

A COMPARISON OF DIFFERENT METHODS FOR CALCULATING TANGENT-STIFFNESS MATRICES IN A MASSIVELY PARALLEL COMPUTATIONAL PERIDYNAMICS CODE

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Acknowledgements



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Outline

- Research Objectives
- Derivation of CTSE
- CTSE and finite-difference, subtractive cancellation
- How to produce a tangent-stiffness (Jacobian) matrix
- Study on verification problem in illustrative code
- Scalability study in *Peridigm* [2] M.L. Parks, D.J. Littlewood, J.A. Mitchell, and S.A. Silling

Research Objectives

- To experimentally test the veracity of complex Taylor Series expansion (CTSE), also called complex-step, for computing Jacobian matrices
- Exam CTSE as an alternative to automatic-differentiation (AD) and finite-difference probing methods for tangent-stiffness (TS) calculation
- To profile the performance in context of Jacobian calculation methods specifically in a production scale, parallelized, code

Derivation of CTSE

Taylor expand in the complex plane

$$f(\beta_n + ih) = f(\beta_n) + \frac{\partial f(\beta_n)}{\partial \beta_n} \frac{ih}{1!} + \frac{\partial^2 f(\beta_n)}{\partial \beta_n^2} \frac{(ih)^2}{2!} + \frac{\partial^3 f(\beta_n)}{\partial \beta_n^3} \frac{(ih)^3}{3!} + \dots$$

Taking the imaginary part of both sides and solving for the first derivative...

$$\frac{\partial f(\beta_n)}{\partial \beta_n} \approx \frac{\text{Im}(f(\beta_n + ih))}{h}$$

Derivation example adapted from work by John Foster and Eric Breseno based upon: Squire and Trapp [3]



Analytical derivative example

Find the derivative of the cosine function...

$$f(x) = \cos(x)$$

Perturb along the imaginary axis

$$f(x + ih) = \cos(x + ih)$$

Trig expand

$$f(x + ih) = \cos(x) \cosh(h) - i \sin(x) \sinh(h)$$

Take imaginary part, divide by h...

Analytical derivative example (contd.)

Apply the previously defined approximation.

$$\frac{\partial f(x)}{\partial x} = -\frac{\sin(x) \sinh(h)}{h}$$

Let $h \rightarrow 0$

$$\frac{\partial f(x)}{\partial x} = \lim_{h \rightarrow 0} -\frac{\sin(x) \sinh(h)}{h}$$

Apply L'Hôpital's Rule

$$\frac{\partial f(x)}{\partial x} = \lim_{h \rightarrow 0} -\frac{\sin(x) \cosh(h)}{1}$$

Finally...

$$\frac{\partial f(x)}{\partial x} = -\sin(x)$$

CTSE and FD, subtractive cancellation

Any time you subtract two [floating point] numbers [in a computer program] which are almost equal, subtractive cancellation will occur, and the difference will not have as much precision as either of the subtrahend or the minuend.
[4] –

Douglas Wilhelm Harder, Department of Electrical and Computer Engineering, University of Waterloo

Subtractive cancellation [4]:

4 digit mantissa; $x_0 = 3.253$, $F'(x_0) = \mathbf{6.505}$

Forward Difference: $F'(x_0) \approx \frac{F(x_0+h) - F(x_0)}{h}$

$$\begin{aligned} F(x) &= x^{2.0} \\ \frac{3.255^{2.0} - 3.253^{2.0}}{.002} &= \\ \frac{10.60 - 10.58}{.002} &= \mathbf{10} \\ 10 &\neq 6.505 \end{aligned}$$



32-bit floating point, 7 digit mantissa; $x_0 = 1.5, F'(x_0) = 3.62203$

$$1 : CD : F'(x_0) \approx \frac{F(x_0+h) - F(x_0-h)}{2h}$$

$$2 : CTSE : F'(x_0) \approx \frac{Im(F(x_0+ih))}{h}$$

$$3 : F(x) = \frac{e^x}{\sin(x)^3 + \cos(x)^3}$$

stepsize : h

h	Equation 1	Equation 2
.1000000E-01	0.362298E+01	0.362109E+01
.1000000E-02	0.362229E+01	0.362202E+01
.1000000E-03	0.362158E+01	0.362203E+01
.1000000E-04	0.360012E+01	0.362203E+01
.1000000E-05	0.357628E+01	0.362203E+01
.1000000E-06	0.476837E+01	0.362203E+01
.1000000E-07	0.000000E+00	0.362203E+01
.1000000E-08	0.000000E+00	0.362203E+01
.1000000E-09	0.000000E+00	0.362203E+01
.1000000E-10	0.000000E+00	0.362203E+01

Example from: Squire and Trapp [3]

CTSE resists subtractive cancellation

The how is simple:

-no difference is taken as in finite-differencing

$$1 : CD : F'(x_0) \approx \frac{F(x_0+h) - F(x_0-h)}{2h}$$

$$2 : CTSE : F'(x_0) \approx \frac{\text{Im}(F(x_0+ih))}{h}$$

How to produce a tangent-stiffness (Jacobian) matrix

$$\text{Analytical: } K_{ij} = \frac{\delta F_i^{int}(x)}{\delta x_j}$$

$$\text{FD: } K_{ij} = \frac{F_i^{int}(x+he_j) - F_i^{int}(x)}{h}$$

$$\text{CD: } K_{ij} = \frac{F_i^{int}(x+he_j) - F_i^{int}(x-he_j)}{2h}$$

$$\text{CTSE: } K_{ij} = \text{Im}\left(\frac{F_i^{int}(x+he_j^{imaginary})}{h}\right)$$

* 'int' signifies derivative of internal force WRT displacement

How the Jacobian is used to solve a force equilibrium problem: algorithm of illustrative code

Inputs: Function pointer for model evaluation, solver parameters

1) Setup:

- a) Define residual
- b) Define convergence criteria

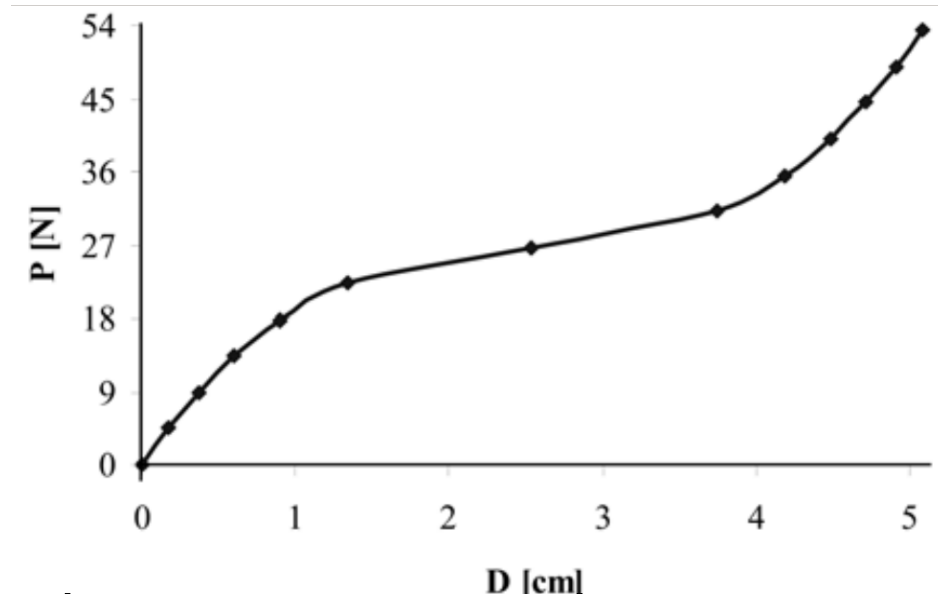
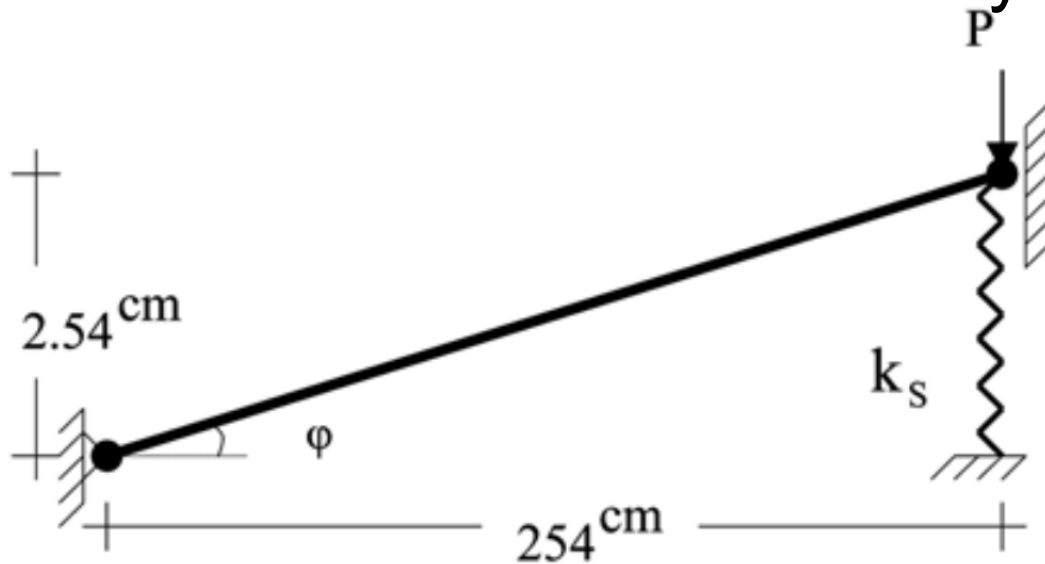
2) Main loop:

- a) Guess equilibrium solution
- b) Compute Jacobian
- c) Compute Newton update using LAPACK GETRF for LU factorization and LAPACK GETRS to solve.
- d) Compute change in residual
- e) Evaluate convergence criteria

3) Report last configuration and performance data

4) Finish or choose another target as for a subsequent load-step

Case study: verification



- Illustrative code implemented with data structures and wrappers from *Trilinos* library [5]

- Serves double duty as simple example implementation of each method, relative to *Peridigm* code

- Verification problem taken from Rezaiee Pajand, M., Alamatian, J. [6] and results reproduced for each method

Case study: verification: problem setup

$$f(D) = 0.5AE(\cos^2 \varphi) \left(\frac{D}{L_0} \right)^2 \left[\frac{D}{L_0} \cos^2 \varphi - 3 \sin \varphi \right] + k_s D + \left(AE \frac{D}{L_0} \right) \sin^2 \varphi$$

$$S_T = 1.5AE(\cos^2 \varphi) \left[\frac{D}{L_0} \cos^2 \varphi - 2 \sin \varphi \right] \left(\frac{D}{L_0} \right) + k_s + \frac{AE \sin^2 \varphi}{L_0}$$

- Force function and analytical Jacobian given
- Apply force boundary condition in 12 load steps, each an Increment of 4.448 N, vary step-size h to measure accuracy response
- Verification is suggested when using a method results in minimum discrepancy wrt 'analytical' solution



Case study: verification: results

Displacement, D, after load-step 12				
Step exponent	Actual cm	AD cm	CS cm	FD cm
0	5.07996	"	"	"
-4	5.07996	"	"	"
-8	5.07996	"	"	"
-12	5.07996	"	"	"
-16	5.07996	"	"	failed
-20	5.07996	"	"	failed

Case study: convergence rate

- Same problem and code as before, now measuring number of iterations taken, not quality of solution
- Step-size is varied to measure effect on convergence rate
- Ideal convergence rate is supposed as the number of iterations the 'analytical' solution method takes.
- Study meant to give context to *Peridigm* iteration speed results, informally



Case study: convergence rate: results

Displacement, D, after load-step 12				
Step exponent	Actual cm	AD cm	CS cm	FD cm
0	63	"	213	417
-4	63	"	"	"
-8	63	"	"	"
-12	63	"	"	65
-16	63	"	"	fail
-20	63	"	"	fail

Implementing CTSE in: *Peridigm*



- Change data-types where possible, cast everywhere else
- Modify copied finite difference model evaluation code to follow CTSE formula
- Add logic to select CTSE for use
- Instrument code for performance comparison
- Compare CTSE, CD, FD, AD for a series of test problems each for single-core and multi-core cases

Scope Stats:

- Refactored code:
3137 lines
- Workflow scripts:
2097 lines
- 1 sample CPU load:
2280 hours
($\frac{1}{4}$ yr on 1 core)
- Simulations:
36 completed



Representative modification: calculating the displacement of a node

-All finite difference methods

```
X_dx = XP[0]-X[0];
X_dy = XP[1]-X[1];
X_dz = XP[2]-X[2];
zeta = sqrt(X_dx*X_dx+X_dy*X_dy+X_dz*X_dz);
Y_dx = YP[0]-Y[0];
Y_dy = YP[1]-Y[1];
Y_dz = YP[2]-Y[2];
dY = sqrt(Y_dx*Y_dx+Y_dy*Y_dy+Y_dz*Y_dz);
```

-CTSE: trivially more complicated

```
X_dx = XP[0]-X[0];
X_dy = XP[1]-X[1];
X_dz = XP[2]-X[2];
zeta = sqrt(X_dx*X_dx+X_dy*X_dy+X_dz*X_dz);

Y_dx = std::complex<double>(YPREAL[0]-YREAL[0], YPIMAGINARY[0]-YIMAGINARY[0]);
Y_dy = std::complex<double>(YPREAL[1]-YREAL[1], YPIMAGINARY[1]-YIMAGINARY[1]);
Y_dz = std::complex<double>(YPREAL[2]-YREAL[2], YPIMAGINARY[2]-YIMAGINARY[2]);
dY = sqrt(Y_dx*Y_dx+Y_dy*Y_dy+Y_dz*Y_dz);
```

Single Core Tests

Mesh Properties:

- Modeled a rectangular prism
- Same object dimensions
- Same number of nodes per family
- Differing horizon, differing number of peridynamic nodes (1000 to 32000 nodes)

Loading Properties:

- Tensile loading in elastic regime
- Same material properties
- Equivalent volume constraints and equivalent load steps

Notes on Operation:

- Each Jacobian calculation method uses same displacement guess
- Speed, accuracy and efficiency are compared between AD, FD, CD and CTSE



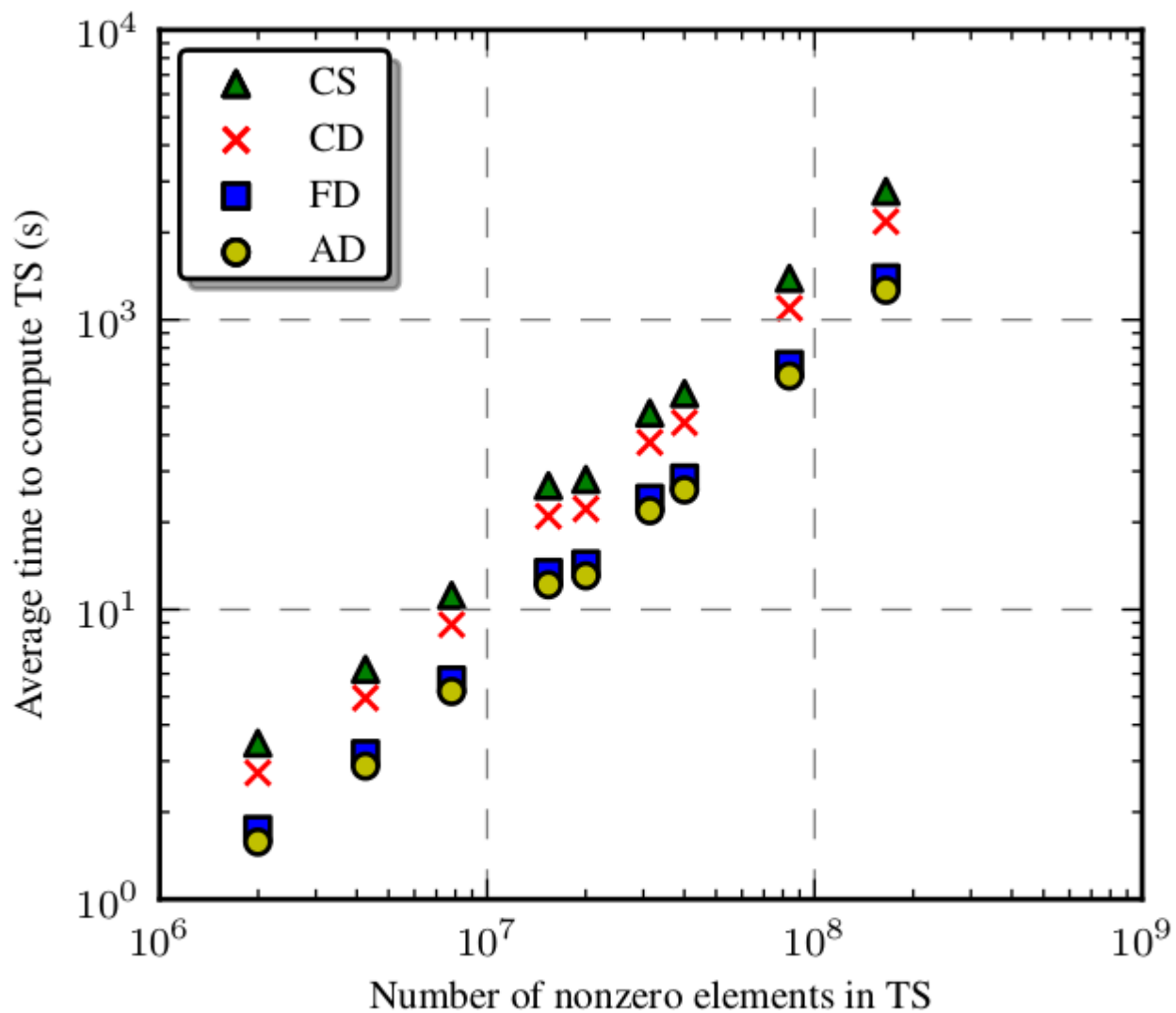


Figure 3.1: Serial test series speed measurements.

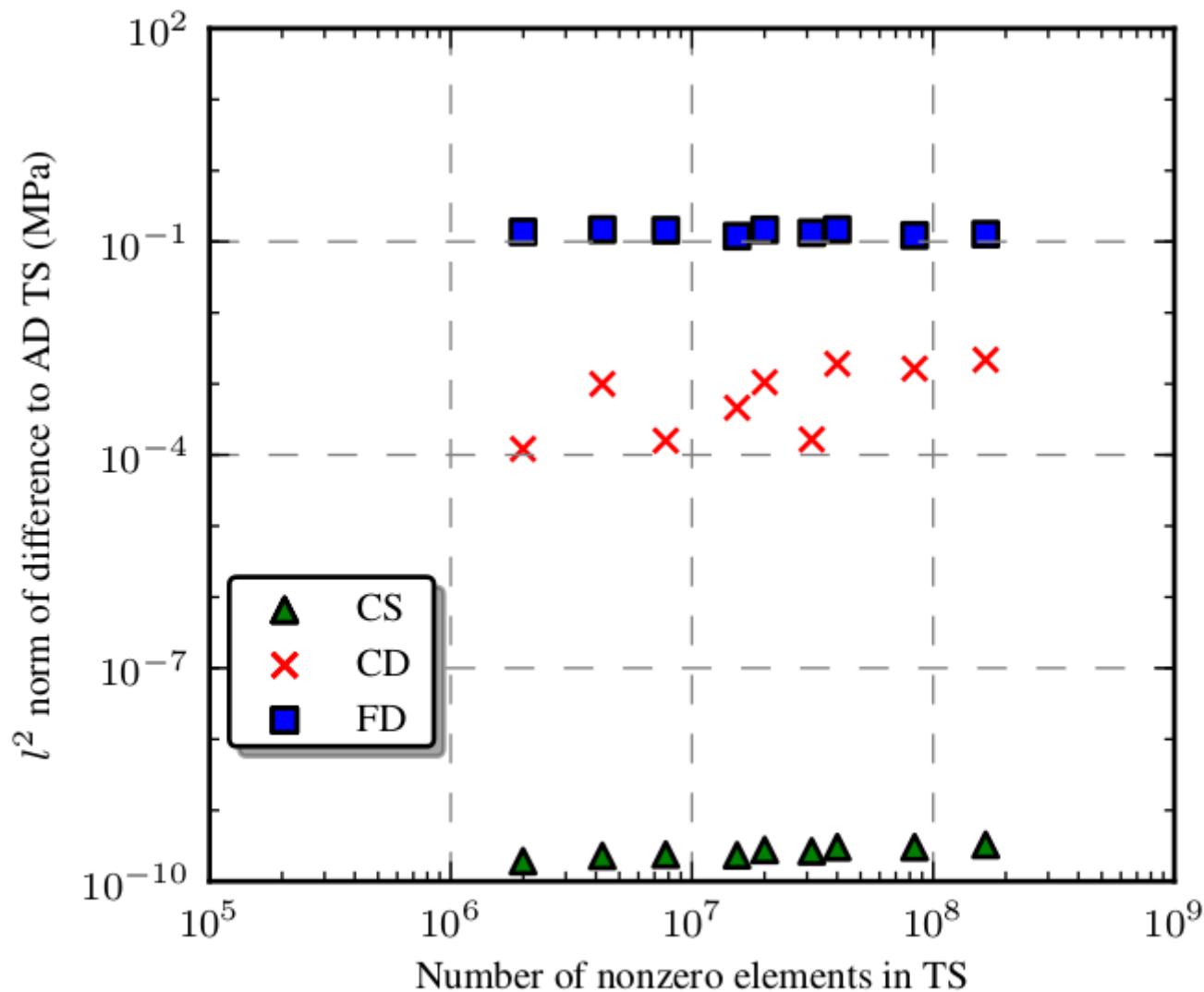


Figure 3.3: Serial test series accuracy measurements.

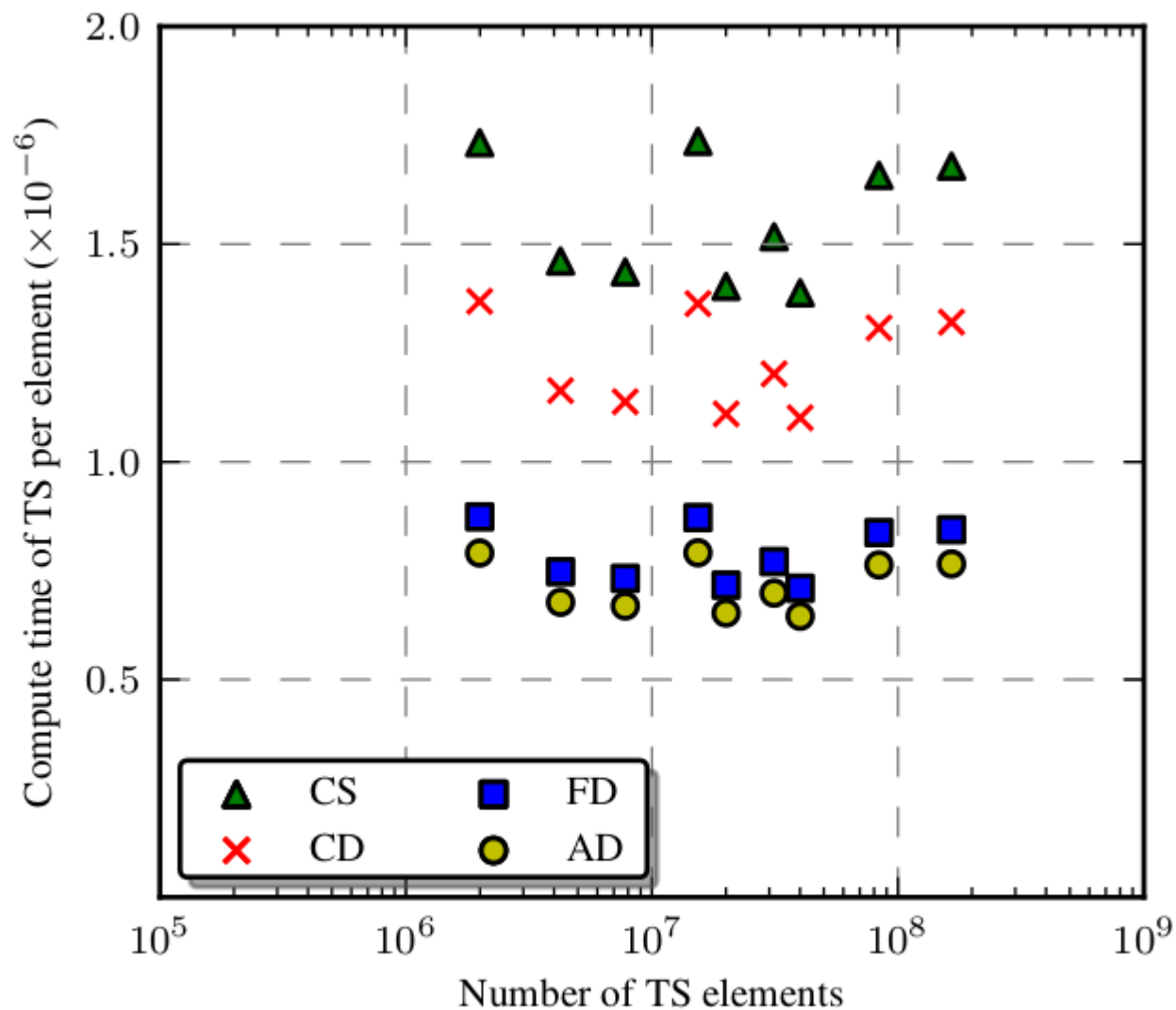


Figure 3.5: Serial test series efficiency measurements.

Multi-core Tests

Mesh Properties:

- Modeled a rectangular prism
- Same object dimensions
- Same horizon, same number of peridynamic nodes (3 million dof)

Loading Properties:

- Tensile loading in elastic regime
- Same material properties
- Equivalent volume constraints, equivalent load steps

Notes on Operation:

- Each Jacobian calculation method uses same displacement guess
- Differing number of cores (32 to 128) used to solve problem, with mesh decomposition differing
- Speed, accuracy and efficiency are compared between AD, FD, CD and CTSE



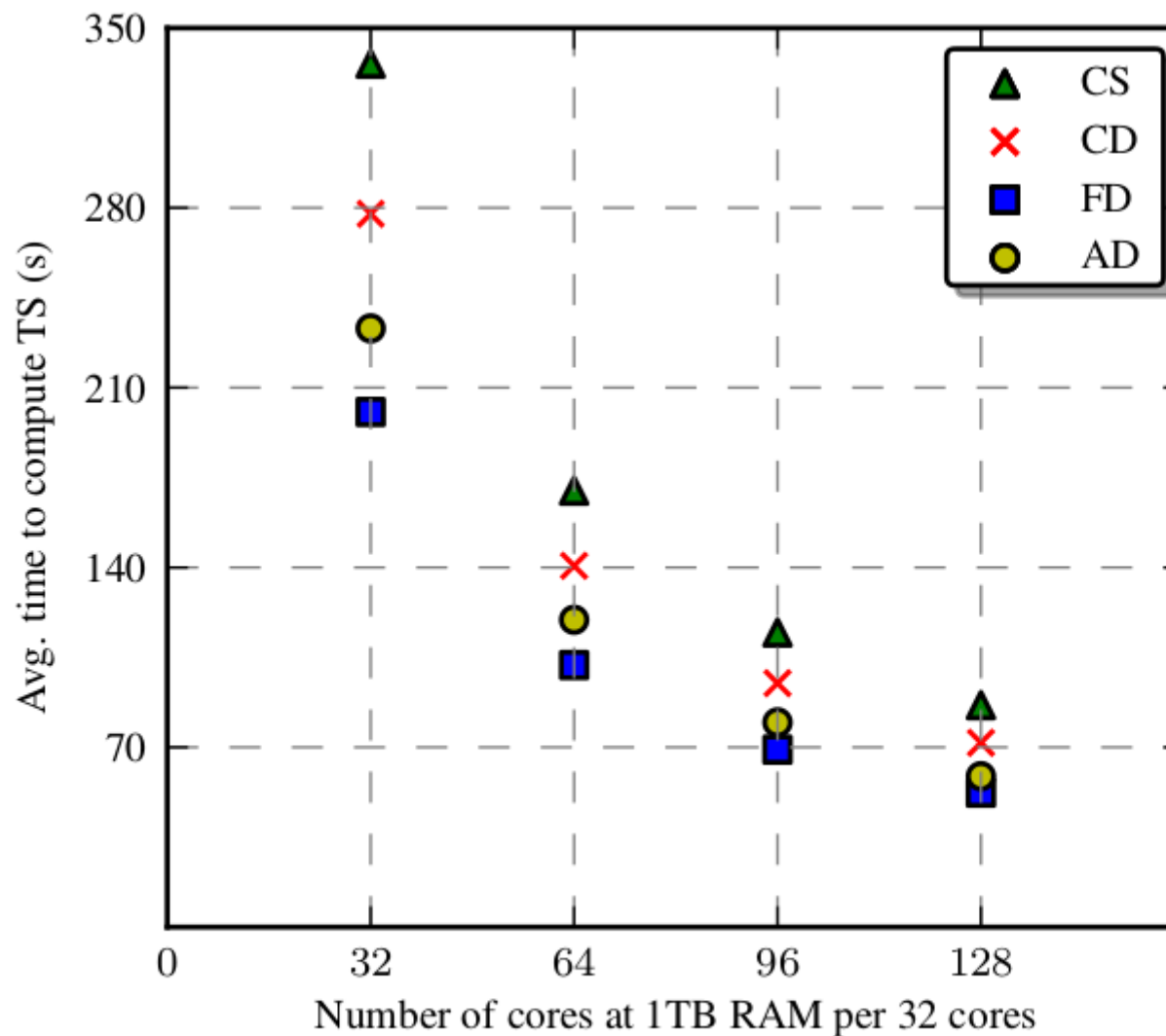


Figure 3.2: Multicore test series speed measurements.

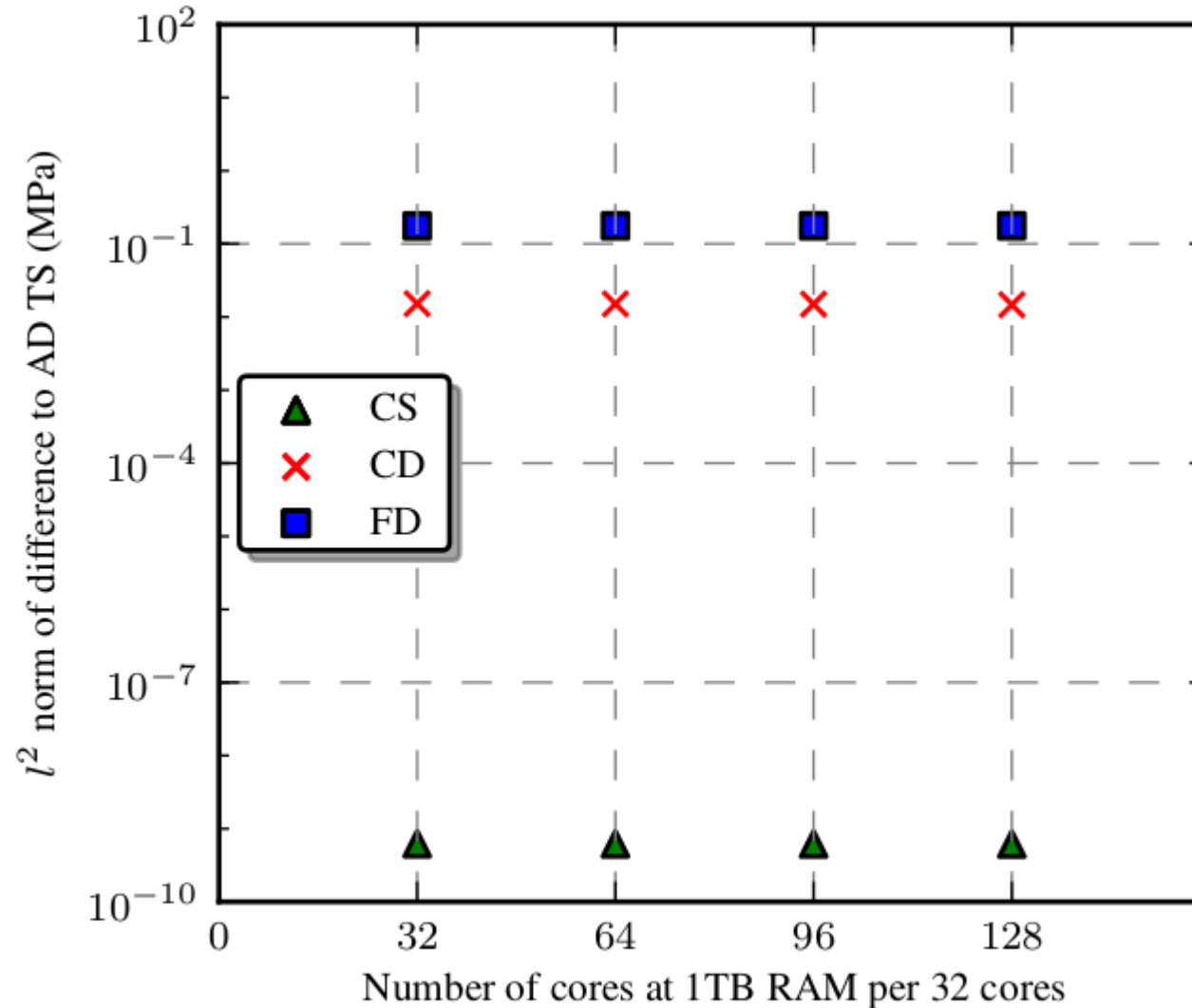


Figure 3.4: Multicore test series accuracy measurements.

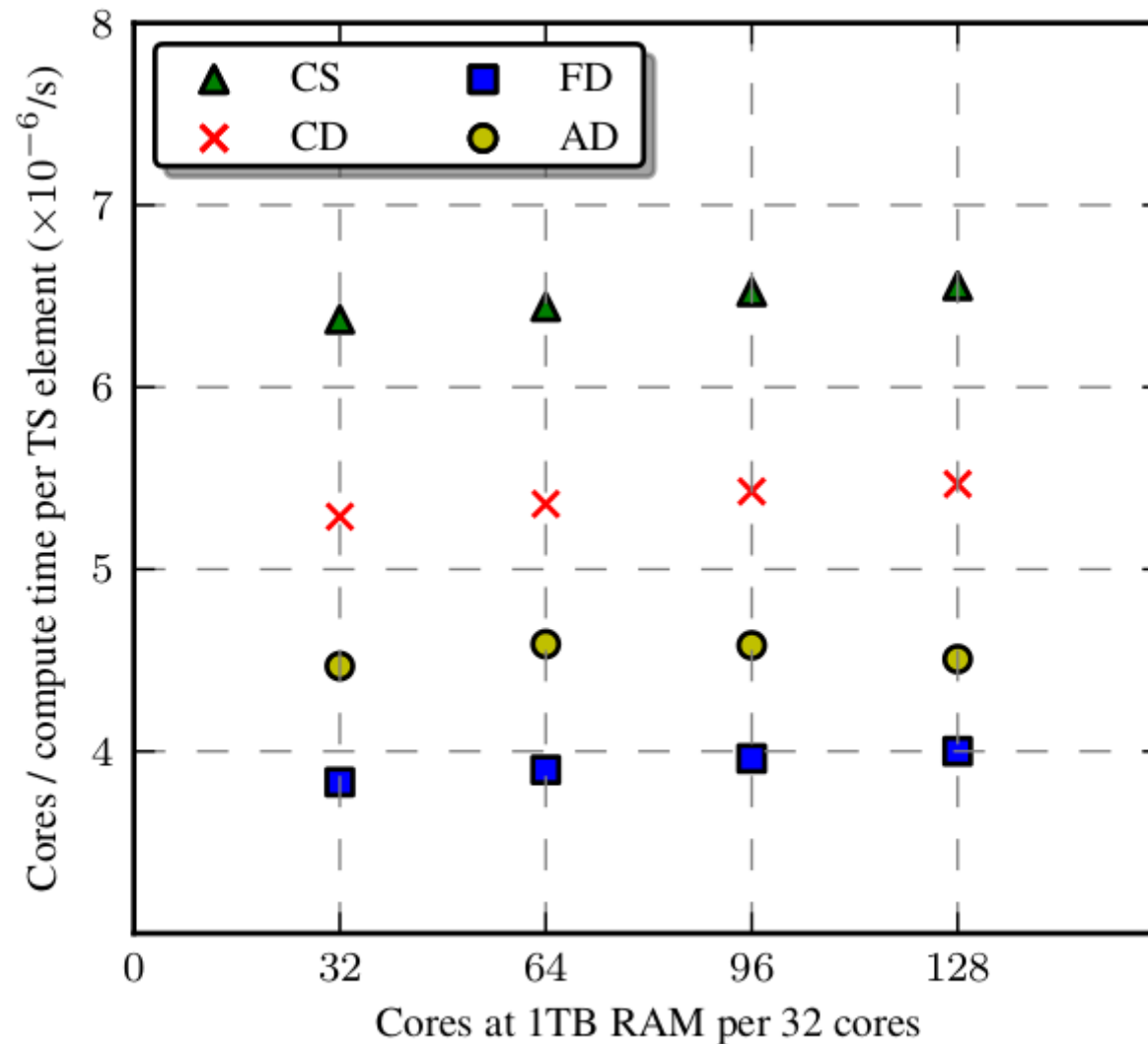


Figure 3.6: Multicore test series efficiency measurements.

Conclusions

Numeric benefits of CTSE:

- high accuracy Jacobians
- resists subtractive cancellation
- fast convergence rate

Practical, but abstract benefits of CTSE:

- requires fewer external libraries than AD does
- native, byte-copyable data-types
- easier for programmer to understand than AD

Drawbacks of CTSE:

- requires complex data-type
- slow iteration speed in a normal implementation



References

[1] Voorhees, Andrew, Harry Millwater, and Ronald Bagley. "Complex Variable Methods for Shape Sensitivity of Finite Element Models." *Finite Elements in Analysis and Design* 47 (2011): 1146-156. Print.

[2] M.L. Parks, D.J. Littlewood, J.A. Mitchell, and S.A. Silling, *Peridigm Users' Guide*, Tech. Report SAND2012-7800, Sandia National Laboratories, 2012.

[3] Squire, William, and George Trapp. "Using Complex Variables to Estimate Derivatives of Real Functions." *SIAM Review* 40.1 (1998): 110. Print.

[4] Harder, Douglas W. "Numerical Analysis for Engineering." *Weaknesses with Floating-point Numbers*. Department of Electrical and Computer Engineering: University of Waterloo, n.d. Web. 18 June 2013.

References

- [5] Heroux, M., Bartlett, R., Howle, V., Hoekstra, R., Hu, J., Kolda, T., Lehoucq, R., Long, K., Pawlowski, R., Phipps, E., Salinger, A., Thornquist, H., Tuminaro, R., Willenbring, J., Williams, A., Stanley, K.: An overview of the trilinos project. ACM Trans. Math. Softw. 31(3), 397–423 (2005). DOI <http://doi.acm.org/10.1145/1089014.108902>
- [6] Rezaiee Pajand, M., ALAMATIAN, J.: The dynamic relaxation method using new formulation for fictitious mass and damping. Structural Engineering and Mechanics 34 (2010)

Data and experimental materials are available at:
<http://idl.utsa.edu/jtfoster/paper-repositories/>