

# Towards Sensitivity Analysis of 3D Subduction Zone Thermal Structure via Model Order Reduction

UC San Diego



## **MTMOD: Megathrust Modeling Framework**

A collaborative effort to advance our understanding of megathrust earthquakes

<https://sites.utexas.edu/mtmod/>

NSF FRES, grant EAR-2121568

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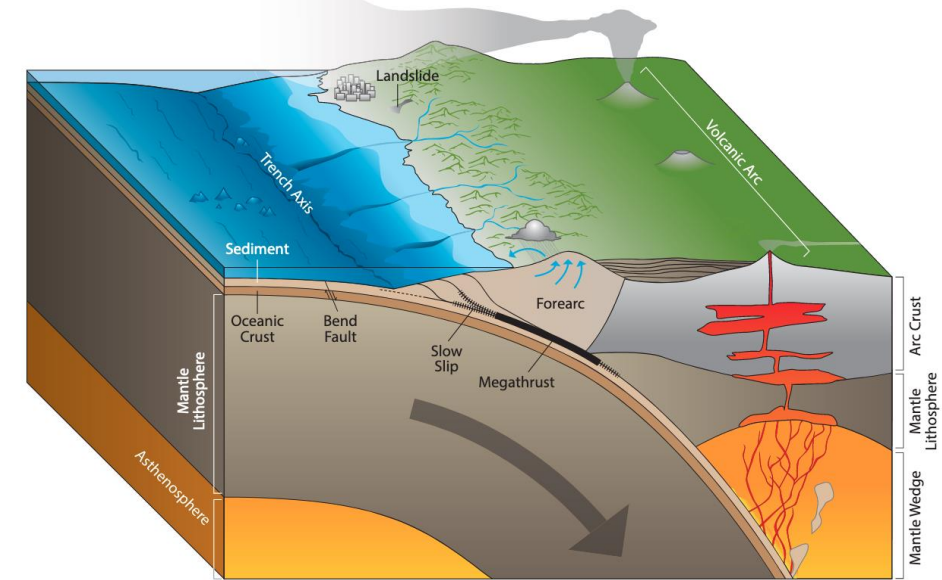
University of California San Diego

# The challenge: quantifying uncertainty in subduction zone temperature

Models are used to investigate subduction zone temperatures and to predict the potential extent of rupture, but they are naturally subject to uncertainty.

Quantifying uncertainty in subduction zone temperature is challenging due to the combination of:

- Multiple sources of uncertainty
- Computationally expensive physical models
- Large parameter space to explore



Modified from Fig S1-1 of SZ4D Implementation plan (2022).

Hyndman & Wang (1993); Tichelaar & Ruff (1993); Oleskevich et al., (1999);  
van Keken et al. (2002); Currie et al. (2004); Syracuse et al. (2010);  
Wada & Wang (2009); Peacock (2020); Penniston-Dorland et al. (2015)

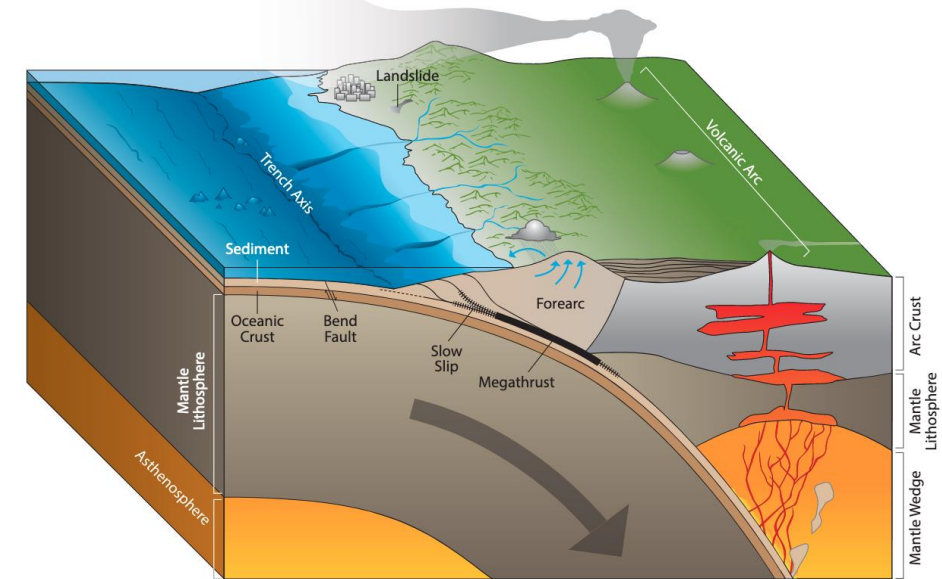
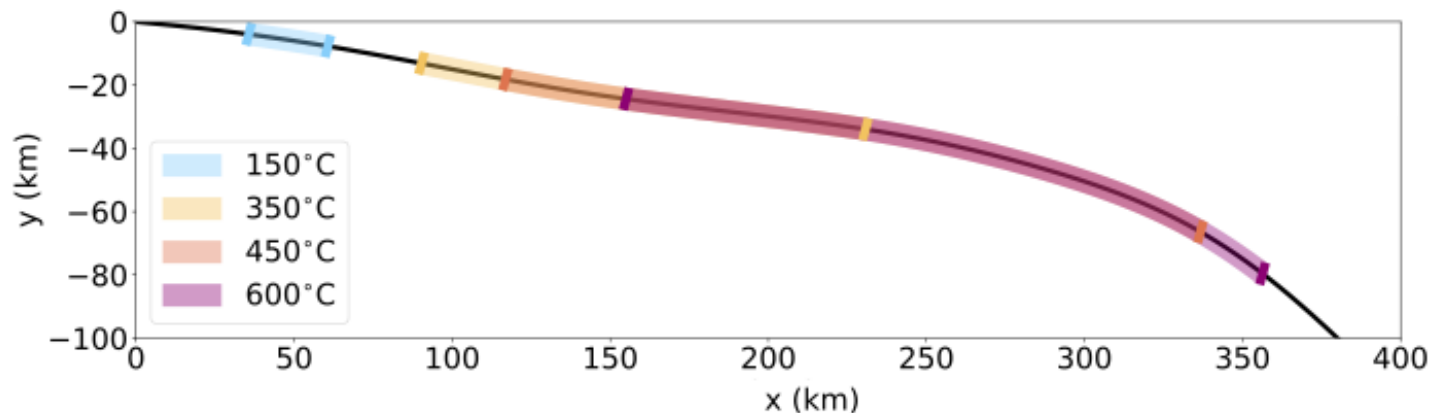
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We used reduced-order modeling to accurately approximate temperature within 2D thermo-mechanical subduction zone models.



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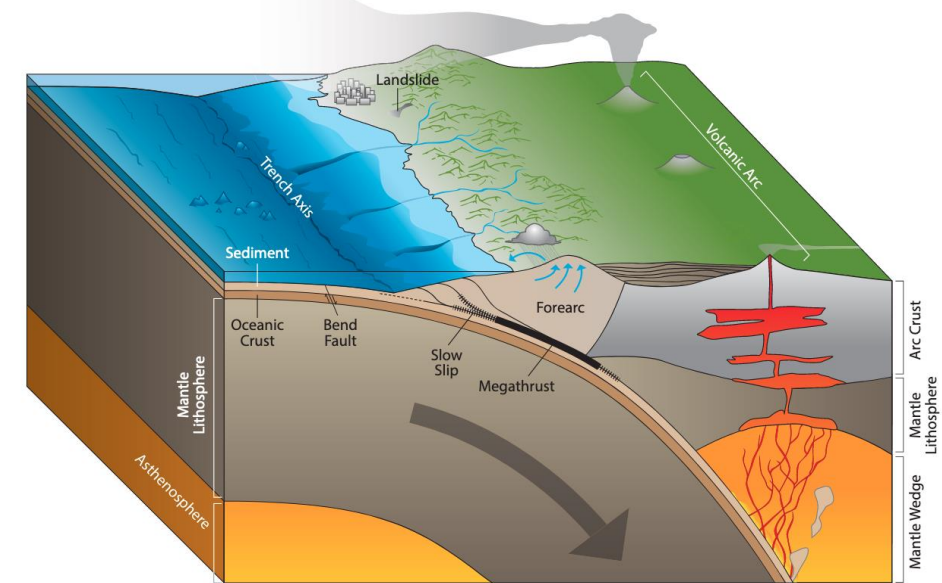
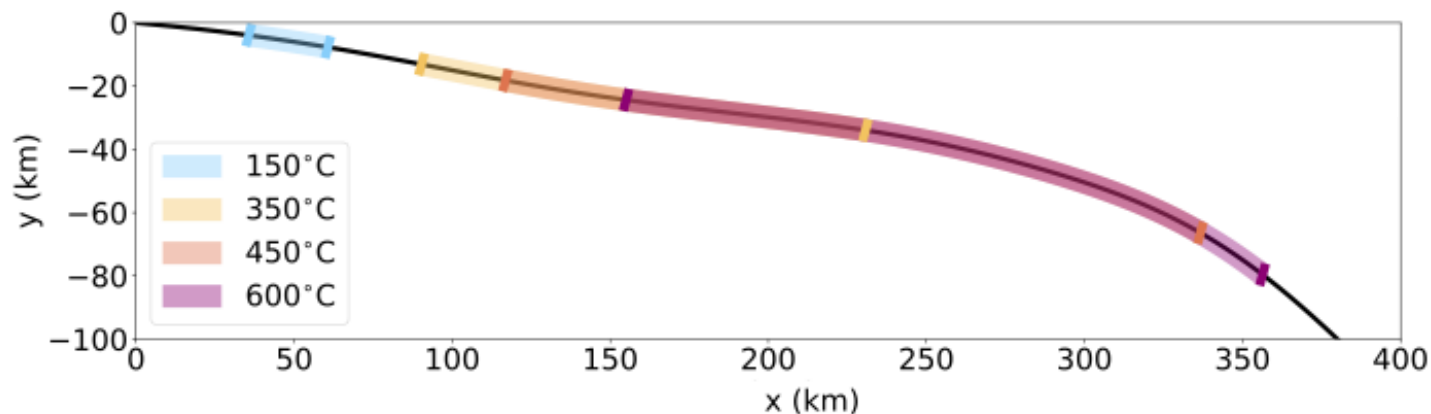
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2D thermal models cannot capture certain 3D effects. We build ROMs for global 3D models of temperature in Cascadia.

- What is the uncertainty in the 3D subduction zone temperature given uncertainty in model inputs?
- Are ROMs feasible for 3D geodynamic models such as this?

# Global 3D model of temperature at Cascadia

Model setup guided by Goldberg & Holt (2024);  
Alisic et al. (2010, 2012).

$D$ : Steinberger & Becker (2018)

$\delta v_s$ : SAVANI, Auer et al. (2014)

$\mathbf{u}$  : velocity  
 $T$  : temperature  
 $\eta$  : shear viscosity  
 $\underline{\underline{\dot{\epsilon}}}$  : deviatoric strain-rate tensor  
 $p$  : pressure  
 $\rho$  : density  
 $c_p$  : specific heat capacity  
 $k$  : thermal conductivity

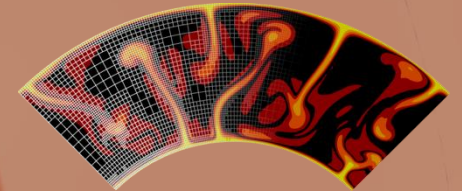
Governing equations:

$$\nabla \cdot \mathbf{u} = 0$$

$$-\nabla \cdot \left( 2\eta(\mathbf{u}, T) \underline{\underline{\dot{\epsilon}}}(\mathbf{u}) \right) + \nabla p = \rho(T) \mathbf{g}$$

$$\rho c_p \left( \frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T \right) - \nabla \cdot (k \nabla T) = 2\eta(\mathbf{u}, T) \underline{\underline{\dot{\epsilon}}}(\mathbf{u}) : \underline{\underline{\dot{\epsilon}}}(\mathbf{u})$$

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ASPECT 2.5.0



# Global 3D model of temperature at Cascadia

## Initial conditions

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$$T(d) = T_b + (T_s - T_b) \operatorname{erfc}\left(\frac{d}{0.8621 D}\right)$$

Linear  
transition

$$\frac{\rho - \rho_{\text{ref}}}{\rho_{\text{ref}}} = \omega \delta v_s, \quad T = T_b - \frac{1}{\alpha} \frac{\rho - \rho_{\text{ref}}}{\rho_{\text{ref}}}$$

Governing equations:

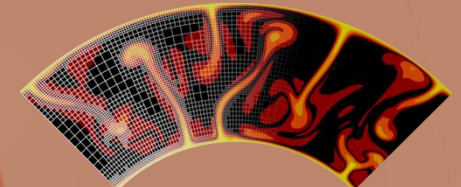
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- $d$  : depth from surface
- $T_b$  : interior mantle temperature
- $T_s$  : surface temperature
- $D$  : lithospheric thickness
- $\rho_{\text{ref}}$  : reference density
- $\omega$  : scaling factor
- $\delta v_s$  : shear wave vel. anomaly

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# Global 3D model of temperature at Cascadia

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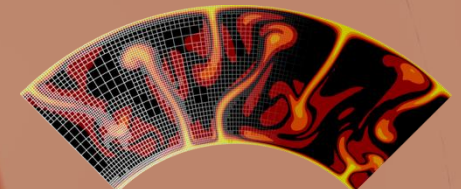
Slab interface and thickness:  
Slab2, Hayes et al. (2018)

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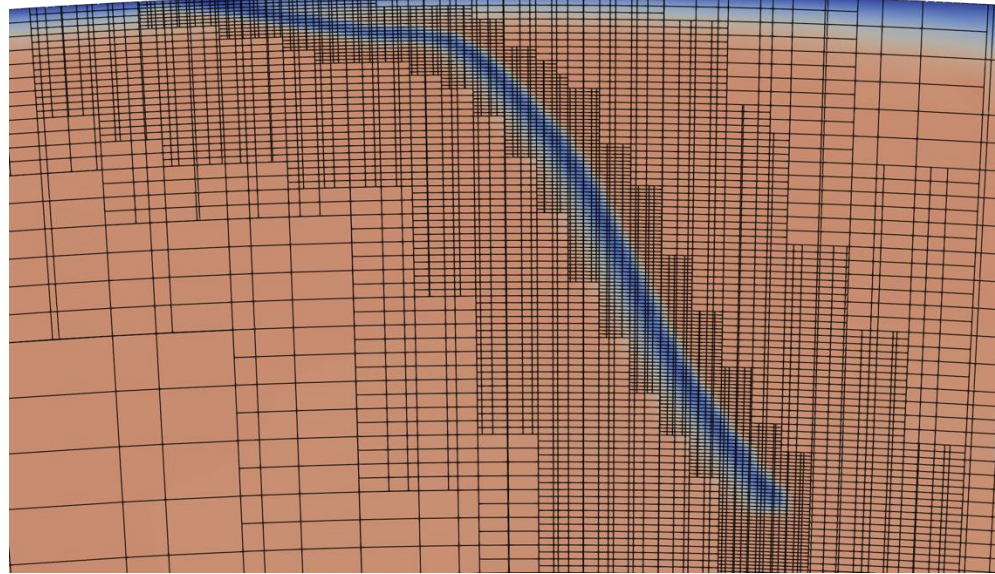
# Global 3D model of temperature at Cascadia

## Initial conditions

$$T(d) = T_b + (T_s - T_b) \operatorname{erfc}\left(\frac{d}{0.8621 D}\right)$$

Linear  
transition

**Mesh resolution  
2.8 km near slab  
interface**

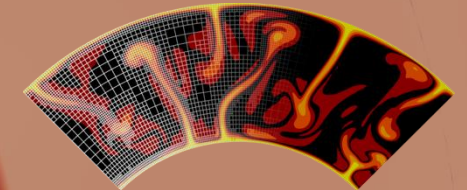


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**ASPECT 2.5.0**



# Global 3D model of temperature at Cascadia

Initial conditions

Boundary conditions

$$T(d) = T_b + (T_s - T_b) \operatorname{erfc}\left(\frac{d}{0.8621 D}\right)$$

Linear  
transition

$$\frac{\rho - \rho_{\text{ref}}}{\rho_{\text{ref}}} = \omega \delta v_s, \quad T = T_b - \frac{1}{\alpha} \frac{\rho - \rho_{\text{ref}}}{\rho_{\text{ref}}}$$

$$T_s = 273 \text{ K} \\ \mathbf{u} \cdot \vec{n} = 0$$

$$\mathbf{u} \cdot \vec{n} = 0 \\ T = 2273 \text{ K}$$

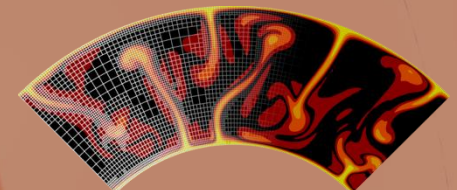
Governing equations:

$$\nabla \cdot \mathbf{u} = 0$$

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Evolved in time to  
 $t = 4 \times 10^4 \text{ yrs}$

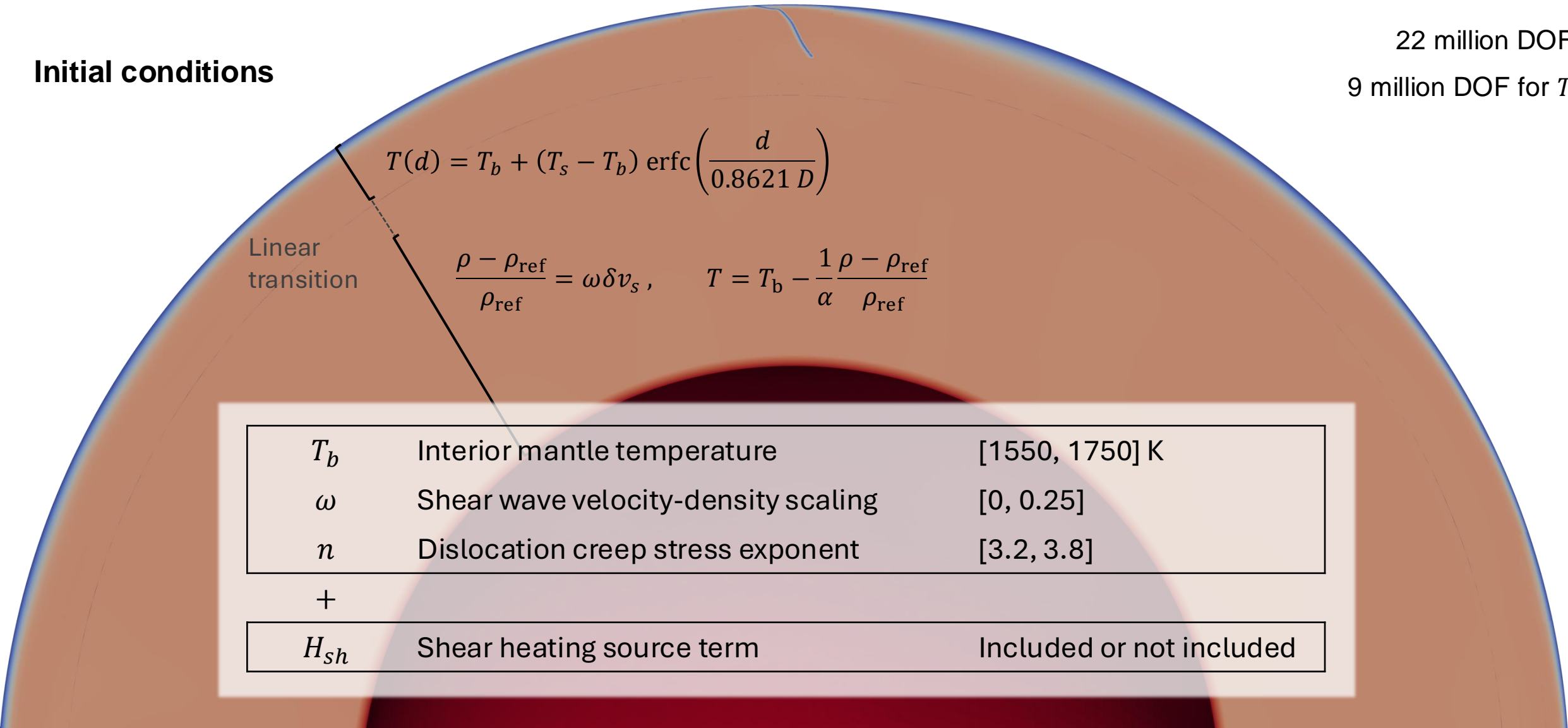


ASPECT 2.5.0

# Global 3D model of temperature at Cascadia

## Initial conditions

22 million DOF  
9 million DOF for  $T$


$$T(d) = T_b + (T_s - T_b) \operatorname{erfc}\left(\frac{d}{0.8621 D}\right)$$

Linear  
transition

$$\frac{\rho - \rho_{\text{ref}}}{\rho_{\text{ref}}} = \omega \delta v_s, \quad T = T_b - \frac{1}{\alpha} \frac{\rho - \rho_{\text{ref}}}{\rho_{\text{ref}}}$$

|          |                                     |                          |
|----------|-------------------------------------|--------------------------|
| $T_b$    | Interior mantle temperature         | [1550, 1750] K           |
| $\omega$ | Shear wave velocity-density scaling | [0, 0.25]                |
| $n$      | Dislocation creep stress exponent   | [3.2, 3.8]               |
| +        |                                     |                          |
| $H_{sh}$ | Shear heating source term           | Included or not included |

# Building accurate, efficient reduced-order models for temperature

The interpolated Proper Orthogonal Decomposition (iPOD) process:

- Assemble model solutions into columns of snapshot matrix  $\mathbf{X}$ , with corresponding parameter vector :

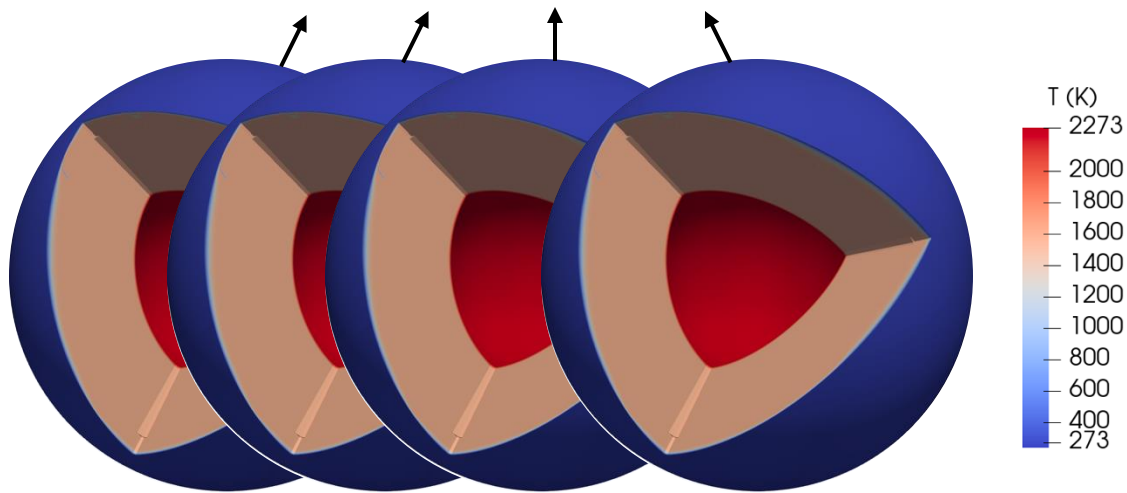
$$\mathbf{X}_{M \times N} = \begin{bmatrix} | & | & | & \dots & | \\ \mathbf{X}_1 & \mathbf{X}_2 & \mathbf{X}_3 & \dots & \mathbf{X}_N \\ | & | & | & \dots & | \end{bmatrix}, \quad \mathbf{Q} = [\mathbf{q}_1, \mathbf{q}_2, \mathbf{q}_3, \dots, \mathbf{q}_N].$$

$\mathbf{q}_i$  is a vector in parameter space,  
e.g.  $\mathbf{q}_i = (T_b, \omega, n)$ .

$\mathbf{X}_{M \times N}$  has  $M \gg N$

$M = \sim 9$  million,

$N = 550$ .



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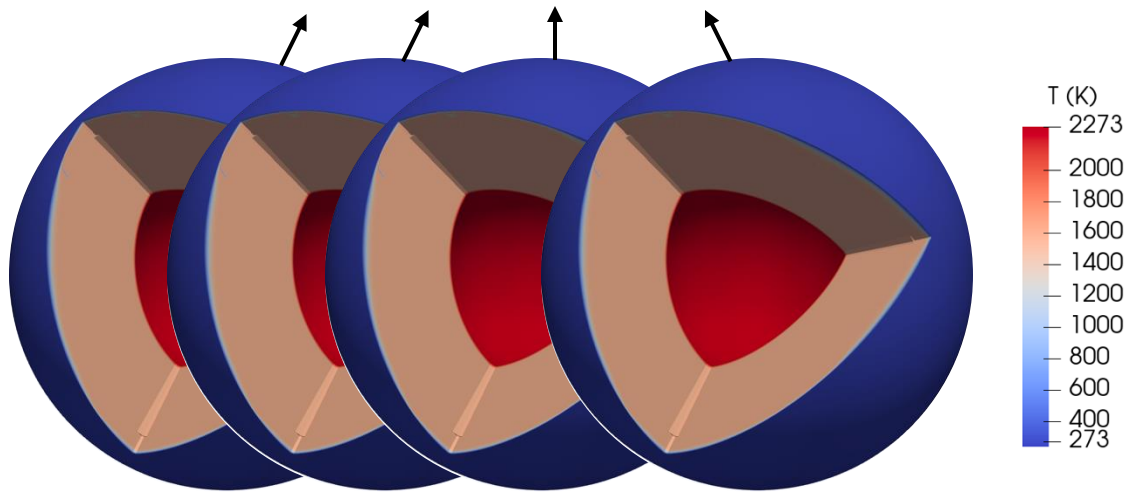
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- Take the Singular Value Decomposition (SVD):

$$\mathbf{X} = \mathbf{U} \mathbf{\Sigma} \mathbf{V}^T.$$

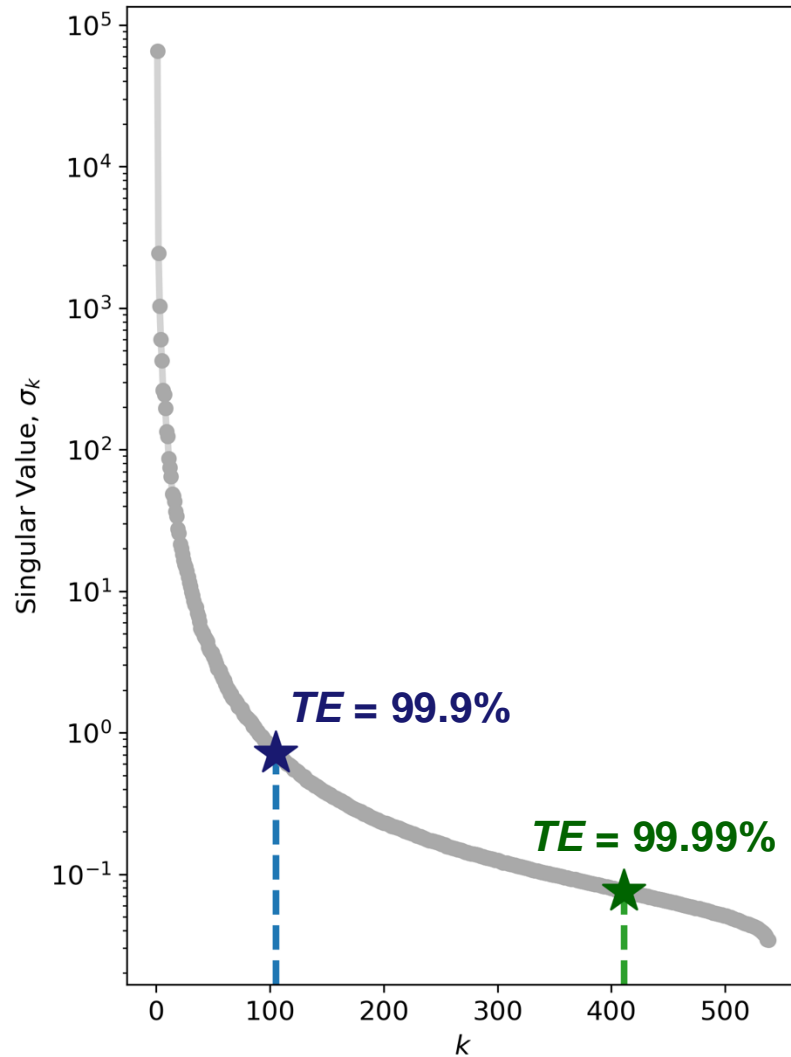
- Interpolate POD coefficients  $\alpha = \mathbf{\Sigma} \mathbf{V}^T$  at a new  $\hat{\mathbf{q}} \notin \mathbf{Q}$  using Radial Basis Function (RBF) interpolation.

- Approximate  $\mathbf{X}(\hat{\mathbf{q}})$  using an optimal orthogonal basis  $\mathbf{U}$  and interpolated coefficients  $\hat{\alpha}$ :

$$\hat{\mathbf{X}}(\hat{\mathbf{q}}) = \mathbf{U} \hat{\alpha}.$$



# Building accurate, efficient reduced-order models for temperature

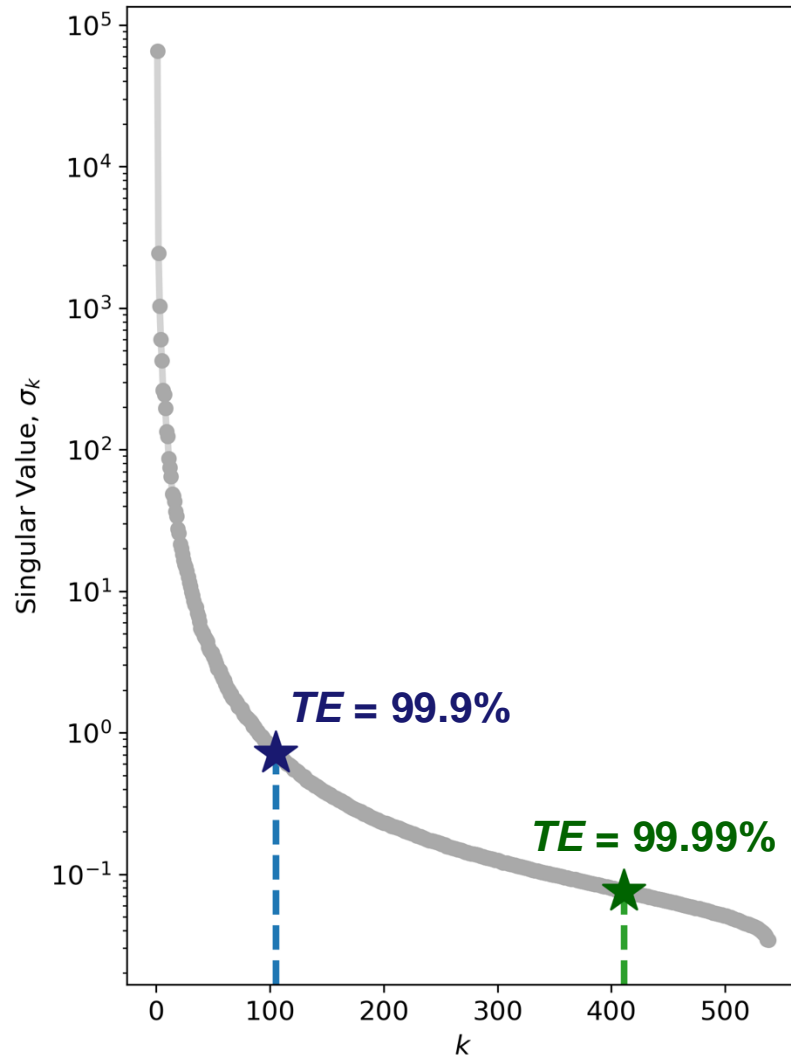


## Truncation

Total energy retained in  $r$  POD modes:  $TE(r) = \frac{\sum_{i=1}^r \sigma_i}{\sum_{i=1}^N \sigma_i}$

$\sigma_i$ :  $i$ th singular value of  $\mathbf{X}$

# Building accurate, efficient reduced-order models for temperature



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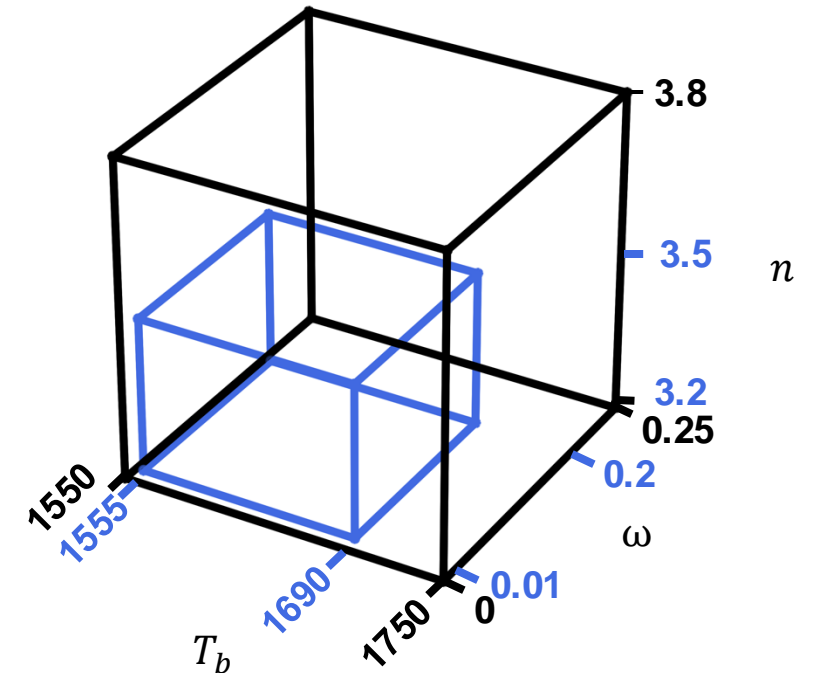
$\sigma_i$ :  $i$ th singular value of  $\mathbf{X}$

## Leave One Out Cross-Validation (LOOCV) error

For all  $\mathbf{q}_k \in \mathbf{Q}$ , build ROM using  $\tilde{\mathbf{X}} = \mathbf{X} \setminus \mathbf{X}_k$  and approximate  $\tilde{\mathbf{X}}(\mathbf{q}_k)$ .

$$CV(k) = \sup |\tilde{\mathbf{X}}(\mathbf{q}_k) - \mathbf{X}_k|$$

- Errors > 100 K on edges of  $\mathbf{Q}$
- Compute **sub-region** of  $\mathbf{Q}$  where  $CV < 30$  K
- Mean error in **sub-region** is 12 K



# Reduced-order model is $10^5$ times faster to evaluate

## Offline ROM construction

|                               |   |
|-------------------------------|---|
| Run forward models            | ~ 5400 sec on 128 MPI ranks x 550 models = 105,600 core-hrs |
| Compute the SVD               | 800 sec on 1 MPI rank                                       |
| Construct the RBF interpolant | 0.96 sec on 1 MPI rank                                      |

## Online phase

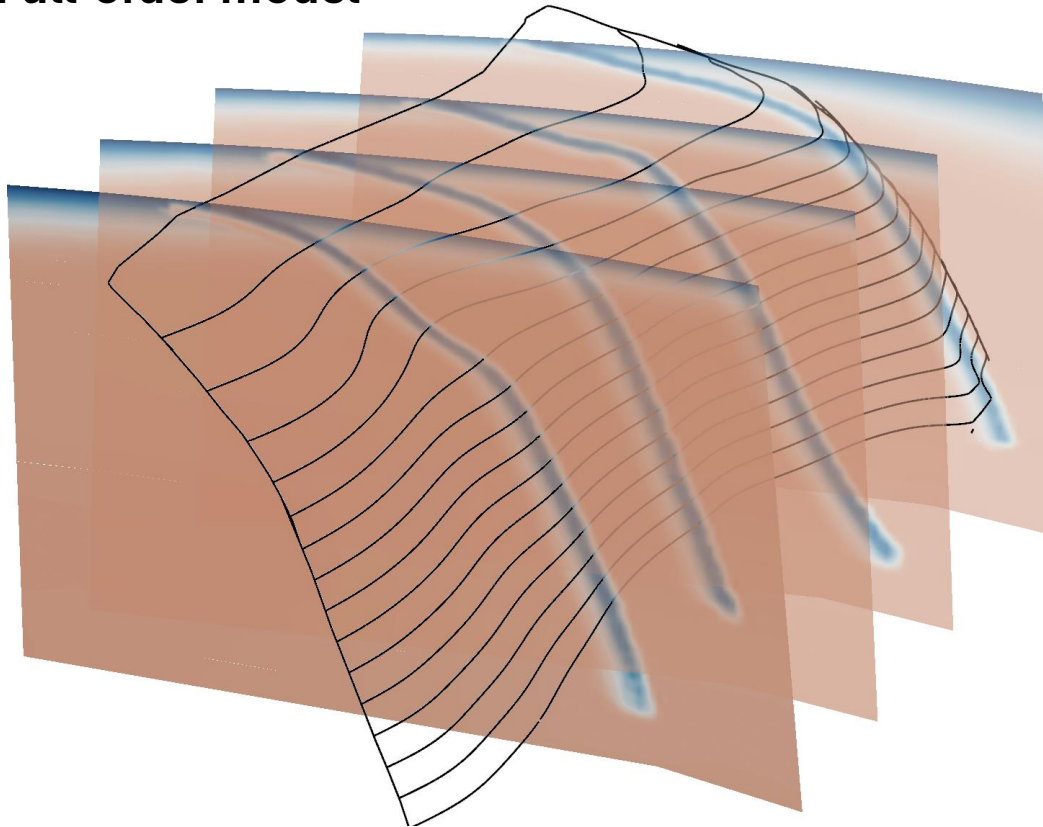
|  |                         |
|--|-------------------------|
| RBF evaluation time  | 0.001 sec on 1 MPI rank |
| Matrix multiplication, $\hat{\mathbf{X}}(\hat{\mathbf{q}}) = \mathbf{U} \hat{\boldsymbol{\alpha}}$ | 4 sec on 1 MPI rank     |

→ **Speedup factor of  $10^5$**  once ROM is constructed.

# Reduced-order model is $10^5$ times faster to evaluate

ROM evaluation is performed for full 3D domain, with slices of Cascadia shown here for clarity.

## Full-order model



**Resources required:**  
**5400 sec on 128 MPI ranks**

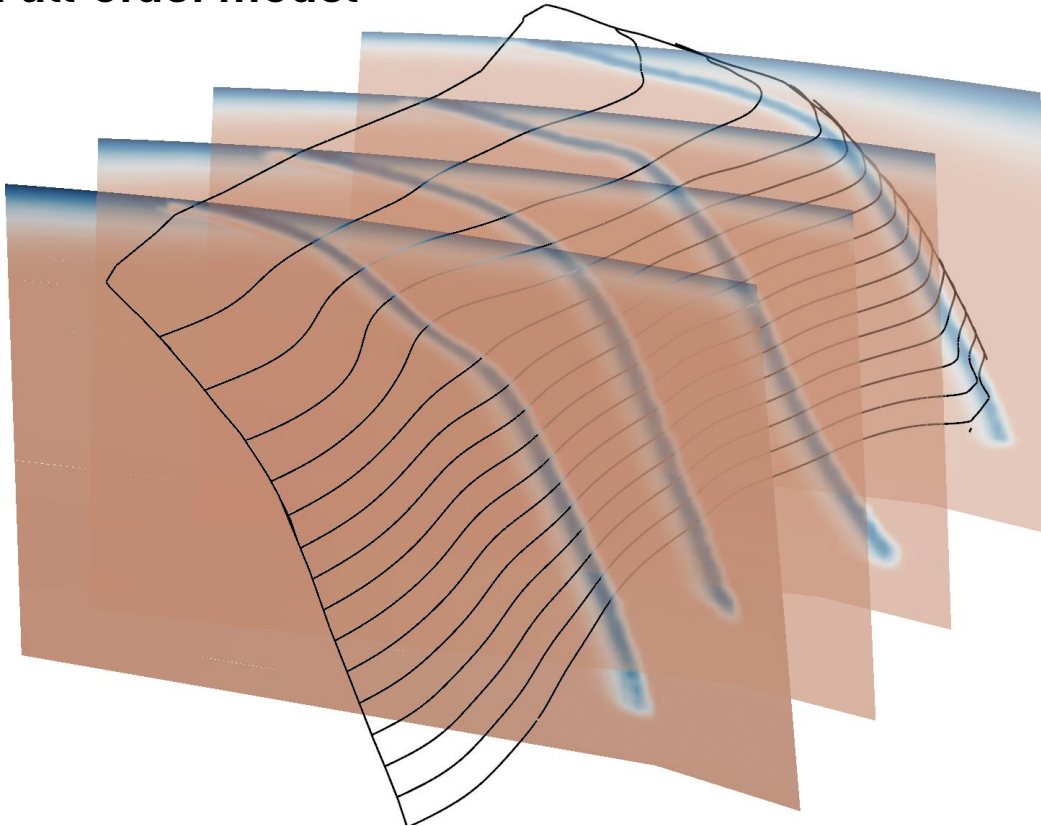




# Reduced-order model is $10^5$ times faster to evaluate

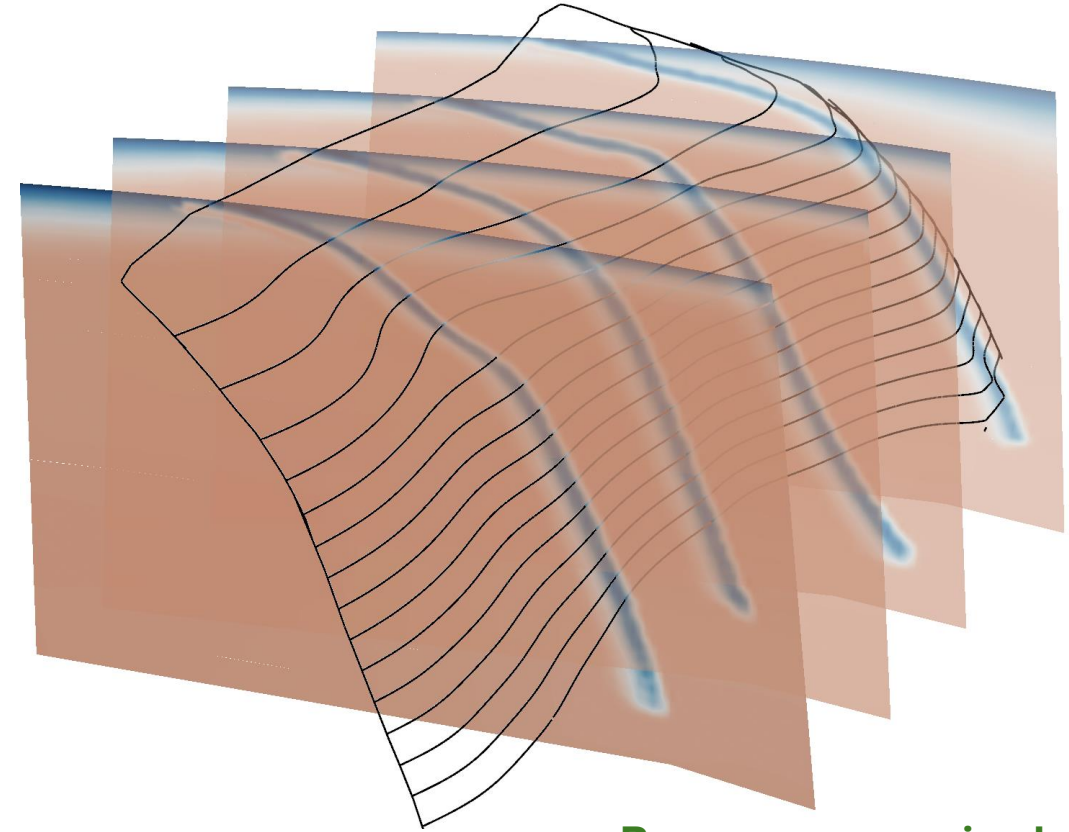
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**Full-order model**



**Resources required:**  
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**Reduced-order model**

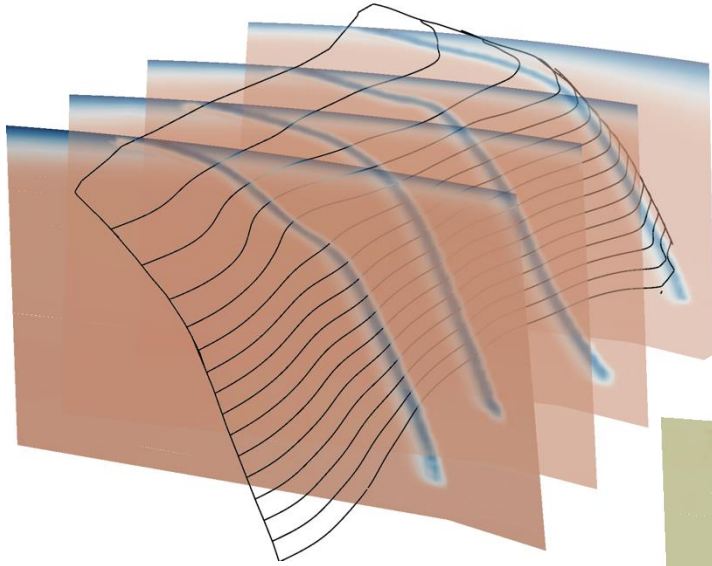


**Resources required:**  
**4 sec on 1 MPI rank**

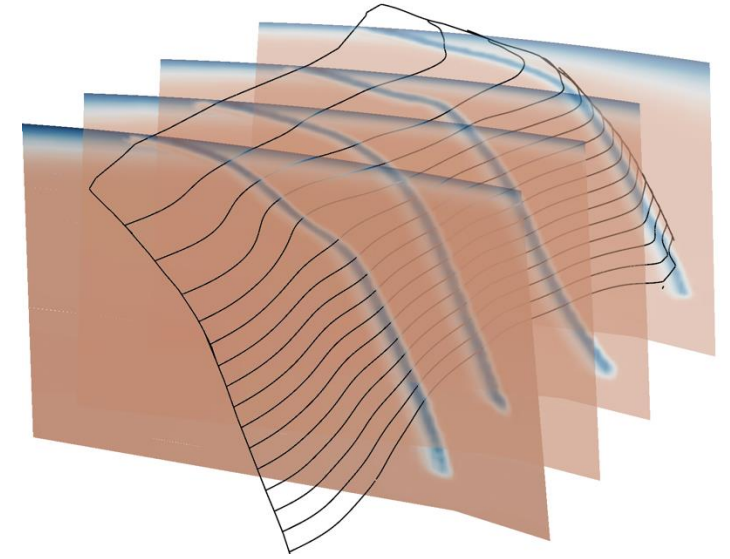


# ROM errors are low in the mantle wedge, higher within the slab

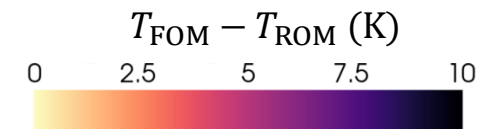
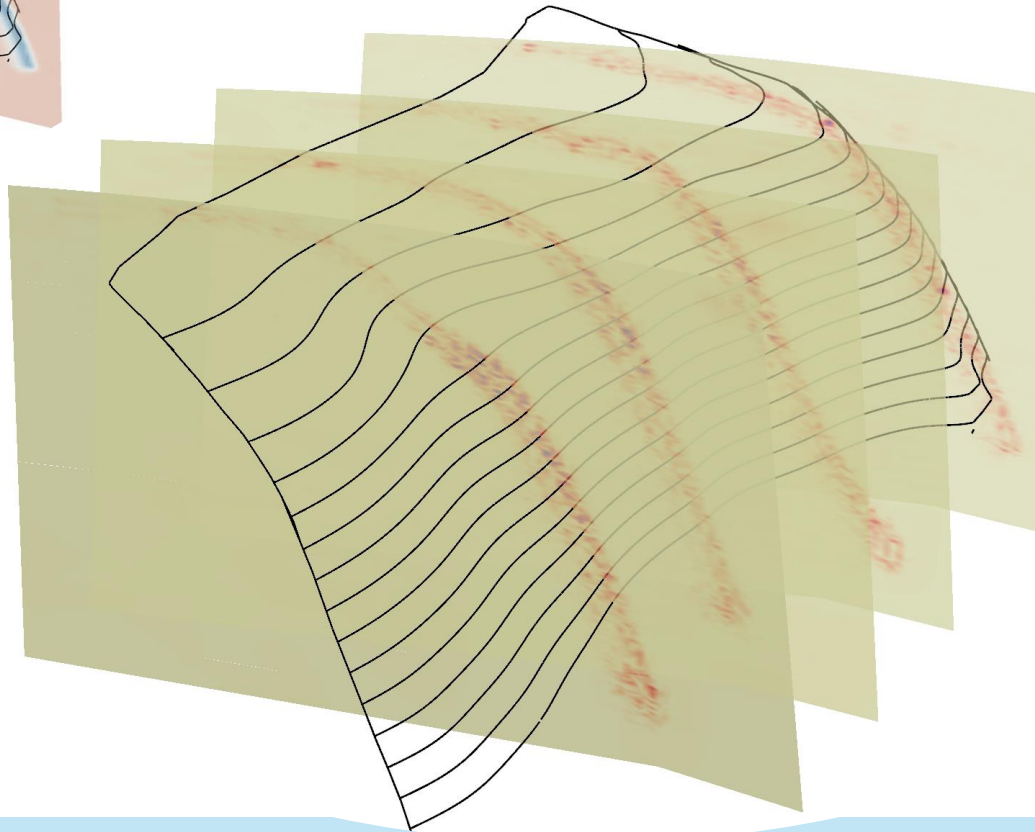
Full-order model



Reduced-order model



ROM error,  $T_{\text{FOM}} - T_{\text{ROM}}$  (K)



# Summary

## Key Takeaways

- Building a ROM to approximate global temperature is feasible.
- FOM-ROM error is  $< 30$  K globally in sub-region of parameter space.
- For Cascadia, errors are low in the mantle wedge and higher within the slab.
- The ROM is  $10^5$ x faster to evaluate than the full-order model.

Preprint for 2D study available  
<https://arxiv.org/abs/2410.02083>



## Outlook

- ROM permits rigorous global sensitivity analysis.
- Plan to expand the ROM to include additional model input parameters such as age of the incoming lithosphere and sediment cover.
- Aim to estimate uncertainty in temperature and potential rupture extent given variability in:
  - Model inputs ( $T_b, \omega, n$ ),
  - Along-margin effects (lithosphere age, sediment cover, along-margin flow).
- Preliminary results indicate that the ROM can be used for viscosity as accurately and efficiently as for temperature.

We would like to thank NSF FRES (grant EAR-2121568) and our MTMOD collaborators including Thorsten Becker at UTIG.