Dynamical Systems Homework 3

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```
[1]: # toc
import sympy as sp
import matplotlib.pyplot as plt

plt.style.use('../maroon_ipynb.mplstyle')
```

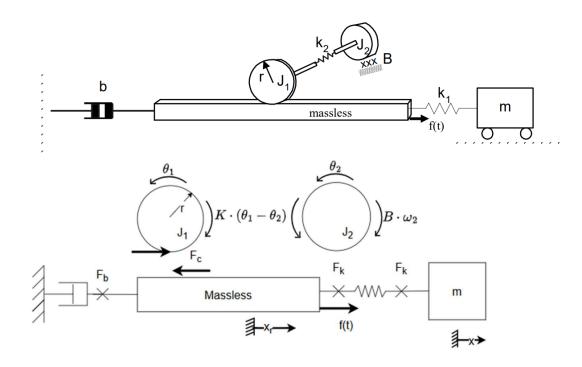
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Problem 1

Given

ME 8613



The constants from the above figure are given as follows:

$$\begin{split} r &= 0.05\,m \\ k_1 &= 1000\,N/m \\ k_2 &= 500\,N/m \\ b &= 100\,N\cdot s/m \\ B &= 2.5\,N\cdot m\cdot s \\ J_1 &= J_2 = 1\,kg\cdot m^2 \\ m &= 1\,kg \end{split}$$

Find

With the above system,

- a. Develop a set of state variable equations. Define the state variable using the general matrix form: $\dot{S} = A \cdot S + B \cdot U$, where A and B are matrices and S is a vector of state variables and U is a vector of inputs. Be careful with labeling since one of the damping coefficients is also labeled B in the figure.
- b. Solve the state variable equations using a 4th order Runge-Kutta numerical method for a total simulation time of 20 seconds and assuming that all initial velocities and spring forces are zero and that f(t) = 10 N. Make sure the check that the number of points used in the simulation is adequate.

- c. Verify your results using energy conservation. Show that at a given time, t, the total energy that has crossed the boundary through inputs and dampers is equal to the total energy stored in the system through mass/inertias and springs.
- d. Use the output matrix form $Y = C \cdot S + D \cdot U$, where Y is the chosen output and C and D are matrices. Use this form to define the contact force between the rack and the pinion using state variable simulation results. Then plot the contact force.
- e. Find the input-output equation between the input force and the contact force. One approach of doing this is the use the ss2tf function in the scipy.signal module.
- f. Use the laplace transform approach to solve the input-output equation and compare with results from part d. Comment on how the roots of the characteristic polynomial affect the response.

Solution

Part A

From the above figure, the massless element is denoted as x_1 and the mass denoted by m is x_2 .

$$\begin{split} 0 &= -F_c - b\frac{d}{dt}x_1(t) + k_1\left(-x_1(t) + x_2(t)\right) + f(t) \\ m\frac{d^2}{dt^2}x_2(t) &= k_1\left(x_1(t) - x_2(t)\right) \\ J_1\frac{d^2}{dt^2}\theta_1(t) &= F_c r + k_2\left(-\theta_1(t) + \theta_2(t)\right) \\ J_2\frac{d^2}{dt^2}\theta_2(t) &= -B\frac{d}{dt}\theta_2(t) + k_2\left(\theta_1(t) - \theta_2(t)\right) \\ \frac{d^2}{dt^2}x_1(t) &= r\frac{d^2}{dt^2}\theta_1(t) \end{split}$$

Let's clean this up a little by considering the velocities v_1 , v_2 , ω_1 , and ω_2 . Also, let's omit considering the coordinate positions in the system and only look to the displacements of the compliance elements. I will define Δx and $\Delta \theta$ as

$$\begin{cases} \Delta x = x_2 - x_1 \\ \Delta \theta = \theta_2 - \theta_1 \end{cases}$$

$$\begin{split} 0 &= -F_c - bv_1(t) + k_1 \Delta x(t) + f(t) \\ m \frac{d}{dt} v_2(t) &= -k_1 \Delta x(t) \\ J_1 \frac{d}{dt} \omega_1(t) &= F_c r + k_2 \Delta \theta(t) \\ J_2 \frac{d}{dt} \omega_2(t) &= -B \omega_2(t) - k_2 \Delta \theta(t) \\ \frac{d}{dt} v_1(t) &= r \frac{d}{dt} \omega_1(t) \end{split}$$

Now we can solve this system for \dot{v}_1 , \dot{v}_2 , $\dot{\omega}_1$ $\dot{\omega}_2$. Additionally, I will solve for F_c to be used later.

$$\begin{split} F_c &= -bv_1(t) + k_1 \Delta x(t) + f(t) \\ \frac{d}{dt} \omega_1(t) &= -\frac{brv_1(t)}{J_1} + \frac{k_1 r \Delta x(t)}{J_1} + \frac{k_2 \Delta \theta(t)}{J_1} + \frac{rf(t)}{J_1} \\ \frac{d}{dt} \omega_2(t) &= -\frac{B\omega_2(t)}{J_2} - \frac{k_2 \Delta \theta(t)}{J_2} \\ \frac{d}{dt} v_1(t) &= -\frac{br^2 v_1(t)}{J_1} + \frac{k_1 r^2 \Delta x(t)}{J_1} + \frac{k_2 r \Delta \theta(t)}{J_1} + \frac{r^2 f(t)}{J_1} \end{split}$$

$$\frac{d}{dt}v_2(t) = -\frac{k_1\Delta x(t)}{m}$$

Notice in the above solution that we don't have any terms that include ω_1 . This is due to the direct algebraic relationship and the order in which sympy solved the system. Therefore, we can ignore the $\dot{\omega}_1$ equation. Also, the solution for F_c is not an ODE so it isn't directly a part of the state space solution.

```
[5]: # Getting the final five equations
eq1 = sp.Eq(d_x.diff(), v2 - v1)
eq2 = sp.Eq(d_theta.diff(), omega2 - v1/r)
eq3 = sp.Eq(v1.diff(), state_sol[v1.diff()])
eq4 = sp.Eq(v2.diff(), state_sol[v2.diff()])
eq5 = sp.Eq(omega2.diff(), state_sol[omega2.diff()])
eqs = [eq1, eq2, eq3, eq4, eq5]
display(*eqs)
```

$$\begin{split} \frac{d}{dt}\Delta x(t) &= -v_1(t) + v_2(t) \\ \frac{d}{dt}\Delta \theta(t) &= \omega_2(t) - \frac{v_1(t)}{r} \\ \frac{d}{dt}v_1(t) &= -\frac{br^2v_1(t)}{J_1} + \frac{k_1r^2\Delta x(t)}{J_1} + \frac{k_2r\Delta \theta(t)}{J_1} + \frac{r^2f(t)}{J_1} \\ \frac{d}{dt}v_2(t) &= -\frac{k_1\Delta x(t)}{m} \\ \frac{d}{dt}\omega_2(t) &= -\frac{B\omega_2(t)}{J_2} - \frac{k_2\Delta \theta(t)}{J_2} \end{split}$$

Answer

$$\begin{bmatrix} \frac{d}{dt} \Delta x(t) \\ \frac{d}{dt} \Delta \theta(t) \\ \frac{d}{dt} v_1(t) \\ \frac{d}{dt} v_2(t) \\ \frac{d}{dt} \omega_2(t) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \frac{r^2}{J_1} \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} f(t) \end{bmatrix} + \begin{bmatrix} 0 & 0 & -1 & 1 & 0 \\ 0 & 0 & -\frac{1}{r} & 0 & 1 \\ \frac{k_1 r^2}{J_1} & \frac{k_2 r}{J_1} & -\frac{b r^2}{J_1} & 0 & 0 \\ -\frac{k_1}{m} & 0 & 0 & 0 & 0 \\ 0 & -\frac{k_2}{J_2} & 0 & 0 & -\frac{B}{J_2} \end{bmatrix} \begin{bmatrix} \Delta x(t) \\ \Delta \theta(t) \\ v_1(t) \\ v_2(t) \\ \omega_2(t) \end{bmatrix}$$