

1 The dynamic behavior of squash balls

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5 The behavior of a squash ball constitutes an excellent case study of the dynamic behavior of rubbery
6 materials. It is shown that the complex viscoelastic behavior of rubber can be investigated using
7 simple drop bounce tests and compression tests. The drop tests show that the coefficient of
8 restitution increases as the ball temperature increases. The compression tests show that as the speed
9 of compression increases or as the ball temperature decreases, the compressive force and the energy
10 loss both increase. These effects are due to the viscoelastic nature of the rubber and are an excellent
11 example of the time-temperature equivalence of polymers. Compression tests were performed on
12 balls with small holes at the base to separate the effects of the internal air pressure from the material
13 deformation. It was found that the internal air pressure contributed about one-third to the
14 compressive force, but contributed little to energy loss. This behavior shows that the rubber material
15 dominates the rebound behavior and that the normal warming up process at the start of a squash
16 game is important to raise the temperature of the rubber rather than to increase the internal air
17 pressure. © 2011 American Association of Physics Teachers.
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19 I. INTRODUCTION

20 The bouncing of a ball is a familiar phenomenon that in-
21 volves complex dynamics and materials behavior. Changes
22 in the physics of the bounce can significantly change the
23 nature of the activity and the chance of injury in many
24 sports. The study of ball bouncing is amenable to simple
25 techniques, is relevant to many students with interests in
26 sports, and involves a range of physics principles that can be
27 explored across a wide educational spectrum.

28 The behavior of squash balls presents an especially inter-
29 esting case due to the nature of their materials and construc-
30 tion. Some balls rely mainly on internal air or gas pressure to
31 provide the dynamic behavior, with tennis balls being the
32 best example. There are good physics lessons here, with balls
33 kept cool before use to minimize gas diffusion, balls being
34 changed after a certain number of games as the internal pres-
35 sure drops, and novel nanocomposite layers in the wall of
36 Wilson double-core balls to reduce diffusion.¹ The behavior
37 of solid balls is determined solely by the ball's material, with
38 examples being baseball, cricket, and field hockey balls.
39 Squash balls are intermediate because they are hollow, but
40 have thick walls and are not internally pressurized. Their
41 behavior is therefore partly controlled by the wall material
42 and partly by the air inside. The rubber used for squash balls
43 also produces interesting changes of the dynamic behavior
44 with temperature, which is the reason that squash balls need
45 to be warmed up before a game starts. It is also possible to
46 use different grades of squash ball (indicated by colored
47 spots), which give different levels of bounce and can be
48 matched to the skill and fitness level of the players.

49 The aim of this paper is to show how the viscoelastic and
50 temperature dependent nature of rubber can be demonstrated
51 using simple experiments. The viscoelastic behavior of rub-
52 ber has applications in tire technology, earthquake protection
53 bearings, vibration damping, and seals (the Challenger Space
54 Shuttle disaster was caused by such behavior). It is a subject
55 in which the structure-property relations of a material can be
56 related from the molecular level (how polymer chain

segments move) to the macrolevel (the mechanical proper- 57
ties) and then to real-world situations. Despite its impor- 58
tance, it is a difficult subject to convey to students. The fol- 59
lowing study presents an interesting, amenable, and 60
alternative way of demonstrating the principles of viscoelas- 61
tic behavior. 62

II. BACKGROUND 63

The most important feature of squash balls is that they 64
have low rebound resilience. The resilience of a material can 65
be thought of as its ability to absorb energy elastically on 66
loading and then to release that energy when the material is 67
unloaded. When a squash ball makes contact with racket 68
strings, a wall, or the floor of a court, some of its energy is 69
stored elastically in the rubber, some in the racket strings, 70
and some in the increased internal air pressure. Some energy 71
will be lost as sound, but more of the energy becomes inter- 72
nal thermal energy in the ball itself. This energy has two 73
effects—the air inside the ball becomes pressurized and the 74
rubber compound from which the ball is made becomes more 75
resilient. As a result, the ball bounces higher. The playing 76
temperature of the squash ball is usually around 45 °C, 77
which is achieved after the ball has been warmed up by the 78
players.² This temperature is where equilibrium is reached, 79
and the thermal energy lost to the strings, walls, floor, and air 80
equals the energy gained from deformation. 81

The rebound resilience is defined as the ratio of the energy 82
remaining in the ball after an impact to the energy before 83
impact. It is related to the coefficient of restitution (COR), 84
which is the ratio of speeds before and after impact. Al- 85
though the rebound resilience is often easier to measure, the 86
COR is more directly relevant to a squash game because it 87
governs the speed of a bounce away from a wall and the 88
floor. A perfectly elastic collision has COR=1 and a rebound 89
resilience of 100%. In this case, the ball bounces and returns 90
to the height at which it was dropped. A perfectly inelastic 91
collision has COR=0, for example, a spherical lump of soft 92
putty. No balls are perfectly elastic, although hard rubber 93
“superballs,” solid metal, and glass marbles bouncing on a 94
rigid and elastic surface come close. 95

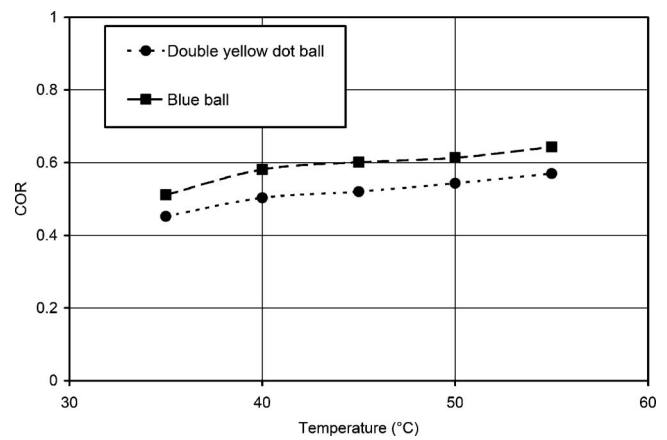


Fig. 1. The temperature dependence of the coefficient of restitution for two types of squash balls.

III. MEASUREMENT OF COEFFICIENT OF RESTITUTION

We used Dunlop international competition double yellow dot balls and Dunlop Max blue balls. The double yellow dot ball is used for competitions and has a low resilience. The Max blue ball has a diameter of 44.8 mm, which is 12% larger than the standard size of 40 mm, has a higher resilience and a 40% longer time between vertical bounces than the double yellow dot, and is designed more for beginners.

The coefficient of restitution of the squash balls was measured using a simple drop test. The collision was between the ball and a wooden squash court floor, creating a testing environment reflecting the nature of the game. The balls were dropped from the viewing balcony of a standard squash court onto the court below (a distance of 3.55 m). A Sony DCR-HC62E video camera operating at 50 frames/s on a rigid tripod was used to record the bounce of the squash ball against a background including a 1 m calibration rule. Six of each type of squash ball were tested at different temperatures achieved by immersion in an electrically powered thermostatic water bath set to various temperatures. The temperature of the ball on impact is somewhat lower due to cooling during the drop, but by dropping balls immediately after removal from the water bath, the cooling is small.

The coefficient of restitution was determined using the relation

$$\text{COR} = \sqrt{\frac{h_2}{h_1}}, \quad (1)$$

where h_1 is the drop height and h_2 is the bounce height. The effects of air resistance were taken into account when calculating the coefficient of restitution from rebound heights using a standard drag coefficient for a sphere and was shown to give about a 3% difference. Although this correction is not described here, such a calculation can be used to demonstrate the use of differential equations and can be solved either analytically or numerically.

The vertical speeds just before impact (about 8.2 m/s) and just after impact were measured from the video images. Although this method is not as precise, the results were in agreement with the coefficient of restitution calculated from rebound heights. Figure 1 shows the results, from which it can be seen that the coefficient of restitution is between 0.45

96 Balls used for all sports exhibit some energy loss due to
 97 damping. Several models have been developed for the be-
 98 havior of balls, which most commonly use combinations of
 99 masses, springs, and dampers to account for energy losses.
 100 These models can account reasonably well for the change in
 101 behavior with speed,^{3,6} but have not been used to deal with
 102 the effects of changes in temperature.
 103 The most common ways of assessing the properties of
 104 balls are to measure the coefficient of restitution and the
 105 force required to compress the ball. Measurements of the
 106 coefficient of restitution are most commonly made by drop-
 107 ping balls onto hard rigid surfaces and measuring the height
 108 of rebound.^{7,8} This height can then be converted into the
 109 speed ratio. Drop tests only give fairly low impact speeds,
 110 which means that measurements at higher speeds require
 111 more advanced measurement systems such as high speed
 112 video photography.⁶ The measurement of the coefficient of
 113 restitution is relevant to the impact speed seen during play,
 114 although in squash, a range of speeds are seen, from the high
 115 speed rebound of a hard shot into the wall compared to a
 116 gentle drop-shot against the wall and then onto the court
 117 floor.⁹
 118 The other common method is to determine the force re-
 119 quired to compress the ball. The compression behavior is
 120 important because it determines the forces and time scales of
 121 impact. For instance, a more compressible ball will have a
 122 slower impact and lower peak forces, which usually means
 123 lower injury potential. However, more compressible base-
 124 balls have a greater chance of chest injury due to the impact,
 125 which produces resonant vibrations in the chest cavity and
 126 vital organs.¹¹ A study of lacrosse balls found that more com-
 127 pressible balls had a greater chance of passing through face
 128 guards.¹⁰ Although squash balls have less potential for injury,
 129 there is major concern over impacts near the eye socket. For
 130 this reason, the World Squash Federation specifies a maxi-
 131 mum compression stiffness.¹² Compression tests are done at
 132 much lower speeds than that found in an impact.
 133 By continually measuring the force-displacement behav-
 134 ior, the hysteresis of the ball (percentage energy lost during
 135 compression and unloading) can be measured, which can
 136 then be related to the dynamic energy losses measured by the
 137 coefficient of restitution.^{7,8} Ideally, the speed of compression
 138 should match the impact speed, but this ideal is difficult to
 139 achieve. Scarton *et al.*¹¹ developed a dynamic hardness mea-
 140 sure from impact force measurements and claimed that this
 141 measure relates more to injury potential.
 142 The aim of our investigation was to examine the mechan-
 143 ics of two types of squash balls using methods amenable to
 144 most educational institutions. To explore the effects of time
 145 scale and temperature on the energy lost during deformation
 146 of a ball, two test methods were used. Drop tests were used
 147 to study the effects of increasing temperature on the coeffi-
 148 cient of restitution. We also measured the force required to
 149 compress the squash balls as a function of speed and tem-
 150 perature.
 151 Previous research suggests that the elasticity of the rubber
 152 is the determining feature of bounce height rather than the
 153 pressure of the air in the ball.¹³ This suggestion was investi-
 154 gated by compressing balls with small holes to allow free
 155 movement of air in and out of the ball. These results allow us
 156 to make comparisons of ball stiffness and rebound resilience
 157 with the World Squash Federation specifications.¹²

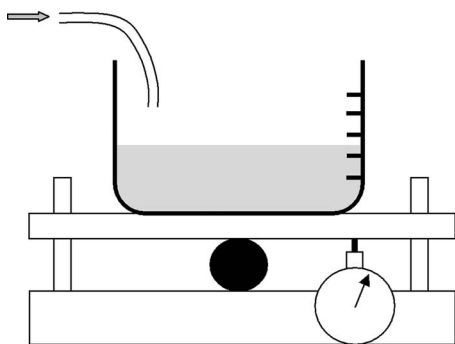


Fig. 2. Simple apparatus for measuring compression and recovery.

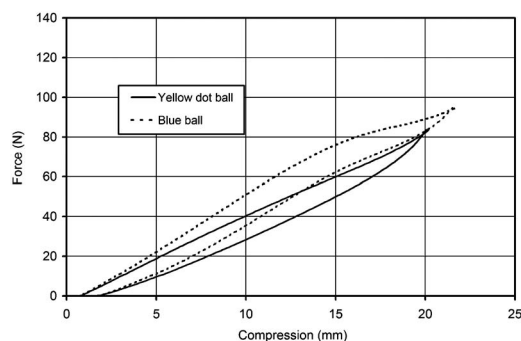


Fig. 4. Force/compression behavior at 100 mm/min for two types of squash balls.

199 and 0.65 (resilience between 20% and 35%), increases with
200 increasing temperature, and is higher for the Max blue balls
201 than for the double yellow dot balls. In a real squash game,
202 the ball speeds could be considerably higher. The World
203 Squash Federation specifications for the double yellow dot
204 ball states that the resilience should be between 26% and
205 33%, as measured in a drop test at 45 °C. Our results give a
206 value of $27.1\% \pm 0.5\%$, which is just inside the lower limit
207 set by the World Squash Federation.

208 IV. COMPRESSION TESTS

209 Compression tests were performed using a Hounsfield
210 25 kN mechanical testing machine with balls compressed
211 between parallel steel plates. The plates were moved together
212 at a constant rate until the deformation reached 20 mm, at
213 which the plates were moved apart at the same rate. The
214 compression rates were 10, 30, 100, 300, and 1000 mm/min.
215 The testing machine includes a load cell above the top com-
216 pression plate. This cell comprises of a stiff bending beam,
217 which is instrumented with strain gauges and allows the
218 force to be recorded continuously during each test. Although
219 this type of equipment is standard to materials testing labo-
220 ratories, not all physics departments have access to this
221 equipment, and a simpler compression apparatus can be con-
222 structed using a water tank for loading and a dial gauge, as
223 shown in Fig. 2. Loading and unloading can be achieved
224 rapidly by filling and emptying tubes, and a video camera
225 can be used to record and then analyze a fast moving dial
226 gauge and the liquid level. The compression to 20 mm was
227 chosen as being half of the ball diameter. This compression

is realistic because the energy of compression to 20 mm is
later shown to be about 1 J, similar to the kinetic energy of
the squash ball in the drop tests.

For each test speed, two balls of each type were each
tested twice. In this way, each ball was tested twice at each
speed and variability from ball to ball could also be assessed.
The first test conducted on a ball gave a higher force than
subsequent tests due to the well-known Mullins effect,
whereby weak bonds formed during manufacture are broken
on the first deformation. Following the first compression,
which was discounted, the results were reproducible, with
standard deviations of the order of 5%. The Mullins effect
was not significant for the drop tests because all balls were
dropped several times before the actual measurements.

Typical force/compression curves are shown in Fig. 3 for
the double yellow dot ball at various test speeds. The two
faster tests shown are offset by 60 and 120 N to show the
behavior clearly on one graph. Figure 3 shows that the force/
compression behavior is not quite linear, with a slight up-
ward curvature. The force on unloading is smaller, giving a
hysteresis loop between loading and unloading. As the test
speed increases, the forces increase and the area of the hys-
teresis loop also increases. Figure 4 shows the force/
compression behavior for the double yellow dot balls and the
Max blue balls, both at a test speed of 100 mm/min. The data
show that the Max blue balls require a slightly higher force
to achieve the same compression, not surprising given their
larger size. There is little difference in the size of the hys-
teresis loops.

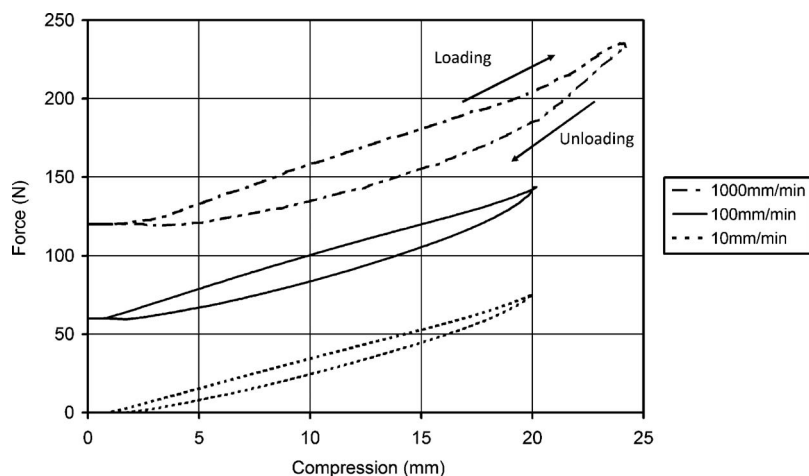


Fig. 3. Force/compression behavior of yellow dot balls at different compression rates.

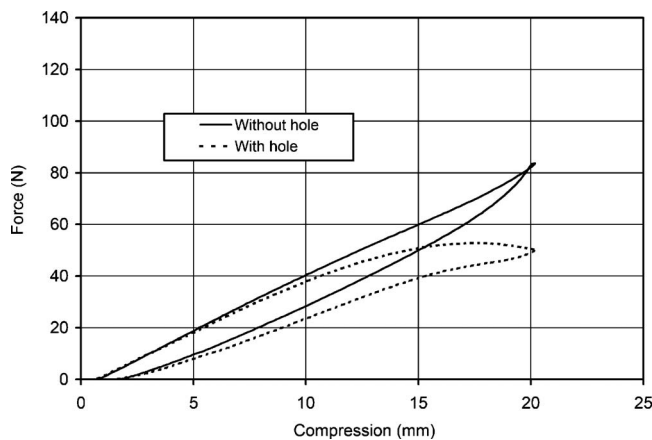


Fig. 5. Force/compression behavior at 100 mm/min for yellow dot balls with and without a hole.

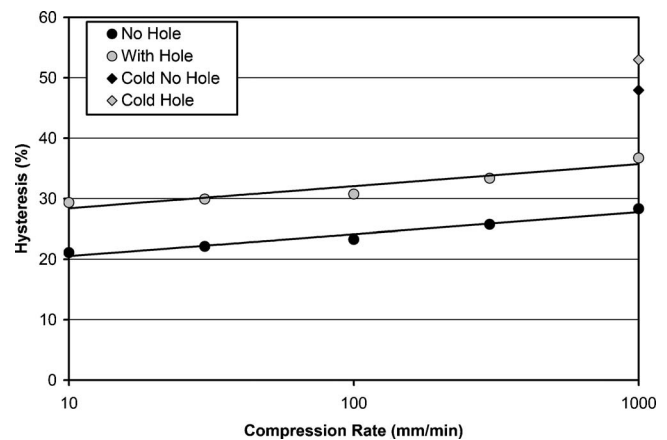


Fig. 7. Variation of hysteresis with rate and temperature for yellow dot balls.

There has long been considerable debate over the relative importance of the rubber and internal air for squash balls.¹² To investigate this importance, compression tests were conducted with squash balls with holes. One small hole of about 3 mm diameter was cut in each ball using a scalpel. The ball was then compressed as described, with the hole carefully positioned at the base of the test so that the effect of the hole on the rubber deformation is minimized. Because the purpose of the hole is to allow free passage of air in and out of the ball, the ball was placed on a steel disk that had a central hole linked to a groove on the base of the disk, thereby allowing free passage of air. The force/compression behavior of the double yellow dot balls with and without holes is shown in Fig. 5. The data show that the initial behavior is almost identical. Only when the compression has reached 15 mm does the hole make a significant difference, causing a decrease in the force. The area of the hysteresis loop is about the same size. Measurements of the area under the loading and unloading curves show that the energy lost by a ball with a hole is only slightly smaller than one without a hole. The force at 20 mm compression is 82 N without a hole, compared to 50 N with a hole, indicating that at this degree of compression about 61% of the compression force of a squash ball arises from rubber deformation, with about 39% arising

from compression of the air inside the ball. More significantly, almost all of the energy lost during a compression comes from deformation of the rubber.

There is a widely held view that the purpose of warming up a squash ball is to achieve more bounce due to the internal air warming and the pressure increasing.² This interpretation is incorrect because it is the rubber that determines almost all of the energy loss, and it is the increase in the rubber temperature that gives a higher bounce.

To demonstrate the effects of deformation speed and temperature on the behavior of squash balls, compression tests were also conducted with cold balls. Although it is possible to use a low temperature chamber around the test machine, such facilities are not that common, and hence a simpler method was used of precooling the balls in a freezer, followed by immediate testing at high speed. Balls were returned to the freezer for at least 1 h between tests. Figure 6 shows the force/compression curves for the double yellow dot balls at 23 and 0 °C, both at a speed of 1000 mm/min. The data show that it takes larger forces to compress the cold ball, and there is also a significantly larger hysteresis loop, which would mean more energy lost during compression and so a lower bounce.

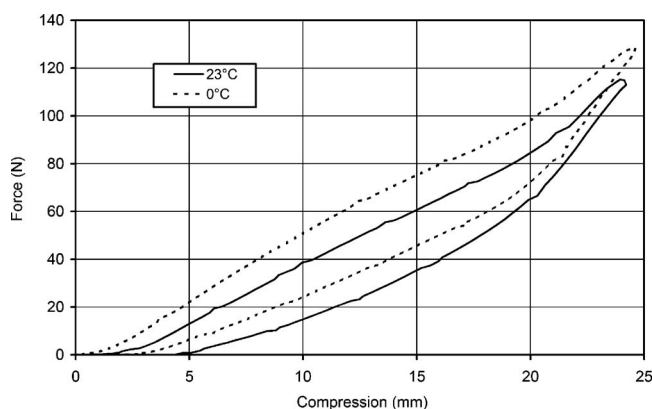


Fig. 6. Force/compression behavior at 1000 mm/min for yellow dot balls at 23 and 0 °C.

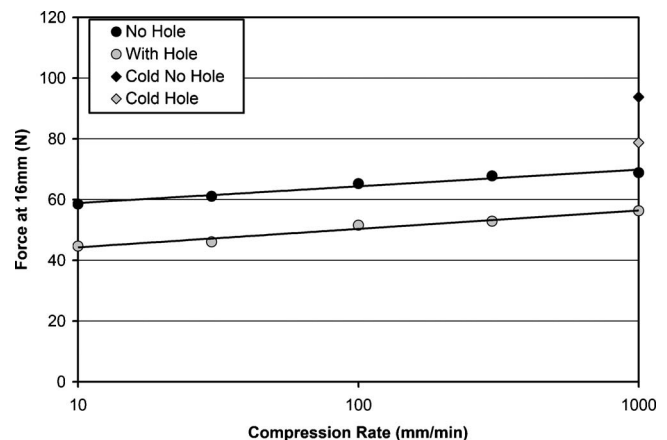


Fig. 8. The variation of force at 16 mm compression with rate and temperature for double yellow dot balls.

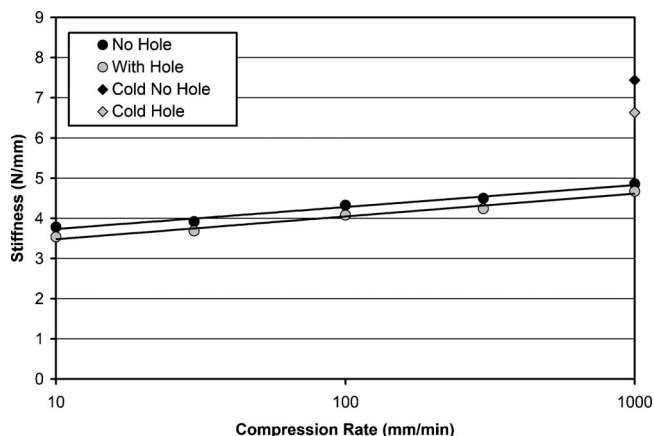


Fig. 9. The variation of stiffness with rate and temperature for double yellow dot balls.

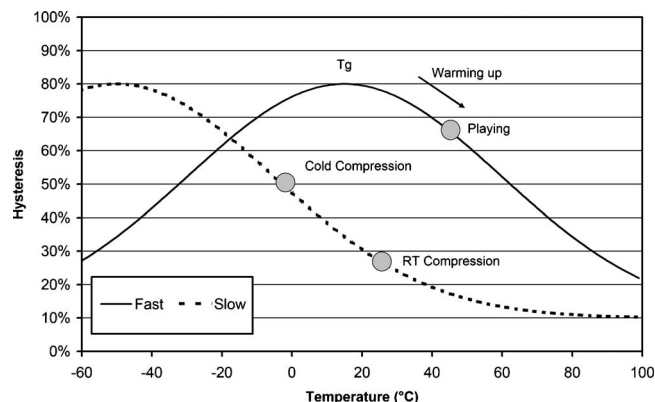


Fig. 10. The effects of temperature and rate on the hysteresis of rubber.

VI. ENERGY LOSS

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By measuring the hysteresis loops of the compression tests and comparing them with the rebound tests, it is possible to investigate the effects of time scale and temperature on the percentage of energy lost during deformation. The coefficient of restitution values were converted to hysteresis as

$$\text{Hysteresis}(\%) = (1 - \text{COR}^2)100. \quad (2)$$

The time scale of the impacts in the bounce tests was estimated by comparing the change in momentum (from the coefficient of restitution results) with a typical average force during impact taken to be 50 N from the compression tests. The average hysteresis values for each test condition are shown in Table I. We see that as the rate of deformation increases, the hysteresis increases, and as the temperature increases, the hysteresis decreases. This dependence is an excellent example of the time-temperature equivalence of the time-dependent (viscoelastic) mechanical behavior of polymers. The mechanical properties arise from the movement of polymer chains. More polymer chain movement occurs with slower compression rates (more time) or at higher temperatures (more mobile chains). This mechanism of deformation leads to the idea that slower compression tests at a low temperature are equivalent to faster compression rates at a higher temperature.

350

Table I. Hysteresis determined from bounce and compression tests. The last two columns are in percent.

Conditions	Deformation time scale (ms)	Hysteresis of double yellow dot balls	Hysteresis of Max blue balls
Bounce at 35 °C	5.5	79.5	73.7
Bounce at 40 °C	6	74.7	66.1
Bounce at 45 °C	6	72.9	63.6
Bounce at 50 °C	6	70.5	62.1
Bounce at 55 °C	6	67.5	58.4
Compression 10 mm/min 23 °C	240,000	21.1	21.4
Compression 30 mm/min 23 °C	80,000	22.1	21.5
Compression 100 mm/min 23 °C	24,000	23.3	22.4
Compression 300 mm/min 23 °C	8,000	25.7	23.6
Compression 1000 mm/min 23 °C	2,400	28.3	25.0
Compression 1000 mm/min 0 °C	2,400	47.9	43.1

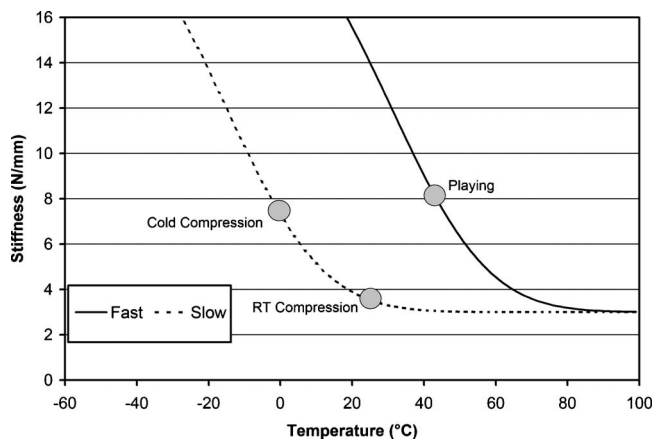


Fig. 11. The effects of temperature and rate on the stiffness of rubber.

to the behavior of a ball during play. This point is more clearly illustrated in Fig. 11, which shows the ball stiffness plotted against temperature for two deformation rates. The stiffness drops dramatically with increasing temperature near T_g and does so at a higher temperature for the faster rate. If the compression tests are used to determine the injury potential of a squash ball, then compression at low temperatures would give a better indication of the stiffness under playing conditions than compression at room temperature, as is currently specified by the World Squash Federation.¹³

VII. COMMENTS

The use of much slower compression tests needs to be treated with caution for predicting squash ball behavior. If such tests are to be used, it is better to use balls cooled to a lower temperature. The use of lower temperatures means the properties are closer to those of much faster rate tests at higher temperatures as found under playing conditions. This understanding suggests that the specifications of the World Squash Federation regarding compression should be modified.

The hysteresis of a polymer is related to its glass-transition temperature T_g , the region where its behavior changes from a hard rigid glassy material (below T_g) to a softer rubbery material (above T_g).¹⁵ Near T_g the stiffness decreases rapidly with temperature, and the hysteresis increases.¹⁵ This behavior occurs because some chain segments are flexible, while some are still more immobile; moving one past another causes energy losses.

Figure 10 shows a schematic of the effect of time scale and temperature on hysteresis for rubber, where T_g (defined as the peak of the curve) is below room temperature. The two curves represent different deformation rates. The faster deformation leads to a T_g that is significantly higher than for the slow rate. The behavior of squash ball rubber is indicated by the gray circles. The playing conditions at 45 °C and fast deformation rates give a large hysteresis. The effects of warming are indicated by the arrow, where increasing temperature leads to a decrease in hysteresis (more bounce). The much slower compression tests are also shown, which explains why the hysteresis is less for the compression tests than for the bounce tests. A more detailed analysis of the results shows that the hysteresis values from the rebound tests are higher than those from the compression tests, even accounting for the effects of loading rate and temperature. The explanation comes from the differences between the two types of tests. In the compression test, the ball is compressed equally on both sides between steel plates at a constant rate. In the rebound test compression is on just one side, onto a slightly compliant wooden floor, and the rate of compression varies through the bounce as the ball slows down and then rebounds. The equivalent curves for the blue balls would be shifted slightly to the left because the different rubber composition has a slightly lower value of T_g .

Figure 10 also shows that if compression tests are to be used to predict the playing behavior of a squash ball, it is better to perform the tests cold as the behavior will be closer

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