

Machine Design Test 1

June 15, 2022

Gabe Morris

```
[1]: # Notebook Preamble
import sympy as sp
import numpy as np
import matplotlib.pyplot as plt
from IPython.display import display, Markdown

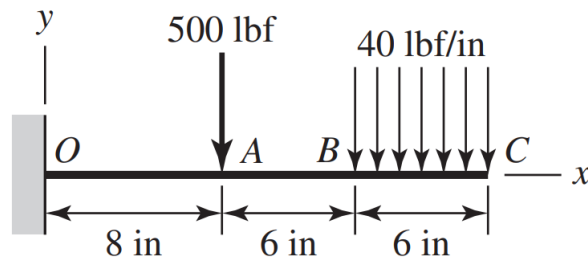
plt.style.use('maroon_ipynb.mplstyle')
```

Contents

1	Problem 3-6	3
1.1	Given	3
1.2	Find	3
1.3	Solution	3
1.3.1	Reaction Forces	3
1.3.2	Bending and Moment Diagram	4
2	Problem 3-17	7
2.1	Given	7
2.2	Find	7
2.3	Solution	7
2.3.1	Part A	7
2.3.2	Part D	8
3	Problem 3-72	10
3.1	Given	10
3.2	Find	10
3.3	Solution	10
4	Problem 3-82	11
4.1	Given	11
4.2	Find	11
4.3	Solution	12
4.3.1	Part A	12
4.3.2	Part B	13
4.3.3	Part C	13
4.3.4	Part D	14
4.3.5	Part E	15

1 Problem 3-6

1.1 Given

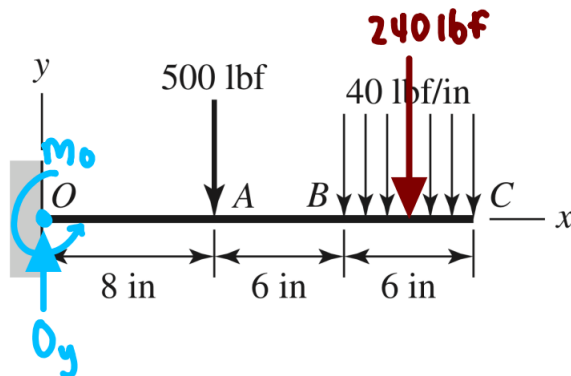


1.2 Find

Find the reaction forces and plot the shear and bending diagram.

1.3 Solution

1.3.1 Reaction Forces

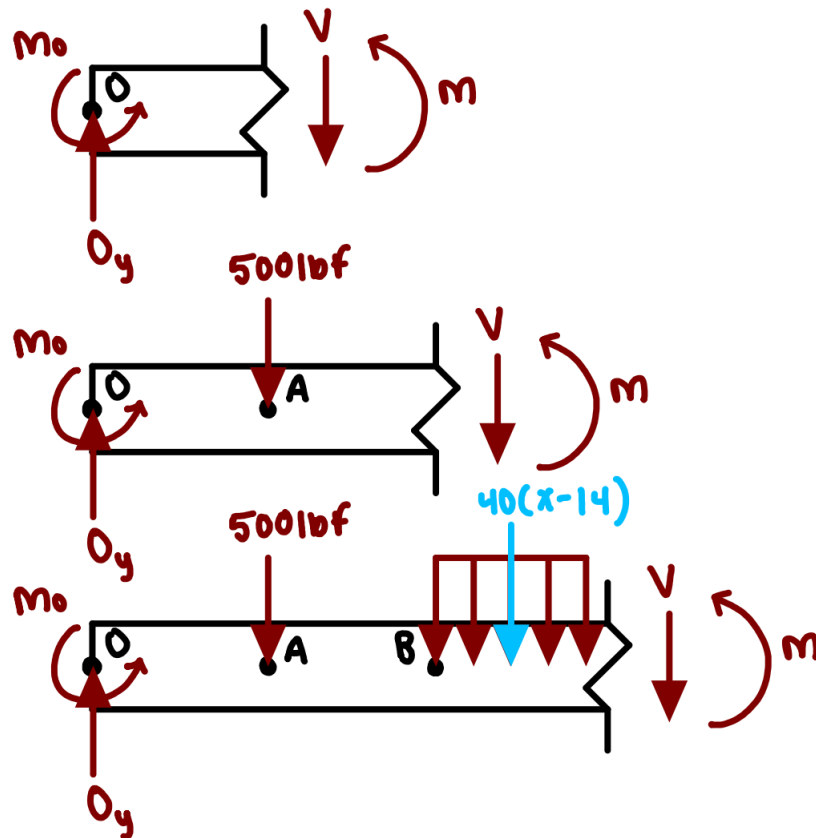


```
[2]: # Getting the reaction forces
Oy_sym, Mo_sym = sp.symbols('O_y M_o')
Oy = 240 + 500
Mo = 500*8 + 240*17
display(sp.Eq(Oy_sym, Oy), sp.Eq(Mo_sym, Mo)) # lbf and lbf*in
```

$$O_y = 740$$

$$M_o = 8080$$

1.3.2 Bending and Moment Diagram



The equation may be described as the piecewise relationship coded below.

```
[3]: V, M, x = sp.symbols('V M x')

# From 0 to A
V1 = Oy
M1 = -Mo + Oy*x

# From A to B
V2 = Oy - 500
M2 = -Mo + Oy*x - 500*(x - 8)

# From B to C
V3 = Oy - 500 - 40*(x - 14)
M3 = -Mo + Oy*x - 500*(x - 8) - 40*(x - 14)*(x - 14)/2

eq1 = sp.Eq(V, sp.Piecewise((V1, (x >= 0) & (x < 8)), (V2, (x >= 8) & (x < 14)), (V3, (x >= 14) & (x <= 20))))
eq2 = sp.Eq(M, sp.Piecewise((M1, (x >= 0) & (x < 8)), (M2, (x >= 8) & (x < 14)), (M3, (x >= 14) & (x <= 20))))
```

```
display(eq1, eq2)
```

$$V = \begin{cases} 740 & \text{for } x \geq 0 \wedge x < 8 \\ 240 & \text{for } x \geq 8 \wedge x < 14 \\ 800 - 40x & \text{for } x \geq 14 \wedge x \leq 20 \end{cases}$$

$$M = \begin{cases} 740x - 8080 & \text{for } x \geq 0 \wedge x < 8 \\ 240x - 4080 & \text{for } x \geq 8 \wedge x < 14 \\ 240x - \frac{(x-14)(40x-560)}{2} - 4080 & \text{for } x \geq 14 \wedge x \leq 20 \end{cases}$$

The important key points for shear are shown in the piecewise function expression above. The key points for the bending moment are,

```
[4]: points = ['O', 'A', 'B', 'C']
     values = [0, 8, 14, 20]
     for p, v in zip(points, values):
         display(sp.Eq(sp.Symbol(f'M_{p}'), eq2.rhs.subs(x, v))) # in lbf*in
```

$$M_O = -8080$$

$$M_A = -2160$$

$$M_B = -720$$

$$M_C = 0$$

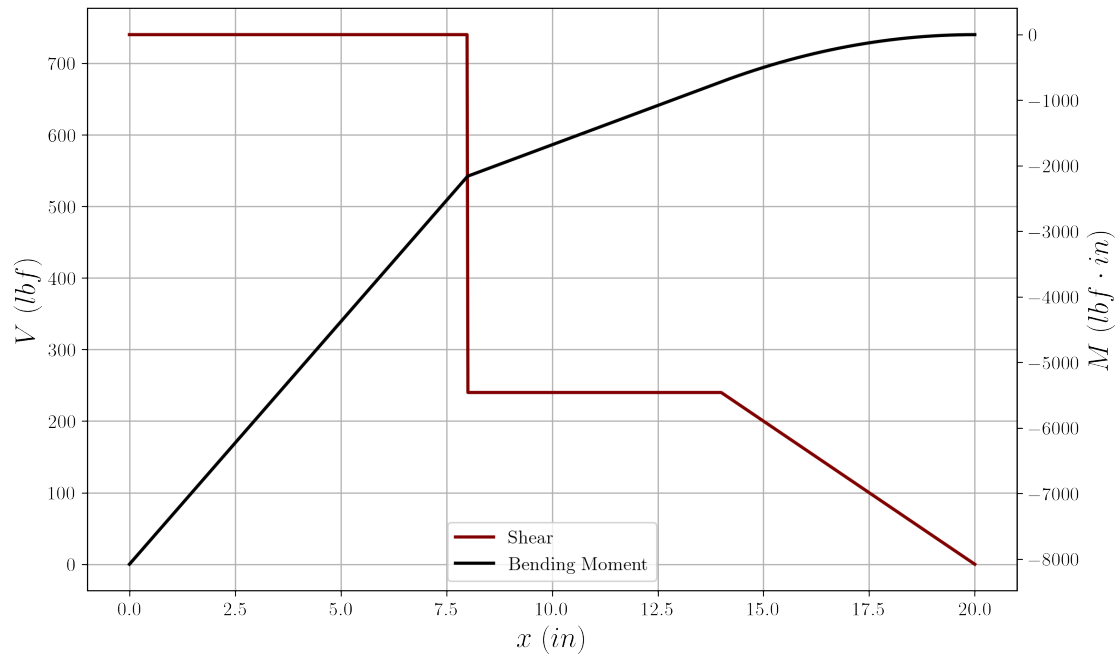
```
[5]: # Getting shear and bending diagram
x_ = np.linspace(0, 20, 1000)
V_ = sp.lambdify(x, eq1.rhs, modules='numpy')
M_ = sp.lambdify(x, eq2.rhs, modules='numpy')

fig, ax = plt.subplots()
ax2 = ax.twinx()

ax.plot(x_, V_(x_), label='Shear')
ax2.plot(x_, M_(x_), label='Bending Moment', color='black')

ax2.grid(visible=False)
ax.legend(handles=[ax.lines[0], ax2.lines[0]], loc='lower center')

ax.set_xlabel('$x$ (in$)')
ax.set_ylabel('$V$ (lbf$)')
ax2.set_ylabel(r'$M$ (lbf\cdot in$)')
plt.show()
```



Notice that the graph has a dual y-axis.

2 Problem 3-17

2.1 Given

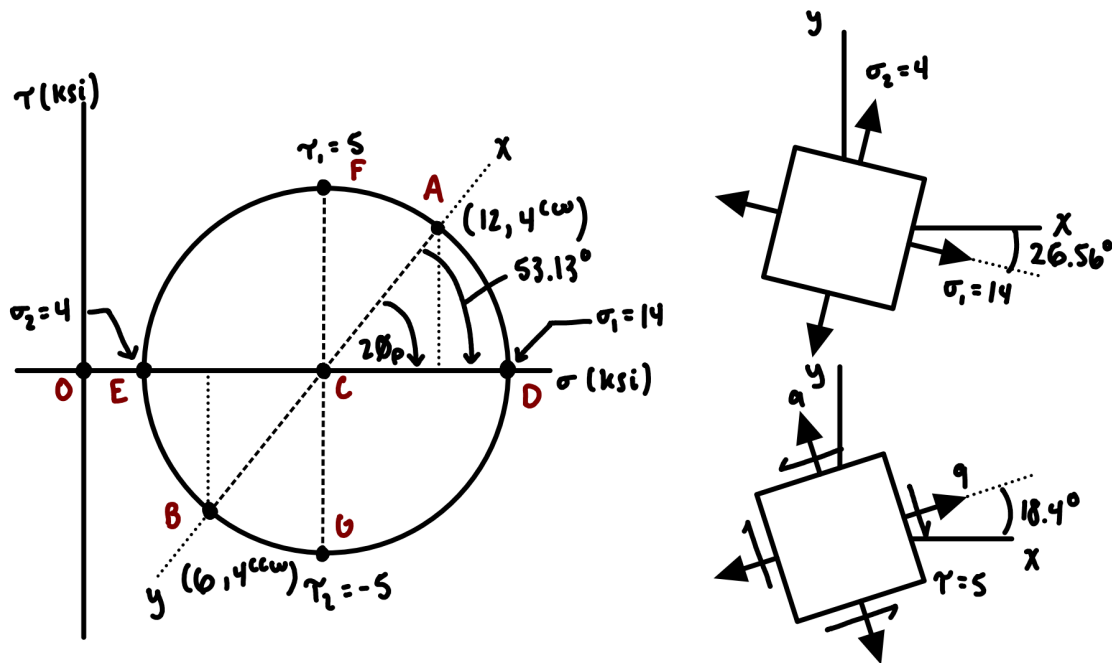
- $\sigma_x = 12 \text{ ksi}$, $\sigma_y = 6 \text{ ksi}$, $\tau_{xy} = 4 \text{ ksi cw}$
- $\sigma_x = 9 \text{ ksi}$, $\sigma_y = 19 \text{ ksi}$, $\tau_{xy} = 8 \text{ ksi cw}$

2.2 Find

Draw the plane stress element as seen in Figure 3-11c and d. Also draw Mohr's circle fully labeled.

2.3 Solution

2.3.1 Part A



Center and Radius:

$$C = \frac{\sigma_x}{2} + \frac{\sigma_y}{2} = 9.0$$

$$R = \sqrt{\tau_{xy}^2 + \left(\frac{\sigma_x}{2} - \frac{\sigma_y}{2}\right)^2} = 5.0$$

Principal Stresses:

$$\sigma_1 = C + R = 14.0$$

$$\sigma_2 = C - R = 4.0$$

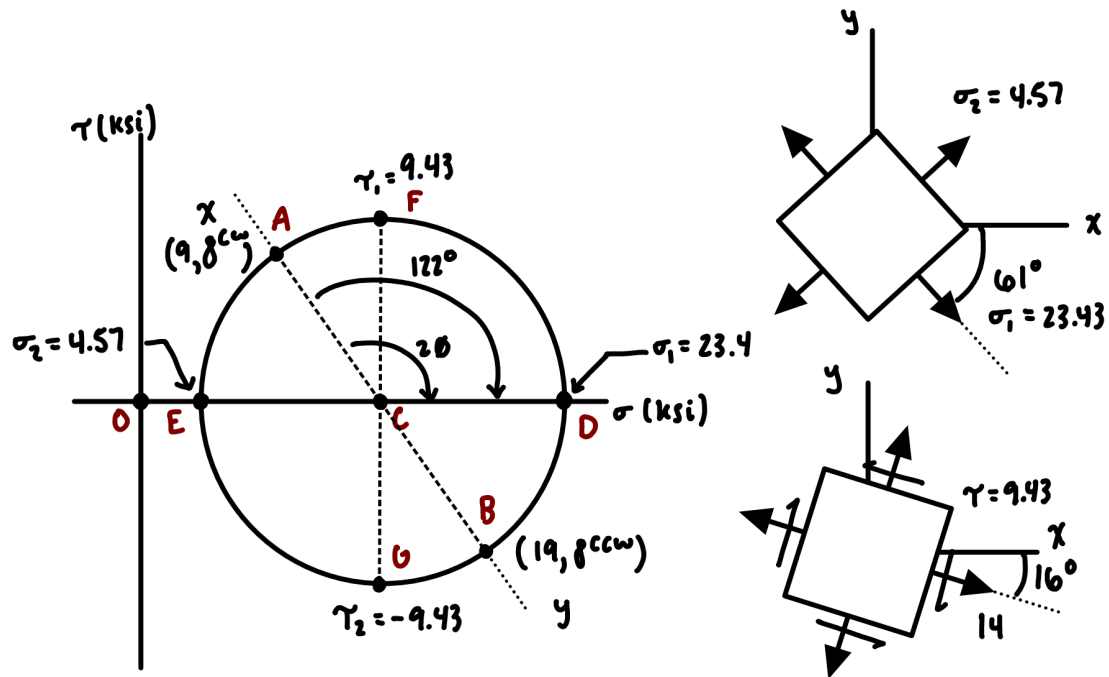
$$\tau_1 = R = 5.0$$

$$\tau_2 = -R = -5.0$$

Angle of Occurrence:

$$2\phi_p = \text{atan}\left(\frac{2\tau_{xy}}{\sigma_x - \sigma_y}\right) = 53.130102354156$$

2.3.2 Part D



Center and Radius:

$$C = \frac{\sigma_x}{2} + \frac{\sigma_y}{2} = 14.0$$

$$R = \sqrt{\tau_{xy}^2 + \left(\frac{\sigma_x}{2} - \frac{\sigma_y}{2}\right)^2} = 9.4339811320566$$

Principle Stresses:

$$\sigma_1 = C + R = 23.4339811320566$$

$$\sigma_2 = C - R = 4.5660188679434$$

$$\tau_1 = R = 9.4339811320566$$

$$\tau_2 = -R = -9.4339811320566$$

Angle of Occurrence:

$$2\phi_p = \text{atan}\left(\frac{2\tau_{xy}}{\sigma_x - \sigma_y}\right) = 122.005383208084$$

3 Problem 3-72

3.1 Given

A 2-foot-long steel bar with a $\frac{3}{4}$ in diameter is to be used as a torsion spring. The torsional stress in the bar is not to exceed 30 *ksi*.

3.2 Find

What is the maximum angle of twist of the bar?

3.3 Solution

Use the following relationship to determine the torque,

$$\tau = \frac{Tc}{J}$$

The angle of twist is,

$$\phi = \frac{TL}{JG}$$

```
[8]: # Find torque
c = sp.S('0.75')/2
J = sp.pi/2*c**4
tau = 30_000
T = tau*J/c
T.n() # torque in lbf*in
```

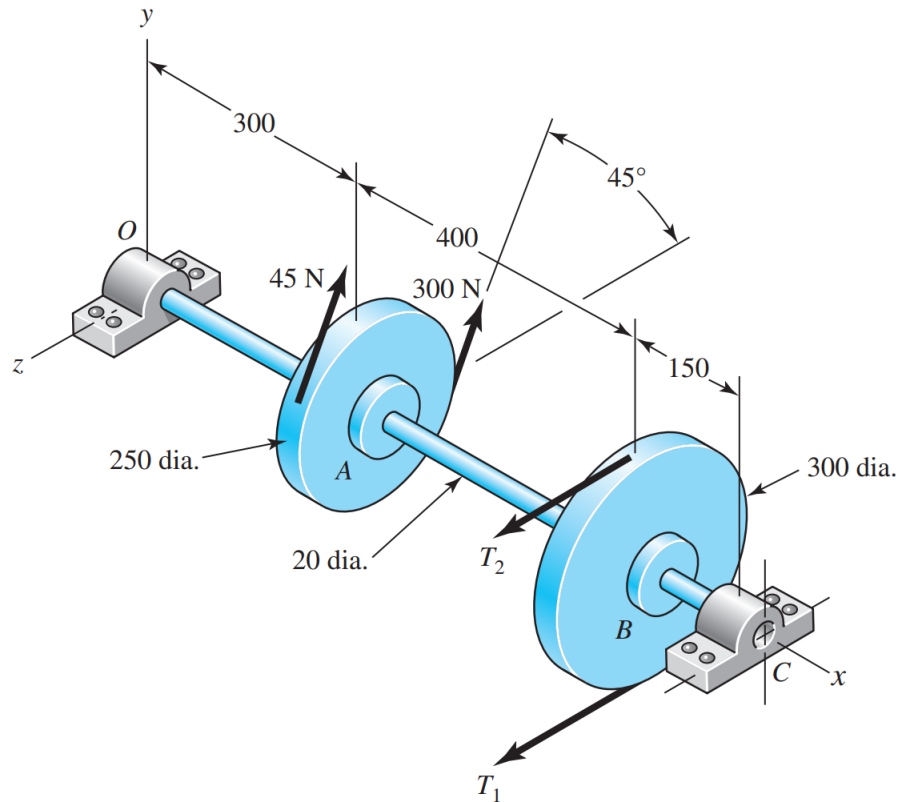
```
[8]: 2485.04887637474
```

```
[9]: # Find angle of twist
G = sp.S('11.5e6') # from Table A-5
L = 24
phi = (T*L/(J*G))
(phi*180/sp.pi).n() # angle of twist in degrees
```

```
[9]: 9.56590405783635
```

4 Problem 3-82

4.1 Given



A counter shaft carrying two V-belt pulleys is shown in the figure. Pulley *A* receives power from a motor through a belt with the belt tensions shown. The power is transmitted through the shaft and delivered to the belt on pulley *B*. Assume the belt tension on the loose side at *B* is 15 percent of the tension on the tight side.

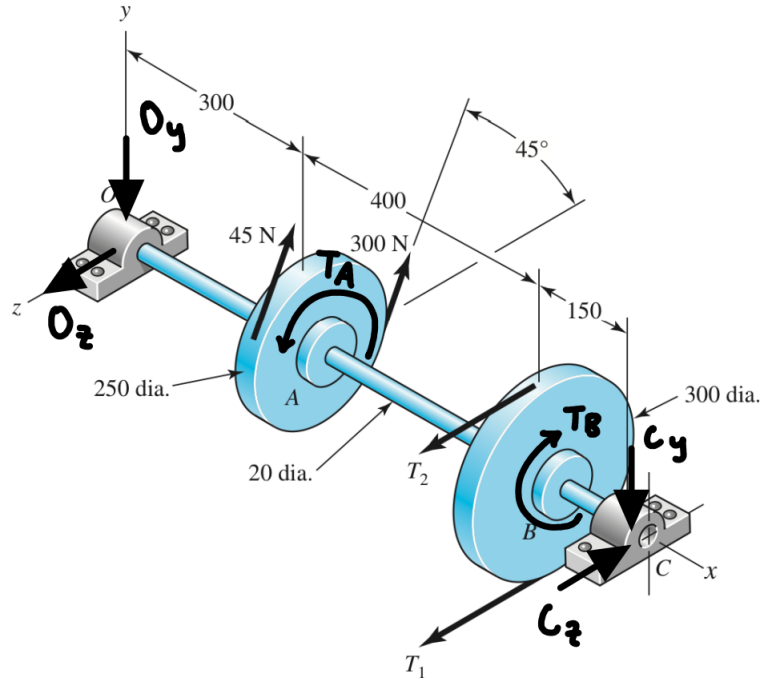
4.2 Find

- Determine the tensions in the belt on pulley *B*, assuming the shaft is running at a constant speed.
- Find the magnitudes of the bearing reaction forces, assuming the bearings act as simple supports.
- Draw shear-force and bending-moment diagrams for the shaft. If needed, make one set for the horizontal plane and another set for the vertical plane.
- At the point of maximum bending moment, determine the bending stress and the torsional shear stress.
- At the point of maximum bending moment, determine the principal stresses and the maximum shear stress.

4.3 Solution

4.3.1 Part A

The directions of the torques about A and B are,



Since the shaft has no angular acceleration, $T_A = T_B$ (with directions shown above). It should also be noted that T_1 must be greater than T_2 because the torque shows that the pulley is more tensile at the bottom.

```
[10]: # Solving for T1 and T2
T1, T2 = sp.symbols('T_1 T_2')
T_A = sp.S('0.125')*(300 - 45)
eq1 = sp.Eq(sp.S('0.15')*(T1 - T2), T_A)
eq2 = sp.Eq(T2, sp.S(0.15)*T1)

[display(eq) for eq in [eq1, eq2, Markdown('---')]]

sol = sp.solve([eq1, eq2], dict=True)[0]
_ = [display(sp.Eq(key, value)) for key, value in sol.items()]
```

$$0.15T_1 - 0.15T_2 = 31.875$$

$$T_2 = 0.15T_1$$

$$T_1 = 250.0$$

$$T_2 = 37.5$$

4.3.2 Part B

```
[11]: # Solving for the reactions
Oy, Oz, Cy, Cz = sp.symbols('O_y O_z C_y C_z')

eq1 = sp.Eq((300 + 45)*sp.sin(sp.pi/4) - Oy - Cy, 0) # Forces in y direction
eq2 = sp.Eq(sol[T1] + sol[T2] + Oz - Cz - (45 + 300)*sp.cos(sp.pi/4), 0) #
    ↪ Forces in z direction
eq3 = sp.Eq(sp.S('0.3')*(45 + 300)*sp.sin(sp.pi/4) - Cy*sp.S('0.85'), 0) #
    ↪ Moments about z-axis
eq4 = sp.Eq(sp.S('0.3')*(45 + 300)*sp.cos(sp.pi/4) - sp.S('0.7')*(sol[T1] +
    ↪ sol[T2]) + Cz*sp.S('0.85'), 0) # Moments about the y-axis

sol2 = sp.solve([eq1, eq2, eq3, eq4], dict=True)[0]
[display(eq) for eq in [eq1, eq2, eq3, eq4, Markdown('---')]]
_ = [display(sp.Eq(key, value)) for key, value in sol2.items()]
```

$$-C_y - O_y + \frac{345\sqrt{2}}{2} = 0$$

$$-C_z + O_z - \frac{345\sqrt{2}}{2} + 287.5 = 0$$

$$-0.85C_y + 51.75\sqrt{2} = 0$$

$$0.85C_z - 201.25 + 51.75\sqrt{2} = 0$$

$$C_y = 86.1006492385973$$

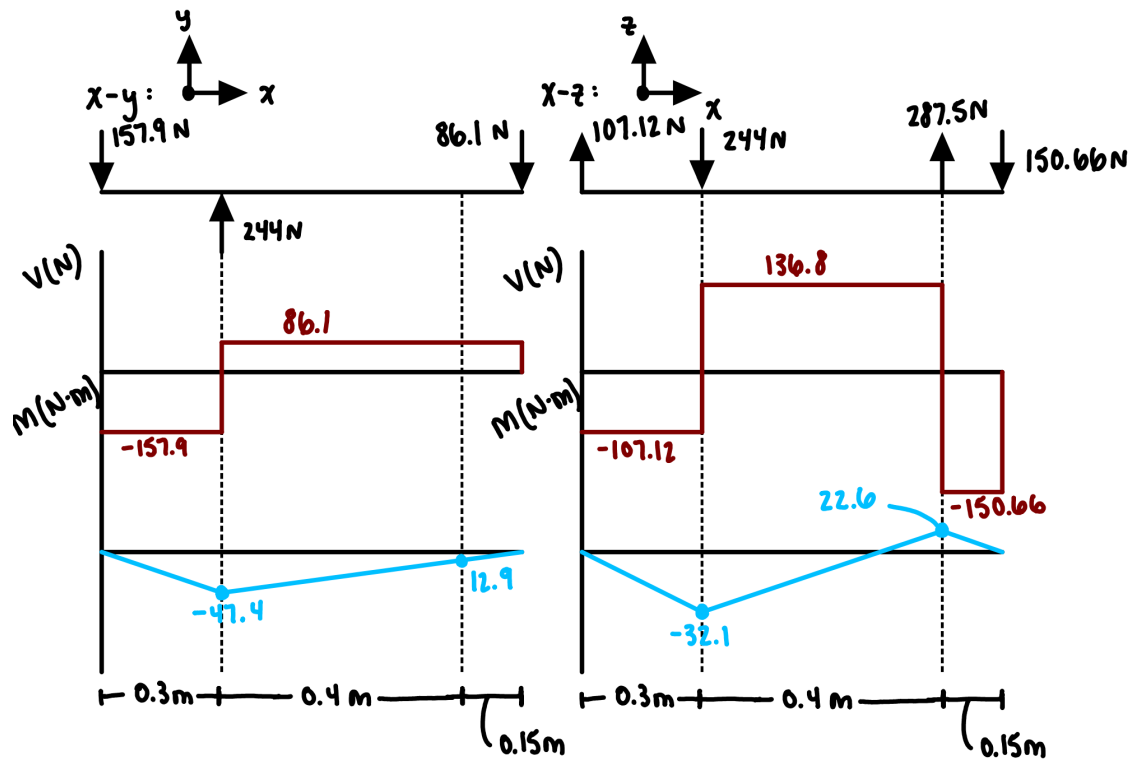
$$O_y = 157.851190270762$$

$$C_z = 150.664056643756$$

$$O_z = 107.115896153115$$

4.3.3 Part C

The shear and bending moment diagram for the two planes is,



4.3.4 Part D

```
[12]: # Getting max bending moment
M_A = sp.sqrt(47.35535708**2 + 32.13476885**2)
M_B = sp.sqrt(12.91509739**2 + 22.59960847**2)
sp.Matrix([M_A, M_B])
```

```
[12]: [57.2291290621938]
      [26.0296377921492]
```

The maximum bending moment occurs at point A.

```
[13]: # Getting the bending stress
c = sp.S('0.01')
sig_x = (M_A*c/(sp.pi/4*c**4)).n()
sig_x # in Pa
```

```
[13]: 72866390.2327375
```

```
[14]: # Getting the torsional stress
t_xz = (31.875*c/(sp.pi/2*c**4)).n()
t_xz # in Pa
```

```
[14]: 20292255.2442167
```

4.3.5 Part E

Center and Radius:

$$C = \frac{\sigma_x}{2} + \frac{\sigma_y}{2} = 36433195.1163688$$

$$R = \sqrt{\tau_{xy}^2 + \left(\frac{\sigma_x}{2} - \frac{\sigma_y}{2}\right)^2} = 41703157.3059383$$

Principle Stresses:

$$\sigma_1 = C + R = 78136352.422307$$

$$\sigma_2 = C - R = -5269962.18956954$$

$$\tau_1 = R = 41703157.3059383$$

$$\tau_2 = -R = -41703157.3059383$$

Angle of Occurrence:

$$2\phi_p = \text{atan}\left(\frac{2\tau_{xy}}{\sigma_x - \sigma_y}\right) = 29.1165652891492$$