

Machine Design Homework 3

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Gabe Morris

```
[1]: # Notebook Preamble
import sympy as sp
import matplotlib.pyplot as plt
from IPython.display import display

plt.style.use('maroon_ipynb.mplstyle')
```

Contents

1	Problem 5-3	3
1.1	Given	3
1.2	Find	3
1.3	Solution	3
1.3.1	Part A	3
1.3.2	Part D	4
1.3.3	Part E	5
2	Problem 5-17	6
2.1	Given	6
2.2	Find	6
2.3	Solution	6
3	Problem 5-19	7
3.1	Given	7
3.2	Find	7
3.3	Solution	7
4	Problem 5-24	8
4.1	Given	8
4.2	Find	8
5	Problem 5-98	9
5.1	Given	9
5.2	Find	9
5.3	Solution	9

1 Problem 5-3

1.1 Given

A ductile AISI 1030 hot-rolled steel bar has a minimum yield strength in tension and compression of 37.5 ksi.

1.2 Find

Use the distortion energy and maximum shear stress theories to determine the factors of safety for the following plane stress states:

- $\sigma_x = 25 \text{ ksi}, \sigma_y = 15 \text{ ksi}$
- $\sigma_x = -12 \text{ ksi}, \sigma_y = 15 \text{ ksi}, \tau_{xy} = -9 \text{ ksi}$
- $\sigma_x = -24 \text{ ksi}, \sigma_y = -24 \text{ ksi}, \tau_{xy} = -15 \text{ ksi}$

1.3 Solution

The relationship comes from Eq. 5-3 (maximum shear stress theory) and Eq. 5-19 (distortion energy theory),

$$\sigma_1 - \sigma_3 = \frac{S_y}{n}$$
$$\sigma' = \frac{S_y}{n}$$

1.3.1 Part A

```
[2]: Sy = sp.S('37.5')

# Getting the principal stresses
sig_x, sig_y, sig_z, tau_xy, tau_zx, tau_yz = sp.symbols(r'\sigma_x \sigma_y \sigma_z \tau_{xy} \tau_{zx} \tau_{yz}')
sig = sp.Symbol(r'\sigma')
sig1, sig2, sig3 = sp.symbols(r'\sigma_1 \sigma_2 \sigma_3')

poly = sig**3 - (sig_x + sig_y + sig_z)*sig**2 + (sig_x*sig_y + sig_x*sig_z + sig_y*sig_z - tau_xy**2 - tau_yz**2 - tau_zx**2)*sig - (sig_x*sig_y*sig_z + 2*tau_xy*tau_yz*tau_zx - sig_x*tau_yz**2 - sig_y*tau_zx**2 - sig_z*tau_xy**2)
display(sp.Eq(poly.simplify(), 0))

def get_principal(sx, sy, sz, txy, tyz, tzx):
    poly_ = poly.subs([(sig_x, sx), (sig_y, sy), (sig_z, sz), (tau_xy, txy), (tau_yz, tyz), (tau_zx, tzx)])
    roots = [sp.re(root.n()) for root in sp.roots(poly_, sig)]
    roots_ = sorted(list(roots), reverse=True)
```

```

for i, j in zip((sig1, sig2, sig3), roots_):
    display(sp.Eq(i, j))
return roots_

def von_mises(s1_, s2_, s3_):
    return (1/sp.sqrt(2)*sp.sqrt((s1_ - s2_)**2 + (s2_ - s3_)**2 + (s3_ -
↪s1_)**2)).n()

s1, s2, s3 = get_principal(25, 15, 0, 0, 0, 0)

```

$$\sigma^3 - \sigma^2 (\sigma_x + \sigma_y + \sigma_z) + \sigma (\sigma_x \sigma_y + \sigma_x \sigma_z + \sigma_y \sigma_z - \tau_{xy}^2 - \tau_{yz}^2 - \tau_{zx}^2) - \sigma_x \sigma_y \sigma_z + \sigma_x \tau_{yz}^2 + \sigma_y \tau_{zx}^2 + \sigma_z \tau_{xy}^2 - 2\tau_{xy}\tau_{yz}\tau_{zx} = 0$$

$$\sigma_1 = 25.0$$

$$\sigma_2 = 15.0$$

$$\sigma_3 = 0$$

```

[3]: # Maximum shear stress theory
Sy/(s1 - s3)

```

[3]: 1.5

```

[4]: # Distortion energy method
s_vm = von_mises(s1, s2, s3)
Sy/s_vm

```

[4]: 1.72061800402921

1.3.2 Part D

```

[5]: s1, s2, s3 = get_principal(-12, 15, 0, -9, 0, 0)

# Maximum shear stress
Sy/(s1 - s3)

```

$$\sigma_1 = 17.724980739588$$

$$\sigma_2 = 0$$

$$\sigma_3 = -14.724980739588$$

[5]: 1.15562540880256

```

[6]: # Distortion
s_vm = von_mises(s1, s2, s3)
Sy/s_vm

```

[6]: 1.33250447722257

1.3.3 Part E

```
[7]: s1, s2, s3 = get_principal(-24, -24, 0, -15, 0, 0)
```

```
# Maximum shear stress  
Sy/(s1 - s3)
```

$$\sigma_1 = 0$$

$$\sigma_2 = -9.0$$

$$\sigma_3 = -39.0$$

```
[7]: 0.961538461538462
```

```
[8]: # Distortion  
s_vm = von_mises(s1, s2, s3)  
Sy/s_vm
```

```
[8]: 1.06023616209996
```

2 Problem 5-17

2.1 Given

An AISI 4142 steel Q&T at $800^\circ F$ exhibits $S_{yt} = 235 \text{ ksi}$, $S_{yc} = 285 \text{ ksi}$, and $\epsilon_f = 0.07$.

$$\sigma_x = -80 \text{ ksi}, \sigma_y = -125 \text{ ksi}, \tau_{xy} = 50 \text{ ksi}$$

2.2 Find

Determine the factor of safety.

2.3 Solution

The strain at failure is above 0.05, which means that the material is considered ductile. We can apply Eq. 5-22,

$$\frac{\sigma_1}{S_t} - \frac{\sigma_3}{S_c} = \frac{1}{n}$$

```
[9]: St, Sc = sp.S(235), sp.S(285)
      s1, _, s3 = get_principal(-80, -125, 0, 50, 0, 0)
      1/(s1/St - s3/Sc)
```

$$\sigma_1 = 0$$

$$\sigma_2 = -47.6707195013467$$

$$\sigma_3 = -157.329280498653$$

```
[9]: 1.81148734105118
```

This answer lines up with the answer in the back of the book.

3 Problem 5-19

3.1 Given

A brittle material has properties $S_{ut} = 30 \text{ ksi}$ and $S_{uc} = 90 \text{ ksi}$.

$$\sigma_x = 20 \text{ ksi}, \tau_{xy} = -10 \text{ ksi}$$

3.2 Find

Using only the modified-Mohr theories, determine the factor of safety.

3.3 Solution

Start by computing the principal stresses.

```
[10]: Sut = 30  
s1, _, _ = get_principal(20, 0, 0, -10, 0, 0)
```

$$\sigma_1 = 24.142135623731$$

$$\sigma_2 = 0$$

$$\sigma_3 = -4.14213562373095$$

For this case, we can use Eq. 5-32a on p. 264,

$$\sigma_1 = \frac{S_{ut}}{n}$$

```
[11]: Sut/s1
```

```
[11]: 1.24264068711929
```

4 Problem 5-24

4.1 Given

ASTM 30 cast iron.

$$\sigma_x = -10 \text{ ksi}, \sigma_y = -25 \text{ ksi}, \text{ and } \tau_{xy} = -10 \text{ ksi}$$

4.2 Find

Determine the factor of safety using the modified-Mohr method.

```
[12]: s1, s2, s3 = get_principal(-10, -25, 0, -10, 0, 0)
```

$$\sigma_1 = 0$$

$$\sigma_2 = -5.0$$

$$\sigma_3 = -30.0$$

Use Eq. 5-32c,

$$n = \frac{-S_{uc}}{\sigma_3}$$

```
[13]: Suc = 109 # Table A-24  
-Suc/s3
```

```
[13]: 3.633333333333333
```


5 Problem 5-98

5.1 Given

A cylinder subjected to internal pressure p_i has an outer diameter of 14 in and a 1-in wall thickness. For the cylinder material, $K_{IC} = 72 \text{ ksi}\sqrt{\text{in}}$, $S_y = 170 \text{ ksi}$, and $S_{ut} = 192 \text{ ksi}$.

5.2 Find

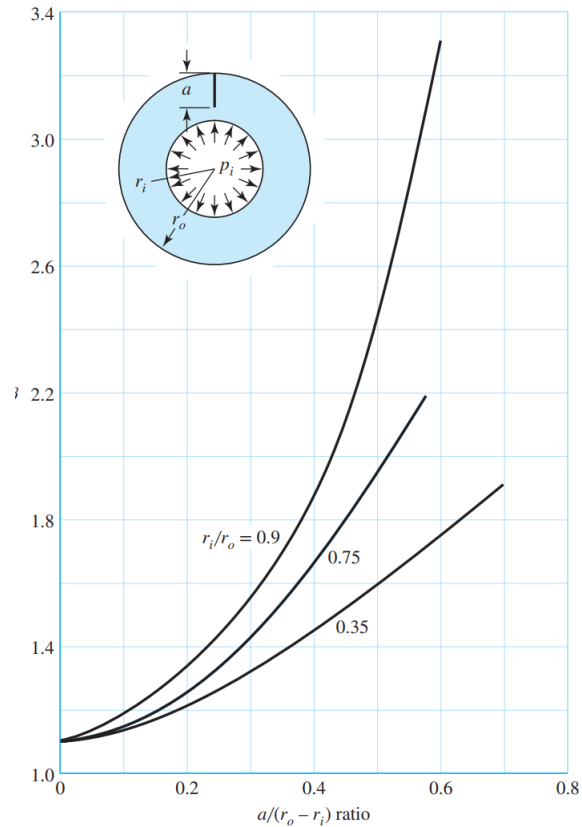
If the cylinder contains a radial crack in the longitudinal direction of depth 0.5 in determine the pressure that will cause uncontrollable crack growth.

5.3 Solution

We use the following relationship,

$$K_I = \beta \sigma \sqrt{\pi a}$$

β may be found from,



```
[14]: a = sp.S('0.5')
      ro, ri = sp.S(7), 6
      a/(ro - ri)
```

```
[14]: 0.5
```

The correct line to use depends on $\frac{r_i}{r_o}$.

```
[15]: ri/ro.n()
```

```
[15]: 0.857142857142857
```

```
[16]: beta = sp.S(2.35) # from the above figure
      K_IC = 72
      sig = K_IC/(beta*sp.sqrt(sp.pi*a))
      sig.n() # ksi
```

```
[16]: 24.4458248416197
```