

IN: INSTRUMENTATION ENGINEERING

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Q.1-Q.20 CARRY ONE MARK EACH

- 1) If $z = x + jy$, where x and y are real, the value of $|e^{jz}|$ is
(GATE IN 2009)
a) 1 b) $e^{\sqrt{x^2+y^2}}$ c) e^y d) e^{-y}
- 2) The value of $\oint \frac{\sin z}{z} dz$, where the contour of integration is a simple closed curve around the origin, is
(GATE IN 2009)
a) 0 b) $2\pi j$ c) ∞ d) $1/(2\pi j)$
- 3) Let $\mathbf{P} \neq \mathbf{0}$ be a 3×3 real matrix. There exist linearly independent vectors \mathbf{x} and \mathbf{y} such that $\mathbf{P}\mathbf{x} = \mathbf{0}$ and $\mathbf{P}\mathbf{y} = \mathbf{0}$. The dimension of the range space of \mathbf{P} is
(GATE IN 2009)
a) 0 b) 1 c) 2 d) 3
- 4) A sphere of unit radius is centered at the origin. The unit normal at a point (x, y, z) on the surface of the sphere is the vector
(GATE IN 2009)
a) (x, y, z) b) $\left(\frac{1}{\sqrt{3}}, \frac{1}{\sqrt{3}}, \frac{1}{\sqrt{3}}\right)$ c) $\left(\frac{x}{\sqrt{3}}, \frac{y}{\sqrt{3}}, \frac{z}{\sqrt{3}}\right)$ d) $\left(\frac{x}{\sqrt{2}}, \frac{y}{\sqrt{2}}, \frac{z}{\sqrt{2}}\right)$
- 5) An LVDT is supplied with a sinusoidal voltage of amplitude 5V and frequency 1kHz. The output is connected to an ac voltmeter. The reading of the voltmeter is 1V for a displacement of 1mm from the null position. When the displacement is 1mm in the opposite direction from the null position, the reading of the voltmeter is
(GATE IN 2009)
a) -1V b) -0.2V c) 1V d) 5V
- 6) The circuit shown in Fig. 1 is

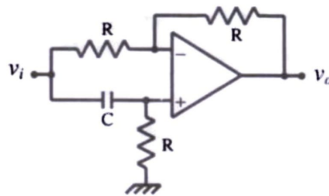


Fig. 1. Circuit Diagram

(GATE IN 2009)

- a) an all-pass filter
 b) a bandpass filter
 c) a highpass filter
 d) a lowpass filter

- 7) The diodes shown in the circuit (Fig. 2) are ideal. A voltage of 0V represents logic 0 and +5V represents logic 1. The logic function Z realized by the circuit for logic inputs X and Y is
 (GATE IN 2009)

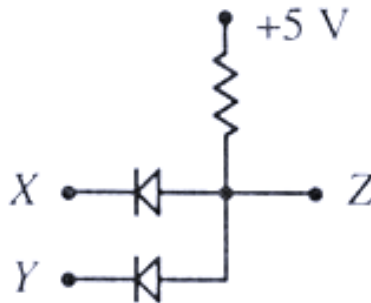


Fig. 2. Circuit Diagram

- a) $Z = X + Y$
 b) $Z = XY$
 c) $Z = \overline{X + Y}$
 d) $Z = \overline{XY}$

- 8) The minimal sum-of-products expression for the logic function f represented by the given Karnaugh map (Fig. 3) is
 (GATE IN 2009)

PQ \ RS	00	01	11	10
00	0	1	0	0
01	0	1	1	1
11	1	1	1	0
10	0	0	1	0

Fig. 3. Karnaugh map

- a) $\overline{Q}S + \overline{P}RS + PQR + \overline{P}RS + \overline{P}Q\overline{R}$
 b) $\overline{Q}S + \overline{P}RS + \overline{P}Q\overline{R} + \overline{P}RS + PQR$
 c) $\overline{P}RS + \overline{P}Q\overline{R} + \overline{P}RS + \overline{P}Q\overline{R}$
 d) $\overline{P}RS + PQR + \overline{P}RS + \overline{P}Q\overline{R}$

- 9) In Fig. 4, the initial state of Q is 0. The output is observed after the application of each clock pulse. The output sequence at Q is
 (GATE IN 2009)

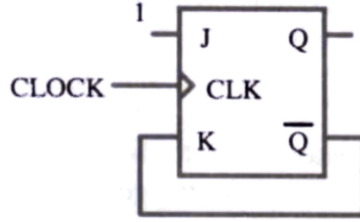


Fig. 4. For Question-9

- a) 0000... b) 1010... c) 1111... d) 1000...

10) The binary representation of the decimal number 1.375 is

(GATE IN 2009)

- a) 1.111 c) 1.011
b) 1.010 d) 1.001

11) Consider a system consisting of microprocessor, memory and peripheral devices connected by a common bus. During DMA data transfer, the microprocessor

(GATE IN 2009)

- a) only reads from the bus
b) only writes to the bus
c) both reads from and writes to the bus
d) neither reads from nor writes to the bus

12) The fundamental period of $x(t) = 2 \sin 2\pi t + 3 \sin 3\pi t$, with t expressed in seconds, is

(GATE IN 2009)

- a) 1s b) 0.67s c) 2s d) 3s

13) A linear time-invariant causal system has a frequency response given in polar form as $\frac{1}{\sqrt{1+\omega^2}} \angle -\tan^{-1}\omega$. For input $x(t) = \sin t$, the output is

(GATE IN 2009)

- a) $\frac{1}{\sqrt{2}} \cos t$ b) $\frac{1}{\sqrt{2}} \cos\left(t - \frac{\pi}{4}\right)$ c) $\frac{1}{\sqrt{2}} \sin t$ d) $\frac{1}{\sqrt{2}} \sin\left(t - \frac{\pi}{4}\right)$

14) A 50% duty cycle square wave with zero mean is used as a baseband signal in an ideal frequency modulator with a sinusoidal carrier of frequency ω_c . The modulated signal is given as an input to an ideal phase demodulator (a circuit that produces an output proportional to the difference in phase of the modulated signal from that of the carrier). The output of the circuit is

(GATE IN 2009)

- a) a square wave
b) a train of impulses with alternating signs
c) a triangular wave
d) a sinusoidal wave

15) Fig. 5 shows a periodic waveform to be displayed on a CRO. A trigger setting which ensures a stationary display is

(GATE IN 2009)

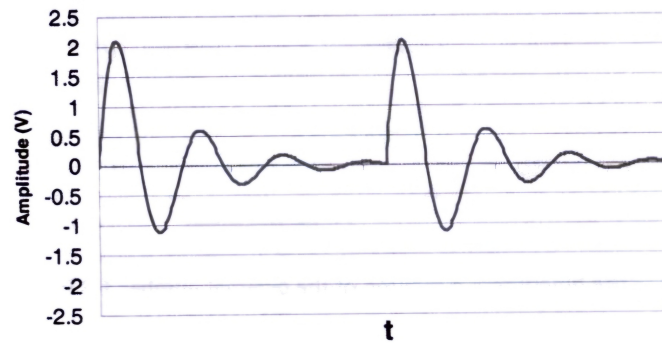


Fig. 5. Waveform

- a) level: 0.2V, slope: -ve
b) level: 0.5V, slope: -ve
c) level: -0.2V, slope: +ve
d) level: 1.8V, slope: -ve
- 16) The input impedance of a CRO is equivalent to a $1\text{M}\Omega$ resistance in parallel with a 45pF capacitance. It is used with a compensated 10-to-1 attenuation probe. The effective input capacitance at the probe tip is
(GATE IN 2009)
- a) 4.5pF
b) 5pF
c) 45pF
d) 450pF
- 17) A galvanometer with internal resistance 100Ω and full-scale current 1mA is used to realize a dc voltmeter with a full scale range of 1V . The full scale range of this voltmeter can be extended to 10V by connecting an external resistance of value
(GATE IN 2009)
- a) $9\text{k}\Omega$
b) $9.9\text{k}\Omega$
c) $10\text{k}\Omega$
d) $11\text{k}\Omega$
- 18) A plant with a transfer function $\frac{2}{s(s+3)}$ is controlled by a PI controller with $K_p = 1$ and $K_i \geq 0$ in a unity feedback configuration. The lowest value of K_i that ensures zero steady state error for a step change in the reference input is
(GATE IN 2009)
- a) 0
b) $1/3$
c) $1/2$
d) 1
- 19) A mass spectrometer is used to resolve peaks corresponding to CO^+ and N_2^+ . The atomic masses are $^{12}\text{C} = 12.0000$, $^{16}\text{O} = 15.9949$ and $^{14}\text{N} = 14.0031\text{amu}$. The resolving power of the mass spectrometer should be atleast
(GATE IN 2009)
- a) 250
b) 350
c) 2500
d) 3500
- 20) Assuming complete dissociation, the pH of a 1mM solution of H_2SO_4 is closest to
(GATE IN 2009)

- a) 3 c) 2.4
b) 2.7 d) 2.1

Q.21 TO Q.60 CARRY TWO MARKS EACH

- 21) The eigenvalues of a (2×2) matrix \mathbf{X} are -2 and -3 . The eigenvalues of the matrix $(\mathbf{X} + \mathbf{I})^{-1} (\mathbf{X} + 5\mathbf{I})$ are
(GATE IN 2009)
a) $-3, -4$ b) $-1, -2$ c) $-1, -3$ d) $-2, -4$
- 22) The matrix $\mathbf{P} \begin{pmatrix} 0 & 0 & 0 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix}$ rotates a vector about the axis $\begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$ by an angle of
(GATE IN 2009)
a) 30° b) 60° c) 90° d) 120°
- 23) A screening test is carried out to detect a certain disease. It is found that 12% of the positive reports and 15% of the negative reports are incorrect. Assuming that the probability of a person getting a positive report is 0.01, the probability that a person tested gets an incorrect report is
(GATE IN 2009)
a) 0.0027 b) 0.0173 c) 0.1497 d) 0.2100
- 24) One of the roots of the equation $x^3 = j$, where j is the positive square root of -1 , is
(GATE IN 2009)
a) j b) $\frac{\sqrt{3}}{2} + j\frac{1}{2}$ c) $\frac{\sqrt{3}}{2} - j\frac{1}{2}$ d) $-\frac{\sqrt{3}}{2} - j\frac{1}{2}$
- 25) The differential equation $\frac{dx}{dt} = \frac{4-x}{\tau}$ with $x(0) = 0$, and the constant $\tau > 0$, is to be numerically integrated using the forward Euler method with a constant integration time step T . The maximum value of T such that the numerical solution of x converges is
(GATE IN 2009)
a) $\tau/4$ b) $\tau/2$ c) τ d) 2τ
- 26) A quantity x is calculated by using the formula
 $x = (p - q)/r$,
The measured values are $p = 9$, $q = 6$, $r = 0.5$.
Assume that the measurement errors in p, q and r are independent. The absolute maximum error in the measurement of each of the three quantities is ϵ . The absolute maximum error in the calculated value of x is
(GATE IN 2009)
a) ϵ b) 2ϵ c) 3ϵ d) 16ϵ
- 27) The response of a first order measurement system to a unit step input is $1 - e^{-0.5t}$, where t is in seconds. A ramp of 0.1 units per second is given as the input to this system. The error in the measured value after transients have died down is
(GATE IN 2009)

- a) 0.02 units b) 0.1 units c) 0.2 units d) 1 unit

28) The source network S is connected to the load network L as shown by dashed lines (in Fig. 6). The power transferred from S to L would be maximum when R_L is

(GATE IN 2009)

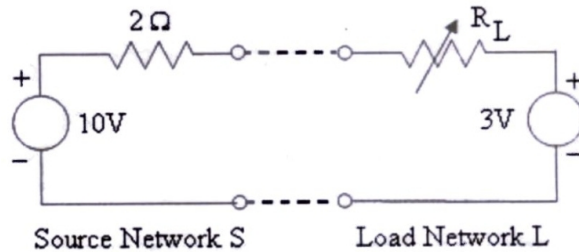


Fig. 6. Circuit Diagram

- a) 0Ω b) 0.6Ω c) 0.8Ω d) 2Ω

29) A stroboscopic system is used for measuring the speed of a rotating shaft. The shaft has one target mark on it. The maximum strobe rate at which synchronism is achieved is r_1 flashes per minute. The next lower flash rate at which synchronism is achieved is r_2 flashes per minute. The speed of the shaft in rpm is:

(GATE IN 2009)

- a) $\frac{r_1 r_2}{r_1 - r_2}$ b) $\frac{r_1 r_2}{r_1 + r_2}$ c) $\frac{r_2^2}{r_1 + r_2}$ d) $\frac{r_1^2}{r_1 + r_2}$

30) Fig. 7 shows the cross-sectional diagram of an orifice flow meter with an orifice radius R . Point 'a' is $30R$ upstream while points 'b' and 'c' are $0.8R$ and $30R$ downstream from the orifice respectively. The pressures at points a, b and c are P_a , P_b and P_c respectively. Then

(GATE IN 2009)

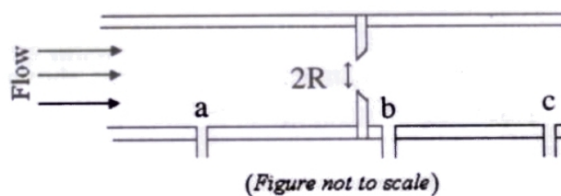


Fig. 7. Cross-sectional Diagram of an orifice flow meter

- a) $P_c > P_b > P_a$ c) $P_a > P_b > P_c$
b) $P_b > P_c > P_a$ d) $P_a > P_c > P_b$

31) The values of the material constant β for the thermistors P and Q are 4000K and 3000K, respectively. The resistance of each thermistor at 298K is $2k\Omega$. At 373K, the ratio of the resistance of thermistor P to that of thermistor Q will be closest to

(GATE IN 2009)

<u>Address</u>	<u>Instruction Code</u>	<u>Mnemonic</u>
1000H	3E 06	MVI A, 06H
1002H	C6 70	ADI 70H
1004H	32 07 10	STA 1007H
1007H	AF	XRA A
1008H	76	HLT

When this program halts, the accumulator contains

(GATE IN 2009)

- a) 00H b) 06H c) 70H d) 76H

- 39) For the input $x(t)$, an ideal impulse sampling system produces the output $y(t) = \sum_{k=-\infty}^{\infty} x(kT) \delta(t - kT)$, where $\delta(t)$ is the Dirac delta function. The system is

(GATE IN 2009)

- a) nonlinear and time invariant
b) nonlinear and time varying
c) linear and time invariant
d) linear and time varying

- 40) The root mean squared value of $x(t) = 3 + 2 \sin(t) \cos(2t)$

(GATE IN 2009)

- a) $\sqrt{3}$ b) $\sqrt{8}$ c) $\sqrt{10}$ d) $\sqrt{11}$

- 41) An analog signal is sampled at 9kHz. The sequence so obtained is filtered by an FIR filter with transfer function $H[z] = 1 - z^{-6}$. One of the analog frequencies for which the magnitude response of the filter is zero is

(GATE IN 2009)

- a) 0.75kHz b) 1kHz c) 1.5kHz d) 2kHz

- 42) The transfer function $H(z)$ of a fourth-order linear phase FIR system is given by $H(z) = (1 + 2z^{-1} + 3z^{-2})G(z)$. Then $G(z)$ is

(GATE IN 2009)

- a) $3 + 2z^{-1} + z^{-2}$ b) $1 + \frac{1}{2}z^{-1} + \frac{1}{3}z^{-2}$ c) $\frac{1}{3} + 2z^{-1} + z^{-2}$ d) $1 + 2z + 3z^2$

- 43) The dc potentiometer shown in the figure has a working current of 10mA with switch S open. Let $R_g + R_1 = 100\Omega$. The galvanometer G can only detect currents greater than $10\mu A$. The maximum percentage error in the measurement of the unknown emf E_x as calculated from the slider position shown in Fig. 13 is closest to

(GATE IN 2009)

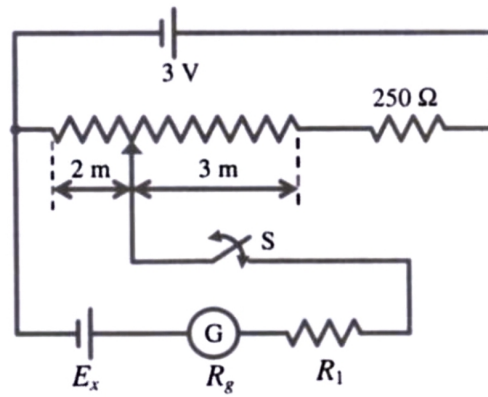


Fig. 13. DC Potentiometer

- a) 0.3 b) 0.5 c) 0.6 d) 1.0

44) A filter is represented by the signal flow graph shown in Fig. 14. Its input is $x(t)$ and output is $y(t)$. The transfer function of the filter is

(GATE IN 2009)

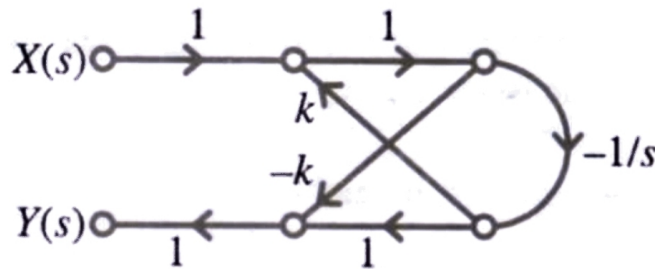


Fig. 14. Signal flow graph

- a) $\frac{-(1+ks)}{(1+k)s}$ c) $\frac{-(1-ks)}{(1-k)s}$
 b) $\frac{s+k}{s+k}$ d) $\frac{s+k}{(1-k)s}$

45) A unity feedback control loop with an open loop transfer function of the form $\frac{K}{s(s+a)}$ has a gain crossover frequency of 1 rad/s and a phase margin of 60° . If an element having a transfer function $\frac{s-\sqrt{3}}{s+\sqrt{3}}$ is inserted into the loop, the phase margin will become

(GATE IN 2009)

- a) 0° b) 30° c) 45° d) 60°

46) A linear time-invariant single-input single-output system has a state space model given by

$$\frac{dx}{dt} = \mathbf{F}x + \mathbf{G}u \quad (1)$$

$$y = \mathbf{H}x \quad (2)$$

where $\mathbf{F} = \begin{pmatrix} 0 & 1 \\ -4 & -2 \end{pmatrix}$; $\mathbf{G} = \begin{pmatrix} 0 \\ 1 \end{pmatrix}$; $\mathbf{H} = \begin{pmatrix} 1 & 0 \end{pmatrix}$.

Here \mathbf{x} is the state vector, u is the input and y is the output.
The damping ratio of the system is

(GATE IN 2009)

- a) 0.25 b) 0.5 c) 1 d) 2

47) A unity feedback system has the transfer function

$$\frac{K(s+b)}{s^2(s+20)}$$

The value of b for which the loci of all the three roots of the closed loop characteristic equation meet at a single point is

(GATE IN 2009)

- a) $\frac{10}{9}$ b) $\frac{20}{9}$ c) $\frac{30}{9}$ d) $\frac{40}{9}$

48) A standard three-lead frontal plane ECG is taken with a normal heart. The peak amplitude of the R-wave is

(GATE IN 2009)

- a) greatest in lead I
b) greatest in lead II
c) greatest in lead III
d) equal in all the leads

49) The operating voltage of an X-ray tube is changed from 40kV to 50kV. The resulting change in the shortest wavelength generated is

(GATE IN 2009)

- a) +20% b) -20% c) +25% d) -36%

50) In a pulsed ultrasound imaging system, a single 5MHz crystal is used both as source and as detector. Bursts of at least 20 cycles are needed for acceptable image quality. The velocity of sound in the tissue being imaged is 1500m/s. The minimum distance of the objects to be imaged should be

(GATE IN 2009)

- a) 12mm b) 6mm c) 3mm d) 1mm

COMMON DATA QUESTIONS

Common Data for Questions 51 to 52

Fig. 15 shows a sample-and-hold circuit using a MOSFET as a switch. The threshold voltage of the MOSFET is +2V. It has zero leakage current in the off state. Assume that the capacitor is ideal.

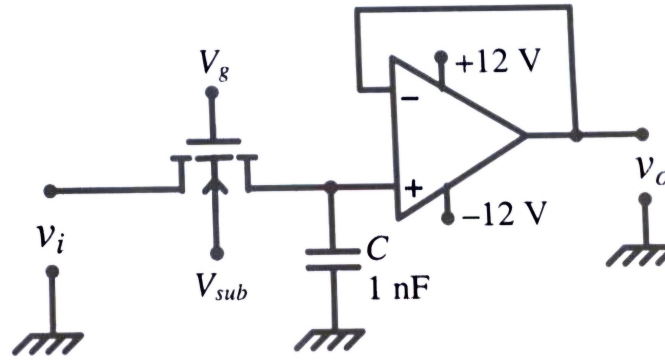


Fig. 15. Sample-and-Hold Circuit

51) The input voltage v_i ranges from -5V to $+5\text{V}$. Appropriate values of V_{sub} , of V_g during sampling, and of V_g during hold are, respectively

(GATE IN 2009)

- | | |
|--|--|
| a) $+12\text{V}$, $\geq +7\text{V}$, and $\leq -3\text{V}$ | c) $+12\text{V}$, $\geq +3\text{V}$, and $\leq -7\text{V}$ |
| b) -12V , $\geq +3\text{V}$, and $\leq -7\text{V}$ | d) -12V , $\geq +7\text{V}$, and $\leq -3\text{V}$ |

52) The circuit is used at a sampling rate of 1kHz , with an A/D converter having a conversion time of $200\mu\text{s}$. The op amp has an input bias current of 10nA . The maximum hold error is

(GATE IN 2009)

- | | | | |
|-----------------|-----------------|-----------------|------------------|
| a) 1mV | b) 2mV | c) 5mV | d) 10mV |
|-----------------|-----------------|-----------------|------------------|

Common Data for Questions 53 and 54:

The circuit shown in Fig. 16 uses three identical transistors with $V_{BE} = 0.7\text{V}$ and $\beta = 100$. Given $R_1 = R_2 = R_3 = 1\text{k}\Omega$, $kT/q_e = 25\text{mV}$. The collector current of transistor Q_3 is 2mA .

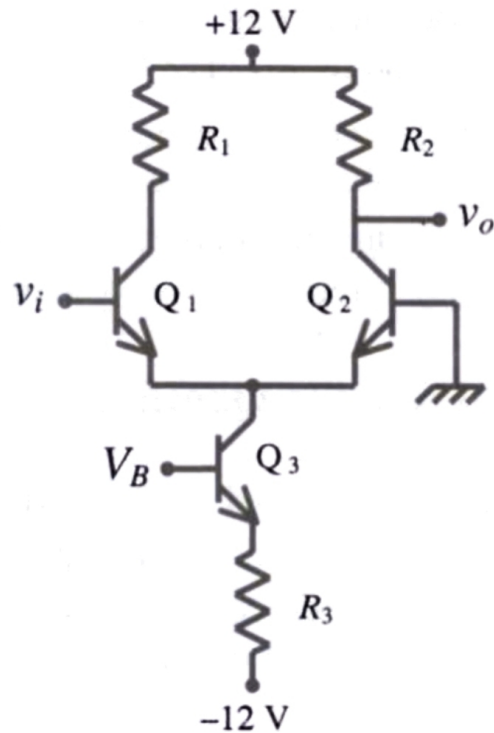


Fig. 16. Circuit Diagram

53) The bias voltage V_B at the base of the transistor Q_3 is approximately

(GATE IN 2009)

- a) $-9.3V$ b) $-10V$ c) $-10.3V$ d) $-11.0V$

54) The small-signal voltage gain of the circuit is

(GATE IN 2009)

- a) 20 c) 20
b) -40 d) 40

Common Data for Questions 55 and 56:

Fig. 17 shows an arrangement for measuring small angular displacements in a vertical plane. A non-conducting tube of length $2l$ and rectangular cross section (width w , height d) is bent along an arc of a circle with radius $R \gg d$ centered at P. Four electrode plates of length l and width w are placed to form two curved parallel plate capacitors C_1 and C_2 with a negligible gap between them. The tube contains water with an air bubble of rectangular cross section (width w , height d) and length $l/4$. The capacitors are connected in a bridge circuit as shown in the figure, where the bridge has ac excitation v_i . Angular displacement $\Delta\theta$ occurs about the point P.

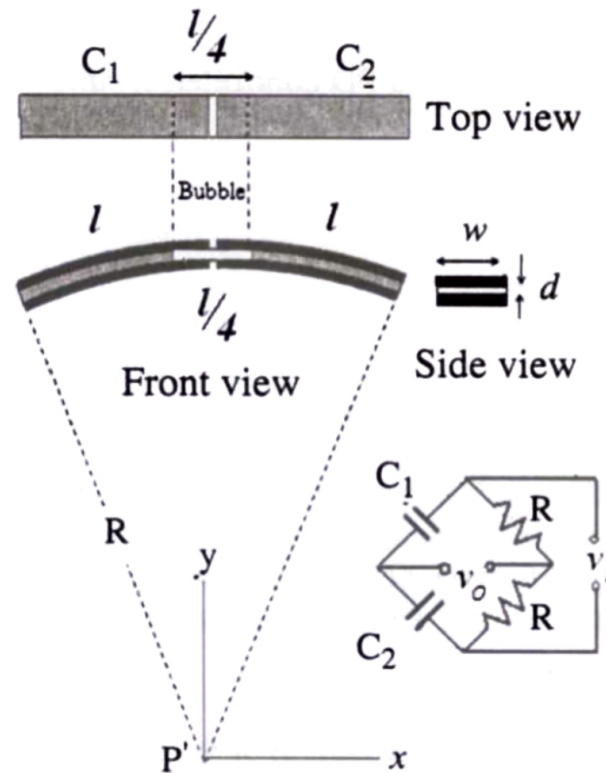


Fig. 17. Setup for measuring small displacements in vertical plane

55) The range of angular displacement (in radians) this system can measure is

(GATE IN 2009)

- a) $-\frac{l}{8R}$ to $+\frac{l}{8R}$ c) $-\frac{3l}{4R}$ to $+\frac{l}{4R}$
 b) $-\frac{l}{4R}$ to $+\frac{l}{4R}$ d) $-\frac{l}{R}$ to $+\frac{l}{R}$

56) The sensitivity $\frac{v_o/v_i}{\Delta\theta}$ is

(GATE IN 2009)

- a) inversely proportional to R and l
 b) inversely proportional to R and directly proportional to l
 c) directly proportional to R and l
 d) directly proportional to R inversely proportional and l

LINKED ANSWER QUESTIONS

Statement for Linked Answer Questions 57 and 58:

A disturbance input $d(t)$ is injected into the unity feedback control loop shown in Fig. 18. Take the reference input $r(t)$ to be a unit step.

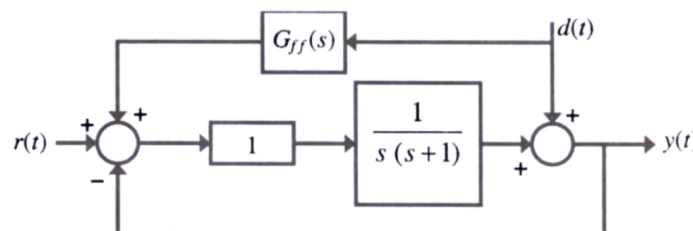


Fig. 18. For Questions 57 and 58

- 57) If the disturbance is measurable its effect on the output can be minimized significantly using a feed-forward controller $G_{ff}(s)$. To eliminate the component of the output due to $d(t) = \sin t$, $G_{ff}(j\omega)|_{\omega=1}$ should be

(GATE IN 2009)

- a) $\frac{1}{\sqrt{2}}\angle -\frac{3\pi}{4}$ b) $\frac{1}{\sqrt{2}}\angle \frac{\pi}{4}$ c) $\sqrt{2}\angle \pi$ d) $\sqrt{2}\angle -\frac{\pi}{4}$

- 58) Let $G_{ff}(s)$ be a PD controller. If $d(t) = \sin 2t$, the amplitude of the frequency component of $y(t)$ due to $d(t)$

(GATE IN 2009)

- a) $\sqrt{\frac{5}{13}}$ b) $\sqrt{\frac{9}{13}}$ c) $\sqrt{\frac{17}{13}}$ d) $\sqrt{\frac{20}{13}}$

Statement for Linked Answer Question 59 and 60:

A Michelson interferometer illuminated with a source of central wavelength λ_0 and spectral width $\Delta\lambda$ is adjusted for equal path difference for the beams returning from the two mirrors. When one of the mirrors is moved by a distance of 0.1mm from this position, 300 fringes move past the field of view. When the mirror is moved further, the fringes completely disappear when the mirror is approximately 4cm from the initial position.

- 59) The central wavelength of the source is

(GATE IN 2009)

- a) 540nm b) 632.8nm c) 667nm d) 720nm

- 60) The spectral width of the source $\Delta\lambda$ is approximately

(GATE IN 2009)

- a) 0.0056nm b) 0.0100nm c) 0.0500nm d) 0.1000nm