

Digital Synchronization Techniques for Reliable Communication

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Abstract—This manual provides a brief description about the design and implementation of digital synchronization techniques for reliable communication.

1. TIME OFFSET: GARDNER TED

Let the m th sample in the r th received symbol time slot be

$$Y_k(m) = X_k + V_k(m), \quad k = 1, \dots, N, m = 1, \dots, M. \quad (1.1)$$

where X_k is the transmitted symbol in the k th time slot and $V_k(m) \sim \mathcal{N}(0, \sigma^2)$. The decision variable for the k th symbol is [1]

$$U_k = \frac{1}{N} \sum_{i=1}^N Y_{k-i} \left(\frac{M}{2} \right) [Y_{k-i+1}(M) - Y_{k-i}(M)] \quad (1.2)$$

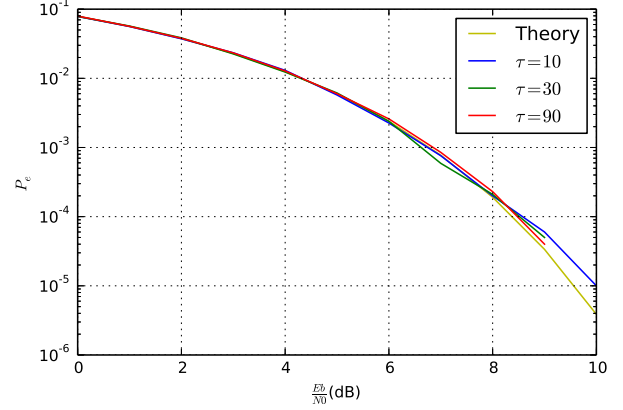


Fig. 1: SNR vs BER for varying τ .

A. Plots

Fig. 1 is generated by the following code

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https://github.com/gadepall/EE5837/raw/master/synctech/codes/time\_sync\_offsets.py
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and shows the variation of the BER with respect to the SNR with different timing offsets τ for $N = 6$.

2. FREQUENCY OFFSET: LR TECHNIQUE

Let the frequency offset be Δf [2]. Then

$$Y_k = X_k e^{j2\pi\Delta f k M} + V_k, \quad k = 1, \dots, N \quad (2.1)$$

From (5.1),

$$Y_k X_k^* = |X_k|^2 e^{j2\pi\Delta f k M} + X_k^* V_k \quad (2.2)$$

$$\Rightarrow r_k = e^{j2\pi\Delta f k M} + \bar{V}_k \quad (2.3)$$

where

$$r_k = Y_k X_k^*, \bar{V}_k = X_k^* V_k, |X_k|^2 = 1 \quad (2.4)$$

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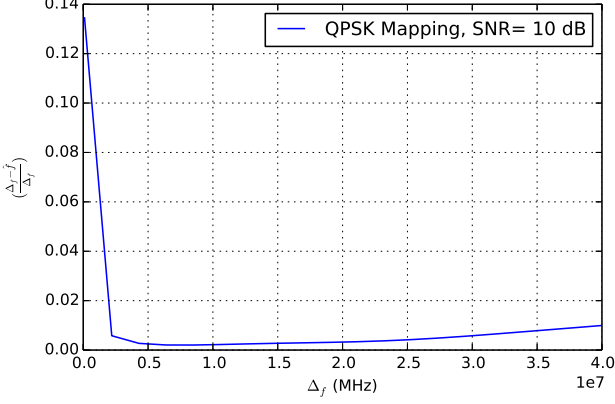


Fig. 2: Error variation with respect to frequency offset.

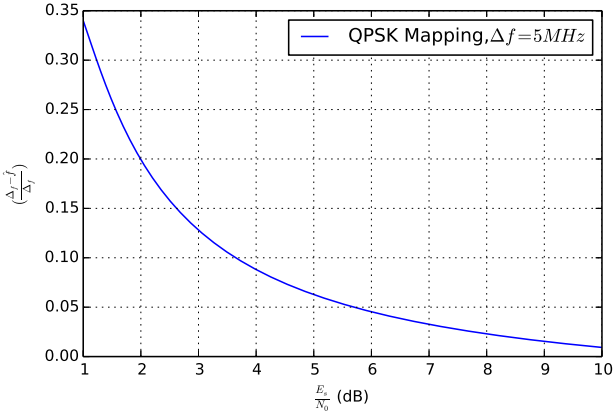


Fig. 3: Error variation with respect to the SNR. $\Delta f = 5$ MHz, Center frequency $f_c = 25$ GHz

The autocorrelation can be calculated as

$$R(k) \triangleq \frac{1}{N-k} \sum_{i=k+1}^N r_i r_{i-k}^*, \quad 1 \leq k \leq N-1 \quad (2.5)$$

Where N is the length of the received signal. For large centre frequency, the following yields a good approximation for frequency offset upto 40 MHz.

$$\Delta \hat{f} \approx \frac{1}{2\pi M} \frac{\sum_{k=1}^P \text{Im}(R(k))}{\sum_{k=1}^P k \text{Re}(R(k))}, \quad P \Delta f M \ll 1 \quad (2.6)$$

where P is the number of pilot symbols.

A. Plots

The number of pilot symbols is $P = 18$. The codes for generating the plots are available at

Fig. 2 shows the variation of the error in the offset estimate with respect to the offset Δf when the SNR = 10 dB. Similarly Fig. 3 shows the variation of the error with respect to the SNR for $\Delta f = 5$ MHz.

3. PHASE OFFSET: FEED FORWARD MAXIMUM LIKELIHOOD (FF-ML) TECHNIQUE

Let the phase offset be $\Delta \phi$ [3]. Then for the k th pilot,

$$Y_k = X_k e^{j\Delta \phi_k} + V_k, \quad k = 1, \dots, P \quad (3.1)$$

From (3.1),

$$Y_k X_k^* = |X_k|^2 e^{j\Delta \phi_k} + X_k^* V_k \quad (3.2)$$

$$\Rightarrow r_k = e^{j\Delta \phi_k} + \bar{V}_k \quad (3.3)$$

where

$$r_k = Y_k X_k^*, \bar{V}_k = X_k^* V_k, |X_k|^2 = 1 \quad (3.4)$$

From (3.3), the estimate for the k th pilot is obtained as

$$\Delta \hat{\phi}_k = \arg(r_k) \quad (3.5)$$

The phase estimate is then obtained using $\Delta \hat{\phi}_k$ in the following update equation as

$$\Delta \theta_k = \Delta \theta_{k-1} + \alpha \text{SAW}[\Delta \hat{\phi}_k - \Delta \theta_{k-1}] \quad (3.6)$$

Where SAW is sawtooth non-linearity

$$\text{SAW}[\phi] = [\phi]_{-\pi}^{\pi} \quad (3.7)$$

and $\alpha \leq 1$. The estimate is then obtained as $\Delta \theta_P$.

A. Plots

Fig. 4 is generated using

https://github.com/gadepall/EE5837/raw/master/synctech/codes/Error_vs_lp.py

and shows the variation of the phase error in the offset estimate with respect to the pilot symbols when the SNR = 10 dB and $\alpha = 0.5$.

Similarly Fig. 5 generated by

https://github.com/gadepall/EE5837/blob/master/synctech/codes/Error_vs_snr.py

shows the variation of the error with respect to the SNR for pilot symbols $P = 18$ and $\alpha = 1$.

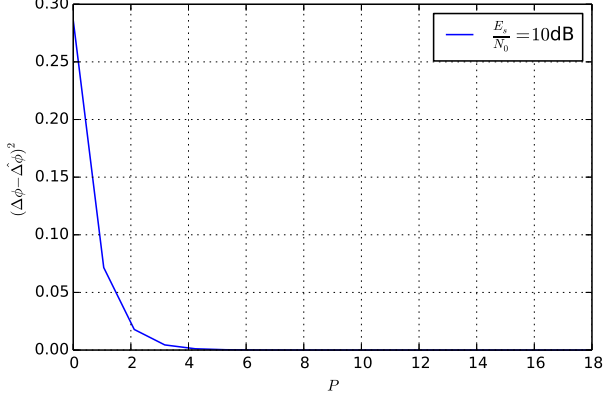


Fig. 4: Phase error variation with respect to pilot symbols

4. AUTOMATIC GAIN CONTROLLER (AGC): DATA-AIDED VECTOR-TRACKER (DA-VT)

Let the random AGC offset α , then the received symbol equation with amplitude offset as,

$$Y_k = \alpha X_k + V_k \quad k = 1, \dots, P \quad (4.1)$$

where $\alpha = \alpha_I + j\alpha_Q$ is the gain parameter. According to [4], the $\hat{\alpha}_k$ estimate for the k th pilot is

$$\alpha_{k+1} = \alpha_k - \gamma [\alpha_k Y_k^P - X_k^P] [X_k^P]^*, \quad (4.2)$$

where γ is the AGC step size.

A. Plots

The following code plots the real and imaginary parts of the gain parameter α with respect

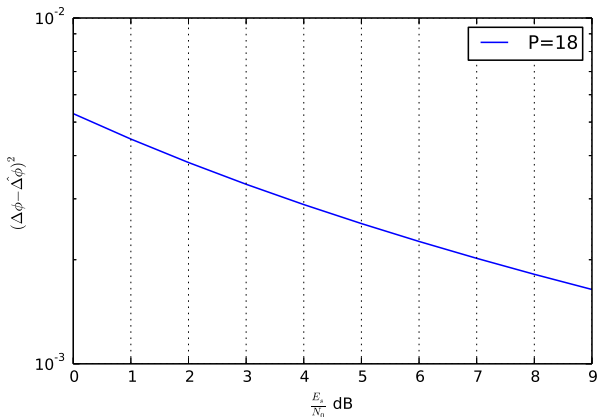


Fig. 5: $\Delta f = 5$ MHz

to the number of pilot symbols P . in Fig. 6. $\gamma = 10^{-3}$, $SNR = 10dB$.

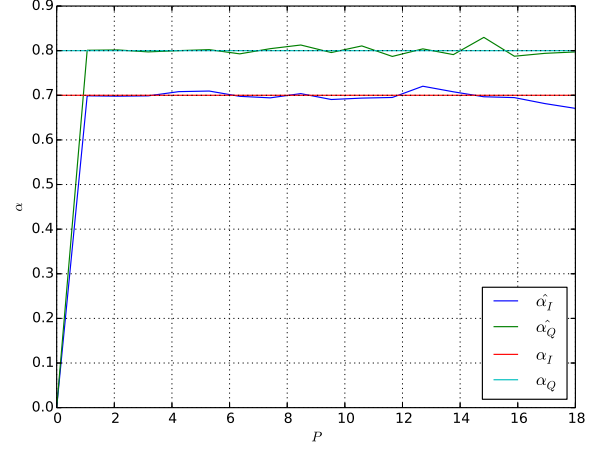


Fig. 6: Convergence of Digital AGC with respect to P .

https://github.com/gadepall/EE5837/raw/master/synctech/codes/Digital_AGC_with_fixed_SNR.py

5. FRAME SYNCHRONIZATION : GLOBAL SUMMATION OF SOF/PLSC DETECTORS

Let the frequency offset be Δf and phase offset be $\Delta\phi$. Then,

$$Y_k = X_k e^{j(2\pi\Delta f k M + \phi_k)} + V_k, \quad k = 1, \dots, N \quad (5.1)$$

assuming that no pilot symbols are transmitted. Let the phase information be θ_k , and defined as

$$\theta(k) = \frac{Y_k}{|Y_k|} \quad (5.2)$$

At the receiver, the header information is available in the form of

$$g_i(l) = x_s(l)x_s(l-i), l = 0, \dots, SOF - 1 \quad (5.3)$$

$$h_i(l) = x_p(l)x_p(l-i), l = 0, \dots, PLSC - 1 \quad (5.4)$$

where x_s are the mapped SOF symbols, x_p are the scrambled PLSC symbols, both modulated using

$\pi/2$ BPSK for $i = 1, 2, 4, 8, 16, 32$. A special kind of correlation is performed to obtain

$$m_i(k) = \sum_{l=0}^{PLSC-1} e^{j(\theta(k-l)-\theta(k-l-i))} h_i(l), \quad (5.5)$$

$$n_i(k) = \sum_{l=0}^{SOF-1} e^{j(\theta(k-l)-\theta(k-l-i))} g_i(l), \quad (5.6)$$

$$k = 1, \dots, N \quad (5.7)$$

Compute

$$p_i(k) = \begin{cases} \max(|n_i(k - PLSC) + m_i(k)|, \\ |n_i(k - PLSC) - m_i(k)|) & k > PLSC \\ \max|m_i(k)| & k < 64 \end{cases} \quad (5.8)$$

GLOBAL variable $G_{R,T}(k)$ [5] defined as,

$$G_{R,T}(k) = \sum_{i \geq 1} p_i(k), \quad i = 1, 2, 4, 8, 16, 32 \quad (5.9)$$

Where,

$$(5.10)$$

$$(5.11)$$

Where $xsof, xscr$ are the mapped symbols of sof and scr using $\frac{\pi}{2}$ BPSK.

REFERENCES

- [1] F. Gardner, "A BPSK/QPSK Timing-Error Detector for Sampled Receivers," *IEEE Transactions on Communications*, vol. 34, no. 5, pp. 423–429, May 1986. [Online]. Available: <https://doi.org/10.1109/TCOM.1986.1096561>
- [2] M. Luise and R. Reggiannini, "Carrier frequency recovery in all-digital modems for burst-mode transmissions," *IEEE Transactions on Communications*, vol. 43, no. 2/3/4, pp. 1169–1178, Feb 1995. [Online]. Available: <https://doi.org/10.1109/26.380149>
- [3] E. Casini, R. D. Gaudenzi, and A. Ginesi, "DVB-S2 modem algorithms design and performance over typical satellite channels," *International Journal of Satellite Communications and Networking*, vol. 22, no. 3, pp. 281–318, 2004. [Online]. Available: <https://onlinelibrary.wiley.com/doi/abs/10.1002/sat.791>
- [4] R. De Gaudenzi and M. Luise, "Analysis and design of an all-digital demodulator for trellis coded 16-QAM transmission over a nonlinear satellite channel," *IEEE Transactions on Communications*, vol. 43, no. 2/3/4, pp. 659–668, Feb 1995. [Online]. Available: <https://doi.org/10.1109/26.380085>
- [5] H. Miyashiro, E. Boutillon, C. Roland, J. Vilca, and D. D'Áz, "Improved Multiplierless Architecture for Header Detection in DVB-S2 Standard," in *2016 IEEE International Workshop on Signal Processing Systems (SiPS)*, Oct 2016, pp. 248–253. [Online]. Available: <https://doi.org/10.1109/SiPS.2016.51>