
SCRIMP

Release 1.1

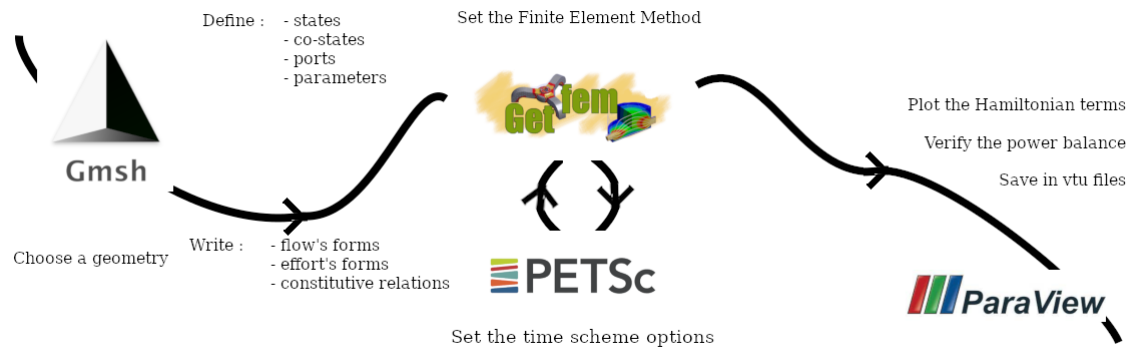
Giuseppe Ferraro, Michel Fournié, Ghislain Haine

Jan 21, 2026

CONTENTS

1	What is SCRIMP?	3
1.1	Port-Hamiltonian systems	3
1.2	Coding philosophy	4
2	User's guide	5
2.1	How to install	5
2.2	Getting started	5
2.3	Examples	12
2.4	Notebooks	51
2.5	Graphical User Interface	52
2.6	Bibliography	52
2.7	Code documentation	55
3	Credits	57
3.1	Development	57
3.2	Funding	57
3.3	Third-party	57
3.4	How to cite SCRIMP?	57
	Python Module Index	59
	Index	61

Simulation and Control of Interactions in Multi-Physics



WHAT IS SCRIMP?

SCRIMP (Simulation and ContRol of Interactions in Multi-Physics) is a python collection, *namely* a package, of *methods* and *classes* for the structure-preserving discretization and simulation of multi-physics models, using the formalism of port-Hamiltonian systems (van der Schaft and Maschke (2002)).

SCRIMP aims at speeding the coding process of the **Partitioned Finite Element Method** on a wide range of (multi-)physical systems (Ferraro *et al.* (2024)), and scrimp and save time!

The documentation is [available in pdf](#).

1.1 Port-Hamiltonian systems

1.1.1 What are they?

Let us sketch a rough portrait of port-Hamiltonian systems as they are considered in **SCRIMP**.

Port-Hamiltonian systems constitute a strongly structured class of control systems with collocated observation. It relies on a functional form \mathcal{H} (the **Hamiltonian**), whose variables α_i are the **states** of the system. The **co-states** $M_i e_i := \delta_{\alpha_i} \mathcal{H}$ are defined as the variational derivative of the Hamiltonian with respect to the states, on the metric induced by the M_i matrices.

The dynamics is provided *via* trajectories belonging in a **Dirac** structure, which can be represented by two matrices (of operators) M symmetric and J skew-symmetric as

$$M \begin{pmatrix} \frac{d}{dt} \alpha_1(t) \\ \vdots \\ \frac{d}{dt} \alpha_k(t) \\ f_R(t) \\ -y_{exp}(t) \\ u_{imp}(t) \end{pmatrix} = J \begin{pmatrix} e_1(t) \\ \vdots \\ e_k(t) \\ e_R(t) \\ u_{exp}(t) \\ -y_{imp}(t) \end{pmatrix}$$

together with **constitutive relations**

$$M_i e_i(t) = \delta_{\alpha_i(t)} \mathcal{H}(\alpha_1(t), \dots, \alpha_k(t)) \quad \mathcal{N}(t, f_R(t), e_R(t)) = 0$$

This structure allows to describe the evolution of the Hamiltonian along the trajectories

$$\frac{d}{dt} \mathcal{H}(\alpha_1(t), \dots, \alpha_k(t)) = -e_R(t)^\top M_R f_R(t) + u_{exp}(t)^\top M_{exp} y_{exp}(t) + u_{imp}(t)^\top M_{imp} y_{imp}(t)$$

The first term of the right-hand side stands for a loss of *energy*, hence the name of *resistive (or dissipative) port* for the couple (f_R, e_R) . The other two terms stands for exchanges with the environment through the *control ports*. One is *explicit*, u_{exp} , as a usual forcing term in the equations (its collocated output y_{exp} plays no role in the dynamics). The other is *implicit*: u_{imp} does not appear directly in the dynamics, and its collocated output y_{imp} plays the role of the Lagrange multiplier imposing the value of u_{imp} .

Each indexed matrix M_ℓ is the appropriate sub-matrix of M .

A very important and useful fact is that the matrices M and J can depend on time and states!

1.1.2 The Partitioned Finite Element Method

The main objective of a **structure-preserving discretization** in the port-Hamiltonian formalism is to obtain a discrete version of the power balance satisfied by the Hamiltonian functional.

A recent scheme, known as the **Partitioned Finite Element Method** (PFEM) (Cardoso-Ribeiro *et al.* (2021)), achieves this goal.

The strategy follows three steps, inspired by the Mixed Finite Element Method for steady-state problem with homogeneous boundary condition

- write the weak form of the system;
- integrate by parts a **partition** of the state (such that *the control appears*); and
- project on finite element spaces.

1.2 Coding philosophy

SCRIMP assumes that the final user is not familiar with numerical simulations. The aim is to facilitate the first step from modelisation to simulation by sticking as much as possible to the port-Hamiltonian framework, getting rid of coding issues.

As such, these simplifications naturally imply a lack of optimization of the code. Nevertheless, the syntax of **SCRIMP** try to let confirmed users to reach finer tuning in order to perform more sophisticated simulations.

A basic usage of **SCRIMP** consists in a script with the following steps:

- Define a *domain*
- Define at least one *state*. And of course, its *co-state*, in order to get a *dynamical port*
- Define a Finite Element Method on this port: give at least an order, at first glance, default values are sufficient
- Define *algebraic ports* (not mandatory) and its FEM
- Define *control ports* (not mandatory) and its FEM
- Define *parameters*
- Write down the forms on the *flow side* of the Dirac structure, *i.e.* the **brick** defining the matrix M
- Write down the forms on the *effort side* of the Dirac structure, *i.e.* the **brick** defining the matrix J
- Write down all the forms defining the *constitutive relations*, always with **bricks**
- Set up time scheme options: again, at first glance, default values are sufficient
- Solve
- Plot
- Export

We try to eliminate as much as possible the *computer-side* of the simulations, by following the port-Hamiltonian vocabulary, always by keeping the possibility of fine tuning available.

USER'S GUIDE

2.1 How to install

2.1.1 Anaconda

The easiest way to install SCRIMP is to use a conda environment.

1. Install [Anaconda](#)
2. Clone the git repository: `git clone https://github.com/g-haine/scrmp`
3. Enter the folder: `cd scrmp`
4. Create the conda environment: `conda env create --file /path/to/scrmp/scrmp.yml`
5. Activate the environment: `conda activate scrmp`
6. Add scrmp to the PATH: `conda develop /path/to/scrmp/`
7. Finish with pip: `pip install -e .`

2.1.2 Tests

You may test your installation by running available examples in the `examples` folder.`

2.1.3 Code structure

SCRIMP is developed as a *package*: the `__init__.py` file of the `/path/to/scrmp/` folder is the root file. Each subdirectory is a sub-package of **SCRIMP**. Files are called *module* in this framework and may be called *via* the command **import**. For instance the module *linalg* gathering linear algebra functions of the *subpackage* *utils* can be imported with `import scrmp.utils.linalg`.

2.1.4 Documentation

You can find this documentation [here](#).

It is automatically built upon the code comments using sphinx.

See [Sphinx](#) for further informations.

2.2 Getting started

In order to start using **SCRIMP**, you have to work in the conda environment *scrmp* from the installation by running `conda activate scrmp`.

To understand the coding philosophy of **SCRIMP**, let us consider the 1D wave equation with Neumann boundary control as a first example

$$\left\{ \begin{array}{ll} \rho(x)\partial_{tt}^2 w(t, x) - \partial_x (T(x)\partial_x w(t, x)) &= 0, \quad t \geq 0, x \in (0, 1), \\ \partial_t w(0, x) &= v_0(x), \quad x \in (0, 1), \\ \partial_x w(0, x) &= s_0(x), \quad x \in (0, 1), \\ -T(0)\partial_x (w(t, 0)) &= u_L(t), \quad t \geq 0, \\ T(1)\partial_x (w(t, 1)) &= u_R(t), \quad t \geq 0, \end{array} \right.$$

where w denotes the deflection from the equilibrium position of a string, ρ is its mass density and T the Young's modulus. **Note** the minus sign on the control at the left end side, standing for the *outward normal* to the domain $(0, 1)$.

The physics giving this equation has to be restated in the port-Hamiltonian formalism first.

2.2.1 Port-Hamiltonian framework

Let $\alpha_q := \partial_x w$ denotes the *strain* and $\alpha_p := \rho \partial_t w$ the *linear momentum*. One can express the total mechanical energy lying in the system \mathcal{H} , the **Hamiltonian**, as

$$\mathcal{H}(t) = \mathcal{H}(\alpha_q(t, x), \alpha_p(t, x)) := \underbrace{\frac{1}{2} \int_0^1 \alpha_q(t, x) T(x) \alpha_q(t, x) dx}_{\text{Potential energy}} + \underbrace{\frac{1}{2} \int_0^1 \frac{\alpha_p(t, x)^2}{\rho(x)} dx}_{\text{Kinetic energy}}.$$

The variables α_q and α_p are known as the **state variables**, or in the present case since \mathcal{H} represents an energy, the **energy variables**.

Computing the **variational derivative** of \mathcal{H} with respect to these variables leads to the **co-state variables**, or in our case the **co-energy variables**, *i.e.*

$$e_q := \delta_{\alpha_q} \mathcal{H} = T \alpha_q, \quad e_p := \delta_{\alpha_p} \mathcal{H} = \frac{\alpha_p}{\rho},$$

that is the *stress* and the *velocity* respectively.

Newton's second law and Schwarz's lemma give the following dynamics

$$\begin{pmatrix} \partial_t \alpha_q \\ \partial_t \alpha_p \end{pmatrix} = \begin{bmatrix} 0 & \partial_x \\ \partial_x & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \end{pmatrix}.$$

Of course, trivial substitutions in this system would lead again to the initial string equation in second-order form. However, by keeping the system as is, an important structure appears. Indeed, the matrix of operators above is *formally* skew-symmetric. In other words, for all test functions f_q and f_p (compactly supported C^∞ functions), one has thanks to integration by parts

$$(f_q \ f_p) \begin{bmatrix} 0 & \partial_x \\ \partial_x & 0 \end{bmatrix} \begin{pmatrix} f_q \\ f_p \end{pmatrix} = 0.$$

Together with the boundary Neumann condition, and defining *collocated* Dirichlet observations, this defines a (Stokes-) **Dirac structure**, where solutions along time, *i.e. trajectories*, will belong.

The port-Hamiltonian system representing a (linear) vibrating string with Neumann boundary control and Dirichlet boundary observation then writes

$$\begin{pmatrix} \partial_t \alpha_q \\ \partial_t \alpha_p \end{pmatrix} = \begin{bmatrix} 0 & \partial_x \\ \partial_x & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \end{pmatrix}, \quad \left\{ \begin{array}{ll} -e_q(t, 0) &= u_L(t), \\ e_q(t, 1) &= u_R(t), \\ y_L(t) &= e_p(t, 0), \\ y_R(t) &= e_p(t, 1), \end{array} \right.$$

$$\begin{cases} e_q &= T\alpha_q, \\ e_p &= \frac{\alpha_p}{\rho}. \end{cases}$$

The two first blocks, giving in particular the dynamics, define the **Dirac structure** of the system. The third block is known as the **constitutive relations**, and is needed to ensure uniqueness of solutions.

The importance of the **Dirac structure** relies, in particular, in the fact that it encloses the **power balance** satisfied by the **Hamiltonian**. Indeed, along the trajectories, one has

$$\frac{d}{dt}\mathcal{H}(t) = \frac{d}{dt}\mathcal{H}(\alpha_q(t), \alpha_p(t)) = \underbrace{y_R(t)u_R(t)}_{\text{power flowing through the right}} + \underbrace{y_L(t)u_L(t)}_{\text{power flowing through the left}}.$$

In other words, the **Dirac structure** encodes the way the system communicates with its environment. In the present example, it says that the variation of the total mechanical energy is given by the power supplied to the system at the boundaries.

Each couple $(\partial_t \alpha_q, e_q)$, $(\partial_t \alpha_p, e_p)$, (u_L, y_L) and (u_R, y_R) is a **port** of the port-Hamiltonian system, and is associated to a physically meaningful term in the **power balance**.

2.2.2 Structure-preserving discretization

The objective of a structure-preserving discretization method is to obtain a **finite-dimensional Dirac structure** that encloses a *discrete version* of the power balance. There is several ways to achieve this goal, but **SCRIMP** focuses on a particular application of the Mixed Finite Element Method, called the **Partitioned Finite Element Method**.

Remark: The 1D case does simplify the difficulties coming from the boundary terms. Indeed, here the functional spaces for the controls u_L, u_R and the observations y_L, y_R are nothing but \mathbb{R} .

Let φ_q and φ_p be smooth test functions, and δ_{mx} denote the Kronecker symbol. One can write the weak formulation of the **Dirac Structure** as follows

$$\begin{cases} \int_0^1 \partial_t \alpha_q(t, x) \varphi_q(x) dx &= \int_0^1 \partial_x e_p(t, x) \varphi_q(x) dx, \\ \int_0^1 \partial_t \alpha_p(t, x) \varphi_p(x) dx &= \int_0^1 \partial_x e_q(t, x) \varphi_p(x) dx, \\ y_L(t) &= \delta_{0x} e_p(t, x), \\ y_R(t) &= \delta_{1x} e_p(t, x). \end{cases}$$

Integrating by parts the second line make the controls appear

$$\begin{cases} \int_0^1 \partial_t \alpha_q(t, x) \varphi_q(x) dx &= \int_0^1 \partial_x e_p(t, x) \varphi_q(x) dx, \\ \int_0^1 \partial_t \alpha_p(t, x) \varphi_p(x) dx &= - \int_0^1 e_q(t, x) \partial_x \varphi_p(x) dx + u_R(t) \varphi_p(1) + u_L(t) \varphi_p(0), \\ y_L(t) &= \delta_{0x} e_p(t, x), \\ y_R(t) &= \delta_{1x} e_p(t, x). \end{cases}$$

Now, let $(\varphi_q^i)_{1 \leq i \leq N_q}$ and $(\varphi_p^k)_{1 \leq k \leq N_p}$ be two finite families of approximations for the q -type port and the p -type port respectively, typically finite element families, and write the discrete weak formulation with those families, one has for all $1 \leq i \leq N_q$ and all $1 \leq k \leq N_p$

$$\begin{cases} \sum_{j=1}^{N_q} \int_0^1 \varphi_q^j(x) \varphi_q^i(x) dx \frac{d}{dt} \alpha_q^j(t) &= \sum_{\ell=1}^{N_p} \int_0^1 \partial_x \varphi_p^\ell(x) \varphi_q^i(x) dx e_p^\ell(t), \\ \sum_{\ell=1}^{N_p} \int_0^1 \varphi_p^\ell(x) \varphi_p^k(x) dx \frac{d}{dt} \alpha_p^\ell(t) &= - \sum_{j=1}^{N_q} \int_0^1 \varphi_q^j(x) \partial_x \varphi_p^k(x) dx e_q^j(t) \\ &\quad + u_R(t) \varphi_p^k(1) + u_L(t) \varphi_p^k(0), \\ y_L(t) &= \sum_{\ell=1}^{N_p} \varphi_p^\ell(0) e_p^\ell(t), \\ y_R(t) &= \sum_{\ell=1}^{N_p} \varphi_p^\ell(1) e_p^\ell(t), \end{cases}$$

which rewrites in matrix form

$$\underbrace{\begin{bmatrix} M_q & 0 & 0 & 0 \\ 0 & M_p & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}}_{=M} \underbrace{\begin{pmatrix} \frac{d}{dt} \alpha_q(t) \\ \frac{d}{dt} \alpha_p(t) \\ -y_L(t) \\ -y_R(t) \end{pmatrix}}_{=J} = \underbrace{\begin{bmatrix} 0 & D & 0 & 0 \\ -D^\top & 0 & B_L & B_R \\ 0 & -B_L^\top & 0 & 0 \\ 0 & -B_R^\top & 0 & 0 \end{bmatrix}}_{=J} \underbrace{\begin{pmatrix} e_q(t) \\ e_p(t) \\ u_L(t) \\ u_R(t) \end{pmatrix}}_{=J},$$

where $\underline{\alpha}_*(t) := (\alpha_*^1(t) \ \cdots \ \alpha_*^{N_*}(t))^\top$, $\underline{e}_*(t) := (e_*^1(t) \ \cdots \ e_*^{N_*}(t))^\top$, and

$$(M_q)_{ij} := \int_0^1 \varphi_q^j(x) \varphi_q^i(x) dx, \quad (M_p)_{k\ell} := \int_0^1 \varphi_p^\ell(x) \varphi_p^k(x) dx,$$

$$(D)_{i\ell} := \int_0^1 \partial_x \varphi_p^\ell(x) \varphi_q^i(x) dx, \quad (B_L)_k := \varphi_p^k(0), \quad (B_R)_k := \varphi_p^k(1).$$

Abusing the language, the left-hand side will be called the **flow** of the **Dirac structure** in **SCRIMP**, while the right-hand side will be called the **effort**.

Now one can approximate the **constitutive relations** in those families by projection of their weak formulations

$$\begin{cases} \int_0^1 e_q(t, x) \varphi_q(x) dx &= \int_0^1 T(x) \alpha_q(t, x) \varphi_q(x) dx, \\ \int_0^1 e_p(t, x) \varphi_p(x) dx &= \int_0^1 \frac{\alpha_p(t, x)}{\rho(x)} \varphi_p(x) dx, \end{cases}$$

from which one can deduce the matrix form of the discrete weak formulation of the constitutive relation

$$\begin{cases} M_q \underline{e}_q(t) &= M_T \underline{\alpha}_q(t), \\ M_p \underline{e}_p(t) &= M_\rho \underline{\alpha}_p(t), \end{cases}$$

where

$$(M_T)_{ij} := \int_0^1 T(x) \varphi_q^j(x) \varphi_q^i(x) dx, \quad (M_\rho)_{k\ell} := \int_0^1 \frac{\varphi_p^\ell(x)}{\rho(x)} \varphi_p^k(x) dx.$$

Finally, the **discrete Hamiltonian** \mathcal{H}^d is defined as the evaluation of \mathcal{H} on the approximation of the **state variables**

$$\mathcal{H}^d(t) := \mathcal{H}(\alpha_q^d(t, x), \alpha_p^d(t)) = \frac{1}{2} \underline{\alpha}_q(t)^\top M_T \underline{\alpha}_q(t) + \frac{1}{2} \underline{\alpha}_p(t)^\top M_\rho \underline{\alpha}_p(t).$$

The **discrete power balance** is then easily deduced from the above matrix formulations, thanks to the symmetry of M and the skew-symmetry of J

$$\frac{d}{dt} \mathcal{H}^d(t) = y_R(t) u_R(t) + y_L(t) u_L(t).$$

Remark: The discrete system that has to be solved numerically is a Differential Algebraic Equation (DAE). There exists some case (as in this example), where one can write the **co-state** formulation of the system by substituting the **constitutive relations** at the continuous level to get a more classical Ordinary Differential Equation (ODE)

$$\begin{bmatrix} \widetilde{M}_q & 0 & 0 & 0 \\ 0 & \widetilde{M}_p & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{pmatrix} \frac{d}{dt} \underline{e}_q(t) \\ \frac{d}{dt} \underline{e}_p(t) \\ -y_L(t) \\ -y_R(t) \end{pmatrix} = \begin{bmatrix} 0 & D & 0 & 0 \\ -D^\top & 0 & B_L & B_R \\ 0 & -B_L^\top & 0 & 0 \\ 0 & -B_R^\top & 0 & 0 \end{bmatrix} \begin{pmatrix} \underline{e}_q(t) \\ \underline{e}_p(t) \\ u_L(t) \\ u_R(t) \end{pmatrix},$$

where this time the mass matrices on the left-hand side are both *weighted* with respect to the physical parameters

$$(\widetilde{M}_q)_{ij} := \int_0^1 T^{-1}(x) \varphi_q^j(x) \varphi_q^i(x) dx, \quad (\widetilde{M}_p)_{k\ell} := \int_0^1 \rho(x) \varphi_p^\ell(x) \varphi_p^k(x) dx.$$

2.2.3 Schema-first workflow

SCRIMP now ships with a declarative configuration system based on YAML/JSON schemas. You can generate a starting template from the command line:

```
python -m scrip.io.schema_loader generate rectangle --output rectangle.yml
```

The resulting file contains domain, integration, FEM and material definitions that are validated with Pydantic. Loading the schema in Python replaces the imperative setup phase:

```
import scrip as S
from scrip.io.schema_loader import load_schema

schema = load_schema("rectangle.yml")
wave = S.DPHS("real")
wave.set_domain(S.Domain(schema.domain))

displacement = S.FEM(schema.fem.fields[0])
wave.add_FEM(displacement)
```

The remainder of this tutorial keeps the imperative snippets for clarity, but every call can be substituted by schema-driven objects when working on larger scenarios.

2.2.4 Coding within SCRIMP

The following code is available in the file `wave_1D.py` of the *sandbox* folder of scrip.

To start, import **SCRIMP** and create a *distributed port-Hamiltonian system* (DPHS) called, *e.g.*, `wave`

```
import scrip as S

wave = S.DPHS("real")
```

Then, define the domain $\Omega = (0, 1)$, with a mesh-size parameter h , and add it to the *DPHS*

```
domain = S.Domain("Interval", {"L": 1., "h": 0.01})
wave.set_domain(domain)
```

This creates a mesh of the interval $\Omega = (0, 1)$.

Important to keep in mind: the domain is composed of regions, denoted by integers. The *built-in* geometry of an interval available in the code returns 1 for the domain Ω , 10 for the left-end and 11 for the right-end. Informations about available geometries and the indices of their regions can be found in the documentation or *via* the function `built_in_geometries()` available in `scrip.utils.mesh`.

On this domain, we define two **states** and add them to the *DPHS*

```
alpha_q = S.State("q", "Strain", "scalar-field")
alpha_p = S.State("p", "Linear momentum", "scalar-field")
wave.add_state(alpha_q)
wave.add_state(alpha_p)
```

and the two associated **co-states**

```
e_q = S.CoState("e_q", "Stress", alpha_q)
e_p = S.CoState("e_p", "Velocity", alpha_p)
wave.add_costate(e_q)
wave.add_costate(e_p)
```

These latter calls create automatically two *non-algebraic ports*, named after their respective **state**. Note that we simplify the notations and do not write `alpha_q` and `alpha_p` but `q` and `p` for the sake of readability.

Finally, we create and add the two control-observation **ports** with

```
left_end = S.Control_Port("Boundary control (left)", "U_L", "Normal force", "Y_L",
    ↪ "Velocity", "scalar-field", region=10)
right_end = S.Control_Port("Boundary control (right)", "U_R", "Normal force", "Y_R",
    ↪ "Velocity", "scalar-field", region=11)
wave.add_control_port(left_end)
wave.add_control_port(right_end)
```

Note the *crucial* keyword **region** to restrict each port to its end. By default, it would apply everywhere.

Syntactic note: although y is the observation in the theory of port-Hamiltonian systems, it is also the second space variable for N-D problems. This name is thus reserved for this latter aim and forbidden in all definitions of a *DPHS*. Nevertheless, the code being case-sensitive, it is possible to name the observation Y . To avoid mistakes, we take the habit to always use this syntax, this is why we denoted our controls and observations with capital letters even if the problem does not occur in this 1D example.

To be able to write the discrete weak formulation of the system, one need to set four finite element families, associated to each **port**. Only two arguments are mandatory: the *name* of the port and the *degree* of the approximations.

```
V_q = S.FEM("q", 2)
V_p = S.FEM("p", 1)
V_L = S.FEM("Boundary control (left)", 1)
V_R = S.FEM("Boundary control (right)", 1)
```

This will construct a family of Lagrange finite elements (default choice) for each port, with the prescribed order. Remember that the boundary is only 2 disconnected points in this 1D case, so the only possibility for the finite element is 1 degree of freedom on each of them: Lagrange elements of order 1 is the easy way to do that.

Of course, this *FEM* must be added to the *DPHS*

```
wave.add_FEM(V_q)
wave.add_FEM(V_p)
wave.add_FEM(V_L)
wave.add_FEM(V_R)
```

Finally, the physical parameters of the experiment have to be defined. In **SCRIMP**, a *parameter* is associated to a *port*.

```
T = S.Parameter("T", "Young's modulus", "scalar-field", "1", "q")
rho = S.Parameter("rho", "Mass density", "scalar-field", "1 + x*(1-x)", "p")
wave.add_parameter(T)
wave.add_parameter(rho)
```

The first argument will be **the string that can be used in forms**, the second argument is a human-readable description, the third one set the kind of the parameter, the fourth one is the mathematical expression defining the parameter, and finally the fifth argument is the *name* of the associated port.

It is now possible to write the weak forms defining the system. *Only the non-zero blocks* are mandatory. Furthermore, the place of the block is automatically determined by GetFEM. The syntax follow a simple rule: the unknown trial function q is automatically associated to the test function Test_q (note the capital T on Test), and so on.

Like we did for each call, the first step is to create the object, then to add it to the *DPHS*. As there is a lot of *bricks*, let us make a loop using a python *list*

```
bricks = [
    # M matrix, on the flow side
    S.Brick("M_q", "q * Test_q", [1], dt=True, position="flow"),
```

(continues on next page)

(continued from previous page)

```

S.Brick("M_p", "p * Test_p", [1], dt=True, position="flow"),
S.Brick("M_Y_L", "Y_L * Test_Y_L", [10], position="flow"),
S.Brick("M_Y_R", "Y_R * Test_Y_R", [11], position="flow"),

# J matrix, on the effort side
S.Brick("D", "Grad(e_p) * Test_q", [1], position="effort"),

S.Brick("-D^T", "-e_q * Grad(Test_p)", [1], position="effort"),
S.Brick("B_L", "-U_L * Test_p", [10], position="effort"),
S.Brick("B_R", "U_R * Test_p", [11], position="effort"),

S.Brick("-B_L^T", "e_p * Test_Y_L", [10], position="effort"),
S.Brick("-B_R^T", "-e_p * Test_Y_R", [11], position="effort"),

# Constitutive relations
S.Brick("-M_e_q", "-e_q * Test_e_q", [1]),
S.Brick("CR_q", "q*T * Test_e_q", [1]),

S.Brick("-M_e_p", "-e_p * Test_e_p", [1]),
S.Brick("CR_p", "p/rho * Test_e_p", [1]),
]

for brick in bricks:
    wave.add_brick(brick)

```

The first argument of a *brick* is a human-readable name, the second one is the form, the third is a list (hence the [and]) of integers, listing all the regions where the form applies. The optional parameter `dt=True` is to inform **SCRIMP** that this block matrix will apply on the time-derivative of the unknown trial function, and finally the option parameter `position="flow"` informs **SCRIMP** that this block is a part of the *flow side* of the Dirac structure, `position="effort"` do the same for the *effort side*, and without this keyword, **SCRIMP** places the *brick* as part of the *constitutive relations*.

Syntactic note: the constitutive relations have to be written under an implicit formulation $F = 0$. Keep in mind that a minus sign will often appear because of that.

The port-Hamiltonian system is now fully stated. It remains to set the controls and the initial values of the states before solving

```

expression_left = "-sin(2*pi*t)"
expression_right = "0."
wave.set_control("Boundary control (left)", expression_left)
wave.set_control("Boundary control (right)", expression_right)

q_init = "2.*np.exp(-50.*(x-0.5)*(x-0.5))"
p_init = "0."
wave.set_initial_value("q", q_init)
wave.set_initial_value("p", p_init)

```

We can now solve the system (with default experiment parameters)

```

wave.solve()

```

To end, one can also add the Hamiltonian terms and plot the contribution of each port to the balance equation

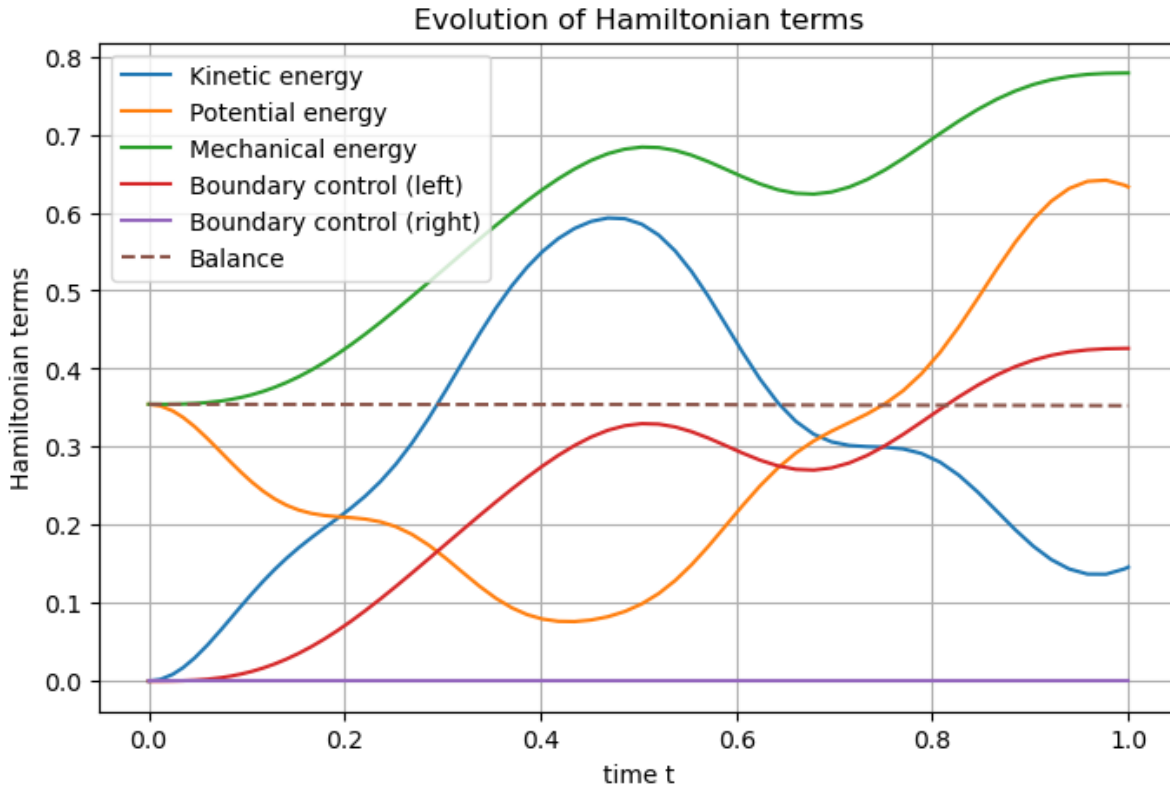
```

wave.hamiltonian.set_name("Mechanical energy")
terms = [
    S.Term("Kinetic energy", "0.5*p*p/rho", [1]),
    S.Term("Potential energy", "0.5*q*T*q", [1]),
]

for term in terms:
    wave.hamiltonian.add_term(term)

wave.plot_Hamiltonian()

```



One can appreciate the *structure-preserving* property by looking at the dashed line, showing the evolution of

$$\mathcal{H}^d(t) - \int_0^t u_R(s)y_R(s)ds - \int_0^t u_L(s)y_L(s)ds.$$

And now? It is time to see [more examples](#).

2.3 Examples

We provide some examples coming from our [publications](#).

2.3.1 The wave equation

Setting

Let us consider the 2D wave equation with *mixed* boundary controls on a bounded rectangle $\Omega := (0, L) \times (0, \ell)$, with boundaries $\Gamma_N := ((0, L) \times \{0, \ell\}) \cup (\{L\} \times (0, \ell))$ and $\Gamma_D := \{0\} \times (0, \ell)$.

The deflection of the membrane from the equilibrium w satisfies classically

$$\left\{ \begin{array}{ll} \rho(x) \partial_{tt}^2 w(t, x) - \operatorname{div} (T(x) \cdot \operatorname{grad} (w(t, x))) &= 0, \quad t \geq 0, x \in \Omega, \\ \partial_t w(0, x) &= v_0(x), \quad x \in \Omega, \\ \partial_x w(0, x) &= s_0(x), \quad x \in \Omega, \\ T(s) \cdot \operatorname{grad} (w(t, s)) &= u_N(t, s), \quad t \geq 0, s \in \Gamma_N, \\ \partial_t w(t, s) &= u_D(t, s), \quad t \geq 0, s \in \Gamma_D, \end{array} \right.$$

where ρ is the mass density and T the Young's modulus. The subscript N stands for **Neumann**, while the subscript D stands for **Dirichlet** (to be fair, this is not really a Dirichlet boundary condition, as it imposes $\partial_t w$ and not w at the boundary Γ_D).

Let us state the physics in the port-Hamiltonian formalism.

Port-Hamiltonian framework

Let $\alpha_q := \operatorname{grad} w$ denotes the *strain* and $\alpha_p := \rho \partial_t w$ the *linear momentum*. One can express the total mechanical energy lying in the system \mathcal{H} , the **Hamiltonian**, as

$$\mathcal{H}(t) = \mathcal{H}(\alpha_q(t, x), \alpha_p(t, x)) := \underbrace{\frac{1}{2} \int_{\Omega} \alpha_q(t, x) \cdot T(x) \cdot \alpha_q(t, x) dx}_{\text{Potential energy}} + \underbrace{\frac{1}{2} \int_{\Omega} \frac{\alpha_p(t, x)^2}{\rho(x)} dx}_{\text{Kinetic energy}}.$$

The **co-energy variables** are, as in the 1D case

$$e_q := \delta_{\alpha_q} \mathcal{H} = T \cdot \alpha_q, \quad e_p := \delta_{\alpha_p} \mathcal{H} = \frac{\alpha_p}{\rho},$$

that is the *stress* and the *velocity* respectively.

Newton's second law and Schwarz's lemma give the following dynamics

$$\begin{pmatrix} \partial_t \alpha_q \\ \partial_t \alpha_p \end{pmatrix} = \begin{bmatrix} 0 & \operatorname{grad} \\ \operatorname{div} & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \end{pmatrix}.$$

Of course, this system allows to recover the initial wave equation in second-order form.

The port-Hamiltonian system representing a (linear) vibrating membrane with mixed boundary controls then writes

$$\begin{aligned} \begin{pmatrix} \partial_t \alpha_q \\ \partial_t \alpha_p \end{pmatrix} &= \begin{bmatrix} 0 & \operatorname{grad} \\ \operatorname{div} & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \end{pmatrix}, \\ \left\{ \begin{array}{ll} e_q(t, s) &= u_N(t, s), \quad t \geq 0, s \in \Gamma_N, \\ e_p(t, s) &= u_D(t, s), \quad t \geq 0, s \in \Gamma_D, \\ y_N(t, s) &= e_p(t, s), \quad t \geq 0, s \in \Gamma_N, \\ y_D(t, s) &= e_q(t, s), \quad t \geq 0, s \in \Gamma_D, \end{array} \right. \\ \left\{ \begin{array}{ll} e_q &= T \cdot \alpha_q, \\ e_p &= \frac{\alpha_p}{\rho}. \end{array} \right. \end{aligned}$$

The **power balance** satisfied by the **Hamiltonian** is

$$\frac{d}{dt} \mathcal{H}(t) = \underbrace{\langle y_N(t, \cdot), u_N(t, \cdot) \rangle_{\Gamma_N}}_{\text{power flowing through } \Gamma_N} + \underbrace{\langle u_D(t, \cdot), y_D(t, \cdot) \rangle_{\Gamma_D}}_{\text{power flowing through } \Gamma_D},$$

where $\langle \cdot, \cdot \rangle_{\Gamma}$ is a boundary duality bracket $H^{\frac{1}{2}}, H^{-\frac{1}{2}}$ at the boundary Γ .

Structure-preserving discretization

Let φ_q and φ_p be smooth test functions on Ω , and ψ_N and ψ_D be smooth test functions on Γ_N and Γ_D respectively. One can write the weak formulation of the **Dirac Structure** as follows

$$\begin{cases} \int_{\Omega} \partial_t \alpha_q(t, x) \varphi_q(x) dx &= \int_{\Omega} \text{grad}(e_p(t, x)) \cdot \varphi_q(x) dx, \\ \int_{\Omega} \partial_t \alpha_p(t, x) \varphi_p(x) dx &= \int_{\Omega} \text{div}(e_q(t, x)) \varphi_p(x) dx, \\ \langle y_N, \psi_N \rangle_{\Gamma_N} &= \langle e_p, \psi_N \rangle_{\Gamma_N}, \\ \langle u_D, \psi_D \rangle_{\Gamma_D} &= \langle e_p, \psi_D \rangle_{\Gamma_D}. \end{cases} \quad (2.1)$$

Integrating by parts the second line make the control u_N and the observation y_D appear

$$\int_{\Omega} \partial_t \alpha_p(t, x) \varphi_p(x) dx = - \int_{\Omega} e_q(t, x) \cdot \text{grad}(\varphi_p(x)) dx + \langle \varphi_p, u_N \rangle_{\Gamma_N} + \langle \varphi_p, y_D \rangle_{\Gamma_D}.$$

Now, let $(\varphi_q^i)_{1 \leq i \leq N_q} \subset L^2(\Omega)$ and $(\varphi_p^k)_{1 \leq k \leq N_p} \subset H^1(\Omega)$ be two finite families of approximations for the q -type port and the p -type port respectively, typically discontinuous and continuous Galerkin finite elements respectively. Denote also $(\psi_N^m)_{1 \leq m_N \leq N_N} \subset H^{\frac{1}{2}}(\Gamma_N)$ and $(\psi_D^m)_{1 \leq m_D \leq N_D} \subset H^{\frac{1}{2}}(\Gamma_D)$. In particular, the latter choices imply that the duality brackets at the boundary reduce to simple L^2 scalar products.

Writing the discrete weak formulation with those families, one has for all $1 \leq i \leq N_q$, all $1 \leq k \leq N_p$, all $1 \leq m_N \leq N_N$ and all $1 \leq m_D \leq N_D$

$$\begin{cases} \sum_{j=1}^{N_q} \int_{\Omega} \varphi_q^j(x) \varphi_q^i(x) dx \frac{d}{dt} \alpha_q^j(t) &= \sum_{\ell=1}^{N_p} \int_{\Omega} \text{grad}(\varphi_p^{\ell}(x)) \cdot \varphi_q^i(x) dx e_p^{\ell}(t), \\ \sum_{\ell=1}^{N_p} \int_{\Omega} \varphi_p^{\ell}(x) \varphi_p^k(x) dx \frac{d}{dt} \alpha_p^{\ell}(t) &= - \sum_{j=1}^{N_q} \int_{\Omega} \varphi_q^j(x) \cdot \text{grad}(\varphi_p^k(x)) dx e_q^j(t) \\ &\quad + \sum_{n_N=1}^{N_N} \int_{\Gamma_N} \varphi_p^k(s) \psi_N^{n_N}(s) ds u_N^{n_N}(t) \\ &\quad + \sum_{n_D=1}^{N_D} \int_{\Gamma_D} \varphi_p^k(s) \psi_D^{n_D}(s) ds y_D^{n_D}(t), \\ \sum_{n_N=1}^{N_N} \langle \psi_N^{n_N}, \psi_N^{m_N} \rangle_{\Gamma_N} y_N^{n_N}(t) &= \sum_{\ell=1}^{N_p} \int_{\Gamma_N} \varphi_p^{\ell}(s) \psi_N^{m_N}(s) ds e_p^{\ell}(t), \\ \sum_{n_D=1}^{N_D} \langle \psi_D^{n_D}, \psi_D^{m_D} \rangle_{\Gamma_D} u_D^{n_D}(t) &= \sum_{\ell=1}^{N_p} \int_{\Gamma_D} \varphi_p^{\ell}(s) \psi_D^{m_D}(s) ds e_p^{\ell}(t), \end{cases} \quad (2.2)$$

which rewrites in matrix form

$$\underbrace{\begin{bmatrix} M_q & 0 & 0 & 0 \\ 0 & M_p & 0 & 0 \\ 0 & 0 & M_N & 0 \\ 0 & 0 & 0 & M_D \end{bmatrix}}_{=M} \begin{pmatrix} \frac{d}{dt} \underline{\alpha}_q(t) \\ \frac{d}{dt} \underline{\alpha}_p(t) \\ -\underline{y}_N(t) \\ \underline{u}_D(t) \end{pmatrix} = \underbrace{\begin{bmatrix} 0 & D & 0 & 0 \\ -D^{\top} & 0 & B_N & -B_D^{\top} \\ 0 & -B_N^{\top} & 0 & 0 \\ 0 & B_D & 0 & 0 \end{bmatrix}}_{=J} \begin{pmatrix} \underline{e}_q(t) \\ \underline{e}_p(t) \\ \underline{u}_N(t) \\ -\underline{y}_D(t) \end{pmatrix},$$

where $\star(t) := (\star^1(t) \ \dots \ \star^{N_{\star}})^{\top}$ and

$$(M_q)_{ij} := \int_{\Omega} \varphi_q^j(x) \cdot \varphi_q^i(x) dx, \quad (M_p)_{k\ell} := \int_{\Omega} \varphi_p^{\ell}(x) \varphi_p^k(x) dx, \quad (2.3)$$

$$(M_N)_{m_N n_N} := \int_{\Gamma_N} \psi_N^{n_N}(s) \psi_N^{m_N}(s) ds, \quad (M_D)_{m_D n_D} := \int_{\Gamma_D} \psi_D^{n_D}(s) \psi_D^{m_D}(s) ds, \quad (2.4)$$

$$(D)_{i\ell} := \int_{\Omega} \text{grad}(\varphi_p^{\ell}(x)) \cdot \varphi_q^i(x) dx,$$

$$(B_N)_{n_N k} := \int_{\Gamma_N} \varphi_p^k(s) \psi_N^{n_N}(s) ds, \quad (B_D)_{m_D \ell} := \int_{\Gamma_D} \varphi_p^{\ell}(s) \psi_D^{m_D}(s) ds,$$

Now one can approximate the **constitutive relations** in those families by projection of their weak formulations

$$\begin{cases} \int_{\Omega} e_q(t, x) \cdot \varphi_q(x) dx &= \int_{\Omega} \alpha_q(t, x) \cdot T(x) \cdot \varphi_q(x) dx, \\ \int_{\Omega} e_p(t, x) \varphi_p(x) dx &= \int_{\Omega} \frac{\alpha_p(t, x)}{\rho(x)} \varphi_p(x) dx, \end{cases}$$

from which one can deduce the matrix form of the discrete weak formulation of the constitutive relation

$$\begin{cases} M_q \underline{e}_q(t) &= M_T \underline{\alpha}_q(t), \\ M_p \underline{e}_p(t) &= M_\rho \underline{\alpha}_p(t), \end{cases}$$

where

$$(M_T)_{ij} := \int_{\Omega} \varphi_q^j(x) \cdot T(x) \cdot \varphi_q^i(x) dx, \quad (M_\rho)_{k\ell} := \int_{\Omega} \frac{\varphi_p^\ell(x)}{\rho(x)} \varphi_p^k(x) dx. \quad (2.5)$$

Finally, the **discrete Hamiltonian** \mathcal{H}^d is defined as the evaluation of \mathcal{H} on the approximation of the **state variables**

$$\mathcal{H}^d(t) := \mathcal{H}(\alpha_q^d(t, x), \alpha_p^d(t)) = \frac{1}{2} \underline{\alpha}_q(t)^\top M_T \underline{\alpha}_q(t) + \frac{1}{2} \underline{\alpha}_p(t)^\top M_\rho \underline{\alpha}_p(t).$$

The **discrete power balance** is then easily deduced from the above matrix formulations, thanks to the symmetry of M and the skew-symmetry of J

$$\frac{d}{dt} \mathcal{H}^d(t) = \underline{y}_N(t)^\top M_N \underline{u}_N(t) + \underline{u}_D(t)^\top M_D \underline{y}_D(t).$$

Simulation

Let us start by importing the scrimp package

```
# Import scrimp
import scrimp as S
```

Now define a real Distributed Port-Hamiltonian System

```
# Init the distributed port-Hamiltonian system
wave = S.DPHS("real")
```

The domain is 2-dimensional, and is a rectangle of length 2 and width 1. We use the built-in geometry `Rectangle` and choose a mesh size parameter of 0.1 with the following command.

```
# Set the domain (using the built-in geometry `Rectangle`)
# Labels: Omega = 1, Gamma_Bottom = 10, Gamma_Right = 11, Gamma_Top = 12, Gamma_Left = 13
rectangle = S.Domain("Rectangle", {"L": 2.0, "l": 1.0, "h": 0.1})

# And add it to the dphs
wave.set_domain(rectangle)
```

Defining the states and co-states, care must be taken: the Strain is a **vector-field**.

```
# Define the variables and their discretizations
states = [
    S.State("q", "Strain", "vector-field"),
    S.State("p", "Linear momentum", "scalar-field"),
]
costates = [
    S.CoState("e_q", "Stress", states[0]),
    S.CoState("e_p", "Velocity", states[1]),
]

# Add them to the dphs
```

(continues on next page)

(continued from previous page)

```

for state in states:
    wave.add_state(state)
for costate in costates:
    wave.add_costate(costate)

```

As the domain is the built-in geometry `Rectangle`, the boundary is composed of four parts, with indices 10, 11, 12 and 13, respectively for the lower, right, upper and left edge. Each of them will have its own control port, allowing *e.g.* **mixed** boundary conditions.

Indeed in the above example, we choose Neumann boundary condition on Γ_N , *i.e.* on 10, 11 and 12, while we choose Dirichlet boundary condition on Γ_D , *i.e.* on 13.

The choice to integrate by part the second line of (2.1) has a consequence for the port at boundary 13, as it is then in the *flow* part of the Dirac structure, as can be seen in (2.2). We indicate this using the keyword `position="flow"`.

```

# Define the control ports
control_ports = [
    S.Control_Port(
        "Boundary control (bottom)",
        "U_B",
        "Normal force",
        "Y_B",
        "Velocity trace",
        "scalar-field",
        region=10,
    ),
    S.Control_Port(
        "Boundary control (right)",
        "U_R",
        "Normal force",
        "Y_R",
        "Velocity trace",
        "scalar-field",
        region=11,
    ),
    S.Control_Port(
        "Boundary control (top)",
        "U_T",
        "Normal force",
        "Y_T",
        "Velocity trace",
        "scalar-field",
        region=12,
    ),
    S.Control_Port(
        "Boundary control (left)",
        "U_L",
        "Velocity trace",
        "Y_L",
        "Normal force",
        "scalar-field",
        region=13,
        position="flow",
    ),
]

```

(continues on next page)

(continued from previous page)

```

    ),
]

# Add them to the dphs
for ctrl_port in control_ports:
    wave.add_control_port(ctrl_port)

```

The choice for the finite element families is often the first difficulty of a simulation. Indeed, it can result in a failing time scheme, or a very instable solution. A key-point to take a first decision is to remember which field needs regularity (in the L^2 -sense) in the Dirac structure. In our case, the p -type variables should be at least $H^1(\Omega)$, as can be inferred from (2.2). Hence, a first choice for the p -type variables is to take continuous Galerkin finite elements of order k . Since the time derivative of q will be, more or less, a gradient of a p -type variable, it will be a discontinuous Galerkin of order $k - 1$ approximation. Finally, at least one trace of these variables, either the control, or the observation, is at most a discontinuous Galerkin of order $k - 1$ approximation. Hence the following choices, with $k = 2$.

```

# Define the Finite Elements Method of each port
FEMs = [
    S.FEM(states[0].get_name(), 1, "DG"),
    S.FEM(states[1].get_name(), 2, "CG"),
    S.FEM(control_ports[0].get_name(), 1, "DG"),
    S.FEM(control_ports[1].get_name(), 1, "DG"),
    S.FEM(control_ports[2].get_name(), 1, "DG"),
    S.FEM(control_ports[3].get_name(), 1, "DG"),
]

# Add them to the dphs
for FEM in FEMs:
    wave.add_FEM(FEM)

```

We can assume anisotropy and heterogeneity in our model by defining the parameters as follows. It has to be kept in mind that a parameter is always linked to a port (*i.e.*, to a pair *flow-effort*). In particular, a parameter linked to a port that is a vector-field, should be a **tensor-field**.

```

# Define physical parameters
parameters = [
    S.Parameter("T", "Young's modulus", "tensor-field", "[[5+x,x*y],[x*y,2+y]]", "q"),
    S.Parameter("rho", "Mass density", "scalar-field", "3-x", "p"),
]

# Add them to the dphs
for parameter in parameters:
    wave.add_parameter(parameter)

```

It is time to define the bricks of our model, *i.e.* the block matrices of our discretization, providing the weak forms given in (2.3), (2.4), and (2.5).

This is probably the most difficult part of the process, and care must be taken. Remember that the syntax is the Generic Weak-Form Language (GWFL), for which an on-line documentation exists on the [GetFEM site](#).

For the block matrices appearing against time derivative of a variable, it is crucial not to forget the keyword `dt=True`.

```

# Define the pHs via `Brick` == non-zero block matrices == variational terms
bricks = [
    ## Define the Dirac structure

```

(continues on next page)

(continued from previous page)

```

# Define the mass matrices from the left-hand side: the `flow` part of the Dirac
↪structure
S.Brick("M_q", "q.Test_q", [1], dt=True, position="flow"),
S.Brick("M_p", "p.Test_p", [1], dt=True, position="flow"),
S.Brick("M_Y_B", "Y_B*Test_Y_B", [10], position="flow"),
S.Brick("M_Y_R", "Y_R*Test_Y_R", [11], position="flow"),
S.Brick("M_Y_T", "Y_T*Test_Y_T", [12], position="flow"),
# The Dirichlet term is applied via Lagrange multiplier == the colocated output
S.Brick("M_Y_L", "U_L*Test_Y_L", [13], position="flow"),
# Define the matrices from the right-hand side: the `effort` part of the Dirac
↪structure
S.Brick("D", "Grad(e_p).Test_q", [1], position="effort"),
S.Brick("-D^T", "-e_q.Grad(Test_p)", [1], position="effort"),
S.Brick("B_B", "U_B*Test_p", [10], position="effort"),
S.Brick("B_R", "U_R*Test_p", [11], position="effort"),
S.Brick("B_T", "U_T*Test_p", [12], position="effort"),
# The Dirichlet term is applied via Lagrange multiplier == the colocated output
S.Brick("B_L", "Y_L*Test_p", [13], position="effort"),
S.Brick("C_B", "-e_p*Test_Y_B", [10], position="effort"),
S.Brick("C_R", "-e_p*Test_Y_R", [11], position="effort"),
S.Brick("C_T", "-e_p*Test_Y_T", [12], position="effort"),
S.Brick("C_L", "-e_p*Test_Y_L", [13], position="effort"),
## Define the constitutive relations
# Hooke's law under implicit form  $-M_{e_q} e_q + CR_q q = 0$ 
S.Brick("-M_{e_q}", "-e_q.Test_e_q", [1]),
S.Brick("CR_q", "q.T.Test_e_q", [1]),
# Linear momentum definition under implicit form  $-M_{e_p} e_p + CR_p p = 0$ 
S.Brick("-M_{e_p}", "-e_p.Test_e_p", [1]),
S.Brick("CR_p", "p/rho*Test_e_p", [1]),
]

# Add all these `Bricks` to the dphs
for brick in bricks:
    wave.add_brick(brick)

```

The last step is to initialize the dphs, by providing the control functions and the initial values for q and p (i.e., the variables that are derivated in time in the model).

```

## Initialize the problem
# The controls expression, ordered as the control_ports
t_f = 5.0
expressions = ["0.", "0.", "0.", f"0.1*sin(4.*t)*sin(4*pi*y)*exp(-10.*pow((0.5*{t_f}-t),
↪2))"]

# Add each expression to its control_port
for control_port, expression in zip(control_ports, expressions):
    # Set the control functions: it automatically constructs the related `Brick`s such
    ↪that  $-M_u u + f(t) = 0$ 
    wave.set_control(control_port.get_name(), expression)

# Set the initial data
q_0 = "[0., 0.]"

```

(continues on next page)

(continued from previous page)

```

wave.set_initial_value("q", q_0)
p_0 = "3*(-20*((x-0.5)*(x-0.5)+(y-0.5)*(y-0.5)))"
wave.set_initial_value("p", p_0)

```

It remains to solve!

```

## Solve in time
# Define the time scheme ("cn" is Crank-Nicolson)
wave.set_time_scheme(ts_type="cn",
                    t_f=t_f,
                    dt_save=0.01,
                    )

# Solve
wave.solve()

```

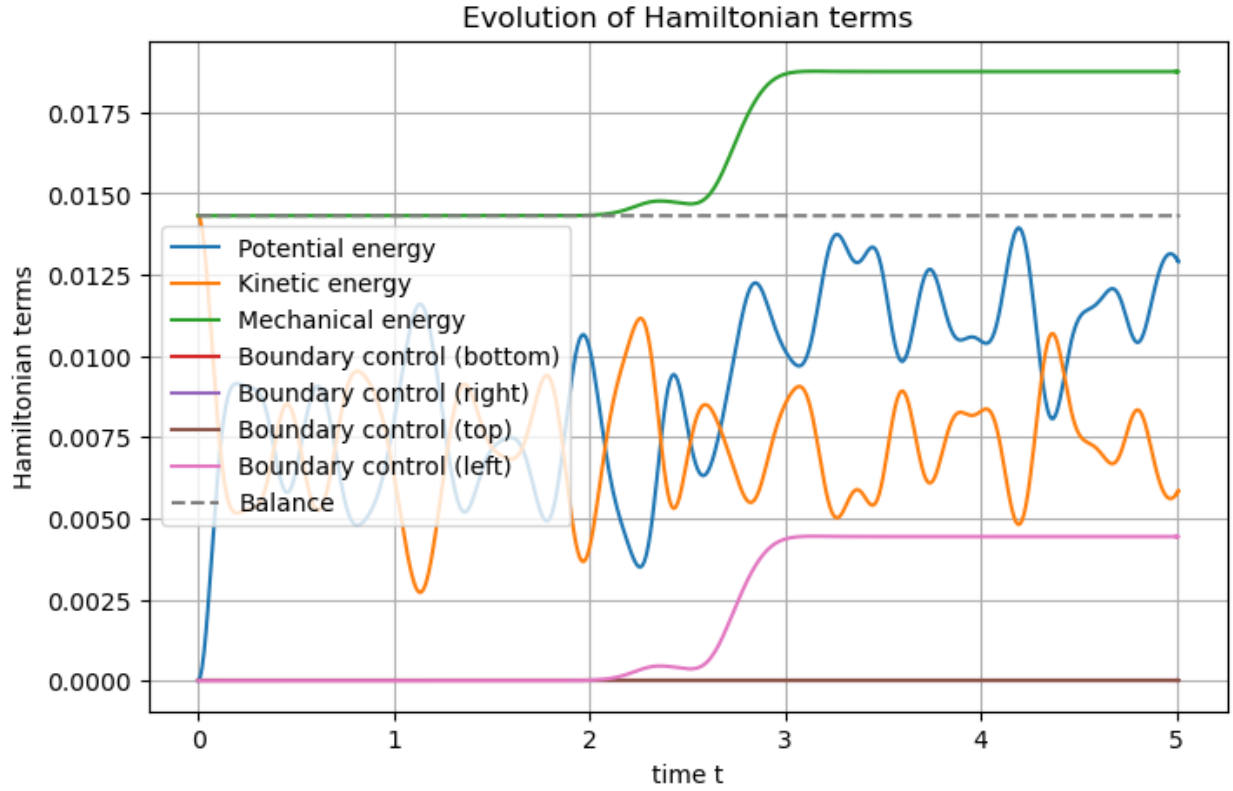
Now we can set the Hamiltonian and plot it.

```

## Post-processing
# Set Hamiltonian's name
wave.hamiltonian.set_name("Mechanical energy")
# Define each Hamiltonian Term
terms = [
    S.Term("Potential energy", "0.5*q.T.q", [1]),
    S.Term("Kinetic energy", "0.5*p*p/rho", [1]),
]
# Add them to the Hamiltonian
for term in terms:
    wave.hamiltonian.add_term(term)

# Plot the Hamiltonian and save the output
wave.plot_Hamiltonian(save_figure=True, filename="Hamiltonian_Wave_2D_Conservative.png")

```



Adding Damping to the dphs

The remaining part of the notebook is focused on the way to deal with *dissipativity*, hence using an **algebraic port**.

Let us come back to the continuous system. Adding a (fluid) damping consists in an additive term in Newton second law, which is proportional to the velocity (in the linear case). More precisely, denoting $\nu \geq 0$ the viscous parameter, one has:

$$\rho(x)\partial_{tt}^2 w(t, x) - \operatorname{div}(T(x) \cdot \operatorname{grad}(w(t, x))) + \nu(x)\partial_t w(t, x) = 0.$$

Using the framework of port-Hamiltonian system, this rewrites:

$$\begin{pmatrix} \partial_t \alpha_q \\ \partial_t \alpha_p \end{pmatrix} = \begin{bmatrix} 0 & \operatorname{grad} \\ \operatorname{div} & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \end{pmatrix} + \begin{pmatrix} 0 \\ -\nu e_p \end{pmatrix}.$$

One could include $-\nu$ inside the matrix of operators, this is the so-called $J - R$ framework. However, it does not exhibit the underlying Dirac structure, as it hides the resistive port. Let us introduce this hidden port, by denoting f_r the flow and e_r the effort, as follows:

$$\begin{pmatrix} \partial_t \alpha_q \\ \partial_t \alpha_p \\ f_r \end{pmatrix} = \begin{bmatrix} 0 & \operatorname{grad} & 0 \\ \operatorname{div} & 0 & -I \\ 0 & I^\top & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \\ e_r \end{pmatrix}, \quad (2.6)$$

and supplemented by the resistive constitutive relation $e_r = \nu f_r$.

Of course, at the discrete level, this will increase the number of degrees of freedom, as two extra variables have to be discretized. Nevertheless, in more complicated situations (e.g. dealing with non-linearities), this is the price to pay to recover a correct discrete power balance.

The **power balance** satisfied by the **Hamiltonian** is then

$$\frac{d}{dt}\mathcal{H}(t) = - \underbrace{\int_{\Omega} \nu(x) f_r^2(t, x)}_{\text{dissipated power}} + \underbrace{\langle y_N(t, \cdot), u_N(t, \cdot) \rangle_{\Gamma_N}}_{\text{power flowing through } \Gamma_N} + \underbrace{\langle u_D(t, \cdot), y_D(t, \cdot) \rangle_{\Gamma_D}}_{\text{power flowing through } \Gamma_D},$$

Another simulation

Let us start a new simulation with damping.

```
# Define a new dphs
wave_diss = S.DPHS("real")

# Set the domain (using the built-in geometry `Rectangle`)
# Labels: Omega = 1, Gamma_Bottom = 10, Gamma_Right = 11, Gamma_Top = 12, Gamma_Left = 13
rectangle = S.Domain("Rectangle", {"L": 2.0, "l": 1.0, "h": 0.1})

# On the rectangle domain
wave_diss.set_domain(rectangle)

# Define the variables
states = [
    S.State("q", "Strain", "vector-field"),
    S.State("p", "Linear momentum", "scalar-field"),
]
costates = [
    S.CoState("e_q", "Stress", states[0]),
    S.CoState("e_p", "Velocity", states[1]),
]

# Add them to the dphs
for (state, costate) in zip(states, costates):
    wave_diss.add_state(state)
    wave_diss.add_costate(costate)

# Define the control ports
control_ports = [
    S.Control_Port(
        "Boundary control (bottom)",
        "U_B",
        "Normal force",
        "Y_B",
        "Velocity trace",
        "scalar-field",
        region=10,
    ),
    S.Control_Port(
        "Boundary control (right)",
        "U_R",
        "Normal force",
        "Y_R",
        "Velocity trace",
        "scalar-field",
        region=11,
    ),
]
```

(continues on next page)

(continued from previous page)

```

    ),
    S.Control_Port(
        "Boundary control (top)",
        "U_T",
        "Normal force",
        "Y_T",
        "Velocity trace",
        "scalar-field",
        region=12,
    ),
    S.Control_Port(
        "Boundary control (left)",
        "U_L",
        "Velocity trace",
        "Y_L",
        "Normal force",
        "scalar-field",
        region=13,
        position="flow",
    ),
]

# Add them to the dphs
for ctrl_port in control_ports:
    wave_diss.add_control_port(ctrl_port)

```

The additional port is defined, added to the system `wave_diss` and a FEM is attached to it. Remark that we use the previously defined objects, *i.e.* we only append the FEM of the resistive port to the list of previously defined FEM objects. We choose continuous Galerkin of order 2, as the resistive effort is of p -type.

```

# Define a dissipative port
port_diss = S.Port("Damping", "f_r", "e_r", "scalar-field")

# Add it to the dphs
wave_diss.add_port(port_diss)

# Define the Finite Elements Method of each port
FEMs = [
    S.FEM(states[0].get_name(), 1, "DG"),
    S.FEM(states[1].get_name(), 2, "CG"),
    S.FEM(control_ports[0].get_name(), 1, "DG"),
    S.FEM(control_ports[1].get_name(), 1, "DG"),
    S.FEM(control_ports[2].get_name(), 1, "DG"),
    S.FEM(control_ports[3].get_name(), 1, "DG"),
    S.FEM("Damping", 2, "CG"),
]

# Add all of them to the dphs
for FEM in FEMs:
    wave_diss.add_FEM(FEM)

```

The parameter ν is obviously linked to the Damping port. It can be heterogeneous, as for the other parameters.

```
# Define physical parameters
parameters = [
    S.Parameter("T", "Young's modulus", "tensor-field", "[[5+x,x*y],[x*y,2+y]]", "q"),
    S.Parameter("rho", "Mass density", "scalar-field", "3-x", "p"),
    S.Parameter("nu", "viscosity", "scalar-field", "0.5*(2.0-x)", "Damping"),
]

# Add them to the dphs
for parameter in parameters:
    wave_diss.add_parameter(parameter)
```

Looking at (2.6), only 3 non-zero block matrices have to be added to the list of the already constructed bricks, for the Dirac structure part. And finally, 2 bricks are needed to discretize the resistive constitutive relation.

```
# Define the pHs via `Brick` == non-zero block matrices == variational terms
bricks = [
    ## Define the Dirac structure
    # Define the mass matrices from the left-hand side: the `flow` part of the Dirac_
    ↳structure
    S.Brick("M_q", "q.Test_q", [1], dt=True, position="flow"),
    S.Brick("M_p", "p.Test_p", [1], dt=True, position="flow"),
    S.Brick("M_Y_B", "Y_B*Test_Y_B", [10], position="flow"),
    S.Brick("M_Y_R", "Y_R*Test_Y_R", [11], position="flow"),
    S.Brick("M_Y_T", "Y_T*Test_Y_T", [12], position="flow"),
    # Mass matrix
    S.Brick("M_r", "f_r*Test_f_r", [1], position="flow"),
    # The Dirichlet term is applied via Lagrange multiplier == the colocated output
    S.Brick("M_Y_L", "U_L*Test_Y_L", [13], position="flow"),
    # Define the matrices from the right-hand side: the `effort` part of the Dirac_
    ↳structure
    S.Brick("D", "Grad(e_p).Test_q", [1], position="effort"),
    S.Brick("-D^T", "-e_q.Grad(Test_p)", [1], position="effort"),
    S.Brick("B_B", "U_B*Test_p", [10], position="effort"),
    S.Brick("B_R", "U_R*Test_p", [11], position="effort"),
    S.Brick("B_T", "U_T*Test_p", [12], position="effort"),
    # The "Identity" operator
    S.Brick("I_r", "e_r*Test_p", [1], position="effort"),
    # Minus its transpose
    S.Brick("-I_r^T", "-e_p*Test_f_r", [1], position="effort"),
    # The Dirichlet term is applied via Lagrange multiplier == the colocated output
    S.Brick("B_L", "Y_L*Test_p", [13], position="effort"),
    S.Brick("C_B", "-e_p*Test_Y_B", [10], position="effort"),
    S.Brick("C_R", "-e_p*Test_Y_R", [11], position="effort"),
    S.Brick("C_T", "-e_p*Test_Y_T", [12], position="effort"),
    S.Brick("C_L", "-e_p*Test_Y_L", [13], position="effort"),
    ## Define the constitutive relations
    # Hooke's law under implicit form ` - M_e_q e_q + CR_q q = 0 `
    S.Brick("-M_e_q", "-e_q.Test_e_q", [1]),
    S.Brick("CR_q", "q.T.Test_e_q", [1]),
    # Linear momentum definition under implicit form ` - M_e_p e_p + CR_p p = 0 `
    S.Brick("-M_e_p", "-e_p*Test_e_p", [1]),
    S.Brick("CR_p", "p/rho*Test_e_p", [1]),
    # Constitutive relation: linear viscous fluid damping ` - M_e_r e_r + CR_r f_r = 0 `
```

(continues on next page)

(continued from previous page)

```

S.Brick("-M_e_r", "-e_r*Test_e_r", [1]),
S.Brick("CR_r", "nu*f_r*Test_e_r", [1]),
]

```

Again, we use the previously defined Brick objects, thus, the whole system is constructed by adding all the bricks.

```

# Add all these `Bricks` to the dphs
for brick in bricks:
    wave_diss.add_brick(brick)

```

The initialization and solve steps are identical to the previous conservative case.

```

## Initialize the problem
# The controls expression, ordered as the control_ports
t_f = 5.
expressions = ["0.", "0.", "0.", f"0.1*sin(4.*t)*sin(4*pi*y)*exp(-10.*pow((0.5*{t_f}-t),
↳ 2))"]

# Add each expression to its control_port
for control_port, expression in zip(control_ports, expressions):
    # Set the control functions: it automatically constructs the related `Brick`s such
    ↳ that  $-M_u + f(t) = 0$ 
    wave_diss.set_control(control_port.get_name(), expression)

# Set the initial data
q_0 = "[0., 0.]"
wave_diss.set_initial_value("q", q_0)
p_0 = "3*(-20*((x-0.5)*(x-0.5)+(y-0.5)*(y-0.5)))"
wave_diss.set_initial_value("p", p_0)

## Solve in time
# Define the time scheme
wave_diss.set_time_scheme(ts_type="cn",
                          t_f=t_f,
                          dt_save=0.01,
                          )

# Solve
wave_diss.solve()

```

Now one can define and plot the Hamiltonian.

```

## Post-processing
# Set Hamiltonian's name
wave_diss.hamiltonian.set_name("Mechanical energy")

# Define each Hamiltonian Term (needed to overwrite the previously computed solution)
terms = [
    S.Term("Potential energy", "0.5*q.T.q", [1]),
    S.Term("Kinetic energy", "0.5*p*p/rho", [1]),
]

# Add them to the Hamiltonian

```

(continues on next page)

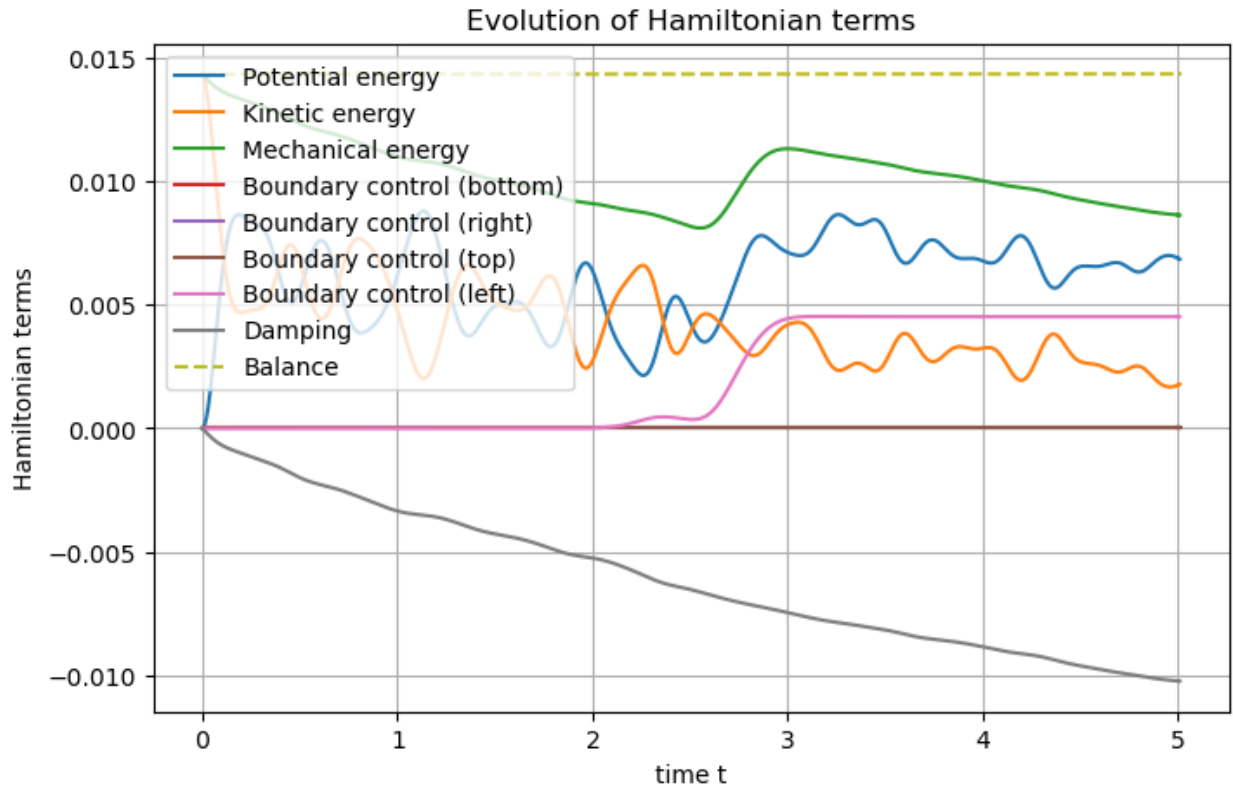
(continued from previous page)

```

for term in terms:
    wave_diss.hamiltonian.add_term(term)

# Plot the Hamiltonian and save the output
wave_diss.plot_Hamiltonian(save_figure=True, filename="Hamiltonian_Wave_2D_Dissipative.
→png")

```



2.3.2 The heat equation

Setting

This example is the first simple case of intrinsically port-Hamiltonian Differential Algebraic Equation (known as pH-DAE).

The so-called *heat equation* is driven by the first law of thermodynamics.

Let $\Omega = (0, 2) \times (0, 1)$ be a bounded open connected set, with mass density $\rho(x)$, for all $x \in \Omega$, and n be the outward unit normal at the boundary $\partial\Omega$. We assume that:

- The domain Ω does not change over time: *i.e.* we work at constant volume in a solid
- No chemical reaction is to be found in the domain
- Dulong-Petit's model: internal energy is proportional to temperature

Let us denotes:

- u the internal energy density
- \mathbf{J}_Q the heat flux

- T the local temperature
- $C_V := \left(\frac{du}{dT}\right)_V$ the isochoric heat capacity

The first law of thermodynamics, stating that in an isolated system, the energy is preserved, reads:

$$\rho(x)\partial_t u(t, x) = -\operatorname{div}(J_Q(t, x)), \quad \forall t \geq 0, x \in \Omega.$$

Under Dulong-Petit's model, one has $u = C_V T$, which leads to

$$\rho(x)C_V(x)\partial_t T(t, x) = -\operatorname{div}(J_Q(t, x)), \quad \forall t \geq 0, x \in \Omega.$$

As constitutive relation, the classical Fourier's law is considered:

$$J_Q(t, x) = -\lambda(x) \cdot \operatorname{grad}(T(t, x)), \quad \forall t \geq 0, x \in \Omega,$$

where λ is the **tensor-valued** heat conductivity of the medium.

We assume furthermore that one wants to control the temperature $T = u_D$ at the lower, right and upper part of the boundary, denoted Γ_D (a **Dirichlet** boundary condition), while the inward heat flux $-J_Q \cdot n = u_N$ will be prescribed at the left edge, denoted Γ_N (a **Neumann** boundary condition). Thus, the observations are $y_D = -J_Q \cdot n$ and $y_N = T$ respectively.

Port-Hamiltonian framework

Let us choose as Hamiltonian the usual quadratic form for parabolic equation

$$\mathcal{H}(T(t, x)) := \frac{1}{2} \int_{\Omega} \rho(x) C_V(x) T^2(t, x) dx.$$

Computing the variational derivative with respect to the weighed L^2 -inner product $(\phi, \psi)_{\Omega} := \int_{\Omega} \rho(x) C_V(x) \phi(x) \psi(x) dx$ leads to a co-state variable $e_T = T$. Hence, the first law of thermodynamics may be written as

$$\begin{pmatrix} \rho C_V T \\ \star \end{pmatrix} = \begin{bmatrix} 0 & -\operatorname{div} \\ \star & 0 \end{bmatrix} \begin{pmatrix} T \\ J_Q \end{pmatrix}.$$

As we want a *formally* skew-symmetric J operator, it has to be completed with $-\operatorname{grad}$, then

$$\begin{pmatrix} \rho C_V T \\ f_Q \end{pmatrix} = \begin{bmatrix} 0 & -\operatorname{div} \\ -\operatorname{grad} & 0 \end{bmatrix} \begin{pmatrix} T \\ J_Q \end{pmatrix},$$

and Fourier's law provides the constitutive relation $J_Q = \lambda f_Q$ to close the system.

Remark: ρC_V appears against the state variable as the weight of the L^2 -inner product, it should not be omitted in the mass matrix at the discrete level.

The **power balance** satisfied by the **Hamiltonian** is

$$\frac{d}{dt} \mathcal{H}(t) = \underbrace{- \int_{\Omega} \lambda \|f_Q(t, x)\|^2 dx}_{\text{dissipated power}} + \underbrace{\langle u_D(t, \cdot), y_D(t, \cdot) \rangle_{\Gamma_D}}_{\text{power flowing through } \Gamma_D} + \underbrace{\langle y_N(t, \cdot), u_N(t, \cdot) \rangle_{\Gamma_N}}_{\text{power flowing through } \Gamma_N},$$

where $\langle \cdot, \cdot \rangle_{\Gamma}$ is a boundary duality bracket $H^{\frac{1}{2}}, H^{-\frac{1}{2}}$ at the boundary Γ .

Structure-preserving discretization

Let φ_T and φ_Q be smooth test functions on Ω , and ψ_N and ψ_D be smooth test functions on Γ_N and Γ_D respectively. One can write the weak formulation of the **Dirac Structure** as follows

$$\left\{ \begin{array}{lcl} \int_{\Omega} \rho(x) C_V(x) \partial_t T(t, x) \varphi_T(x) dx & = & - \int_{\Omega} \operatorname{div} (J_Q(t, x)) \varphi_T(x) dx, \\ \int_{\Omega} f_Q(t, x) \cdot \varphi_Q(x) dx & = & - \int_{\Omega} \operatorname{grad} (T(t, x)) \cdot \varphi_Q(x) dx, \\ \langle y_D, \psi_D \rangle_{\Gamma_D} & = & \langle -J_Q \cdot n, \psi_D \rangle_{\Gamma_D}, \\ \langle u_N, \psi_N \rangle_{\Gamma_N} & = & \langle -J_Q \cdot n, \psi_N \rangle_{\Gamma_N}. \end{array} \right.$$

Integrating by parts the second line make the control u_N and the observation y_D appear

$$\int_{\Omega} f_Q(t, x) \cdot \varphi_Q(x) dx = \int_{\Omega} T(t, x) \operatorname{div} (\varphi_Q(x)) dx - \langle u_D, \varphi_Q \cdot n \rangle_{\Gamma_D} - \langle y_N, \varphi_Q \cdot n \rangle_{\Gamma_N}.$$

Now, let $(\varphi_T^i)_{1 \leq i \leq N_T} \subset L^2(\Omega)$ and $(\varphi_Q^k)_{1 \leq k \leq N_Q} \subset H_{\operatorname{div}}(\Omega)$ be two finite families of approximations for the T -type port and the Q -type port respectively, typically discontinuous and continuous Galerkin finite elements respectively. Denote also $(\psi_N^m)_{1 \leq m \leq N_N} \subset H^{\frac{1}{2}}(\Gamma_N)$ and $(\psi_D^m)_{1 \leq m \leq N_D} \subset H^{\frac{1}{2}}(\Gamma_D)$. In particular, the latter choices imply that the duality brackets at the boundary reduce to simple L^2 scalar products.

Writing the discrete weak formulation with those families, one has for all $1 \leq i \leq N_T$, all $1 \leq k \leq N_Q$, all $1 \leq m_N \leq N_N$ and all $1 \leq m_D \leq N_D$

$$\left\{ \begin{array}{lcl} \sum_{j=1}^{N_T} \int_{\Omega} \varphi_T^j(x) \rho(x) C_V(x) \varphi_T^i(x) dx \frac{d}{dt} T^j(t) & = & - \sum_{\ell=1}^{N_Q} \int_{\Omega} \operatorname{div} (\varphi_Q^{\ell}(x)) \varphi_T^i(x) dx J_Q^{\ell}(t), \\ \sum_{\ell=1}^{N_Q} \int_{\Omega} \varphi_Q^{\ell}(x) \varphi_Q^k(x) dx f_Q^{\ell}(t) & = & \sum_{j=1}^{N_T} \int_{\Omega} \varphi_T^j(x) \operatorname{div} (\varphi_Q^k(x)) dx T^j(t) \\ & & - \sum_{n_D=1}^{N_D} \int_{\Gamma_D} \varphi_Q^k(s) \cdot n(s) \psi_D^{n_D}(s) ds u_D^{n_D}(t) \\ & & - \sum_{n_N=1}^{N_N} \int_{\Gamma_N} \varphi_Q^k(s) \cdot n(s) \psi_N^{n_N}(s) ds y_N^{n_N}(t), \\ \sum_{n_D=1}^{N_D} \langle \psi_D^{n_D}, \psi_D^{m_D} \rangle_{\Gamma_D} y_D^{m_D}(t) & = & - \sum_{\ell=1}^{N_Q} \int_{\Gamma_D} \varphi_Q^{\ell}(s) \cdot n(s) \psi_D^{m_D}(s) ds J_Q^{\ell}(t), \\ \sum_{n_N=1}^{N_N} \langle \psi_N^{n_N}, \psi_N^{m_N} \rangle_{\Gamma_N} u_N^{m_N}(t) & = & - \sum_{\ell=1}^{N_Q} \int_{\Gamma_N} \varphi_Q^{\ell}(s) \cdot n(s) \psi_N^{m_N}(s) ds J_Q^{\ell}(t), \end{array} \right.$$

which rewrites in matrix form

$$\underbrace{\begin{bmatrix} M_T & 0 & 0 & 0 \\ 0 & M_Q & 0 & 0 \\ 0 & 0 & M_D & 0 \\ 0 & 0 & 0 & M_N \end{bmatrix}}_{=M} \begin{pmatrix} \frac{d}{dt} \underline{T}(t) \\ \underline{f_Q}(t) \\ -\underline{y_D}(t) \\ \underline{u_N}(t) \end{pmatrix} = \underbrace{\begin{bmatrix} 0 & D & 0 & 0 \\ -D^{\top} & 0 & B_D & -B_N^{\top} \\ 0 & -B_D^{\top} & 0 & 0 \\ 0 & B_N & 0 & 0 \end{bmatrix}}_{=J} \begin{pmatrix} \underline{T}(t) \\ \underline{J_Q}(t) \\ \underline{u_D}(t) \\ -\underline{y_N}(t) \end{pmatrix},$$

where $\underline{\star}(t) := (\star^1(t) \ \cdots \ \star^{N_{\star}})^{\top}$ and

$$\begin{aligned} (M_T)_{ij} &:= \int_{\Omega} \varphi_T^j(x) \varphi_T^i(x) dx, & (M_Q)_{k\ell} &:= \int_{\Omega} \varphi_Q^{\ell}(x) \cdot \varphi_Q^k(x) dx, \\ (M_D)_{m_D n_D} &:= \int_{\Gamma_D} \psi_D^{n_D}(s) \psi_D^{m_D}(s) ds, & (M_N)_{m_N n_N} &:= \int_{\Gamma_N} \psi_N^{n_N}(s) \psi_N^{m_N}(s) ds, \\ (D)_{i\ell} &:= - \int_{\Omega} \operatorname{div} (\varphi_Q^{\ell}(x)) \cdot \varphi_T^i(x) dx \\ (B_D)_{n_D k} &:= - \int_{\Gamma_D} \varphi_Q^k(s) \cdot n(s) \psi_D^{n_D}(s) ds, & (B_N)_{m_N \ell} &:= - \int_{\Gamma_N} \varphi_Q^{\ell}(s) \cdot n(s) \psi_N^{m_N}(s) ds, \end{aligned}$$

Now one can approximate the **constitutive relation**

$$\int_{\Omega} J_Q(t, x) \cdot \varphi_Q(x) dx = \int_{\Omega} f_Q(t, x) \cdot \lambda(x) \cdot \varphi_Q(x) dx,$$

from which one can deduce the matrix form of the discrete weak formulation of the constitutive relation

$$M_Q \underline{J_Q}(t) = \Lambda \underline{f_Q}(t),$$

where

$$(\Lambda)_{k\ell} := \int_{\Omega} \varphi_Q^\ell(x) \cdot \lambda(x) \cdot \varphi_Q^k(x) dx.$$

Finally, the **discrete Hamiltonian** \mathcal{H}^d is defined as the evaluation of \mathcal{H} on the approximation of the **state variable**

$$\mathcal{H}(t) := \mathcal{H}(T^d(t)) = \frac{1}{2} \underline{T}(t)^\top M_T \underline{T}(t).$$

The **discrete power balance** is then easily deduced from the above matrix formulations, thanks to the symmetry of M and the skew-symmetry of J

$$\frac{d}{dt} \mathcal{H}^d(t) = -\underline{f}_Q(t)^\top \Lambda \underline{f}_Q(t)^\top + \underline{u}_D(t)^\top M_D \underline{y}_D(t) + \underline{y}_N(t)^\top M_N \underline{u}_N(t).$$

Simulation

As usual, we start by importing the **SCRIMP** package. Then we define the Distributed Port-Hamiltonian System and attach a (built-in) domain to it.

```
# Import scrimp
import scrimp as S

# Init the distributed port-Hamiltonian system
heat = S.DPHS("real")

# Set the domain (using the built-in geometry `Rectangle`)
# Omega = 1, Gamma_Bottom = 10, Gamma_Right = 11, Gamma_Top = 12, Gamma_Left = 13
heat.set_domain(S.Domain("Rectangle", {"L": 2.0, "l": 1.0, "h": 0.1}))
```

The next step is to define the state and its co-state. Care must be taken here: both are the temperature T , since the parameter ρC_V have been taken into account as a weight in the L^2 -inner product. Hence, one may save some computational burden by using `substituted=True` which says to **SCRIMP** that the co-state is substituted into the state! Only **one** variable is approximated and will be computed in the sequel.

However, note that one could define a state e (namely the *internal energy*), and add Dulong-Petit's law as a constitutive relation $e = C_V T$ as usual.

```
# Define the variables and their discretizations and add them to the dphs
states = [
    S.State("T", "Temperature", "scalar-field"),
]
costates = [
    # Substituted=True indicates that only one variable has to be discretized on this_
    ↪ port
    S.CoState("T", "Temperature", states[0], substituted=True)
]
```

Let us define the algebraic port.

```
ports = [
    S.Port("Heat flux", "f_Q", "J_Q", "vector-field"),
]
```

And finally the control ports on each of the four boundary part.


```

control_ports = [
    S.Control_Port(
        "Boundary control (bottom)",
        "U_B",
        "Temperature",
        "Y_B",
        "- Normal heat flux",
        "scalar-field",
        region=10,
        position="effort",
    ),
    S.Control_Port(
        "Boundary control (right)",
        "U_R",
        "Temperature",
        "Y_R",
        "- Normal heat flux",
        "scalar-field",
        region=11,
        position="effort",
    ),
    S.Control_Port(
        "Boundary control (top)",
        "U_T",
        "Temperature",
        "Y_T",
        "- Normal heat flux",
        "scalar-field",
        region=12,
        position="effort",
    ),
    S.Control_Port(
        "Boundary control (left)",
        "U_L",
        "- Normal heat flux",
        "Y_L",
        "Temperature",
        "scalar-field",
        region=13,
        position="flow",
    ),
]

```

Add all these objects to the DPHS.

```

for state in states:
    heat.add_state(state)
for costate in costates:
    heat.add_costate(costate)
for port in ports:
    heat.add_port(port)
for ctrl_port in control_ports:
    heat.add_control_port(ctrl_port)

```

Now, we must define the finite element families on each port. As stated in the beginning, **only the φ_Q family needs a stronger regularity**. Let us choose continuous Galerkin approximation of order 2. Then, the divergence of φ_Q is easily approximated by discontinuous Galerkin of order 1. At the boundary, this latter regularity will then occur, hence the choice of discontinuous Galerkin of order 1 as well.

```
FEMs = [
    S.FEM(states[0].get_name(), 1, FEM="DG"),
    S.FEM(ports[0].get_name(), 2, FEM="CG"),
    S.FEM(control_ports[0].get_name(), 1, FEM="DG"),
    S.FEM(control_ports[1].get_name(), 1, FEM="DG"),
    S.FEM(control_ports[2].get_name(), 1, FEM="DG"),
    S.FEM(control_ports[3].get_name(), 1, FEM="DG"),
]
for FEM in FEMs:
    heat.add_FEM(FEM)
```

It is now time to define the parameters, namely ρ , C_V and λ . For the sake of simplicity, we assume that ρ will take C_V into account.

```
# Define the physical parameters
parameters = [
    S.Parameter("rho", "Mass density times heat capacity", "scalar-field", "3.", "T"),
    S.Parameter(
        "Lambda",
        "Heat conductivity",
        "tensor-field",
        "[[1e-2,0.],[0.,1e-2]]",
        "Heat flux",
    ),
]
# Add them to the dphs
for parameter in parameters:
    heat.add_parameter(parameter)
```

Now the non-zero block matrices of the Dirac structure can be defined using the Brick object, as well as the constitutive relation, *i.e.* Fourier's law.

```
# Define the Dirac structure and the constitutive relations block matrices as `Brick`
bricks = [
    # Add the mass matrices from the left-hand side: the `flow` part of the Dirac
    ↳ structure
    S.Brick("M_T", "T*rho*Test_T", [1], dt=True, position="flow"),
    S.Brick("M_Q", "f_Q.Test_f_Q", [1], position="flow"),
    S.Brick("M_Y_B", "Y_B*Test_Y_B", [10], position="flow"),
    S.Brick("M_Y_R", "Y_R*Test_Y_R", [11], position="flow"),
    S.Brick("M_Y_T", "Y_T*Test_Y_T", [12], position="flow"),
    # Normal trace is imposed by Lagrange multiplier on the left side == the collocated
    ↳ output
    S.Brick("M_Y_L", "U_L*Test_Y_L", [13], position="flow"),
    # Add the matrices from the right-hand side: the `effort` part of the Dirac structure
    S.Brick("D", "-Div(J_Q)*Test_T", [1], position="effort"),
    S.Brick("-D^T", "T*Div(Test_f_Q)", [1], position="effort"),
    S.Brick("B_B", "-U_B*Test_f_Q.Normal", [10], position="effort"),
    S.Brick("B_R", "-U_R*Test_f_Q.Normal", [11], position="effort"),
```

(continues on next page)

(continued from previous page)

```

S.Brick("B_T", "-U_T*Test_f_Q.Normal", [12], position="effort"),
# Normal trace is imposed by Lagrange multiplier on the left side == the collocated_
↪output
S.Brick("B_L", "-Y_L*Test_f_Q.Normal", [13], position="effort"),
S.Brick("C_B", "J_Q.Normal*Test_Y_B", [10], position="effort"),
S.Brick("C_R", "J_Q.Normal*Test_Y_R", [11], position="effort"),
S.Brick("C_T", "J_Q.Normal*Test_Y_T", [12], position="effort"),
S.Brick("C_L", "J_Q.Normal*Test_Y_L", [13], position="effort"),
## Define the constitutive relations as getfem `brick`
# Fourier's law under implicit form - M_e_Q e_Q + CR_Q Q = 0
S.Brick("-M_J_Q", "-J_Q.Test_J_Q", [1]),
S.Brick("CR_Q", "f_Q.Lambda.Test_J_Q", [1]),
]
for brick in bricks:
    heat.add_brick(brick)

```

As controls, we assume that the temperature is prescribed, while the inward heat flux is proportional to the temperature (*i.e.* we consider an impedance-like absorbing boundary condition). This is easily achieved in **SCRIMP** by calling the variable in the expression of the control to apply.

The initial temperature profile is compatible with these controls, and has a positive bump centered in the domain.

```

# Initialize the problem
expressions = ["1.", "1.", "1.", "0.2*T"]

for control_port, expression in zip(control_ports, expressions):
    # Set the control functions (automatic construction of bricks such that -M_u u +_
    ↪f(t) = 0)
    heat.set_control(control_port.get_name(), expression)

# Set the initial data
heat.set_initial_value("T", "1. + 2.*np.exp(-50*((x-1)*(x-1)+(y-0.5)*(y-0.5))**2)")

```

We can now solve our Differential Algebraic Equation (DAE) using, *e.g.*, a Backward Differentiation Formula (BDF) of order 4.

```

## Solve in time
# Define the time scheme ("bdf" is backward differentiation formula)
heat.set_time_scheme(t_f=5.,
                    ts_type="bdf",
                    ts_bdf_order=4,
                    dt=0.01,
                    )

# Solve
heat.solve()

```

The Hamiltonian may be defined, computed and plot.

```

### Post-processing
# Set Hamiltonian name
heat.hamiltonian.set_name("Lyapunov formulation")
# Define the term

```

(continues on next page)

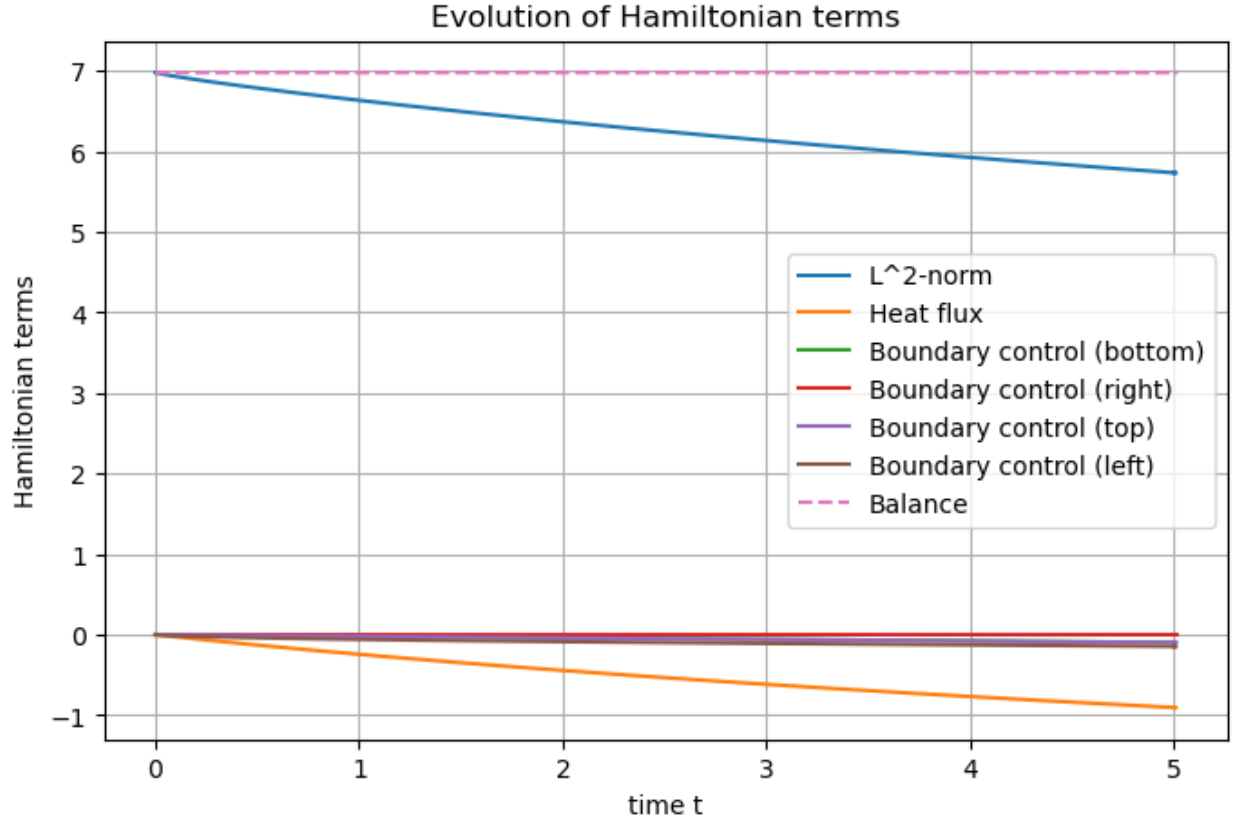
(continued from previous page)

```

terms = [
    S.Term("L^2-norm", "0.5*T*rho*T", [1]),
]
# Add them to the Hamiltonian
for term in terms:
    heat.hamiltonian.add_term(term)

# Plot the Hamiltonian
heat.plot_Hamiltonian(save_figure=True, filename="Hamiltonian_Heat_2D.png")

```



2.3.3 Another wave equation

Setting

The objective of this example is to show how sub-domains may be used, and how substitutions reduce the computational burden: it assumes that [this 2D wave example](#) has already been studied.

Substitutions

The damped wave equation as a port-Hamiltonian system writes

$$\begin{pmatrix} \partial_t \alpha_q \\ \partial_t \alpha_p \\ f_r \end{pmatrix} = \begin{bmatrix} 0 & \text{grad} & 0 \\ \text{div} & 0 & -I \\ 0 & I^\top & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \\ e_r \end{pmatrix},$$

where α_q denotes the strain, α_p is the linear momentum, e_q is the stress, e_p is the velocity and (f_r, e_r) is the dissipative port.

This system must be close with **constitutive relations**, which are

$$e_q = T \cdot \alpha_q, \quad e_p = \frac{\alpha_p}{\rho}, \quad e_r = \nu f_r,$$

where T is the Young's modulus, ρ the mass density and ν the viscosity. Inverting these relations and substituting the results in the port-Hamiltonian system leads to the **co-energy formulation** (or more generally **co-state formulation**)

$$\begin{pmatrix} T^{-1} \cdot \partial_t e_q \\ \rho \partial_t e_p \\ \nu^{-1} e_r \end{pmatrix} = \begin{bmatrix} 0 & \text{grad} & 0 \\ \text{div} & 0 & -I \\ 0 & I^\top & 0 \end{bmatrix} \begin{pmatrix} e_q \\ e_p \\ e_r \end{pmatrix}.$$

At the discrete level, this allows to reduce the number of degrees of freedom by two.

Remark: In the example, ν only acts on a sub-domain, *i.e.* it is theoretically null on the complementary, and thus is not invertible! To be able to invert it, it is then mandatory to restrict the dissipative port to the sub-domain where $\nu > 0$.

Simulation

Let us start quickly until the definition of the dissipative port.

```
# Import scrimp
import scrimp as S

# Init the distributed port-Hamiltonian system
wave = S.DPHS("real")

# Set the domain (using the built-in geometry `Concentric`)
# Labels: Disk = 1, Annulus = 2, Interface = 10, Boundary = 20
omega = S.Domain("Concentric", {"R": 1.0, "r": 0.6, "h": 0.1})

# And add it to the dphs
wave.set_domain(omega)

## Define the variables
states = [
    S.State("q", "Stress", "vector-field"),
    S.State("p", "Velocity", "scalar-field"),
]

# Use of the `substituted=True` keyword to get the co-energy formulation
costates = [
    S.CoState("e_q", "Stress", states[0], substituted=True),
    S.CoState("e_p", "Velocity", states[1], substituted=True),
]

# Add them to the dphs
for state in states:
    wave.add_state(state)
for costate in costates:
    wave.add_costate(costate)
```

In order to restrict the dissipative port to the internal disk, we use the `region` keyword.

```
# Define the dissipative port, only on the subdomain labelled 1 = the internal disk
ports = [
    S.Port("Damping", "e_r", "e_r", "scalar-field", substituted=True, region=1),
```

(continues on next page)

(continued from previous page)

```

]

# Add it to the dphs
for port in ports:
    wave.add_port(port)

```

The control port is only at the external boundary, labelled by 20 in **SCRIMP**.

```

# Define the control port
control_ports = [
    S.Control_Port(
        "Boundary control",
        "U",
        "Normal force",
        "Y",
        "Velocity trace",
        "scalar-field",
        region=20,
    ),
]

# Add it to the dphs
for ctrl_port in control_ports:
    wave.add_control_port(ctrl_port)

```

The sequel is as for the already seen examples.

```

# Define the Finite Elements Method of each port
FEMs = [
    S.FEM(states[0].get_name(), 1, "DG"),
    S.FEM(states[1].get_name(), 2, "CG"),
    S.FEM(ports[0].get_name(), 1, "DG"),
    S.FEM(control_ports[0].get_name(), 1, "DG"),
]

# Add them to the dphs
for FEM in FEMs:
    wave.add_FEM(FEM)

# Define physical parameters: care must be taken,
# in the co-energy formulation, some parameters are
# inverted in comparison to the classical formulation
parameters = [
    S.Parameter(
        "Tinv",
        "Young's modulus inverse",
        "tensor-field",
        "[[5+x,x*y],[x*y,2+y]]",
        "q",
    ),
    S.Parameter("rho", "Mass density", "scalar-field", "3-x", "p"),
    S.Parameter(

```

(continues on next page)

(continued from previous page)

```

        "nu",
        "Viscosity",
        "scalar-field",
        "10*(0.36-(x*x+y*y))",
        ports[0].get_name(),
    ),
]

# Add them to the dphs
for parameter in parameters:
    wave.add_parameter(parameter)

```

Regarding the Brick objects, there is a major difference with the previous examples: here, we need to list **all** the sub-domain labels for the wave equation, hence the [1,2]. On the other hand, the dissipation only occurs on the internal disk, labelled 1, and thus the block matrices corresponding to the identity operators which implement the dissipation **must be restrict to [1]**.

```

# Define the pHs via `Brick` == non-zero block matrices == variational terms
# Since we use co-energy formulation, constitutive relations are already taken into
# account in the mass matrices M_q and M_p
bricks = [
    ## Define the Dirac structure
    # Define the mass matrices from the left-hand side: the `flow` part of the Dirac
    ↳structure
    S.Brick("M_q", "q.Tinv.Test_q", [1, 2], dt=True, position="flow"),
    S.Brick("M_p", "p*rho*Test_p", [1, 2], dt=True, position="flow"),
    S.Brick("M_r", "e_r/nu*Test_e_r", [1], position="flow"),
    S.Brick("M_Y", "Y*Test_Y", [20], position="flow"),
    # Define the matrices from the right-hand side: the `effort` part of the Dirac
    ↳structure
    S.Brick("D", "Grad(p).Test_q", [1, 2], position="effort"),
    S.Brick("-D^T", "-q.Grad(Test_p)", [1, 2], position="effort"),
    S.Brick("I_r", "e_r*Test_p", [1], position="effort"),
    S.Brick("B", "U*Test_p", [20], position="effort"),
    S.Brick("-I_r^T", "-p*Test_e_r", [1], position="effort"),
    S.Brick("-B^T", "-p*Test_Y", [20], position="effort"),
    ## Define the constitutive relations
    # Already taken into account in the Dirac Structure!
]

# Add all these `Bricks` to the dphs
for brick in bricks:
    wave.add_brick(brick)

```

The remaining part of the code have already been explain in previous examples.

```

## Initialize the problem
# The controls expression
expressions = ["0.5*Y"]

# Add each expression to its control_port
for control_port, expression in zip(control_ports, expressions):

```

(continues on next page)

(continued from previous page)

```

# Set the control functions (automatic construction of bricks such that  $-M_u u + u$ 
↪  $f(t) = 0$ )
wave.set_control(control_port.get_name(), expression)

# Set the initial data
wave.set_initial_value("q", "[0., 0.]")
wave.set_initial_value("p", "2.72**(-20*((x-0.5)*(x-0.5)+(y-0.5)*(y-0.5)))")

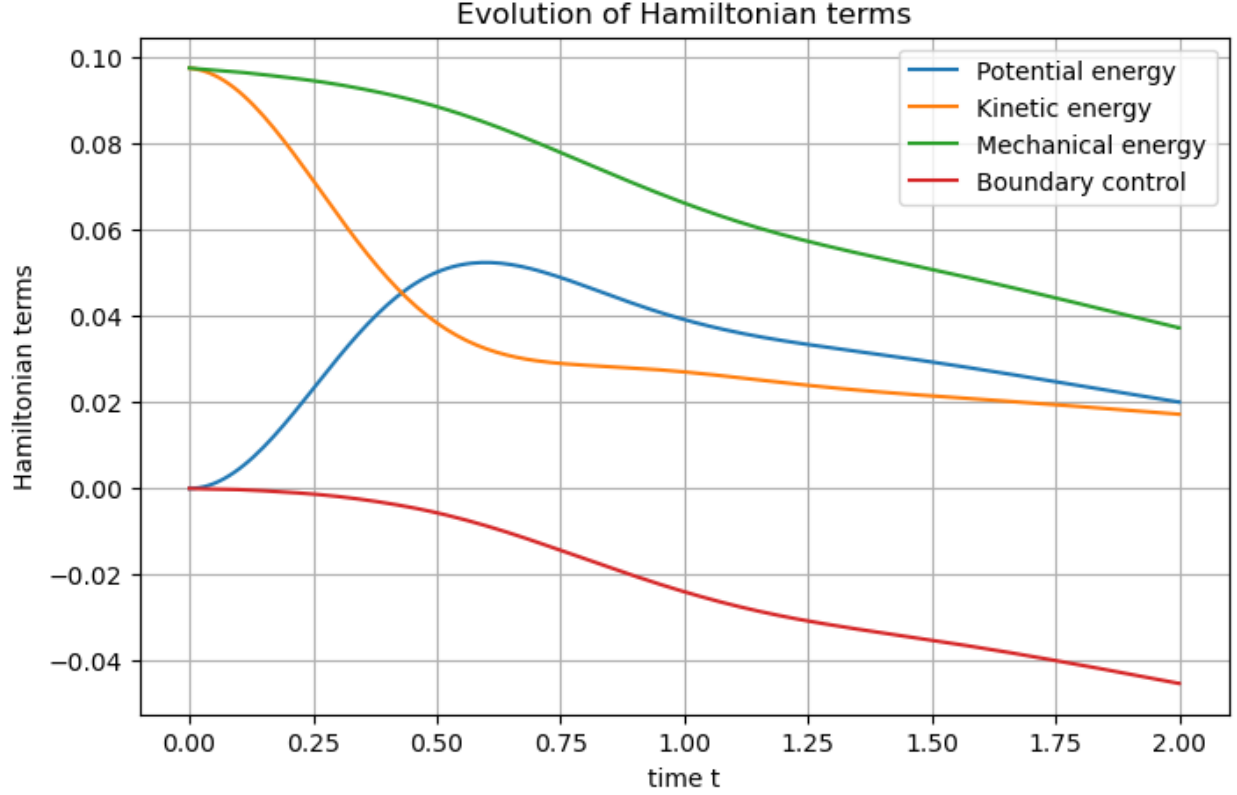
## Solve in time
# Define the time scheme ("cn" is Crank-Nicolson)
wave.set_time_scheme(ts_type="cn",
                     t_f=2.0,
                     dt_save=0.01,
                     )

# Solve
wave.solve()

## Post-processing
## Set Hamiltonian's name
wave.hamiltonian.set_name("Mechanical energy")
# Define each Hamiltonian Term
terms = [
    S.Term("Potential energy", "0.5*q.Tinv.q", [1, 2]),
    S.Term("Kinetic energy", "0.5*p*p*rho", [1, 2]),
]
# Add them to the Hamiltonian
for term in terms:
    wave.hamiltonian.add_term(term)

# Plot the Hamiltonian and save the output
wave.plot_Hamiltonian(save_figure=True)

```

2.3.4 Heat wave coupling

Setting

It is assumed that the 2D wave equation, the 2D wave equation in co-energy formulation and the 2D heat equation have already been studied.

The objective of this example is to deal with interconnection in the sense of port-Hamiltonian systems.

We are interested in the coupled heat-wave system which can be formulated as follows: let $\Omega := \Omega_W \cup \Omega_H$ be a bounded domain in \mathbb{R}^2 such that $\Omega_W \cap \Omega_H = \emptyset$, we denote $\Gamma_I := \partial\Omega_W \cap \partial\Omega_H$ the interface between the two domains, and $\Gamma_W := \partial\Omega_W \setminus \Gamma_I$ and $\Gamma_H := \partial\Omega_H \setminus \Gamma_I$. The system of equations reads

$$\begin{cases} \partial_t T(t, x) = \operatorname{div}(\operatorname{grad}(T(t, x))), & \forall t \geq 0, x \in \Omega_H, \\ \partial_{tt}^2 w(t, x) = \operatorname{div}(\operatorname{grad}(T(t, x))), & \forall t \geq 0, x \in \Omega_H, \\ T(t, s) = 0, & \forall t \geq 0, s \in \Gamma_H, \\ w(t, s) = 0, & \forall t \geq 0, s \in \Gamma_W, \end{cases}$$

together with the transmission conditions across the interface

$$\begin{cases} T(t, s) = \partial_t w(t, s), & \forall t \geq 0, s \in \Gamma_I, \\ \partial_{n_H} T(t, s) = -\partial_{n_W} w(t, s), & \forall t \geq 0, s \in \Gamma_I, \end{cases}$$

where n_H is the outward normal to Ω_H and n_W is the outward normal to Ω_W . Hence, $n_H = -n_W$ on Γ_I .

Port-Hamiltonian framework

- The heat equation

The heat equation reads

$$\begin{pmatrix} \partial_t T \\ e_Q \end{pmatrix} = \begin{bmatrix} 0 & -\text{div} \\ -\text{grad} & 0 \end{bmatrix} \begin{pmatrix} T \\ e_Q \end{pmatrix},$$

together with the boundary ports

$$\begin{cases} u_H^I &= T, & \Gamma_I, \\ y_H^I &= e_Q \cdot n_H, & \Gamma_I, \end{cases}$$

and

$$\begin{cases} u_H &= T, & \Gamma_H, \\ y_H &= e_Q \cdot n_H, & \Gamma_H. \end{cases}$$

- The wave equation

The Dirichlet boundary condition has to be relaxed by $\partial_t w = 0$ to fit the port-Hamiltonian framework. Providing this adaptation and the notation $p := \partial_t w$ and $q := \text{grad}(w)$, the wave equation reads

$$\begin{pmatrix} \partial_t q \\ \partial_t p \end{pmatrix} = \begin{bmatrix} 0 & \text{grad} \\ \text{div} & 0 \end{bmatrix} \begin{pmatrix} q \\ p \end{pmatrix},$$

together with the boundary ports

$$\begin{cases} u_W^I &= q \cdot n_W, & \Gamma_I, \\ y_W^I &= p, & \Gamma_I, \end{cases}$$

and

$$\begin{cases} u_W &= q \cdot n_W, & \Gamma_H, \\ y_W &= p, & \Gamma_H. \end{cases}$$

- The interconnection

The transmission condition at the interface may be recast as a power-preserving interconnection. It can be either a **gyrator** or a **transformer** interconnection, depending on the chosen causality for each system. We the above choices, we have a **gyrator interconnection**, indeed, one has

$$u_H^I = y_w^I, \quad u_W^I = y_H^I.$$

Structure-preserving discretization

- The heat equation

We use the div-div formulation already presented in the [2D heat equation](#) example, *i.e.* we obtain the following system

$$\underbrace{\begin{bmatrix} M_T & 0 & 0 & 0 \\ 0 & M_Q & 0 & 0 \\ 0 & 0 & M_H^I & 0 \\ 0 & 0 & 0 & M_H \end{bmatrix}}_{=M} \begin{pmatrix} \frac{d}{dt} \underline{T}(t) \\ \underline{e_Q}(t) \\ -\underline{y_H^I}(t) \\ -\underline{y_H}(t) \end{pmatrix} = \underbrace{\begin{bmatrix} 0 & D & 0 & 0 \\ -D^\top & 0 & B_H^I & B_H \\ 0 & -(B_H^I)^\top & 0 & 0 \\ 0 & -(B_H)^\top & 0 & 0 \end{bmatrix}}_{=J} \begin{pmatrix} \underline{T}(t) \\ \underline{e_Q}(t) \\ \underline{u_H^I}(t) \\ \underline{u_H}(t) \end{pmatrix},$$

- The wave equation

We use the grad-grad formulation already presented in the [2D wave equation](#) example, *i.e.* we obtain the following system

$$\underbrace{\begin{bmatrix} M_q & 0 & 0 & 0 \\ 0 & M_p & 0 & 0 \\ 0 & 0 & M_W^I & 0 \\ 0 & 0 & 0 & M_W \end{bmatrix}}_{=M} \begin{pmatrix} \frac{d}{dt} \underline{q}(t) \\ \frac{d}{dt} \underline{p}(t) \\ -\underline{y_W^I}(t) \\ \underline{u_W}(t) \end{pmatrix} = \underbrace{\begin{bmatrix} 0 & D & 0 & 0 \\ -D^\top & 0 & B_W^I & -B_W^\top \\ 0 & -(B_W^I)^\top & 0 & 0 \\ 0 & B_W & 0 & 0 \end{bmatrix}}_{=J} \begin{pmatrix} \underline{q}(t) \\ \underline{p}(t) \\ \underline{u_W^I}(t) \\ -\underline{y_W}(t) \end{pmatrix},$$

- The transformer interconnection

This condition is easy to implement, and leads to

$$M_H^I \underline{u}_H^I(t) = M_W^I \underline{y}_W^I(t), \quad M_W^I \underline{u}_W^I(t) = M_H^I \underline{y}_H^I(t).$$

Simulation

Let us start as usual, but using now the Concentric built-in geometry.

```
# Import scrimp
import scrimp as S

# Init the distributed port-Hamiltonian system
hw = S.DPHS("real")

# Set the domain (using the built-in geometry `Concentric`)
# Labels: Disk = 1, Annulus = 2, Interface = 10, Boundary = 20
omega = S.Domain("Concentric", {"R": 1.0, "r": 0.6, "h": 0.1})

# And add it to the dphs
hw.set_domain(omega)
```

It is important to remember here one of the objective of this example: to understand the `region` keyword.

For our study case, the heat equation will lie on a region `heat_region`, while the wave equation will lie on another region `wave_region`. And this has to be stated when defining the states and co-states, and everytime an integral (either the *weak forms* or the *Hamiltonian terms*) occurs.

```
# Define the states and costates, needs the heat and wave region's labels
heat_region = 1
wave_region = 2
states = [
    S.State("T", "Temperature", "scalar-field", region=heat_region),
    S.State("p", "Velocity", "scalar-field", region=wave_region),
    S.State("q", "Stress", "vector-field", region=wave_region),
]

# Use of the `substituted=True` keyword to get the co-energy formulation
costates = [
    S.CoState("T", "Temperature", states[0], substituted=True),
    S.CoState("p", "Velocity", states[1], substituted=True),
    S.CoState("q", "Stress", states[2], substituted=True),
]

# Add them to the dphs
for state in states:
    hw.add_state(state)
for costate in costates:
    hw.add_costate(costate)
```

The same is true for the resistive port for the heat equation.

```
# Define the algebraic port
ports = [
    S.Port("Heat flux", "e_Q", "e_Q", "vector-field", substituted=True, region=heat_
```

(continues on next page)

(continued from previous page)

```

    region),
]

# Add it to the dphs
for port in ports:
    hw.add_port(port)

# Define the control ports
control_ports = [
    S.Control_Port(
        "Interface Heat",
        "U_T",
        "Heat flux",
        "Y_T",
        "Temperature",
        "scalar-field",
        region=10,
        position="effort"
    ),
    S.Control_Port(
        "Interface Wave",
        "U_w",
        "Velocity",
        "Y_w",
        "Velocity",
        "scalar-field",
        region=10,
        position="effort"
    ),
    # This port will be either for the wave or the heat equation
    # It corresponds to the exterior circle of radius R
    S.Control_Port(
        "Boundary",
        "U_bnd",
        "0",
        "Y_bnd",
        ".",
        "scalar-field",
        region=20,
        position="flow"
    ),
]

# Add it to the dphs
for ctrl_port in control_ports:
    hw.add_control_port(ctrl_port)

```

For the FEM choices, see the previous examples.

```

# Define the Finite Elements Method of each port
k = 1
FEMs = [

```

(continues on next page)

(continued from previous page)

```

S.FEM("T", k, "DG"),
S.FEM("Heat flux", k+1, "CG"),
S.FEM("Interface Heat", k, "DG"),
S.FEM("p", k+1, "CG"),
S.FEM("q", k, "DG"),
S.FEM("Interface Wave", k, "DG"),
S.FEM("Boundary", k, "DG"),
]

# Add them to the dphs
for FEM in FEMs:
    hw.add_FEM(FEM)

```

The Brick object does not have an *optional* region keyword, it is mandatory: more precisely, it requires a list of regions as third argument.

```

# Define the pHs via `Brick` == non-zero block matrices == variational terms
# Since we use co-energy formulation, constitutive relations are already taken into
# account in the mass matrices M_q and M_p
bricks = [
    # === Heat: div-div
    S.Brick("M_T", "T*Test_T", [heat_region], dt=True, position="flow"),
    S.Brick("M_Q", "e_Q.Test_e_Q", [heat_region], position="flow"),
    S.Brick("M_Y_T", "Y_T*Test_Y_T", [10], position="flow"),

    S.Brick("D_T", "-Div(e_Q)*Test_T", [heat_region], position="effort"),
    S.Brick("D_T^T", "T*Div(Test_e_Q)", [heat_region], position="effort"),
    S.Brick("B_T", "U_T*Test_e_Q.Normal", [10], position="effort"),
    S.Brick("B_T^T", "e_Q.Normal*Test_Y_T", [10], position="effort"),

    # === Wave: grad-grad
    S.Brick("M_p", "p*Test_p", [wave_region], dt=True, position="flow"),
    S.Brick("M_q", "q.Test_q", [wave_region], dt=True, position="flow"),
    S.Brick("M_Y_w", "Y_w*Test_Y_w", [10], position="flow"),

    S.Brick("D_w", "-q.Grad(Test_p)", [wave_region], position="effort"),
    S.Brick("D_w^T", "Grad(p).Test_q", [wave_region], position="effort"),
    S.Brick("B_w", "U_w*Test_p", [10], position="effort"),
    S.Brick("B_w^T", "p*Test_Y_w", [10], position="effort"),
]

# === Boundary depends on where is the heat equation / wave equation
if wave_region==1:
    bricks.append(S.Brick("M_Y_bnd", "Y_bnd*Test_Y_bnd", [20], position="flow"))
    bricks.append(S.Brick("B_bnd", "U_bnd*Test_e_Q.Normal", [20], position="effort"))
    bricks.append(S.Brick("B_bnd^T", "e_Q.Normal*Test_Y_bnd", [20], position="effort"))
else:
    bricks.append(S.Brick("M_Y_bnd", "U_bnd*Test_Y_bnd", [20], position="flow"))
    bricks.append(S.Brick("B_bnd", "Y_bnd*Test_p", [20], position="effort"))
    bricks.append(S.Brick("B_bnd^T", "p*Test_Y_bnd", [20], position="effort"))
for brick in bricks:
    hw.add_brick(brick)

```

Finally, the **gyrator** interconnection for a system is just an output feedback from the other. The subtlety is that, while

the normal along Γ_I depends from which side it is computed *on paper*, this is not the case *numerically*: a minus sign is necessary.

```
# Set the controls
# === Gyration interconnection
hw.set_control("Interface Heat", "Y_w")
# CAREFUL: the numerical normal is the same for both sub-domains! Hence the minus sign.
hw.set_control("Interface Wave", "-Y_T")
# === Dirichlet boundary condition
hw.set_control("Boundary", "0.")

# Set the initial data
hw.set_initial_value("T", "5.*np.exp(-25*((x-0.6)*(x-0.6)+y*y))")
hw.set_initial_value("p", "5.*np.exp(-25*((x-0.6)*(x-0.6)+y*y))")
hw.set_initial_value("q", "[0.,0.]")

## Solve in time
# Define the time scheme ("bdf" is backward differentiation formula)
hw.set_time_scheme(ts_type="bdf",
                   t_f=15.,
                   dt=0.001,
                   dt_save=0.05,
                   ksp_type="preonly",
                   pc_type="lu",
                   pc_factor_mat_solver_type="mumps",
                   )

# Solve
hw.solve()
```

We end as usual with the Hamiltonian plot. Since our study case is known to be strongly stable, but never exponential nor uniformly in the initial state, we may also invoke the `get_Hamiltonian` method to make a log-log view of its evolution.

```
## Post-processing
## Set Hamiltonian's name
hw.hamiltonian.set_name("Hamiltonian")
# Define each Hamiltonian Term
terms = [
    S.Term("Lyapunov heat", "0.5*T*T", [heat_region]),
    S.Term("Kinetic energy", "0.5*p*p", [wave_region]),
    S.Term("Potential energy", "0.5*q.q", [wave_region]),
]
# Add them to the Hamiltonian
for term in terms:
    hw.hamiltonian.add_term(term)

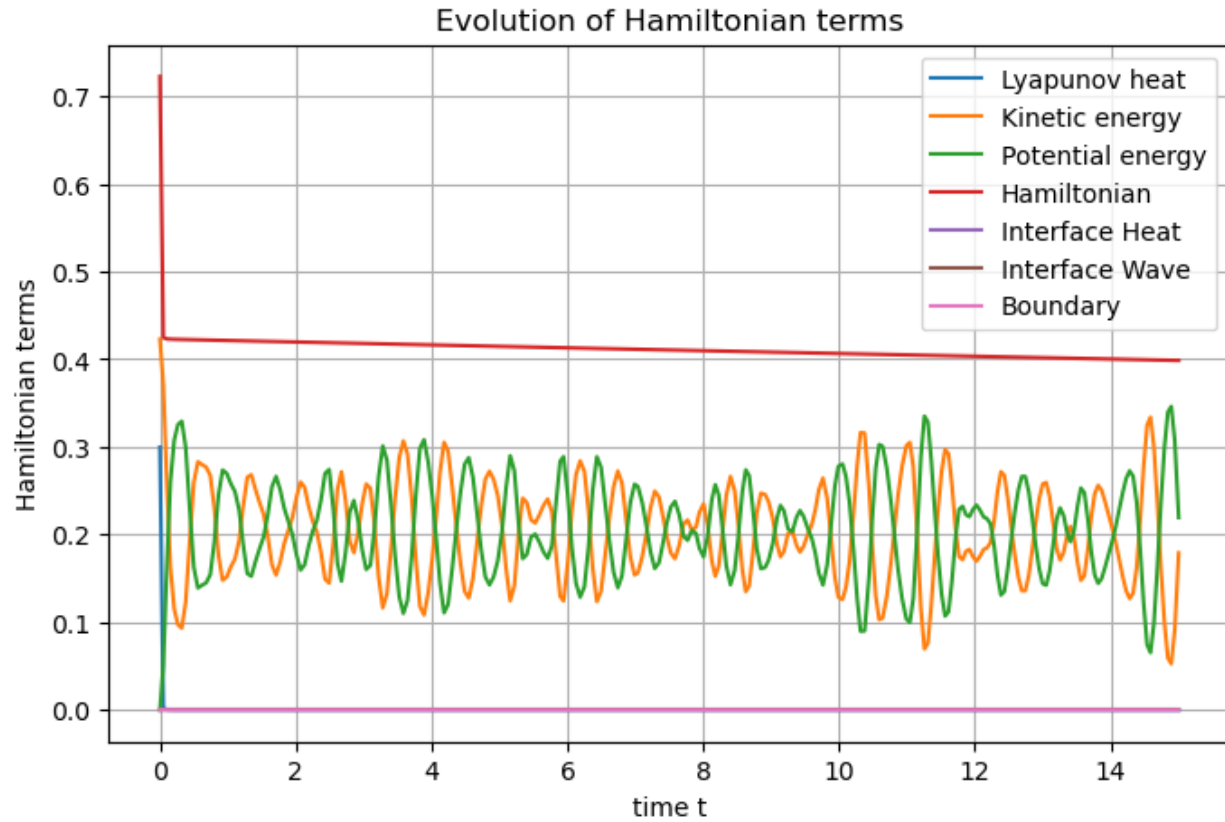
# Plot the Hamiltonian and save the output
hw.plot_Hamiltonian(save_figure=True, filename="Hamiltonian_Heat"+str(heat_region)+"_Wave
↪ "+str(wave_region)+"_2D.png")

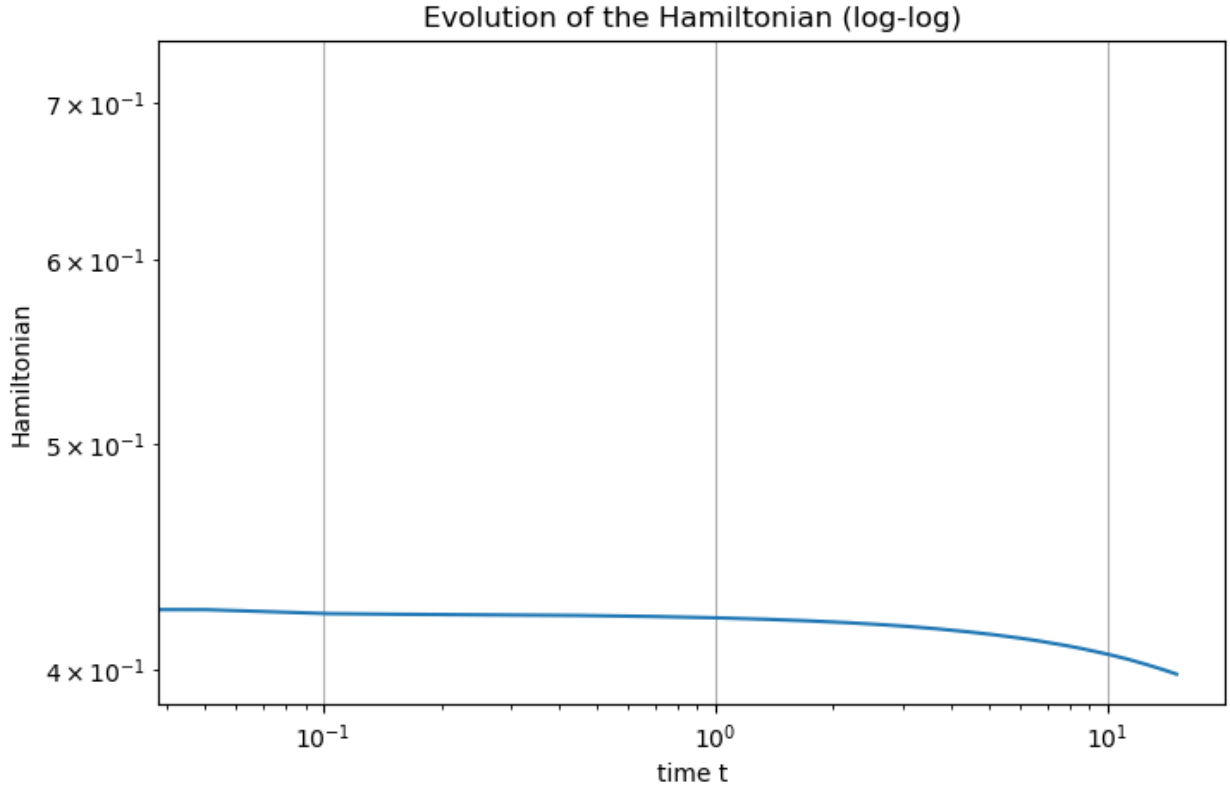
# Plot the Hamiltonian in log-log scale
t = hw.solution["t"]
Hamiltonian = hw.get_Hamiltonian()
```

(continues on next page)

(continued from previous page)

```
import matplotlib.pyplot as plt
fig = plt.figure(figsize=[8, 5])
ax = fig.add_subplot(111)
ax.loglog(t, Hamiltonian)
ax.grid(axis="both")
ax.set_xlabel("time t")
ax.set_ylabel("Hamiltonian")
ax.set_title("Evolution of the Hamiltonian (log-log)")
plt.show()
```





2.3.5 The shallow water equation

Setting

The objective of this example is to show how to deal with **non-linearity**.

Let us consider a bounded domain $\Omega \subset \mathbb{R}^2$. The shallow water equations are constituted of two conservation laws

$$\begin{pmatrix} \partial_t h \\ \partial_t p \end{pmatrix} = \begin{bmatrix} 0 & -\text{div} \\ -\text{grad} & \frac{1}{h} G(\omega) \end{bmatrix} \begin{pmatrix} e_h \\ e_p \end{pmatrix},$$

where h is the height of the fluid, v is the velocity, ρ is the fluid density (supposed constant), $p := \rho v$ is the linear momentum, $\omega := \text{curl}_{2D}(v) := \partial_x v_y - \partial_y v_x$ is the vorticity, $G(\omega) := \rho \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \omega$, $e_h = \frac{1}{2} \rho \|v\|^2 + \rho gh$ is the total pressure and $e_p = hv$ is the volumetric flow of the fluid. Thus, the first line of the matrix equation represents the conservation of the mass (or volume, since the fluid is assumed to be incompressible) and the second represents the conservation of linear momentum.

Port-Hamiltonian framework

One can define the system Hamiltonian (or total energy) as a functional of h and p , which are thus called energy variables

$$\mathcal{H}(h, p) := \frac{1}{2} \int_{\Omega} \frac{h(t, x) \|p(t, x)\|^2}{\rho} + \rho gh^2(t, x) dx.$$

The co-energy variables can be computed from the variational derivative of the Hamiltonian such that

$$\begin{aligned} e_h &= \delta_h \mathcal{H} = \frac{1}{2} \rho \|v\|^2 + \rho gh, \\ e_p &= \delta_p \mathcal{H} = hv. \end{aligned}$$

The time-derivative of the Hamiltonian can then be obtained computed and depends only on the boundary variables

$$\frac{d}{dt}\mathcal{H} = - \int_{\partial\Omega} e_h(t, s) e_p(t, s) \cdot n(s) ds,$$

which enables to define collocated control and observation distributed ports along the boundary $\partial\Omega$. For example, one may define

$$\begin{aligned} u_{\partial} &= -e_p \cdot n, \\ y_{\partial} &= e_h, \end{aligned}$$

and the power-balance is given by a product between input and output boundary ports. The system is lossless, and conservative in the absence of control.

Structure-preserving discretization

First, let us multiply the linear momentum conservation equation by h .

Let us consider sufficiently regular test functions φ and Φ on Ω , and ψ test functions at the boundary $\partial\Omega$. The weak form of the previous equations reads

$$\begin{cases} (\partial_t h, \varphi)_{L^2} &= -(\operatorname{div}(h e_p), \varphi)_{L^2}, \\ (h \partial_t p, \Phi)_{(L^2)^2} &= -(h \operatorname{grad}(e_h), \Phi)_{(L^2)^2} + \left(\operatorname{curl}_{2D}(p) \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} e_p, \Phi \right)_{(L^2)^2}, \\ (y_{\partial}, \psi)_{\partial\Omega} &= (e_h, \psi)_{\partial\Omega}. \end{cases}$$

Applying integration by parts on the first line leads to

$$\begin{cases} (\partial_t h, \varphi)_{L^2} &= (h e_p, \operatorname{grad}(\varphi))_{L^2} + (h u_{\partial}, \varphi)_{\partial\Omega}, \\ (h \partial_t p, \Phi)_{(L^2)^2} &= -(h \operatorname{grad}(e_h), \Phi)_{(L^2)^2} + \left(\operatorname{curl}_{2D}(p) \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} e_p, \Phi \right)_{(L^2)^2}, \\ (y_{\partial}, \psi)_{\partial\Omega} &= (e_h, \psi)_{\partial\Omega}. \end{cases}$$

Furthermore, the weak form of the constitutive relations write

$$\begin{cases} (e_h, \varphi)_{L^2} &= (\rho g h, \varphi)_{L^2} + \left(\frac{\|p\|^2}{2\rho}, \varphi \right)_{L^2}, \\ (e_p, \Phi)_{(L^2)^2} &= \left(\frac{p}{\rho}, \Phi \right)_{(L^2)^2}. \end{cases}$$

Now, let us choose three finite families $(\varphi^i)_{1 \leq i \leq N_h} \subset H^1(\Omega)$, $(\Phi^k)_{1 \leq k \leq N_p} \subset (L^2(\Omega))^2$ and $(\psi^m)_{1 \leq m \leq N_{\partial}}$ and project the weak formulations on them: for all $1 \leq i \leq N_h$, all $1 \leq k \leq N_p$ and all $1 \leq m \leq N_{\partial}$

$$\begin{cases} \sum_{j=1}^{N_h} \frac{d}{dt} h^j (\varphi^j, \varphi^i)_{L^2} &= \sum_{\ell=1}^{N_p} e_p^{\ell} (h^d \Phi^{\ell}, \operatorname{grad}(\varphi^i))_{L^2} + \sum_{n=1}^{N_{\partial}} u_{\partial}^n (h^d \psi^n, \varphi^i)_{\partial\Omega}, \\ \sum_{\ell=1}^{N_p} \frac{d}{dt} p^{\ell} (h^d \Phi^{\ell}, \Phi^k)_{(L^2)^2} &= - \sum_{j=1}^{N_h} e_h^j (h^d \operatorname{grad}(\varphi^j), \Phi^k)_{(L^2)^2} \\ &\quad + \sum_{\ell=1}^{N_p} e_p^{\ell} \left(\operatorname{curl}_{2D}(p^d) \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \Phi^{\ell}, \Phi^k \right)_{(L^2)^2}, \\ \sum_{n=1}^{N_{\partial}} y_{\partial}^n (\psi^n, \psi^m)_{\partial\Omega} &= \sum_{j=1}^{N_h} e_h^j (\varphi^j, \psi^m)_{\partial\Omega}, \end{cases}$$

where $h^d := \sum_{i=1}^{N_h} h^i \varphi^i$ is the approximation of h and $p^d := \sum_{k=1}^{N_p} p^k \Phi^k$ is the approximation of p . The constitutive relations read for all $1 \leq i \leq N_h$ and all $1 \leq k \leq N_p$

$$\begin{cases} \sum_{j=1}^{N_h} e_h^j (\varphi^j, \varphi^i)_{L^2} &= \sum_{j=1}^{N_h} h^j (\rho g \varphi^j, \varphi^i)_{L^2} + \sum_{\ell=1}^{N_p} p^{\ell} \left(\frac{\Phi^{\ell} \cdot p^d}{2\rho}, \varphi^i \right)_{L^2}, \\ \sum_{\ell=1}^{N_p} e_p^{\ell} (\Phi^{\ell}, \Phi^k)_{(L^2)^2} &= \sum_{\ell=1}^{N_p} p^{\ell} \left(\frac{\Phi^{\ell}}{\rho}, \Phi^k \right)_{(L^2)^2}. \end{cases}$$

Defining \star the vector gathering the coefficient of the approximation of the variable \star in its appropriate finite family, one may write the discrete weak formulations in matrix notation

$$\begin{bmatrix} M_h & 0 & 0 \\ 0 & M_p[h^d] & 0 \\ 0 & 0 & M_\partial \end{bmatrix} \begin{pmatrix} \underline{h} \\ \underline{p} \\ -\underline{y}_\partial \end{pmatrix} = \begin{bmatrix} 0 & D[h^d] & B[h^d] \\ -D[h^d]^\top & G[p^d] & 0 \\ -B^\top & 0 & 0 \end{bmatrix} \begin{pmatrix} \underline{e}_h \\ \underline{e}_p \\ \underline{u}_\partial \end{pmatrix}.$$

where the matrices are given by

$$\begin{aligned} (M_h)_{ij} &:= (\varphi^j, \varphi^i)_{L^2} & (M_p[h^d])_{k\ell} &:= (h^d \Phi^\ell, \Phi^k)_{(L^2)^2}, \\ (D[h^d])_{i\ell} &:= (h^d \Phi^\ell, \text{grad}(\varphi^i))_{L^2}, & (B[h^d])_{in} &:= (h^d \psi^n, \varphi^i)_{\partial\Omega}, \end{aligned}$$

and

$$(M_\partial)_{mn} := (\psi^n, \psi^m)_{\partial\Omega}, \quad (B)_{in} := (\psi^n, \varphi^i)_{\partial\Omega}.$$

The constitutive relations read

$$\begin{bmatrix} M_h & 0 \\ 0 & M_p \end{bmatrix} \begin{pmatrix} \underline{e}_h \\ \underline{e}_p \end{pmatrix} = \begin{bmatrix} Q_h & P_h[h^d] \\ 0 & Q_p \end{bmatrix} \begin{pmatrix} \underline{h} \\ \underline{p} \end{pmatrix},$$

where the matrices are given by

$$\begin{aligned} (M_p)_{k\ell} &:= (\Phi^\ell, \Phi^k)_{(L^2)^2}, & (Q_h)_{ij} &:= (\rho g \varphi^j, \varphi^i)_{L^2}, \\ (P_h[h^d])_{i\ell} &:= \left(\frac{\Phi^\ell \cdot p^d}{2\rho}, \varphi^i \right)_{L^2}, & (Q_d)_{k\ell} &:= \left(\frac{\Phi^\ell}{\rho}, \Phi^k \right)_{(L^2)^2}. \end{aligned}$$

With these definition, one may prove the **discrete power balance**

$$\frac{d}{dt} \mathcal{H}^d(t) = \underline{u}_\partial^\top(t) M_\partial \underline{y}_\partial(t).$$

Simulation

The beggining is classical: first import, then create the dphs and set the domain.

```
# Import scrimp
import scrimp as S

# Init the distributed port-Hamiltonian system
swe = S.DPHS("real")

# Set the domain (using the built-in geometry `Rectangle`)
# Labels: Omega = 1, Gamma_Bottom = 10, Gamma_Right = 11, Gamma_Top = 12, Gamma_Left = 13
swe.set_domain(S.Domain("Rectangle", {"L": 2.0, "l": 0.5, "h": 0.1}))
```

Then the states and co-states.

```
# Define the states and costates
states = [
    S.State("h", "Fluid height", "scalar-field"),
    S.State("p", "Linear momentum", "vector-field"),
]
costates = [
```

(continues on next page)

(continued from previous page)

```

    S.CoState("e_h", "Pressure", states[0]),
    S.CoState("e_p", "Velocity", states[1]),
]

# Add them to the dphs
for state in states:
    swe.add_state(state)
for costate in costates:
    swe.add_costate(costate)

```

And the control ports.

```

# Define the control ports
control_ports = [
    S.Control_Port(
        "Boundary control 0",
        "U_0",
        "Normal velocity",
        "Y_0",
        "Fluid height",
        "scalar-field",
        region=10,
        position="effort",
    ),
    S.Control_Port(
        "Boundary control 1",
        "U_1",
        "Normal velocity",
        "Y_1",
        "Fluid height",
        "scalar-field",
        region=11,
        position="effort",
    ),
    S.Control_Port(
        "Boundary control 2",
        "U_2",
        "Normal velocity",
        "Y_2",
        "Fluid height",
        "scalar-field",
        region=12,
        position="effort",
    ),
    S.Control_Port(
        "Boundary control 3",
        "U_3",
        "Normal velocity",
        "Y_3",
        "Fluid height",
        "scalar-field",
        region=13,
    ),
]

```

(continues on next page)

(continued from previous page)

```

        position="effort",
    ),
]

# Add them to the dphs
for ctrl_port in control_ports:
    swe.add_control_port(ctrl_port)

```

Regarding the FEM, this is more challenging, as non-linearity are present. Nevertheless, let us stick to the way we choose until now: since the h -type variables will be derived, thus we choose continuous Galerkin approximations of order $k+1$. The other energy variable is taken as continuous Galerkin approximation of order k , while boundary terms are given by discontinuous Galerkin approximations of order k .

```

# Define the Finite Elements Method of each port
k = 1
FEMs = [
    S.FEM(states[0].get_name(), k+1, FEM="CG"),
    S.FEM(states[1].get_name(), k, FEM="CG"),
    S.FEM(control_ports[0].get_name(), k, "DG"),
    S.FEM(control_ports[1].get_name(), k, "DG"),
    S.FEM(control_ports[2].get_name(), k, "DG"),
    S.FEM(control_ports[3].get_name(), k, "DG"),
]

# Add them to the dphs
for FEM in FEMs:
    swe.add_FEM(FEM)

```

The parameters are *physically meaningful*!

```

# Define physical parameters
rho = 1000.
g = 10.
parameters = [
    S.Parameter("rho", "Mass density", "scalar-field", f"{rho}", "h"),
    S.Parameter("g", "Gravity", "scalar-field", f"{g}", "h"),
]

# Add them to the dphs
for parameter in parameters:
    swe.add_parameter(parameter)

```

Here are the difficult part. We need to define the weak form of each block matrices, and take non-linearities into account. To do so, the GFWL of GetFEM is transparent, but it is mandatory to say to **SCRIMP** that the **Brick** is non-linear, using the keyword `linear=False`. It is also possible to ask for this block to be considered *explicitly* in the time scheme (*i.e.* it will be computed with the previous time step values and be considered as a right-hand side), as done for the gyroscopic term below, using the keyword `explicit=True`.

```

# Define the pHs via `Brick` == non-zero block matrices == variational terms
# Some macros for the sake of readability
swe.gf_model.add_macro('div(v)', 'Trace(Grad(v))')
swe.gf_model.add_macro('Rot', '[[0,1],[-1,0]]')
swe.gf_model.add_macro('Curl2D(v)', 'div(Rot*v)')

```

(continues on next page)

(continued from previous page)

```

swe.gf_model.add_macro('Gyro(v)', 'Curl2D(v)*Rot')
bricks = [
    # Define the mass matrices of the left-hand side of the "Dirac structure" (position=
    ↪ "flow")
    S.Brick("M_h", "h * Test_h", [1], dt=True, position="flow"),
    S.Brick("M_p", "h * p . Test_p", [1], dt=True, linear=False, position="flow"),
    S.Brick("M_Y_0", "Y_0 * Test_Y_0", [10], position="flow"),
    S.Brick("M_Y_1", "Y_1 * Test_Y_1", [11], position="flow"),
    S.Brick("M_Y_2", "Y_2 * Test_Y_2", [12], position="flow"),
    S.Brick("M_Y_3", "Y_3 * Test_Y_3", [13], position="flow"),

    # Define the first line of the right-hand side of the "Dirac structure" (position=
    ↪ "effort")
    S.Brick("-D^T", "h * e_p . Grad(Test_h)", [1], linear=False, position="effort"),
    # with the boundary control
    S.Brick("B_0", "- U_0 * Test_h", [10], position="effort"),
    S.Brick("B_1", "- U_1 * Test_h", [11], position="effort"),
    S.Brick("B_2", "- U_2 * Test_h", [12], position="effort"),
    S.Brick("B_3", "- U_3 * Test_h", [13], position="effort"),
    # Define the second line of the right-hand side of the "Dirac structure" (position=
    ↪ "effort")
    S.Brick("D", "- Grad(e_h) . Test_p * h", [1], linear=False, position="effort"),
    # with the gyroscopic term (beware that "Curl" is not available in the GWFL of ↪
    ↪ getfem)
    S.Brick("G", "(Gyro(p) * e_p) . Test_p", [1], linear=False, explicit=True, position=
    ↪ "effort"),
    # Define the third line of the right-hand side of the "Dirac structure" (position=
    ↪ "effort")
    S.Brick("C_0", "- e_h * Test_Y_0", [10], position="effort"),
    S.Brick("C_1", "- e_h * Test_Y_1", [11], position="effort"),
    S.Brick("C_2", "- e_h * Test_Y_2", [12], position="effort"),
    S.Brick("C_3", "- e_h * Test_Y_3", [13], position="effort"),

    ## Define the constitutive relations (position="constitutive", the default value)
    # For e_h: first the mass matrix WITH A MINUS because we want an implicit ↪
    ↪ formulation  $0 = - M e_h + F(h)$ 
    S.Brick("-M_e_h", "- e_h * Test_e_h", [1]),
    # second the linear part as a linear brick
    S.Brick("Q_h", "rho * g * h * Test_e_h", [1]),
    # third the non-linear part as a non-linear brick (linear=False)
    S.Brick("P_h", "0.5 * (p . p) / rho * Test_e_h", [1], linear=False),
    # For e_p: first the mass matrix WITH A MINUS because we want an implicit ↪
    ↪ formulation  $0 = - M e_p + F(p)$ 
    S.Brick("-M_e_p", "- e_p . Test_e_p", [1]),
    # second the LINEAR brick
    S.Brick("Q_p", "p / rho . Test_e_p", [1]),
]
for brick in bricks:
    swe.add_brick(brick)

```

As we just look at how it works, let us consider a step in the height, no initial velocity, and homogeneous Neumann boundary condition. This should look like a dam break experiment in a rectangular tank.

Remark: note the use of `np`, *i.e.* numpy, in the definition of the initial height h_0 .

```
## Initialize the problem
swe.set_control("Boundary control 0", "0.")
swe.set_control("Boundary control 1", "0.")
swe.set_control("Boundary control 2", "0.")
swe.set_control("Boundary control 3", "0.")

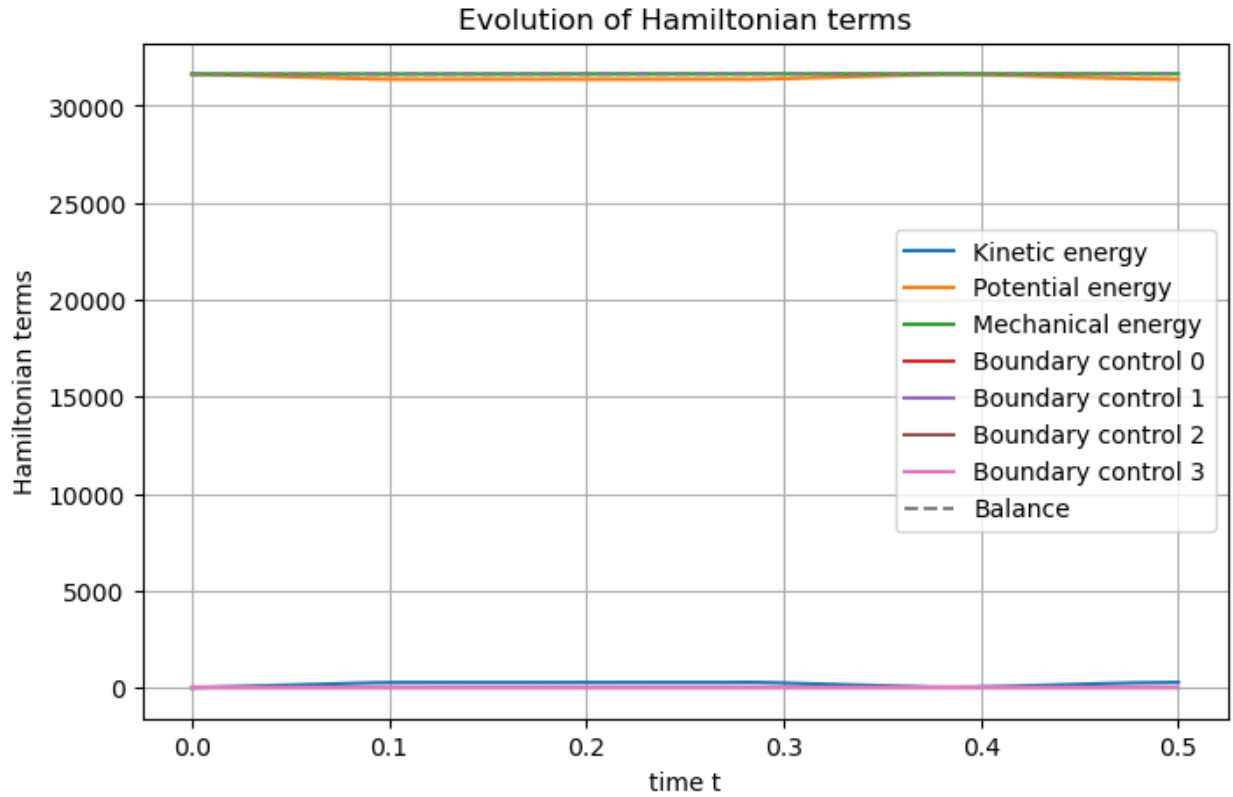
# Set the initial data
swe.set_initial_value("h", "3. - (np.sign(x-0.5)+1)/3.")
swe.set_initial_value("p", f"[ 0., 0.]")

## Solve in time
# Define the time scheme
swe.set_time_scheme(
    ts_type="bdf",
    ts_bdf_order=4,
    t_f=0.5,
    dt=0.0001,
    dt_save=0.01,
)

# Solve the system in time
swe.solve()
```

The Hamiltonian are then defined, computed, and shown.

```
## Post-processing
# Set Hamiltonian's name
swe.hamiltonian.set_name("Mechanical energy")
# Define Hamiltonian terms
terms = [
    S.Term("Kinetic energy", "0.5*h*p.p/rho", [1]),
    S.Term("Potential energy", "0.5*rho*g*h*h", [1]),
]
# Add them to the Hamiltonian
for term in terms:
    swe.hamiltonian.add_term(term)
# Plot the Hamiltonian
swe.plot_Hamiltonian(save_figure=True, filename="Hamiltonian_Inviscid_Shallow_Water_2D.
→png")
```



2.4 Notebooks

Some examples coming from our [publications](#) are available in [jupyter notebook](#) format inside the `notebooks` folder in `examples`.

2.4.1 Install jupyter

To begin with, you'll need to install jupyter.

It can be done in the `scrimp` environment with:

1. `conda activate scrimp`
2. `conda install jupyter ipykernel`
3. `python -m ipykernel install --user --name scrimp --display-name "Python (scrimp)"`

2.4.2 Run jupyter

Then, run in the `notebooks` folder:

`jupyter notebook &`

And choose a notebook to launch.

If you aim at learning **SCRIMP**, the preferred order to study the notebooks is:

- Wave_1D
- Wave_2D
- Heat_2D

- Wave_2D_CoEnergy
- Heat_Wave_2D
- Shallow_water_2D

2.5 Graphical User Interface

As to increase the facility to perform simulations from scratch, a Graphical User Interface (GUI) is available to help beginners and confirmed users to scrimp and save time by sketching a first launchable script.

#TO COMPLETE#

2.6 Bibliography

Port-Hamiltonian systems is an ever-growing research area as it proposes a powerful framework for the control of multi-physics systems.

The following list of publications presents the main results of ours behind **SCRIMP**.

2.6.1 Articles

- Haïne, Ghislain and Matignon, Denis and Serhani, Anass. **Numerical Analysis of a Structure-Preserving Space-Discretization for an Anisotropic and Heterogeneous Boundary Controlled N-Dimensional Wave Equation As a Port-Hamiltonian System.** (2023) *International Journal of Numerical Analysis and Modeling*, 20 (1). 92-133. DOI:10.4208/ijnam2023-1005
- Haïne, Ghislain and Matignon, Denis and Monteghetti, Florian. **Long-time behavior of a coupled heat-wave system using a structure-preserving finite element method.** (2022) *Mathematical Reports*, 22 (1-2). 187-215. PDF
- Mora, Luis A. and Le Gorrec, Yann and Matignon, Denis and Ramirez, Hector and Yuz, Juan I.. **On port-Hamiltonian formulations of 3-dimensional compressible Newtonian fluids.** (2021) *Physics of Fluids*, 33 (11). 117117. DOI:10.1063/5.0067784
- Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis and Lefèvre, Laurent. **A Partitioned Finite Element Method for power-preserving discretization of open systems of conservation laws.** (2021) *IMA Journal of Mathematical Control and Information*, 38 (2). 493-533. DOI:10.1093/imamci/dnaa038
- Brugnoli, Andrea and Haïne, Ghislain and Serhani, Anass and Vasseur, Xavier. **Numerical Approximation of Port-Hamiltonian Systems for Hyperbolic or Parabolic PDEs with Boundary Control.** (2021) *Journal of Applied Mathematics and Physics*, 09 (06). 1278-1321. DOI:10.4236/jamp.2021.96088
- Brugnoli, Andrea and Alazard, Daniel and Pommier-Budinger, Valérie and Matignon, Denis. **Port-Hamiltonian flexible multibody dynamics.** (2021) *Multibody System Dynamics*, 51 (3). 343-375. DOI:10.1007/s11044-020-09758-6
- Brugnoli, Andrea and Alazard, Daniel and Pommier-Budinger, Valérie and Matignon, Denis. **A port-Hamiltonian formulation of linear thermoelasticity and its mixed finite element discretization.** (2021) *Journal of Thermal Stresses*, 44 (6). 643-661. DOI:10.1080/01495739.2021.1917322
- Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis and Pommier-Budinger, Valérie. **Port-Hamiltonian model of two-dimensional shallow water equations in moving containers.** (2020) *IMA Journal of Mathematical Control and Information*, 37 (4). 1348-1366. DOI:10.1093/imamci/dnaa016
- Brugnoli, Andrea and Alazard, Daniel and Pommier-Budinger, Valérie and Matignon, Denis. **Port-Hamiltonian formulation and symplectic discretization of plate models Part I: Mindlin model for thick plates.** (2019) *Applied Mathematical Modelling*, 75. 940-960. DOI:10.1016/j.apm.2019.04.035

- Brugnoli, Andrea and Alazard, Daniel and Pommier-Budinger, Valérie and Matignon, Denis. **Port-Hamiltonian formulation and symplectic discretization of plate models. Part II : Kirchhoff model for thin plates.** (2019) *Applied Mathematical Modelling*, 75. 961-981. DOI:10.1016/j.apm.2019.04.036
- Aoues, Saïd and Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis and Alazard, Daniel. **Modeling and Control of a Rotating Flexible Spacecraft: A Port-Hamiltonian Approach.** (2019) *IEEE Transactions on Control Systems Technology*, 27 (1). 355-362. DOI:10.1109/TCST.2017.2771244
- Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis and Pommier-Budinger, Valérie. **A port-Hamiltonian model of liquid sloshing in moving containers and application to a fluid-structure system.** (2017) *Journal of Fluids and Structures*, 69. 402-427. DOI:10.1016/j.jfluidstructs.2016.12.007

2.6.2 Book Chapters

- Haine, Ghislain and Matignon, Denis. **Structure-Preserving Discretization of a Coupled Heat-Wave System, as Interconnected Port-Hamiltonian Systems.** (2021) In: *Geometric Science of Information*. Springer International Publishing AG, 191-199. DOI:10.1007/978-3-030-80209-7_22
- Serhani, Anass and Matignon, Denis and Haine, Ghislain. **A Partitioned Finite Element Method for the Structure-Preserving Discretization of Damped Infinite-Dimensional Port-Hamiltonian Systems with Boundary Control.** (2019) In: *Geometric Science of Information*. Springer International Publishing AG, Cham, Suisse, 549-558. DOI:10.1007/978-3-030-26980-7_57

2.6.3 Proceedings

- Brugnoli, Andrea and Haine, Ghislain and Matignon, Denis. **Explicit structure-preserving discretization of port-Hamiltonian systems with mixed boundary control.** (2022) In: 25th International Symposium on Mathematical Theory of Networks and Systems (MTNS 2022), 12 September 2022 - 16 September 2022 (Bayreuth, Germany).
- Haine, Ghislain and Matignon, Denis and Monteghetti, Florian. **Structure-preserving discretization of Maxwell's equations as a port-Hamiltonian system.** (2022) In: 25th International Symposium on Mathematical Theory of Networks and Systems (MTNS 2022), 12 September 2022 - 16 September 2022 (Bayreuth, Germany).
- Haine, Ghislain and Lefèvre, Laurent and Matignon, Denis. **PFEM: a mixed structure-preserving discretization method for port-Hamiltonian systems.** (2022) In: International Workshop on Operator Theory and its Applications, 6 September 2022 - 10 September 2022 (Cracovie, Poland).
- Brugnoli, Andrea and Matignon, Denis. **A port-Hamiltonian formulation for the full von-Kármán plate model.** (2022) In: 10th European Nonlinear Dynamics Conference (ENOC), 17 July 2022 - 22 July 2022 (Lyon, France).
- Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis and Lefèvre, Laurent. **A Partitioned Finite Element Method (PFEM) for power-preserving discretization of port-Hamiltonian systems (pHs) with polynomial nonlinearity.** (2022) In: European Nonlinear Dynamics Conference (ENOC 2022), 17 July 2022 - 22 July 2022 (Lyon, France).
- Hélie, Thomas and Matignon, Denis. **Nonlinear damping laws preserving the eigenstructure of the momentum space for conservative linear PDE problems: a port-Hamiltonian modelling.** (2022) In: 10th European Nonlinear Dynamics Conference (ENOC), 17 July 2022 - 22 July 2022 (Lyon, France).
- Bendimerad-Hohl, Antoine and Haine, Ghislain and Matignon, Denis and Maschke, Bernhard. **Structure-preserving discretization of a coupled Allen-Cahn and heat equation system.** (2022) In: 4th IFAC Workshop on Thermodynamic Foundations of Mathematical Systems Theory - TFMST 2022, 25 July 2022 - 27 July 2022 (Montreal, Canada).
- Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis and Lefèvre, Laurent. **Dissipative Shallow Water Equations: a port-Hamiltonian formulation.** (2021) In: Lagrangian and Hamiltonian Methodes for Nonlinear

Control (7th LHMNC 2021), 11 October 2021 - 13 October 2021 (Berlin, Germany).

- Haine, Ghislain and Matignon, Denis. **Incompressible Navier-Stokes Equation as port-Hamiltonian systems: velocity formulation versus vorticity formulation.** (2021) In: Lagrangian and Hamiltonian Methodes for Nonlinear Control (7th LHMNC 2021), 11 October 2021 - 13 October 2021 (Berlin, Germany).
- Brugnoli, Andrea and Rashad, Ramy and Califano, Federico and Stramigioli, Stefano and Matignon, Denis. **Mixed finite elements for port-Hamiltonian models of von Kármán beams.** (2021) In: Lagrangian and Hamiltonian Methodes for Nonlinear Control (LHMNLC 2021), 11 October 2021 - 13 October 2021 (Berlin, Germany).
- Brugnoli, Andrea and Alazard, Daniel and Pommier-Budinger, Valérie and Matignon, Denis. **Structure-preserving discretization of port-Hamiltonian plate models.** (2021) In: Mathematical Theory of Networks and Systems, August 2021 - August 2021 (Cambridge, United Kingdom).
- Brugnoli, Andrea and Matignon, Denis and Haine, Ghislain and Serhani, Anass. **Numerics for Physics-Based PDEs with Boundary Control: the Partitioned Finite Element Method for Port-Hamiltonian Systems.** (2021) In: SIAM Conference on Computational Science and Engineering (CSE21), 1 March 2021 - 5 March 2021 (Virtual conference).
- Brugnoli, Andrea and Cardoso-Ribeiro, Flávio Luiz and Haine, Ghislain and Kotyczka, Paul. **Partitioned finite element method for structured discretization with mixed boundary conditions.** (2020) In: 21th IFAC World Congress, 11 July 2020 - 17 July 2020 (Berlin, Germany).
- Mora, Luis A. and Gorrec, Yann Le and Matignon, Denis and Ramirez, Hector and Yuz, Juan I.. **About Dissipative and Pseudo Port-Hamiltonian Formulations of Irreversible Newtonian Compressible Flows.** (2020) In: The 21st World Congress of The International Federation of Automatic Control (IFAC 2020), 11 July 2020 - 17 July 2020 (Virtual event, Germany).
- Payen, Gabriel and Matignon, Denis and Haine, Ghislain. **Modelling and structure-preserving discretization of Maxwell's equations as port-Hamiltonian system.** (2020) In: The 21st World Congress of The International Federation of Automatic Control (IFAC 2020), 11 July 2020 - 17 July 2020 (Virtual event, Germany).
- Treton, Anne-Sophie and Haine, Ghislain and Matignon, Denis. **Modelling the 1D piston problem as interconnected port-Hamiltonian systems.** (2020) In: The 21st World Congress of The International Federation of Automatic Control (IFAC 2020), 11 July 2020 - 17 July 2020 (Virtual event, Germany).
- Brugnoli, Andrea and Alazard, Daniel and Pommier-Budinger, Valérie and Matignon, Denis. **Interconnection of the Kirchhoff plate within the port-Hamiltonian framework.** (2020) In: 2019 IEEE 58th Conference on Decision and Control (CDC), 11 December 2019 - 13 December 2019 (Nice, France).
- Cardoso-Ribeiro, Flávio Luiz and Brugnoli, Andrea and Matignon, Denis and Lefèvre, Laurent. **Port-Hamiltonian modeling, discretization and feedback control of a circular water tank.** (2020) In: 2019 IEEE 58th Conference on Decision and Control (CDC), 11 December 2019 - 13 December 2019 (Nice, France).
- Serhani, Anass and Haine, Ghislain and Matignon, Denis. **Anisotropic heterogeneous n-D heat equation with boundary control and observation : I. Modeling as port-Hamiltonian system.** (2019) In: 3rd IFAC Workshop on Thermodynamic Foundations for a Mathematical Systems Theory (TFMST 2019), 3 July 2019 - 5 July 2019 (Louvain-la-Neuve, Belgium).
- Serhani, Anass and Haine, Ghislain and Matignon, Denis. **Anisotropic heterogeneous n-D heat equation with boundary control and observation : II. Structure-preserving discretization.** (2019) In: 3rd IFAC Workshop on Thermodynamic Foundations for a Mathematical Systems Theory (TFMST 2019), 3 July 2019 - 5 July 2019 (Louvain-la-Neuve, Belgium).
- Brugnoli, Andrea and Alazard, Daniel and Pommier-Budinger, Valérie and Matignon, Denis. **Partitioned finite element method for the Mindlin plate as a port-Hamiltonian system.** (2019) In: 3rd IFAC Workshop on Control of Systems Governed by Partial Differential Equations CPDE 2019, 20 May 2019 - 24 May 2019 (Oaxaca, Mexico). (Unpublished)

- Serhani, Anass and Matignon, Denis and Haine, Ghislain. **Partitioned Finite Element Method for port-Hamiltonian systems with Boundary Damping: Anisotropic Heterogeneous 2D wave equations.** (2019) In: 3rd IFAC/IEEE CSS Workshop on Control of Systems Governed by Partial Differential Equations CPDE and XI Workshop Control of Distributed Parameter Systems (CDPS 2019), 20 May 2019 - 24 May 2019 (Oaxaca, Mexico).
- Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis and Lefèvre, Laurent. **A structure-preserving Partitioned Finite Element Method for the 2D wave equation.** (2018) In: 6th IFAC Workshop on Lagrangian and Hamiltonian Methods for Nonlinear Control, 1 May 2018 - 4 May 2018 (Valparaíso, Chile).
- Alazard, Daniel and Aoues, Saïd and Cardoso-Ribeiro, Flávio Luiz and Matignon, Denis. **Disturbance rejection for a rotating flexible spacecraft: a port-Hamiltonian approach.** (2018) In: 6th IFAC Workshop on Lagrangian and Hamiltonian Methods for Nonlinear Control, 1 May 2018 - 4 May 2018 (Valparaíso, Chile).
- Serhani, Anass and Matignon, Denis and Haine, Ghislain. **Structure-Preserving Finite Volume Method for 2D Linear and Non-Linear Port-Hamiltonian Systems.** (2018) In: 6th IFAC Workshop on Lagrangian and Hamiltonian Methods for Nonlinear Control, 1 May 2018 - 4 May 2018 (Valparaíso, Chile).

2.7 Code documentation

This part of the documentation is generated automatically from the python source using [SPHINX](#).

2.7.1 Folders

`scrimp.examples`

We provide some examples coming from our [publications](#).

The equations are explained [here](#).

Wave

Heat

Heat-Wave coupling

Shallow water

`scrimp.utils`

This folder contains useful functions that are beyond the port-Hamiltonian framework used in **SCRIMP**.

Config

- file: `utils/config.py`
- authors: Ghislain Haine
- date: 23 jun. 2023
- brief: functions to configure SCRIMP

`scrimp.utils.config.set_paths(path=None)`

Set the default path of `scrimp`

Args:

path (str): the path

`scrimp.utils.config.set_verbose(verbose=1)`

Set the verbosity level of scrimp (0: quiet, 1: info, 2: debug)

In *quiet* mode, debug are saved in a log file.

Args:

verbose (int): the level of verbosity, defaults to 1

`scrimp.utils.config.set_verbose_gf(verbose)`

Set the verbosity level of getfem

Args:

verbose (int): the level of verbosity

Linear algebra

Mesh

`scrimp.sandbox`

The sandbox folder is the **recommended** folder to work in.

It already contains the example of the 1D wave equation presented [here](#).

2.7.2 Distributed port-Hamiltonian system

2.7.3 Domain

2.7.4 Hamiltonian / Term

2.7.5 Port / Parameter

2.7.6 State

2.7.7 Co-state

2.7.8 Control

2.7.9 FEM

2.7.10 Brick

3.1 Development

Please report bug at: ghislain.haine@isae.fr, Giuseppe.Ferraro@isae-superaero.fr

Current developers: Antoine Bendhimerad-Hohl, Giuseppe Ferraro, Michel Fournié, Ghislain Haine

Past: Andrea Brugnoli, Melvin Chopin, Florian Monteghetti, Anass Serhani, Xavier Vasseur

Please read the [LICENSE](#)

3.2 Funding

- ANR Project [IMPACTS](#) – IMplicit Port-hAmiltonian ConTrol Systems
- AID School Project [FAMAS](#) – Fast & Accurate MAXwell Solver
- ANR-DFG Project [INFIDHEM](#) – INterconnected inFinite-Dimensional systems for HEterogeneous Media

3.3 Third-party

The two **main** libraries used as core for SCRIMP are:

- [GetFEM](#) – An open-source finite element library
- [PETSc](#) – The Portable, Extensible Toolkit for Scientific Computation

Meshing is facilitated using (although not mandatory) [GMSH](#) – A three-dimensional finite element mesh generator

Post-processing visualization is encouraged via [ParaView](#) – Post-processing visualization engine

and finally, SCRIMP also needs for some routines

- [matplotlib](#) – Visualization with Python
- [numpy](#) – A well-known package for scientific computing

One of our choice for IDE is [Spyder](#) – A scientific Python development environment

3.4 How to cite SCRIMP?

Ferraro G, Fournié M, Haine G. *Simulation and control of interactions in multi-physics, a Python package for port-Hamiltonian systems*. **IFAC-PapersOnLine**, 2024;58(6):119–24.

```
@article{Ferraro_2024,  
  title={{Simulation and control of interactions in multi-physics, a Python package for_  
↪port-Hamiltonian systems}},  
  volume={58},  
  ISSN={2405-8963},  
  DOI={10.1016/j.ifacol.2024.08.267},  
  number={6},  
  journal={IFAC-PapersOnLine},  
  publisher={Elsevier BV},  
  author={Ferraro, Giuseppe and Fournié, Michel and Haine, Ghislain},  
  year={2024},  
  pages={119--124}  
}
```

PYTHON MODULE INDEX

S

`scrimp.utils.config`, [55](#)

INDEX

M

module

 scrimp.utils.config, [55](#)

S

scrimp.utils.config

 module, [55](#)

set_paths() (*in module scrimp.utils.config*), [55](#)

set_verbose() (*in module scrimp.utils.config*), [55](#)

set_verbose_gf() (*in module scrimp.utils.config*), [56](#)