional) Ka-band phase noise modelling: phase noise profile according to in TR38.803.	
PRACH design	Each company should provide details on configuration (i.e. format, SCS, N_CS, ...). New formats are not precluded.	
Metric	PRACH detection rate, FAR (Based on the preamble pool size is not less than 64), CDF of estimation error for frequency/timing,	
Receiver	Companies are encouraged to report the receiver for PRACH detection.	

Table 6.1.2-3: PRACH study cases

	Elevation angle	Differential delay	UL Frequency offset (Both S- and Ka-band) (with compensation of common Doppler)	Beam Set at satellite
Case 1	90 degree for LEO	Small	Large	Set-2
Case 2	45 degree for LEO	Medium	Medium	Set-2
Case 3	10 degree for GEO and 30 degree for LEO	Large	Small	Set-2
Case 4	With both open loop timing and frequency compensation	Small	Small	Set-2

NOTE 1: As the baseline, the number of UEs that simultaneously access the network in a single random access occasion (RO) is 2. The two UEs may have different timing offsets/Doppler, which are randomly picked within the [0 Max_differential_delay]/[-max_UL_frequency_offset max_UL_frequency_offset] per case;

NOTE 2: Fixed power offset between UEs is 3dB.

NOTE 3: The SINR of the stronger UE for simulation is based on the SNR from link budget (with bandwidth for UL = 1MHz for VSAT in Ka, and Handheld for S) with additional offset of [-6-10 log10(Bandwidth [MHz])] dB per case where the -6 dB degradation is introduced as additional margin.

The following table provides the LLS parameters for data transmission performance evaluation.

Table 6.1.2-4: LLS parameters for data transmission performance evaluation

Parameters	S-band	Ka-band
Carrier frequency	2 GHz	DL 20 GHz, UL 30 GHz
Channel coding scheme	NR channel coding	
Subcarrier spacing	15 kHz, 30 kHz	60 kHz, 120 kHz
Channel estimation	Realistic estimation	
Frequency offset	Residual Frequency error after DL synchronisation: [0.1] ppm assuming UL pre-compensation	
Frequency drift	[Doppler rate values provided in Table 6.1.1.1-8]	
Frequency tracking	Option 1: drift pre-compensation is assumed Option 2: no pre-compensation is assumed	
UE speed	3 km/h	0 km/h, 1000 km/h
Channel model	For GEO (optional): Baseline TDL/CDL model in [2], with delay/angular scaling factors equals to the mean delay/angular spread and mean K factor based on the selected channel conditions. These parameters should be provided by the companies. For LEO: Baseline TDL/CDL model in [2], with delay/angular scaling factors equals to the mean delay/angular spread and mean K factor based on the selected channel conditions. These parameters should be provided by the companies.	
Satellite antenna configuration	1Tx/Rx	1Tx/Rx
UE antenna configuration	(1, 1, 2) with omni-directional antenna element	VSAT with 60 cm equivalent aperture diameter
Phase noise Model	S-band phase noise modelling (optional) Ka-band phase noise modelling: phase noise profile according to TR 38.803	
Metrics	BLER, Throughput	

HPA non-linearity modelling is not considered as part of the baseline for link level simulations.

PAPR optimizations for downlink channels are not necessary to be specified for NTN at least for Rel-17.

6.1.3 Link Budget Analysis

6.1.3.1 Link Budget Calculation

Carrier-to-noise-and-interference ratio (CNIR) of transmission link between satellite and UE can be derived by carrier-to-noise ratio (CNR) and carrier-to-interference ratio (CIR) as follows

$$\text{CNIR [dB]} = 10\log_{10}(10^{-0.1\text{CNR [dB]}} + 10^{-0.1\text{CIR [dB]}}) \quad (6.1.3.1-1)$$

The formula for CNR calculation is

$$\text{CNR [dB]} = \text{EIRP [dBW]} + \frac{G}{T} [\text{dB/K}] - k [\text{dBW/K/Hz}] - PL_{FS} [\text{dB}] - PL_A [\text{dB}] - PL_{SM} [\text{dB}] - PL_{SL} [\text{dB}] - PL_{AD} [\text{dB}] - B [\text{dBHZ}] \quad (6.1.3.1-2)$$

where EIRP is effective isotropic radiated power (EIRP), G/T is antenna-gain-to-noise-temperature, k is Boltzmann constant and equals to -228.6 dBW/K/Hz, PL_{FS} is free space path loss, PL_A is atmospheric path loss due to gases and rain fades, PL_{SM} is shadowing margin, PL_{SL} is scintillation loss, PL_{AD} is additional loss, for example degradation due to feeder links in case of non-regenerative systems, and B is channel bandwidth.

Antenna-gain-to-noise-temperature G/T can be derived by [2]

$$G/T [\text{dB}] = G_R [\text{dBi}] - N_f [\text{dB}] - 10\log_{10}(T_0 [\text{K}] + (T_a [\text{K}] - T_0 [\text{K}])10^{-0.1N_f [\text{dB}]}) \quad (6.1.3.1-3)$$

where G_R is receive antenna gain, N_f is noise figure, T_0 is ambient temperature and T_a is antenna temperature. Receive antenna gain G_R can be obtained by

$$G_R [\text{dBi}] = \begin{cases} G_{R,e} [\text{dBi}] + 10\log_{10}(N_{R,a}) - L_p [\text{dE}], & \text{array antenna} \\ 10\log_{10}\left(\eta \cdot \pi^2 \cdot \frac{D[m]^2}{\lambda[m]^2}\right), & \text{parabolic antenna} \end{cases} \quad (6.1.3.1-4)$$

where $G_{R,e}$ is receive antenna element gain, $N_{R,a}$ is the number of receive antenna elements, L_p is polarization loss, η is the antenna aperture efficiency (a dimensionless parameter with typical values for parabolic antennas from 0.55 to 0.70), D is the equivalent antenna diameter, and λ is the wavelength.

EIRP can be calculated by

$$\text{EIRP [dBW]} = P_T [\text{dBW}] - L_C [\text{dB}] + G_T [\text{dBi}] \quad (6.1.3.1-5)$$

where P_T is antenna transmit power, L_C is cable loss, and G_T is transmit antenna gain and can be derived by

$$G_T [\text{dBi}] = \begin{cases} G_{T,e} [\text{dBi}] + 10\log_{10}(N_{T,a}), & \text{array antenna} \\ 10\log_{10}\left(\eta \cdot \pi^2 \cdot \frac{D[m]^2}{\lambda[m]^2}\right), & \text{parabolic antenna} \end{cases} \quad (6.1.3.1-6)$$

where $G_{T,e}$ is transmit antenna element gain and $N_{T,a}$ is the number of transmit antenna elements.

6.1.3.2 Parameters

The parameter configuration for link budget analysis is listed in Table 6.1.3.2-1.

Table 6.1.3.2-1: Parameter configuration for link budget analysis

Parameters	Notes
Carrier frequency	2 GHz for DL and UL (S-band), 20 GHz for DL and 30 GHz for UL (Ka-band)
System bandwidth	30 MHz (S-band), 400 MHz (Ka-band)
Channel bandwidth	DL: system bandwidth/ frequency reuse factor UL: UL in S-band (handheld UE): 360 kHz Otherwise: system bandwidth/ frequency reuse factor Note: The UL bandwidth may be a challenge.
Satellite altitude	600 km, 1200 km, 35786 km
Target elevation angle	30° (LEO), 12.5° (GEO-Set 1) , 20° (GEO –Set 2)
Atmospheric loss	Equation (6.6-8) in [2]
Shadowing margin	0 dB for VSAT as terminal and 3 dB for others
Scintillation loss	Section 6.6.6 in [2] Ionospheric loss: $A_{IS} = 2.2 \text{ dB}$ (note 1) Tropospheric loss: Table 6.6.6.2.1-1 of [2]
Additional loss	0 dB
Clear sky conditions	Yes
Frequency reuse factor	1, 2, 3
Average CIR within a satellite beam based on logarithmic mean	<p>Based on single satellite system-level calibration methodology, statistics for average CIR are only collected for the UEs located in the central beam of the 19-beamlayout. The central beam boresight direction is computed based on the target elevation angle assumption. When the generated beam has a partial or full coverage outside the earth, it is discarded.</p> <p>For DL calibration, CIR is computed by averaging CIR over UEs randomly distributed over the reference beam (UE distribution assumption of Table 6.1.1.1-5). (See Figure 6.1.3.2-1 for UE bandwidth allocation, and Figure 6.1.1.1-1 and Figure 6.1.1.1-2 for beam deployment).</p> <p>For UL calibration, For Handheld device, the channel bandwidth is 360 kHz. For VSAT, the channel bandwidth equals the system bandwidth allocated to each beam divided by 10. The devices in one beam are allocated on adjacent frequency resources. The same resource allocation is assumed for all the beams.</p> <p>CIR is computed by averaging over 10 simultaneously transmitting UEs randomly distributed over the reference beam (UE distribution assumption of Table 6.1.1.1-5). (See Figure 6.1.3.2-2 for UE bandwidth allocation, and Figure 6.1.1.1-1 and Figure 6.1.1.1-2 for beam deployment)</p> <p>The averaging should be performed over multiple realizations.</p>
Satellite antenna polarization	Circular polarization
Polarization reuse	Enable if frequency reuse factor = 2 is considered.
Terminal type	Ka-band: VSAT S band: (M, N, P) = (1,1,2)
Free space path loss	Equation (6.6-2) in [2]
Terminal RF parameters	Table 6.1.1-3
Satellite RF parameters	Set-1 in Table 6.1.1-1 and Set-2 in Table 6.1.1-2
Polarization loss	The considerations of Section 6.1.1.1 on Polarization loss apply.
Outcome	CNIR
NOTE 1: Based on P3 curve for 1% of time from Figure 6.6.6.1.4-1 of [2] after frequency scaling.	
$A_{IS} = P_{fluc} @ 4\text{GHz} \times 0.5^{-1.5} / \sqrt{2} = 1.1 \times 0.5^{-1.5} / \sqrt{2} = 2.2 \text{ dB}$	

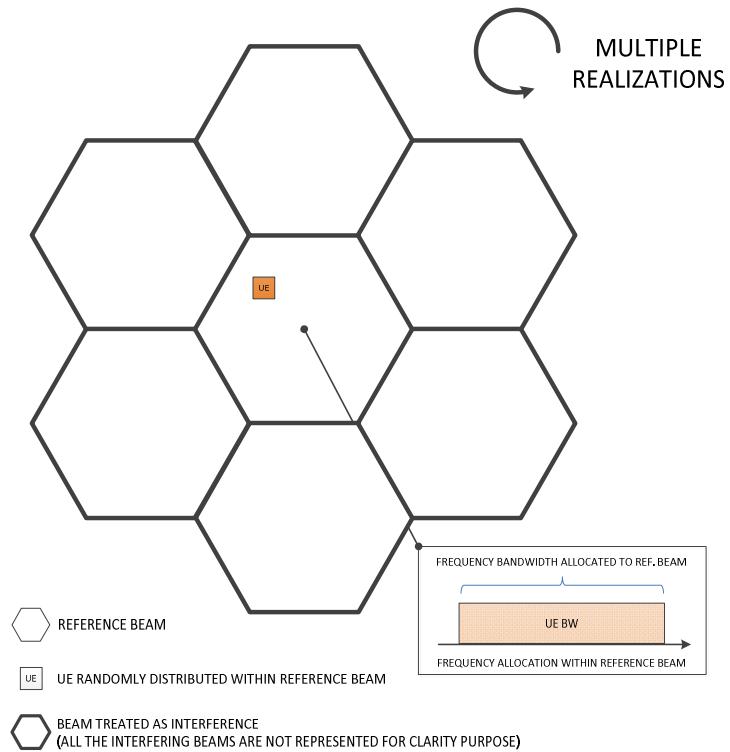


Figure 6.1.3.2-1: Illustration of UE bandwidth allocation in DL calibration

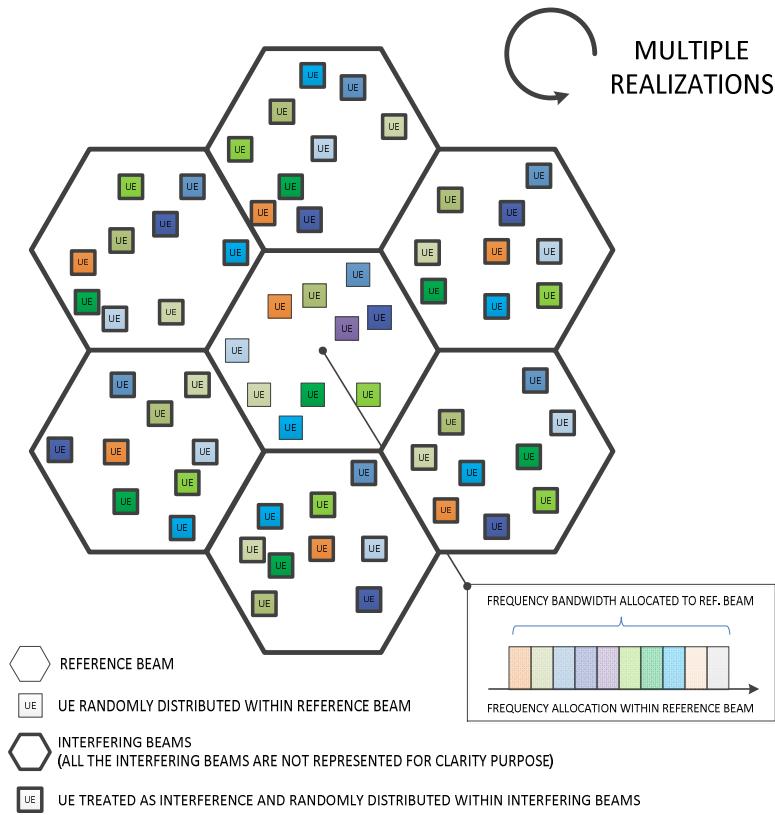


Figure 6.1.3.2-2: Illustration of UE bandwidth allocation in UL calibration

6.1.3.3 Link Budget Results

Table 6.1.3.3-1: Link budgets results

Case	Transmission mode	Frequency [GHz]	TX: EIRP [dBm]	RX: G/T [dB/T]	Bandwidth [MHz]	Free space path loss [dB]	Atmospheric loss [dB]	Shadow fading margin [dB]	Scintillation Loss [dB]	Polarization loss [dB]	Additional losses [dB]	CNR [dB]
SC1	DL	20.0	96.0	15.9	400.0	210.6	1.2	0.0	1.1	0.0	0.0	11.6
	UL	30.0	76.2	28.0	400.0	214.1	1.1	0.0	1.1	0.0	0.0	0.5
SC2	DL	20.0	91.2	15.9	133.3	210.6	1.2	0.0	1.1	0.0	0.0	11.6
	UL	30.0	76.2	28.0	133.3	214.1	1.1	0.0	1.1	0.0	0.0	5.2
SC3	DL	20.0	93.0	15.9	200.0	210.6	1.2	0.0	1.1	0.0	0.0	11.6
	UL	30.0	76.2	28.0	200.0	214.1	1.1	0.0	1.1	0.0	0.0	3.5
SC4	DL	2.0	103.8	-31.6	30.0	190.6	0.2	3.0	2.2	0.0	0.0	0.0
	UL	2.0	23.0	19.0	0.4	190.6	0.2	3.0	2.2	0.0	0.0	-10.9
SC5	DL	2.0	99.0	-31.6	10.0	190.6	0.2	3.0	2.2	0.0	0.0	0.0
	UL	2.0	23.0	19.0	0.4	190.6	0.2	3.0	2.2	0.0	0.0	-10.9
SC6	DL	20.0	60.0	15.9	400.0	179.1	0.5	0.0	0.3	0.0	0.0	8.5
	UL	30.0	76.2	13.0	400.0	182.6	0.5	0.0	0.3	0.0	0.0	18.4
SC7	DL	20.0	55.2	15.9	133.3	179.1	0.5	0.0	0.3	0.0	0.0	8.5
	UL	30.0	76.2	13.0	133.3	182.6	0.5	0.0	0.3	0.0	0.0	23.1
SC8	DL	20.0	57.0	15.9	200.0	179.1	0.5	0.0	0.3	0.0	0.0	8.5
	UL	30.0	76.2	13.0	200.0	182.6	0.5	0.0	0.3	0.0	0.0	21.4
SC9	DL	2.0	78.8	-31.6	30.0	159.1	0.1	3.0	2.2	0.0	0.0	6.6
	UL	2.0	23.0	1.1	0.4	159.1	0.1	3.0	2.2	0.0	0.0	2.8
SC10	DL	2.0	74.0	-31.6	10.0	159.1	0.1	3.0	2.2	0.0	0.0	6.6
	UL	2.0	23.0	1.1	0.4	159.1	0.1	3.0	2.2	0.0	0.0	2.8
SC11	DL	20.0	66.0	15.9	400.0	184.5	0.5	0.0	0.3	0.0	0.0	9.1
	UL	30.0	76.2	13.0	400.0	188.0	0.5	0.0	0.3	0.0	0.0	13.0
SC12	DL	20.0	61.2	15.9	133.3	184.5	0.5	0.0	0.3	0.0	0.0	9.1
	UL	30.0	76.2	13.0	133.3	188.0	0.5	0.0	0.3	0.0	0.0	17.8
SC13	DL	20.0	63.0	15.9	200.0	184.5	0.5	0.0	0.3	0.0	0.0	9.1
	UL	30.0	76.2	13.0	200.0	188.0	0.5	0.0	0.3	0.0	0.0	16.0
SC14	DL	2.0	84.8	-31.6	30.0	164.5	0.1	3.0	2.2	0.0	0.0	7.2
	UL	2.0	23.0	1.1	0.4	164.5	0.1	3.0	2.2	0.0	0.0	-2.6
SC15	DL	2.0	80.0	-31.6	10.0	164.5	0.1	3.0	2.2	0.0	0.0	7.2
	UL	2.0	23.0	1.1	0.4	164.5	0.1	3.0	2.2	0.0	0.0	-2.6
SC16	DL	20.0	88.0	15.9	400.0	210.4	0.8	0.0	0.5	0.0	0.0	4.8
	UL	30.0	76.2	20.0	400.0	213.9	0.7	0.0	0.5	0.0	0.0	-6.3
SC17	DL	20.0	83.2	15.9	133.3	210.4	0.8	0.0	0.5	0.0	0.0	4.8
	UL	30.0	76.2	20.0	133.3	213.9	0.7	0.0	0.5	0.0	0.0	-1.6
SC18	DL	20.0	85.0	15.9	200.0	210.4	0.8	0.0	0.5	0.0	0.0	4.8
	UL	30.0	76.2	20.0	200.0	213.9	0.7	0.0	0.5	0.0	0.0	-3.3
SC19	DL	2.0	98.3	-31.6	30.0	190.4	0.1	3.0	2.2	0.0	0.0	-5.2
	UL	2.0	23.0	14.0	0.4	190.4	0.1	3.0	2.2	0.0	0.0	-15.7
SC20	DL	2.0	93.5	-31.6	10.0	190.4	0.1	3.0	2.2	0.0	0.0	-5.2
	UL	2.0	23.0	14.0	0.4	190.4	0.1	3.0	2.2	0.0	0.0	-15.7
SC21	DL	20.0	52.0	15.9	400.0	179.1	0.5	0.0	0.3	0.0	0.0	0.5
	UL	30.0	76.2	5.0	400.0	182.6	0.5	0.0	0.3	0.0	0.0	10.4
SC22	DL	20.0	47.2	15.9	133.3	179.1	0.5	0.0	0.3	0.0	0.0	0.5
	UL	30.0	76.2	5.0	133.3	182.6	0.5	0.0	0.3	0.0	0.0	15.1
SC23	DL	20.0	49.0	15.9	200.0	179.1	0.5	0.0	0.3	0.0	0.0	0.5
	UL	30.0	76.2	5.0	200.0	182.6	0.5	0.0	0.3	0.0	0.0	13.4
SC24	DL	2.0	72.8	-31.6	30.0	159.1	0.1	3.0	2.2	0.0	0.0	0.6
	UL	2.0	23.0	-4.9	0.4	159.1	0.1	3.0	2.2	0.0	0.0	-3.2
SC25	DL	2.0	68.0	-31.6	10.0	159.1	0.1	3.0	2.2	0.0	0.0	0.6
	UL	2.0	23.0	-4.9	0.4	159.1	0.1	3.0	2.2	0.0	0.0	-3.2

SC26	DL	20.0	58.0	15.9	400.0	184.5	0.5	0.0	0.3	0.0	0.0	1.1
	UL	30.0	76.2	5.0	400.0	188.0	0.5	0.0	0.3	0.0	0.0	5.0
SC27	DL	20.0	53.2	15.9	133.3	184.5	0.5	0.0	0.3	0.0	0.0	1.1
	UL	30.0	76.2	5.0	133.3	188.0	0.5	0.0	0.3	0.0	0.0	9.8
SC28	DL	20.0	55.0	15.9	200.0	184.5	0.5	0.0	0.3	0.0	0.0	1.1
	UL	30.0	76.2	5.0	200.0	188.0	0.5	0.0	0.3	0.0	0.0	8.0
SC29	DL	2.0	78.8	-31.6	30.0	164.5	0.1	3.0	2.2	0.0	0.0	1.2
	UL	2.0	23.0	-4.9	0.4	164.5	0.1	3.0	2.2	0.0	0.0	-8.6
SC30	DL	2.0	74.0	-31.6	10.0	164.5	0.1	3.0	2.2	0.0	0.0	1.2
	UL	2.0	23.0	-4.9	0.4	164.5	0.1	3.0	2.2	0.0	0.0	-8.6

NOTE: The link budget calculations including CIR and CINR results contributed by the companies are available in [24].

6.1.4 Multiple satellites simulation

6.1.4.1 Simulation cases

For multiple satellites simulation, the cases defined for single satellite in Table 6.1.1.1-9 can be reused. Prioritization on the LEO can be considered for multiple satellites simulation.

6.1.4.2 Methodology for multiple satellites simulation

To emulate the effects of multiple satellites, the following two options can be considered:

- Option-1: simulation based on the reference constellation

In this option, as mentioned in [22][25][26], a reference constellation should be defined to construct the satellite and beam layout as shown in Figure 6.1.4.2-1, with corresponding parameters, e.g., number of orbit/satellites, number of beam illustrated in Figure 6.1.4.2-2. Detailed parameters can be determined jointly with consideration on the RF characteristic of beams together with design principle for constellation, e.g., how to achieve global coverage. Furthermore, the simulated area must be defined, because the coverage of the constellation depends on where on earth users are located.

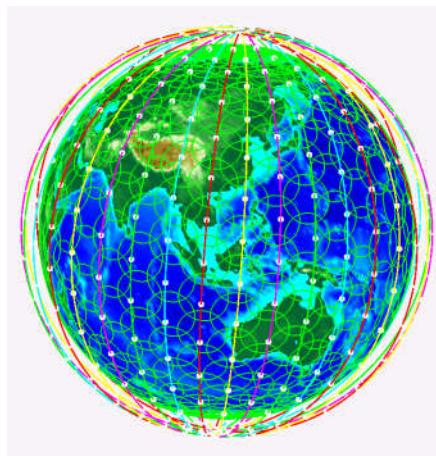


Figure 6.1.4.2-1: Illustration of exemplified satellite constellation

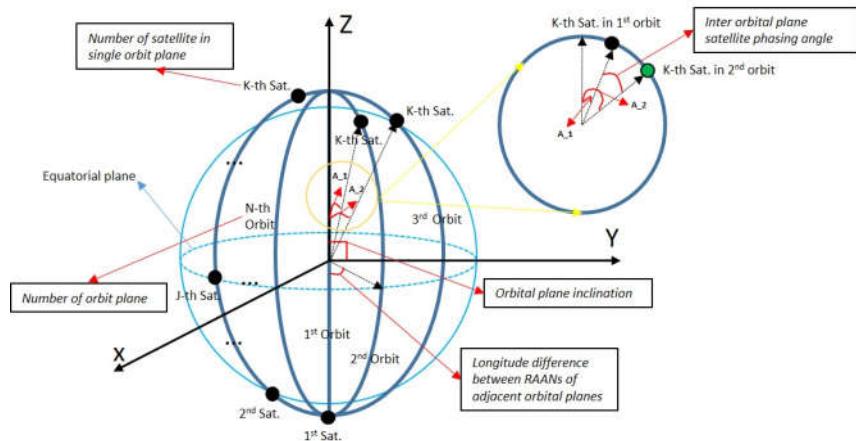


Figure 6.1.4.2-2: Illustration of parameters for satellite constellation (e.g., polar orbit with clock-wise movement)

- Option-2: simulation based on the regional beam layouts for multiple satellites

In this option, as mentioned in [27], regional beam layout for multiple satellites can be constructed as shown in Figure 6.1.4.2-3, e.g., beam with same colour belong to single satellite. Fixed orbit inclination can be assumed for simplicity and additional parameters, e.g., number of orbit, satellite per orbit, are introduced to enable the flexibility on the coverage for the overall beam layout. Reuse of the same satellite RF parameters as the single satellite simulation is feasible. Instead of using 7 satellites, a simpler scenario focused on throughput can also be constructed using 3 satellites as outlined in [28].

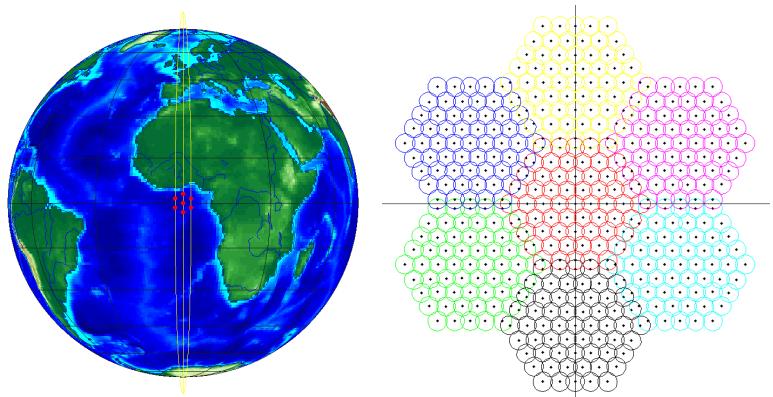


Figure 6.1.4.2-3: Illustration of regional beam layouts for multiple satellites

6.2 Physical layer control procedures

6.2.1 Timing relationships

The propagation delays in terrestrial mobile systems are usually less than 1 ms. In contrast, the propagation delays in NTN are much longer, ranging from several milliseconds to hundreds of milliseconds depending on the altitudes of the spaceborne or airborne platforms and payload type in NTN. Dealing with such long propagation delays requires modifications of many timing aspects in NR from physical layer to higher layers, including the timing advance (TA) mechanism.

In an NTN, a UE may need to apply a large TA value that leads to a large offset in its DL and UL frame timing. Figure 6.2.1-1 illustrates a scenario, where the UE applies a large TA and gNB's DL and UL frame timing are aligned. Another

solution proposed does not need the alignment between gNB's DL and UL frame, illustrated in Figure 6.2.1-2, where the UE applies a UE specific differential TA and a common TA offset in the gNB's DL and UL frame timing exists. However, for the solution illustrated in Figure 6.2.1-2, additional complexity is needed at network side to manage corresponding scheduling timing for this scenario. Various NR physical layer timing relationships need to be enhanced to cope with the large offset in the UE's DL and UL frame timing.

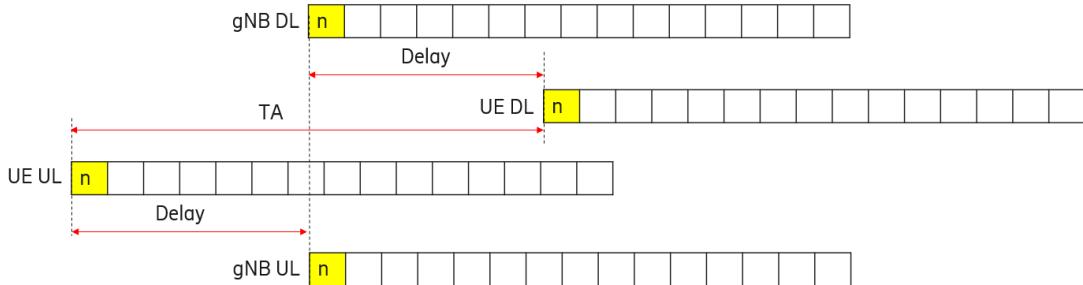


Figure 6.2.1-1: An illustration of large TA in NTN that results in a large offset in the UE's DL and UL frame timing

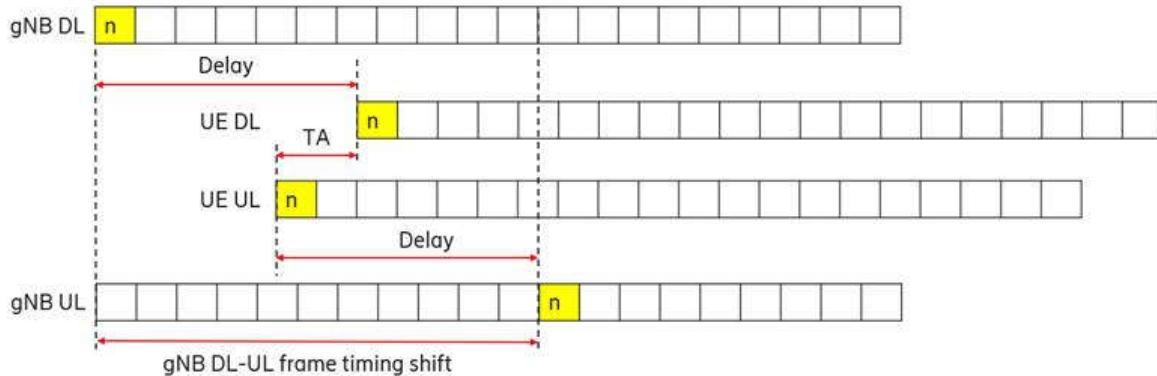


Figure 6.2.1-2: An illustration of TA in NTN that results in a large offset in the gNB's DL and UL frame timing

6.2.1.1 Background

The existing NR timing relationships are described as follows.

- **PDSCH reception timing:** When the UE is scheduled to receive PDSCH by a DCI, the DCI indicates the slot offset K_0 among other things. The slot allocated for the PDSCH is $\lfloor n \cdot \frac{\mu_{PDSCH}}{\mu_{PDCCH}} \rfloor + K_0$, where n is the slot with the scheduling DCI, K_0 is based on the numerology of PDSCH, and μ_{PDSCH} and μ_{PDCCH} are the subcarrier spacing configurations for PDSCH and PDCCH, respectively. The value of K_0 is in the range of 0, ..., 32.
- **Transmission timing for PUSCH scheduled by DCI:** When the UE is scheduled to transmit PUSCH by a DCI, the DCI indicates the slot offset K_1 among other things. The slot allocated for the PUSCH is $\lfloor n \cdot \frac{\mu_{PUSCH}}{\mu_{PDCCH}} \rfloor + K_1$, where n is the slot with the scheduling DCI, K_1 is based on the numerology of PUSCH, and μ_{PUSCH} and μ_{PDCCH} are the subcarrier spacing configurations for PUSCH and PDCCH, respectively. The value of K_1 is in the range of 0, ..., 32.
- **Transmission timing for PUSCH scheduled by RAR grant:** With reference to slots for a PUSCH transmission scheduled by a RAR UL grant, if a UE receives a PDSCH with a RAR message ending in slot n for a

corresponding PRACH transmission from the UE, the UE transmits the PUSCH in slot $n + K_2 + \Delta$, where K_2 and Δ are provided in TS 38.214.

- **Transmission timing for HARQ-ACK on PUCCH:** With reference to slots for PUCCH transmissions, for a PDSCH reception ending in slot n or a SPS PDSCH release through a PDCCH reception ending in slot n , the UE provides corresponding HARQ-ACK information in a PUCCH transmission within slot $n + K_1$, where K_1 is a number of slots and is indicated by the PDSCH-to-HARQ-timing-indicator field in the DCI format, if present, or provided by dl-DataToUL-ACK. $K_1 = 0$ corresponds to the last slot of the PUCCH transmission that overlaps with the PDSCH reception or with the PDCCH reception in case of SPS PDSCH release.
- **MAC CE action timing:** When the HARQ-ACK corresponding to a PDSCH carrying a MAC-CE command is transmitted in slot n , the corresponding action and the UE assumption on the downlink configuration indicated by the MAC-CE command shall be applied starting from the first slot that is after slot $n + 3N_{\text{slot}}^{\text{subframe}, \mu} + n + 3N_{\text{slot}}^{\text{subframe}, \mu} + K_{\text{offset}}$, where $N_{\text{slot}}^{\text{subframe}, \mu}$ denotes the number of slots per subframe for subcarrier spacing configuration μ .
- **Transmission timing for CSI on PUSCH:** The transmission timing of CSI on PUSCH follows the general transmission timing for DCI scheduled PUSCH.
- **CSI reference resource timing:** The CSI reference resource for a CSI report in uplink slot n' is defined by a single downlink slot $n - n_{\text{CSI_ref}}$, where $n = \lfloor n' \cdot \frac{2^{\mu_{\text{DL}}}}{2^{\mu_{\text{UL}}}} \rfloor$. Here, μ_{DL} and μ_{UL} are the subcarrier spacing configurations for DL and UL, respectively. The value of $n_{\text{CSI_ref}}$ depends on the type of CSI report and is defined in TS 38.214.
- **Aperiodic SRS transmission timing:** If a UE receives a DCI triggering aperiodic SRS in slot n , the UE transmits aperiodic SRS in each of the triggered SRS resource set(s) in slot $\lfloor n \cdot \frac{2^{\mu_{\text{SRS}}}}{2^{\mu_{\text{PDCCH}}}} \rfloor + k$, where k is configured via higher layer parameter slotOffset for each triggered SRS resources set and is based on the subcarrier spacing of the triggered SRS transmission, μ_{SRS} and μ_{PDCCH} are the subcarrier spacing configurations for triggered SRS and PDCCH carrying the triggering command respectively.

The existing NR timing definitions involving DL-UL timing interaction may not hold when there is a large offset in the UE's DL and UL frame timing in NTN. Thus, the timing relationships need to be enhanced.

6.2.1.2 Enhancements

The PDSCH reception timing is defined solely from DL timing perspective. It is not impacted by the large offset in the UE's DL and UL frame timing and thus enhancement is not needed.

The other timing relationships described in Section 6.2.1.1 involve DL-UL timing interaction and thus need to be enhanced for NTN. The enhancement can be to introduce an offset K_{offset} and applying it to modify the relevant timing relationships.

- For the transmission timing of DCI scheduled PUSCH (including CSI on PUSCH), the slot allocated for the PUSCH can be modified to be $\lfloor n \cdot \frac{2^{\mu_{\text{PUSCH}}}}{2^{\mu_{\text{PDCCH}}}} \rfloor + K_2 + K_{\text{offset}}$.
- For the transmission timing of RAR grant scheduled PUSCH, the UE transmits the PUSCH in slot $n + K_2 + \Delta + K_{\text{offset}}$.
- For the transmission timing of HARQ-ACK on PUCCH, the UE provides corresponding HARQ-ACK information in a PUCCH transmission within slot $n + K_1 + K_{\text{offset}}$.
- For the MAC CE action timing, the corresponding action and the UE assumption on the downlink configuration indicated by the MAC-CE command shall be applied starting from the first slot that is after slot $n + XN_{\text{slot}}^{\text{subframe}, \mu} + K_{\text{offset}} + n + 3N_{\text{slot}}^{\text{subframe}, \mu} + K_{\text{offset}}$, where the value of X may depend on NTN UE capability and may not necessarily be equal to 3. How to determine the value of X is for further study.

- For the CSI reference resource timing, the CSI reference resource is given in the downlink slot $n = n_{CSI_ref} - K_{offset}$.
- For the transmission timing of aperiodic SRS, the UE transmits aperiodic SRS in each of the triggered SRS resource set(s) in slot $\left| \frac{n_{SRS}}{n_{FDCH}} \right| + k + K_{offset}$.

The values of K_{offset} may be different for each of the identified timing relationships that need to be modified for NTN.

The values of K_{offset} can be per beam or per-cell. It is for further study whether K_{offset} is derived from broadcast information or is signalled by higher layers. The possibility of extending the range K_1 and/or K_2 beyond what is supported in NR Rel-15 can be further discussed when the specifications are developed.

6.2.2 Uplink power control

The following uplink power control solutions were discussed during the study item phase:

- One source [29] proposed beam-specific configuration for power control parameter P_0 and common $\alpha_{b,f,c}(f)$ parameter for all beams;
- Two sources ([30] and [31]) proposed UE prediction of its own transmission power using other available information such as satellite ephemeris and UE trajectory
- One source ([32]) proposed adaptive uplink power control based on adaptive UE configuration of Layer 3 filter coefficients (i.e., configuring multiple Layer 3 filter coefficients and letting UE select one of the Layer 3 filter coefficients based on measured RSRP).
- One source [33] proposed that UE can be configured with different uplink power control parameters such as P_0 and alpha parameters for disabled and enabled HARQ processes.
- One source [31] proposed that the transmission power of different UEs can be adjusted as a group with a reference UE transmission power. In addition, the source proposed a mechanism to disable closed loop power control.

The above optimizations were discussed without any convergence to a particular solution. As a result, it was concluded that NR Release-15 power control schemes can be used for NTN.

6.2.3 AMC and delayed CSI feedback

Two sources ([32] and [34]) contributed link-level simulation results to show the effect of increased CSI feedback delay (i.e., CSI aging) on throughput performance. The observations from these results are summarized below:

- Observation 1: For NTN-TDL-C (LOS) channel model, the two sources ([32] and [34]) show that the performance loss due to CSI aging is low to marginal. For instance, at an SNR of 10 dB at a UE speed of 3 km/hr,
 - Source 1 [32] results show that there is a throughput loss of around 10% as the feedback delay increases from 6 ms to 40 ms, and
 - Source 2 [34] results show that the spectral efficiency degrades by around 12% as the feedback delay increases from 6 ms to 46 ms.
- Observation 2: For NTN-TDL-A (NLOS) channel model, the two sources ([32] and [34]) show that the performance loss is more significant. For instance, at an SNR of 10 dB at a UE speed of 3 km/hr,
 - Source 1 [32] results show that there is a throughput loss of around 38% as the feedback delay increases from 6 ms to 40 ms, and
 - Source 2 [34] results show that the spectral efficiency degrades by around 28% as the feedback delay increases from 6 ms to 46 ms.

- Observation 3: For NTN-TDL-A (NLOS) channel model, Source 1 [32] shows that the performance loss saturates beyond a certain feedback delay for a given UE speed. For instance, the throughput loss saturates beyond 40 ms feedback delay at a UE speed of 3 km/hr.
- Observation 4: For both NTN-TDL-C (LOS) and NTN-TDL-A (NLOS) channel models, Source 1 [32] shows that with a UE speed of 30 km/hr, there is almost no observable performance loss as the feedback delay increases from 6 ms to 201 ms.

Based on the above results from the two sources ([32] and [34]), it is concluded that the performance loss due to increased CSI feedback delay depends on both the channel conditions as well as the UE speed:

- In LOS conditions, results from two sources show that the performance loss due to CSI aging is low to marginal at a UE speed of 3 km/hr.
- In NLOS conditions, results from two sources show that the performance loss due to CSI aging is significant at a UE speed of 3 km/hr.
- In both LOS and NLOS conditions, results from one source show that there is no observable performance loss due to CSI aging at a UE speed of 30 km/hr.

One solution to address the issue of performance losses due to CSI aging that was evaluated is based on CSI reporting with channel averaging to capture the long-term fading. This solution was evaluated by two sources ([32] and [34]) to show the effect of channel averaging on the performance when there is large CSI feedback delay. The evaluations results show the following observation:

- At 3 km/hr UE speed with ideal channel estimation, channel averaging to capture long-term fading does not improve throughput compared to the case with no channel averaging.

Based on the above results, the following is concluded regarding the effect of channel averaging on the performance when there is large CSI feedback delay:

Based on results from two sources ([32] and [34]), channel averaging to capture long-term fading does not improve throughput compared to the case with no channel averaging at a UE speed of 3 km/hr with ideal channel estimation.

A second solution to address the issue of performance losses due to CSI aging that was evaluated is uses CSI prediction-based link adaptation. Two sources ([35] and [34]) provided additional simulation results to show the effect of CSI prediction on throughput performance. These evaluations show the following observation:

- Performance gains can be achieved with the introduction of CSI feedback with prediction when compared to CSI feedback without prediction.
 - For NTN-TDL-A (NLOS) channel model, Source 2 [34] results show that the spectral efficiency can be improved by 10% at an SNR of 10 dB and a UE speed of 3 km/hr.
 - For NTN-TDL-B (NLOS) channel model, Source 3 ([35]) results show a 10% throughput improvement at an SNR of 10 dB and a UE speed of 3 km/hr.

During discussions related to prediction-based CSI, some sources were of the view that this can be achieved via implementation without any specification impact. One source was of the view that prediction-based CSI may involve specification impact (e.g., UE reports additional parameters, e.g., variant rate of CQI, in CSI). Based on the above results, the following is concluded regarding the effect of prediction-based CSI on the performance when there is large CSI feedback delay:

Based on results from two sources under NLOS conditions, CSI prediction improves throughput compared to the case with no CSI prediction.

- CSI prediction can be achieved via implementation and there is no consensus on specification changes with respect to CSI prediction enhancements for NTN.

A few other solutions were discussed but there were no evaluation results available for these solutions. The solutions without evaluation results are given below:

- Introduction of finer granularity of CQI to allow more accurate choice of MCS on a stable LoS channel proposed by two sources ([36] and [37]).

- Introduction of new BLER targets for CQI reporting in order to limit number of retransmissions and thereby latency proposed by three sources ([38], [39] and [36]).
- Application of a lower modulation order and coding rate than that based on the reported CQI values by the gNB to guarantee the reliability at the potential cost of spectrum efficiency [31], [33]
- Introduction of a CQI report disabling mechanism based on certain conditions such as satellite and/or UE location and speed, channel condition, etc. For example, if the distance between the UE and the satellite is very large and/or the propagation delay is larger than a certain threshold, CQI reporting is disabled [31].

Based on the results and discussion, the following is concluded for AMC and delayed CSI feedback:

The CSI framework specified in NR Rel-15 can be used for NTN link adaptation at least for LOS scenarios. Further optimizations were discussed without any convergence on particular solutions.

6.2.4 Beam management and polarization support

The proposals for beam management in NTN that were discussed during study phase are summarized below:

- Two sources ([40], [34]) proposed that for frequency reuse 1, rel-15 beam management can be used. For frequency reuse > 1, it was proposed that two Rel-15 based schemes are possible: (1) where one BWP is used for each satellite beam (proposed in [40] and [34]), and (2) where one component carrier is used per satellite beam (proposed in [40]).
- One source [41] proposed to consider additional beam management CSI-RS configurations to support different satellite implementation needs.
- One source [42] proposed to introduce a mechanism where both the Uplink and Downlink BWPs are switched simultaneously using a single DCI to support fast satellite beam switching.
- One source [29] proposed that the concept of BWP can be used for frequency resource allocation among NTN beams, and that the network may configure a specific active BWP for UEs in a beam.
- One source [35] proposed to increase the number of BWPs for NTN.

The proposed solutions for beam management for NTN were quite diverse and convergence to one particular solution was not possible at the conclusion of the study phase. Hence, the following conclusion was drawn for NTN beam management:

The rel-15/16 beam management and BWP operation are considered as baseline for NTN. Beam management and BWP operation for NTN with frequency reuse should be discussed further when specifications are developed.

Note that service link switching is seen as a part of beam management mechanism in NR NTN.

Another issue raised several sources is on polarization mode configuration/signalling. In NTN networks, neighbouring cells may use different polarization modes (RHCP and LHCP) to mitigate inter-cell interference. Furthermore, there may be UEs with different antenna types. Some UEs may be equipped with linearly polarized antennas, while some other UEs may be equipped with circularly polarized antennas. Three sources ([32], [35], and [40]) proposed that it is beneficial to signal the polarization mode for NTN in certain scenarios (particularly when the UE is capable of differentiating RHCP and LHCP with the circularly or linearly polarized antennas). Based on the discussion, the following is concluded:

Signalling of polarization mode is beneficial for NTN in certain scenarios. Whether to support the signalling can be discussed further when specifications are developed.

6.2.5 Impact of feeder link switch

For the issue of feeder link switch and its potential impact on PHY layer procedures, the following conclusion is made:

Impacts of feeder link switch on physical layer procedures can be further discussed when specifications are developed.

6.3 Uplink timing advance/RACH procedure

6.3.1 General

The following aspects have been studied based on NR Rel-15/16 design:

- 1) DL synchronization via SSB
- 2) Random access via PRACH
- 3) Maintenance for UL timing advance and frequency synchronization

The evaluations and analysis are conducted considering on characteristics of satellite communication systems, e.g., possibly large cell coverage and high Doppler. Meanwhile, the impacts due to some typical implementations in existing satellite systems, e.g., partial frequency pre-compensation for DL and timing post-compensation at satellite network side, are also taken into account. According to the corresponding results, solutions and conclusions along with some observations are presented.

6.3.2 DL synchronization

According to the simulation assumptions in Table 6.1.2-1, the performance evaluation on the DL synchronization performance is conducted. The corresponding results from [43], [44], [45], [46], [47] are summarized in [48]. It is observed that for DL initial synchronization, robust performance can be provided by the SSB design in Rel-15 in case of GEO and LEO with beam specific pre-compensation of common frequency shift, e.g., conducted with respect to the spot beam center at network side, respectively.

However, for the LEO without pre-compensation of the frequency offset, additional complexity is needed at UE receiver to achieve robust DL initial synchronization performance based on Rel-15 SSB. No further enhancement on the SSB is needed.

Additionally, w.r.t the performance on the DL timing/frequency tracking, no issues have been identified based on Rel-15/16 NR design. Potential optimization can be further considered in potential normative phase if necessary.

6.3.3 Random access

According to the simulation assumptions in Table 6.1.2-2, the performance of Rel-15 PRACH design is verified in several typical scenarios for NTN as listed in Table 6.1.2-3.

Based on the results summarized in [49], [50], it is observed that with assumption on pre-compensation of timing and frequency offset (e.g., if UE knowledge of geo-location of the UE at the requisite level of accuracy is available) at UE side for UL transmission, existing Rel-15 PRACH formats and preamble sequences can be reused. The necessity of additional enhancements, e.g., repetitions and/or larger sub-carrier spacing, to ensure UL coverage can be further discussed in the normative work.

However, in case pre-compensation of timing and frequency offset is not performed at UE side for UL transmission, enhanced PRACH formats and/or preamble sequences should be supported with following options:

- Option-1: A single Zadoff-Chu sequence based on larger SCS, repetition number. Additional usage of CP and Ncs can be further determined in normative work [51], [52], [53], [54].
- Option-2: A solution based on multiple Zadoff-Chu sequences with different roots [54], [55], [56]
- Option-3: Gold/m-sequence as preamble sequence with additional process, e.g., modulation and transform precoding [57], [51]
- Option-4: A single Zadoff-Chu sequence with combination of scrambling sequence [58], [59], [51]

Further discussions to down select these candidates are needed in the normative work.

6.3.4 Maintenance for UL timing advance and frequency synchronization

With consideration on the larger cell coverage, long round trip time (RTT) and high Doppler, enhancements are considered to ensure the performance for timing and frequency synchronization for UL transmission.

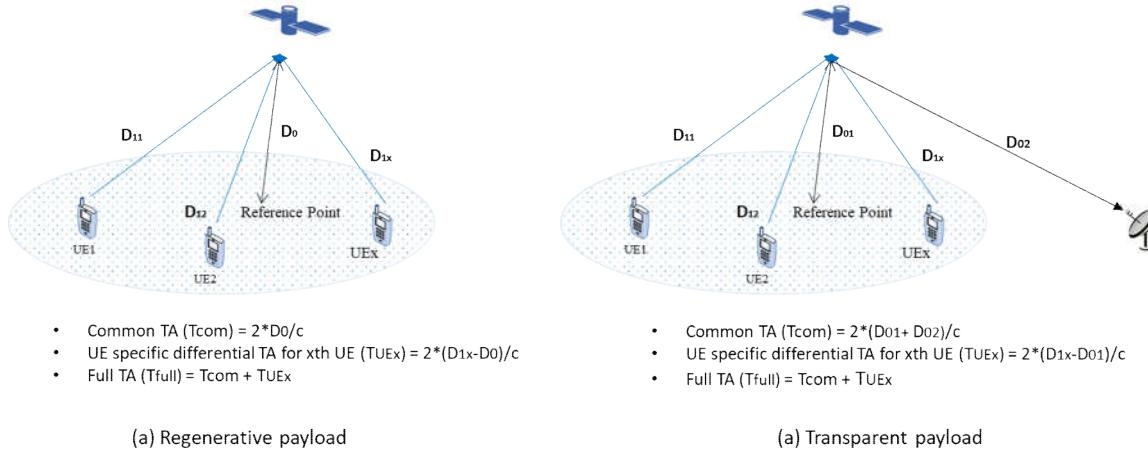


Figure 6.3.4-1: Illustration of the TA components in NTN (For simplicity, TA offset $N_{TA\ offset}$ is not plotted.)

For the timing advance (TA) in the initial access and the subsequent TA maintenance, the following solutions are identified with an illustration of the definition of terminology given in Figure 6.3.4-1:

- Option 1: Autonomous acquisition of the TA at UE with UE known location and satellite ephemeris.

In this way, the required TA value for UL transmission including PRACH can be calculated by the UE. The corresponding adjustment can be done, either with UE-specific differential TA or full TA (consisting of UE specific differential TA and common TA).

W.r.t the full TA compensation at the UE side, both the alignment on the UL timing among UEs and DL and UL frame timing at network side can be achieved. However, in case of satellite with transparent payload, further discussion on how to handle the impact introduced by feeder link will be conducted in normative work. Additional needs for the network to manage the timing offset between the DL and UL frame timing can be considered, if impacts introduced by feeder link is not compensated by UE in corresponding compensation.

W.r.t the UE specific differential TA only, additional indication on a single reference point should be signalled to UEs per beam/cell for achieving the UL timing alignment among UEs within the coverage of the same beam/cell. Timing offset between DL and UL frame timing at the network side should also be managed by the network regardless of the satellite payload type.

With concern on the accuracy on the self-calculated TA value at the UE side, additional TA signalling from network to UE for TA refinement, e.g., during initial access and/or TA maintenance, can be determined in the normative work.

- Option 2: Timing advanced adjustment based on network indication

In this way, the common TA, which refers to the common component of propagation delay shared by all UEs within the coverage of same satellite beam/cell, is broadcasted by the network per satellite beam/cell. The calculation of this common TA is conducted by the network with assumption on at least a single reference point per satellite beam/cell.

The indication for UE-specific differential TA from network as the Rel-15 TA mechanism is also needed. For satisfying the larger coverage of NTN, extension of value range for TA indication in RAR, either explicitly or implicitly, is identified. Whether to support negative TA value in corresponding indication will be determined in the normative phase.

Moreover, indication of timing drift rate, from the network to UE, is also supported to enable the TA adjustment at UE side.

For calculation of common TA in the above two options, single reference point per beam is considered as the baseline. Whether and how to support the multiple reference points can be further discussed in the normative work.

For the UL frequency compensation, at least for LEO system, the following solutions are identified with consideration on the beam specific post-compensation of common frequency offset at the network side:

- Option-1: Both the estimation and pre-compensation of UE-specific frequency offset are conducted at the UE side. The acquisition of this value can be done by utilizing DL reference signals, UE location and satellite ephemeris.
- Option-2: The required frequency offset for UL frequency compensation at least in LEO systems is indicated by the network to UE. The acquisition on this value can be done at the network side with detection of UL signals, e.g., preamble.

Indication of compensated frequency offset values by the network is also supported in case that compensation of the frequency offset is conducted by the network in the uplink and/or the downlink respectively. However, indication of Doppler drift rate is not necessary.

The detailed signalling design for the above enhancements will be determined in the normative work.

6.4 More delay-tolerant re-transmission mechanisms

Two main aspects of more delay-tolerant re-transmission mechanisms have been studied

- Disabling of HARQ in NR NTN
- HARQ optimization in NR-NTN

HARQ Round Trip Time in NR is of the order of several milliseconds. The propagation delays in NTN are much longer, ranging from several milliseconds to hundreds of milliseconds depending on the satellite orbit. The HARQ RTT can be much longer in NTN. It was identified early in the study phase that there would be a need to discuss potential impact and solutions on HARQ procedure. RAN1 has focussed on physical layer aspects while RAN2 has focused on MAC layer aspects.

6.4.1 Disabling of HARQ in NR NTN

RAN2 made recommendation in Section 7.2.1.4 HARQ. It was discussed that when UL HARQ feedback is disabled, there could be issues if (i) MAC CE and RRC signalling are not received by UE, or (ii) DL packets not correctly received by UE for a long period of time without gNB knowing it.

The following were discussed without convergence on the necessity of introducing such solutions for NTN when HARQ feedback is disabled

- Indicate HARQ disabling via DCI in new/re-interpreted field [60], [61]
- New UCI feedback for reporting DL transmission disruption and or requesting DL scheduling changes [62], [63]

The following possible enhancements for slot-aggregation or blind repetitions were considered. There is no convergence on the necessity of introducing such enhancements for NTN.

- Greater than 8 slot-aggregation [64]
- Time-interleaved slot aggregation [65]
- New MCS table [66]

6.4.2 HARQ Optimization for NR NTN

Solutions to avoid reduction in peak data rates in NTN were discussed. One solution is to increase the number of HARQ processes to match the longer satellite round trip delay to avoid stop-and-wait in HARQ procedure. Another solution is to disable UL HARQ feedback to avoid stop-and-wait in HARQ procedure and rely on RLC ARQ for reliability. The

throughput performance for both types of solutions was evaluated at link level and system level by several contributing companies.

The observations from the evaluations performed on the effect of the number of HARQ processes on performance are summarized as follows:

- Three sources [72][64][70] provided link-level simulations of throughput versus SNR with the following observations:
 - One source simulated with a TDL-D suburban channel with elevation angle of 30 degrees with BLER target of 1% for RLC ARQ with 16 HARQ processes, and BLER targets 1% and 10% with 32/64/128/256 HARQ processes. There was no observable gain in throughput with increased number of HARQ processes compared to RLC layer re-transmission with RTT in {32, 64, 128, 256} ms.
 - One source simulated with a TDL-D suburban channel with elevation angle of 30 degrees with BLER targets of 0.1% for RLC ARQ with 16 HARQ processes, and BLER targets 1% and 10% with 32 HARQ processes. An average throughput gain of 10% was observed with 32 HARQ processes compared to RLC ARQ with 16 HARQ processes with RTT = 32 ms.
 - One source provides the simulation results in following cases with RTT = 32 ms, e.g., assuming BLER targets at 1% for RLC ARQ with 16 HARQ processes, BLER targets 1% and 10% with 32 HARQ processes. There is no observable gain in throughput with 32 HARQ processes compared to RLC ARQ with 16 HARQ processes in case that channel is assumed as TDL-D with delay spread/ K-factor taken from system channel model in suburban scenario with elevation angle 30. Performance gain can be observed with other channels, especially, up to 12.5% spectral efficiency gain is achieved in case that channel is assumed as TDL-A in suburban with 30° elevation angle. Moreover, simulation based on the simulation with consideration on other scheduling operations: (i) additional MCS offset, (ii) MCS table based on lower efficiency (iii) slot aggregation with different BLER targets are conducted. Significant gain can be observed with enlarging the HARQ process number.
- One source [73] provided system level simulations for LEO=1200 km with 20% resource utilisation, 16 and 32 HARQ processes, 15 and 20 UEs per cell, proportional fair scheduling, and no frequency re-use. The spectral efficiency gain per user with 32 HARQ processes compared to 16 HARQ processes depends on the number of UEs. With 15 UEs per beam, an average spectral efficiency gain of 12% at 50% per centile is observed. With 20 UEs per cell there is no observable gain.

The following options were considered with no convergence on which option to choose:

- Option 1: Keep 16 HARQ process IDs and rely on RLC ARQ for HARQ processes with UL HARQ feedback disabled via RRC
- Option 2: Greater than 16 HARQ process IDs with UL HARQ feedback enabled via RRC with following consideration
 - UE capability if greater than 16 HARQ process IDs
 - Keep 4-bit HARQ process ID field in DCI

The following solutions were considered for greater than 16 HARQ processes keeping the 4-bit HARQ process ID field in DCI:

- Slot number based [62], [67], [68], [60], [69]
- Virtual process ID based with HARQ re-transmission timing restrictions [61]
- Reuse HARQ process ID within RTD (time window) [69]
- Re-interpretation of existing DCI fields with assistance information from higher layers [70]

One source also considered solutions where the HARQ process ID field is increased beyond 4 bits [65]

With regards to HARQ enhancements for soft buffer management and stop-and-wait time reduction, the following options were considered with no convergence on which, if any, of the options, to choose:

- Option 1: Pre-active/pre-emptive HARQ to reduce stop-and-wait time [71], [66]
- Option 2: Enabling / disabling of HARQ buffer usage configurable on a per UE and per HARQ process [67], [64], [69]
- Option 3: HARQ buffer status report from the UE [67]

The number of HARQ processes with additional considerations for HARQ feedback, HARQ buffer size, RLC feedback, and RLC ARQ buffer size should be discussed further when specifications are developed.

7 Radio protocol issues and related solutions

7.1 Requirements and key issues

7.1.1 Delay

In order to reduce the standardization work, the table here below identifies the worst case NTN scenarios to be considered for the delay constraint.

Table 7.1-1: NTN scenarios versus delay constraints, Source [2]

NTN scenarios	A	B	C1	C2	D1	D2
	<i>GEO transparent payload</i>	<i>GEO regenerative payload</i>	<i>LEO transparent payload</i>	<i>LEO regenerative payload</i>		
Satellite altitude	35786 km				600 km	
Relative speed of Satellite with respect to earth		negligible			7.56 km per second	
Min elevation for both feeder and service links			10° for service link and 10° for feeder link			
Typical Min / Max NTN beam foot print diameter (note 1)		100 km / 3500 km			50 km / 1000 km	
Maximum propagation delay contribution to the Round Trip Delay on the radio interface between the gNB and the UE	541.46 ms (Worst case)	270.73 ms	25.77 ms		12.89 ms	
Minimum propagation delay contribution to the Round Trip Delay on the radio interface between the gNB and the UE	477.48 ms	238.74 ms	8 ms		4 ms	
Maximum Delay variation as seen by the UE (note 2)	Negligible		Up to +/- 40 µs/sec (Worst case)		Up to +/- 20 µs/sec	
NOTE 1:	The beam foot print diameter are indicative. The diameter depends on the orbit, earth latitude, antenna design, and radio resource management strategy in a given system.					
NOTE 2:	The delay variation measures how fast the round trip delay (function of UE-satellite-NTN gateway distance) varies over time when the satellite moves towards/away from the UE. It is expressed in µs/s and is negligible for GEO scenario					
NOTE 3:	Void					
NOTE 4:	Speed of light used for delay calculation is 299792458 m/s.					

When several non-terrestrial network scenarios feature a maximum in terms of delay constraints, it is sufficient to study only one of these scenarios.

- NTN Scenario based on GEO with transparent payload for RTD and delay difference constraints
- NTN Scenario based on LEO with transparent payload and moving beams for the delay variation related constraint

As per the duplex mode:

- Down-prioritize TDD in this study item
- There is no TDD-specific timing requirements and solutions on layer 2 due to propagation delay.

7.2 User plane enhancements

7.2.1 MAC

7.2.1.1 Random Access

7.2.1.1.1 4-Step RACH Procedure

7.2.1.1.1.1 RACH capacity evaluation

The Physical Random Access Channel (PRACH) uses Slotted Aloha as access method. The PRACH preamble collision probability between contending system access attempts on a PRACH radio resource is calculated as:

$$P(\text{collision}) = 1 - e^{-\frac{\rho}{M}}$$

Where M is the number of configured access opportunities per second, and ρ is the random access arrival rate per second.

The random access capacity can be calculated by looking at the random access opportunities, the collision probability supported, the frequency used for frequent multiplexing and how many preambles that are configured for each random access opportunities.

If we denote the maximum number of PRACH opportunities per second as ρ , which is given by the PRACH configuration, such as preamble format, PRACH configuration index as well as whether the spectrum is paired/unpaired and whether it is for FR1 or FR2, as shown in Table 6.3.3.2-2 to Table 6.3.3.2-4 in [TS 38.211].

Furthermore the PRACH occasions may be frequency multiplexed by up to $F = 8$ different locations in frequency for the same PRACH occasion in time. Then the M as mentioned above is computed as:

$$M = \rho * p_{\text{configured}} * F,$$

Where $p_{\text{configured}}$ is the number of configured preambles available, where the maximum value is 64.

The number of the random access arrival rate per second supported is thus:

$$\gamma_{\text{supported}} = -\ln(1 - P(\text{collision})) * M = -\ln(1 - P(\text{collision})) * \rho * p_{\text{configured}} * F$$

The supported user densities UE density is thus given by:

$$\text{supported UE density} = \frac{\gamma_{\text{supported}}}{\text{coverage} * \text{RACH per second per UE}}$$

As an example, for PRACH configuration 27 the slots that are available in an SFN are the slots 0, 1, 2, 3, 4, 5, 6, 7, 8, 9 giving 1000 PRACH opportunities per second. In the table below some more examples are given for FR1 paired:

Note that all the PRACH format used in the calculation are given as an example and it is up to RAN1 to discuss and decide the applicable PRACH format in NTN.

Table 7.2.1.1.1-1: Examples of PRACH configuration for PR1 paired

Freq range and config	Preamble format	PRACH Config Index	PRACH opportunities per second (ρ)
FR1 paired	0	0	6,25
FR1 paired	0	21	200
FR1 paired	0	27	1000
FR1 paired	2	41	100

Given the collision rate being 0.01, the number of configured preambles for CBRA being 56, preamble format 0, PRACH config index 27, $F = 8$ we get the following as an example:

Table 7.2.1.1.1-2: Supported UE density for typical GEO and LEO cell

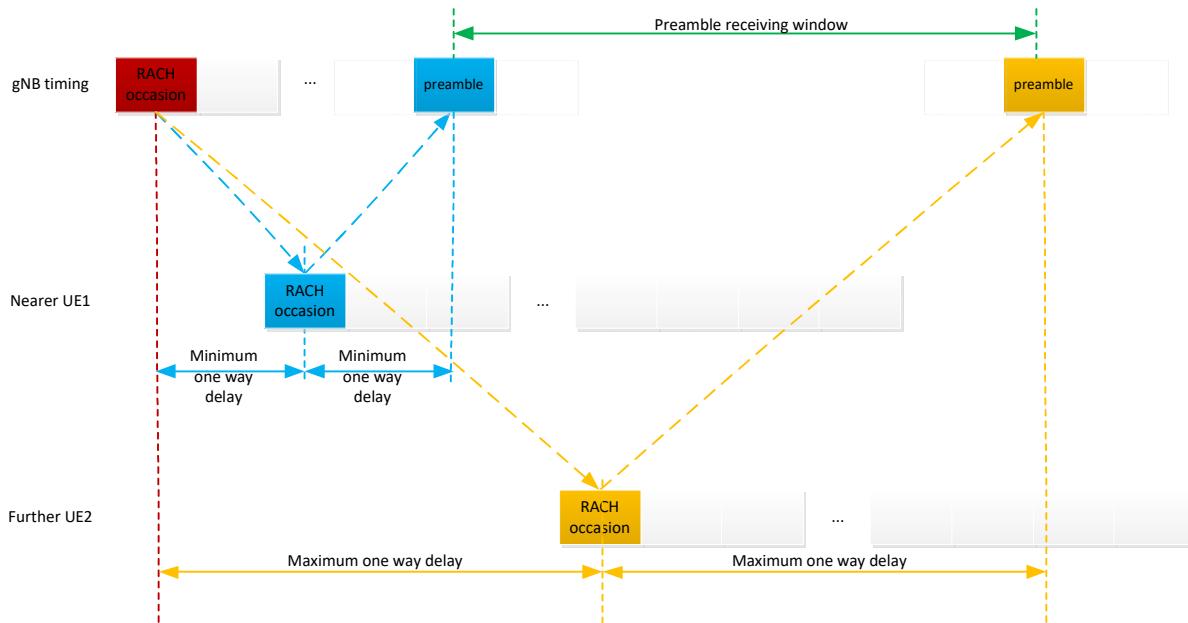
	Coverage (km²)	RACH per second per UE	Supported UE density
GEO	650000 (hex with r=500km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~596 UE/km ²
	650000	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~25 UE/km ²
	650000	0.0017 (= 1 time per 10 min per UE)	~4 UE/km ²
	162500 (hex with r=250km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~2383 UE/km ²
	162500	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~99 UE/km ²
	162500	0.0017 (= 1 time per 10 min per UE)	~16 UE/km ²
LEO	26000 (hex with r=100km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~14893 UE/km ²
	26000	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~620 UE/km ²
	26000	0.0017 (= 1 time per 10 min per UE)	~101 UE/km ²
	6500 (hex with r=50km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~59571 UE/km ²
	6500	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~2479 UE/km ²
	6500	0.0017 (= 1 time per 10 min per UE)	~405 UE/km ²

7.2.1.1.1.2 4-step RACH enhancements for Non-Terrestrial Networks

Enhancement to preamble detection

Problem Statement

In NTN, differential delay could be experienced by two UEs within the same cell. As a result, the preambles sent by different UEs in the same RACH occasion (RO) may reach the network at different time. As shown in Figure 7.2.1.1.1.2-1, to make sure the network can receive preambles from all the UEs, the preamble receiving window should start from [RO timing + minimum one way delay * 2] and end with [RO timing + maximum one way delay * 2].

**Figure 7.2.1.1.1.2-1: Preamble receiving window in NTN**

When a preamble is received, the network needs to know which RO the preamble is related to in order to estimate the accurate timing advance. If the RO periodicity is not long enough, as shown in Figure 7.2.1.1.1.2-2, the preamble receiving windows for two consecutive ROs may be overlapped with each other, making it difficult for the network to link the received preamble to the corresponding RO.

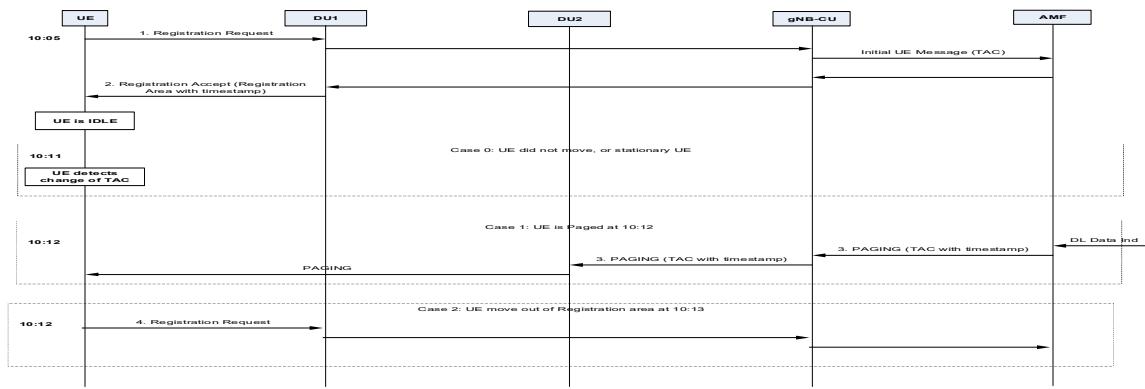


Figure 7.2.1.1.2-2: Ambiguity on preamble reception at the network side

Possible solutions:

- 1) Proper PRACH configuration in the time domain. The interval between two consecutive RO should be larger than $2 * \text{maximum delay difference}$ within the cell.
- 2) Preamble division. Preambles should be divided into groups and mapped to different RO, such that ROs with timing separation less than $2 * \text{maximum delay difference}$ are always assigned with different groups of preambles.

Frequency hopping can also be studied, e.g., network uses frequency hopping of preambles to identify the RO based on the specific frequency band in which the preamble is received.

Solutions related to 2-step RACH can also be studied when the 2-step RACH procedure is more stable. For the case when 2-step RACH is used, assistance information, e.g., SFN index can be included in MsgA to help network link the received preamble to the corresponding RO.

Based on the current specs, the ambiguity of preamble reception can only be avoided by solution (1), i.e. proper configuration of RACH resource, in which case the time interval between two consecutive RO is larger than the maximum delay difference*2 within the cell.

The typical cell size and the corresponding maximum delay difference*2 are given as follows:

Table 7.2.1.1.2-1: Maximum delay difference*2 for typical GEO and LEO cell

	Typical cell size	Maximum delay difference*2
GEO	1000 km	6.44ms
	500km	3.26ms
LEO	200 km	LEO600: 1.306ms LEO1200: 1.308ms
	100 km	LEO600: 0.654ms LEO1200: 0.654ms

Referring to Table 6.3.3.2-2 to Table 6.3.3.2-3 in TS 38.211, only limited PRACH configuration can meet the requirement on RO interval at time domain, which can significantly impact the RACH density to be supported in time domain.

For a typical GEO cell (1000km in size), the time interval between two consecutive RO should be larger than 6.44ms. For a typical GEO cell (500km in size), the time interval between two consecutive RO should be larger than 3.26ms. While for a typical LEO cell (200km or 100km in size), the time interval between two consecutive RO should be larger than 1.308ms and 0.654ms, respectively. Examples of potential PRACH configurations for a typical GEO or LEO cell are given as follows:

Note that all the PRACH format used in the calculation are given as an example and it is up to RAN1 to discuss and decide the applicable PRACH format in NTN.

Table 7.2.1.1.1.2-2: Examples of feasible PRACH configurations for a typical GEO or LEO cell

	Cell size	Freq range and config	Preamble format	PRACH Config Index	PRACH opportunities per second (s)
GEO	1000km	FR1 paired	0	16	100
		FR1 paired	1	44	100
		FR1 paired	2	58	100
	500km	FR1 paired	0	19	200
		FR1 paired	1	47	200
		FR1 paired	3	78	200
LEO	200km	FR1 paired	0	25	500
		FR1 paired	3	84	500
	100km	FR1 paired	0	27	1000
		FR1 paired	3	86	1000

Given the collision rate being 0.01, the number of configured preambles for CBRA being 56, preamble format 0, PRACH config index 8, $F = 8$ we get the following as an example:

Table 7.2.1.1.1.2-3: Supported UE density for typical GEO and LEO cell when the time interval between two consecutive RO is larger than the maximum delay difference*2 within the cell

	Coverage (km ²)	RACH per second per UE	Supported UE density
GEO	650000 (hex with r=500km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~60 UE/km ²
	650000	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~2 UE/km ²
	650000	0.0017 (= 1 time per 10 min per UE)	~0 UE/km ²
	162500 (hex with r=250km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~477 UE/km ²
	162500	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~20 UE/km ²
	162500	0.0017 (= 1 time per 10 min per UE)	~3 UE/km ²
LEO	26000 (hex with r=100km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~7446 UE/km ²
	26000	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~310 UE/km ²
	26000	0.0017 (= 1 time per 10 min per UE)	~51 UE/km ²
	6500 (hex with r=50km)	$1.157 * 10^{-5}$ (= 1 time per day per UE)	~59571 UE/km ²
	6500	$2.78 * 10^{-4}$ (= 1 time per hour per UE)	~2479 UE/km ²
	6500	0.0017 (= 1 time per 10 min per UE)	~405 UE/km ²

Enhancement to random access response window

Problem Statement

After transmitting the Random Access Preamble (Msg1), the UE monitors the PDCCH for the Random Access Response (RAR) message (Msg2). The response window (*ra-ResponseWindow*) starts at a determined time interval after the preamble transmission. If no valid response is received during the *ra-ResponseWindow*, a new preamble is sent. If more than a certain number of preambles have been sent, a random access problem will be indicated to upper layers. [75]

In terrestrial communications, the RAR is expected to be received by the UE within a few milliseconds after the transmission of the corresponding preamble. In NTN the propagation delay is much larger and therefore, so the RAR cannot be received by the UE within the specified time interval specified for terrestrial communications. Therefore, the behaviour of *ra-ResponseWindow* should be modified to support NTN.

Possible Solution

Introduce an offset for the start of the *ra-ResponseWindow* for NTN. The offset shall be configurable to accommodate different scenarios.

In addition to delaying the start of *ra-ResponseWindow*, it is worth considering whether an extension of *ra-ResponseWindow* is necessary to support NTN. In NTN the propagation delay is much larger than in terrestrial networks. Therefore, the RAR cannot be received by the UE within the time interval, of *ra-ResponseWindow*, having values specific to terrestrial networks.

For UE with location information, if the exact round trip delay can be estimated as an offset to delay the *ra-ResponseWindow*, there appears to be no need for extending the *ra-ResponseWindow*.

For UE without location information, the exact round trip delay cannot be computed to deduct the accurate offset of the *ra-ResponseWindow*.

Figure 7.2.1.1.1.2-3 illustrates a worst case in which a UE with minimum one way transmission delay and a UE with maximum one way transmission delay (e.g. locates at cell edge) initiate random access using the same time-frequency resource.

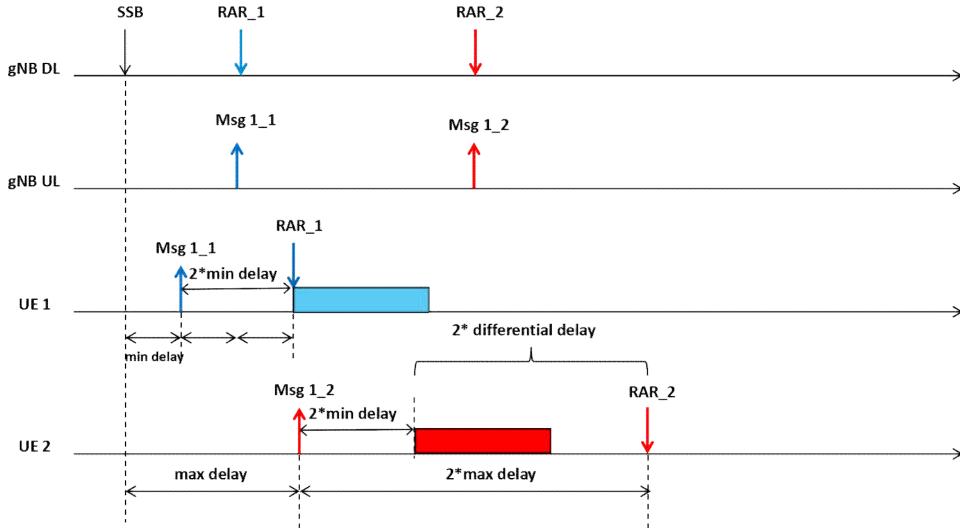


Figure 7.2.1.1.1.2-3: RAR window in NTN

Assuming the configured offset to delay the start of the RAR window equals to $2 * \text{minimum delay}$ and neglecting the process delay between reception of preamble and transmission of RA Response at gNB side, it can be observed that the RAR monitoring duration shall cover at least $2 * \text{maximum differential delay}$. Otherwise RAR for UE will fall out of RAR window. The maximum differential delay is defined as maximum one way delay minus minimum one way delay. Furthermore, time flexibility is required for the NW to schedule the RARs which means several milliseconds should be added on top of the $2 * \text{maximum differential delay}$.

Note that the maximum differential delay within one cell is 10.3ms for GEO and 3.18ms for LEO. For GEO case, $2 * \text{maximum differential delay} = 20.6\text{ms} > 10\text{ms}$. For LEO, $2 * \text{maximum differential delay} = 6.36 \text{ ms} < 10 \text{ ms}$. Thus, for UE without location information, extension of the *ra-ResponseWindow* is required and can be applied in both GEO and LEO.

When the *ra-ResponseWindow* is extended, including LSBs of SFN in Msg2 can be a baseline in NTN. Whether to modify the RA-RNTI calculation formula or define some parameters in the formula can be discussed in WI phase.

Enhancement to contention resolution timer

Problem Statement

When the UE sends an RRC Connection Request (Msg3), it will monitor for Msg4 in order to resolve a possible random-access contention. The *ra-ContentionResolutionTimer* starts after Msg3 transmission. The maximum configurable value of *ra-ContentionResolutionTimer* is large enough to cover the Round Trip Delay in NTN. However, to save UE power, the behavior of *ra-ContentionResolutionTimer* should be modified to support NTN.

Possible Solution

Introduce an offset for the start of the *ra-ContentionResolutionTimer* for NTN.

Enhancement to timing advance

Problem Statement

Timing Advance (TA) is used to adjust the uplink frame timing relative to the downlink frame timing. As shown in Figure 7.2.1.1.2-4 (b), the DL and UL timing is aligned at gNB with timing advance. The timing advance is twice the value of the propagation delay. Different UEs usually have different timing advance.

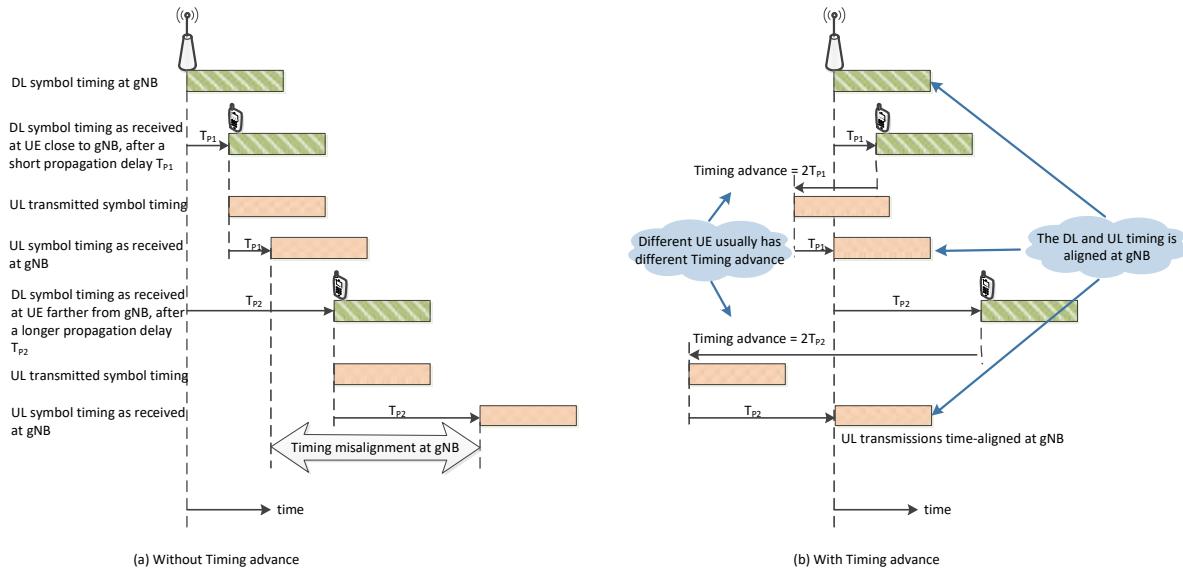


Figure 7.2.1.1.2-4: Timing alignment at gNB side

The timing advance is derived from the UL received timing and sent by the gNB to the UE. UE uses the timing advance to advance/delay its timings of transmissions to the gNB so as to compensate for propagation delay and thus time align the transmissions from different UEs with the receiver window of the gNB. There are two possible ways for gNB to provide timing advance to UE:

- (1) Initial timing advance during random access procedure:** gNB derives the timing advance by measuring the received random access preamble and sends the value to UE via the Timing Advance Command field in MAC RAR [75].

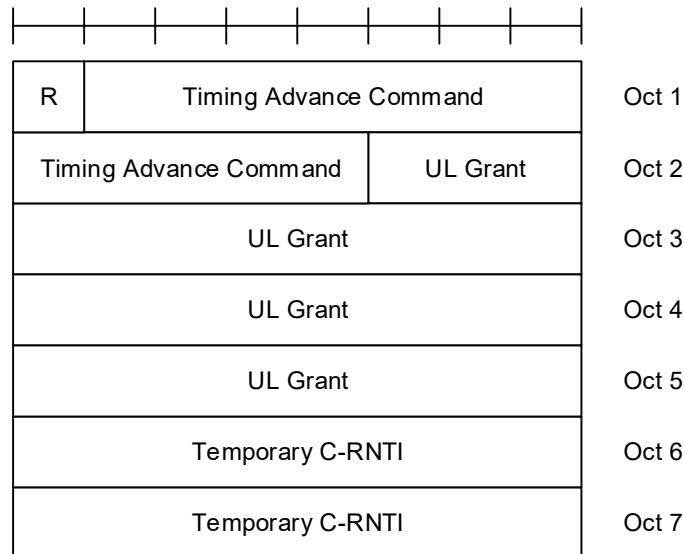


Figure 7.2.1.1.2-5: MAC RAR

In NR, Uplink frame number for transmission from the UE shall start $(N_{TA} + N_{TA,offset})T_c$ before the start of the corresponding downlink frame at the UE [TS 38.213].

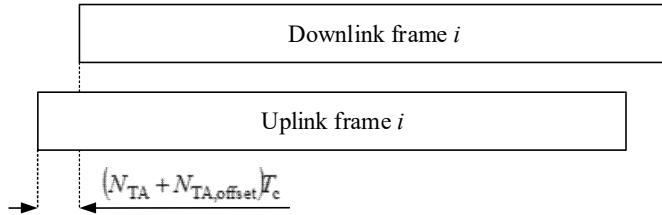


Figure 7.2.1.1.2-6: Uplink-downlink timing relation

$N_{TA,offset}$ is provided in SIB1 with the following possible values:

n-TimingAdvanceOffset ENUMERATED { n0, n25600, n39936 } OPTIONAL, -- Need S
 In case of random access response, a timing advance command, T_A for a TAG indicates N_{TA} values by index values of $T_A = 0, 1, 2, \dots, 3846$, where an amount of the time alignment for the TAG with SCS of $2^\mu \cdot 15\text{ kHz}$ is $N_{TA} = T_A \cdot 16 \cdot 64 / 2^\mu$. N_{TA} is defined in [TS 38.211] and is relative to the SCS of the first uplink transmission from the UE after the reception of the random access response.

$$T_c = 1/(\Delta f_{\max} \cdot N_f), \text{ where } \Delta f_{\max} = 480 * 10^3 \text{ Hz and } N_f = 4096.$$

The maximum timing advance in NR which can be compensated during initial access is calculated in the following Table.

Table 7.2.1.1.2-4: Maximum timing advance compensated during initial access for different SCS

μ	SCS = $2^\mu \cdot 15\text{ kHz}$	Maximum timing advance compensated during initial access
0	15	2ms
1	30	1ms
2	60	0.5ms
3	120	0.27ms
4	240	0.15ms

(2) Timing advance refinement in RRC_CONNECTED: gNB derives the timing advance by measuring the UL transmission and refines the timing advance via the Timing Advance Command MAC CE.

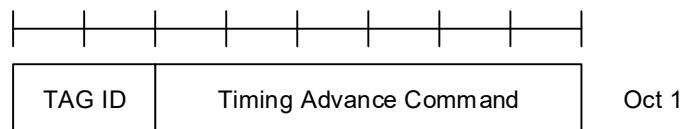


Figure 7.2.1.1.2-7: Timing Advance Command MAC CE

The timing advance command, T_A , for a TAG indicates adjustment of a current N_{TA} value, $N_{TA,old}$, to the new N_{TA} value, $N_{TA,new}$, by index values of $T_A = 0, 1, 2, \dots, 63$, where for a SCS of $2^\mu \cdot 15\text{ kHz}$,

$$N_{TA,new} = N_{TA,old} + (T_A - 31) \cdot 16 \cdot 64 / 2^\mu \quad [\text{TS 38.213}].$$

The maximum timing advance which can be adjusted via Timing Advance Command is calculated in the following table:

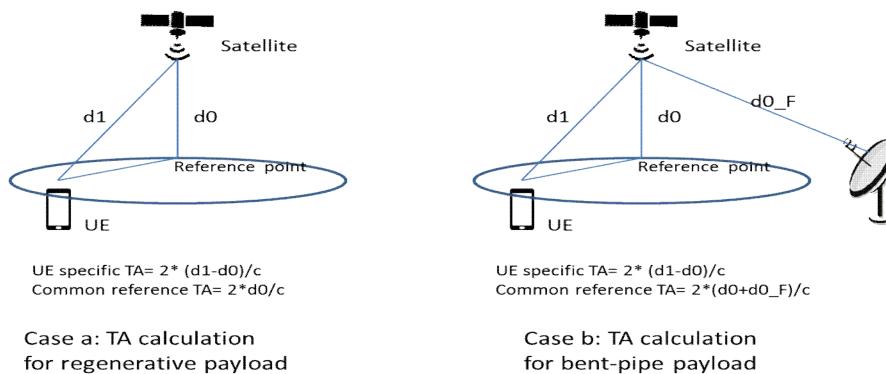
Table 7.2.1.1.2-5: Maximum timing advance adjusted via Timing Advance Command

Fehler! Es ist nicht möglich, durch die Bearbeitung von Feldfunktionen Objekte zu erstellen.Fehler ! Es ist nicht möglich, durch die Bearbeitung von Feldfunktionen Objekte zu erstellen.	SCS = Fehler! Es ist nicht möglich, durch die Bearbeitung von Feldfunktionen Objekte zu erstellen. kHz	Maximum timing advance compensated via Timing Advance Command
0	15	0.017ms
1	30	0.008ms
2	60	0.004ms
3	120	0.002ms
4	240	0.001ms

As mentioned above, the timing advance is twice the propagation delay. In NTN, the maximum round trip delay is 541.46ms for GEO and 25.77ms for LEO. The timing advance in NR as calculated in Table 7.2.1.1.2-1 and Table 7.2.1.1.2-2 is far from sufficient. Solutions for both UE with and without GNSS-capabilities should be considered.

Possible Solutions

As shown in Figure 7.2.1.1.2-8, the value of common TA is determined by d_0 for regenerative payload and $d_0+d_{0_F}$ for bent-pipe payload while the value of UE specific TA is determined by d_1-d_0 .

**Figure 7.2.1.1.2-8: Common TA and UE specific TA calculation**

For UE without location information, broadcasting a common TA for NTN or extending the value range of the existing TA offset broadcast in system information is the baseline for initial timing advance during random access procedure in NTN. Compensating the common TA at network side by implementation can be discussed in WI phase. The UE specific TA is compensated via Timing Advance Command field in random access response.

For UE with location information, the following framework should be considered as a baseline for UE to perform initial timing advance during 4-step random access procedure:

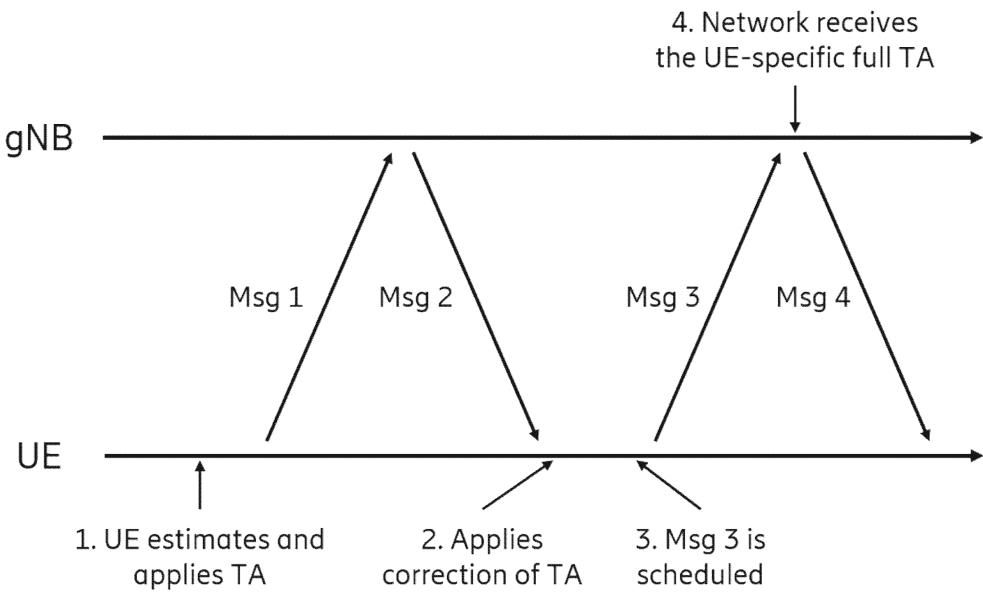


Figure 7.2.1.1.2-9: Framework on 4-step random access procedure for UE with location information

- 1) Estimation and application of the timing advance with respect to the satellite before UE sending Msg1 (i.e. random access preamble) to the network. The details are to be decided during the work item phase, but examples of how this can be achieved:
 - a. For regenerative architecture: the satellite position could be needed for UE to estimate the UE-to-satellite delay. For acquiring the satellite position, the position may either be acquired through satellite ephemeris or broadcasted in System Information.
 - b. For transparent architecture: the estimation is a bit more involved as the delay that needs to be estimated is between the UE and the gNB interface on the ground. Some options are:
 - i. To broadcast the position of the satellite along with the delay from satellite to gateway where the gNB interface is situated.
 - ii. Signal ephemeris along with gateway position to the UE.
 - iii. Signal the feeder link delay or to have the gNB to compensate feeder link delay so that UE only estimates the service link delay.
- 2) In Msg2, when the UE receives the RAR, it applies a timing advance correction for the UE-based estimation. Since the UE is now estimating the timing advance the UE may now both under- and overestimate the timing advance, there may need to be some adjustments of the timing advance to deal with this.
- 3) The network schedules Msg3 without knowing the absolute value of the timing advance. This can be solved by for instance:
 - c. Using the maximum propagation delay of the cell to schedule the UE.
 - d. Using maximum differential delay
- 4) Network receives Msg3 and gets to know the timing advance of the UE. At this point both UE and network are both aware of the UE-specific timing advance.

For UE with location information, another option is that UE only compensates its specific TA when sending msg1, where UE specific TA is determined by d_1-d_0 . Network compensates the common TA, where the common TA is determined by the distance between a reference point and the gNB. d_1 , d_0 and the reference point are illustrated in figure 7.2.1.1.2-8 for regenerative payload.

Broadcasting the delays in case of moving cells efficiently and avoid frequent updates will be considered during the work item phase.

7.2.1.1.2 2-Step RACH Procedure

2-step random access procedure, which can be helpful in mitigating the impact of the transmission delay, has been identified to be beneficial in NTN. The following figure gives an example of 2-step RACH procedure. The MsgA of the 2-step RACH includes a preamble on PRACH and a payload on PUSCH. After MsgA transmission, the UE monitors for a response from the network within a configured window. If contention resolution is received successfully in MsgB, it ends the random access procedure.

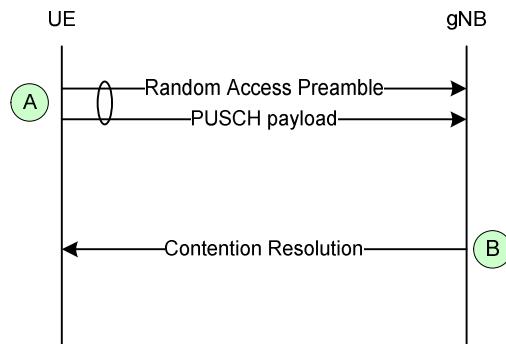


Figure 7.2.1.1.2-1: Example of 2-step RACH

The main challenge for UE with location information to perform initial timing advance during 4-step random access procedure is that the network has to schedule Msg3 without knowing the absolute value of the initial timing advance applied at the UE side. As a sequence, the network may have to schedule UE using the maximum propagation delay of the cell. While in 2-step random access procedure, UE can include some assistance information in the PUSCH payload for network to know the value of TA applied by UE. The following framework should be considered as a baseline for UE to perform initial timing advance during 2-step random access procedure:

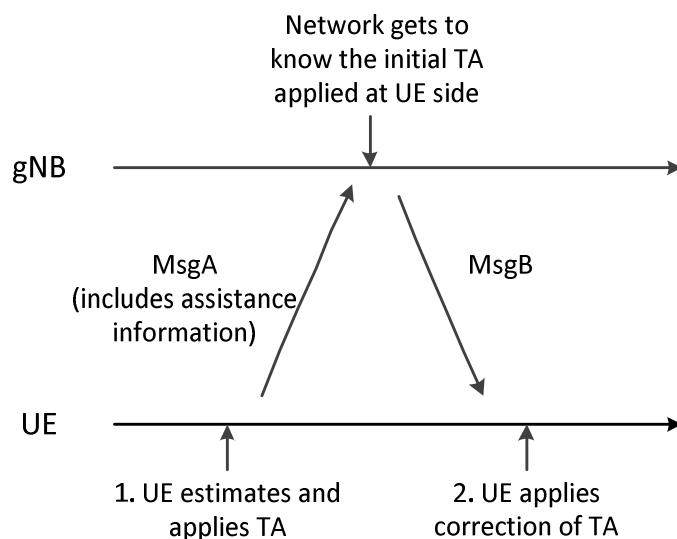


Figure 7.2.1.1.2-2: Framework on 2-step random access procedure for UE with location information

1. UE estimate and apply the initial timing advance before transmission of MsgA. UE will include assistance information in the PUSCH payload for network to know the value of initial timing advance applied by UE.
2. If contention resolution is successful UE apply a timing advance correction for the UE-based estimation in MsgB. By this time, both UE and network is aware of the final UE specific timing advance.

7.2.1.1.3 Random access enhancements to address mobility issues

- **RACH back-off indication:** A back-off indication may be provided in the HO command message, with back-off achieved via random number generation within an interval, or via explicit setting of different back-off indications in the RACH sync reconfiguration message.
- **RACH-less HO:** Based on satellite ephemeris and UE location, the UE can estimate the required TA value of the target gNB enabling the UE to perform RACH-less handover. The feasibility of this solution given the large propagation delay and possible uncertainties in satellite/UE position can be discussed in WI phase.
- **2-step RACH:** The agreements of the 2-step RACH WI will be used as baseline, and further enhancements for NTN may be considered.

7.2.1.1.4 Co-existence with different random access capabilities

Problem Statement

If there are both UEs that have GNSS and non-GNSS capabilities and given that the random access scheme for these might be different, then it should be possible for the network to separate the resources and control access to the network given that the random access procedures and the resource may look very different.

Possible Solution

One possible solution is for the network to be able to configure separate resources and differentiate these based on GNSS capabilities.

7.2.1.2 Discontinuous Reception (DRX)

Problem Statement

The Discontinuous Reception (DRX) supports UE battery saving by reducing the PDCCH monitoring time. Several RRC configurable parameters are used to configure DRX. [75][TS38.331]

A modification of *drx-LongCycleStartOffset*, *drx-StartOffset*, *drx-ShortCycle*, *drx-ShortCycleTimer*, *drx-onDurationTimer*, *drx-SlotOffset* and *drx-InactivityTimer* is not needed to support NTN for the reason that the timer values were inspected to accommodate the RTD of NTN system.

drx-HARQ-RTT-TimerDL is the minimum duration before a downlink assignment for HARQ retransmission is expected by the MAC entity. In terrestrial communications this is configurable in the range of a few ms, which is too small for a communication-link with a satellite. *drx-HARQ-RTT-TimerUL* is the same as *drx-HARQ-RTT-TimerDL* just for the uplink.[75][TS38.331]

If HARQ is supported by NTN, the handling of *drx-HARQ-RTT-TimerDL* and *drx-HARQ-RTT-TimerUL*, should be modified to support NTN.

drx-RetransmissionTimerDL presents the maximum time until a downlink retransmission is received. The timer starts latest after 4ms after the corresponding transmission. During this timer runs, the UE monitors the PDCCH. *drx-RetransmissionTimerUL* is the same as *drx-RetransmissionTimerDL* just for the uplink.[75][TS38.331]

A modification of *drx-RetransmissionTimerDL* and *drx-RetransmissionTimerUL* is not needed to support NTN.

Possible Solution

If HARQ feedback is enabled by NTN, an offset is added for *drx-HARQ-RTT-TimerDL* and *drx-HARQ-RTT-TimerUL* to support NTN.

Problem Statement

If HARQ feedback is disabled or enabled for only a certain number of HARQ process IDs, according to [75], the UE might be forced to monitor the PDCCH for retransmission opportunities that never will happen and thus waste energy that reduces the battery lifetime.

Possible Solution

A simple solution for the feedback to the transmission of DL TBs is to confirm that the current implementation of the specification [75] does not start the *drx-HARQ-RTT-TimerDL* if HARQ feedback is disabled.

A simple solution for the transmission of UL TBs is to agree to have an addition to the specification [75] that the UE should only start the *drx-HARQ-RTT-TimerUL* if HARQ feedback is enabled for the corresponding HARQ process. The exact formulation can be discussed in WI phase.

Problem Statement

In NTN with long propagation delays, the UE should avoid monitoring the PDCCH and thus save energy when nothing will be received due to long RTTs, see Figure 7.2.1.2-1. When DRX is configured, the UE is either in Active time and continuously monitor the PDCCH, or, it is in non-Active time and allowed to save energy by not monitoring the PDCCH. The Active time occasions are mainly controlled by network configurations but at some occasions the UE enters Active time without the control of the network, e.g. after:

- Sending a Scheduling Request
- Replying to the RAR in Contention-Free Random Access

In both these cases, the UE would have to monitor the PDCCH for at least one RTT before any type of response is possible to be received.

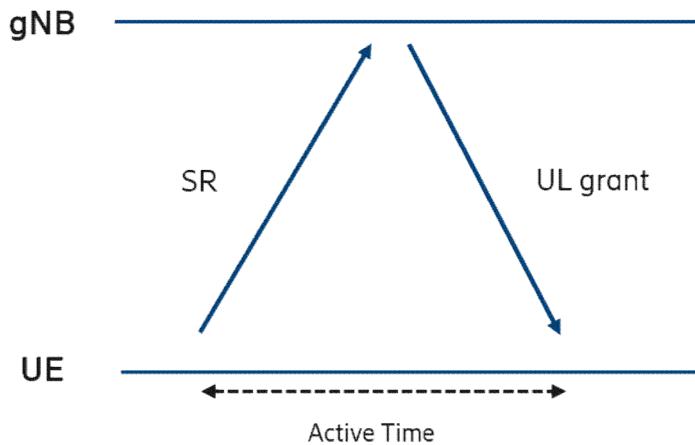


Figure 7.2.1.2-1: Example of UE-initiated active period time after sending SR

Possible Solution

A possible solution to save battery is to allow UE to discontinuously monitor the PDCCH during this time. It should however be noted that the network may schedule the UE directly after one of the cases above. The exact details should be discussed during the work phase.

On DRX after SR, as an example:

- UE starts offset to trigger the start of DRX active time after sending SR request on PUCCH, thus UE would not be required to monitor SR response (i.e PDCCH) while offset is running.

The details should be addressed during the work item phase, but some examples of the case of replying to the RAR in Contention-Free Random Access:

- the gNB may include an offset to trigger the start DRX Active time via RAR;
- The UE may have an RTT-variable configured.

7.2.1.2.1 DRX enhancements

Problem Statement

If HARQ is disabled and HARQ blind (re)transmissions are used then the DRX procedures may have some impact, see Figure 7.2.1.2-2.

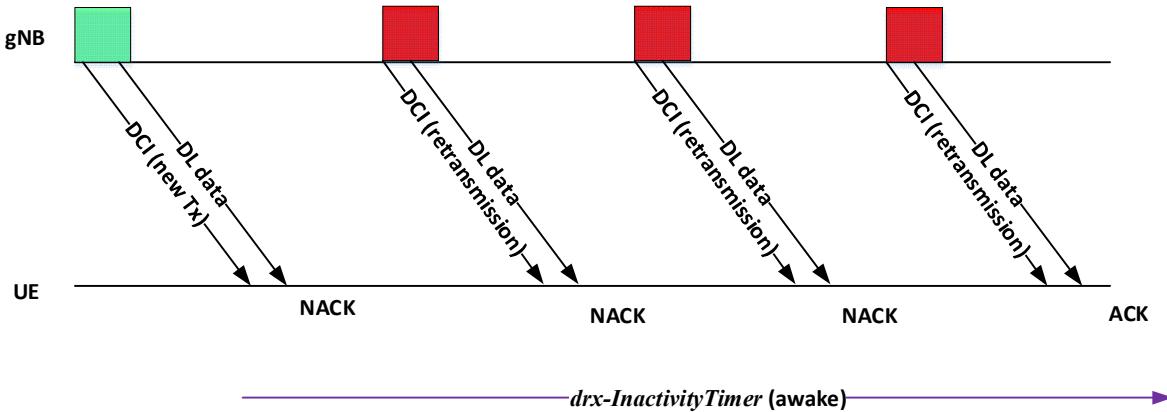


Figure 7.2.1.2-2: Example of blind HARQ (re)transmissions during drx-InactivityTimer

Possible Solution

One possible solution is to start the drx-RetransmissionTimer upon network scheduling via PDCCH so that UE can sleep in between blind HARQ (re)transmissions.

Some possible solutions to this are:

- On drx-InactivityTimer:
 - Use legacy drx-InactivityTimer in order to give gNB time to schedule blind HARQ (re)transmissions.
 - Use a dedicated drx-InactivityTimer for blind HARQ (re)transmissions.
- Start of drx-RetransmissionTimerDL may have a different set of solutions:
 - Can be started when the UE receives a PDCCH scheduling data.
 - Can be scheduled by PDCCH, where the details can be discussed during a work-item phase.
- Start of drx-RetransmissionTimerUL should also be considered.

Problem Statement

After RTT milliseconds, as seen from the UE, the network is allowed to reuse HARQ process IDs and could start sending DCI allocations to the UE. Since this period of time rarely will coincide with the active time of the UE DRX cycle, the network will likely need to delay any transmission to the first available onDuration period after that RTT ms have elapsed, introducing an extra delay on top of that introduced by the RTT of the NTN, see Figure 7.2.1.2-3.

Possible Solution/Option

This extra delay can be avoided by allowing the UE to leave its DRX state at the time when the first possible DCI could be received on PDCCH.

Some options on this could be:

- A longer value of drx-InactivityTimer can be configured for sufficient time for monitoring the new transmissions. And if the NW consider there is no transmission expected, it can send UE into DRX by DRX command to stop the monitoring of PDCCH.
- Short DRX cycle can be configured in the first few RTTs to monitor the PDCCH for new transmission and re-transmissions, and a long DRX will be used after expiration of short DRX.
- UE could enter active time and start monitoring the PDCCH after RTT milliseconds from the oldest not yet acknowledged transport block.
- UE could start the drx-RetransmissionTimerDL regardless of whether the data was successfully decoded or not.

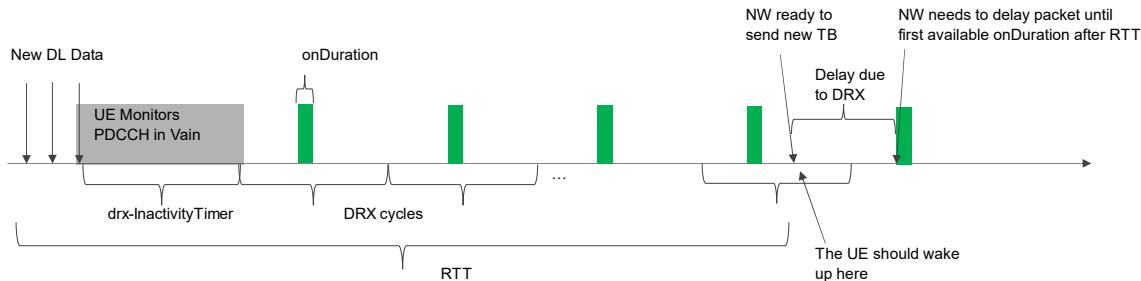


Figure 7.2.1.2-3: Unnecessary monitoring of PDCCH and extra delay due to HARQ stalling

7.2.1.3 Scheduling Request

Problem Statement

A UE can use a Scheduling Request (SR) to request UL-SCH resources from the gNB for a new transmission or a transmission with a higher priority. SR transmission is configured by RRC. During the prohibit timer (*sr-ProhibitTimer*) is active, no further SR is initiated. [75] The *sr-ProhibitTimer* will at latest expire after 128ms [76] and initiate a SR. For GEO systems the value range is not sufficient because the RTD is larger.

The *sr-ProhibitTimer* should be modified to support NTN.

Possible Solution

The value range of *sr-ProhibitTimer* should be extended to support NTN.

7.2.1.4 HARQ

The MAC sublayer supports error correction and/or repetition through HARQ as in NR Release 15. The HARQ functionality ensures delivery between peer entities at Layer 1.

For NTN the network could disable uplink HARQ feedback for downlink transmission at the UE receiver e.g. to support long propagation delays. Even if HARQ feedback is disabled, the HARQ processes are still configured. Enabling / disabling of HARQ feedback is a network decision signalled semi-statically to the UE by RRC signalling. The enabling / disabling of HARQ feedback for downlink transmission should be configurable on a per UE and per HARQ process basis via RRC signalling.

For NTN the network could disable HARQ uplink retransmission at the UE transmitter. Even if HARQ uplink retransmissions are disabled, the HARQ processes are still configured. The enabling / disabling of HARQ uplink retransmission could be configurable on a per UE, per HARQ process and per LCH basis. Details can be decided in a normative phase. And the LCP impact caused by disabling the HARQ uplink retransmission configuration can be discussed in the WI phase.

The network criteria of enabling / disabling HARQ feedback are not specified. Examples for possible criteria are latency or throughput service requirements, transmission roundtrip time etc. Other criteria are not excluded. Semi-Persistent Scheduling should to be supported for HARQ processes with enabled and disabled HARQ feedback. Details can be decided in the WI phase.

Multiple transmissions of the same TB in a bundle (e.g. MAC schedules packets in a bundle with pdsch-AggregationFactor > 1 in downlink and pusch-AggregationFactor > 1 in the uplink) according to NR Rel.15 are possible and might be useful to lower the residual BLER, particularly in case HARQ feedback is disabled. Soft combining of multiple transmissions according to NR Rel.15 is supported in the receiver. Multiple transmissions of the same TB (e.g. MAC schedules the same TB on the same HARQ process without the NDI being toggled) are possible and might also be useful to lower the residual BLER, particularly in case HARQ feedback is disabled. For the uplink this behaviour can be realised within the Rel.15 specification, minor changes on the UE procedure might be needed for the downlink transmission. Soft combining of multiple transmissions of the same TB by the MAC scheduler (e.g. MAC schedules the same TB on the same HARQ process without the NDI being toggled) according to NR Rel.15 is supported in the receiver.

If the feedback is disabled for a selective number (i.e. not all) of HARQ processes, the configuration parameters for different HARQ processes may need to be different.

7.2.1.5 Uplink scheduling

7.2.1.5.1 Assignment of uplink resources

Problem Statement

The typical procedure when data arrives in the buffer is to trigger a Buffer Status Report and if the UE does not have any uplink resources for transmitting the BSR, the UE will go on to do a Scheduling Request to ask for resources. Since the scheduling request is only an indication telling the network that the UE requires scheduling, the network will not know the full extent of the resources required to schedule the UE, thus first the network may typically schedule the UE with a grant large enough to send a BSR so that the network may schedule the UE more accordingly as seen in Figure 7.2.1.5-1.

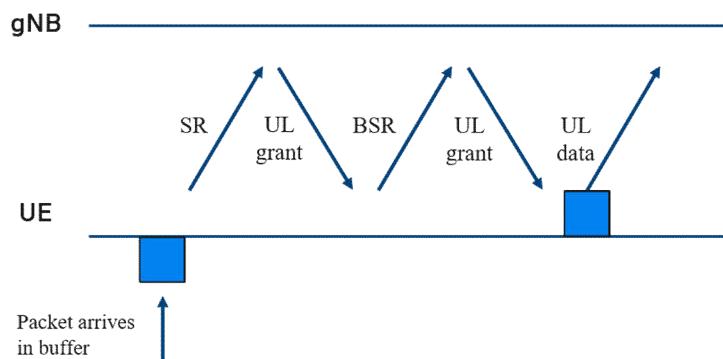


Figure 7.2.1.5-1: Scheduling of UE transmission

In non-terrestrial networks the drawback of this procedure is that it would take at least 2 Round-trip times from data arriving in the buffer at the UE side until it can be properly scheduled with resources that would fit the data and the required QoS. Due to the large propagation delays this may become prohibitively large.

Possible Solutions/options

In order to mitigate the problem there may be a number of possible solutions. In Table 7.2.1.5-1 some different options in terms of their pros, cons and delays have been characterized. However the feasibility of the solutions has not been discussed in detail and will be addressed during the work item phase.

Table 7.2.1.5-1: Scheduling enhancement options

Scheduling option	Pros	Cons	Delays*
SR-BSR procedure	- Low resource overhead required	- Large delays	At least 2 RTTs of delay
Sending large grant in response to SR	- Potentially low resource overhead	- Still takes 2 RTTs before UE has the BSR - Might be a waste in terms of resources since network is still not aware of the buffer situation of the UE	1 – 2 RTTs
Configured grant	- Low latency with right configuration	- Large overhead - Trade-off between latency and overhead	0 – 1 RTT**
BSR-indication in SR	- Low latency with correct configuration	- Large spec-impact - Resource overhead impact unclear, larger than SR	1 RTT
BSR over 2-step random access	- Low latency - Low overhead	- RACH resources required	0 – 1 RTT**

* the number of RTTs before full scheduling based on BSR can begin.
 ** if configured grant/2-step allocation is large enough and data can be transmitted in the grant.

7.2.2 RLC

7.2.2.1 Status Reporting

Problem Statement

A status report can be triggered by the polling procedure or by detection of reception failure of an AMD PDU which is indicated by the expiration of t-Reassembly. This timer is started when an AMD PDU segment is received from lower layer, is placed in the reception buffer, at least one byte segment of the corresponding SDU is missing and the timer is not already running. The procedure to detect loss of RLC PDUs at lower layers by expiration of timer t-Reassembly is used in RLC AM as well as in RLC UM. [TS 38.322] The timer t-Reassembly can be configured by fixed values between 0 and 200ms [76]. For the terrestrial case this timer covers the largest time interval in which the individual segments of the corresponding SDU have to arrive out of order at the receiver due to SDU segmentation and/or HARQ retransmissions before a status report and consequently an ARQ-retransmission is triggered. If HARQ is supported by NTN, an extension of the t-Reassembly timer could become necessary, because then the timer should cover the maximum time allowed for HARQ transmission which will probably be a value larger than the RTD.

If HARQ is supported by NTN, the timer t-Reassembly should be modified to support NTN.

Possible Solution

If HARQ is supported by NTN, the value range of *t-Reassembly* should be extended to support NTN.

One possible solution to extend *t-Reassembly* would be to consider the UE-specific round-trip delay, *RTD*, the number of allowed HARQ-retransmission attempts *nrof_HARQ_retrans*, as well as a configurable offset to account for possible delays on UE and network-side, *scheduling_offset*:

$$t\text{-Reassembly} = RTD * nrof_HARQ_retrans + scheduling_offset$$

This would ensure that the HARQ delay can be correctly accounted for reassembling.

No modification of the t-PollRetransmit timer and of the t-statusProhibit timer are needed to support NTN.

7.2.2.2 RLC Sequence Numbers

Problem statement

12bit and 18bit are specified as possible RLC AM sequence number (SN) field length in NR [TS 38.322]. The maximum *AM_Window_Size* results in 131 072.

The sequence number space needed for a radio bearer depends on the data rate that is to be supported, the retransmission time (i.e the RTD, the number of retransmissions and the scheduling delay) as well as the average size of the RLC SDUs.

The basic formula for calculating the supportable RLC bit rate for one radio bearer is

$$RLC_data_rate = RLC_SDU_size \cdot 2^{(SN_length - 1)} / RetransmissionTime,$$

For selecting reasonable values:

- RLC_SDU_size depends entirely on the specific traffic and it is difficult to give a good estimate for a typical SDU size. For continuous data, it is probably more likely that the RLC SDUs are bigger rather than small. Sizes of 500 and 1500 Bytes are considered here.
- SN_length: Selecting the SN field length depends on the application, but for continuous and high-rate applications, the SN field length should be chosen to be large.
- RetransmissionTime: In RLC, the retransmission time of RLC SDUs is dependent on the time that it takes for the transmitting RLC entity to retransmit an RLC SDU when it is lost. RLC retransmissions are based on RLC status reporting and these need to be scheduled the way any data need to be scheduled, thus the retransmission time may be difficult to characterize. One simplification for the retransmission time would be $RetransmissionTime = (RTD \cdot (\maxRetxThreshold+1))$. With $RTD = (25.77 \text{ ms}, 541.46 \text{ ms})$ and $\maxRetxThreshold = (1, 4)$ we get retransmission times (51.54 ms, 128.85 ms, 1082.92 ms, 2707.3 ms) which rounded up to account for scheduling delays become (75 ms, 150 ms, 1.5 s, 3.0 s).
- RTD depends on the considered scenario. In GEO satellite systems 541.46ms is assumed as maximum RTD for the transparent architecture, while in LEO satellite systems with transparent architecture 25.77 ms is assumed.
- maxRetxThreshold: In NTN, HARQ may be disabled and therefore retransmissions in the RLC layer are essential for a reliable communication link. Nevertheless, the latency as seen by the core network or the application becomes extremely large if too many retransmissions are being configured. The maximum number of RLC retransmissions in NTN will be limited by interactions with higher layer and will be smaller compared to terrestrial networks. 1 or 4 RLC retransmissions are considered here.

Table 7.2.2.2-1 and Table 7.2.2.2-2 presents supportable RLC bit rates for different sets of parameter, for GEO satellite systems and LEO satellite systems, respectively.

Table 7.2.2.2-1: Supportable RLC bit rates for GEO satellite systems with transparent architecture

RLC_SDU_size	SN_length	RTD	maxRetxThreshold	RetransmissionTime	RLC_data_rate
500Byte	18	541.46 ms	1	1.5 s	350 Mbps
1500Byte	18	541.46 ms	1	1.5 s	1 049 Mbps
500Byte	18	541.46 ms	4	3.0 s	175 Mbps
1500Byte	18	541.46 ms	4	3.0 s	524 Mbps

Table 7.2.2.2-2: Supportable RLC bit rates for LEO satellite systems with transparent architecture

RLC_SDU_size	SN_length	RTD	maxRetxThreshold	RetransmissionTime	RLC_data_rate
500Byte	18	25.77 ms	1	75.0 ms	6 991 Mbps
1500Byte	18	25.77 ms	1	75.0 ms	20 972 Mbps
500Byte	18	25.77 ms	4	150.0 ms	3 495 Mbps
1500Byte	18	25.77 ms	4	150.0 ms	10 486 Mbps

Considering Table B.2-1, it is observed that the airplanes connectivity which targets an experience data rate of 360 Mbps for DL is the most challenging usage scenario for NTN in terms of data rate.

Assuming a retransmission time of 3.0 s or 1.5 s, which represents a GEO satellite system with transparent architecture and an RLC SDU size of 500 Byte, the NTN targeted experience data rate for usage scenario airplanes connectivity cannot be achieved.

Assuming a retransmission time of 150 ms, which represents a LEO satellite system with transparent architecture and an RLC SDU size of 500 Byte or larger the NTN targeted experience data rate can be achieved for the considered usage scenarios.

Possible Solution

There are three options identified to cope with this limitation:

- Option 1: The current specification is applied for NTN without any changes. The targeted experience data rate for usage scenario airplanes connectivity may at least temporarily not be supported for the above mentioned configurations of RLC SDU size, RLC SN field length and maximum number of RLC retransmissions in case of GEO satellite systems with transparent architecture.
- Option 2: Extending the RLC SN length.
- Option 3: Reducing the delays that it takes to perform an RLC retransmission.

7.2.3 PDCP

7.2.3.1 SDU Discard

Problem Statement

The transmitting PDCP entity shall discard the PDCP SDU when the discardTimer expires for a PDCP SDU or when a status report confirms the successful delivery [TS 38.322]. The discardTimer can be configured between 10 ms and 1500 ms or can be switched off by choosing infinity [76].

The discardTimer mainly reflects the QoS requirements of the packets belonging to a service. However, by choosing the expiration time of the discardTimer or the QoS requirements, the RTD as well as the number of retransmissions on RLC layer and/or HARQ shall be considered. By increasing the expiration time of discardTimer, one should keep in mind that extended timer values will increase the amount of required memory for the buffer.

Modification of the discardTimer can be discussed in the WI phase.

7.2.3.2 Reordering and In-order Delivery

Problem Statement

In order to detect loss of PDCP Data PDUs, there is the timer t-Reordering which is started or reset when a PDCP SDU is delivered to upper layers [TS 38.322]. The maximum configurable expiration time is 3000 ms [76]. This might limit the overall number of retransmissions of the RLC AM ARQ protocol for NTN.

Modification of the t-Reordering timer can be discussed in the WI phase.

7.2.3.3 PDCP Sequence Number and Window Size

Problem statement

12bit and 18bit are specified as possible PDCP sequence number (SN) field length in NR [TS 38.323]. Resulting in a maximum of 262 144 different SNs or a Window_Size of 131 072.

The sequence number space needed for a radio bearer depends on the data rate that is to be supported, the retransmission time as well as the average size of the PDCP SDUs.

The basic formula for calculating the supportable PDCP bit rate for one radio bearer is

$$\text{PDCP_data_rate} = \text{PDCP_SDU_size} \cdot 2^{(\text{pdcn-SN-Size}-1)} / \text{PDCP_RetransmissionTime},$$

For selecting reasonable values:

- PDCP_SDU_size: As the RLC_SDU_size, it depends entirely on the specific traffic and it is difficult to give a good estimate for a typical SDU size. For continuous data, it is probably more likely that the PDCP SDUs are bigger rather than small. In general, PDCP packets might be larger than RLC packets because of possible segmentation in RLC layer, however, for large data rate it is assumed that they are in the same range as RLC_SDU_size. Sizes of 500 and 1500 Bytes are considered here.
- pdcp-SN-Size: Selecting the SN field length depends on the application, but for continuous and high-rate applications, the SN field length should be chosen to be large.
- PDCP_RetransmissionTime is the time seen by the PDCP layer between creation of the packet and registration of successful or failed transmission. If HARQ is disabled, it mainly depends on the RLC RetransmissionTime. (75ms, 150ms, 1.5s, 3.0s) are considered here. These numbers result from a round trip delay of RTD = (25.77ms, 541.46ms) and RLC maxRetxThreshold = (1,4), see section 7.2.2.2

Table 7.2.3.3-1 and Table 7.2.3.3-2 presents supportable PDCP bit rates for different sets of parameter, for GEO satellite systems and LEO satellite systems, respectively.

Table 7.2.3.3-1: Supportable PDCP bit rates for GEO satellite systems with transparent architecture

PDCP_SDU_size	pdcp-SN-Size	PDCP_RetransmissionTime	PDCP_data_rate
500 Byte	18	1.5 s	350 Mbps
1500 Byte	18	1.5 s	1049 Mbps
500 Byte	18	3.0 s	175 Mbps
1500 Byte	18	3.0 s	524 Mbps

Table 7.2.3.3-2: Supportable PDCP bit rates for LEO satellite systems with transparent architecture

PDCP_SDU_size	pdcp-SN-Size	PDCP_RetransmissionTime	PDCP_data_rate
500 Byte	18	75 ms	6991 Mbps
1500 Byte	18	75 ms	20972 Mbps
500 Byte	18	150 ms	3495 Mbps
1500 Byte	18	150 ms	10486 Mbps

Considering Table B.2-1, it is observed that the airplanes connectivity which targets an experience data rate of 360 Mbps for DL is the most challenging usage scenario for NTN in terms of data rate.

Assuming a PDCP retransmission time of 3.0 s or 1.5 s, which represents a GEO satellite system with transparent architecture and a PDCP SDU size of 500 Byte, the NTN targeted experience data rate for usage scenario airplanes connectivity cannot be achieved.

Assuming a PDCP retransmission time of 150 ms, which represents a LEO satellite system with transparent architecture and an RLC SDU size of 500 Byte or larger the NTN targeted experience data rate can be achieved for the considered usage scenarios.

Possible Solution

There are three options identified to cope with this limitation:

Option 1: The current specification is applied for NTN without any changes. The targeted experience data rate for usage scenario airplanes connectivity may at least temporarily not be supported for the above mentioned configurations of PDCP SDU size, PDCP SN field length and maximum number of RLC retransmissions in case of GEO satellite systems with transparent architecture.

Option 2: Extending the PDCP SN length.

Option 3: Reducing the delays that it takes to perform retransmissions.

7.2.4 SDAP

The SDAP layer is responsible for the mapping between QoS flows and DRBs [9]. It is not affected by the large round trip delays (RTD) occurring in NTN. There are no modifications needed in the SDAP layer to support non-terrestrial networks.

7.3 Control plane enhancements

Satellite beams or satellites are not considered to be visible from UE perspective in NTN. This does not preclude differentiating at the PLMN level the type of network (e.g. NTN vs. terrestrial).

NOTE: Rel-15 definitions are considered as a baseline for NTN

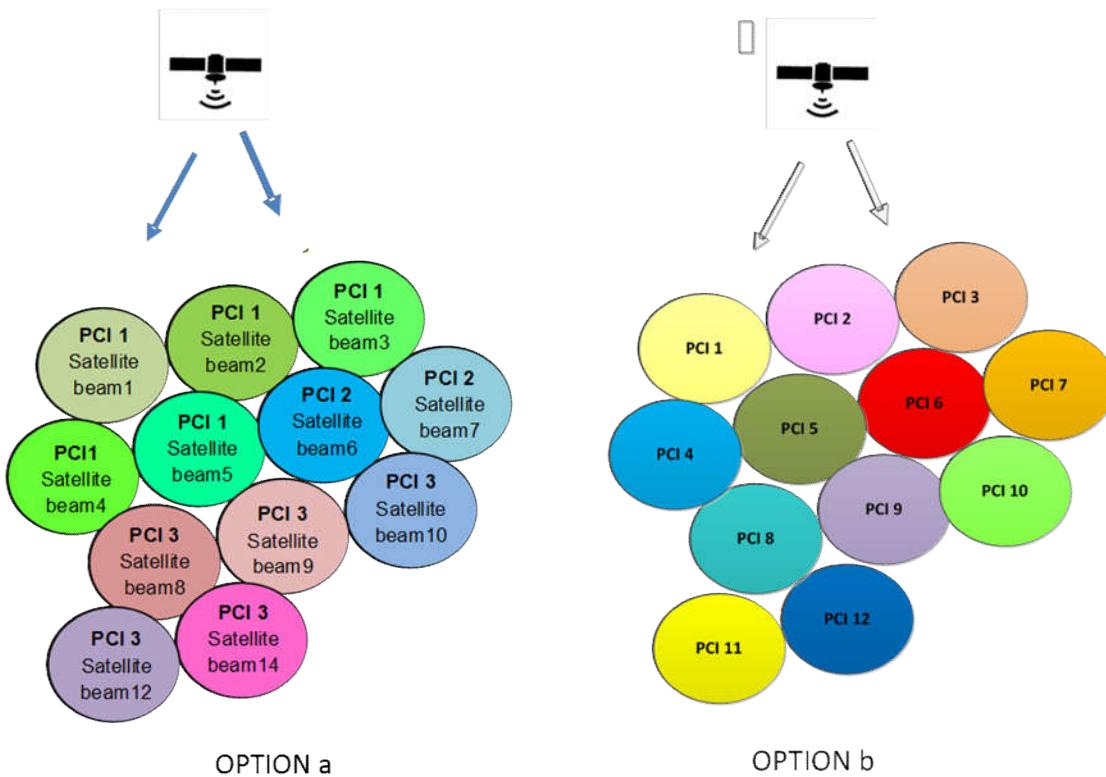


Figure 7.3-1: Options for PCI mapping into satellite beams

Both options a) same PCI for several satellite beams and b) one PCI per satellite beam, can be considered in NTN. A satellite beam can consist of one or more SSB beams. One cell (PCI) can have maximum of L SSB beams, where L can be 4, 8 or 64 depending on the band.

Similar to TN, one or several SSB index can be used per PCI to separate SSB transmission on different beams.

In TN, the mapping of antenna ports or physical beams to SSB index is left for implementation. In NTN, the association between satellite beams and SSBs index is left for implementation (i.e. it will not be specified).

Two different type of UE categories are supported by NTN: 1) with GNSS support, 2) without GNSS support.

The use of satellite ephemeris, time and UE location can be used in RAN for mobility purposes.

As per tracking area:

- For GEO, the current tracking area management is assumed as a baseline
- For LEO with moving beams study fixed and moving tracking area solutions

7.3.1 Idle mode mobility enhancements

7.3.1.1 General Tracking Area Issues [16]

Satellites may provide very large cells, covering hundreds of kilometres, and consequently would lead to large tracking areas. In this scenario the tracking area updates (TAUs) are minimal, however the paging load could be high because it then relates to the number of devices in the tracking area.

Moving cells and consequently moving tracking areas would be difficult to manage in the network as the contrast between the TAU and the paging signalling load would be too extreme to find a practical compromise.

On one hand, small tracking Areas would lead to massive TAU signalling for UE at the boundary between 2 TAs as illustrated in figure 7.3.1.1-1.

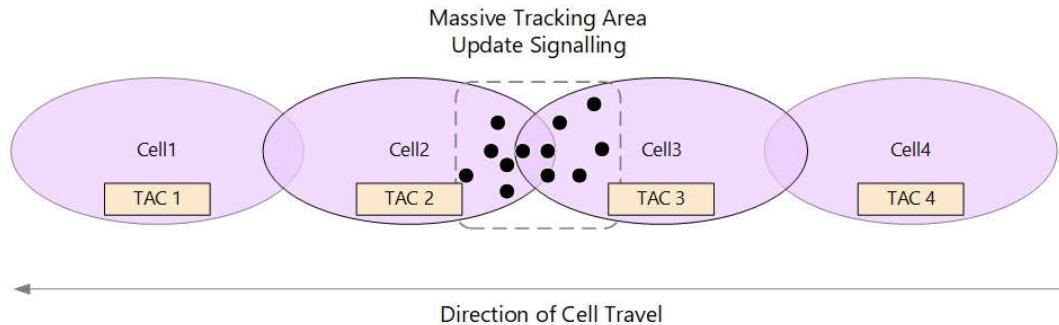


Figure 7.3.1.1-1: Moving Cells and Small tracking Areas leading to massive TAU signalling

On the other hand, wide tracking Areas would lead to high paging load in the satellite beams as illustrated in Figure 7.3.1.1-2.

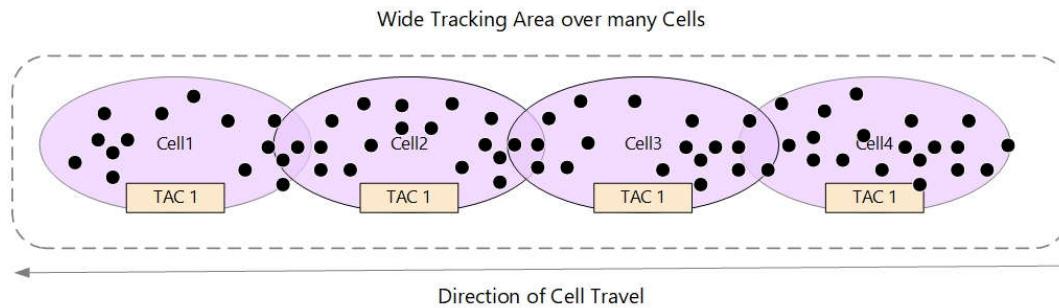


Figure 7.3.1.1-2: Moving Cells and wide tracking Areas leading to higher Paging load

However, Tracking areas must be dimensioned to minimise the TAUs as this is more signalling-intensive than paging on the network.

In practical tracking area design, one of the criteria affecting the performance and capacity is the limiting capabilities of MME/AMF platforms and the radio channel capacity.

Ping-pong effect generating excessive TAU, and it can be minimised by ensuring 10-20% overlaps between the adjacent cells and appropriate allocation of TAI List to UEs especially at the edge of cells/TAs.

7.3.1.2 Moving Tracking Area for NTN LEO, Scenario C2 and D2 [17]

Moving tracking area means that the tracking area sweeps over the ground as the cells move. Due to high speed movement of satellite, the satellite beam and therefore the cell providing coverage for an earth stationary UE will be changed frequently. As a result, a stationary UE would have to keep performing Registration area update (can also be called as tracking area update, i.e. TAU) in RRC_IDLE state. For each Registration area update, the UE needs to initiate connection with the network. For Rel-15 NR this requires 4-steps of the random access procedure followed by some RRC message exchange over the service link. This can become a non-acceptable overhead if all IDLE mode UEs in the registration area need to perform tracking area update (TAU) frequently as the LEO satellite passes by. If the geographical area covered by the Registration area is large, this issue may become slightly less severe. However, size of the Registration area and paging capacity forms a trade-off as the UE may need to be paged via all cells belonging to the Registration area and thus the paging capacity may become an issue when network initiated calls arrive.

7.3.1.3 Fixed Tracking Area for NTN LEO, Scenario C2 and D2 [17]

7.3.1.3.1 Approach 1: For the case when UE location information is unavailable

In order not to have TAU performed frequently by the UE triggered by the satellite motion, the tracking area may be designed to be fixed on ground. For NTN LEO, this implies that while the cells sweep on the ground, the tracking area code (i.e. TAC) broadcasted is changed when the cell arrives to the area of next planned earth fixed tracking area location.

The TAC, or a list of TACs, broadcasted by the gNB needs to be updated as the gNB enters to the area of next planned tracking area. When the UE detects entering a tracking area that is not in the list of tracking areas that the UE previously registered in the network, a mobility registration update procedure will be triggered.

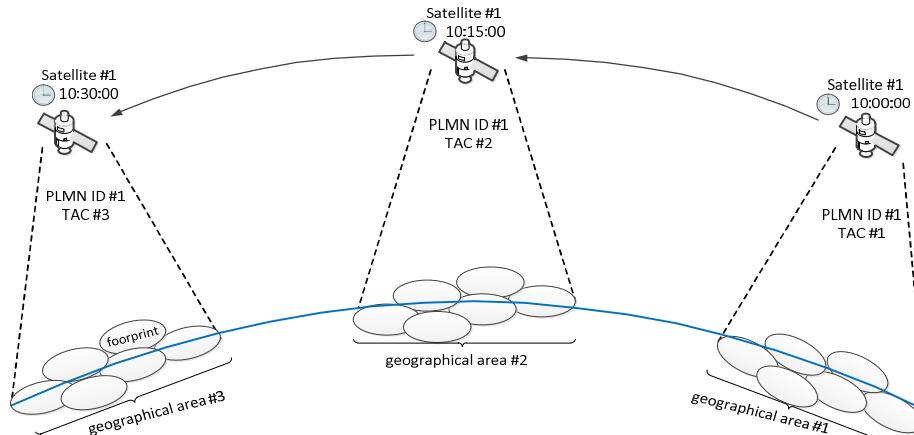


Figure 7.3.1.3.1-1: An example of updating TAC and PLMN ID in real-time for scenario C2 and D2

As shown in Figure 7.3.1.3.1-1, network update the broadcast TAC in real time according to the ephemeris and confirm the broadcast TAC is associated with the geographical area covered by the satellite beam. UE listens to TAI = PLMN ID + TAC and determines to trigger registration area update procedure based on the broadcast TAC and PLMN ID when it moves out of the registration area.

This approach allows to use Rel-15 NR network procedures and can be applied to UE with or without location information.

Two possible options should be studied to update the broadcast TAC:

"hard switch" option: one cell broadcast only one TAC per PLMN. The new TAC replaces the old TAC and there may be some fluctuation at the border area. As shown in Figure 7.3.1.3.1-2, the UE will see its TAC changing like TAC-2->TAC-1->TAC-2 from T1 to T3.

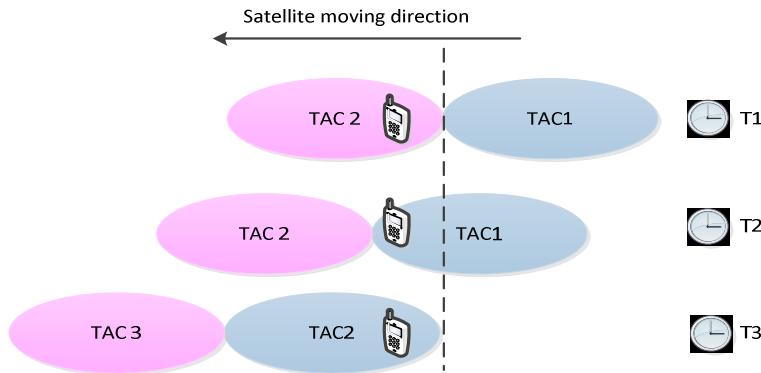


Figure 7.3.1.3.1-2: TAC fluctuation at the border area

"soft switch" option: one cell can broadcast more than one TACs per PLMN. The cell adds the new TAC in its system information in addition to the old and removes the old a bit later. If there is a chain of TAs, the TA list adds one TA more and removes one old while the cell sweeps the ground. This also reduces the amount of TAUs for UEs that happen to be located at the border area. However, for the "soft switch" option, the more TACs a cell broadcast, the heavier paging load it experiences, which usually leads to a significant imbalance distribution of paging load among cells. Thus, there is a trade-off between paging load and balancing the fluctuation of actual TA area enabled by the soft switch to be considered in network planning and implementation.

In some area, the gNB may not be able to provide NTN service and thus not broadcast TAC(s).

7.3.1.3.2 Approach 2: For the case when UE location information is available

One possible solution is to divide the earth into a lot of geographical areas and each geographical area is mapped to a certain TAC. During initial registration, UE derives the TAC based on its location information (the mapping rule between the geographical area and the TAC value is kept both on UE side and network side), forms the TAI based on the derived TAC and broadcast PLMN ID and reports the TAI to network via Registration Request message. The AMF confirms the reported TAI and includes a TAI list as a registration area the UE is registered to in the Registration Accept message.

When UE moves to a new geographical area, UE derives the TAC based on the location information and forms the TAI based on the derived TAC and PLMN ID. If UE detects entering a tracking area that is not in the list of tracking areas that the UE previously registered to, a mobility registration update procedure will be triggered. UE reports the TAI derived by itself to network via Registration Request message. The AMF confirms the reported TAI and include a new TAI list for the UE in the Registration Accept message. The UE, upon receiving a Registration Accept message, shall delete its old TAI list and store the received TAI list.

7.3.1.3.3 Tracking Area recommendation

Fixed Tracking Area is recommended for the WI phase

7.3.1.4 Enhancements to idle/inactive UE mobility procedure

For the idle/inactive mode UE procedures in NTN, NR mechanism in TN system is regarded as the baseline. Regarding the adaptation of existing procedures, followings issues were considered.

- For too frequent SI update issue, no problematic case was identified. This issue can be solved by network implementation.
- Under earth-fixed tracking area mechanism, cells sweeping the Earth do not cause heavy signalling burden because of frequent TAU for the LEO satellites.
- For UEs with low transmission power camping on the cell with high altitude issue, if UE is able to identify GEO cell, it can be left for UE implementation to avoid this issue and no additional mechanism is needed.

7.3.1.5 Mobility state estimation mechanism

For GEO satellites, the cell coverage is very large so that UE's mobility will happen very rare. For LEO satellites, the UE's speed can be ignored compared to the speed of LEO satellites. Therefore, as use case of MSE is not clear in both GEO and LEO case, the MSE mechanism for NTN usage is left for implementation decision.

7.3.1.6 Using ephemeris information and UE location information

Ephemeris information and UE location information can be used to help UEs perform measurement and cell selection/reselection, in addition to PCI and frequency information included in the broadcast system information. How to deliver and utilize the information can be defined in the WI phase.

7.3.1.7 System information broadcast

As LEO satellites are moving in predictable path, so their neighbour cell list is also predictable. The neighbour cell list can be provided via broadcast system information, as is currently done in NR.

7.3.2 Connected mode mobility enhancements

For GEO NTN, mobility management procedures require adaptations to accommodate large propagation delay. In particular radio link management may require specific configuration.

For LEO NTN, mobility management procedures should be enhanced to take into account satellite movement related aspects such as measurement validity, UE velocity, movement direction, large and varying propagation delay and dynamic neighbour cell set.

7.3.2.1 Mobility Challenges for Non-Terrestrial Networks

7.3.2.1.1 Latency associated with mobility signalling

Propagation delay in NTN is orders of magnitude higher than terrestrial systems, introducing additional latency to mobility signalling such as measurement reporting, reception of the HO command, and HO request/ACK (if the target cell originates from a different satellite).

The basic handover procedure is illustrated in Figure 7.3.2.1.1-1, and the processing delay in both gNB side and UE side are marked.

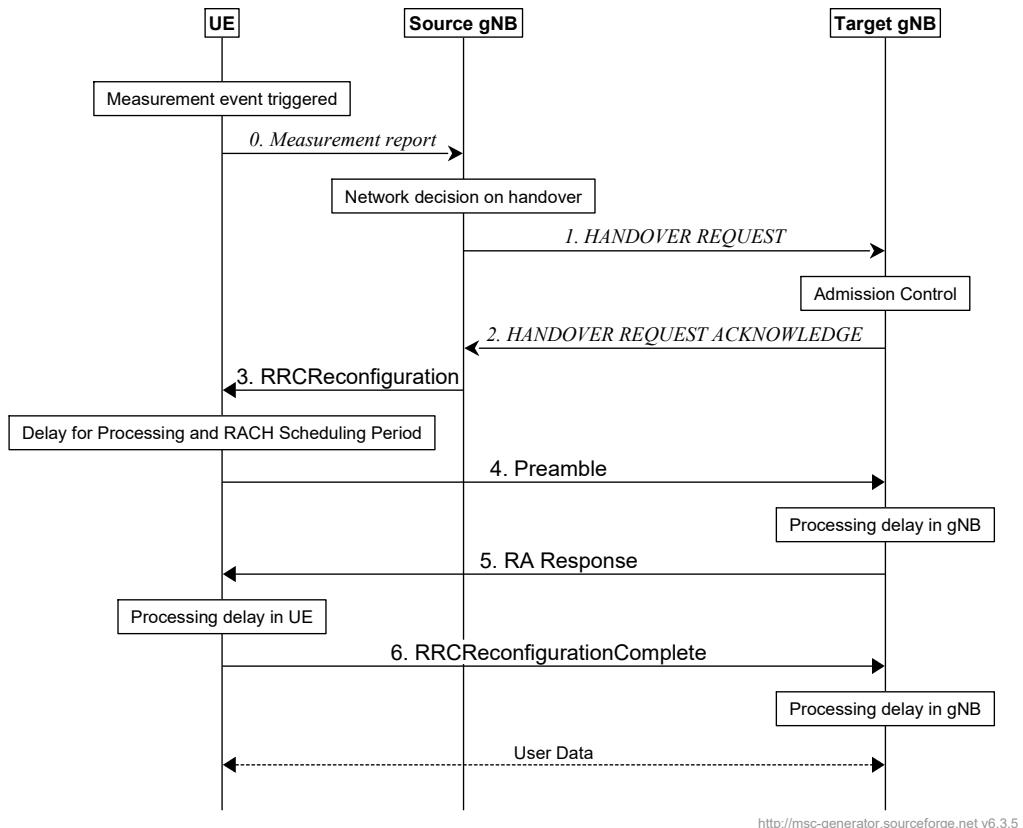


Figure 7.3.2.1.1-1: Handover procedure

The service interruption time is defined in TR 36.881 by the time between when the UE stops transmission/reception with the source gNB and the time when target gNB resumes transmission/reception. The interruption time is however different regarding to uplink and downlink.

For the downlink the interruption time can be defined as the time from network sending RRCReconfiguration with sync (Step 3) until the target gNB receives the RRCReconfigurationComplete (Step 6). Since the gNB cannot send more data after step 3, and it can continue after it receives RRCReconfigurationComplete. For the uplink, the UE can potentially continue sending data to the source gNB until RRCReconfiguration with sync is received, the interruption time can be defined as the time from UE receiving RRCReconfiguration with sync (Step 3) until the target gNB receives the RRCReconfigurationComplete (Step 6).

Without considering latencies such as RRC processing delay and UE retuning its frequency circuits (which is smaller than the RTT), the interruption time would be 2 RTT (about 1080ms) for downlink and 1.5 RTT (about 810ms) for uplink.

GEO scenarios are characterized by much larger propagation delay than LEO, however the latter requires consideration of satellite movement. To avoid extended service interruption, latency associated with mobility signalling should be addressed with high priority in both cases. Solutions developed may apply to both scenarios.

NOTE: Although such latency may result in a service interruption, it does not necessarily mean the UE will miss the HO command.

7.3.2.1.2 Measurement Validity

Extending Rel-15 measurement-based mobility mechanisms to NTN may introduce the risk of outdated measurements given sufficient delay between transmission of the measurement report and reception of the HO command. The measurements may no longer be valid, possibly leading to an incorrect mobility action e.g. early/late handover.

Although LEO scenarios exhibit less propagation delay, satellite movement may have an impact on measurement validity. Satellite ephemeris and/or UE location may be beneficial in addressing this challenge.

Measurement validity is not anticipated to be a challenge in GEO scenarios given the large cell size/overlap, small signal variation, and relatively low UE mobility. GEO scenarios may thus be addressed by suitable configuration using existing Rel-15 mechanisms.

7.3.2.1.3 Cell overlap and reduced signal strength variation

In terrestrial systems, a UE can determine it is near a cell edge due to a clear difference in RSRP as compared to cell center. Such an effect may not be as pronounced in non-terrestrial deployments, resulting in a small difference in signal strength between two beams in a region of overlap. As the Rel-15 handover mechanism is based on measurement events (e.g. A3), the UE may thus have difficulty distinguishing the better cell.

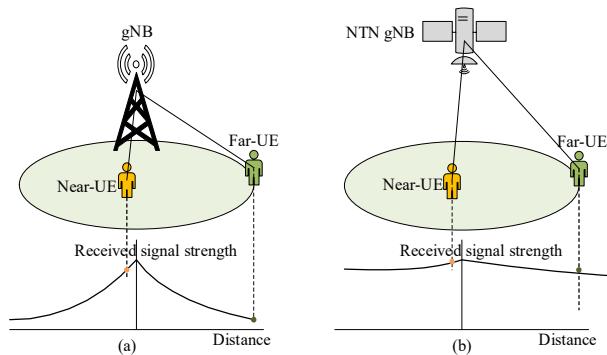


Figure 7.3.2.1.3-1: A sketch of near-far effect in different scenarios: (a) Terrestrial Network; (b) NTN

To avoid an overall reduction in HO robustness due to the UE ping-ponging between cells, this challenge should be addressed with high priority for both GEO and LEO scenarios.

Location information and/or satellite ephemeris would be useful in addition to measurement results, and solutions may apply to both scenarios.

7.3.2.1.4 Frequent and unavoidable handover

Satellites in non-GEO orbits move with high speed relative to a fixed position on earth, leading to frequent and unavoidable handover for both stationary and moving UEs. This may result in significant signalling overhead and impact power consumption, as well as exacerbating other potential challenges related to mobility e.g. service interruption due to signalling latency.

For a UE travelling at a constant speed and direction, the maximum time it can remain connected to a cell is approximated by dividing the cell diameter by UE speed. For NTN LEO deployments, the cell size is divided by the relative speed between the satellite and the UE, where a UE moving in the same direction as the satellite subtracts from the relative speed, and a UE moving in the opposite direction increases relative speed, described by the equation below:

$$\text{Time to HO(s)} = \frac{\text{cell size(km)}}{\text{UE speed } \left(\frac{\text{km}}{\text{hr}} \right) \cdot \left(\frac{1\text{hr}}{3600\text{s}} \right) + \text{satellite speed } \left(\frac{\text{km}}{\text{s}} \right)}$$

The scenario of cell diameter = one 50 km diameter beam will represent the lower bound (i.e. worst-case scenario for HO frequency), and cell diameter = 1000 km will be taken as the upper bound (i.e. best-case scenario for HO frequency).

Substituting reference values from 4.2-2 and 7.1-1 into the above equation, the maximum time a UE can remain in an NTN cell (i.e. the UE connects immediately at cell edge and leaves at the opposite cell edge) for the min/max cell diameter and relative speed is listed in the table below:

Table 7.3.2.1.4-1: Time to HO for min/max cell diameter and varying UE speed

Cell Diameter Size (km)	UE Speed (km/hr)	Satellite Speed (km/s)	Time to HO (s)
50 (lower bound)	+500	7.56 (NOTE 1)	6.49
	-500		6.74
	+1200		6.33
	-1200		6.92
	Neglected		6.61
	+500		129.89
1000 (upper bound)	-500		134.75
	+1200		126.69
	-1200		138.38
	Neglected		132.28

Neglecting UE movement, a UE served by an NTN LEO cell of diameter 50 km and 1000 km may remain connected for a maximum of 6.61 seconds and 132.38 seconds respectively due to satellite movement. Considering UE movement, this will vary by approximately +/- 4%. By neglecting satellite speed and setting UE speed to 500 km/hr as per table 7.1-1, this is equivalent to a terrestrial UE being served by a cell diameter ranging from approximately 0.918 km (NOTE 2) to 18.39 km.

From the above analysis, it is concluded that HO frequency in LEO NTN can be similar to that experienced by a terrestrial UE on a high-speed train, however this represents a worst-case scenario and is not indicative of a typical terrestrial network. It is not anticipated that frequent HO will occur in GEO due to large cell size limiting the impact of UE speed. It is further assumed in LEO scenarios UE speed is a negligible factor in HO frequency given the relative speed of the satellite, and this will principally be an issue for LEO with moving beams.

NOTE 1: This value may need to be updated further pending clarification from satellite companies (e.g. if this is the ground speed, and what altitude this value corresponds to).

NOTE 2: it is assumed that this is the minimum cell diameter possible (i.e. the UE travels directly through the full cell diameter). Should the UE only travel through an edge portion of the coverage the cell must be larger.

7.3.2.1.5 Dynamic neighbour cell set

In non-GEO deployments satellites constantly move with respect to a fixed point on earth. Such movement may have several implications to the UE, such as how long a candidate cell will remain valid.

Given the deterministic movement of satellites in LEO, the network may be able to compensate for the changing cell set via existing Rel-15 mechanisms, possibly with the aid of UE location.

As GEO satellites are relatively static, dynamic neighbour cell set is not anticipated to be a challenge.

[NOTE: Enhancements, if developed, should be coordinated with cell selection/re-selection in the IDLE/INACTIVE section]

7.3.2.1.6 Handover for a large number of UEs

Considering the large cell size of non-terrestrial networks, many devices may be served within a single cell. Depending on constellation assumptions (e.g. propagation delay and satellite speed) and UE density, a potentially very large number of UEs may need to perform HO at a given time, leading to possibly large signalling overhead and service continuity challenges.

Though the actual number of UEs performing HO at a given time will vary based on UE density, a general approximation can be made by observing the time it takes for the cell to move completely out of the original footprint ("c" in Figure 7.3.2.1.6-1), at which point all UEs served in the cell at time T ("a") must be handed over to a new cell. Dividing the total number of connected UEs by the time it takes for the cell to perform this transition can thus provide a general approximation of the average rate UEs must hand-out of a cell for a given cell diameter.

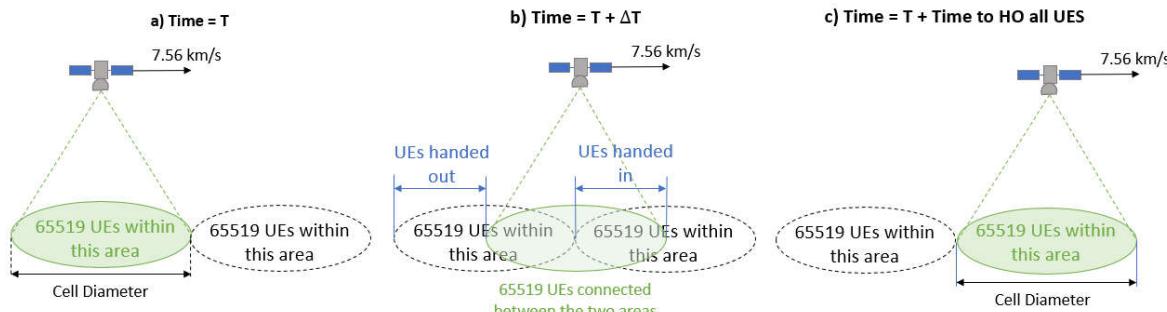


Figure 7.3.2.1.6-1: Transition of UEs as a cell moves completely out of original coverage area

However, as UEs are "handing-out" from the area no longer served by the cell, other UEs are also "handing-in" from the new area of coverage (as shown in "b)"). Assuming for simplicity a relatively uniform distribution of UEs, the rate of UEs leaving the cell will be approximately equal to the rate of UEs entering the cell. Therefore, the total mobility for the cell (hand-in + hand-out) will be approximately 2x the rate of hand-out.

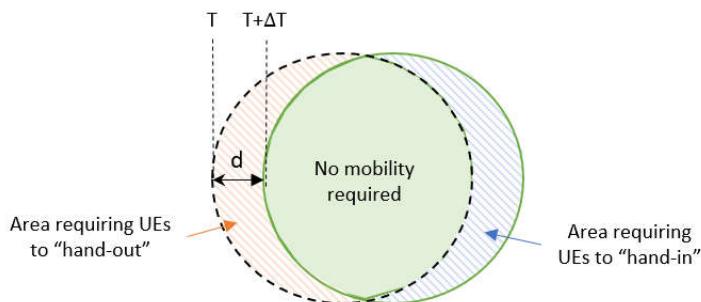


Figure 7.3.2.1.6-2: Comparison of Area requiring UEs to "hand-in" vs. "hand-out" of a cell

For the values provided in Table 7.3.2.1.6-1, the maximum number of UEs possible with the current maximum C-RNTI value (i.e. 65519) (NOTE 1) will remain connected to the cell at all times (e.g. the rate of UEs leaving a cell is equal to the rate of UEs entering a cell) to estimate the worst-case scenario, and UE movement is neglected.

Table 7.3.2.1.6-1: Average HO rate for a given cell diameter, assuming 65519 connected UEs (NOTE 1)

Cell Diameter (km)	Approximate Cell Area (km ²)	Average UE density (UE/km ²)	Satellite speed (km/s)	Time to HO all UEs in cell (s)	Average "hand-out" rate (UE/s)	Average HO Rate (in+out) (UEs/s)
50	1964	33.36	7.56 (NORE 2)	6.61	9912	19824
100	7854	8.34		13.23	4952	9904
250	49087	1.33		33.07	1981	3962
500	196000	0.33		66.14	991	1982
1000	785000	0.08		132.28	495	990

It is anticipated that the continuous movement of satellites in LEO scenarios with moving beams is the main challenge to be addressed with priority, and that the GEO scenario will not be greatly affected due to the large cell size/overlap and low relative UE speed.

NOTE 1: The above analysis assumes the current maximum C-RNTI value (i.e. 65519 connected UEs). This analysis may be updated should the C-RNTI value be modified in NTN (e.g. to accommodate higher average UE densities for large cell diameters).

NOTE 2: This value may need to be updated further pending clarification from satellite companies (e.g. if this is the satellite speed on the ground, and what altitude this value corresponds to).

FFS: An analysis of "Peak HO rate" e.g. should the satellite move over a small area with many UEs, and how the HO rate would change considering steerable satellite beams.

7.3.2.1.7 Impact of Propagation Delay Difference on Measurements

Consider a UE served by a LEO satellite S1, however also within coverage of an incoming LEO satellite S2. The UE should perform measurements of the neighbouring cells originating from S2 for mobility purposes based on the measurement configuration provided to the UE, however the propagation delay difference from the UE to satellite S1 and the UE to satellite S2 may vary significantly.

If the SMTC measurement gap configuration does not consider the propagation delay difference, the UE may miss the SSB/CSI-RS measurement window and will thus be unable to perform measurements on the configured reference signals. This challenge is captured for both GEO and LEO scenarios, and is to be addressed with priority for LEO scenarios.

FFS: The scale of this problem in GEO given the stationary nature of GEO satellites.

7.3.2.2 Mobility Enhancements for Non-Terrestrial Networks

7.3.2.2.1 Enhancements to Measurement Configuration/Reporting

- Conditional triggering of measurement reporting: The triggering of measurement reporting can be based on UE location. This may be based on UE location vs a reference location, or a combination of location and RSRP/RSRQ.
- Inclusion of location information in the measurement report: Location information may be piggy backed onto the measurement report to provide the network additional information when determining whether to HO. Additional design considerations (e.g. signalling overhead impacts and potential privacy concerns) can be addressed in a work item phase.
- Network compensation of propagation delay difference between satellites: The network can compensate for propagation delay differences in the UE measurement window, e.g. via system information, or in a UE specific manner via dedicated signalling. Other solutions to this issue are not precluded.

7.3.2.2.2 Conditional Handover

- Measurement-based triggering: Agreements in the mobility enhancements WI are to be taken as baseline. Configuration of triggering thresholds and/or which measurement events to use as triggers should consider the NTN environment e.g. the small variation of the cell quality measured in cell center and at cell edge in NTN.
- Location (UE and Satellite) triggering: additional triggering conditions based on UE and satellite location can be considered in NTN and may be considered independently or jointly with another trigger (e.g. measurement based). Location-based conditional HO in LEO scenarios should consider deterministic satellite movement. For example, the location triggering condition may be expressed as distance between the UE and the satellite.
- Time(r)-based triggering: Several triggering conditions considering the time a region is served can be considered. This may be based on UTC time, or a timer-based solution, and may be considered independently or jointly with another trigger (e.g. measurement based). Time-based conditional HO in LEO scenarios should consider deterministic satellite movement.
- Timing advance value based triggering: additional triggering conditions based on timing advance value to the target cell can be considered in NTN and may be considered independently or jointly with another trigger.
- Elevation angles of source and target cells based triggering: additional triggering conditions based on elevation angles of source and target cells can be considered in NTN and may be considered independently or jointly with another trigger.

Table 7.3.2.2.2-1: Pros and Cons of the different triggering conditions

Triggering Method	Advantages	Disadvantages
Measurement-based	<ul style="list-style-type: none"> • Less specification impact (i.e. similar to terrestrial network); • Is supported in Rel-16 mobility enhancements WI; • Relies on UE estimates and established channel estimation techniques; • Is based on receiving power and cell quality. 	<ul style="list-style-type: none"> • Would require neighbouring cell lists, which may be difficult given the fast-moving nature of LEO satellites or under inconsistent/deviating cell coverage; • Small RSRP/RSRQ variation in regions of cell overlap and propagation delay may make measurement-based triggering (e.g. A3 events) unreliable; • May be difficult to ensure UE performs handover to a specific country.
Location-based	<ul style="list-style-type: none"> • Useful when cell boundaries are dispersed/undefined; • Can enable mandatory HO based on UE location; • A precise trigger as UE location can be known with a degree of accuracy; • Able to predict/pre-emptively configure triggering condition using satellite ephemeris and deterministic satellite movement; • Would be useful to overcome issue of small RSRP/RSRQ variation in regions of cell overlap; • UE may need to perform fewer measurements for HO purposes. • Since timing advance is derived based on the distance between UE and the satellite, configuring the distance as a triggering condition directly can help reduce complexity and power consumption in the UE side in calculating the timing advance. 	<ul style="list-style-type: none"> • The UE may trigger HO to an unavailable cell (e.g. the NTN cell has deviated or is inconsistent, under varying channel conditions, or if the network sets the wrong triggering condition); • Some UEs may not have positioning capability. • UE must continuously track the satellites trajectory, and the network will need up-to-date UE location information which may introduce high overhead.
Time/Timer-based	<ul style="list-style-type: none"> • Can be useful to maintain service continuity if UE loses terrestrial coverage; • Can enable mandatory HO based on timing; • Network can configure different timing lengths to mitigate possible RACH congestion; • Can work with satellite ephemeris and exploit the deterministic movement of satellites; • UE may need to perform fewer measurements for HO purposes. 	<ul style="list-style-type: none"> • The UE may trigger HO to an unavailable cell (e.g. the NTN cell has deviated or is inconsistent, varying channel conditions, or if the network sets the wrong triggering condition); • Depending on the accuracy of the ephemeris data and mobility of the UE, this may not be an accurate trigger which could, e.g. result in early/late HO; • Maintaining multiple timers for every UE could introduce high overhead.
Timing advance value based triggering	<ul style="list-style-type: none"> • Timing advance based triggering fits well for the issue where UE needs to pre-compensate time when sending the RACH preamble in order the target cell to receive the preamble properly. 	<ul style="list-style-type: none"> • Requires GNSS capable UEs. Support for this needs to be explicitly added as not part of Rel-16.

	<ul style="list-style-type: none"> Further, due to small difference to RSRP/RSRQ values between overlapping cells, timing advance based triggering may provide better accuracy for the triggering point. 	
Elevation angles of source and target cells based triggering:	<ul style="list-style-type: none"> Beneficial for handover regions that are irregular shaped 	<ul style="list-style-type: none"> UE needs to evaluate elevation angle based on UE location and satellite ephemeris data

7.3.2.2.3 Mobility Configuration

Broadcast configuration: common signalling in the HO configuration (e.g. T304 and spCellConfigCommon) can be broadcast, possibly via SIB. Although some mobility information common to all UEs may be broadcast, further evaluation on impact to signalling overhead is required given HO command is UE specific and requires dedicated signalling.

The following criteria can be used as baseline to evaluate the impact/benefit of broadcast signalling:

- 1) Will enough UEs share the same value of common signalling to justify broadcasting values vs. dedicated signalling?
- 2) Will these values remain valid for long enough such that they will not require frequent modification (either via dedicated signalling or updated broadcast message) thus reducing signalling overhead savings?
- 3) How long will it take for the UE to receive the minimum required information for NTN access?

Further analysis may be performed to identify other possible signalling applicable to broadcast transmission (e.g. common delay, other parameters of the RRCCoreConfiguration message), whether certain areas of the network are more suitable to broadcast signalling (e.g. at the edge of coverage between terrestrial and non-terrestrial), or whether typical HO configurations (possibly with additional delta configuration) can be provided via an index. All signalling between the UE, source, and target gNB should be considered in evaluation.

7.3.2.3 Connected mode mobility for feeder link switch for LEO NTN [18]

Connected mode mobility for feeder link switch, or due to interface change, from the network perspective is captured in Sections 8.6 and 8.7. From Uu perspective, there is difference between Architecture Option 1 that is transparent payload and Architecture Options 2-5 (listed in Section 8.7.1) that are regenerative payload. For further details, see Sec. 8.3.1.

7.3.2.4 Connected mode mobility assumptions

RAN2 will prioritize analysis of mobility challenges/enhancements for transparent GEO (A) and LEO with moving beam (C2, D2) architectures during the study item phase.

NOTE 1: Only cell level mobility is considered from a RAN2 perspective

NOTE 2: Additional scenarios may be considered pending outcome of NTN study in RAN1.

7.3.3 Paging issue

7.3.3.1 Paging Capacity

Following parameters should be considered for calculation of paging capacity

- Paging Frames (PF) per second: N_{PF}
- Paging Occasions (PO) per PF: $N_{PO_{perPF}}$
- Maximum number of paging records in paging message: $N_{UE_{perPO}}$

- User density (UEs/km²)
- Satellite beam diameter: in km
- NO_Traffic: fraction of UEs in the cell with network originated traffic
- Arrival session or call rate: average requested paging occasions per hour and per UE
- Number of cells in per tracking area: M

7.3.3.1.1 Paging capacity of non-multibeam cell

In a non-multibeam scenario 4 out of 10 subframes per PF can be used for paging that is there can be at most 4 PO per PF. A paging message can only be sent in a PO. The paging message can at most include 32 paging records in the paging message where each paging record includes the UE identities of the UEs being paged. The theoretical paging capacity as maximum number of UEs paged per second in an NR non-multibeam cell is thus limited by:

$$\text{Supported Paging Capacity per second} = N_{PF} \times N_{POperPF} \times N_{UEperPO}$$

As each RF can be configured to be a PF, the resulting maximum paging capacity with 100 PF per second is thus $4 \times 100 = 400$ PO per second. This implies that theoretically, an NR cell can page $32 \times 400 = 12\,800$ UEs per second, or equivalently, more than 46 Million UEs per hour ($12\,800 \times 60 \times 60$).

The supported paging capacity should be compared with the required paging per cell, which can be calculated as:
Expected arrival rate per cell per second = $A \times \text{UE density} \times \text{arrival session rate}$

If the tracking area is larger than one cell and the base station needs to blindly page all the UEs that it want to reach in all cells, then in the worst case the required arrival rate would be:

$$\text{Expected arrival rate per TA per second} = M \times A \times \text{UE density} \times \text{arrival session rate}$$

The paging capacity should also be considered together with the cell's capacity to support UEs accessing the cell. After being paged, the UE accesses the cell using a random-access procedure which starts by the UE transmitting a random-access preamble on the physical random-access channel (PRACH). PRACH capacity is calculated in Section X.

7.3.3.1.2 Example of calculation

Given the cell area of a hexagonal cell has a radius of r as in Figure 1, the cell area can be expressed as

$$A = \frac{\sqrt{3}}{2} * ISD^2 = 2 * \sqrt{3} * r^2. \text{ If the cell area is an ellipsoid the area can be expressed as } A = \pi * r_1 * r_2. \text{ For example, for the cell radius of } r = 250\text{km, the area is } A = 163\,000\text{km}^2.$$

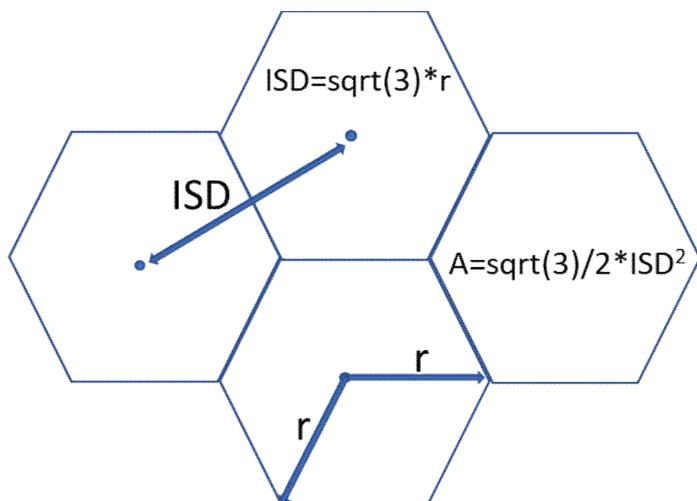


Figure 7.3.3-1: Area of a hexagonal cell with radius r

Some examples of the paging channel load which is calculated as

Expected arrival rate per cell per second / Supported Paging Capacity per second can be seen in Table 7.3.3.1-1 with different deployments.

Table 7.3.3.1-1: Paging channel loads for a given arrival session rate and UE density

N_{PP}	N_{poperPP}	N_{UEperPU}	UE density [UE/km ²]	Arrival session rate	M	r [km]	Paging channel load
4, 100, 32			400	1 per hour	1	250	141%
4, 100, 32			400	1 per 24 hours	1	250	5%
4, 100, 32			20	1 per hour	1	250	7%
4, 100, 32			20	1 per 24 hours	1	250	0,25%

Furthermore the supported UE density given the UE arrival session rate per UE, which is highly dependent on the size of the beam, can be calculated by:

$$\frac{\text{Supported arrival rate}}{\text{arrival session rate} \times A} = \text{Supported UE density}$$

Table 7.3.3.1-2: Supported UE densities for a given arrival session rate

N_{PP}	N_{poperPP}	N_{UEperPU}	Arrival session rate	M	r [km]	UE density [UE/km ²]
4, 100, 32			1 per hour	1	250	~280
4, 100, 32			1 per 24 hours	1	250	~6780

One can also compare the paging capacity requirements scale with the TA size and different arrival rates, in the worst case considering that UE does not know where any of the UEs are located and thus pages the same IDs across the whole tracking area:

$$\text{Arrival rate per TA per second} = M \times A \times \text{UE density} \times \text{arrival session rate}$$

In the Figure 7.3.3-2 and Figure 7.3.3-3 the required paging capacity is shown if the cell is circular with a radius of 200 km and 500 km, the UE density is 620 UE/km², and arrival session rate is 1/24*x, where x is 0.2 and 0.5 leading to arrival session rate of 0.008 and 0.021.

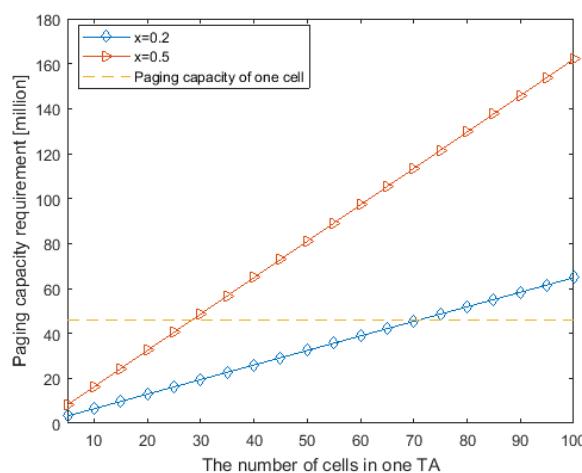


Figure 7.3.3-2: Paging capacity requirement in LEO scenario

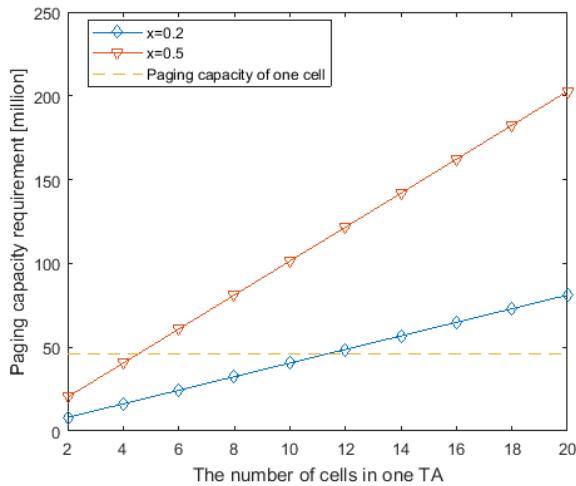


Figure 7.3.3-3: Paging capacity requirement in GEO scenario

7.3.4 Radio Link Monitoring

Void

7.3.5 PLMN identities deployment

Deployment of PLMNs with specific PLMN IDs for NTN cells and TN cells, or between different type of NTN platforms (GEO or LEO), is considered as a preferred option, however the configuration of common PLMN identities is not precluded.

7.3.6 Ephemeris Data for NTN

7.3.6.1 Representation of Complete Ephemeris Data

Ephemeris data contains the information about the orbital trajectories of artificial satellites as described in Annex A. There are different possible representations of ephemeris data. One possibility is to use orbital parameters, e.g. semi-major axis, eccentricity, inclination, right ascension of the ascending node, argument of periaxis, mean anomaly at a reference point in time, and the epoch. The first five parameters can determine an orbital plane, and the other two parameters are used to determine exact satellite location at a time. A description table for the orbital parameters and the corresponding illustrations are as below.

Table 7.3.6.1-1: Essential Elements of Ephemeris

Orbital plane parameters	\sqrt{a}	Square root of semi major axis (semi-major axis)
	e	Eccentricity (eccentricity)
	i_0	Inclination angle at reference time (inclination)
	Ω_0	Longitude of ascending node of orbit plane (right ascension of the ascending node)
	ω	Argument of perigee (argument of periaxis)
Satellite level parameters	M_0	Mean anomaly at reference time (true anomaly and a reference point in time)
	t_{0s}	Ephemeris reference time (the epoch)

NOTE: True anomaly is the actual measured angle in the orbital plane between the vector extending from the focus to the point of periapsis and the vector extending from the focus to the object's actual position. Mean anomaly is the angle between the periapsis point and the imagined position of an object for the same elapsed time since periapsis for a circular orbit around the same body with the same orbital position. The key difference is that mean anomaly always increases linearly with time. The true anomaly, in general, does not, except if the orbital is circular, in which case the mean anomaly and true anomaly are almost identical. True and mean anomaly can be linked together thanks to the eccentric anomaly.

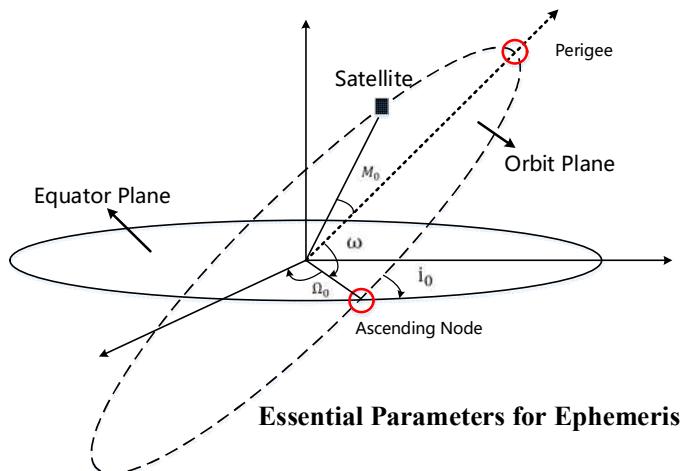


Figure 7.3.6-1: Satellite Orbit and Keplerian Elements

Another possible option is to provide the location of the satellite in coordinates (x, y, z) , e.g. ECEF coordinates. For anything else than GEO, additionally a velocity vector (vx, vy, vz) and again a reference point in time are needed.

NOTE: It seems that this option has the drawback that – for LEO satellites – it prevents the UE from extrapolating the satellite track for more than a very short time into the future. Since a LEO satellite moves very fast, the given position (x, y, z) may be outdated in a short period of time. And since the satellite moves in an elliptical orbit, providing a velocity vector (vx, vy, vz) does not help much; so it remains to be studied the required accuracy – to determine the satellite location with acceptable precision. As a result, the satellite would need to provide (e.g. broadcast) an updated location very often, about every few minutes. Furthermore, for the same reason it is unclear how to pre-provision a UE with ephemeris information in coordinates.

7.3.6.2 Provision and Use of Ephemeris Data

In all cases, the minimum representation needs at least seven double-precision floating point numbers, plus some overhead. This means that, for satellite networks with many satellites, the ephemeris data can be quite substantial. The exact data size for a LEO network depends on the number of satellites, which may be several hundreds, and the accuracy of which the ephemeris parameters are represented.

In a satellite network, the orbits of all satellites are however not independent, as several satellites typically share a common orbital plane. To reduce the amount of data needed, the ephemeris data could provide information not for every single satellite, but only for the common orbital planes. Even for a network with 100 orbital planes, the ephemeris data would then amount to only a few kB. The ephemeris data may be provisioned a file containing the ephemeris data in the uSIM of the UE or directly in UE itself.

As mentioned above, the size of the ephemeris data can be quite substantial for networks with many satellites, and easily exceeds the capacity of a uSIM which is one way for pre-provisioning the ephemeris data, which typically is 128 kB. The ephemeris data file on the uSIM may thus contain only information about the orbital planes. In this case, the ephemeris data would not provide the location of a specific satellite but describe an arc in the sky above the UE which the UE would need to scan for a satellite. According to the definitions of orbital parameters, the first five parameters, i.e. semi-major axis, eccentricity, inclination, right ascension of the ascending node, argument of periapsis, are used to determine the elliptical orbit. So these parameters can be provisioned to UE as baseline ephemeris data.

These baseline ephemeris data or orbital planes may be indexed and further quantized and sub-indexed. The indexes can then be used in RRC in an efficient way to point to stored ephemeris data. The UE can be given information about ephemeris data of other cells by using the ephemeris plane information. For example, when a UE is asked to do RRM measurements, the UE is given the index of the orbital plane where the cell to be measured can be found.

With the help of ephemeris data, a UE may search for the first NTN cell it could connect to. After detecting PSS/SSS (SSB) of a cell broadcasted by a satellite, the UE may be able to read the initial system information of that cell. Ideally, before attempting to access the cell, the UE knows the RTT well enough to be able to do random access. For this, the initial system information may need to contain further ephemeris information on the exact location of the cell (or the satellite broadcasting the cell). This information can be given with respect to the orbital plane that the UE already has information about.

Considering that the orbit-plane level orbital parameters are not sufficient to derive the satellite position while the satellite level orbital parameters is more helpful for UE to search for the first NTN cell and perform initial access, it is worthwhile evaluating some other solutions to provide satellite level orbital parameters. In addition to the first five orbital parameters for orbital plane, the other two orbital parameters including mean anomaly at a reference point in time and the epoch are used to determine the exact satellite location at a time.

As mentioned above, the main concern for proving the satellite level orbital parameters is about the size of such information. However, there is no need for a UE to store orbital parameters for all the satellites. If the orbital parameters per satellite are pre-provisioned, UE only needs to store the ephemeris data for the satellites that may serve UE. Another possible solution to address the size concern of the satellite level orbital parameters is to broadcast the orbital parameters of the serving satellite and several neighbouring satellites which will be sufficient for initial access and mobility handling at UE side. Thus, the following solutions can be considered to provide orbital parameters per satellite:

- Pre-provision satellite level orbital parameters for all the satellites that may serve the UE in uSIM/UE and the ephemeris data for each satellite can be linked to a satellite ID or index. Broadcast the satellite ID or index of the serving satellite in system information so that UE is able to find the corresponding detailed ephemeris data stored in uSIM to derive the position coordinates of the serving satellite. The satellite ID or index of neighbour satellites can also be provided to UE via system information or dedicated RRC signalling to assist mobility handling.
- Broadcast satellite level orbital parameters of the serving satellite in system information and UE will derive the position coordinates of the serving satellite. The ephemeris data of the neighbouring satellites can also be provided to UE via system information or dedicated RRC signalling.. In case the baseline orbital plane parameters are provisioned in uSIM/UE, only mean anomaly at a reference point in time and the epoch need to be broadcasted to UE, in this way signalling overhead can be reduced significantly.

7.3.6.3 Updating Stored Ephemeris Data

For the solutions in which the orbital parameters for the common orbit planes or for all the satellites that may serve the UE are pre-provisioned, the accuracy of the prediction of a satellite orbit or the satellite position decreases the further in the future one tries to extend the prediction. It might thus be needed to update the ephemeris data stored in the UE. The validity time of stored ephemeris data might depend on the orbital parameters of the NTN satellite, and on the required accuracy of its prediction. Since the validity time determines the frequency of the updates, it should be studied further.

The main purpose of the ephemeris data provided by network is to provide the UE with ephemeris data for initial access, e.g. if it is expected to be switched off for a longer time; or in other words, as a replacement for the data stored in the UE. As such, it may also contain information on orbital plane level or on satellite level.

The UE should always use the most current ephemeris data. Once the UE has obtained new ephemeris data, the parameters stored in the UE are thus obsolete and should no longer be used or be overwritten with the newer values. Every parameter in the UE has an associated priority statement. By giving the parameters in the UE lower priority, the UE can be prevented from using the obsolete values stored in the UE.

7.4 Earth fixed cells vs Earth moving cells

Compared to LEO based Earth moving cells scenario where cells are moving on the ground, LEO based Earth fixed cells scenario refer to NTN that provide cells fixed with respect to a certain location on the Earth during a certain time duration. This can be achieved with NTN platforms generating steerable beams which footprint is fixed on the ground.

The same solutions identified for Earth moving cell scenario can also be applied for Earth fixed cell scenario, however whether specific solutions are necessary (or preferred) for each scenario can be further evaluated in the normative phase (See [74]).

8 Issues and related solutions for NG-RAN architecture and interface protocols

8.1 Tracking area management

The concept of Registration and Tracking areas pertains in the context of Non-Terrestrial networks, and is similar to NR based cellular system in following aspects:

- a tracking area corresponds to a fixed geographical area.
- tracking areas (TA) is utilized for UE access control, location registration, paging and mobility management.
- a registration area encompasses one or several tracking areas.

The objective is to track the UE, in order to minimize the use of radio resources for paging.

8.1.1 NTN cells are fixed w.r.t the ground

For scenarios A, B, C1 and D1, the NTN cells are fixed on the ground. Hence a tracking area may correspond to one or several NTN cells. The 3GPP-defined tracking area management and paging procedures can apply as is. In case of C1 and D1, the LEO satellites generate beams with temporary Earth fixed footprints. In other words, the beam footprints are stationary over a given NTN cell on ground for a certain amount of time before they change their focus area over another NTN cell. It is possible to assign each NTN cell to a tracking area. This requires the satellite to change the broadcasted tracking area code between two successive NTN cells covered.

NOTE 1: For scenarios C1, the TA list and paging messages could be sent by the same gNB to the NTN cell via all satellites covering this NTN cell.

NOTE 2: For scenarios D1, the TA list and paging messages could be sent by the gNB on board all satellites covering this NTN cell.

8.1.2 NTN cells are moving w.r.t the ground

For scenarios C2 and D2, the NTN cells move on the ground as the satellites move on their orbital planes. This requires some adaptations to the TA management and paging procedure.

Hence we shall focus the study on scenario C2 and D2 for the idle/inactive mode mobility.

It is worth noting that, as long as the TA is always uniquely coupled with the relevant cell(s), it may still be possible to apply legacy core network procedures (e.g. paging) even to a moving TA. In such case, however, it seems beneficial to differentiate such a TA from a fixed / "non-NTN" TA. In principle, this could be done by reserving a range of identifier(s) for TAs associated with NTN moving cells. However, this might restrict the possible TA address space and might not be desirable from the operator's point of view.

Another alternative would be to extend the TAC IE signalled over NGAP and XnAP with a TA Type IE, defined as e.g. ENUMERATED (NTN, NTN with moving cells, ...) so that the receiving node can identify that the cells associated with this TA are related to a NTN, and/or are not stationary with respect to the ground. Alternatively, this indication may be at cell level or gNB level.

The non-terrestrial and terrestrial networks could be assigned either same or different PLMNs.

- In case of two different PLMNs for terrestrial and non-terrestrial networks, both tracking area layouts can be independently defined preventing overlaps between tracking areas of a given layout. This would be in line with the current definition of TAs.

- In case of a shared PLMN, the operator is responsible for defining tracking areas and assigning the TAIs to be used by the terrestrial network, and to be used by the non-terrestrial network. Overlapping between these tracking areas are possible.

The main idea is to decouple the TA management from the NTN cell pattern. In that case, registration and tracking areas are arbitrary geographical areas defined by the operator. (FFS)

It is assumed that not all UEs are capable of positioning.

The following applies to scenarios C2 and D2.

8.1.2.1 Tracking Area defined on satellite

In this option, a NTN cell only have one TAI per PLMN ID, i.e. same as terrestrial cell. This also allows the gNB to reuse current NGAP procedure, i.e. the INITIAL UE MESSAGE contains one TAI of the serving cell.

In Scenario C2 and D2, when the LEO satellite moves, the coverage of the TAI also changes. A stationary UE may see the TAI keeps changing. Some solutions were described in the Section 8.3. Similar issue is also discussed in SA2, and the related proposals are also captured in SA2 TR23.737, Solution #7.

8.1.2.2 Tracking Area defined on earth

In this option, it keeps the principle that the TAI is related to a specific geographical area, but a NTN cell may have to broadcast multiple TAIs per PLMN ID, which does not align with the principle that a cell only have one TAI per PLMN ID.

When the NTN cell covers multiple Tracking Areas (either fully, or partially), the NTN cell will broadcast all related TAIs. From a UE perspective, the UE recognizes the Tracking Area by the TAI broadcasted over the air. The "observed" Tracking Area by the UE keeps changing. The following aspects need to be further considered.

Which TAI is to be provided to CN on NG interface?

During the Initial UE Message procedure, the UE's location, i.e. TAI+CGI, is provided to the CN. When a NTN cell broadcast multiple TAIs, one option is provide all TAIs to the AMF. The AMF may have difficulty to provide an effective Registration Area to the UE. The other option is to only provide one TAI to the AMF. The gNB need to determine which TAI is to be provided to the AMF when a NTN cell broadcast multiple TAIs.

How to enforce a regional/country policy?

If UE's location can be determined during (or before) the registration procedure, the NG-RAN node provide the UE's location to the network during the registration, and the regional/country policy will be enforced. Otherwise, as soon as the UE enters in connected mode, the network will be able to determine its location and regional/country policy will be enforced.

8.2 Registration Update and Paging Handling

In Non-Terrestrial non-GEO Network, the satellites moves across the geographical area of interest, its antenna beams will cover different portions of that area.

In a NTN beam with a foot print moving on earth, a fixed association between the non-GEO NTN beam and TAI would lead to moving TAIs on ground. In terrestrial RANs the geographical area for tracking the UE, also called Tracking Area (TA) is associated to the TAI broadcasted by the RAN.

As in the terrestrial RAN, there is no one-to-one correspondence between moving NTN beams and geo-area on Earth, i.e., the TAIs broadcasted by the Non-GEO satellite will sweep over Earth. A stationary UE will see different NTN beams/TAIs over the time. With current Registration Update procedure, the stationary UE has to keep performing Registration Updates upon the change of NTN beam. This brings a challenge to current Registration Update and Paging. In the following, we study possible solutions based on whether the UE can determine its location or not.

8.2.1 Option 1: UE is capable to determine its location

In the following it is assumed that the UE has the capability to determine its location (e.g. by GNSS). In this case the satellite can page the UE based on UE's location information.

In terrestrial network, the AMF is in charge of mapping a tracking area where the UE is located to determine the list of gNBs that pages the UE. In NTN, one can use the UE location to do an equivalent mapping and determine the list of gNBs that page the UE.

The mapping could be made in the AMF. For this, the AMF is made aware of UE location, along with some assistance information, e.g. UE type or UE speed information. AMF has also to be aware of satellite ephemeris.

Alternatively, this mapping could be made in the RAN. When a UE has to be paged, the AMF determines the RAN access node(s) where to send the paging message from the TAI as usual. The NTN based NG-RAN can then select the satellite beams where to broadcast the paging from its knowledge of UE last location and satellites ephemeris. However this raises several issues as paging failure coordination between RAN and CN and Idle UE context management in RAN, and would require further studies.

8.2.1.1 Mapping of UE location to gNB list in the AMF

The example procedure for UE location based paging could be illustrated by the figure below:

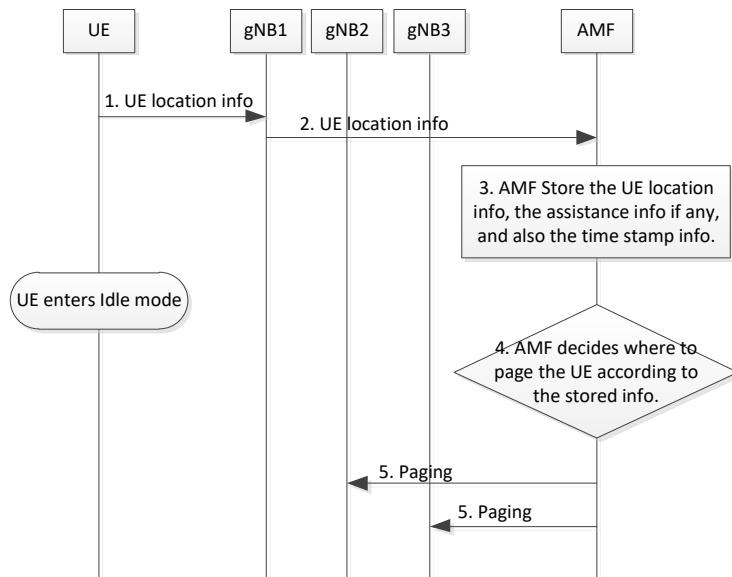


Figure 8.2.1.1-1: UE location based paging (example)

- Step 1: UE report the location info to gNB1, the report may also include some assistance info such as UE type, speed info, more details need to be further studied.
- Step 2: Upon receiving of the UE location report, gNB1 forwards the location info and the assistance info if have to AMF.
- Step 3: AMF stores the UE location info, the assistance info if any, and also the corresponding time stamp. The information is kept in AMF when UE is released to Idle.
- Step 4: When AMF wants to page the UE, it selects the gNB(s) which could cover the UE location according to the stored info and ephemeris.
- Step 5: AMF sends the Paging message to the selected gNB(s), including the location info and the assistance info if any. Upon reception of the Paging message, the gNB may decide which satellite(s) or beam(s) to be paged and page the UE accordingly.

NOTE: If the location based paging is failed, AMF may extend the paging area and re-send the UE according to its paging policy, e.g. re-send the paging in the whole registration area of the UE.

8.2.2 Option 2: UE is not capable to determine its location

In the following, it is assumed that the UE has no capability to determine its location. Four potential solutions have been identified.

8.2.2.1 Solution 1: Timing window based Registration update and paging

This solution assumes moving identifiers on ground.

The satellite can page the UE based on RA.

The following is one possible solution (details may be refined).

In this option, the Tracking Area is associated with the timing information for how long it is valid related to a geo-area. For example, a geo-area will be served by NTN beam#1 with TAC#1 during 10:01 – 10:10, NTN beam#2 with TAC#2 during 10:11 – 10:20, etc. an example call flow is shown as below:

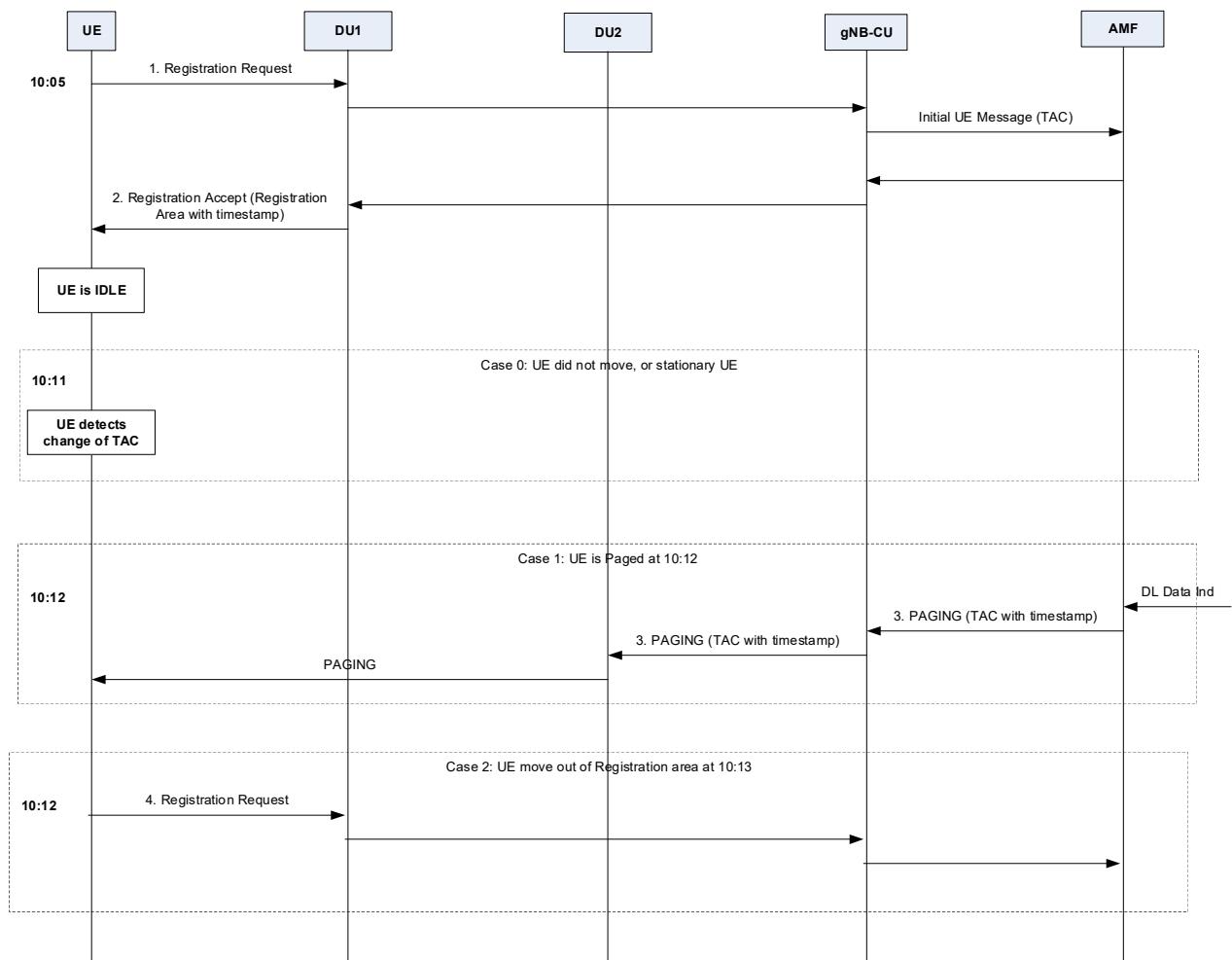


Figure 8.2.2-1: UE Registration procedure (example)

- Step 1: at 10:05, UE initiates Registration procedure. The REGISTRATION REQUEST message is sent to AMF. Just like normal initial access, the CU provides the TAC#1 to AMF with current NGAP procedure.
- Step 2: AMF replies with REGISTRATION ACCEPT message. The AMF determines the UE's location will be covered by TAC#1 during 10:01-10:10, TAC#2 during 10:11-10:20, etc. The determination is based on

- The ephemeris information of the satellites, i.e. the information as to which NTN beam covers a specific location.
- The location of the UE, in terms of TAC/NTN beam ID of UE's current or last 3GPP access. The UE may include its location information in the NAS REGISTRATION REQUEST message, or other NAS message.

The determination may be performed by querying a database.

The REGISTRATION ACCEPT message includes enhanced Registration Area information, consisting of a list of TAIs with timing information (in this example, AMF would like the UE to initiate a Registration Update 10-min later)

- + TAC#1 with (10:05 – 10:10)
- + TAC#2 with (10:11 – 10:15)

Later, UE enters RRC_IDLE.

Case 0: UE did not move during 10:05 – 10:11

- At 10:11, NTN beam#1 moved out of the UE's area. The UE's area is now covered by NTN beam#2 with TAC#2. The UE detected the TAC of the serving cell is changed to TAC#2. UE checks the TAC#2 against the enhanced Registration Area received in Step 2 (see Figure 8.2.2-1). TAC#2 is in the Registration Area assigned by the AMF in the REGISTRATION ACCEPT message (Step 2), and the timing information match (i.e. TAC#2 only for 10:11-10:15), this means the UE is still in the Registration Area, thus no need to perform Registration Update.

NOTE: This reuses the current Registration Update trigger.

Case 1: at 10:12, the UE is paged.

- Step 3 (see Figure 8.2.2-1): at 10:12, a DL data is received for the UE. AMF determines the target tracking area based on the UE's last location (i.e. TAC#1 at 10:05), and the Tracking area information for this area (i.e. TAC#1 during 10:01-10:10, and TAC#2 during 10:11-10:20). In this example, AMF knows the UE's last location and will be served by NTN beam#2 with TAC#2 during 10:11-10:20. AMF sends the Paging message with TAC#2 to the NG-RAN.

Normal Service Request procedure is performed.

Case 2: at 10:13, the UE move out of the Registration Area

- Step 4 (see Figure 8.2.2-1): at 10:13, the UE detects current NTN beam broadcasting TAC#1. Even TAC#1 is in the Registration Area assigned by the AMF in the REGISTRATION ACCEPT message (Step 2), but the timing information does not match (i.e. TAC#1 only for 10:01-10:10, but not for 10:13), this means the UE is moving out of current Registration Area. So the UE initiates a Registration Update procedure.

Advantage for this option is:

- Reuse current Registration Update trigger, i.e. TS23.501, "perform Mobility Registration Update procedure if the current TAIs of the serving cell (see TS 37.340 [31]) is not in the list of TAIs that the UE has received from the network;"
- Reuse current TAC broadcast mechanism, i.e. NTN beam always broadcasts the same TAC.
- Less changes to RAN and CN.

8.2.2.2 Solution 2: UE assisted TA list report/registration and paging

This solution assumes stationary identifiers on ground.

The satellite pages the UE based on RA, i.e. TAI list.

The following is one potential solution. (Details may be refined)

In this option, the TAI is broadcast in system information in NTN cell based on fixed TA planning area on ground:

- Step 1: Setup a fixed TA map on the Earth's surface.
- Step 2: Dynamically update the broadcast TAI according to the satellite's position.
- Step 3: UE monitors and reports list of received broadcast TAIs for registration procedure.
- Step 4: During the registration procedure, AMF provides a TAI list to the UE, which defines the UE-specific registration area used for paging.
- Step 5: UE measures and records the observed TAI list of the best cells with respect to time.
- Step 6: UE compares the TAI list assigned by AMF with the observed TAI from Step 5 and determines whether it is still within the registration area or not (details may be refined).
- Step 7: If UE concludes that it has left the registration area, it initiates the Registration Update procedure and reports the observed TAI list to AMF by which AMF may assign a new UE-specific TAI list. The determination of the observed TAI list in UE including adding or deleting a TAI is possible alternative.

8.2.2.3 Solution 3: Multi-Tracking Area ID based Registration update and paging

Instead of broadcasting a single TAI, the satellite could broadcast a list of TAIs of covered TAs, in order to allow for TAs to be a subset of the satellite beam coverage area. The satellite could then adopt the list of TAIs with respect to its beam coverage area. In case of transparent satellites, the gNB on the ground may be preconfigured with the list of TAIs to be used. In case of regenerative satellites, the network node on the satellite may be preconfigured with the list of TAIs to be used, for example by using validity time window information for each TAI list entry in a similar manner as described in 8.3.2.1.

The advantage of this approach is that the Tracking Area (TA) definition as non-overlapping areas on the ground is still valid and the current paging mechanisms can be reused.

Figure 8.2.2-3 shows an example with countries that are equivalent to tracking areas. Four TAs are defined: TA1: Germany, TA2: Austria, TA3: Switzerland and TA4 Liechtenstein (Note that it is also possible to define multiple TAs per country). Three satellites (red, green and blue) are covering parts of the area shown as red beam, green beam and blue beam. In the top figure the red satellite broadcasts three TAIs, i.e. TAI2, TAI3 and TAI4 as its beam footprint is covering TA2, TA3, and TA4. Similarly, the green satellite broadcasts TAI1 and TAI3, while the blue satellite broadcasts TAI1, TAI2, TAI3 and TAI4. The bottom figure shows the same TAs, while the satellites and their respective coverage areas moved. Hence, the list of broadcasted TAIs for the red and green satellites changed, but stayed the same for the blue satellite.

In the example, a UE located in Austria (TAI2), would be paged within both blue and red satellite beams according to the upper figure. According to the lower figure, it would be paged within both blue and green satellite beams.

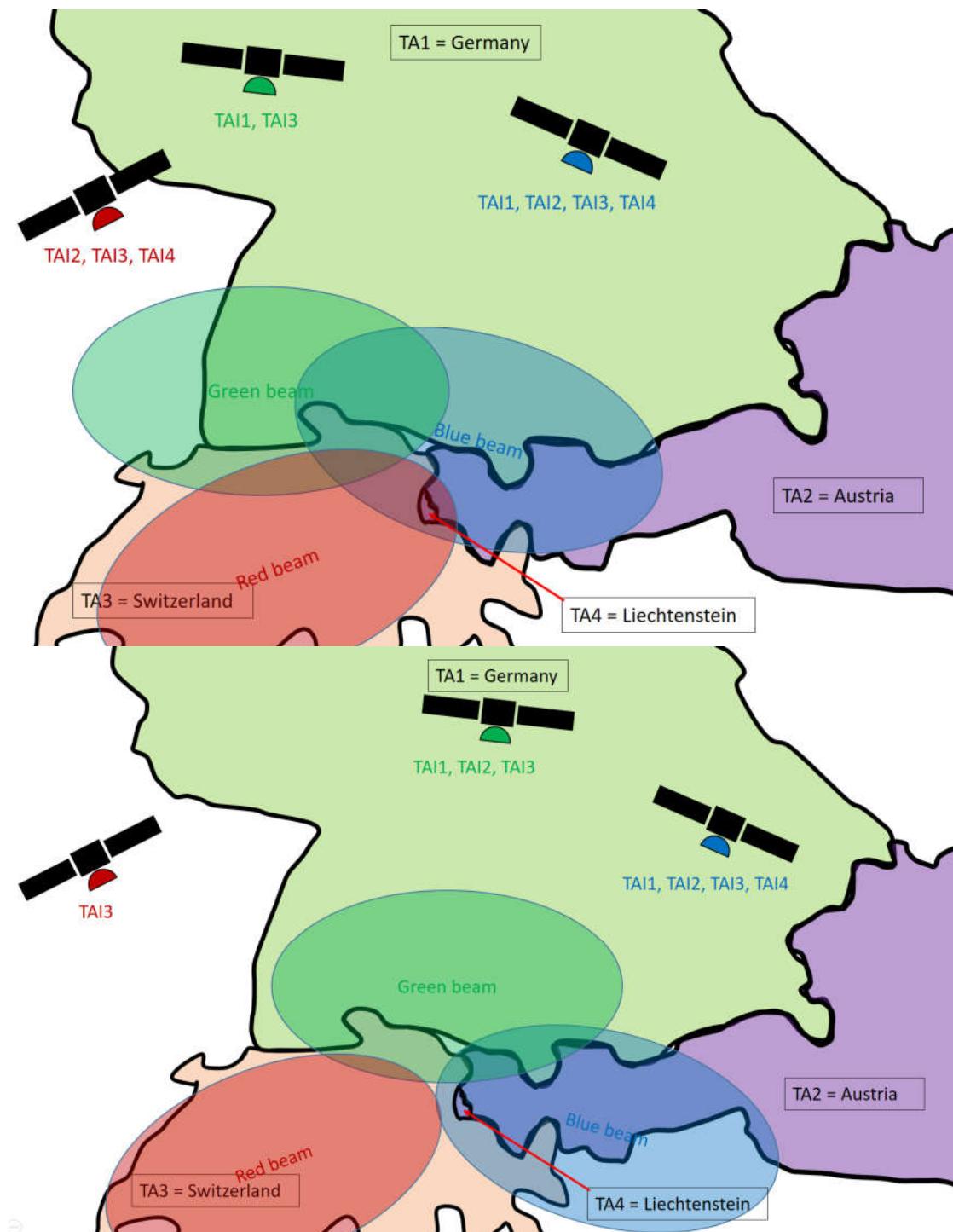


Figure 8.2.2-3: Illustration of the solution using country areas as exemplary tracking areas (two exemplary time instances are shown from top to bottom)

8.2.2.4 Solution 4: UE location determined by NTN based NG-RAN

The earth footprint of a satellite beam depends on the satellite altitude and the elevation angle, but may be quite large compared to usual terrestrial cell size. Hence, the trade-off between TA size and registration update is different for NTN compared to terrestrial networks.

When a UE registers initially, or makes registration area updates, or switches to connected mode, the NTN based NG-RAN gets a UE location inform, from serving beam identification for example. A periodic registration area update could be sufficient to track a UE in idle mode, the RA update periodicity being tuned according to UE type or observed mobility behaviour.

Moreover, the RAN could have other means to locate a UE.

Hence, even if the UE is not capable to determine its location on its own, it could be assumed that the RAN has a knowledge of UE location. Then paging methods based on UE location knowledge can apply.

8.3 Connected mode mobility

There are different types of hand-overs in Non-Terrestrial networks:

- Intra-satellite hand-over (between cells served by same satellite)
- Inter-satellite hand-over (between cells served by different satellite)
- Inter-access hand-over (between cellular and satellite access)

There can be some variants depending on whether the satellite is transparent or regenerative (gNB or partial gNB on board the satellite)

The table identifies the applicable NG-RAN hand-over procedures for each of the NTN hand-over scenarios.

Table 8.3-1: NG-RAN procedures versus NTN hand-over scenarios

NTN Hand-over scenarios	Transparent satellite	Regenerative satellite (gNB on board)	Regenerative satellite (gNB-DU on board)
Intra satellite hand-over	Intra-gNB handover procedure or Inter-gNB handover procedure	intra gNB hand-over procedure	Intra-gNB-CU Mobility/Intra-gNB-DU handover or Inter-gNB-CU handover (See clause 8.2.1.2 in TS 38.401)
Inter satellite hand-over	Inter-gNB handover procedure or Intra-gNB handover procedure (See clause 9.2.3 in TR 38.300)	inter gNB hand-over procedure (See clause 9.2.3 in TR 38.300)	Intra-gNB-CU Mobility/Inter-gNB-DU Mobility or Inter-gNB-CU handover (See clause 8.2.1.1 in TS 38.401)
Inter access hand-over		Inter AMF/UPF hand-over procedure or Intra AMF/UPF hand-over procedure (out of RAN scope)	Intra-gNB handover procedure or Inter-gNB handover procedure

In each case, the relevant mobility procedures may require some adaptations to accommodate the extended latency of satellite access.

An inter-access hand-over (between cellular and satellite access) is considered by utilizing an inter gNB procedure via the 5GCN (e.g. for Satellite with on board processed payload) or via the Xn (e.g. for satellite with transparent payload).

It is assumed that not all UEs are capable of positioning.

8.3.1 Architecture Classification

In the following sections, the architecture options previously described will be referred to as follows:

- 1) Transparent based non-terrestrial access network (Sec. 5.1);
- 2) Regenerative satellite and split gNB (Sec. 5.2.2);
- 3) Regenerative satellite and on-board gNB(s) (Sec. 5.2.1);
- 4) Regenerative satellite with Inter-Satellite Links (ISLs), gNB processed payload (Sec. 5.2.1);

5) gNB processed payload, Relay-like architecture (Sec. 5.2.3).

8.3.2 Intra-gNB Mobility ("Monolithic gNB")

In this case, all necessary signalling is confined to within the gNB, with no signalling impact on NG or Xn. For the case of "monolithic" gNB, this is supported without any standards impact by Architectures 1, 3, 4, and 5.

8.3.3 Intra-DU Mobility

In this case, all necessary signalling is confined to within the DU, with no signalling impact on F1. This is supported by Architecture 2 without any standards impact.

8.3.4 Intra-gNB/Inter-DU Mobility

This is supported by current inter-DU mobility. In Architecture option 2, the F1 signalling is transferred over SRI.

Single logic DU across multiple satellites is precluded.

8.3.5 Inter-gNB Mobility

8.3.5.1 Xn Mobility

For Architectures 1 and 2, Xn interfaces (if present) are terminated at the ground station; in these cases, Xn mobility is possible without any standards impact.

There is no Xn in Architecture 3, so in this case it is not possible to support Xn mobility.

For Architecture 4, Xn mobility is only possible between satellite-hosted gNBs.

Some further observations should be made on the issue of Xn mobility involving NTNs. In current NG-RAN specifications, Xn mobility is the mechanism of choice when moving between neighbour cells, ensuring the best performance and with minimal core network involvement thanks to the use of a "horizontal" interface, Xn. When considering NTNs, the concept of neighbour cells is going to be different, and at least two different cases should be considered:

- 1) Two "neighbour" cells belonging to NTNs;
- 2) Two "neighbour" cells, of which one is served by a terrestrial RAN, and the other by an NTN.

For the first case, if the two cells are served by two different logical nodes (e.g. satellites) within the NTN, it seems possible to set up Xn and use it for Xn mobility. This is indeed the case with Arch. 4, in which Xn would be transported on ISLs.

For the second case, the Xn-based mobility is only possible if an Xn exists between the NTN gNB and terrestrial gNB.

Architecture 5 (relay-like, Xn is terminated in the satellite but goes through the NTN-donor) seems to suffer from this problem. Therefore, in theory Arch. 5 supports Xn mobility between satellite-gNBs and terrestrial gNBs, but its performance seems questionable due to the above observations.

8.3.5.2 Mobility through the 5GC

In Architectures 1 and 2, NG is terminated at the ground station; in these cases, mobility through the CN is supported without any standards impact.

In Architectures 3, 4 and 5, NG is terminated at the satellite, so NG traffic needs to be transported over the SRI: mobility through the CN is possible.

8.3.6 Mobility due to interface change

In this case, the UE mobility (hand-over) is due to the change of the interface, for example, when the satellite moves out of the coverage of current radio network node on the ground, and the UE connects to either a new radio network node on the ground or a new network node on board the satellite.

- In Architecture Option 1, 3, 4 and 5, this means the change of AMF.
- In Architecture Option 2, this means the change of gNB-CU.

Due to the change of interface, all UEs need to be handover to new network node (i.e. AMF in Architecture Option 1, 3, 4 and 5, gNB-CU in Option 2). Handover all connected UEs in a short period can cause significant signalling load. Further study is needed.

For Mobility due to interface change, it may cause significant signalling load in all architecture options. Further study is needed.

8.3.6.1 Architecture option with gNB on board satellite

To mitigate the signalling load issue during the mobility due to NG interface change, a possible option is the Satellite implements two logical gNBs (e.g. gNB1 and gNB2). gNB1 connect to AMF1, and gNB2 connect to AMF2. gNB1 and gNB2 can share the same resource and UE context.

Since gNB1 and gNB2 are collocated in the same satellite and can share the resource, it can be assumed that same resource is used to serve the UE when the UE is handover from gNB1 to gNB2. So it may be possible to avoid the Handover Resource Allocation procedure. Current Handover Resource Allocation procedure allows the target AMF to update some UE context, e.g. the NG-U UL F-TEID. If Handover Resource Allocation procedure is not performed, the updated UE context may need to be sent from AMF to gNB1, then to gNB2 via an interface on board the satellite.

Using AMF re-allocation might be another option.

This clause illustrated one possible option to mitigate the interface change with high load management, other implementation are not precluded.

8.3.6.2 Architecture option with gNB-DU on board satellite

To mitigate the signalling load issue during the mobility due to F1 interface change, a possible option is the satellite implements 2 logical DUs (e.g. DU1 and DU2). DU1 connect to CU1, and DU2 connect to CU2. DU1 and DU2 can share the same resource and UE context.

Since DU1 and DU2 are collocated in the same satellite and can share the same resource, it can be assumed that the same resource keeps serving the UE when it is handover from DU1 to DU2. In that way it may be possible to avoid the F1 UE Context Setup procedure during inter-DU handover. Current F1 UE Context Setup procedure allows the target CU to update some F1AP UE context, e.g. gNB-CU UE F1AP ID, etc. If F1 UE Context Setup procedure is not performed, the updated F1AP UE context may need to be sent from CU to DU1, then to DU2 via an interface on board the satellite.

One possible call flow is shown as below.

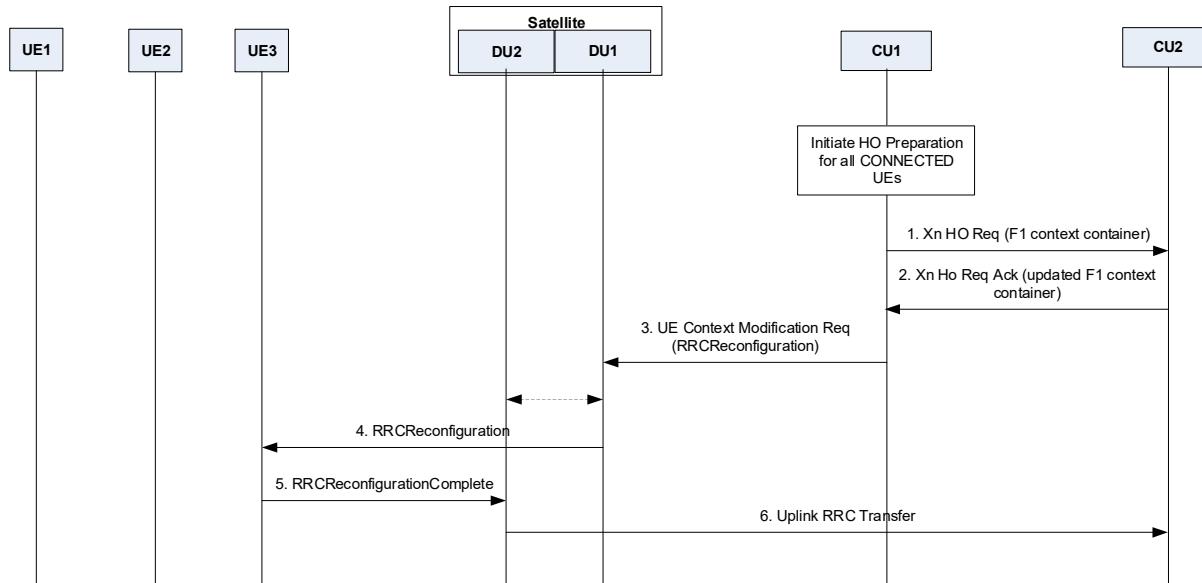


Figure 8.3-1: CU change example

- DU1 setup F1 with CU1. DU2 setup F1 with CU2. UEs are served by DU1/CU1.
- Step 1: CU1 determines the need to initiate handover preparation procedure for all connected UEs. CU1 send Xn Handover Request message to CU2. The Xn Handover Request message includes an indication that the handover is triggered due to CU switch, and a container for UE F1AP context. By this indication, CU2 will not send F1AP UE CONTEXT REQUEST to target DU.
- Step 2: The Xn Handover Request Acknowledge message includes a container for the updated F1AP context, e.g. CU2 may allocate a new gNB-CU UE F1AP ID.
- Step 3: CU1 forward the RRC Reconfiguration message to DU1. CU1 also include the new updated F1AP context. By implementation method, DU2 know the F1AP context to be used with CU2.
- Step 4: DU1 forward the RRC Reconfiguration message to UE
- Step 5: UE send RRC Reconfiguration Complete message to DU2
- Step 6: DU2 forward the RRC Reconfiguration Complete message to CU2. The normal handover procedure continues.

This clause illustrated one possible option to mitigate the interface change with high load management, other implementation are not precluded.

8.3.7 Summary

The table below summarises the applicability of hand-over procedures for different NTN architectures.

Table 8.3-2: Mobility support for the various NTN architectures

	Arch. 1	Arch. 2	Arch. 3	Arch. 4	Arch. 5
Intra-gNB mobility ("monolithic" gNB)	Supported, no standards impact	Does not apply	Supported, no standards impact	Supported, no standards impact	Supported, no standards impact
Intra-DU mobility	Does not apply	Supported, no standards impact	Does not apply	Does not apply	Does not apply
Inter-DU mobility	Does not apply	Supported, no standards impact	Does not apply	Does not apply	Does not apply
Xn mobility	Supported, no standards impact	Supported, no standards impact	Depends on Xn over SRI, no standards impact	Supported if Xn exists	Possible in theory, but performance seems questionable
Mobility through the 5GC	Supported, no standards impact	Supported, no standards impact	Supported, no standards impact	Supported, no standards impact	Supported, no standards impact

8.4 Transport aspects

In the transparent case, a NTN GW connects directly to one or several satellites via SRI. In the regenerative case, a NTN GW can directly connect to one or several satellites via SRI, or indirectly connect to one or several satellites via ISL. Hence the NG protocol is transported over SRI, and may also be transported over ISL.

A gNB is connected to the 5GCN. The transport of this logical interface can be realized over SRI and possibly over ISL.

The satellite may embark additional transport routing functions that are out of RAN scope.

SRI transports 3GPP-RAN specified protocols i.e., transmits the NG interface signalling packets.

ISL can transport:

- Xn interface signalling packets and enable coordination between gNBs on board adjacent satellites, and especially to support UE mobility, from a source gNB to a target gNB.
- Data packets, in case traffic functions are hosted on board the satellites.
- NG interface signalling packets
- F1 interface signalling packets

8.4.1 Characteristics of transport links in NTN

8.4.1.1 Characteristics of SRI on the feeder link

Transport over SRI may be subject to the following constraints:

- 1) Much longer propagation delay with respect to terrestrial transport links – the typical length for an Earth-satellite link can go from a few thousands of km (LEO scenario) to several tens of thousands of km (GEO scenario). Hence the one way delay over the SRI ranges from 6 ms (LEO at 600 km and 10° elevation) to ~136 ms (GEO at 35788 km and 10° elevation);
- 2) Possibly higher outage probability with respect to terrestrial transport links when the SRI operates at mm-wave, which is heavily impacted by atmospheric propagation impairments (e.g. rain attenuation). However this is mitigated through Uplink power control, Adaptive Coding and Modulation and/or space diversity schemes. Typically a feeder link is dimensioned to provide availability up to 99.999% with site diversity;
- 3) The SRI may become unavailable

- a. due to atmospheric attenuation when SRI operates at mm-wave
- b. when the satellite disappears below the horizon in LEO constellation

Therefore mobility management is typically activated to ensure a seamless service continuity and 0 ms interruption time, as described in Section 8.4.1.3.

In the transparent payload case,

- a GEO or a LEO satellite can be connected to several NTN-GW at a given time. Each NTN-GW will address different radio resources of the satellite.
- a feeder link switch over can be performed using two distinct radio resources simultaneously to ensure a packet loss less switch over. This procedure is network originated.

In the regenerative payload case,

- a LEO satellite can be connected to only one NTN-GW at a time except during feeder link switch over to ensure a seamless service continuity following the make before break approach.
- a feeder link switch over can be based on a make before break strategy to obtain a loss less switch over. This is transparent to the UE for layer 3 and below NG-RAN procedures. This procedure is network originated.

8.4.1.2 Characteristics of Inter Satellite link

In the LEO case, the one-way ISL propagation delay is constellation specific. Values around 10ms may be considered as typical.

Inter Satellite Links in LEO constellations typical feature an availability probability of 99.999%.

8.4.1.3 Characteristics of NTN GW

In the case of transparent satellite, the NTN GW supports all necessary functions to forward the signal of NR-Uu interface.

In the case of regenerative satellite, the NTN GW is a Transport Network Layer node, and supports all necessary transport protocols, e.g. the NTN GW acts as an IP router. The SRI provides IP trunk connections between the NTN GW and the Satellite to transport respectively NG or F1 interfaces.

8.4.1.4 Ephemeris

Satellite ephemeris information may be used to predict feeder link switchover occurrences, mobility management events (idle and connected mode), radio resource management, as well as pre/post compensation of common delay/Doppler shift/variation in NTN based NG-RAN.

The satellite ephemeris information may also be beneficial to 5GC, e.g. mobility management.

There may be an OAM requirement to configure the satellite ephemeris information in the RAN and CN. The ephemeris information can be expressed in an ASCII file using Two-Line Element (TLE) format, which is a de facto standard.

8.4.2 Transporting F1 over the SRI

According to the definitions given in TS 38.401 [3], the CU hosts the RRC, SDAP and PDCP protocols, and the DU hosts RLC, MAC and PHY layers; the CU controls the operation of one or more DUs. When F1 is transported over the SRI, the above functionality may be subject to the following constraints as described in 8.4.1.1.

Long propagation delay might be addressed by setting appropriate timers (up to implementation) so that operation in the various protocol layers is not disrupted by the NTN use case. However, the fact that RRC is terminated in the CU poses an additional criticality: if the CU is on the ground, the roundtrip time for a single RRC message between the UE and the CU corresponds to twice the Earth-satellite link (the RRC message travels through Uu over the NR air interface and then, transported over F1, through the SRI). Regardless of whether current NR RRC can withstand this additional

constraint, this might put any NTN architecture based on CU-DU split (described in Sec. 5.3.2) at a disadvantage with respect to all others in terms of RRC latency.

The impact of outage probability might be analysed by comparing the typical maximum outage duration for an Earth-satellite link at mm-wave frequency band with the time it takes for a CU to declare a UE "lost" and start removing the context (typically less than a minute). In case of an SRI outage, this will negatively impact the CU operation.

In addition, the fact that there are two Earth-satellite paths involved between the CU and the UE, may also negatively impacts all CU-DU-split-based architecture options with respects to all others also in terms of outage: the outage probability of these architectures depends on the combined outage probability on both links. This will depend on the performance of the SRI.

Using multiple Earth-satellite links to transport the same F1 interface by exploiting SCTP multi-homing, or multiple SCTP associations between CU and DU, might possibly mitigate the SRI unavailability due to outage or gateway switching at the cost of additional latency. This would be a trade-off between link outage de-correlation and added latency: the further apart the Earth stations are, the more the link outages would de-correlate, thereby decreasing the combined link outage, but the total distance to the CU (hence the F1 latency) would increase, thereby increasing latency.

8.4.3 Applicability of Xn to NTNs

8.4.3.1 List of Current Xn Functions

There was no contributions highlighting a restriction against the list of function supported in TS 38.420 [11] during the Study item.

8.4.3.2 Inter-Satellite Xn

UE mobility management for inter-satellite Xn seems beneficial, of course under the assumption that both satellite-gNBs connect to the same AMF pool. Purely from an architecture point of view, NR-NR DC is not precluded (with one satellite acting as Master and the other as Secondary), although further analysis would be needed (e.g. on RRC aspects, out of RAN3 scope) before concluding that NR-NR DC is supported. Energy saving is also not precluded purely from an architecture point of view, although in this case there seems to be some benefit, with one satellite notifying another of cell activation/deactivation as part of e.g. constellation reconfiguration.

Xn-U functions are applicable to mobility and DC, so the same considerations apply.

From the above it descends that inter-satellite Xn seems beneficial, although further analysis may be needed to assess the feasibility of NR-NR DC in such a scenario.

From topology point of view, the Inter-Satellite Xn may be conveyed directly over ISL or via SRI.

8.4.3.3 On-ground NTN-terrestrial Xn

This would support Xn-based UE mobility and NR-NR DC features between on ground NTN gNB and a terrestrial gNB, requires that both types of gNB connects to the same AMF pool.

Another feature is the support of Earth-satellite cell activation/deactivation notification over Xn. For example, a terrestrial gNB may notify a satellite covering the same area that it is switching off one or more of its cells, and the satellite may decide to "take over" the corresponding coverage area, and vice versa.

However the benefits of these features was not evaluated.

8.4.3.4 Transporting Xn over SRI

Transporting Xn over an Earth-satellite link between on board NTN gNB and terrestrial gNB has challenges, but it can be configured if the transport performance of SRI allows so.

For example, in a LEO scenario, when a satellite moves below the horizon, all its Xn interfaces to terrestrial gNBs will become unavailable, and this may trigger subsequent actions at application protocol and/or SCTP level in the relevant terrestrial gNBs. The opposite will happen when the satellite appears at the horizon: Xn setups may be triggered to

some terrestrial gNBs. This creates a technical issue, as it will lead to CP signalling surges corresponding to changes in visibility of the LEO satellites.

Furthermore depending on the outage performance of the SRI, Xn may become unavailable for some periods of time. This may trigger interface re-establishment toward all corresponding terrestrial gNBs, generating CP signalling surges at every outage event. This would happen for all Xn interface terminated in the on board NTN -gNB impacted by the outage event.

Therefore the benefit of this configuration was not evaluated.

8.5 Network Identities Handling

8.5.1 General

One of the most basic assumptions in the design of terrestrial radio access networks is that the RAN is stationary, and the UE moves. All network design choices, from physical layer parameters to network identities, have been specified with the above assumption in mind. When studying NTNs, however, the RAN is not necessarily stationary any more, depending on the type of satellite system (e.g. GEO vs. non-GEO). Examples of geometrical coverages of a satellite are given in [TR 22.822 Rel-16].

8.5.2 GEO based NTN (Scenario A and B)

Geostationary satellites are closer to the case of terrestrial RAN since they do not move with respect to their geographical coverage area. As far as network identities are concerned (e.g. gNB IDs, cell IDs, TAC, etc.), they do not seem to pose any additional issues with respect to the case of terrestrial RAN.

8.5.3 Non-GEO based NTN (Scenario C and D)

Non-GEO satellites (LEO, MEO and HEO), on the other hand, may provide additional challenges, because their coverage may move due to their orbital movement. One of the consequences, for example, is that mobility actions by the network will result from the combination of satellite movement and UE movement.

As the satellite moves across the geographical area of interest, its satellite beams will cover different portions of that area. The following scenarios could be envisaged for associating *logical* network identifiers to *physical* satellite beams:

- 1) The association between physical satellite beams and logical cells is continuously reconfigured so that the same gNB ID, cell ID and TAC are always associated to the same geographical area ("Stationary identifiers on ground");
- 2) The association between physical satellite beams and logical cells is fixed, so that the gNB ID, cell ID and TAC follow the satellite beam(s) and "sweep" across the coverage area ("Moving identifiers on ground").

Notice that in both cases the required configuration is internal to the gNB (satellite system) serving the concerned cells.

In both cases, once the satellite moves out of coverage (e.g. below the horizon), the corresponding cell network identifier(s) will become unavailable in the coverage area. This may trigger multiple NG and/or Xn setup or configuration update procedures toward the rest of the RAN. This may be critical when comparing the different architecture options. Ephemeris information could assist decisions to trigger interface setup and/or configuration updates.

8.5.3.1 Stationary Identifiers on ground

A stationary UE on the ground will always be covered by the same cell identifiers in the same position (similarly to the terrestrial network scenario). This is only possible for earth-fixed beams. Depending on how closely the granularity of the satellite beams enables to contour the desired coverage area, there could be slight variations in coverage. However, apart from the frequent NG and/or Xn setup or configuration update, it seems there would be no other impact.

8.5.3.2 Moving Identifiers on ground

A stationary UE on the ground will be covered by different cell identifiers in the same position, according to the satellite motion. The moving satellite is likely to provide multiple cells, which will all move together; therefore, their respective neighbour relations will remain unchanged with respect to the satellite motion. However relative position between satellites may vary so that PCI confusion is possible. If the same frequency is used by the NTN and Terrestrial Network at a given location, then this may cause PCI confusion as well.

8.5.3.3 Possible Implications on Neighbour Relationships

One aspect to further consider is what happens with respect to fixed (e.g. terrestrial) RAN nodes: in principle, the neighbour relation between two cells belonging to respectively a fixed RAN and a moving RAN or to two different moving RAN keeps changing reusing current mechanisms such as e.g. ANR between a fixed RAN and a moving RAN.

8.5.3.4 Possible PCI Conflicts

Moving cells can create PCI conflicts, namely PCI collisions (when two cells with the same PCI become direct neighbours) and PCI confusion (when two cells with same PCI become neighbours of one cell). The result of those PCI conflicts can be radio link failures (PCI collision) or handover failures (PCI confusion). Unfortunately, it is not always possible to detect that the root cause of those failures were a PCI problem, and not another mobility problem. PCI problems can be avoided by two principle methods

- If there are less cells than PCIs, then we can certainly assign unique PCIs. Similarly, if we can partition the cells into groups, where we can guarantee that groups are sufficiently spatially separated, we can partition the PCIs appropriately and assign unique PCIs within the groups.
- In case it is difficult to assign unique PCIs within the groups, it may require to regularly verify whether the PCI allocation is still appropriate and re-plan PCIs otherwise. For NTN architecture with gNB-CU on ground, the Xn interface can help the gNB-CU to detect the PCI collision and the PCI confusion. For NTN architecture option with gNB on satellite, the Xn over ISL or Xn over SRI, is needed for satellite gNB to detect the PCI collision and the PCU confusion.

In some scenarios, the NTN cell may need to change PCI. For example, in case a gNB-CU change with gNB-DU on satellite, the NTN cell may have to change PCI in order to force a handover procedure, which is used to reconfigure the UE with new parameters generated by the new gNB-CU. In these scenarios, a NTN cell may need to be preconfigured with multiple PCIs, i.e. to be used with different gNB-CUs. Alternatively, the gNB-CU may reconfigure the new PCI.

Existing Xn interface and F1 interface can be reused for distributed PCI selection and PCI reconfiguration.

8.6 User Location

A non-terrestrial network may provide global, or multi-country coverage. This imposes new challenges as compared to the terrestrial networks. For example, different policies may apply in different countries. The policies are enforced while the UE is in RRC CONNECTED mode.

The coverage area of one satellite beam may cover (parts of or) more than one country at times, while the satellite field of view may be larger than a country.

The User Location Information, i.e. NTN cell id, may not provide sufficient accuracy to the network to ensure that the right, country-specific policies can be applied. A more accurate UE location determination scheme for RRC CONNECTED UE may be needed to enforce country-specific policies.

When the UE cannot report the exact position information for some reason, such as GPS loss or do not have position capability, the national granularity can be obtained from the PLMN of the terrestrial network. For example, the UE can read and report the surrounding cells PLMN.

The UE location information could be report by several ways:

- Option 1: the UE can report the location information to the AMF through the NAS message, e.g. during the Registration Procedure;
- Option 2: Upon the reception of the UE's location information from the UE, the gNB forwards it to the AMF. In this manner, the network side can control the UE report more strictly.

8.7 Feeder link switch over

8.7.1 Principles

During NTN operation, it may become necessary to switch the feeder link (SRI) between different NTN GWs toward the same satellite. This may be due to e.g. maintenance, traffic offloading, or (for LEO) due to the satellite moving out of visibility with respect to the current NTN GW. The switchover should be performed without causing service disruption to the served UEs. This can be done in different ways according to the NTN architecture option deployed.

8.7.1.1 Transparent Satellite

8.7.1.1.1 Transparent LEO, Architecture Option 1, different gNBs

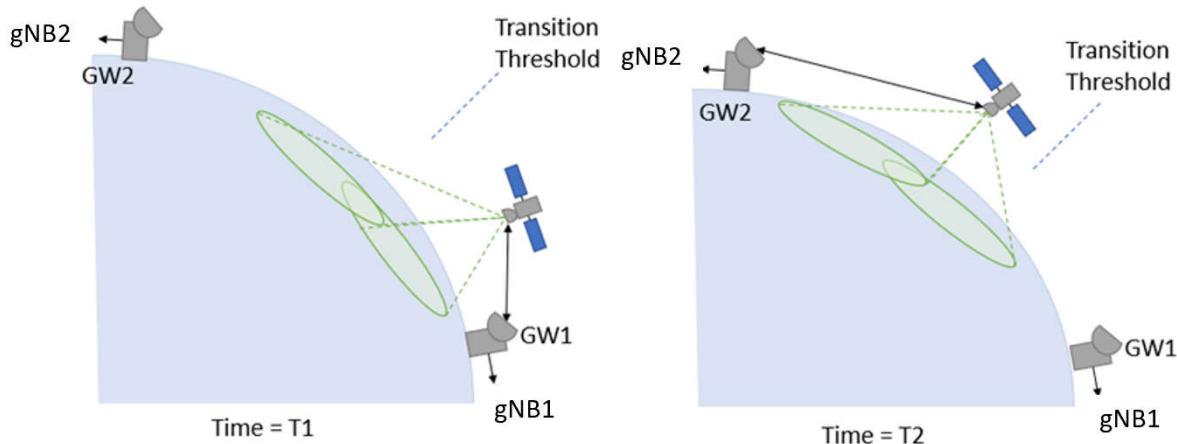


Figure 8.7.1.1-1: Feeder link switch for transparent LEO NTN

Figure 8.7.1.1-1 shows the feeder link switch for transparent LEO. As seen from the figure, in the transparent case the gNB is on earth thus there will be a switch from gNB1 to gNB2. If the satellite can be served by one feeder link at a time it means that with Rel-15 NR assumptions the RRC connection for all UEs served by the gNB1 (via GW1) needs to be dropped. After gNB2 (via GW2) takes over, the UEs may be able to find the reference signals corresponding to gNB2 and perform initial access on a cell belonging to gNB2.

Figure 8.7.1.1-2 shows one possible solution to enable service continuity for feeder link switch. At time T1, the satellite is approaching the geographical location where the transition to be served by next GW will happen. At time T1.5, the satellite is served by two GWs and at time T2 the transition to next GW is finished.

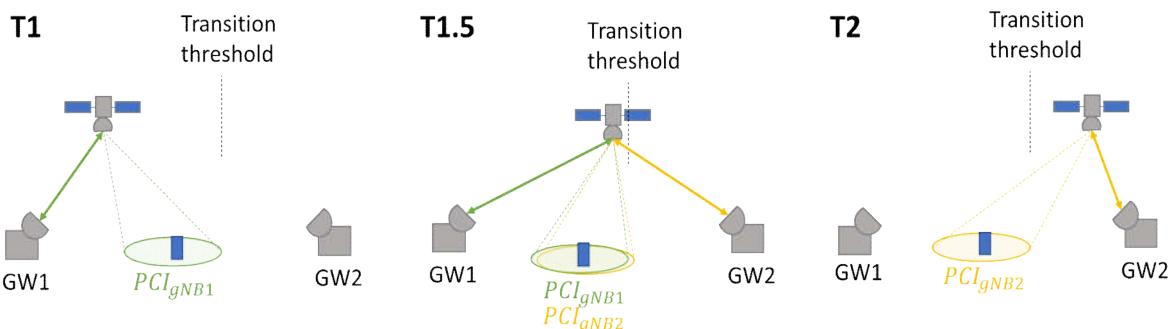


Figure 8.7.1.1-2: Feeder link switch over for LEO transparent satellite with two feeder links serving the satellite during the switch

Assuming two feeder link connections serving via the same satellite during the transition (time T1.5 in Figure 8.7.1.1-2), there exists a HO based solution that should be feasible with Rel-15 or close to Rel-15 assumptions. This assumes that it is possible to represent cells of two different gNBs over a given area via the same satellite but via different NTN-GWs. The two gNBs may utilize different radio resources of the transparent satellite to ensure both gNBs are visible to the UE (overlapping coverage areas) simultaneously. During the switch, the gNB2 which serves the satellite via GW2 may start transmitting the CD-SSBs of its cells on synchronization raster points that are different from those of the gNB1. UEs could have a HO from PCI belonging to gNB1 to PCI belonging to gNB2. This could be a blind HO (network decision without measurement) or assisted with measurements. Alternatively, the gNB1 may be present for a first time-period and configure a conditional handover to the gNB2, after which the gNB2 is available for a second time-period where the UEs can then perform the radio handover. Furthermore, the mobility solution may need to also mitigate for the fact that the UEs may observe very similar RSRP/RSRQ of the service links, provided by the source and target gNBs, because the reference signals are transmitted from the same satellite. One solution may be left to network implementation, e.g. setting proper event A5 thresholds for conditional handover to enable handover, or to rely on radio propagation time instead or in combination with the RSRP/RSRQ radio measurements. Relying on radio propagation time includes taking the RTT experienced by the UE into account in handover decisions. Either as condition in CHO or in network HO decision.

Figure 8.7.1.1-3 shows another possible solution to enable service continuity for feeder link switch. At time T1, the satellite stops to transfer the signalling from the serving GW1. At time T2, the satellite starts to transfer the signalling from the target GW2.



Figure 8.7.1.1-3: Feeder link switch over for LEO transparent satellite with one feeder links serving the satellite during the switch

Assuming only one feeder link connection serving via the same satellite is applicable during the transition, which means the signal of the serving cell will be not available during time T1 to time T2. To make the UE access to the serving cell again, two potential options are listed below:

Solution 1: Feeder link hard switch procedure is based on accurate time control

Assuming the old feeder link serves the satellite until to T1 and the new feeder link begins to serve the satellite from T2. This assumes that the cells of the source gNB(s) are represented over a given area at any time before T1, and the new cells of the target gNB(s) are represented from time T2.

As there's no overlap of source cells and target cells from the gNB(s) located at the old and the new NTN GWs, the switch over relies on accurate time control. The handover command should be sent to all the UEs before T1, e.g. CHO. The UE should not initiate the handover procedure immediately upon receiving the Handover Command, instead, UE should initiate the handover procedure after T2, and thus an activation time should be included in the handover command to all the connected UEs.

Solution 2: Feeder link hard switch procedure is based on conditional RRC re-establishment

Considering the large cell size of NTN, it might be an extremely difficult problem for gNB1 to send HO commands to a large number of UEs respectively in a short time. A part of UEs may not be able to perform HO in time, as a result, radio link failure may be detected and then UEs initiate the RRC reestablishment procedure. It will take a long time to restore RRC connection, which may involve RLF detection, cell selection and potential reestablishment failure, as a result it has an influence on the service continuity. Thus it may be beneficial for network to provide assistance information (e.g. next cell identity and/or reestablishment conditions) to trigger UE RRC reestablishment instead. Besides, the assistance information can be sent to UE via SIB instead of dedicated signalling respectively, as a result, the signalling overhead caused by the large number of UEs can be effectively reduced.

How to enable cells of two gNB via the transparent LEO satellite can be defined in the WI phase.

8.7.1.1.2 Transparent LEO NTN, Architecture Option 1, same gNB

It is also possible the transparent satellite is served before and after the feeder link switch by the same gNB. In this case, both feeder links are connected to the same gNB, but through different NTN-GWs.

Assuming two feeder link connections serving via the same satellite during the transition, it could be possible for the gNB to keep the DL reference signals and to keep the cell "alive".

Note: In this case, it may be possible to not to need a HO if the security keys of gNB can be kept but there may merely be an interruption, or slight discontinuity in DL transmissions. It should be also noted that the need for reconfiguration with sync(HO), or without sync, depends on whether gNB configuration remain the same or not during the switch.

Assuming only one feeder link connection serving via the same satellite during the transition, the satellite will need to first stop relaying using the feeder link connection with the NTN-GW1 and then start relaying using the target NTN-GW2. In this scenario the cell cannot be kept "alive" without interruption and there will be a discontinuity in DL transmissions as illustrated in Figure 8.7.1.1-4.

For Feeder link hard switch, the solutions captured in 8.7.1.1.1 in different gNBs scenario can be also applied to this same gNB scenario.

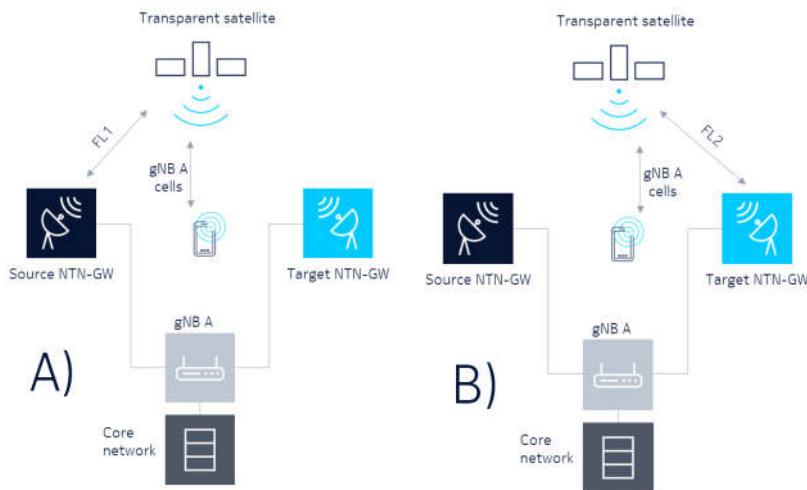


Figure 8.7.1.1-4: Using 1 gNB and 2 feeder links in a transparent satellite

At time A) the gNB A is connected with the source NTN-GW and serving the UE. At time B) the gNB A is serving users via the target NTN-GW.

The switchover relies on the temporary overlap of cells from the gNBs located at the old and the new NTN GWs. The UEs are then handed over from the old to the new gNB, before the old gNB detaches from the satellite. It is a prerequisite that the cells from the new gNB are seen as neighbours by the old gNB, hence Xn needs to be up and running between the two gNBs. Furthermore, the whole process (from UEs measuring the new cells to handover completion) needs to take place before the old gNB detaches from the satellite (potentially critical for the LEO case).

It may be beneficial for the two gNBs to exchange information at Xn Setup and/or NG-RAN Node Configuration Update about the satellite(s) potentially involved, for example:

- A list of satellites to which the gNB connects;
- For each satellite in the list, an ID, a list of cell(s) from the gNB which is served through the satellite, and the ephemeris data for the satellite.

8.7.1.2 Regenerative Satellite, Split gNB

The switchover can be supported for this architecture option only if the gNB-CU on the ground is centralized. In this case, both NTN GWs are part of the TNL transporting the F1 interface between the gNB-DU on the satellite and the centralized gNB-CU. The switchover is then equivalent to adding/removing an SCTP association between the CU and the DU. According to current specifications, this is triggered from the gNB-CU.

Option A: The DU may signal, at F1 Setup and/or DU Configuration Update, the relevant satellite information (e.g. satellite ID, ephemeris data); the CU may take it into consideration when configuring the TNL.

Option B: The CU may take into consideration, the relevant satellite information (e.g. satellite ID, ephemeris data) when configuring the TNL transporting the F1 interface.

8.7.1.3 Regenerative Satellite, with full gNB on board, Architecture Options 3-5

In this architecture option, the full gNB is onboard of the satellite as payload. If we consider the LEO case, from Uu perspective, this case is considerably simpler than the transparent LEO NTN as the Uu is only transmitted via service link as compared to being transmitted via service and feeder links. The feeder link switch can be transparent at Uu interface as long as the security keys of the gNB can be preserved. Figure 8.7.1.3-1 depicts the situation.

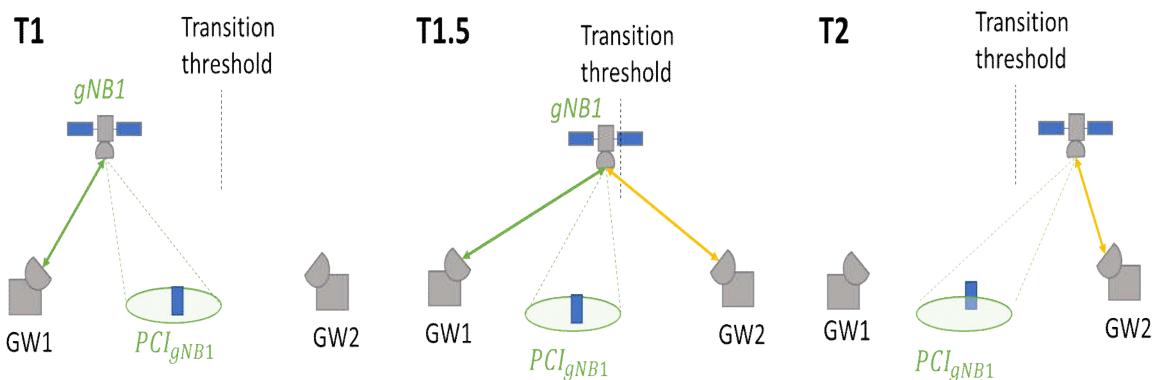


Figure 8.7.1.3-1: Feeder link switch over for regenerative LEO with full gNB as payload with two feeder links serving the satellite during the switch

The other situation, when using full gNB and one feeder link during the switch entails there will be a break in satellite – NTN GW connectivity, when the feeder link is switched from the source NTN GW to the target NTN GW. To smoothen the feeder link switch, the configuration of transport association for the target NTN-GW feeder link may be signalled before the source NTN-GW feeder link breaks. In principle, the gNB may continue to broadcast system information while the switch is ongoing, but refrain from scheduling any users, since the feeder link connectivity to Earth is not available. In this way, the cell(s) will not disappear from UE perspective. If the AMF does not change, the switch is transparent to the UEs except for a U-plane delay, because cell ID, MIB, SI remains the same. Figure 8.7.1.3-2 depicts this situation.

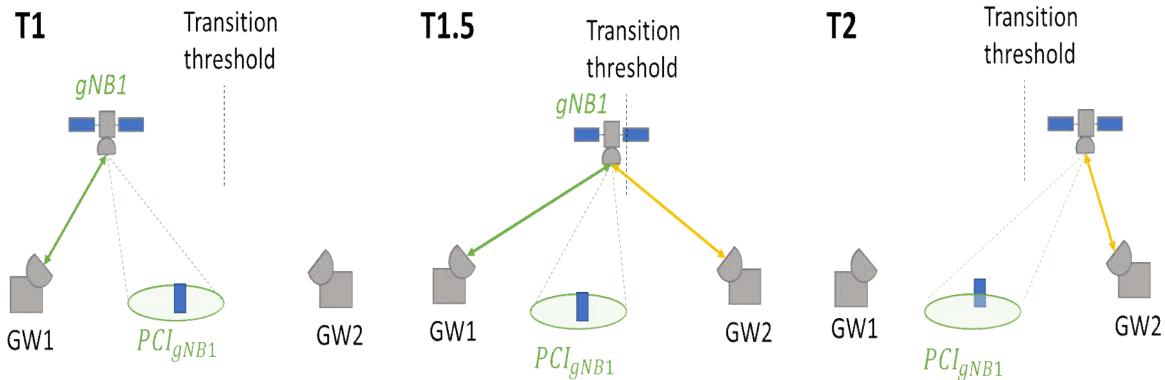


Figure 8.7.1.3-2: Feeder link switch over for regenerative LEO with full gNB as payload with two feeder links serving the satellite during the switch

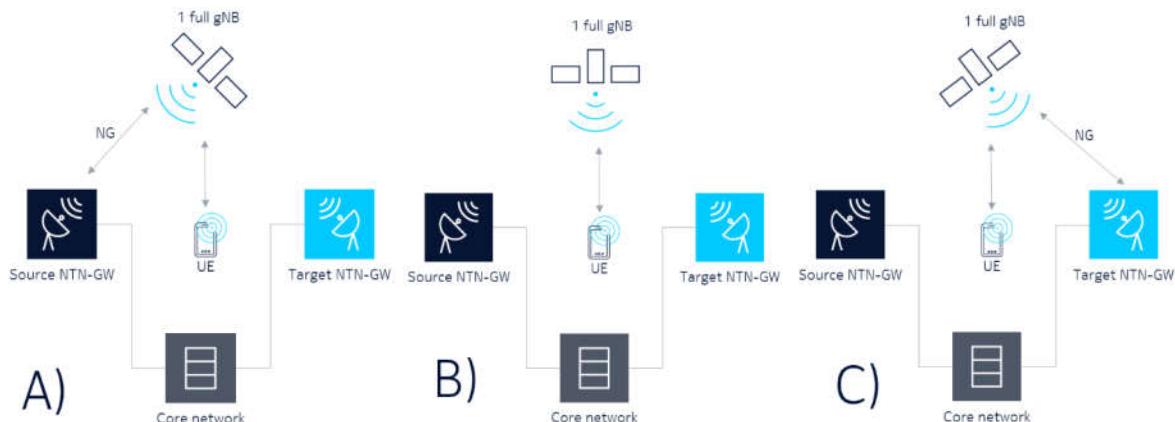


Figure 8.7.1.3-3: Feeder link switch over for regenerative LEO with full-gNB as payload with one feeder link serving the satellite during the switch

8.7.1.3.1 Regenerative LEO NTN with one gNB-DU as payload, Architecture Options 3-5

In case of having a CU-DU split with one DU on the satellite, while the CU is on the ground and one feeder link, the same gNB-CU may be connected to both the source and the target NTN GW the F1 may be re-routed to the target NTN GW at a specific point in time. In this case the switch may be transparent to the UEs except a user-plane delay. The gNB-DU may continue to broadcast system information, but not schedule UEs. Note that the gNB CU refers to a combination of gNB CU user plane or gNB CU control plane.

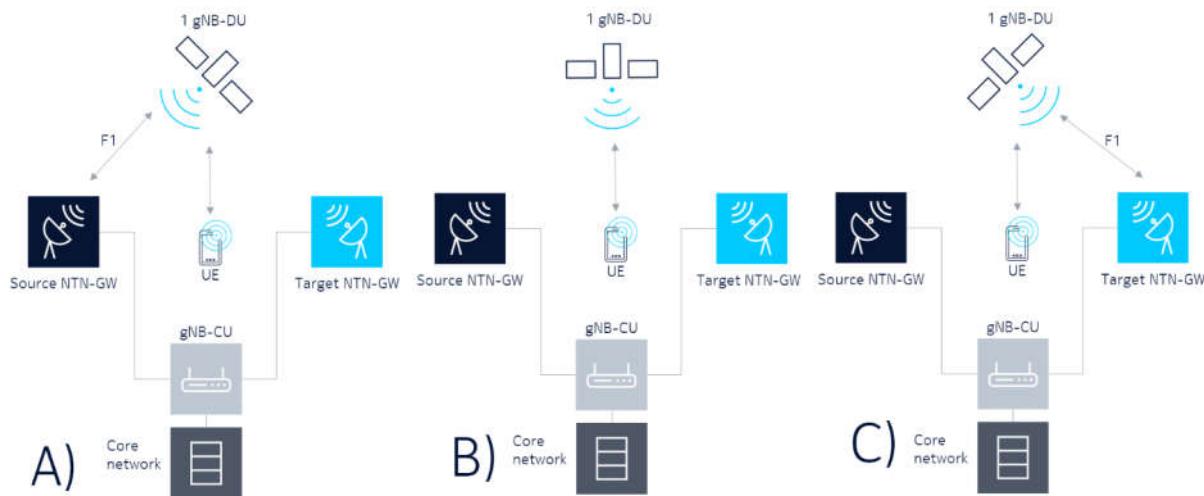


Figure 8.7.1.3.1-1: Using 1 gNB-DU on the satellite and 1 feeder link

At time A) the gNB-DU is connected with the source NTN-GW and serving the UE. At time B) the feeder link switch is taking place and the gNB-DU is not connected with any NTN-GW. The gNB-DU may still broadcast system information to the UE. At time C) the gNB-DU is serving users via the target NTN-GW. In case the gNB-DU connects to a new gNB-CU at time C) the UE would need to perform a handover or cell reselection.

If the gNB-CU is changed the gNB-DU will initiate the F1 setup procedure to connect with the next gNB-CU (note a gNB-DU can only connect to one gNB-CU at a time and thus the connection with the current gNB-CU must first be terminated). When the connection between the new gNB-CU and the gNB-DU is established through the target NTN GW the cell ID, MIB, and SI will need to be updated to reflect the new gNB-CU configuration. This will imply a drop of the connection for all UEs in the coverage area, who can reconnect to the new gNB-CU after the switch. The scenario is illustrated in Figure 8.7.1.4-1

If the gNB-CU is changed the UEs will be disconnected with RLF, because a HO requires both source to target CU to communicate with the DU on the satellite, and this is not possible because a DU can only be connected to one CU at a time.

In this case, both NTN GWs are part of the TNL transporting the F1 interface between the gNB on the satellite and the AMF. The switchover is then equivalent to adding/removing an SCTP association between the gNB and the AMF. According to current specifications, this is triggered from the AMF. The gNB may signal, at NG Setup and/or RAN Configuration Update, the relevant satellite information (e.g. satellite ID, ephemeris data); the AMF may take it into consideration when configuring the TNL.

8.7.1.3.2 Regenerative LEO NTN with two gNBs, or gNB-DUs as payload, Architecture Options 3-5

Having two gNB-DUs with individual feeder link connections entails the UEs may perform intra-gNB-CU inter-gNB-DU mobility (in case the gNB-CU does not change). This is significantly faster than a gNB-CU change, which corresponds to a regular gNB-gNB handover, but also includes F1 communication and the related delays.

8.7.2 Procedures

8.7.2.1 Transparent payload case

The switchover may be predictable (e.g. based on the LEO satellite ephemeris information and NTN GWs location) or event-triggered (e.g. for maintenance). In this case, it could be beneficial to introduce a dedicated, non-UE-associated Xn procedure (Satellite Connection Request) to signal from the old to the new gNB that it should connect to the specified satellite, optionally including the list of cells served through the satellite.

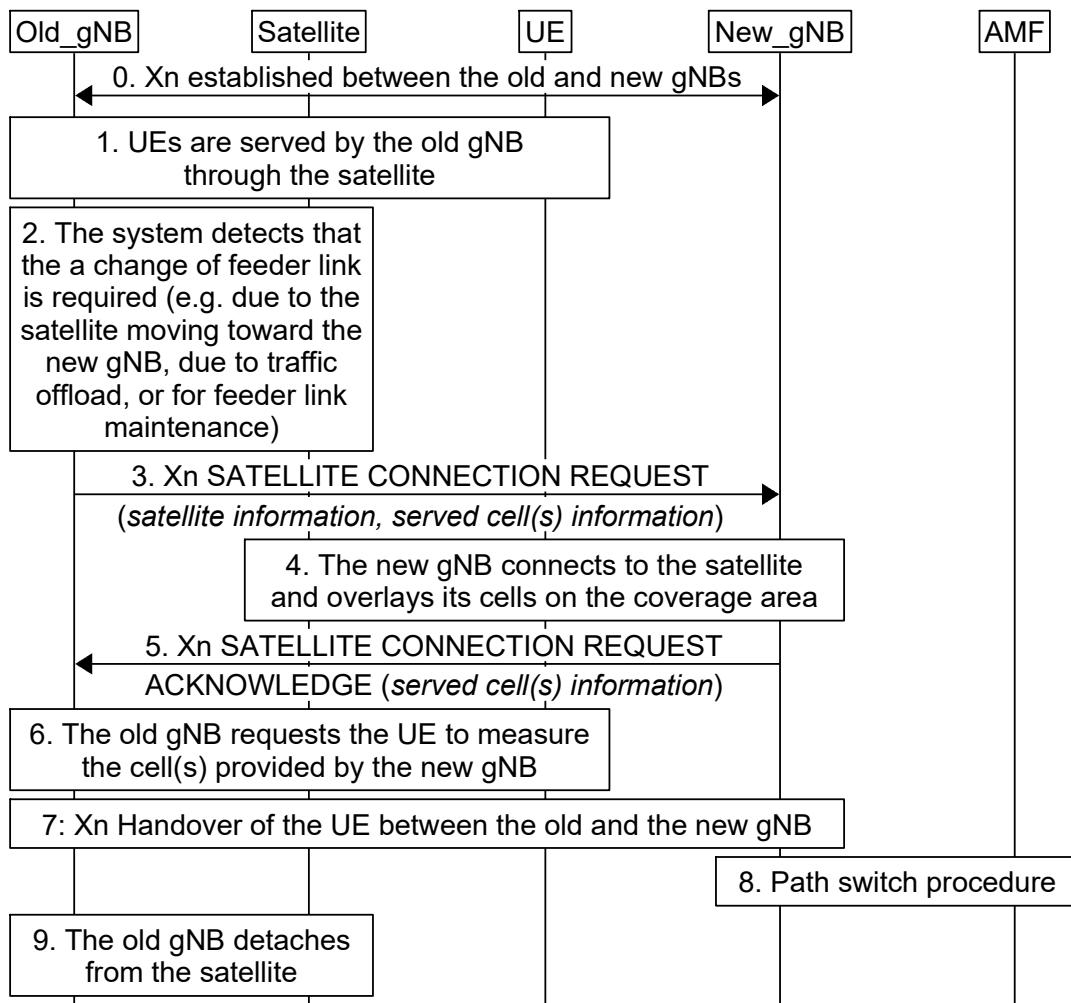


Figure 8.7.2.1-1: Feeder link switch over procedure for transparent LEO satellite (Scenario C2)

This above described procedure allows a soft switch procedure.

Alternatively, a hard switch procedure could be considered to allow for no simultaneous connectivity between satellite and the 2 NTN-GWs.

This would require to prepare and execute the hand-over precisely using ephemeris data and accurate time information.

8.7.2.2 Regenerative payload case (gNB on board)

As the LEO satellite moves out a specific geographic area, the satellite may be out of the serving area of the NTN Gateway, and needs to connect to a new NTN Gateway. There are two further cases:

Case 1: the satellite remains in the coverage area of current AMF.

To use the new NTN Gateway for the SCTP with the current AMF, the satellite/gNB has to use a new IP address that is anchored in the NTN Gateway. The satellite/gNB could use the multiple TNAs by adding the new SCTP IP address then remove the old SCTP IP address. This may result in the termination of the existing SCTP, and setup a new SCTP using the new IP address. Alternatively, the satellite/gNB may use Mobile IP, or Proxy Mobile IP to maintain the SCTP with the current AMF using the current IP address. The NG interface remains unaffected after the satellite/gNB connects to current AMF via the new NTN Gateway.

=> Considering that NTN-GW is transport network node, this case can be supported by existing NG procedure (set-up, configuration update, etc.) without modification

Case 2: the satellite moves into a coverage of a new AMF.

The satellite/gNB need to setup the connection with a new AMF.

How to handle the NG connection with the old AMF?

There is no NG release procedure. It is unclear whether the gNB/AMF can use the indication from the SCTP layer, e.g. the satellite/gNB initiates a SCTP Shutdown before it leaves the old AMF. This should be treated differently than the abnormal case, e.g. satellite/gNB lost the connection with the AMF due to bad satellite radio connection. Since the satellite/gNB will connect to the same AMF in the near future, there may be no need to release the NG.

=> Therefore we may enhance the NG procedure for example the satellite/gNB and AMF may suspend the NG interface and keep the application level configuration data when the satellite/gNB leaves, then resume the NG interface when the satellite/gNB connects to the same AMF later.

How to setup the NG connection with the new AMF?

A gNB can setup NG connection with multiple AMFs. So it is possible that the satellite/gNB setup the NG with the new AMF, while still keep the NG with the old AMF.

=> No impact to NG procedure is expected

8.7.2.3 Regenerative payload case (gNB split)

As the LEO satellite moves out of a specific geographic area, the satellite/gNB-DU loose the connection with current NTN Gateway, and needs to connect to a new NTN Gateway. There are two further cases:

Case 1: the satellite remains in the coverage area of current gNB-CU.

To use the new NTN Gateway for the SCTP with the current gNB-CU, the satellite/gNB-DU has to use a new IP address that is anchored in the NTN Gateway. The satellite/gNB-DU could use the multiple TNAs by adding the new SCTP IP address then remove the old SCTP IP address. This may results the termination of the existing STCP, and setup a new SCTP using the new IP address. Alternatively, the satellite/gNB-DU may use Mobile IP, or Proxy Mobile IP to maintain the SCTP with the current gNB-CU using the current IP address. The F1 interface remains unaffected after the satellite/gNB-DU connects to current gNB-CU via the new NTN Gateway.

=> Considering that NTN-GW is transport network node, this case can be supported by existing F1 procedure (set-up, configuration update, etc.) without modification

Case 2: the satellite moves into a coverage of a new gNB-CU.

The satellite/gNB-DU need to setup the new F1 with the new gNB-CU. There are some issues that need to be further studied:

Issue 1: How to handle the F1 connection with the old gNB-CU?

There is no F1 release procedure. It is unclear whether the gNB-CU/DU can use the indication from the SCTP layer, e.g. the satellite/gNB-DU initiates a SCTP Shutdown before it leaves the old gNB-CU. This should be treated differently than the abnormal case, e.g. satellite/gNB-DU lost the connection with the gNB-CU due to bad satellite radio connection. Since the satellite/gNB-DU will connect to the same CU in the near future, there may be no need to release the F1. Instead, the satellite/gNB-DU and gNB-CU may suspend the F1 interface and keep the application level configuration data when the satellite/gNB-DU leaves, then resume the F1 interface when the satellite/gNB-DU connects to the same gNB-CU later.

=> Therefore we may enhance the F1 procedure for example the satellite/gNB-DU and CU may suspend the F1 interface and keep the application level configuration data when the satellite/gNB-DU leaves, then resume the F1 interface when the satellite/gNB-DU connects to the same CU later.

Issue 2: how to setup the F1 connection with the new gNB-CU?

According to current F1AP, one DU can only connect to one CU. It is not possible for the DU to setup the F1 with the new CU, while still keep the F1 with the old CU. One possibility is to have 2 DUs on the satellite. While the 1st DU connects to the old gNB-CU, the 2nd DU setup the connection with the new gNB-CU.

=> No impact to F1 procedure is expected

8.8 Operations & Maintenance (O&M)

The Non-Terrestrial Networks architecture shall fulfil the O&M requirements on transport of O&M information between the Management System on the ground and Non-Terrestrial Node(s) on the satellite.

If possible, the software (or upgrade) should be ensured.

Referring to the architecture scenarios clause 8.3.1:

Table 8.8-1: O&M support for the various architectures

	Arch. 1	Arch. 2	Arch. 3	Arch. 4	Arch. 5
Transport of O&M information	Supported, no standards impact – Minimum (Alarm)	Supported, no standards impact – Full O&M	Supported, no standards impact – Full O&M	Supported, no standards impact – Full O&M	Does not apply
Hardware maintenance	Not supported	Not supported	Not supported	Not supported	Not supported
Software maintenance	Supported	Supported	Supported	Supported	Not supported

NOTE: the hardware maintenance and the software maintenance in case of Arch.1 should be rare.

9 Recommendations on the way forward

9.1 Recommendations from RAN1

Based on the evaluation results of this study, it can be concluded that:

- Class 3 UE can be served by LEO and GEO in S-band with appropriate beam layout (including potential frequency reuse and/or polarization reuse).
- Other UE (e.g. VSAT and phase array) with high TX/RX antenna gains can be served by LEO and GEO in both S-band and Ka-band with appropriate beam layout (including potential frequency reuse and/or polarization reuse)

Existing Rel-15 and Rel-16 NR functionalities form a very good basis for supporting NTN scenarios (LEO and GEO).

There are however issues due to long propagation delays, large Doppler effects, and moving cells in NTN. To address the identified issues, for a potential normative phase, it is proposed to focus on the following:

- Timing relationship enhancements
- Enhancements on UL time and frequency synchronization
- Enhancement on the PRACH sequence and/or format in the case pre-compensation of timing and frequency offset is not done at UE side

In addition, the following topics should be discussed when specifications are developed:

- Beam management and BWP operation for NTN with frequency reuse.
 - Including signalling of polarization mode
- Feeder link switch impact on physical layer procedures in case of LEO scenarios

- Number of HARQ process with additional considerations such as HARQ feedback/buffer size and RLC ARQ feedback/buffer size in the case of LEO and GEO scenarios
- Support of enabling / disabling of HARQ feedback.

In addition, discussions identified in clauses 6.2 to 6.4 of the document without conclusions, can be continued.

PAPR optimizations for downlink channels are not necessary to be specified for NTN at least for Rel-17.

9.2 Recommendations from RAN2

Based on the study performed, Rel.15 and NR can support NTN scenarios with enhancements identified below to be considered as part of the normative work.

In general,

- Offset based solutions for timer adaptations are preferred to support all NTN scenarios.
- Earth fixed tracking area is recommended.

The Rel-15's user plane procedures apply to NTN with enhancements to the following features

- MAC
 - Random access:
 - Definition of an offset for the start of the ra-ResponseWindow for NTN and extension of the ra-ResponseWindow duration to support UE without location information.
 - Introduction of an offset for the start of the ra-ContentionResolutionTimer to resolve Random access contention
 - Solutions for resolving preamble ambiguity and extension of RAR window.
 - Adaptations for UEs with GNSS capabilities; timing advance and msg3 scheduling.
 - Timing advance: TA calculation and signaling adaptation to deal with NTN maximum round trip delay in LEO and GEO scenarios for UE with and without UE location information.
 - DRX:
 - If HARQ feedback is enabled, an offset should be added for *drx-HARQ-RTT-TimerDL* and *drx-HARQ-RTT-TimerUL*.
 - If HARQ is turned off per HARQ process, adaptions in HARQ procedure may be required
 - Options for UE power saving for SR and CFRA can be discussed during work item phase
 - Scheduling Request: Extension of the value range of *sr-ProhibitTimer*
 - HARQ
 - enabling / disabling of uplink HARQ feedback for downlink transmission at the UE receiver should be configurable per UE and per HARQ process.
 - enabling / disabling of HARQ uplink retransmission should be configurable per UE or per HARQ process. The LCP impact caused by disabling the HARQ uplink retransmission configuration and its impact on UE's uplink transmission should be discussed in the work item phase.
 - Multiple transmission of the same TB to lower residual BLER should also be configured.
- RLC
 - Status reporting: Extension of the value range of *t-Reassembly*

- Sequence Numbers: extension of the SN space only for GEO scenarios will be discussed during the work item phase
- PDCP
 - SDU discard: Extension of the value range of *discardTimer* will be discussed during the work item phase.
 - Sequence Numbers: extension of the SN space for GEO scenarios will be discussed during the work item phase.

The Rel-15's control plane procedures apply to NTN with enhancements to the mobility management procedures when considering Earth moving beam footprint option.

- Idle mode:
 - Definition of additional assistance information for cell selection/reselection (e.g. using UE location information, satellite Ephemeris information)
 - Use earth-fixed tracking area to avoid frequent TAU
 - NTN cell specific information in SIB
- Connected mode:
 - Definition of schemes to reduce service interruption during Hand-Over due to large propagation delay (especially in the case of GEO transparent)
 - Definition of schemes to tackle frequent handover and high handover rate due to satellite movement (e.g. LEO NTN)
 - Definition of schemes to improve handover robustness due to small signal strength variation in regions of beam overlap
 - Definition of schemes to compensate for propagation delay differences in the UE measurement window between cells originating from different satellites, especially for LEO NTN
- Other mobility enhancements:
 - Additional CHO triggering conditions (e.g. location/time based), and adaptation of measurement-based thresholds and events to the NTN environment.
 - Possible enhancements to mobility configuration (e.g. to support broadcast configuration)
 - Enhancements to measurement configuration/reporting (e.g. pre-triggering based solutions)
 - Service continuity for mobility from TN to NTN and from NTN to TN systems

The Rel-16's user plane 2 step RACH procedure can be considered during the WI phase with possible enhancements:

- The required adaptations will be discussed during the WI phase, such as inclusion of assistance information, e.g., SFN index, in MsgA etc.
- The trade-off between latency gain and UL overhead impact caused in NTN scenarios by the introduction of 2-step RACH procedure can be further discussed during the normative work.

The same solutions identified for Earth moving cell scenario can also be applied for Earth fixed cell scenario, however whether specific solutions are necessary (or preferred) for each scenario can be further evaluated in the normative phase.

9.3 Recommendations from RAN3

There are no showstoppers to support any identified architecture options in clause 8:

- Transparent satellite based NG-RAN architecture

- Regenerative satellite based NG-RAN architectures

The Regenerative satellite based NG-RAN architectures with gNB processed payload based on relay-like architecture was not studied due to the pending work on IAB support (WI IAB_NR).

For a potential normative phase, it is proposed to focus on the following

- GEO based satellite access with transparent payloads
- LEO based satellite access with transparent or regenerative payloads

No specific issues have been identified to support the split regenerative payload case (gNB-DU on board) ; some protocol adaptation may be needed in a potential normative phase.

In case, the architecture option based on relay-like architecture (IAB) needs to be supported in non-terrestrial networks, further study will be needed.

9.4 Other assumptions

The NTN study results apply to GEO scenarios as well as all NGSO scenarios with circular orbit at altitude greater than or equal to 600 km.

For other NTN scenarios with orbits less than 600 km as UAS (including HAPS) scenario, no specific analyses have been performed during this study item. However, considering the characteristics of UAS such as delay (altitude), footprint size (differential delay) and Doppler identified in this study item, the same enhancements as LEO may be applicable for UAS because their values and variation rates are lower than LEO. The enhancements for LEO are not necessarily required for UAS scenarios when delay, footprint and Doppler can be similar or equivalent values with those of terrestrial network, but the detailed conditions were not discussed in this study item, as well.

Annex A: Satellite ephemeris

A.1 Key parameters

Key parameters of orbital mechanics of all commercial satellites are publicly available from multiple sources. This information is called ephemeris, which is used by astronomers to describe the location and orbital behaviour of stars and any other astronomic bodies.

Typically, ephemeris is expressed in an ASCII file using Two-Line Element (TLE) format. The TLE data format encodes a list of orbital elements of an Earth-orbiting object in two 70-column lines. The contents of the TLE table are reproduced below.

Table A.1-1: First line of the ephemeris

Field	Columns	Content
1	01–01	Line number (1)
2	03–07	Satellite number
3	08–08	Classification (U=Unclassified)
4	10–11	International Designator (Last two digits of launch year)
5	12–14	International Designator (Launch number of the year)
6	15–17	International Designator (piece of the launch)
7	19–20	Epoch Year (last two digits of year)
8	21–32	Epoch (day of the year and fractional portion of the day)
9	34–43	First Time Derivative of the Mean Motion divided by two
10	45–52	Second Time Derivative of Mean Motion divided by six (decimal point assumed)
11	54–61	BSTAR drag term (decimal point assumed)
12	63–63	The number 0 (originally this should have been "Ephemeris type")
13	65–68	Element set number. Incremented when a new TLE is generated for this object.
14	69–69	Checksum (modulo 10)

Table A.1-2: Second line of the ephemeris

Field	Columns	Content
1	01–01	Line number (2)
2	03–07	Satellite number
3	09–16	Inclination (degrees)
4	18–25	Right ascension of the ascending node (degrees)
5	27–33	Eccentricity (decimal point assumed)
6	35–42	Argument of perigee (degrees)
7	44–51	Mean Anomaly (degrees)
8	53–63	Mean Motion (revolutions per day)
9	64–68	Revolution number at epoch (revolutions)
10	69–69	Checksum (modulo 10)

The TLE format is an expression of mean orbital parameters "True Equator, Mean Equinox", filtering out short term perturbations.

From its TLE format data, the SGP4 (Simplified General Propagation) model [10] is used to calculate the location of the space object revolving about the earth in True Equator Mean Equinox (TEME) coordinate. Then it can be converted into the Earth-Centered, Earth-Fixed (ECEF) Cartesian x, y, z coordinate as a function of time.

The instantaneous velocity at that time can also be obtained. In ECEF coordinate, z-axis points to the true North, while x axis and y axis intersects 0-degrees latitude and longitude respectively as illustrated below.

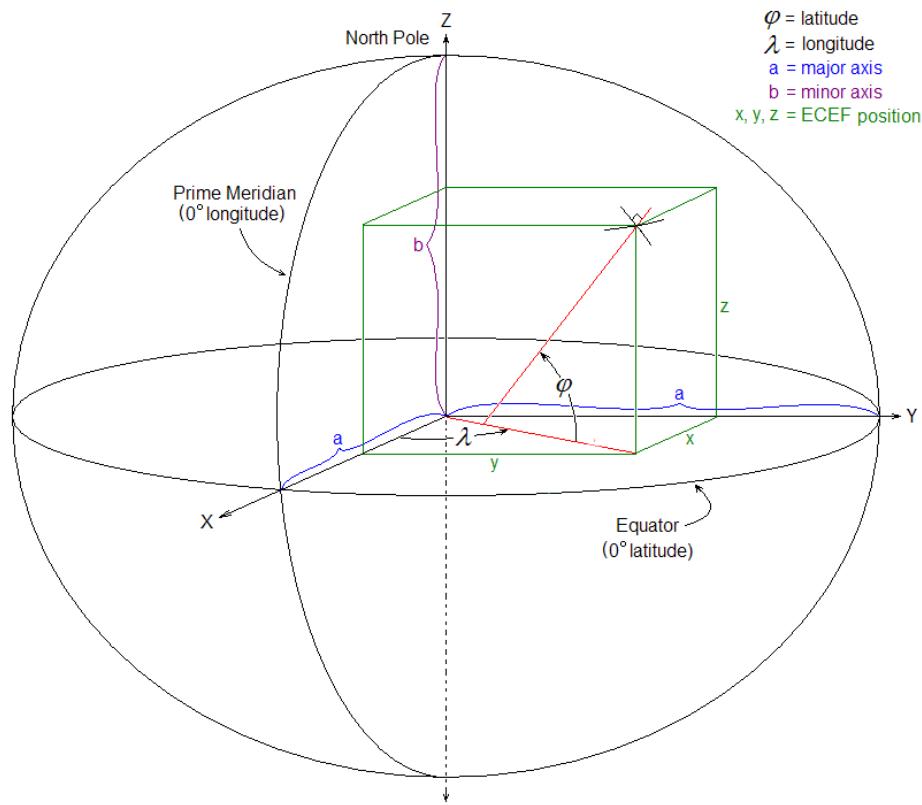


Figure A.1-1: Earth-Centered, Earth-Fixed (ECEF) coordinates in relation to latitude and longitude
 (source <https://en.wikipedia.org/wiki/ECEF>)

An example of ephemeris converted into ECEF format for the Telestar-19 satellite is shown below as an example below.

Epoch (day, hr, min, sec)	X[km]	Y[km]	Z[km]	dX/dt[km/s]	dY/dt[km/s]	dZ/dt [km/s]
2018-10-26 02:00:00.000	19151.529	-37578.251	17.682	-0.00151	-0.00102	-0.00106
2018-10-26 02:05:00.000	19151.073	-37578.556	17.359	-0.00152	-0.00101	-0.00109
2018-10-26 02:10:00.000	19150.614	-37578.855	17.029	-0.00154	-0.00099	-0.00112
2018-10-26 02:15:00.000	19150.150	-37579.151	16.690	-0.00155	-0.00098	-0.00114

Given a specific point in time, it is straightforward to calculate the satellite location by interpolation. The example given above refers to a geosynchronous (GEO) satellite, in which the epoch interval is 5 minutes. For LEO satellites, the intervals may be much shorter, on the order of seconds.

Annex B: KPI and evaluation assumptions

B.1 Key Performance Indicators

KPIs defined in TR38.913 are considered.

B.2 Performance targets for evaluation purposes

This table includes performance values that may be used for theoretical analysis or simulations.

The values relate to targeted performances, but should not be considered as strict requirements.

Table B.2-1: Non-Terrestrial network target performances per usage scenarios

Usage scenarios	Experience data rate (note 2)		Overall UE density per km2	Activity factor (note 3)	Max UE speed	Environment	UE categories	Sources
	DL	UL						
Pedestrian	2 Mbps	60 kbps	100	1,50%	3 km/h	Extreme coverage	Handheld	Data rate => see 7.10.1 "extreme coverage performance" in [13]; Activity factor: see table 6.1.6-1 "extreme rural" in [13]
Pedestrian 2	2 Mbps	250 kbps	100	1,50%	3 km/h	Extreme coverage	Handheld	NGMN (https://www.ngmn.org/) project on Extreme Long-Range Communications for Deep Rural Coverage
Vehicular connectivity	50 Mbps	25 Mbps	TBD	N.A.	250 km/h	Along roads in low population density areas	Vehicular mounted	data rate and activity factor in TS 22.261[12]
Stationary	50 Mbps	25 Mbps	TBD	N.A.	0 km/h	Extreme coverage	Building mounted	Data rate => assuming per end-user 50/25 Mbps data rate and an average of 5 end-user devices per stationary UE) rate and 20% activity factor per end-user device
Airplanes connectivity	360 Mbps	180 Mbps	TBD	N.A.	1 000 km/h	Open area	Airplane mounted	Data rate => assuming per end-user 15/7.5 Mbps data rate and 20% activity factor per end-user devices (See [12]); number of users per airplane: average aircraft size (assuming 120 users per plane)
IoT connectivity (note 4)	2 kbps	10 kbps	400	1,00%	0 km/h	Extreme coverage	IoT	Device density => [15] ; Data rate and activity factor => derived from [14] annex E.2 "Traffic models for Cellular IoT"
Public Safety	3.5 Mbps	3.5 Mbps	TBD	N.A	100 km/h	Open area	Handheld	Section 7.1 of TS 22.280 (To the extent feasible, it is expected that the end user's experience is similar regardless if the MCX Service is used with a 3GPP network or based on the use of a ProSe direct communication path. Covers pedestrian speed through medium vehicular speeds.)
Public Safety	3.5 Mbps	3.5 Mbps	TBD	N.A	250 km/h	Open area	Vehicle mounted	Section 7.1 of TS 22.280 (To the extent feasible, it is expected that the end user's experience is similar regardless if the MCX Service is used with a 3GPP network or based on the use of a ProSe direct communication path.)

NOTE 1: Void

NOTE 2: As defined in [12]

NOTE 3: As defined in [12]

NOTE 4: This refers to low power wide area service capability

NOTE 5: This does not preclude the definition of performance parameters for other usage scenarios in future stages

Signalling (control plane) and data (User plane) interruption time should be made as much as possible equivalent as in terrestrial systems except in the case of handover between satellite and terrestrial access. In the latter case, this interruption time will depend on the satellite orbit.

Annex C: Regulatory Aspects

In the ITU Radio Regulations (ITU, 2016) the interference to any GEO network caused by a NGSO system is strictly constrained. One restriction to the system is that a NGSO system shall not cause unacceptable interference into any GEO network in the fixed satellite service for uplink and downlink in the same frequency (in-line interference), shown in Figure C-1. For that reason, (ITU, 2016) limits the maximum equivalent power flux densities (EPFD) of the NGSO system to values which are not sufficient to enable satellite communication.

This document will focus on both the service uplink from the UE to the NGSO system (interfering the receiver on board of a GEO satellite) and the service downlink from the NGSO system to the UE (interfering a GEO receive station on earth).

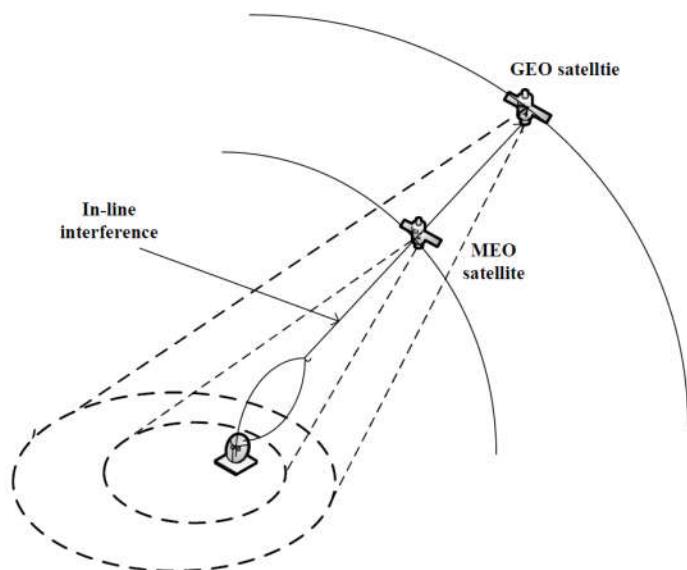


Figure C-1: In-line interference caused by NGSO systems (MEO or LEO)

Service uplink from UE to NGSO satellite:

Satellite specific user terminals are partly equipped with a dish antenna to reach high signal gains, due to its high directivity. Especially for frequencies in the FR2 and the use of satellite specific user terminals on ground with high directive antennas the problem of in-line interference arises for the service uplink in satellite system.

We look at a scenario in which the UE uses a directive antenna to communicate with a NGSO satellite. It may further be able to track the movement of the NGSO satellite with its antenna. Given the high directivity it is possible that the UE will glare a GEO satellite that is located in the same direction as the NGSO from the UE's perspective. As the uplink transmission power could exceed the ITU regulatory constraints for in-line interference of the protected GEO satellites, this issue has to be addressed already in the initial and random access phase. In the following we assume that the UE is aware of its position as well as the network.

The problem with a heavy deployment of NGSO systems arises with so-called in-line interference. This type of interference occurs, whenever a NGSO satellite crosses the line of sight path of an Earth station and a GEO satellite as depicted in Figure C-1.

To avoid that the cell of the NGSO satellite has to be switched off completely, only the UE's with highly directive antennas, which are pointing towards the GEO satellite should be disabled or hand over to other NGSO satellites.

Service downlink from NGSO satellite to UE:

In this case, the downlink signal from a NGSO satellite is interfering a GEO receive station on earth. The satellite beam pointing towards the GEO ground station has either to be steered to another direction or has to be switched off completely. The GEO receive station especially for FR2 are already deployed and protected by ITU regulations.

As a conclusion, in-line interference between NGSO and GSO satellite systems might occur especially when highly directive antennas are used in NTN scenarios and solutions to comply with the ITU regulatory constraints for in-line interference shall be specified for both uplink and downlink.

Annex D (Informative): Change history

Change history							
Date	Meeting	TDoc	CR	Rev	Cat	Subject/Comment	New version
2018-08	RAN3#101	R3-185304				Skeleton TR	0.0.0
2018-08	RAN3#101	R3-185333				Agreed version including pCRs of R3-184522, R3-185235, R3-185310	0.1.0
2018-10	RAN3#101 bis, RAN2#103 bis	R3-186269				Agreed version including pCRs of R2-1815953, R3-186257, R3-186112, R3-186214	0.2.0
2018-11	RAN3#102 , RAN2#104	R3-187281				Agreed version including pCRs of R3-187113, R3-187193, R3-187195, R3-187196, R3-187273, R2-1816538, R2-1818514	0.3.0
2019-03	RAN3#103 , RAN2#105	R3-191167				Agreed version including pCRs of R2-1900564, R2-1902554, R3-191023, R3-191025, R3-191026, R3-191027, R3-191029, R3-191030, R3-191031, R3-191032, R3-191146	0.4.0
2019-04	RAN3#103 bis, RAN2#105 bis, RAN1#96bi s	R3-192186				Agreed version including pCRs of R2-1905297, R3-191276, R3-191631, R3-192103, R3-192110, R3-192111, R3-192113, R3-192115, R3-192170, R3-192169, R3-192119, R3-192171, R3-192121, R3-192117	0.5.0
2019-04	Post RAN3#103 bis	R3-192189				Removal of R3-192117 changes ¹ . Corrections of chapter 5 headers numbering. Corrections of chapter 8 headers numbering	0.6.0
2019-05	RAN3#104 , RAN2#106 , RAN1#97	R3-193293				Agreed version including pCRs of R3-192758, R3-193207, R3-193208, R3-193209, R3-193212, R3-193216, R3-193277, R3-193287, R3-192783, R3-193182, R3-193049, R3-193217, R3-193218, R2-1906302, R2-1907970, R2-1908243, R1-1907836	0.7.0
2019-09	RAN3#105 , RAN2#10 7, RAN1#98	R3-194796				Agreed version including Agreements of Chairman's notes of RAN1#98 as well as pCRs of R2-1910685, R2-1911748	0.8.0
2019-10	RAN3#105 bis,RAN2# 107bis, RAN1#98bi s	R3-196330				Agreed version including Agreements of Chairman's notes of RAN1#98bis as well as pCRs of R2-1913969, R2-1914055, R2-1914056, R2-1914069, R2-1914070, R2-1914194, R2-1914196, R2-1914198	0.9.0
2019-12	RAN3#106 , RAN2#10 8, RAN1#99	R3-197795				pCRs of R1-1913436, R1-1913455, R1-1913426, R1-1913402, R1-1913427, R1-1913260, R2-1914721, R2-1916376, R2-1916386, R2-1916392, R2-1916393, R2-1916396, R3-197002, R2-1916414, R2-1916415, R2-1916469, R2-1916351	0.10.0
2019-12	RAN#86	RP-192504				TR Submission to TSG RAN plenary for approval	1.0.0
2019-12	RAN#86	RP-193062				Corrections to TP implementation	1.1.0
2019-12	RAN#86					TR approved by TSG RAN plenary	16.0.0

¹ TDOC agreed unseen at RAN3#103bis but not uploaded on time during the meeting!