

ELEC353 Lecture Notes Set 13

The homework assignments are posted on the course web site.

http://users.encs.concordia.ca/~trueman/web_page_353.htm

Homework #7: Do homework #7 by March 8, 2019.

Homework #8: Do homework #8 by March 15, 2019.

Homework #9: Do homework #9 by March 22, 2019.

Tutorial Workshop #8: Friday March 8, 2019.

Tutorial Workshop #9: Friday March 15, 2019.

Tutorial Workshop #10: Friday March 22, 2019.

Final exam date: Tuesday April 23, 2019, 9:00 to 12:00, in H531.

Topics to be Covered

Transmission Lines (TLs)

- Wave Equation and Solution - done
- Solving a TL Circuit - done
- Standing Wave Patterns - done
- Impedance Matching – today's class
- Bandwidth of Digital Signal

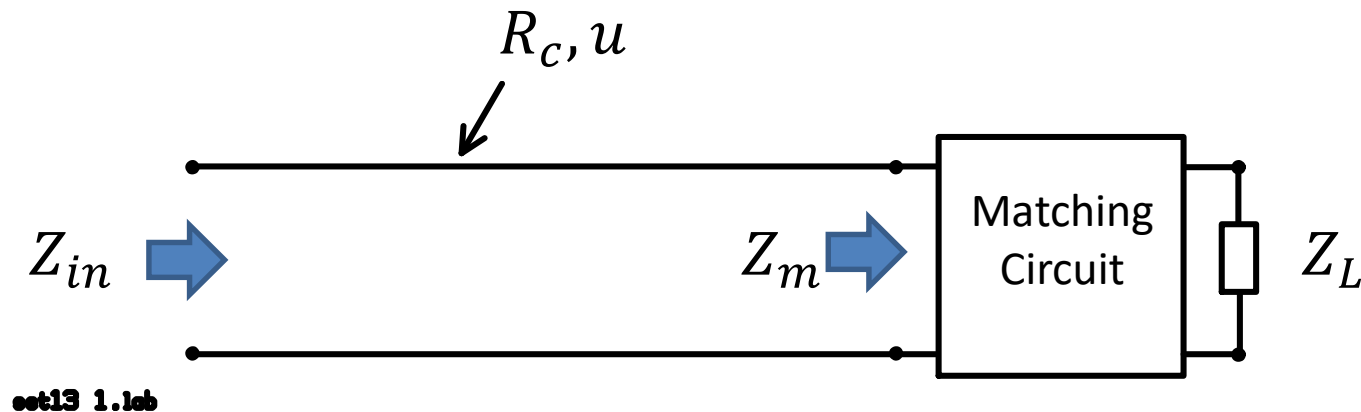
Plane Waves

- Maxwell's Equations and the Wave Equation
- Plane waves
- Material Boundaries
- Transmission Through a Wall

Antennas

Impedance Matching

Inan and Inan Section 3.5



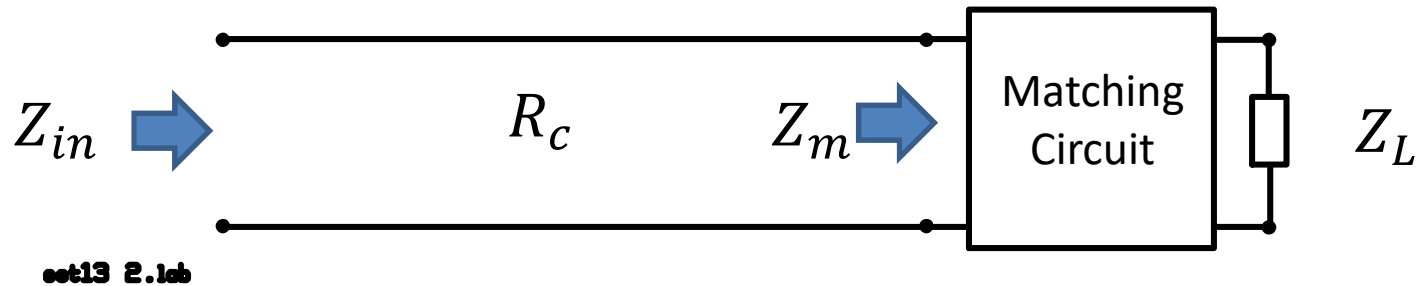
What can we use for the “matching circuit”?

- Quarter wave transformer
- Line plus quarter wave transformer
- Many other schemes are available!

The matching circuit is designed to provide a perfect match at the “center frequency” f_0 .

The **bandwidth** of the match is the range of frequencies over which the match is “sufficiently good”.

Return Loss



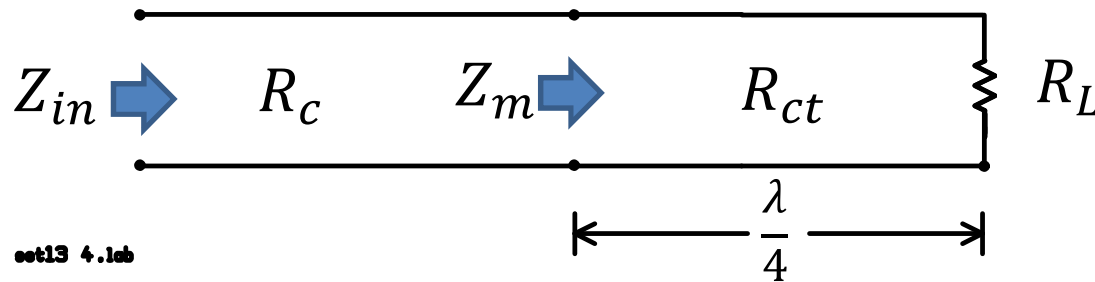
$$\Gamma_m(f) = \frac{Z_m(f) - R_c}{Z_m(f) + R_c}$$

- The “return loss” is defined as

$$R.L. = 20\log|\Gamma_m| \text{ decibels or “dB”}.$$
- For consumer electronics, the maximum reflection coefficient is often set at $|\Gamma_{max}| = 0.316$, so $R.L. \leq -10 \text{ dB}$.
- For precision applications, $|\Gamma_{max}| = 0.1$ is often used, so $R.L. \leq -20 \text{ dB}$.
- The bandwidth is defined as the frequency range over which the reflection coefficient meets the standard that $|\Gamma_m| \leq |\Gamma_{max}|$.
- Connectors have a return loss of -30 to -40 dB.
- A “matched load” has a return loss of about -40 dB.

Quarter-Wave Transformer

Inan and Inan Section 3.5.3



$$Z_m = R_{ct} \frac{Z_L + jR_{ct} \tan \beta L}{R_{ct} + jZ_L \tan \beta L} = R_{ct} \frac{R_L + jR_{ct} \tan \beta L}{R_{ct} + jR_L \tan \beta L}$$

$$L = \frac{\lambda}{4} \quad \beta L = \frac{2\pi}{\lambda} \frac{\lambda}{4} = \frac{\pi}{2} \quad \tan \beta L = \tan \frac{\pi}{2} \rightarrow \infty$$

$$Z_m = R_{ct} \lim_{\tan \beta L \rightarrow \infty} \frac{R_L + jR_{ct} \tan \beta L}{R_{ct} + jR_L \tan \beta L}$$

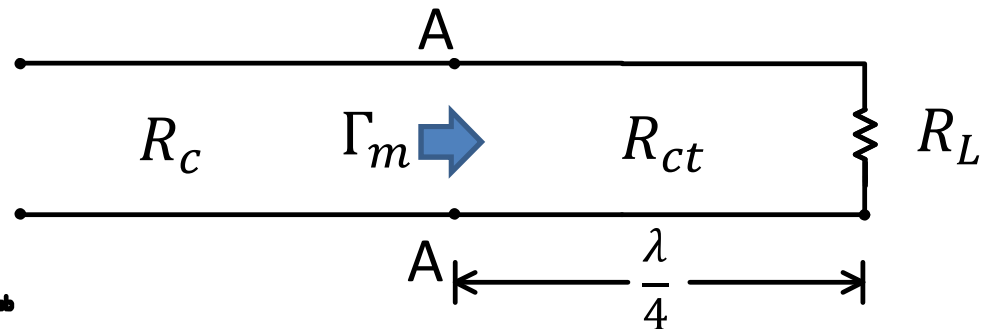
$$Z_m = R_{ct} \lim_{\tan \beta L \rightarrow \infty} \frac{jR_{ct} \tan \beta L}{jR_L \tan \beta L} = \frac{R_{ct}^2}{R_L} \quad \text{so } Z_m = \frac{R_{ct}^2}{R_L}$$

We want $Z_m = R_c$ so $\frac{R_{ct}^2}{R_L} = R_c$ so choose $R_{ct} = \sqrt{R_c R_L}$

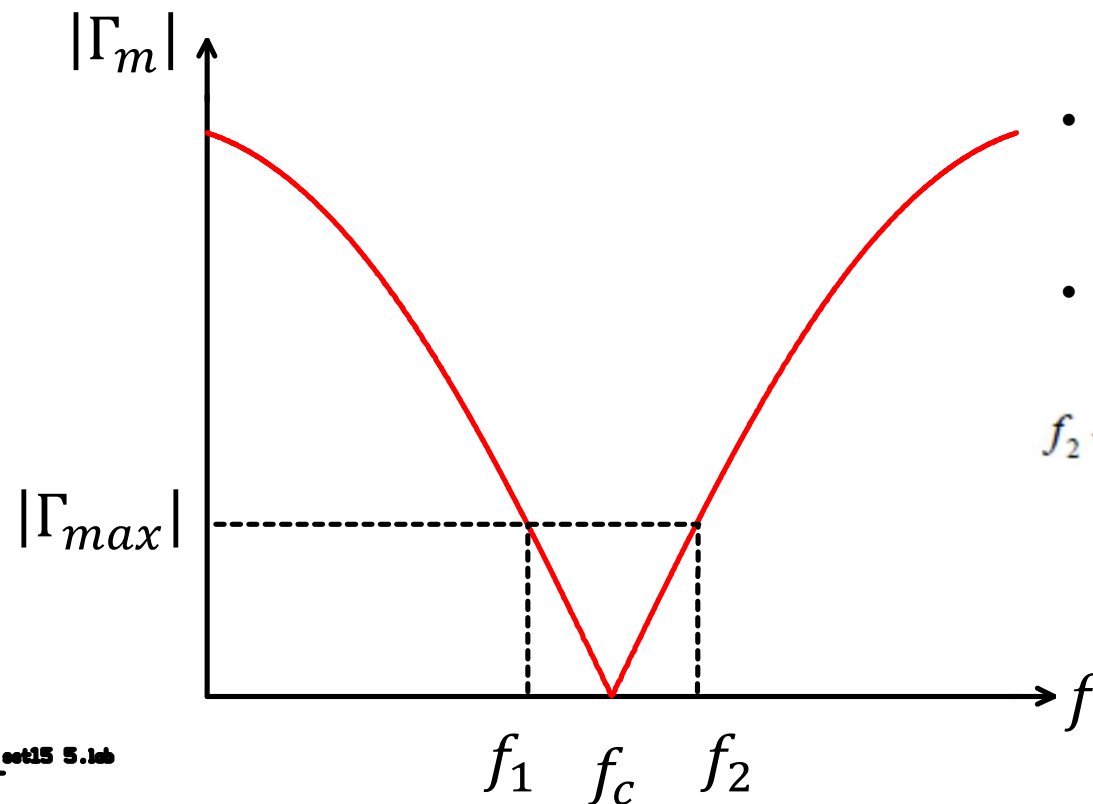
What is the bandwidth?

At terminals AA:

$$\Gamma_m(f) = \frac{Z_m(f) - R_c}{Z_m(f) + R_c}$$



set13 4.1ab



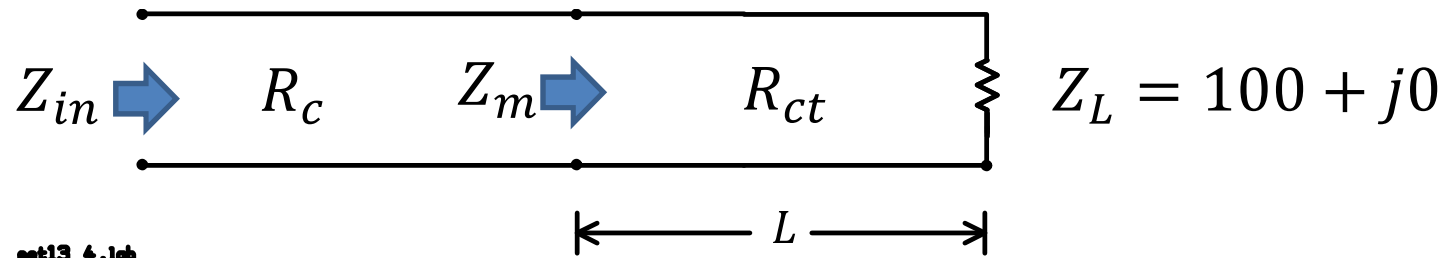
set15 5.1ab

- The bandwidth is the frequency range for which $|\Gamma_m| \leq |\Gamma_{max}|$,
 $BW = f_2 - f_1$
- Formula for the bandwidth:

$$f_2 - f_1 \approx f_c \left[2 - \frac{4}{\pi} \cos^{-1} \left(\frac{\Gamma_m}{\sqrt{1 - \Gamma_m^2}} \frac{2\sqrt{R_c R_L}}{|R_L - R_c|} \right) \right]$$

David Pozar, "Microwave Engineering", Addison-Wesley, 1990.

Example: quarter-wave transformer



At 850 MHz, an antenna with an input impedance of $Z_L = 100 + 0j$ ohms must be matched to a transmission line of characteristic impedance $R_c = 50$ ohms. The speed of travel on the transmission line is $u = 30$ cm/ns.

1. Design a quarter-wave transformer by choosing the length L and the characteristic impedance R_{ct} .
2. Use Pozar's formula to find the bandwidth for a return loss of 20 dB or better.
3. Verify that your design works with TRLINE.
4. Use TRLINE to find the bandwidth of the match and compare with Pozar's value.

Solution

$$f_c = 850 \text{ MHz} \qquad \lambda = \frac{u}{f_c} = \frac{300}{850} = 35.29 \text{ cm.}$$

$$L = \frac{\lambda}{4} = \frac{35.29}{4} = 8.82 \text{ cm.}$$

$$R_{ct} = \sqrt{R_c R_L} = \sqrt{50 \cdot 100} = 70.71 \text{ ohms.}$$

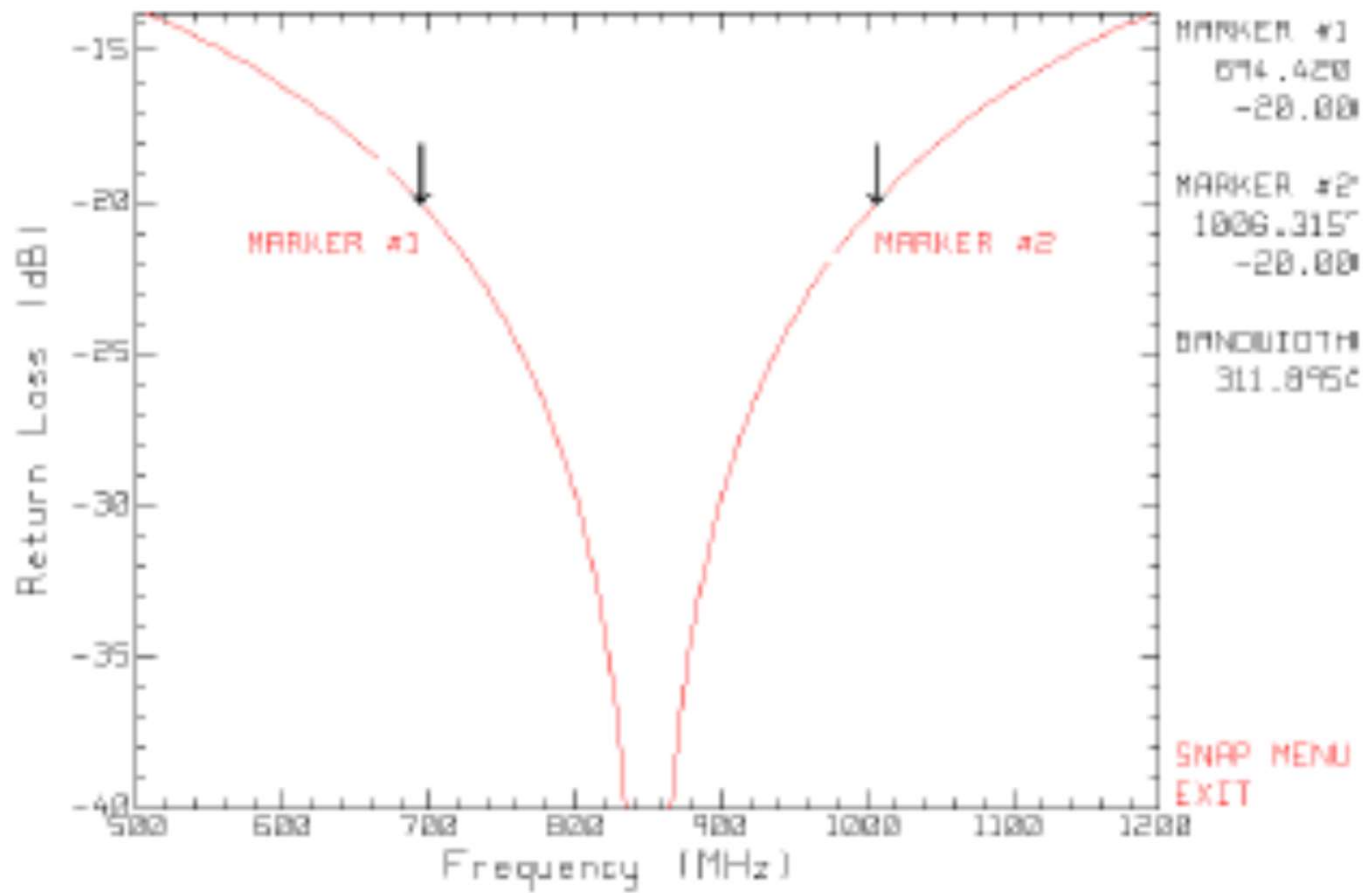
$$\text{return loss of 20 dB} \qquad -20 \log \Gamma_m = 20 \text{ dB} \qquad \Gamma_m = 0.1$$

$$f_2 - f_1 \approx f_c \left[2 - \frac{4}{\pi} \cos^{-1} \left(\frac{\Gamma_m}{\sqrt{1 - \Gamma_m^2}} \frac{2\sqrt{R_c R_L}}{|R_L - R_c|} \right) \right]$$

$$f_2 - f_1 \approx 850 \left[2 - \frac{4}{\pi} \cos^{-1} \left(\frac{0.1}{\sqrt{1 - 0.1^2}} \frac{2 \cdot 70.71}{|100 - 50|} \right) \right]$$

$$f_2 - f_1 \approx 850 \left[2 - \frac{4}{\pi} \cdot 1.28253 \right] = 311.95 \text{ MHz}$$

Use TRLINE to find the bandwidth

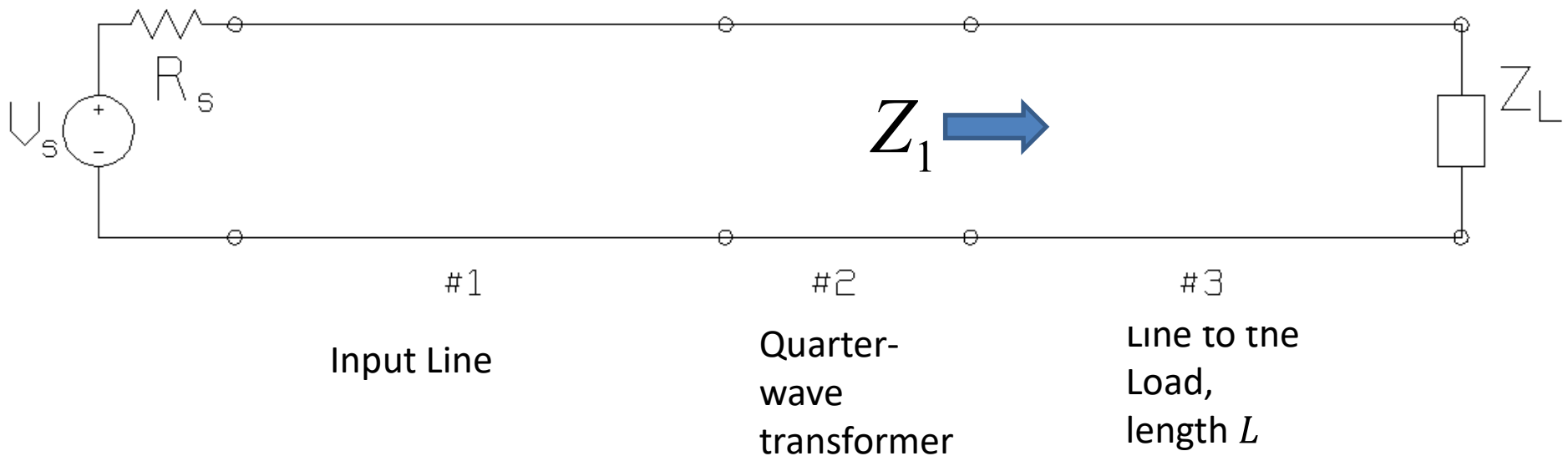


This agrees well with the Pozar formula, $f_2 - f_1 \approx 311.95$ MHz.

Matching a Complex-Valued Load

How do we match a complex-valued load?

Match a load of $Z_L = 100 - j45$ ohms to a transmission line with $R_c = 50$ ohms at 850 MHz. The speed of travel on the transmission lines is $u = 30$ cm/ns.

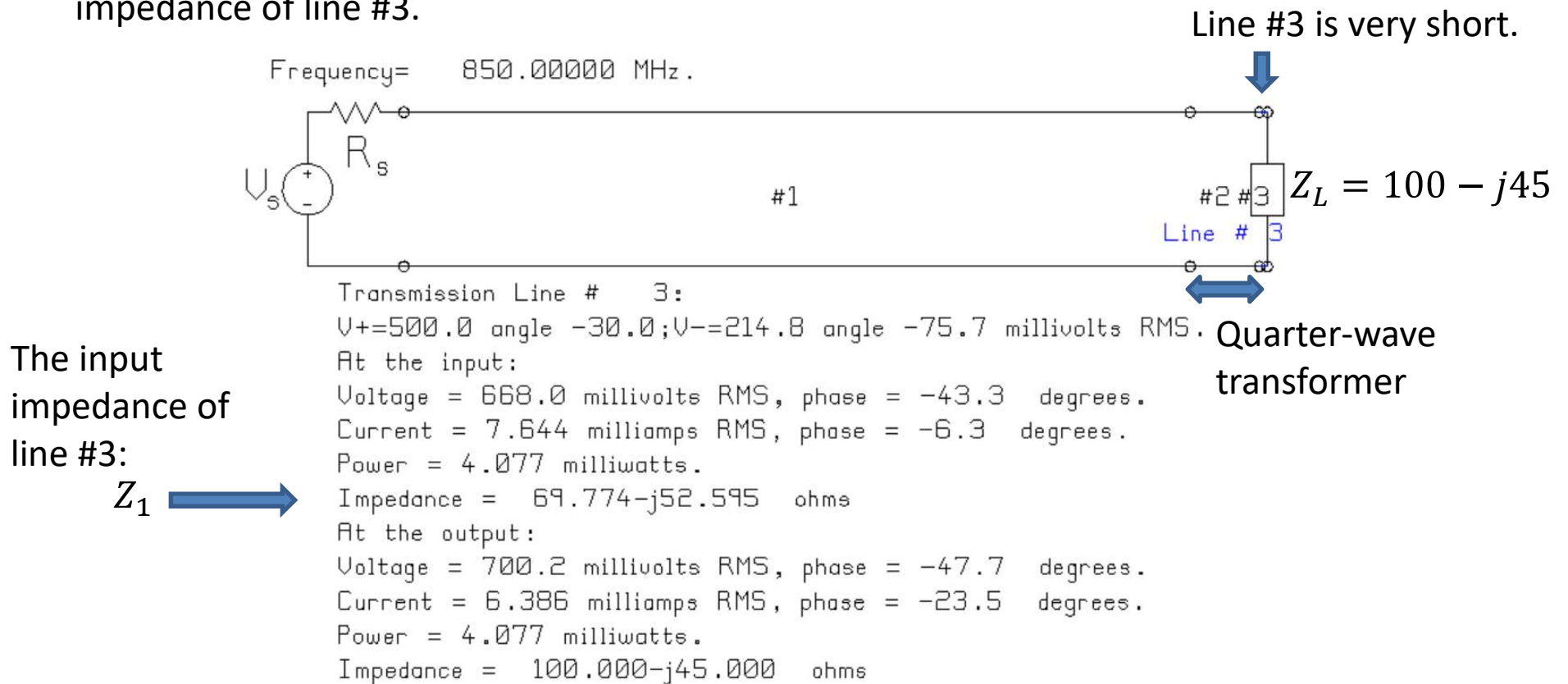


Idea: put a transmission line in series with the load and adjust the length to get a real-valued input impedance.

Trial and Error Solution

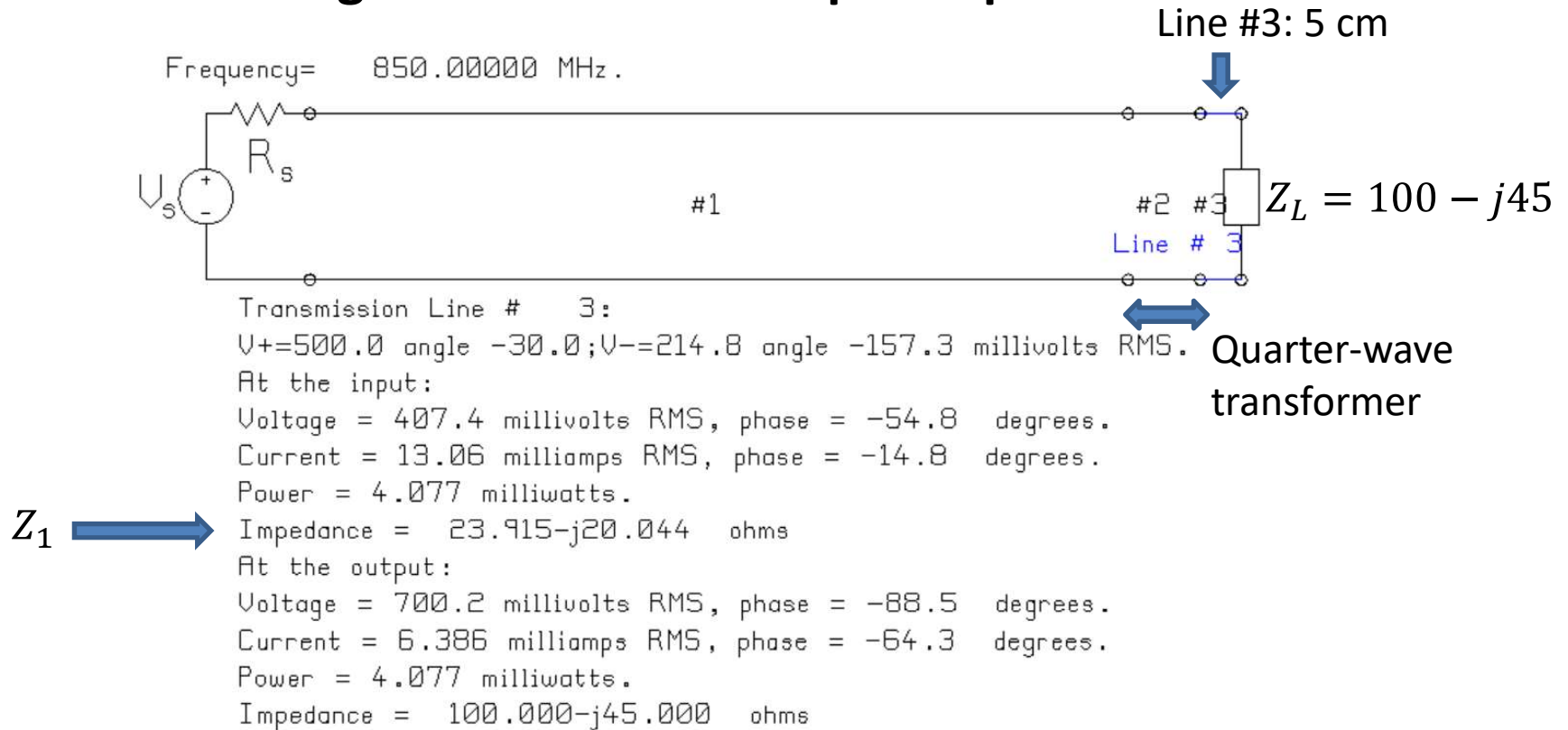
The transformer length is $\frac{\lambda}{4} = \frac{u/f}{4} = \frac{300/850}{4} = 0.0882 \text{ m}$

Start with line #3 short and gradually increase the length. Monitor Z_1 , the input impedance of line #3.



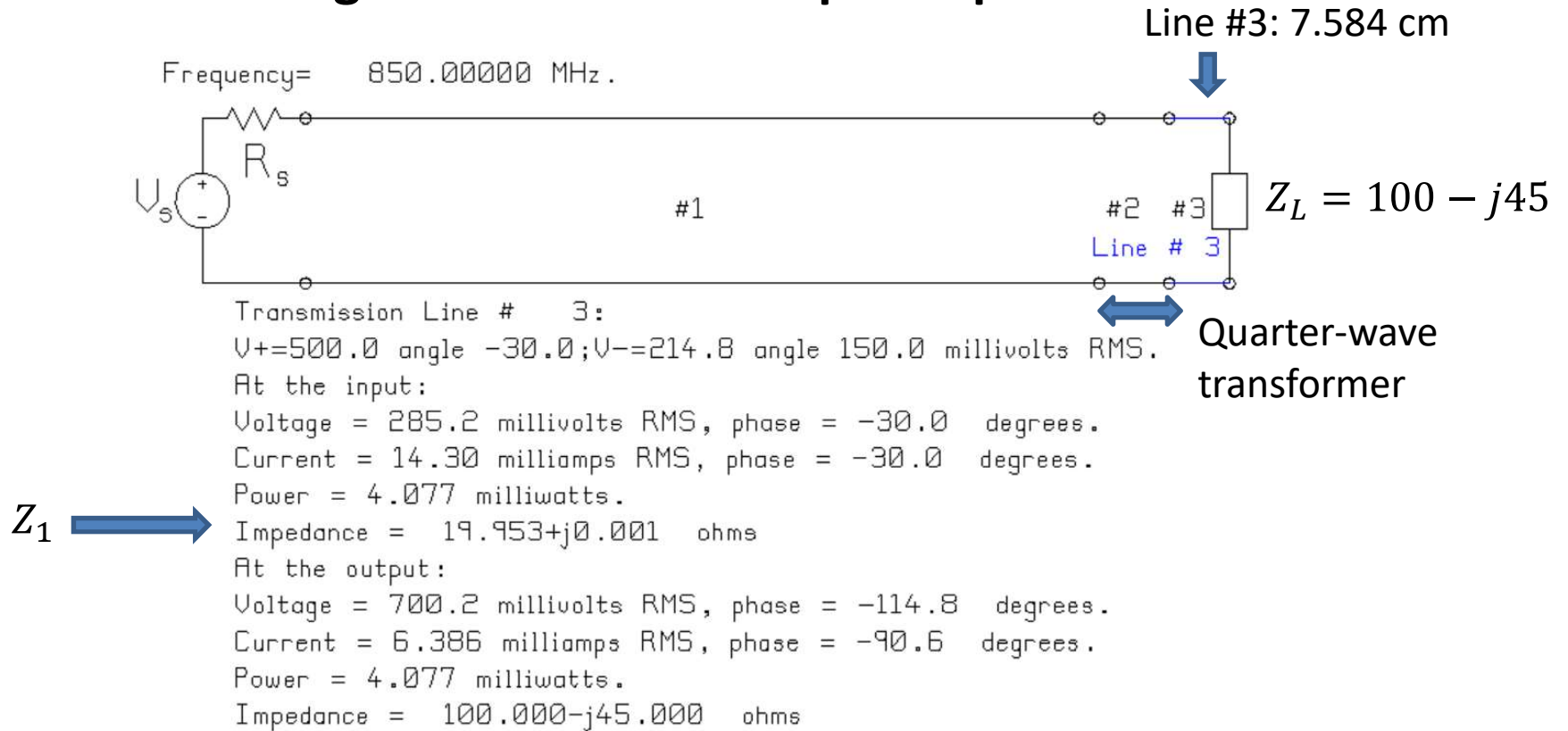
$$Z_1 = 69.774 - j52.595$$

Make line #3 longer and watch the input impedance:



$$Z_1 = 23.915 - j20.044$$

Make line #3 longer and watch the input impedance:

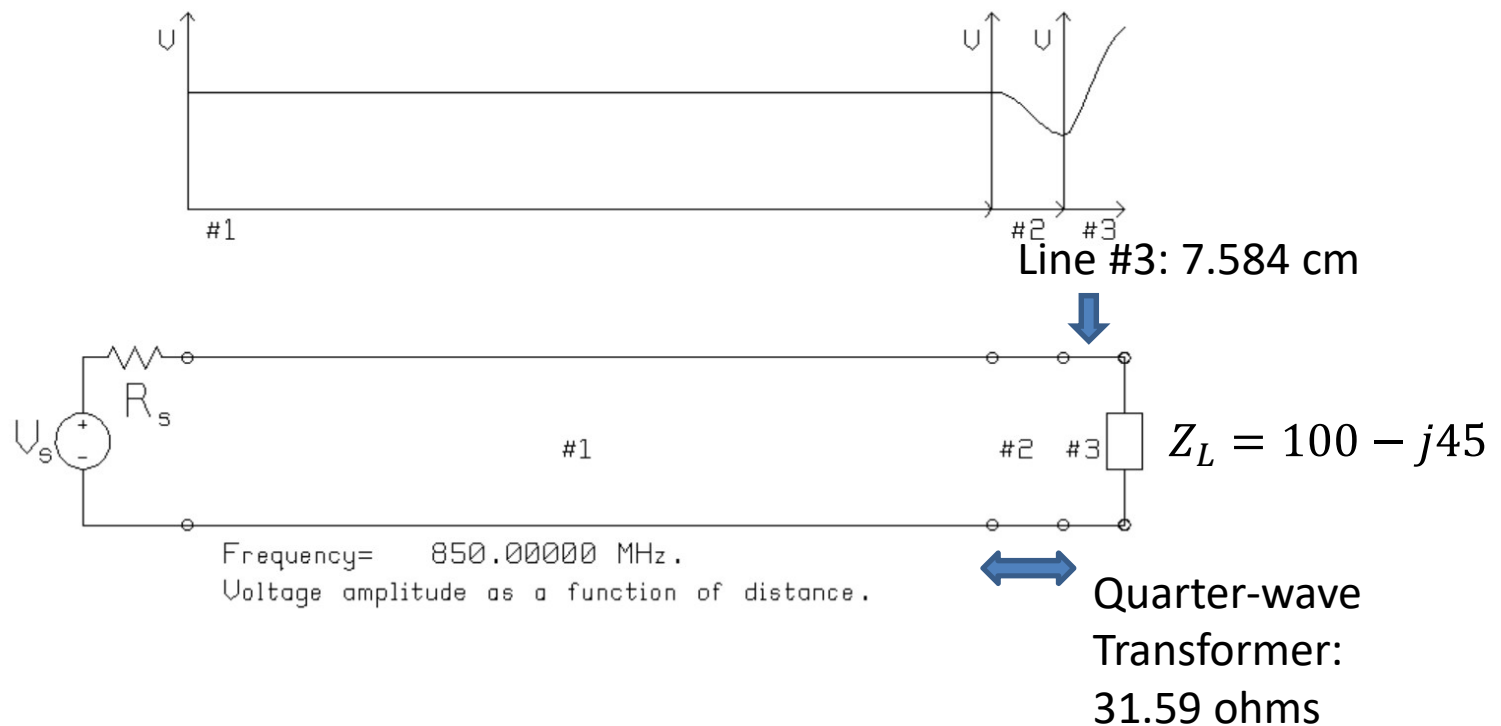


$$Z_1 = 19.953 + j0.001$$

Design the quarter-wave transformer:

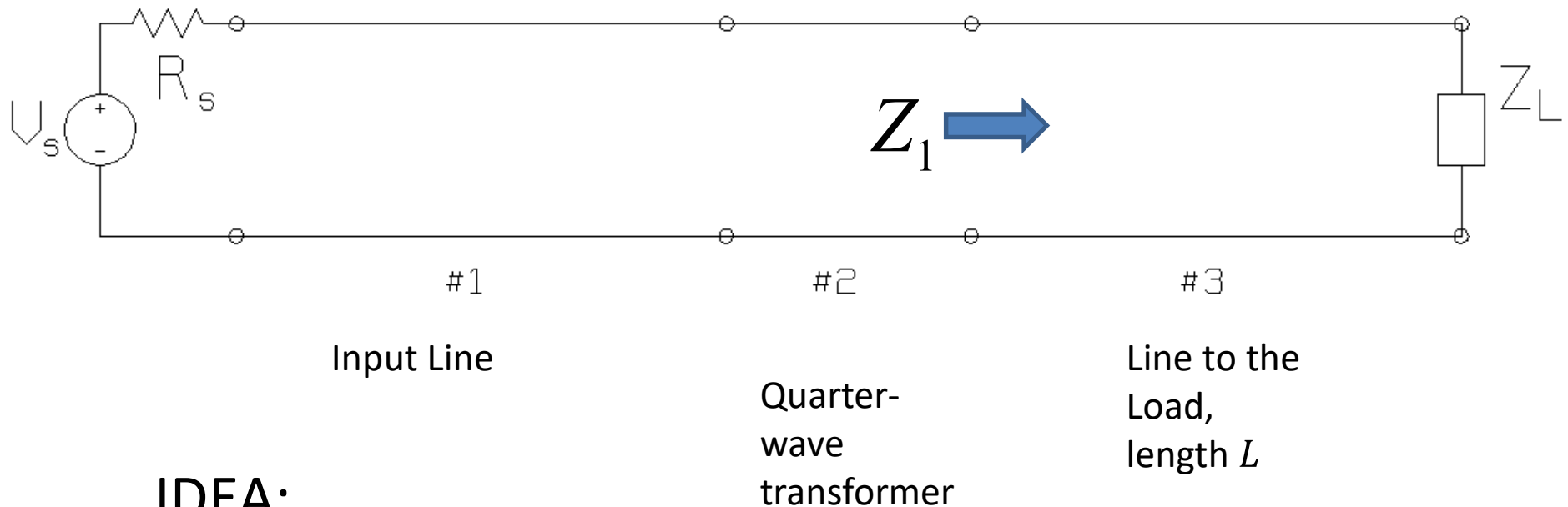
Choose $R_{ct} = \sqrt{R_c R_L} = \sqrt{50 \times 19.953} = 31.59 \text{ ohms}$

Line # 1 VSWR= 1.0006
 Line # 2 VSWR= 1.5833
 Line # 3 VSWR= 2.5059



The voltage on the input transmission line (line #1) is constant with position. There is (almost) no reflected wave and the VSWR is 1.0006.

Matching a Complex-Valued Load



IDEA:

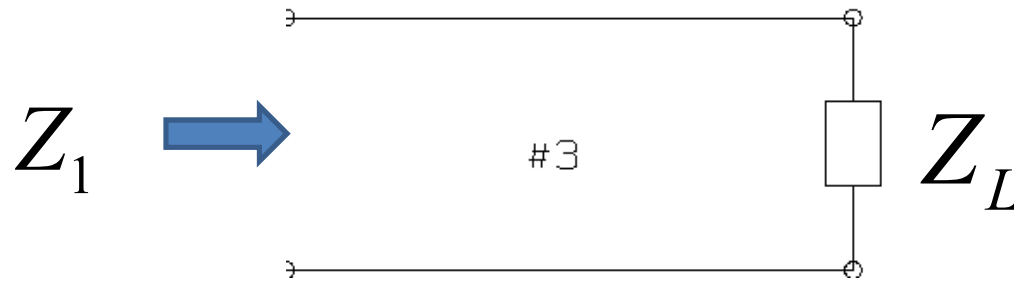
- Put a transmission line in series with the load.
- Choose the length L of line #3 so that the input impedance is resistive:

$$Z_1 = R_1 + j0$$

- Design a quarter-wave transformer to match R_1

$$Z_t = \sqrt{Z_0 R_1}$$

Choose the line length so that Z_1 is real:



From a previous class (set 11):

$$Z(z) = \frac{V(z)}{I(z)} = R_c \frac{1 + \Gamma_L e^{-j2\beta L} e^{j2\beta z}}{1 - \Gamma_L e^{-j2\beta L} e^{j2\beta z}}$$

At the input at $z = 0$:

$$\text{Define } \Gamma_1 = \Gamma_L e^{-j2\beta L}$$

$$Z_1 = R_c \frac{1 + \Gamma_L e^{-j2\beta L}}{1 - \Gamma_L e^{-j2\beta L}} = R_c \frac{1 + \Gamma_1}{1 - \Gamma_1} \quad \text{where} \quad \Gamma_1 = \Gamma_L e^{-j2\beta L}$$

If Γ_1 is real then Z_1 is real. Choose L to make Γ_1 real:

$$\Gamma_L = |\Gamma_L| e^{j\phi} \quad \text{then} \quad \Gamma_1 = \Gamma_L e^{-j2\beta L} = |\Gamma_L| e^{j(\phi - 2\beta L)}$$

Make Γ_1 real:

$$\Gamma_1 = |\Gamma_L| e^{j(\phi - 2\beta L)}$$

$$\Gamma_1 = |\Gamma_L| \cos(\phi - 2\beta L) + j|\Gamma_L| \sin(\phi - 2\beta L)$$

- Make the imaginary part zero:

$$\sin(\phi - 2\beta L) = 0$$

$$\phi - 2\beta L = \pm n\pi$$

$$L = \frac{\phi \mp n\pi}{2\beta}$$

- This formula gives two line lengths that are different by a quarter of a wavelength.

Find the input resistance $Z_1 = R_1 + j0$,
 with $L = \frac{\phi \mp n\pi}{2\beta}$

From a previous slide:

$$\Gamma_L = |\Gamma_L| e^{j\phi} \quad Z_1 = R_c \frac{1 + \Gamma_L e^{-j2\beta L}}{1 - \Gamma_L e^{-j2\beta L}} = R_c \frac{1 + |\Gamma_L| e^{j\phi} e^{-j2\beta L}}{1 - |\Gamma_L| e^{j\phi} e^{-j2\beta L}}$$

$$Z_1 = R_c \frac{1 + |\Gamma_L| e^{j(\phi - 2\beta L)}}{1 - |\Gamma_L| e^{j(\phi - 2\beta L)}}$$

$$Z_1 = R_c \frac{1 + |\Gamma_L| \cos(\phi - 2\beta L) + j|\Gamma_L| \sin(\phi - 2\beta L)}{1 - |\Gamma_L| \cos(\phi - 2\beta L) - j|\Gamma_L| \sin(\phi - 2\beta L)}$$

$$Z_1 = R_c \frac{1 + |\Gamma_L| \cos(\phi - 2\beta L) + j|\Gamma_L| \sin(\phi - 2\beta L)}{1 - |\Gamma_L| \cos(\phi - 2\beta L) - j|\Gamma_L| \sin(\phi - 2\beta L)}$$

We chose $\phi - 2\beta L = \pm n\pi$ so $\sin(\phi - 2\beta L) = \sin(\pm n\pi) = 0$
 $\cos(\phi - 2\beta L) = \cos(\pm n\pi) = \pm 1$

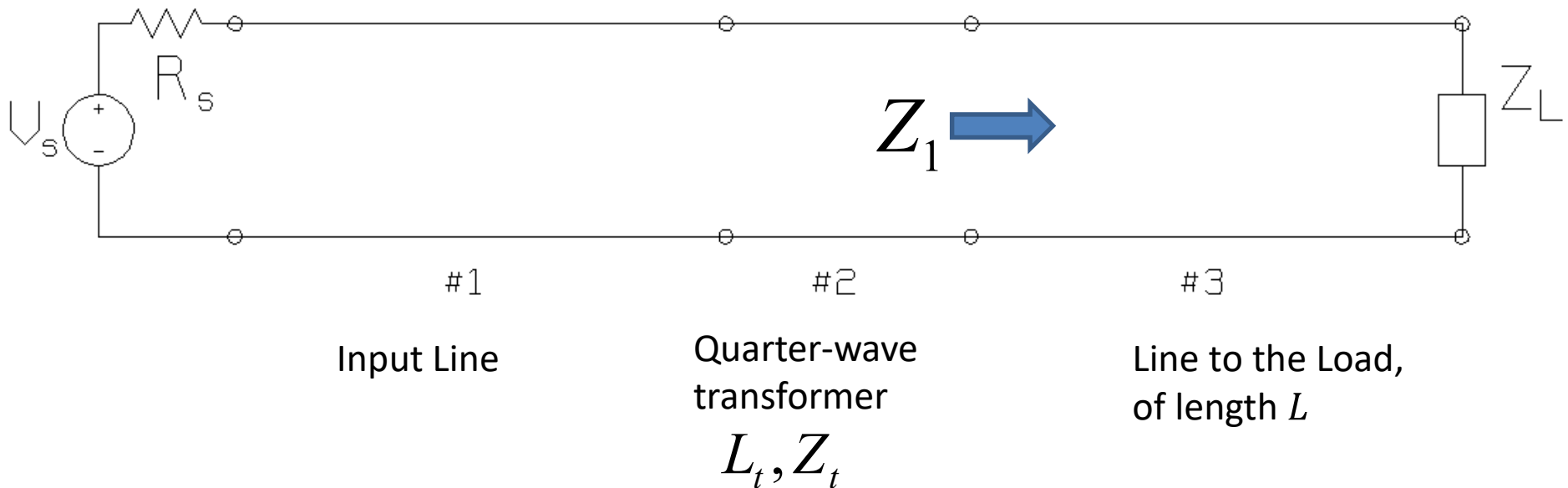
$$Z_1 = R_c \frac{1 + |\Gamma_L|(\pm 1)}{1 - |\Gamma_L|(\pm 1)}$$

$$Z_1 = R_c \frac{1 \pm |\Gamma_L|}{1 \mp |\Gamma_L|}$$

We choose L to make Z_1 is real, $Z_1 = R_1 + j0$:

$$R_1 = R_c \frac{1 \pm |\Gamma_L|}{1 \mp |\Gamma_L|}$$

Design procedure: choose L and Z_t



Reflection coefficient at the load: $\Gamma_L = |\Gamma_L| e^{j\phi}$

• Step 1: Choose the line length: $L = \frac{\phi \mp n\pi}{2\beta}$

• Find the input resistance $R_1 = R_c \frac{1 + |\Gamma_L| \cos(\phi - 2\beta L)}{1 - |\Gamma_L| \cos(\phi - 2\beta L)}$

• Find the transformer characteristic impedance: $Z_t = \sqrt{Z_0 R_1}$

• Find the transformer length, $L_t = \lambda/4$

Example

Match a load of $Z_L = 100 - j45$ ohms to a transmission line with $R_c = 50$ ohms at 850 MHz. The speed of travel on the transmission lines is $u = 30$ cm/ns.

Solution

Find the reflection coefficient:

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{100 - j45 - 50}{100 - j45 + 50} = \frac{50 - j45}{150 - j45} \frac{67.28 \angle -42.0^\circ}{156.6 \angle -16.7^\circ} = 0.4295 \angle -25.3^\circ$$

$$|\Gamma_L| = 0.4295 \quad \phi = \angle \Gamma_L = -25.3^\circ$$

Find the phase constant:

$$\lambda = \frac{u}{f} = \frac{300}{850} = 0.3529 \text{ meters}$$

$$\beta = \frac{2\pi}{\lambda} = \frac{360}{\lambda} = 1020 \text{ degrees per meter}$$

Find the line length L :

$$L = \frac{\phi \mp n\pi}{2\beta} = \frac{-25.3 \mp 180n}{2(1020)}$$

$$L = 7.584 \text{ cm, and } L = 16.41 \text{ cm.}$$

For $L=7.584$ cm, find R_1 using the formula with cosine, so that the correct sign is obtained:

$$R_1 = R_c \frac{1 + |\Gamma_L| \cos(\phi - 2\beta L)}{1 - |\Gamma_L| \cos(\phi - 2\beta L)} \quad |\Gamma_L| = 0.4295 \quad \phi = \angle \Gamma_L = -25.3^\circ$$

$$\beta L = 1020 \times 0.07584 = 77.36$$

$$\cos(\phi - 2\beta L) = \cos(-25.3^\circ - 2 \times 77.36) = \cos(-180.02) = -1$$

$$R_1 = 50 \frac{1 + 0.4295 \times (-1)}{1 - 0.4295 \times (-1)} = 19.95$$

For L=16.41 cm:

$$\beta L = 1020 \times 0.1641 = 167.38^\circ$$

$$\cos(\phi - 2\beta L) = \cos(-25.3^\circ - 2 \times 167.38) = \cos(-360.06) = 1$$

$$R_1 = 50 \frac{1 + 0.4295x(+1)}{1 - 0.4295x(+1)} = 125.3$$

Hence,

$$\text{For } L=7.584 \text{ cm, } R_1 = 19.95 \text{ so } Z_t = \sqrt{Z_0 R_1} = \sqrt{50 \times 19.95} = 31.58$$

$$\text{For } L=16.41 \text{ cm, } R_1 = 125.3 \text{ so } Z_t = \sqrt{Z_0 R_1} = \sqrt{50 \times 125.3} = 79.15$$

The wavelength is $\lambda = 0.3529$

$$\text{The transformer length is } L_t = \frac{\lambda}{4} = \frac{0.3529}{4} = 0.0882 \text{ m}$$

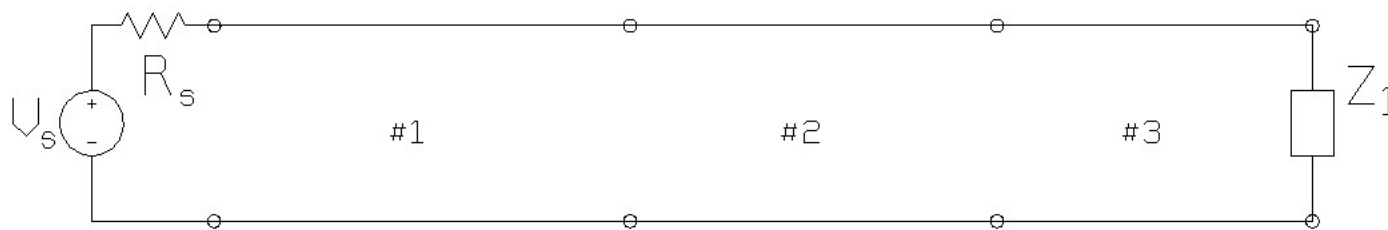
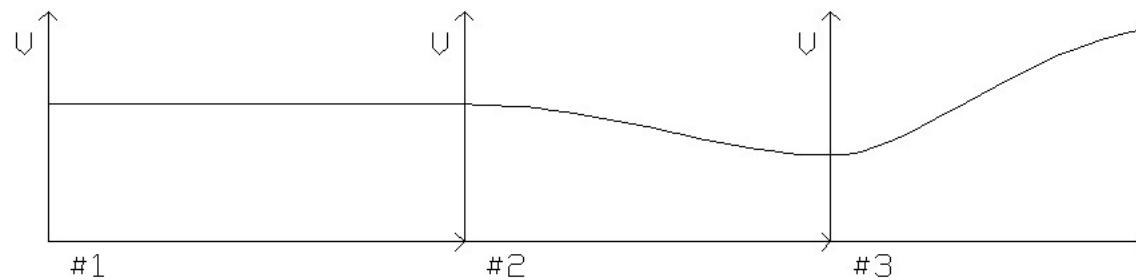
Use TRLINE to verify the design:

For $L=7.584$ cm, $R_1 = 19.95$ so $Z_t = \sqrt{Z_0 R_1} = \sqrt{50 \times 19.95} = 31.58$

Line # 1 VSWR= 1.0007

Line # 2 VSWR= 1.5828

Line # 3 VSWR= 2.5059

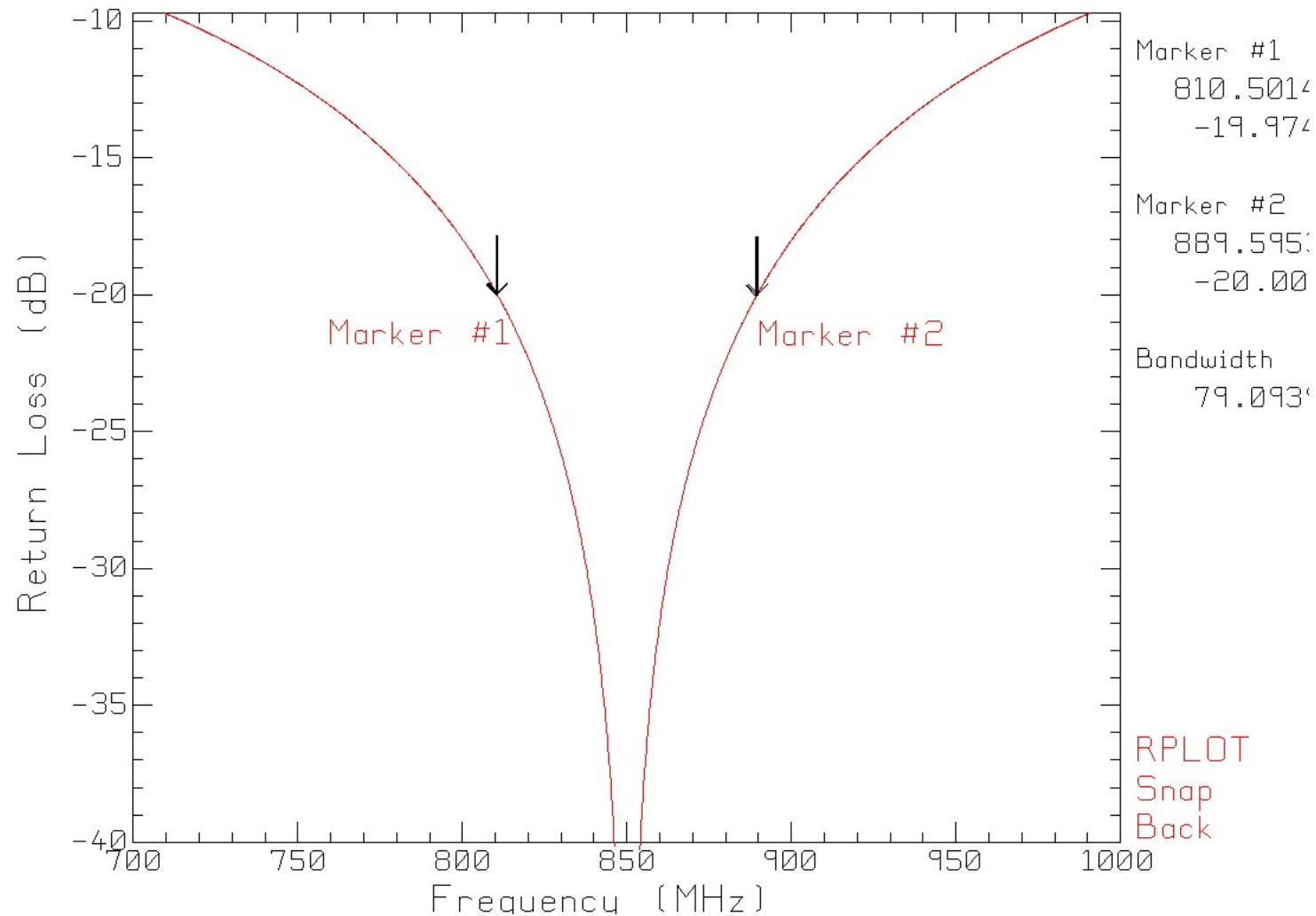


Frequency= 850.000 MHz.

Voltage amplitude as a function of distance.

[Back](#)

Use TRLINE to find the bandwidth:



For a return loss of 20 dB or better, the bandwidth is 79.0 MHz.