

ESD Homework 2

March 7, 2022

```
[1]: import sympy as sp
from msu_esd import cross_flow_unmixed, log_mean_temp_difference,
    ↪parallel_single_pass, counter_single_pass
```

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1 Problem 1

1.1 Given

Water enters a counterflow, double-pipe heat exchanger at a rate of $70 \frac{kg}{min}$ and is heated from $15^\circ C$ to $60^\circ C$ by an oil with a specific heat of $1.9 \frac{kJ}{kg K}$. The oil enters at $116^\circ C$ and leaves at $27^\circ C$. The overall heat transfer coefficient is $300 \frac{W}{m^2 K}$

1.2 Find

- What heat transfer area is required?
- What area is required if all conditions remain the same except that a shell and tube heat exchanger is used, with the water making one shell pass and the oil making two tube passes?
- What exit water temperature would result if, for the exchanger of part (a), the water flow rate were decreased to $50 \frac{kg}{min}$

1.3 Solution

The specific heat of water will be taken at the average temperature of the water entrance and exit ($C_p = 4.18 \frac{kJ}{kg K}$)

1.3.1 Part A

The oil is the hot fluid and the water is the cold fluid. The condition is unmixed because the fluids never meet.

```
[2]: # Declare constants as given
mc_ = 70
Cp_c_, Cp_h_ = 4.18, 1.9
Tc_in_, Tc_out_ = 15, 60
Th_in_, Th_out_ = 116, 27
U_ = 300

Cc, Ch, Th_out, Th_in, Tc_out, Tc_in = sp.symbols(r'C_c C_h T_{h\,out} \_
→T_{h\,in} T_{c\,out} T_{c\,in}')

# Solving for Ch
eq = sp.Eq(Cc*(Tc_out - Tc_in), Ch*(Th_in - Th_out))
eq
```

[2]: $C_c(-T_{c,in} + T_{c,out}) = C_h(T_{h,in} - T_{h,out})$

```
[3]: Ch_solved = sp.solve(eq, Ch)[0]
Ch_solved
```

[3]:
$$\frac{C_c(-T_{c,in} + T_{c,out})}{T_{h,in} - T_{h,out}}$$

```
[4]: # Solving for Cc
Cc_ = mc_*Cp_c_
Cc_ # kJ per (min deg C)
```

```
[4]: 292.59999999999997
```

```
[5]: Ch_ = Cc_*(Tc_out_ - Tc_in_)/(Th_in_ - Th_out_)
Ch_ # kJ per (min deg C)
```

```
[5]: 147.94382022471908
```

```
[6]: C_min_ = min([Ch_, Cc_])
C_min_ # kJ per (min deg C)
```

```
[6]: 147.94382022471908
```

```
[7]: # Get actual q
q_act_ = Cc_*(Tc_out_ - Tc_in_)
q_act_ # kJ per min
```

```
[7]: 13166.999999999998
```

```
[8]: # Get q max
q_max_ = C_min_*(Th_in_ - Tc_in_)
q_max_ # kJ per min
```

```
[8]: 14942.325842696626
```

```
[9]: # Effectiveness
epsilon_ = q_act_/q_max_
epsilon_
```

```
[9]: 0.8811881188118813
```

```
[10]: # C
C_ = C_min_/Cc_
C_
```

```
[10]: 0.5056179775280899
```

```
[11]: # Find the ntu value
ntu_ = cross_flow_unmixed(epsilon_, C_)
ntu_
```

```
[11]: 4.180545804015178
```

The NTU relationship is,

$$NTU = \frac{UA}{C_{min}} \rightarrow A = NTU \frac{C_{min}}{U}$$

```
[12]: # Finding the area (unit manipulation added)
A_ = ntu*C_min_/U_*1000/60
A_ # m2
```

```
[12]: 34.36032871502362
```

1.3.2 LMTD Method

```
[13]: T_ = log_mean_temp_difference(Th_in_, Th_out_, Tc_in_, Tc_out_)
q_act_/(U_*T_)*1000/60
```

```
[13]: 25.60989880574635
```

2 Problem 2

2.1 Given

The attributes of the inlet streams to a heat exchanger are,

Stream	Inlet Temperature ($^{\circ}F$)	Capacity ($\frac{Btu}{hr^{\circ}F}$)
Hot	600	50,000
Cold	500	25,000

The UA product in $\frac{Btu}{hr^{\circ}F}$ for the heat exchanger is given by,

$$UA = \frac{1}{\frac{0.12}{C_h^{0.8}} + \frac{0.06}{C_c^{0.8}} + 2 \times 10^{-7}}$$

where C_h and C_c are the capacities in $\frac{Btu}{hr^{\circ}F}$.

2.2 Find

Using only the NTU method,

- Find the outlet temperatures and rating for a parallel flow arrangement
- Find the outlet temperatures and rating for a counter flow arrangement
- Find the outlet temperatures and rating if two of these heat exchangers are placed in series and are operated in a parallel flow arrangement. What are the interface temperatures?
- Find the outlet temperatures and rating if two of these heat exchangers are placed in series and operated in a counterflow arrangement. What are the interface temperatures?
- Based on the results of the above, discuss the utility of placing parallel and counterflow heat exchangers in series.

2.3 Solution

```
[14]: # Define known constants with units mentioned in the given statement
Cc_ = 25_000
Ch_ = 50_000
Tc_in_ = 500
Th_in_ = 600

# Find the value for UA
# First a symbolic definition
UA = 1/(0.12/Ch**0.8 + 0.06/Cc**0.8 + 2e-7)
UA
```

[14]:
$$\frac{1}{\frac{0.06}{C_c^{0.8}} + \frac{0.12}{C_h^{0.8}} + 2.0 \cdot 10^{-7}}$$

```
[15]: UA_ = float(UA.subs([(Cc, Cc_), (Ch, Ch_)]))  
      UA_ # In Btu per (hr*deg F)
```

```
[15]: 25457.073923275435
```

```
[16]: # Find NTU  
      C_min_ = min([Cc_, Ch_])  
      NTU_ = UA_/C_min_  
      NTU_
```

```
[16]: 1.0182829569310174
```

```
[17]: # Get the C_value  
      C_ = C_min_/max([Cc_, Ch_])  
      C_
```

```
[17]: 0.5
```

2.3.1 Part A

We know the NTU value and C , which is enough to solve for the effectiveness.

```
[18]: # Get the effectiveness/rating  
      # Assuming a one pass parallel  
      parallel_effectiveness = parallel_single_pass(NTU_, C_, find='e')  
      parallel_effectiveness
```

```
[18]: 0.5219372748457521
```

```
[19]: # Find q max  
      q_max_ = C_min_*(Th_in_ - Tc_in_)  
      q_max_ # Btu per hr
```

```
[19]: 2500000
```

```
[20]: # Find the actual q  
      q_act_ = q_max_*parallel_effectiveness  
      q_act_ # In btu per hour
```

```
[20]: 1304843.1871143803
```

```
[21]: # Find cold outlet temperature  
      Tc_out_A = q_act_/Cc_ + Tc_in_  
      Tc_out_A # deg F
```

```
[21]: 552.1937274845752
```

```
[22]: # Find the hot outlet temperature
Th_out_A = Th_in_ - q_act_/Ch_
Th_out_A # deg F
```

[22]: 573.9031362577124

2.3.2 Part B

Everything is the same except the effectiveness correlation is different.

```
[23]: # Solving for the effectiveness/rating
counter_effectiveness = counter_single_pass(NTU_, C_, find='e')
counter_effectiveness
```

[23]: 0.5703958472801851

```
[24]: q_act_ = q_max_*counter_effectiveness
q_act_ # Btu per hr
```

[24]: 1425989.6182004628

```
[25]: # Find cold outlet temperature
Tc_out_B = q_act_/Cc_ + Tc_in_
Tc_out_B # deg F
```

[25]: 557.0395847280186

```
[26]: # Find the hot outlet temperature
Th_out_B = Th_in_ - q_act_/Ch_
Th_out_B # deg F
```

[26]: 571.4802076359907

2.3.3 Part C

In order to solve this, take the outlet temperatures solved in the previous problems and apply that to the next heat exchanger in the series. The values of NTU , C , ξ , and UA are all the same because the capacity and conductance does not change.

```
[27]: # From the part A in deg F
Tc_in_ = Tc_out_A
Th_in_ = Th_out_A

q_max_ = C_min_*(Th_in_ - Tc_in_)
q_max_ # Btu per hr
```

[27]: 542735.2193284292


```
[28]: q_act_ = parallel_effectiveness*q_max_  
q_act_ # Btu per hr
```

```
[28]: 283273.7413390919
```

```
[29]: Tc_out_ = q_act_/Cc_ + Tc_in_  
Tc_out_ # deg F
```

```
[29]: 563.5246771381389
```

```
[30]: Th_out_ = Th_in_ - q_act_/Ch_  
Th_out_ # deg F
```

```
[30]: 568.2376614309305
```

2.4 Answer

- $\xi = 0.522$, $T_{c,out} = 552.19^\circ F$, $T_{h,out} = 573.90^\circ F$
- $\xi = 0.570$, $T_{c,out} = 557.04^\circ F$, $T_{h,out} = 571.48^\circ F$
- Effectiveness and temperatures at the interface is the same as Part A. Coming out of the second heat exchanger is: $T_{c,out} = 563.52^\circ F$, $T_{h,out} = 568.2^\circ F$
- d.