Machine Design Final Exam

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```
[1]: # Notebook Preamble
     import sympy as sp
     import matplotlib.pyplot as plt
     from IPython.display import display
     plt.style.use('maroon_ipynb.mplstyle')
     def sub_return(expression, substitution, sym=None):
         Displays a substituted expression and returns the value.
         :param expression: Symbolic expression
         :param substitution: A list of tuples to be passed into the .sub method
         :param sym: An optional symbol to display prior to operations
         :return: A simplified value of what is substituted.
         HHHH
         with sp.evaluate(False):
             expr_sub = expression.subs(substitution)
         simp = expr_sub.doit().n()
         if sym is None:
             lev1 = sp.Eq(expression, expr_sub)
             lev2 = sp.Eq(lev1, simp, evaluate=False)
             display(lev2)
         else:
             lev1 = sp.Eq(sym, expression)
             lev2 = sp.Eq(lev1, expr_sub, evaluate=False)
             lev3 = sp.Eq(lev2, simp, evaluate=False)
             display(lev3)
         return simp
     def get_principal(s_x, s_y, t_xy):
         Shows the principal stress calculations for a 2D element.
         :param s_x: normal stress along the x-axis
         :param s_y: normal stress along the y-axis
```

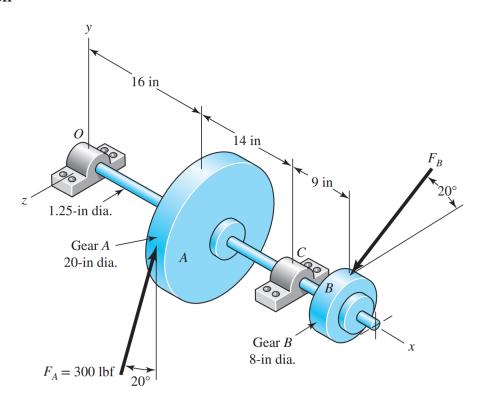
```
:param t_xy: shear stress on face x in the direction of y
    :return: principal stresses
    s_x_, s_y_, t_xy_ = sp.symbols(r'\sigma_x \sigma_y \tau_{xy}')
    symbols_ = sp.symbols(r'\sigma_1 \sigma_2 \tau_1 \tau_2')
    expr1_ = (s_x_ + s_y_)/2 + sp.sqrt(((s_x_ - s_y_)/2)**2 + t_xy_**2)
    expr2_ = (s_x_ + s_y_)/2 - sp.sqrt(((s_x_ - s_y_)/2)**2 + t_xy_**2)
    expr3_ = sp.sqrt(((s_x_ - s_y_)/2)**2 + t_xy_**2)
    expr4_ = -sp.sqrt(((s_x_ - s_y_)/2)**2 + t_xy_**2)
    sub_list = [(s_x, s_x), (s_y, s_y), (t_xy, t_xy)]
    ans = \Pi
    for sym_, expr_ in zip(symbols_, [expr1_, expr2_, expr3_, expr4_]):
        ans.append(sub_return(expr_, sub_list, sym=sym_))
    return ans
def von_mises(s_x, s_y, s_z, t_xy, t_yz, t_zx):
   return 1/sp.sqrt(2)*sp.sqrt((s_x - s_y)**2 + (s_y - s_z)**2 + (s_z -
 \Rightarrows_x)**2 + 6*(t_xy**2 + t_yz**2 + t_zx**2))
```

Contents

1		olem 3-83
	1.1	Given
	1.2	Find
	1.3	Solution
		1.3.1 Part A and Part B
		1.3.2 Part C
		1.3.3 Part D
		1.3.4 Part E
2		olem 5-36
	2.1	Given
	2.2	Find
	2.3	Solution
		2.3.1 Element A
		2.3.2 Element B

1 Problem 3-83

1.1 Given



A gear reduction unit uses the countershaft shown in the figure above. Gear A receives power from another gear with a transmitted force F_A applied at the 20° pressure angle as shown. The power is transmitted through the shaft and delivered through gear B through a transmitted force F_B at the pressure angle shown.

1.2 Find

- a. Determine the force F_B , assuming the shaft is running at a constant speed.
- b. Find the bearing reaction forces, assuming the bearings act as simple supports.
- c. Draw a shear-force and bending moment diagrams for the shaft. If needed, make one set for the horizontal plane and another set for the vertical plane.
- d. At the point of maximum bending moment, determine the bending stress and the torsional shear stress.
- e. At the point of maximum bending moment, determine the principal stresses and the maximum shear stress.

1.3 Solution

1.3.1 Part A and Part B

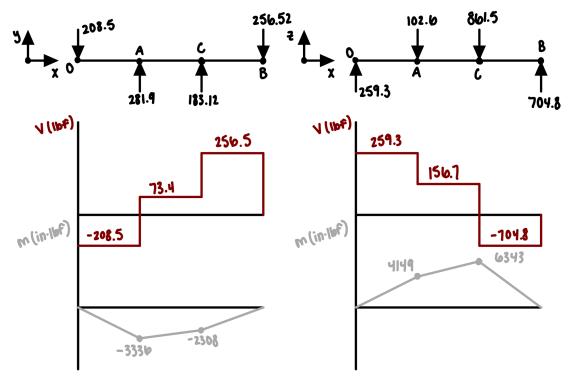
 F_B and the reaction forces may be found by summing the forces and taking the moments about the point O.

```
[2]: # Using matrices takes less thinking and more letting python do the work.
     Oy, Oz, Cy, Cz, F_B = sp.symbols('O_y O_z C_y C_z F_B')
     zero = sp.ZeroMatrix(3, 1)
     F_A_mat = sp.Matrix([0, 300*sp.cos(sp.rad(20)), -300*sp.sin(sp.rad(20))])
     F_B_mat = sp.Matrix([0, -F_B*sp.sin(sp.rad(20)), F_B*sp.cos(sp.rad(20))])
     0 = sp.Matrix([0, 0y, 0z])
     C = sp.Matrix([0, Cy, Cz])
     # Sum forces
     sys1 = sp.Eq(0 + F_A_mat + F_B_mat + C, zero)
     # Sum moments about O
     rA = sp.Matrix([16, 0, 10])
     rC = sp.Matrix([16 + 14, 0, 0])
     rB = sp.Matrix([16 + 14 + 9, 4, 0])
     sys2 = sp.Eq(rA.cross(F_A_mat) + rC.cross(C) + rB.cross(F_B_mat), zero)
     sol = sp.solve([sys1, sys2], dict=True)[0]
     for key, value in sol.items():
         display(sp.Eq(key, value.n())) # lbf
    C_y = 183.118820416782
    C_z = -861.477082334154
    F_{B} = 750.0
```

 $O_y = -208.511499158303$ $O_z = 259.313659742423$

The reaction forces above assume all positive directions.

1.3.2 Part C



1.3.3 Part D

The magnitudes of the moment at section A and section C must be compared.

```
[3]: M_A = sp.sqrt(sp.S('3336.18399')**2 + sp.S('4149.01856')**2)

M_C = sp.sqrt(sp.S('6342.92519')**2 + sp.S('2308.63597')**2)

display(M_A, M_C)
```

5323.95328927262

6750.00000058625

```
[4]: # M_C is the greater value
M_C = sp.S(6750) # in*lbf
d = sp.S('1.25')
sig = M_C*32/(sp.pi*d**3) # psi
T = 300*sp.cos(sp.rad(20))*10 # static torque
tau = T*16/(sp.pi*d**3) # psi
display(sig.n(), tau.n())
```

35202.5269328378

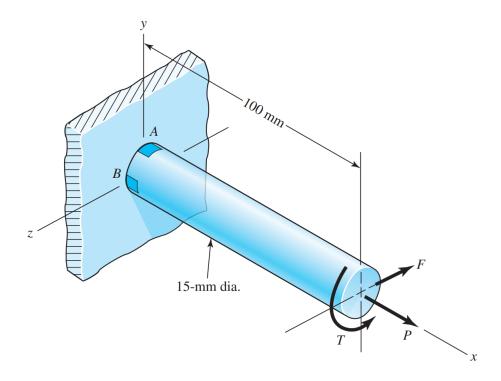
7351.01217595663

1.3.4 Part E

$$\begin{split} &\sigma_1 = \frac{\sigma_x}{2} + \frac{\sigma_y}{2} + \sqrt{\tau_{xy}^2 + \left(\frac{\sigma_x}{2} - \frac{\sigma_y}{2}\right)^2} = \frac{1}{2} \cdot 0 + \frac{1}{2} \cdot 35203.0 + \sqrt{7351.0^2 + \left(\left(-\frac{1}{2}\right)0 + \frac{1}{2} \cdot 35203.0\right)^2} = \\ &36675.875 \\ &\sigma_2 = \frac{\sigma_x}{2} + \frac{\sigma_y}{2} - \sqrt{\tau_{xy}^2 + \left(\frac{\sigma_x}{2} - \frac{\sigma_y}{2}\right)^2} = -\sqrt{7351.0^2 + \left(\left(-\frac{1}{2}\right)0 + \frac{1}{2} \cdot 35203.0\right)^2 + \frac{1}{2} \cdot 0 + \frac{1}{2} \cdot 35203.0} = \\ &-1473.375 \\ &\tau_1 = \sqrt{\tau_{xy}^2 + \left(\frac{\sigma_x}{2} - \frac{\sigma_y}{2}\right)^2} = \sqrt{7351.0^2 + \left(\left(-\frac{1}{2}\right)0 + \frac{1}{2} \cdot 35203.0\right)^2} = 19074.625 \\ &\tau_2 = -\sqrt{\tau_{xy}^2 + \left(\frac{\sigma_x}{2} - \frac{\sigma_y}{2}\right)^2} = -\sqrt{7351.0^2 + \left(\left(-\frac{1}{2}\right)0 + \frac{1}{2} \cdot 35203.0\right)^2} = -19074.625 \end{split}$$

2 Problem 5-36

2.1 Given



The figure above illustrates that the factor of safety for a machine element depends on the particular point selected for analysis. The bar is made of AISI 1006 cold-drawn steel and is loaded by the forces $F = 0.55 \, kN$, $P = 4.0 \, kN$, and $T = 25 \, N \cdot m$.

2.2 Find

Find the factor of safety for both elements using the distortion energy method.

2.3 Solution

The yield strength is $S_y=280\,MPa.$

2.3.1 Element A

```
[6]: P = sp.S(4_000)
Sy = sp.S(280e6)
T = sp.S(25)
d = sp.S('0.015')
F = sp.S('0.55e3')
1 = sp.S('0.1')
```

```
sig_x = 4*P/(sp.pi*d**2)
      tau_xy = 16*T/(sp.pi*d**3) - 4*sp.S('0.55e3')/(3*(sp.pi/4)*(sp.S('0.015')**2))
      display(sig_x.n(), tau_xy.n()) # Pa
     22635369.6841807
     33575798.364868
 [7]: sig_prime = von_mises(sig_x, 0, 0, tau_xy, 0, 0)
      sig_prime.n() # Pa
 [7]: 62404828.8857068
 [8]: (Sy/sig_prime).n()
 [8]:
4.48683226922735
     2.3.2 Element B
 [9]: sig_x = 32*F*1/(sp.pi*d**3) + 4*P/(sp.pi*d**2)
      tau_xy = 16*T/(sp.pi*d**3)
      display(sig_x.n(), tau_xy.n()) # Pa
     188628080.701506\\
     37725616.1403011
[10]: sig_prime = von_mises(sig_x, 0, 0, tau_xy, 0, 0)
      sig_prime.n() # Pa
[10]: 199625196.727842
[11]: (Sy/sig_prime).n()
```

[11]: 1.40262854884865