

AI25btech11020

- 1) For the transformation shown below, if one of the eigenvalues is 6, the other eigenvalue of the matrix is

$$\begin{pmatrix} X \\ Y \end{pmatrix} = \begin{pmatrix} 5 & -2 \\ -2 & 2 \end{pmatrix} \begin{pmatrix} x \\ y \end{pmatrix}$$

- 2) The solution of the differential equation

$$\frac{d^2 y}{dx^2} = \frac{dy}{dx}$$

- a) $y = e^x + C$ c) $y = C_1 e^{-x} + C_2$
b) $y = e^{-x} + C$ d) $y = C_1 e^x + C_2$

(GATE MT 2016)

[where, C, C_1 and C_2 are constants]

- 3) If $\mathbf{V} = x^2y\hat{i} + y^2x\hat{j} + xyz\hat{k}$, the divergence of \mathbf{V} is

- a) $x^3y + y^3x + xyz^2$
b) $x^2y + y^2x + xyz$
c) $5xy$
d) 0

(GATE MT 2016)

- 4) The first law of thermodynamics can be stated as

- a) $dE = \delta Q - \delta W$
b) $dQ = dE - \delta W$
c) $\delta W - dQ + dE$
d) $dW = \delta Q - \delta E$

[where, E, Q and W denote internal energy, heat and work, respectively] (GATE MT 2016)

- 5) In a typical Ellingham diagram for the oxides, the $C + O_2 = CO_2$ line is nearly horizontal because

- a) The slope of the line is equal to the enthalpy change at standard state, which is approximately zero in this case
- b) The slope of the line is equal to the entropy change at standard state, which is approximately zero in this case
- c) CO_2 shows non-ideal behaviour
- d) CO_2 is a gaseous oxide

(GATE MT 2016)

- 6) Activation energy of a chemical reaction, homogeneous or heterogeneous, is graphically estimated from a plot between

- a) k versus T
b) $1/k$ versus T
c) $1/k$ versus $\ln T$
d) $\ln k$ versus $1/T$

[where, k is the rate constant and T is the absolute temperature] (GATE MT 2016)

- 7) The passive film in stainless steel forms above the

- Primary passive potential
- Breakdown potential
- Trans-passive potential
- Pitting potential

(GATE MT 2016)

- a) Dislocation pile-up
b) Large number of slip systems
- c) Low stacking fault energy
d) Dislocation climb

(GATE MT 2016)

19) Creep resistance decreases due to

- a) Small grain size
b) Fine dispersoid size
- c) Low stacking fault energy
d) High melting point

(GATE MT 2016)

20) The operation NOT associated with casting is

- a) Gating
b) Stack Moulding
- c) Fettling
d) Calendaring

(GATE MT 2016)

21) Of the following welding processes

- [P] Laser Beam Welding
[Q] Submerged Arc Welding
[R] Metal Inert Gas Welding

the width of the heat-affected zone in decreasing order is

- a) $P > Q > R$
b) $Q > R > P$
c) $R > P > Q$
d) $P > R > Q$

(GATE MT 2016)

22) Railway tracks are typically manufactured using

- a) Forging
b) Extrusion
c) Deep Drawing
d) Rolling

(GATE MT 2016)

23) For dye-penetrant test, identify the **CORRECT** statement

- a) Pre- and post-cleaning of parts are not required
b) Internal defects can be detected
c) Surface oxides helps in crack identification
d) Dye with low contact angle is required

(GATE MT 2016)

24) Aluminium powder having an apparent density of 810 kg.m^{-3} is compacted in a cylindrical die at 600 MPa. The density of the as-pressed aluminium compact is 1755 kg.m^{-3} . If the height of the as-pressed compact is 12 mm, the fill height (in mm) required is (GATE MT 2016)

25) A rolling mill has a roll diameter of 200 mm. If coefficient of friction is 0.1, then the maximum possible reduction (in mm) during rolling of a 250 mm thick plate is (GATE MT 2016)

26) A hot body cools according to the following equation

$$\frac{dT}{dt} = -cT$$

where, T is the instantaneous temperature at time t, and the constant $c = 0.05 \text{ s}^{-1}$. Reduce the differential equation into its finite difference form **using forward difference**. For maintaining numerical stability, the maximum value of the time step Δt (in seconds) is (GATE MT 2016)

27) Solve the equation $x = e^{-x}$ using Newton-Raphson method. Starting with an initial guess value $x_0 = 0$, the value of x after the first iteration is (GATE MT 2016)

28) A coin is tossed three times. It is known that out of the three tosses, one is a **HEAD**. The probability of the other two tosses also being **HEADs** is (GATE MT 2016)

29) The vector parallel to the plane $3x - 2y + z = -1$ is

- a) $\hat{i} + \hat{j} - \hat{k}$
- b) $3\hat{i} - 2\hat{j} + \hat{k}$
- c) $-\hat{i} + \hat{j} - \hat{k}$
- d) $3\hat{i} - 2\hat{j} + 2\hat{k}$

(GATE MT 2016)

30) The value of the integral

$$\int_0^{\pi/2} x \sin x \, dx =$$

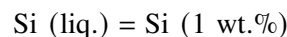
(GATE MT 2016)

31) The grain sizes (in μm) measured at five locations in an alloy sample are: 16, 14, 18, 15 and 13. The mean, median and standard deviation of grain sizes respectively are (in μm)

- a) 15.2, 15 and 1.7
- b) 15.2, 15 and 1.9
- c) 15.8, 15 and 1.9
- d) 15.2, 16 and 1.7

(GATE MT 2016)

32) The change of standard state from pure liquid to 1 wt.% for Si dissolved in liquid Fe at 1873 K is expressed as



Given that the activity coefficient of Si at infinite dilution in Fe is 10^3 , the standard Gibbs free energy change (in kJ) for this equilibrium is

(GATE MT 2016)

33) The following experimental data are available for a hypothetical binary liquid system A-B at 1073 K

Atom fraction of A	0.2	0.4	0.5	0.7	1.0
Partial pressure of A (bar)	0.01	0.04	0.06	0.07	0.08

When the atom fraction of A is 0.4, the activity of A in the liquid is

(GATE MT 2016)

34) The lining of a box-type furnace is made up of a refractory layer and steel plate as shown in the figure. Steady state temperature at the surface of the refractory is 1273 K and that at the outer steel surface is 473 K. If the steady-state heat flux through the refractory-steel plate composite is 1600 W.m^{-2} , and heat flow is along x-direction, the thermal contact resistance ($\text{W}^{-1}.\text{m}^2\text{K}$) between refractory and steel is

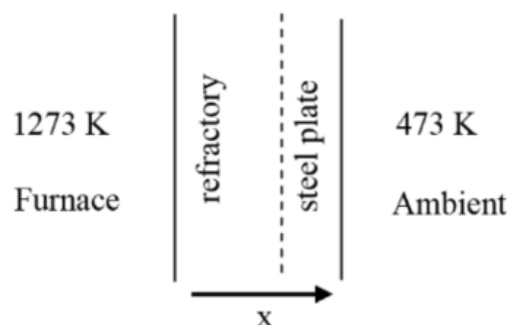


Fig. 3.

Given data:

Thermal conductivity of refractory: $1.2 \text{ W.m}^{-1}\text{K}^{-1}$

Thickness of refractory lining: 80 mm

Thermal conductivity of steel: $32 \text{ W.m}^{-1}\text{K}^{-1}$

Thickness of steel plate: 4 mm

(GATE MT 2016)

- 35) The height of a liquid metal column in a cylindrical vessel is 3.2 m. At time $t = 0$, liquid metal is drained out from the vessel through a small nozzle located at the base of the vessel. Neglecting frictional losses, the initial mass flow rate (in kg.s^{-1}) through the nozzle is

Given data:

Density of liquid metal Nozzle diameter: 7000 kg

Nozzle discharge coefficient: 30 mm

(GATE MT 2016)

- 36) Match entities listed in **Column I** with their correct dimensions given in **Column II**:

Column I

[P] Drag coefficient

[Q] Mass transfer coefficient

[R] Viscosity

[S] Mass flux

Column II

[1] $\text{M L}^{-1}\text{T}^{-1}$

[2] $\text{M L}^{-2}\text{T}^{-1}$

[3] $\text{M}^0 \text{L}^0 \text{T}^0$

[4] $\text{M}^0 \text{L T}^{-1}$

a) P-3, Q-4, R-1, S-2

b) P-3, Q-1, R-2, S-4

c) P-1, Q-4, R-2, S-3

d) P-4, Q-3, R-1, S-2

(GATE MT 2016)

- 37) Direct Reduced Iron (DRI) produced from a gas based process contains Fe, FeO, C and remainder being gangue. The chemical composition of DRI is: *Total Fe = 92 wt.% and Metallic Fe = 84 wt.%*. The weight percent of FeO in DRI is

(GATE MT 2016)

- 38) Mould heat flux (q_m) for billet casters is expressed (in SI unit) as a function of distance below the meniscus (z)

$$q_m(z) = \left[2.67 - 0.33\sqrt{\frac{z}{U_c}} \right] \times 10^6 \quad (0 \leq z \leq L_m)$$

If mould length (L_m) is 0.8 m and casting speed (U_c) is 0.2 m.s^{-1} , the average mould flux (in MW.m^{-2}) is

(GATE MT 2016)

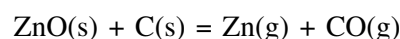
- 39) In BOF steelmaking, 5 metric ton of lime containing 90 wt.% CaO is used to refine 100 metric ton of hot metal containing 93.2 wt.% Fe. The slag produced during refining contains 40 wt.% CaO and 22 wt.% FeO. Neglecting material losses, the yield of Fe (in %) is (GATE MT 2016)
- 40) In vacuum degassing of steel, 14 ppm of dissolved nitrogen is in equilibrium with 1 mbar of nitrogen gas at 1873 K. At the same temperature, if the pressure is lowered to 0.7 mbar, the equilibrium nitrogen content (in ppm) is (GATE MT 2016)
- 41) During isothermal phase transformation (in solid-state), fraction transformed is measured at two different transformation times:

Transformation Time, t (s)	Fraction Transformed, f
75	0.11
150	0.37

(1)

Assuming Avrami kinetics [$f = 1 - \exp(-kt^n)$], the fraction transformed in 300 seconds is (GATE MT 2016)

- 42) Zinc oxide is reduced at a constant temperature in a closed reactor using ZnO(s) and C(s) as the only starting materials. The following reactions are assumed to be at thermodynamic equilibrium:



Assume ideal gas behaviour. Based on mole balance, the relationship applicable to the system at equilibrium is

- a) $p_{Zn} = p_{CO} + 2p_{CO_2}$
 b) $p_{Zn} = 2p_{CO} + p_{CO_2}$
 c) $p_{Zn} = p_{CO} + p_{CO_2}$
 d) $p_{Zn} = 0.5p_{CO} + 2p_{CO_2}$

(GATE MT 2016)

- 43) The critical nucleus size (in nm) when copper melt is under-cooled by 100 K is

Given data:

Melting point: 1356 K

Density: 8900 kg.m^{-3}

Solid-liquid interfacial energy: 0.5 Jm^{-2}

Latent heat of freezing: 13000 J.mol^{-1}

Molar volume: $7 \times 10^{-6} \text{ m}^3 \text{mol}^{-1}$

- a) 0.36 b) 1.55 c) 3.65 d) 7.30

(GATE MT 2016)

- 44) The density and corresponding crystallinity of two poly-propylene material are given below

Density, kg.m^{-3}	Crystallinity, %
904	62.8
895	54.4

The density of totally amorphous poly-propylene (in kg.m^{-3}) is:

- a) 723 b) 841 c) 905 d) 956

(GATE MT 2016)

- 45) A simplified energy band-diagram of an intrinsic semiconductor at thermal equilibrium (300 K) is shown. In the accompanying table, which one of the four columns correctly represents the listed parameters? Assume same effective mass for electrons and holes.

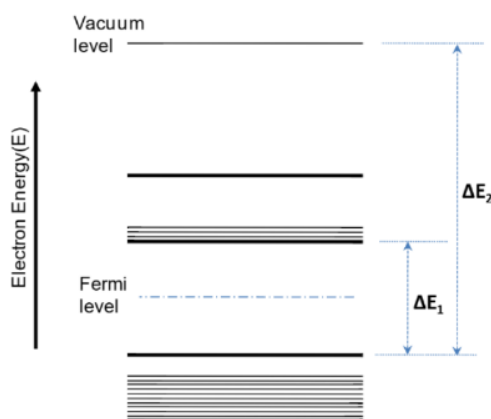


Fig. 4.

Parameter	Column 1	Column 2	Column 3	Column 4
Band-gap	ΔE_1	ΔE_1	ΔE_2	ΔE_1
Electron affinity	$\Delta E_2/2$	ΔE_1	$\Delta E_2/2$	$\Delta E_1 - (\Delta E_2/2)$
Work function	$\Delta E_1 + \Delta E_2$	$\Delta E_2 - (\Delta E_1/2)$	$\Delta E_1 - \Delta E_2/2$	$\Delta E_2 + (\Delta E_1/2)$

- a) Column 1 b) Column 2 c) Column 3 d) Column 4

(GATE MT 2016)

- 46) A binary phase diagram is shown in the schematic.

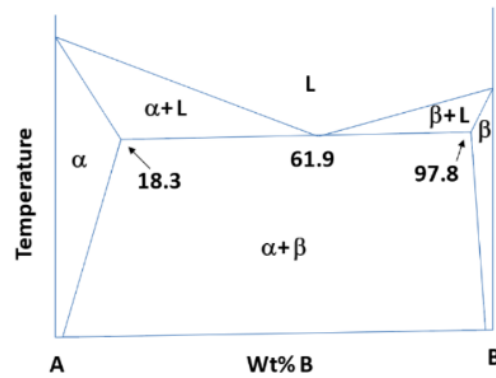


Fig. 5.

Upon complete solidification of a binary alloy system A-B, the fraction of pro-eutectic α -phase present is 0.50. The alloy composition in terms of wt% B is: (GATE MT 2016)

- 47) Fatigue behaviour of an aluminium alloy is shown in the S N plot. A piston rod made of this material is subjected to: (i) 1000 cycles at 420 MPa, followed by (ii) 1000 cycles at 300 MPa.

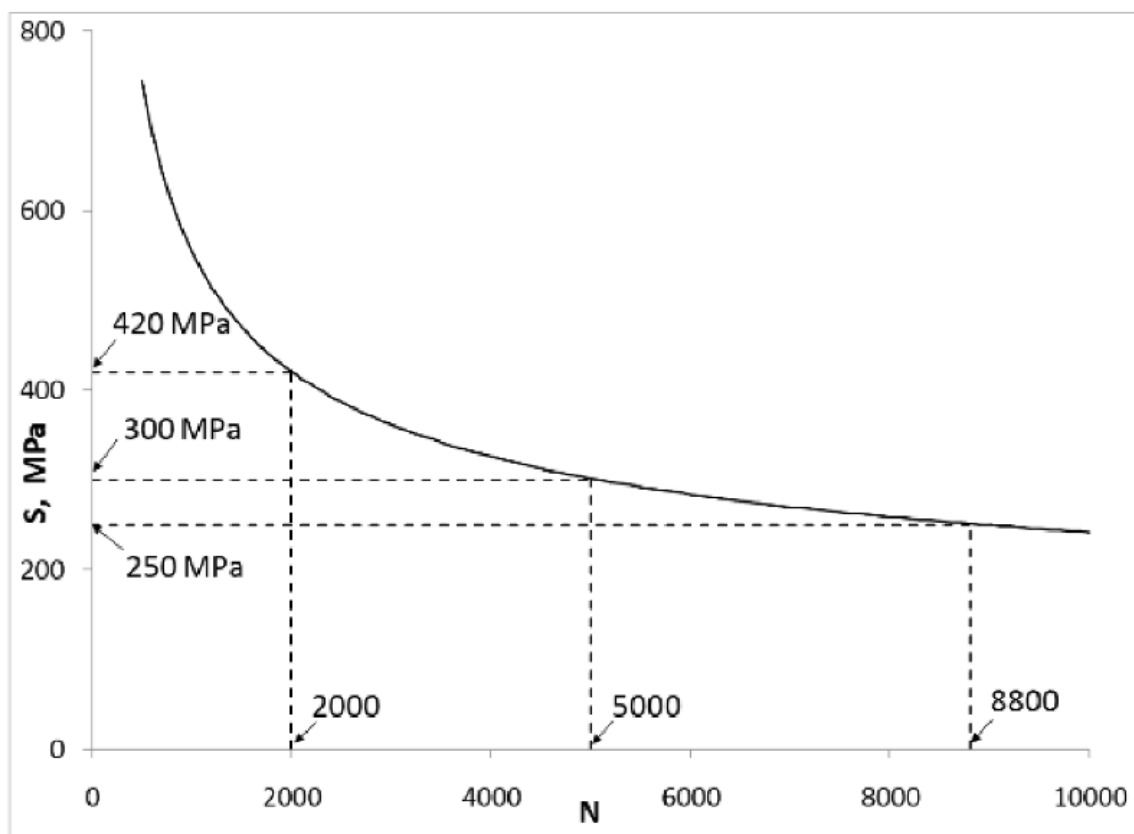


Fig. 6.

Using Miner's rule of cumulative damage, the remaining fatigue life (in terms of number of cycles) at stress of 250 MPa is (GATE MT 2016)

- 48) A glass plate has two parallel cracks. One of them is an internal crack of length $5 \mu\text{m}$ and the other is a surface crack of length $3 \mu\text{m}$. A tensile stress is applied perpendicular to the crack surfaces. The fracture stress (in MPa) is

Given data (for glass plate):

Young's Modulus = 70 GPa

Surface energy per unit area = 1 J.m^{-2} (GATE MT 2016)

- 49) A tensile stress is applied along the [100] direction in a FCC metal crystal. The critical resolved shear stress is 6 MPa. The tensile stress (in MPa) required for initiating slip on the (111) slip plane is (GATE MT 2016)
- 50) For a bcc metal the ratio of the surface energy per unit area of the (100) plane to that of the (110) plane is (GATE MT 2016)
- 51) For a polymer reinforced with 40 vol.% glass fiber, the elastic modulus (in GPa) along the transverse direction is

- a) 5.6 b) 8.1 c) 30.1 d) 43.4

[$E_{\text{glass fiber}} = 70 \text{ GPa}$; $E_{\text{polymer}} = 3.5 \text{ GPa}$] (GATE MT 2016)

- 52) In a sand-mould, a sprue of 0.25 m height and a top cross-section area of 2.2 m^2 is provided to maintain the melt flow rate at $4 \text{ m}^3\text{s}^{-1}$. To prevent aspiration of molten metal, the maximum cross-section area (in m^2) at the base of the sprue is (GATE MT 2016)
- 53) For casting a cylindrical aluminum bloom having a length of 1000 mm and diameter of 750 mm, the approximate solidification time (in minutes) estimated using Chvorinov's rule is

- a) 45 b) 316 c) 440 d) 620

[The mould constant is 2 s/mm^2] (GATE MT 2016)

- 54) A liquid phase sintered SiC-Ni composite has a solid-solid grain boundary energy ($\gamma_{\text{SiC-SiC}}$) of 0.80 J.m^{-2} and a solid-liquid ($\gamma_{\text{SiC-Ni}}$) interfacial energy of 0.45 J.m^{-2} . For a SiC grain size of $20 \mu\text{m}$, the average interparticle (SiC-SiC) neck size (in μm) is:

- a) 3.03 b) 4.28 c) 9.16 d) 18.32

(GATE MT 2016)

- 55) Match the deformation processes in Column I with the corresponding stress states listed in Column II

Column I	Column II
Wire Drawing	[1] Direct Compression
Forging	[2] Indirect Compression
Stretch Forming	[3] Tension
Cutting	[4] Shear

- a) P-1; Q-2; R-3; S-4 c) P-2; Q-1; R-3; S-4
- b) P-1; Q-2; R-4; S-3 d) P-2; Q-1; R-4; S-3

(GATE MT 2016)