# EE25BTECH11002 - Achat Parth Kalpesh

QUESTIONS 1-20 (1 MARK EACH)

1) Given  $y = x^2 + 2x + 10$ , the value of  $\frac{dy}{dx}\Big|_{x=1}$  is equal to

(GATE-IN 2008)

a) 0

b) 4

c) 12

d) 13

2)  $\lim_{x\to 0} \frac{\sin x}{x}$  is

(GATE-IN 2008)

a) indeterminate

b) 0

c) 1

d) ∞

3) The power supplied by the dc voltage source in the circuit shown below is Fig. 1 (GATE-IN 2008)

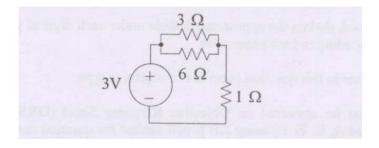


Fig. 1.

a) 0 W

- b) 1.0 W
- c) 2.5 W
- d) 3.0 W
- 4) The current I supplied by the dc voltage source in the circuit shown below is Fig. 2 (GATE-IN 2008)

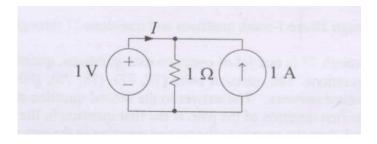


Fig. 2.

a) 0 A

b) 0.5 A

c) 1 A

d) 2 A

5) For signal conditioning of a piezoelectric type transducer we require

(GATE-IN 2008)

- a) a charge amplifier
- b) a differential amplifier

- c) an instrumentation amplifier
- d) a transconductance amplifier
- 6) A linear variable differential transformer (LVDT) is

- a) a displacement transducer
- b) an impedance matching transformer
- c) a differential temperature sensor
- d) an auto transformer
- 7) The temperature being sensed by a negative temperature coefficient (*NTC*) type thermistor is linearly increasing. Its resistance will (GATE-IN 2008)
  - a) linearly increase with temperature
- c) linearly decrease with temperature
- b) exponentially increase with temperature
- d) exponentially decrease with temperature
- 8) For a single stage BJT common base amplifier,

(GATE-IN 2008)

- a) current gain as well as voltage gain can be greater than unity
- b) current gain can be greater than unity but voltage gain is always less than unity
- c) voltage gain can be greater than unity but current gain is always less than unity
- d) current gain as well as voltage gain is always less than unity
- 9) In the circuit shown below Fig. 3, the ideality factor n of the diode is unity and the voltage drop across it is 0.7 V. The dynamic resistance of the diode at room temperature is approximately voltage gain can be greater than unity but current gain is always less than unity (GATE-IN 2008)

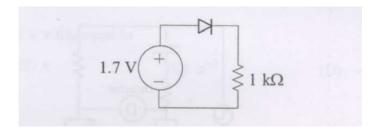


Fig. 3.

a) 15 Ω

b) 25 Ω

c)  $50 \Omega$ 

d)  $700 \Omega$ 

10) An ideal op-amp has the characteristics of an ideal

(GATE-IN 2008)

- a) voltage controlled voltage source
- c) current controlled voltage source
- b) voltage controlled current source
- d) current controlled current source
- 11) The inverters in the ring oscillator circuit shown below Fig. 4 are identical. If the output waveform has a frequency of 10 MHz, the propagation delay of each inverter is (GATE-IN 2008)

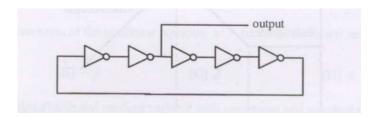


Fig. 4.

a) 5 ns

b) 10 ns

c) 20 ns

- d) 50 ns
- 12) A 2K×8 bit RAM is interfaced to an 8-bit microprocessor. If the address of the first memory location in the RAM is 0800H, the address of the last memory location will be (GATE-IN 2008)

- a) 1000H
- b) 0FFFH
- c) 4800H
- d) 47FFH
- 13) The fundamental period of the discrete-time signal  $x[n] = e^{j(\frac{5\pi}{6})n}$  is

(GATE-IN 2008)

a)  $\frac{6}{5\pi}$ 

b)  $\frac{12}{5}$ 

c) 6

- d) 12
- 14) Which one of the following discrete-time systems is time invariant?

(GATE-IN 2008)

- a) y[n] = nx[n]
- b) y[n] = x[3n]
- c) y[n] = x[-n]
- d) y[n] = x[n-3]
- 15) If a curent of  $\left[-6\sqrt{2}\sin\left(100\pi t\right) + 6\sqrt{2}\cos\left(300\pi t + \frac{\pi}{4}\right) + 6\sqrt{2}\right]A$  is passed through a true RMS ammeter, the meter reading will be (GATE-IN 2008)
  - a)  $6\sqrt{2}$  A
- b)  $\sqrt{126} \text{ A}$
- c) 12 A

- d)  $\sqrt{216}$  A
- 16) If the ac bridge circuit shown below Fig. 5 is balanced, the element Z can be a (GATE-IN 2008)

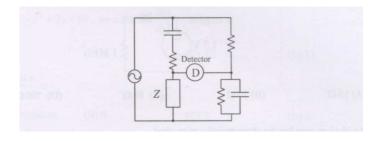


Fig. 5.

a) pure capacitor

c) R-L series combination

b) pure inductor

- d) R-L parallel combination
- 17) The Bode asymptotic plot of a transfer function is given belowFig. 6. In the frequency range shown, the transfer function has (GATE-IN 2008)

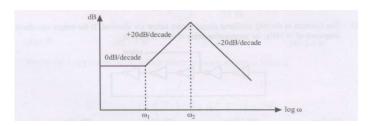


Fig. 6.

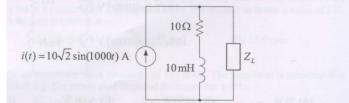
a) 3 poles and 1 zero

c) 2 poles and 1 zero

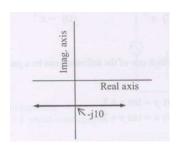
b) 1 pole and 2 zeros

- d) 2 poles and 2 zeros
- 18) For radioisotope imaging, an Anger camera is fitted with a parallel hole collimator. If the thickness of the collimator is increased, the camera (GATE-IN 2008)
  - a) resolution and sensitivity will increase
  - b) resolution and sensitivity will decrease
  - c) resolution will increase and sensitivity will decrease
  - d) resolution will decrease and sensitivity will increase
- 19) In the standard 12-lead ECG recording system, the minimum number of electrodes required to be attached to a human subject for recording any one of the unipolar chest lead signals is (GATE-IN 2008)

	a) 1	b) 2	c) 4	d) 5				
20)	O) A laser light with a wavelength of 633 nm is passed through 1 cm length of tissue and 2 cm length of glass. The refractive indices of tissue and glass are 1.33 and 1.5 respectively. The velocities of laser light in the tissue and in the glass are in the ratio of (GATE-IN 2008)							
	a) 1.33: 0.75	b) 1.33: 3.0	c) 1.33: 1.5	d) 1.5: 1.33				
		Questions 21-7	5 (2 marks each)					
21)	The expression $e^{-lnx}$ for	x > 0 is equal to		(GATE-IN 2008)				
	a) -x	b) <i>x</i>	c) $x^{-1}$	d) $-x^{-1}$				
22)	Consider the differential of this differential equat	equation $\frac{dy}{dx} = 1 + y^2$ . Whition?	ch one of the following ca	an be a particular solution (GATE-IN 2008)				
	a) $y = tan(x+3)$	b) $y = tanx + 3$	c) $x = tan(y+3)$	d) x = tany + 3				
23)	Consider the function y interval 2 to 5 is	$y = x^2 - 6x + 9.$ The maxi	mum value of y obtained	d when x varies over the (GATE-IN 2008)				
	a) 1	b) 3	c) 4	d) 9				
24)	It is known that two root will be	ots of the nonlinear equat	$x^3 - 6x^2 + 11x - 6 =$	0 are 1 and 3. The third (GATE-IN 2008)				
	a) <i>j</i>	b) - <i>j</i>	c) 2	d) 4				
25)	25) Consider a Gaussian distributed random variable with zero mean and standard deviation $\sigma$ . The value of its cumulative distribution function at the origin will be (GATE-IN 2008)							
	a) 0	b) 0.5	c) 1	d) $10 \sigma$				
26) A random variable is uniformly distributed over the interval 2 to 10. Its variance will be (GATE-IN 2008)								
	a) $\frac{16}{3}$	b) 6	c) $\frac{256}{9}$	d) 36				
27) The Fourier transform of $x(t) = e^{-at}u(-t)$ , where $u(t)$ is the unit step function, (GATE-IN 2008)								
	<ul><li>a) exists for any real va</li><li>b) does not exist for any</li></ul>			e of a is strictly negative e of a is strictly positive				
28) In the circuit shown below Fig. 7 the maximum power that can be transferred to the load ZL is (GATE-IN 2008)								
	10 V (2001)							
	10Ω ≶							



- a) 250 W
- b) 500 W
- c) 1000 W
- d) 2000 W
- 29) A complex variable Z = x + j0.1 has its real part x varying in the range  $-\infty$  to  $\infty$ . Which of the following is the locus (shown in thick lines) of  $\frac{1}{Z}$  in the complex plane? (GATE-IN 2008)



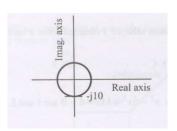
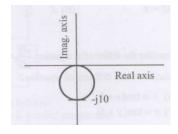


Fig. 10.

Fig. 8.

a)

c)



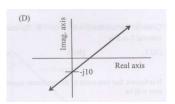


Fig. 11.

Fig. 9.

b)

d)

30) For the circuit shown belowFig. 12 the input resistance  $R_{11} = \frac{V_1}{I_1}\Big|_{I_2=0}$  is

(GATE-IN 2008)

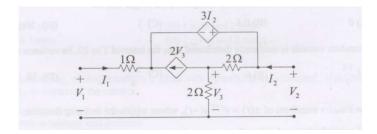


Fig. 12.

a)  $-3 \Omega$ 

b) 2 Ω

c) 3 Ω

- d) 13 Ω
- 31) In the circuit shown below Fig. 13 the average power consumed by the  $1\Omega$  resistor is (GATE-IN 2008)

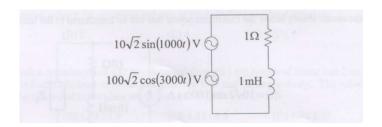


Fig. 13.

- a) 50 W
- b) 1050 W
- c) 5000 W
- d) 10100 W
- 32) Which one of the following equations is valid for the circuit shown below? Fig. 14 (GATE-IN 2008)

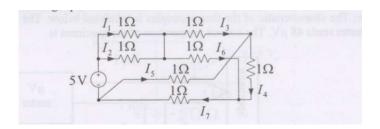


Fig. 14.

- a)  $I_3 + I_5 I_6 + I_7 = 0$ b)  $I_3 I_5 + I_6 + I_7 = 0$

- c)  $I_3 + I_5 + I_6 + I_7 = 0$ d)  $I_3 + I_5 + I_6 I_7 = 0$
- 33) For the circuit shown below Fig. 15 the steady-state current I is

(GATE-IN 2008)

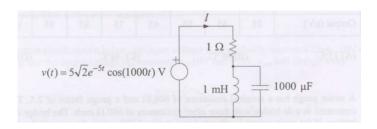


Fig. 15.

a) 0 A

- b)  $5\sqrt{2}\cos(1000t)A$  c)  $5\sqrt{2}\cos(1000t \frac{\pi}{4})A$  d)  $5\sqrt{2}A$
- 34) For the circuit shown below Fig. 16 the voltage across the capacitor is

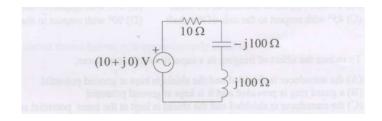


Fig. 16.

- a) (10 + i0) V
- b) (100 + i0) V
- c) (0 + j100) V
- d) (0 i100) V
- 35) The speed of a gear having 60 teeth is measured using a proximity sensor. The output of the proximity sensor is fed to a counter with a gating time of 1s. The counter indicates a value of 120. The speed at which the gear is rotating is

  (GATE-IN 2008)
  - a) 60 rpm
- b) 120 rpm
- c) 600 rpm
- d) 1200 rpm
- 36) A piezoelectric type accelerometer has a sensitivity of 100 mV/g. The transducer is subjected to a constant acceleration of 5 g. The steady state output of the transducer will be (GATE-IN 2008)
  - a) 0 V

- b) 100 mV
- c) 0.5 V

- d) 5 V
- 37) A pair of identical thermocouples is employed for measuring the temperature of a specimen as shown below. Fig. 17 The characteristic of the thermocouples is tabulated below. The reference junction is at  $2^{\circ}$ C. The meter reads 48  $\mu$ V. The correct temperature of the specimen is (GATE-IN 2008)

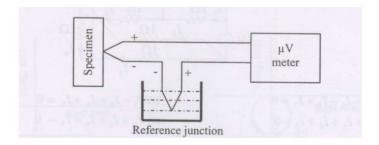


Fig. 17.

Temperature ( ${}^{\circ}C$ )	0	10	20	30	40	50	60	70	80	90
Output (µV)	35	45	55	65	75	85	95	105	115	125
TABLE I										

a) 13°C

b) 46°C

c) 48°C

- d) 50°C
- 38) A strain gauge has a nominal resistance of  $600\Omega$  and a gauge factor of 2.5. The strain gauge is connected in a dc bridge with three other resistances of  $600\Omega$  each. The bridge is excited by a 4 V battery. If the strain gauge is subjected to a strain of  $100 \, \mu\text{m/m}$ , the magnitude of the bridge output will be (GATE-IN 2008)
  - a) 0*V*

- b) 250 μV
- c)  $500 \mu V$
- d)  $750 \mu V$
- 39) The torque in a rotating shaft is measured using strain gauges. The strain gauges must be positioned on the shaft such that the axes of the strain gauges are at (GATE-IN 2008)
  - a)  $0^{\circ}$  with respect to the axis of the shaft
- c) 45° with respect to the axis of the shaft
- b) 30° with respect to the axis of the shaft
- d) 90° with respect to the axis of the shaft
- 40) To reduce the effect of fringing in a capacitive type transducer,

- a) the transducer is shielded and the shield is kept at ground potential
- b) a guard ring is provided and it is kept at ground potential
- c) the transducer is shielded and the shield is kept at the same potential as the moving plate

- d) a guard ring is provided and it is kept at the same potential as the moving plate
- 41) A differential amplifier shown below Fig. 18 has a differential mode gain of 100 and a CMRR of 40 dB. If  $V_1 = 0.55$ V and  $V_2 = 0.45$  V, the output  $V_0$  is (GATE-IN 2008)

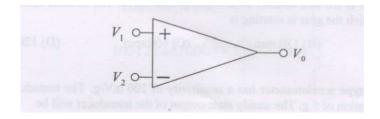


Fig. 18.

a) 10 V

- b) 10.5 V
- c) 11 V

d) 15 V

42) The op-amp circuit shown below Fig. 19 is that of a

(GATE-IN 2008)

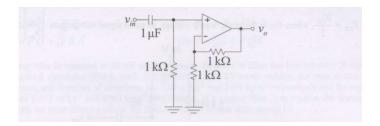


Fig. 19.

- a) low-pass filter with a maximum gain of 1
- c) high-pass filter with a maximum gain of 1
- b) low-pass filter with a maximum gain of 2
- d) high-pass filter with a maximum gain of 2
- 43) In the op-amp circuit shown below Fig. 20, the input voltage  $v_{in}$  is gradually increased from -10V to +10V. Assuming that the output voltage  $v_{out}$  saturates at -10V and +10V,  $V_{out}$  will change from (GATE-IN 2008)

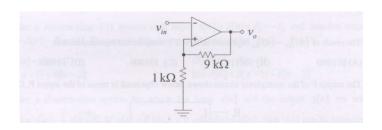


Fig. 20.

- a) -10 V to +10 V when  $v_{in}$  =-1 V b) -10 V to +10 V when  $v_{in}$  = +1 V d) +10 V to -10 V when  $v_{in}$  = +1 V
- 44) For the op-amp circuit shown below Fig. 21,  $v_0$  is approximately equal to

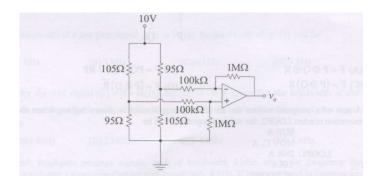


Fig. 21.

- a) -10 V
- b) -5 V

- c) +5 V
- d) +10 V
- 45) In the amplifier circuit shown below Fig. 22, assume  $V_{BE} = 0.7$  V and the  $\beta$  of the transistor and the values of  $C_1$  and  $C_2$  are extremely high. If the amplifier is designed such that at the quiescent point its  $V_{CE} = \frac{V_{CC}}{2}$  where  $V_{CC}$  is the power supply voltage, its small signal voltage gain  $|\frac{V_{out}}{V_{in}}|$  will be (GATE-IN 2008)

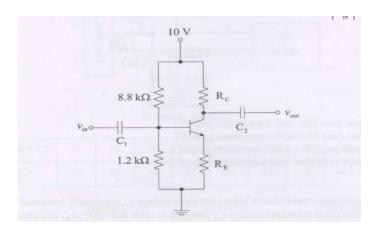


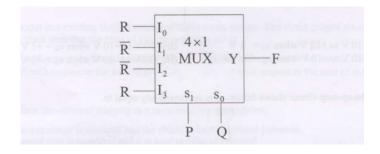
Fig. 22.

a) 3.75

b) 4.5

c) 9

- d) 19
- 46) The result of  $(45)_{10}$   $(45)_{16}$  expressed in 6-bit 2's complement representation is (GATE-IN 2008)
  - a) 011000
- b) 100111
- c) 101000
- d) 101001
- 47) The output F of the multiplexer circuit shown below Fig. 23 expressed in terms of the inputs P, Q and R is (GATE-IN 2008)



	MOV C, A LOOP1: INR A DAA JC LOOP2 INR C JNC LOOP1 LOOP2: NOP (GATE-IN 2008)						
	a) 63 H	b) 64 H	c) 99 H	d) 100 H			
49)	The minimum sum of $P\bar{Q}RS + P\bar{Q}R\bar{S} + \bar{P}\bar{Q}R\bar{S}$	products form of the Book $S\bar{S}$	blean expression $Y = \bar{P}\bar{Q}$	$Q\bar{R}\bar{S} + P\bar{Q}\bar{R}\bar{S} + P\bar{Q}\bar{R}S + (GATE-IN 2008)$			
	a) $Y = P\bar{Q} + \bar{Q}\bar{S}$ b) $Y = P\bar{Q} + \bar{Q}R\bar{S}$		c) $Y = P\bar{Q} + \bar{Q}\bar{R}\bar{S}$ d) $Y = \bar{Q}\bar{S} + P\bar{Q}R$				
50)	0) An X-ray tube is operated at 80 kV anode voltage. In order to filter the low intensity X-rays, a 2.5 mm thick aluminum filter is used. It is given that at 80 kV anode voltage, the mass attenuation coefficients and densities of aluminum are 0.02 m <sup>2</sup> kg <sup>-1</sup> and 2699 kg m <sup>-3</sup> respectively and for copper these are 0.075 m <sup>2</sup> kg <sup>-1</sup> and 8960 kg m <sup>-3</sup> respectively. If a copper filter is to replace the aluminum filter with the same filtering effect, the thickness of the copper filter should be (GATE-IN 2008)						
	a) 0.2 mm	b) 0.66 mm	c) 1.5 mm	d) 5 mm			
51)	an interface with a liver are 0.075 Np cm <sup>-1</sup> /MH of fat-liver interface is	e travels from a transducer tissue at normal incidence Iz and 0.1 Np cm <sup>-1</sup> / $MHz0.1. Taking both attenuationsse when it returns to the$	e. The amplitude attenuation respectively. The amplitude and reflection losses in	on factors of fat and liver ade reflectivity coefficient			
	a) 0.74	b) -2.6	c) -6	d) -33			
52)		e LTI system with input <i>x</i> atput of the system will be		impulse response $h[n] =$ (GATE-IN 2008)			
	a) $\delta[n] - \delta[n-2]$ b) $\delta[n] - \delta[n-1]$		c) $\delta[n-1] + \delta[n-2]$ d) $\delta[n] + \delta[n-1] + \delta[n$	(i-2]			
53)		e system for which the in $= 0$ for $n < 0$ and $x[n] =$					
	a) $\left(\frac{-1}{3}\right)^n u[n]$	b) $\left(\frac{1}{3}\right)^n u[n]$	c) $(3)^n u[n]$	d) $(-3)^n u[n]$			

54) If the bandwidth of a low-pass signal g(t) is 3 kHz, the bandwidth of  $g^2(t)$  will be (GATE-IN 2008)

a)  $F = P \oplus Q \oplus R$  b) F = PQ + QR + RP c)  $F = (P \oplus Q)R$  d)  $F = (P \oplus Q)\bar{R}$ 

reaches LOOP2, the value of register C will be

48) A part of a program written for an 8085 microprocessor is shown below. When the program execution

	a) $\frac{3}{2}$ MHz	b) 3 MHz	c) 6 kHz	d) 9 kHz			
55)	Consider the AM signal $s(t) = [1+m(t)]\cos 2\pi ft$ . It is given that the bandwidth of the real, low-pass message signal $m(t)$ is 2 kHz. If $f_c = 2$ MHz, the bandwidth of the band-pass signal $s(t)$ will be (GATE-IN 2008)						
	a) 2.004 Hz	b) 2 kHz	c) 4 kHz	d) 2 kHz			
56)	tiplexed over a band-pa adjacent signals should	ssage signals, each of bar ass channel with bandwid be of 500 Hz width and channel, the value of B sl	th B kHz. If the guard be there is no need to provi	oand in between any two			
	a) 30	b) 34.5	c) 35	d) 35.5			
57)	The region of converge (GATE-IN 2008)	ence of the z-transform of	of the discrete-time signa	$1 x[n] = 2^n u[n] \text{ will be}$			
	a) $ z  > 2$	b) $ z  < 2$	c) $ z  > \frac{1}{2}$	d) $ z  < \frac{1}{2}$			
58)	B) The step response of a linear time invariant system is $y(t) = 5 e^{-10t} u(t)$ , where $u(t)$ is the unit step function. If the output of the system corresponding to an impulse input $\delta(t)$ is $h(t)$ , then $h(t)$ is (GATE-IN 2008)						
	a) $-50 e^{-10t} u(t)$ b) $5 e^{-10t} \delta(t)$		c) 5 $u(t)$ -50 $e^{-10t}$ $\delta(t)$ d) 5 $\delta(t)$ -50 $e^{-10t}$ $u(t)$				
59)	59) A 2 A full-scale PMMC type dc ammeter has a voltage drop of 100 mV at 2 A. The meter can be converted into a 10 A full-scale dc ammeter by connecting a (GATE-IN 2008)						
	a) 12.5 m $\Omega$ resistor in p b) 12.5 m $\Omega$ resistor in s		c) $50.0 \text{ m}\Omega$ resistor in pd) $50.0 \text{ m}\Omega$ resistor in s				
60)	O) A $3\frac{1}{2}$ digit, 200 mV full scale DVM has an accuracy specification of $\pm$ 0.5% of reading plus 5 counts. When the meter reads 100 mV, the voltage being measured is (GATE-IN 2008)						
	<ul><li>a) any value between 99</li><li>b) any value between 99</li></ul>		c) exactly 99.5 mV d) exactly 100 mV				
61)	A 230 V, 5 A, 50 Hz single phase house service energy meter has a meter constant of 360 rev/kWhr. The meter takes 50 s for making 51 revolutions of the disc when connected to a 10 kW, unity power factor load. The error in the reading of the meter is (GATE-IN 2008)						
	a) 0 %	b) +0.5 %	c) -2.0 %	d) +2.0 %			

62) The op-amp based circuit of a half wave rectifier electronic voltmeter shown below Fig. 24 uses a *PMMC* ammeter with a full scale deflection (FSD) current of 1 mA and a coil resistance of 1 k $\Omega$ . The value of R that gives FSD for a sinusoidal input voltage of 100 mV (*RMS*) is (GATE-IN 2008)

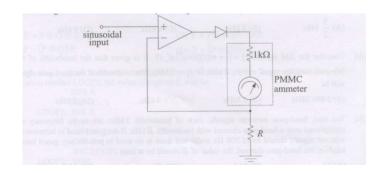


Fig. 24.

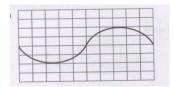
a) 45 Ω

b)  $67.5 \Omega$ 

c) 100 Ω

d) 144.4 Ω

63) The x and y sensitivities of an analog oscilloscope are set as 2 ms/cm and 1V/cm respectively. The trigger is set at 0V with negative slope. An input of  $2 \cos(100\pi t + 30^\circ)$  V is fed to the y input of the oscilloscope. The waveform seen on the oscilloscope will be (GATE-IN 2008)



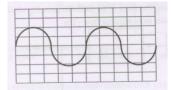
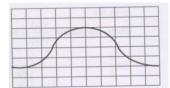


Fig. 25.

a)

c)

Fig. 27.



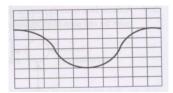


Fig. 26.

Fig. 28.

b)

d)

- 64) The open loop transfer function of a unity feedback system is  $G(s) = \frac{K(s+2)}{(s+1+j1)(s+1-j1)}$ . The root locus plot of the system has (GATE-IN 2008)
  - a) two breakaway points located at s = -0.59 and s = -3.41
  - b) one breakaway point located at s = -0.59
  - c) one breakaway point located at s = -3.41
  - d) one breakaway point located at s = -1.41
- 65) If a first order system and its time response to a unit step input are as shown below in Fig. 29, the gain K is (GATE-IN 2008)

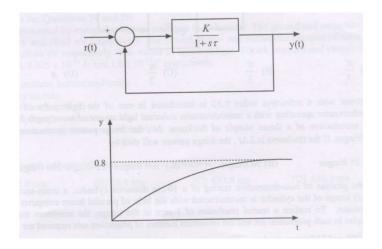


Fig. 29.

a) 0.25

b) 0.8

c) 1

d) 4

66) The state space representation of a system is given by

$$\dot{x} = \begin{pmatrix} 0 & 1 \\ 0 & -3 \end{pmatrix} x + \begin{pmatrix} 1 \\ 0 \end{pmatrix} u \tag{1}$$

$$y = \begin{pmatrix} 1 & 0 \end{pmatrix} x \tag{2}$$

The transfer function  $\frac{Y(s)}{U(s)}$  of the system will be

(GATE-IN 2008)

a)  $\frac{1}{s}$ 

b)  $\frac{1}{s(s+3)}$ 

c)  $\frac{1}{s+3}$ 

d)  $\frac{1}{s^2}$ 

67) A closed loop control system is shown below. Fig. 30 The range of the controller gain  $K_C$  which will make the real parts of all the closed loop poles more negative than -1 is (GATE-IN 2008)

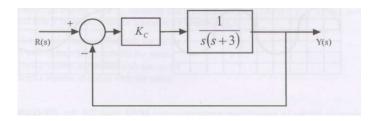


Fig. 30.

- a)  $K_C > -4$
- b)  $K_C > 0$
- c)  $K_C > 2$
- d)  $K_C < 2$

68) For the closed loop system shown below Fig. 31 to be stable, the value of time delay  $T_D$  (inseconds) should be less than (GATE-IN 2008)

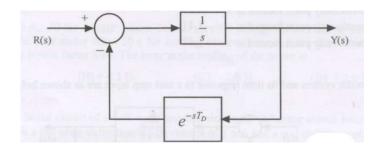


Fig. 31.

- a)  $\frac{\pi}{4}$ b)  $\frac{\pi}{3}$ c)  $\frac{\pi}{2}$ d)  $\pi$
- 69) A tissue with a refractive index 1.33 is introduced in one of the light paths of a Michelson interferometer operating with a monochromatic coherent light source of wavelength 589 nm. After the introduction of a tissue sample of thickness  $\Delta t$ , the fringe pattern is observed to shift by 50 fringes. If the thickness is  $2 \Delta t$ , the fringe pattern will shift by (GATE-IN 2008)
  - a) 25 fringes
- b) 50 fringes
- c) 100 fringes
- d) 200 fringes
- 70) In the process of non-destructive testing of a 10 cm diameter cylinder, a cross-sectional (transaxial) image of the cylinder is reconstructed with the help of parallel beam computer tomography technique. To realize a spatial resolution of 1 mm in the image, the minimum number of ray samples in each projection set and the minimum number of projection sets required are (GATE-IN 2008)
  - a) 200 and 315 respectively

c) 200 and 629 respectively

b) 100 and 315 respectively

d) 100 and 629 respectively

#### COMMON DATA QUESTIONS

**Common Data for Questions 71,72 and 73** A data acquisition system (DAS) shown below Fig. 32 employs a successive approximation type 12-bit ADC having a conversion time of 5  $\mu$ s.

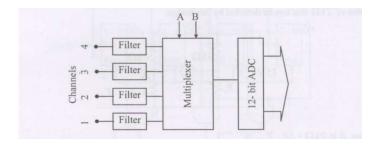


Fig. 32.

71) The quantization error of the ADC is

(GATE-IN 2008)

d) 
$$+ 0.048 \%$$

72) The system is used as a single channel DAS with channel 1 selected as input to the ADC which is set in the continuous conversion mode. For avoiding aliasing error, the cutoff frequency  $f_c$  of the (GATE-IN 2008) filter in channel 1 should be

a)  $f_c < 100 \text{ kHz}$ 

c)  $100 \text{ kHz} < f_c < 200 \text{ kHz}$ 

b)  $f_c = 100 \text{kHz}$ 

- d)  $f_c = 200 \text{ kHz}$
- 73) If the multiplexer is controlled such that the channels are sequenced every 5 us as 1, 2, 1, 3, 1, 4, 1, 2, 1, 3, 1, 4, 1, ...., the input connected to channel 1 will be sampled at the rate of (GATE-IN 2008)
  - a) 25k samples/s
- b) 50k samples/s
- c) 100k samples/s
- d) 200k samples/s

## Common Data for Questions 74 and 75

Laser light is generated by energizing helium-neon gas in a chamber. The ground and metastable states of helium are 0 eV and 20.61 eV respectively. The ground, higher and metastable energies of neon are 0 eV, 18.70 eV and 20.66 eV respectively. The values of speed of light, Planck constant and charge of electron are  $3 \times 10^8$  m/s,  $6.625 \times 10^{-34}$  4 Js and  $1.6 \times 10^{19}$  C respectively.

74) In this process, helium molecules

(GATE-IN 2008)

a) play no role

c) give energy to neon molecules

b) produce laser light

d) absorb energy from neon molecules

75) Wavelength of laser light generated in this process is

(GATE-IN 2008)

- a) 61.6 nm
- b) 66.4 nm
- c) 633.8 nm
- d) 650.3 nm

Linked Answer Questions: Q.76 to Q.85 carry two marks each

## Statement for Linked Answer Questions 76 and 77:

In the Wheatstone bridge shown below Fig. 33 the galvanometer G has a current sensitivity of 1  $\mu$ A/mm, a resistance of 2.5 k $\Omega$ and a scale resolution of 1 mm. Let  $\Delta R$  be the minimum increase in R from its nominal value of 2k $\Omega$  that can be detected by this bridge.

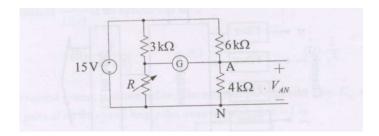


Fig. 33.

76) When R is  $2k\Omega + \Delta R$ ,  $V_{AN}$  is

(GATE-IN 2008)

a) 6 V

- b) 6.0024 V
- c) 6.0038 V
- d) 6.005 V

77) The value of  $\Delta R$  is approximately

(GATE-IN 2008)

- a)  $2.8 \Omega$
- b)  $3.4 \Omega$
- c)  $5.2 \Omega$
- d)  $12 \Omega$

#### Statement for Linked Answer Questions 78 and 79:

In the circuit shown below Fig. 34 the steady-state is reached with the switch K open. Subsequently the switch is closed at time t = 0.

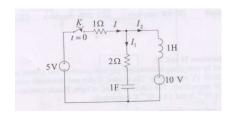


Fig. 34.

78) At time  $t = 0^+$ , current I is

(GATE-IN 2008)

a)  $-\frac{5}{3}$  A

b) 0 A

c)  $\frac{5}{3}$  A

d)  $\infty$  A

79) At time  $t = 0^+, \frac{dI_2}{dt}$ 

(GATE-IN 2008)

- a) -5 A/s
- b)  $-\frac{10}{3}$  A/s
- c) 0 A/s

d) 5A/s

# Statement for Linked Answer Questions 80 and 81:

Consider the counter circuit shown below.Fig. 35

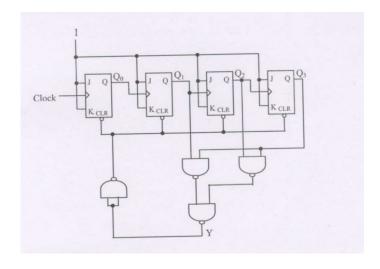


Fig. 35.

80) In the above figure, Y can be expressed as

(GATE-IN 2008)

- a)  $Q_3(Q_2 + Q_1)$
- b)  $Q_3 + Q_2Q_1$
- c)  $\overline{Q_3(Q_2+Q_1)}$
- d)  $\overline{Q_3 + Q_2 Q_1}$

81) The above circuit is a

(GATE-IN 2008)

- a) Mod-8 Counter
- b) Mod-9 Counter
- c) Mod-10 Counter
- d) Mod-11 Counter

Statement for Linked Answer Questions of and of. Consider a unity feedback system with open loop transfer function  $G(s) = \frac{1+6s}{s^2(1+s)(1+2s)}$  (GATE-IN 2008) 82) The phase crossover frequency of the system in radians per second is

a) 0.125

b) 0.25

c) 0.5

d) 1

83) The gain margin of the system is

d) 1

A unity feedback to a unit step in	Statement for Linked Answer Questions 84 and 85: A unity feedback system has open loop transfer function $G(s) = \frac{100}{s(s+p)}$ . The time at w to a unit step input reaches its peak is $\frac{\pi}{8}$ seconds. The damping coefficient for the closed loop system is					
84) The damping co	The damping coefficient for the closed loop system is					
a) 0.4	b) 0.6	c) 0.8	d) 1			
85) The value of p i	.s		(G	ATE-IN 2008)		

c) 0.5

a) 6 b) 12 c) 14 d) 16

b) 0.25

a) 0.125