Dynamical Systems Homework 3

March 19, 2025

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```
[1]: # toc
import control as ct
import matplotlib.pyplot as plt
import numpy as np
import sympy as sp
from scipy.integrate import solve_ivp, cumulative_trapezoid

plt.style.use('../maroon_ipynb.mplstyle')
```

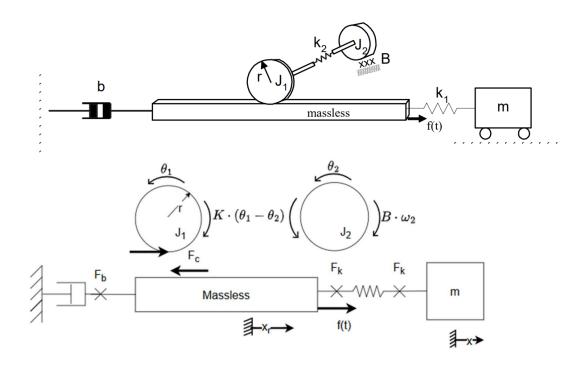
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Problem 1

Given

ME 8613



The constants from the above figure are given as follows:

$$\begin{split} r &= 0.05\,m \\ k_1 &= 1000\,N/m \\ k_2 &= 500\,N/m \\ b &= 100\,N\cdot s/m \\ B &= 2.5\,N\cdot m\cdot s \\ J_1 &= J_2 = 1\,kg\cdot m^2 \\ m &= 1\,kg \end{split}$$

Find

With the above system,

- a. Develop a set of state variable equations. Define the state variable using the general matrix form: $\dot{S} = A \cdot S + B \cdot U$, where A and B are matrices and S is a vector of state variables and U is a vector of inputs. Be careful with labeling since one of the damping coefficients is also labeled B in the figure.
- b. Solve the state variable equations using a 4th order Runge-Kutta numerical method for a total simulation time of 20 seconds and assuming that all initial velocities and spring forces are zero and that f(t) = 10 N. Make sure the check that the number of points used in the simulation is adequate.

- c. Verify your results using energy conservation. Show that at a given time, t, the total energy that has crossed the boundary through inputs and dampers is equal to the total energy stored in the system through mass/inertias and springs.
- d. Use the output matrix form $Y = C \cdot S + D \cdot U$, where Y is the chosen output and C and D are matrices. Use this form to define the contact force between the rack and the pinion using state variable simulation results. Then plot the contact force.
- e. Find the input-output equation between the input force and the contact force. One approach of doing this is the use the ss2tf function in the scipy.signal module.
- f. Use the laplace transform approach to solve the input-output equation and compare with results from part d. Comment on how the roots of the characteristic polynomial affect the response.

Solution

Part A

From the above figure, the massless element is denoted as x_1 and the mass denoted by m is x_2 .

```
[2]: # Define symbols
r, k1, k2, b, B, J1, J2, m, t, s = sp.symbols('r k1 k2 b B J1 J2 m t s', u real=True, positive=True)
th1, th2 = sp.Function('theta_1')(t), sp.Function('theta_2')(t)
x1, x2 = sp.Function('x1')(t), sp.Function('x2')(t)
f, F_c = sp.Function('f')(t), sp.Function('F_c')(t)

# Construct equations
eq1 = sp.Eq(0, f - F_c - b*x1.diff() + k1*(x2 - x1))
eq2 = sp.Eq(m*x2.diff(t, 2), k1*(x1 - x2))
eq3 = sp.Eq(J1*th1.diff(t, 2), F_c*r + k2*(th2 - th1))
eq4 = sp.Eq(J2*th2.diff(t, 2), k2*(th1 - th2) - B*th2.diff())
eq5 = sp.Eq(x1.diff(t, 2), r*th1.diff(t, 2))
eqs = [eq1, eq2, eq3, eq4, eq5]
display(*eqs)
```

$$\begin{split} 0 &= -b\frac{d}{dt}x_1(t) + k_1\left(-x_1(t) + x_2(t)\right) - F_c(t) + f(t) \\ m\frac{d^2}{dt^2}x_2(t) &= k_1\left(x_1(t) - x_2(t)\right) \\ J_1\frac{d^2}{dt^2}\theta_1(t) &= k_2\left(-\theta_1(t) + \theta_2(t)\right) + rF_c(t) \\ J_2\frac{d^2}{dt^2}\theta_2(t) &= -B\frac{d}{dt}\theta_2(t) + k_2\left(\theta_1(t) - \theta_2(t)\right) \\ \frac{d^2}{dt^2}x_1(t) &= r\frac{d^2}{dt^2}\theta_1(t) \end{split}$$

Let's clean this up a little by considering the velocities v_1 , v_2 , ω_1 , and ω_2 . Also, let's omit considering the coordinate positions in the system and only look to the displacements of the compliance elements. I will define Δx and $\Delta \theta$ as

$$\begin{cases} \Delta x = x_2 - x_1 \\ \Delta \theta = \theta_2 - \theta_1 \end{cases}$$

```
[3]: d_theta = sp.Function(r'\Delta\theta')(t)
d_x = sp.Function(r'\Delta x')(t)

v1, v2 = sp.Function('v1')(t), sp.Function('v2')(t)
omega1, omega2 = sp.Function(r'\omega_1')(t), sp.Function(r'\omega_2')(t)

subs = [
    (x2 - x1, d_x),
    (th2 - th1, d_theta),
    (x1.diff(), v1),
    (x2.diff(), v2),
    (th1.diff(), omega1),
    (th2.diff(), omega2)
]

eqs = [eq.subs(subs) for eq in eqs]
display(*eqs)
```

$$\begin{split} 0 &= -bv_1(t) + k_1 \Delta x(t) - F_c(t) + f(t) \\ m \frac{d}{dt} v_2(t) &= -k_1 \Delta x(t) \\ J_1 \frac{d}{dt} \omega_1(t) &= k_2 \Delta \theta(t) + r F_c(t) \\ J_2 \frac{d}{dt} \omega_2(t) &= -B \omega_2(t) - k_2 \Delta \theta(t) \\ \frac{d}{dt} v_1(t) &= r \frac{d}{dt} \omega_1(t) \end{split}$$

Now we can solve this system for \dot{v}_1 , \dot{v}_2 , $\dot{\omega}_1$ $\dot{\omega}_2$. Additionally, I will solve for F_c to be used later.

$$\begin{split} F_c(t) &= -bv_1(t) + k_1 \Delta x(t) + f(t) \\ \frac{d}{dt} \omega_1(t) &= -\frac{brv_1(t)}{J_1} + \frac{k_1 r \Delta x(t)}{J_1} + \frac{k_2 \Delta \theta(t)}{J_1} + \frac{rf(t)}{J_1} \\ \frac{d}{dt} \omega_2(t) &= -\frac{B\omega_2(t)}{J_2} - \frac{k_2 \Delta \theta(t)}{J_2} \\ \frac{d}{dt} v_1(t) &= -\frac{br^2 v_1(t)}{J_1} + \frac{k_1 r^2 \Delta x(t)}{J_1} + \frac{k_2 r \Delta \theta(t)}{J_1} + \frac{r^2 f(t)}{J_1} \end{split}$$

$$\frac{d}{dt}v_2(t) = -\frac{k_1\Delta x(t)}{m}$$

Notice in the above solution that we don't have any terms that include ω_1 . This is due to the direct algebraic relationship and the order in which sympy solved the system. Therefore, we can ignore the $\dot{\omega}_1$ equation. Also, the solution for F_c is not an ODE so it isn't directly a part of the state space solution.

```
[5]: # Getting the final five equations
eq1 = sp.Eq(d_x.diff(), v2 - v1)
eq2 = sp.Eq(d_theta.diff(), omega2 - v1/r)
eq3 = sp.Eq(v1.diff(), state_sol[v1.diff()])
eq4 = sp.Eq(v2.diff(), state_sol[v2.diff()])
eq5 = sp.Eq(omega2.diff(), state_sol[omega2.diff()])
eqs = [eq1, eq2, eq3, eq4, eq5]
display(*eqs)
```

$$\begin{split} \frac{d}{dt}\Delta x(t) &= -v_1(t) + v_2(t) \\ \frac{d}{dt}\Delta \theta(t) &= \omega_2(t) - \frac{v_1(t)}{r} \\ \frac{d}{dt}v_1(t) &= -\frac{br^2v_1(t)}{J_1} + \frac{k_1r^2\Delta x(t)}{J_1} + \frac{k_2r\Delta \theta(t)}{J_1} + \frac{r^2f(t)}{J_1} \\ \frac{d}{dt}v_2(t) &= -\frac{k_1\Delta x(t)}{m} \\ \frac{d}{dt}\omega_2(t) &= -\frac{B\omega_2(t)}{J_2} - \frac{k_2\Delta \theta(t)}{J_2} \end{split}$$

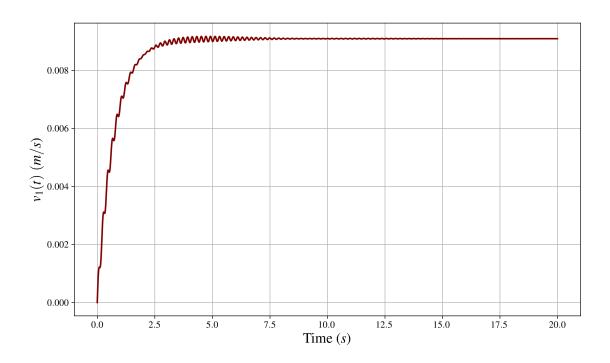
Answer

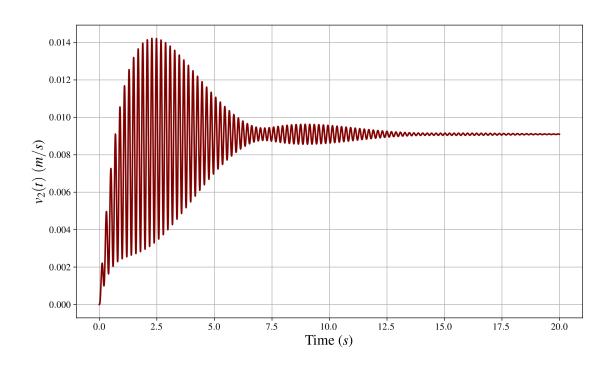
$$\begin{bmatrix} \frac{d}{dt}\Delta x(t) \\ \frac{d}{dt}\Delta \theta(t) \\ \frac{d}{dt}v_1(t) \\ \frac{d}{dt}v_2(t) \\ \frac{d}{dt}\omega_2(t) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \frac{r^2}{J_1} \\ 0 \\ 0 \end{bmatrix} \begin{bmatrix} f(t) \end{bmatrix} + \begin{bmatrix} 0 & 0 & -1 & 1 & 0 \\ 0 & 0 & -\frac{1}{r} & 0 & 1 \\ \frac{k_1r^2}{J_1} & \frac{k_2r}{J_1} & -\frac{br^2}{J_1} & 0 & 0 \\ -\frac{k_1}{m} & 0 & 0 & 0 & 0 \\ 0 & -\frac{k_2}{J_2} & 0 & 0 & -\frac{B}{J_2} \end{bmatrix} \begin{bmatrix} \Delta x(t) \\ \Delta \theta(t) \\ v_1(t) \\ v_2(t) \\ \omega_2(t) \end{bmatrix}$$

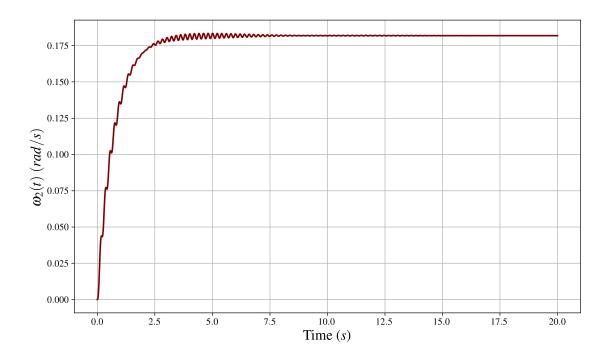
Part B

All we need to do is construct a python function that will return the right hand side of the equation above.

```
[7]: r_ = 0.05
     k1 = 1000
     k2_{-} = 500
     b_{-} = 100
     B_num = 2.5
     J1_{-} = J2_{-} = 1
     m_{-} = 1
     sub_vals = [
         (r, sp.Rational(5, 100)),
         (k1, k1_{-}),
         (k2, k2_),
         (b, b_),
         (B, sp.Rational(5, 2)),
         (J1, J1_),
         (J2, J2_),
         (m, m_)
     f_lamb = lambda t_: 10
     A_ = np.float64(A.subs(sub_vals))
     B_ = np.float64(B_sym.subs(sub_vals)).flatten()
     def state_vars(t_, y):
         return A_@y + B_*f_lamb(t_)
     sol1 = solve_ivp(state_vars, (0, 20), [0]*5, method='RK45', rtol=1e-9, __
      ⇒atol=1e-12)
     for i in range(2, 5):
         fig, ax = plt.subplots()
         ax.plot(sol1.t, sol1.y[i])
         unit = '\$(m/s\$)' if i != 4 else '\$(rad/s)\$'
         label = sp.latex(list(S)[i])
         ax.set_ylabel(f'${label}$ {unit}')
         ax.set_xlabel(f'Time ($s$)')
         plt.show()
```







The above uses scipy's RK45 solver, which is more convenient for determining the correct step size. Also, I am only showing the solutions for the velocities as they have more meaning than the displacements. This is why I'm a fan of not combining the state variables into a displacement, but this method is easier to do by hand and has fewer equations.

Verification of Parts A-B

Part C

We can further verify the results by testing to see if the energy was conserved with the following relationship:

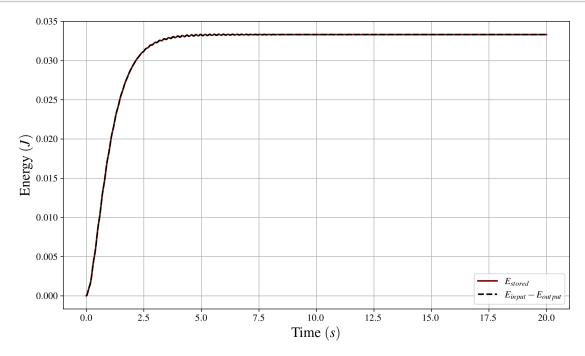
$$E_{stored}(t) = E_{input}(t) - E_{output}(t) \label{eq:estored}$$

```
E_stored = KE + PE

# input power
P_input = f_lamb(sol1.t)*v1_
E_input = cumulative_trapezoid(P_input, sol1.t, initial=0)

# output power
P_output = b_*v1_**2 + B_num*omega2_**2
E_output = cumulative_trapezoid(P_output, sol1.t, initial=0)

fig, ax = plt.subplots()
ax.plot(sol1.t, E_stored, label=r'$E_{stored}$')
ax.plot(sol1.t, E_input - E_output, label=r'$E_{input}-E_{output}$', ls='--')
ax.set_xlabel('Time $(s)$')
ax.set_ylabel(r'Energy $(J)$')
ax.legend()
plt.show()
```



Part D

You can see from the previous work that the contact force is

```
[9]: \begin{bmatrix} \texttt{state\_sol}[\texttt{F\_c}] \\ -bv_1(t) + k_1 \Delta x(t) + f(t) \end{bmatrix}
```

This means that you can represent C and D as

$$C = \begin{bmatrix} k_1 & 0 & -b & 0 & 0 \end{bmatrix}, \quad D = \begin{bmatrix} 1 \end{bmatrix}.$$

```
[10]: C = np.array([[k1_, 0, -b_, 0, 0]])
D = np.array([[1]])

ss = ct.ss(A_, B_.reshape(-1, 1), C, D)
ss
```

[10]:

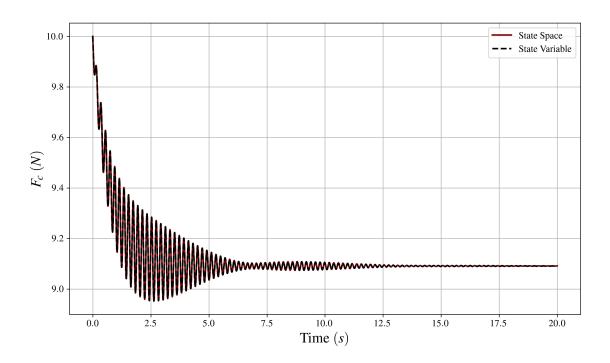
$$\begin{pmatrix} 0 & 0 & -1 & 1 & 0 & 0 \\ 0 & 0 & -20 & 0 & 1 & 0 \\ 2.5 & 25 & -0.25 & 0 & 0 & 0.0025 \\ -1 & \cdot 10^3 & 0 & 0 & 0 & 0 & 0 \\ \hline 0 & -500 & 0 & 0 & -2.5 & 0 \\ \hline 1 & \cdot 10^3 & 0 & -100 & 0 & 0 & 1 \end{pmatrix}$$

Here I used the control package to define the state space object. This library is more full-proof for this kind of work, and it offers an alternative to the matlab code in the undergraduate system dynamics book.

```
[11]: # Getting the contact force using the control package
    t_array = np.linspace(0, 20, sol1.t.size)
    _, F_c_ = ct.forced_response(ss, T=t_array, U=f_lamb(t_array))

# Here is the solution using the original solution
F_c_original = -b_*v1_ + k1_*d_x_ + f_lamb(t_array)

fig, ax = plt.subplots()
    ax.plot(t_array, F_c_, label='State Space')
    ax.plot(sol1.t, F_c_original, label='State Variable', ls='--')
    ax.set_xlabel('Time $(s)$')
    ax.set_ylabel('$F_c$ $(N)$')
    ax.legend()
    plt.show()
```



Part E

The control package has a function to transform this to a transfer function. We can also find the transfer function algebraically with sympy.

```
[12]: ct_tf = ct.ss2tf(ss) ct_tf
```

```
Answer
```

$$\frac{s^5 + 2.5s^4 + 2000s^3 + 3750s^2 + 1\times10^6s + 1.25\times10^6}{s^5 + 2.75s^4 + 2003s^3 + 4131s^2 + 1.002\times10^6s + 1.375\times10^6}$$

```
[13]: # Getting the symbolic solution
    eqs_with_contact = eqs + [sp.Eq(F_c, state_sol[F_c])]

laplace = lambda expr: sp.laplace_transform(expr, t, s, noconds=True)

initial = [
    (d_x.subs(t, 0), 0),
    (d_theta.subs(t, 0), 0),
    (v1.subs(t, 0), 0),
    (v2.subs(t, 0), 0),
    (omega2.subs(t, 0), 0)
]
```

$$\mathcal{L}_{t}\left[\Delta x(t)\right](s) = \frac{mr^{2}s\left(-mr^{2}s}\left(-mr^{2}s\left(-\frac{mr^{2}s}\left(-\frac{mr^{2}s\left(-mr^{2}s\left(-mr^{2}s\left(-mr^{2}s\left(-$$

 $\mathcal{L}_{t}\left[F_{c}(t)\right](s) = \frac{\left(BJ_{1}k_{1}s^{2} + BJ_{1}ms^{4} + Bk_{1}k_{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{1}k_{1}k_{2} + BJ_{1}ms^{4} + Bbk_{1}r^{2}s + Bbmr^{2}s^{3} + Bk_{1}k_{2} + Bk_{1}mr^{2}s^{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{1}s^{3} + J_{1}J_{2}ms^{4}s^{2} + Bbmr^{2}s^{3} + Bk_{1}k_{2} + Bk_{1}mr^{2}s^{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{1}s^{3} + J_{1}J_{2}ms^{4}s^{2} + Bbmr^{2}s^{3} + Bk_{1}k_{2} + Bk_{1}mr^{2}s^{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{1}s^{3} + Bk_{1}k_{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{1}s^{3} + Bk_{1}k_{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{1}s^{3} + Bk_{1}k_{2} + Bk_{2}ms^{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{1}s^{3} + Bk_{2}ms^{2} + J_{1}J_{2}k_{2}s^{3} + Bk_{2}ms^{2} + J_{1}J_{2}k_{2}s^{3} + Bk_{2}ms^{2} + J_{1}J_{2}k_{2}s^{3} + Bk_{2}ms^{2} + Bk_{2}ms^{2} + J_{1}J_{2}k_{2}s^{3} + Bk_{2}ms^{2} + J_{1}J_{2}k_{2}s^{3} + Bk_{2}ms^{2} + J_{2}ms^{2} + Bk_{2}ms^{2} + J_{2}ms^{2} + Bk_{2}ms^{2} + Bk_$

Very large expressions! Note that the denominator is the same across all results. This means we are doing good!

```
[14]: # Only getting the contact force and substituting values
sp_tf = sol_s[laplace(F_c)]/laplace(f)
sp_tf = sp_tf.subs(sub_vals).simplify()
sp_tf
```

[14]: $\frac{4 \left(2 s^5+5 s^4+4000 s^3+7500 s^2+2000000 s+2500000\right)}{8 s^5+22 s^4+16025 s^3+33050 s^2+8015000 s+11000000}$

The results are a match.

Verification of Parts D-E

Part F

```
[15]: # Taking the inverse laplace to solve for F_c
F_c_s = sp_tf*10/s
num, den = sp.fraction(F_c_s)
num = sp.Poly(num.expand(), s)
den = sp.Poly(den.expand(), s)
F_poly = num.as_expr()/den.as_expr()
# f_c_t = sp.inverse_laplace_transform(F_poly, s, t)
# f_c_t
F_poly
```

[15]:

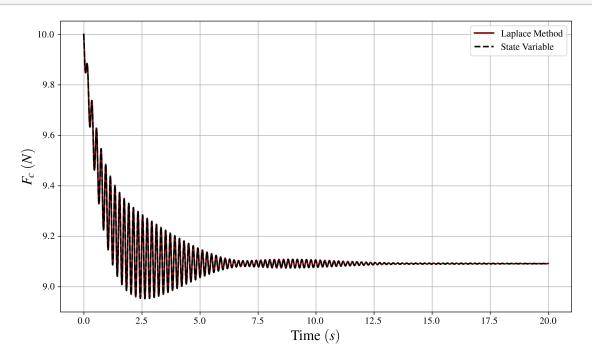
```
\frac{80s^5 + 200s^4 + 160000s^3 + 300000s^2 + 80000000s + 100000000}{8s^6 + 22s^5 + 16025s^4 + 33050s^3 + 8015000s^2 + 110000000s}
```

That above cell will result in an error due to complexity. I tried getting this symbolically with MatLab as well. I guess we can do it manually.

```
[16]: # Find roots
      r1, r2, r3, r4, r5, r6 = roots = sp.nroots(den)
      display(*roots)
      factor_den = sp.prod([(s - root) for root in roots])
      F c s = num/8/factor den
      F_c_s.n(5)
      -1.3750300358734
      0
      -0.379308107105189 - 31.1793861747501i
      -0.379308107105189 + 31.1793861747501i
      -0.308176874958113 - 32.0682682599475i
      -0.308176874958113 + 32.0682682599475i
[16]:
                          10.0s^5 + 25.0s^4 + 20000.0s^3 + 37500.0s^2 + 1.0 \cdot 10^7 s + 1.25 \cdot 10^7
      \overline{s(s+1.375)(s+0.30818-32.068i)(s+0.30818+32.068i)(s+0.37931-31.179i)(s+0.37931+31.179i)}
[17]: C1 = (F_c_s*s).subs(s, 0).simplify()
      C2 = (F_c_s*(s + -r1)).subs(s, r1).simplify()
      C3 = (F c s*(s + -r3)).subs(s, r3).simplify()
      C4 = (F_c_s*(s + -r4)).subs(s, r4).simplify()
      C5 = (F_c_s*(s + -r5)).subs(s, r5).simplify()
      C6 = (F_c_s*(s + -r6)).subs(s, r6).simplify()
      F_c_s_rhs = C1/s + C2/(s - r1) + C3/(s - r3) + C4/(s - r4) + C5/(s - r5) + C6/(s - r5)
       \hookrightarrow(s - r6)
      F_c_s_rhs.n(5)
      [17]: -0.1001 - 0.010002i
                             \frac{-0.1001 + 0.010002i}{s + 0.37931 - 31.179i} + \frac{0.10772 - 0.01024i}{s + 0.30818 + 32.068i} + \frac{0.10772 + 0.01024i}{s + 0.30818 - 32.068i}
      \frac{0.89384}{s+1.375} + \frac{9.0909}{s}
      The above representation is good enough for sympy to take the inverse Laplace.
[18]: f_c_t = sp.inverse_laplace_transform(F_c_s, s, t)
      f_c_t_lamb = sp.lambdify(t, f_c_t, modules='numpy')
      fig, ax = plt.subplots()
      ax.plot(t_array, np.real(f_c_t_lamb(t_array)), label='Laplace Method')
      ax.plot(sol1.t, F c original, label='State Variable', ls='--')
      ax.set_xlabel('Time $(s)$')
      ax.set ylabel('$F c$ $(N)$')
```

ax.legend()

plt.show()



```
[19]: # Roots of cp
_, cp_den = sp.fraction(sp_tf)
cp_roots = sp.nroots(cp_den)
display(*cp_roots)
```

- -1.3750300358734
- -0.379308107105189 31.1793861747501i
- -0.379308107105189 + 31.1793861747501i
- -0.308176874958113 32.0682682599475i
- -0.308176874958113 + 32.0682682599475i

We can get the time constant.

```
[20]: # Getting time constant
    cp_roots_ = np.complex64(cp_roots)
    taus = -1/np.real(cp_roots_)
    tau_max = np.max(taus)
    float(tau_max) # dominant root
```

[20]: 3.244889736175537

[21]: float(4.6*tau_max)

[21]: 14.926492691040039

The analysis above shows us that the system should reach steady state in about 15 seconds and the graphs confirm this.

```
[22]: # Getting peak to peak oscillation periods
1/np.imag(cp_roots_[1:])*2*np.pi # seconds
```

[22]: array([-0.2015173 , 0.2015173 , -0.19593155, 0.19593155], dtype=float32)

Looking at the imaginary component shows us that we should have oscillations from peak to peak at 0.2 second time intervals. The graphs show this as well!