# **1:** 30 points

## Uncertainty modeling

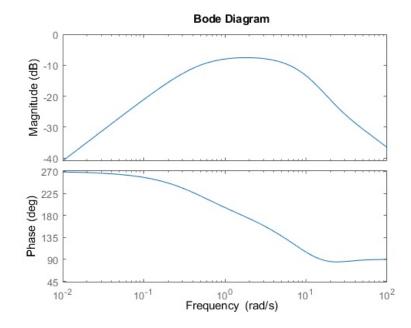
(a) Consider a "true" plant  $G(s) = \frac{3e^{-0.1s}}{(2s+1)(0.1s+1)^2}$ . Derive and plot the additive uncertainty weight when the nominal model is  $G(s) = \frac{3}{2s+1}$ .

$$G = G_N + W_{\alpha}(s) \Delta$$

$$W_{\alpha}(s) \Delta = G - G_N$$

$$W_{\alpha} = \frac{3(e^{-0.1s} - (0.1s + 1)^2)}{(2s+1)(0.1s+1)^2}$$

```
%Problem 1a
s = tf('s');
G_true = 3*exp(-0.1*s)/(2*s+1)/(0.1*s+1)^2;
G_n = 3/(2*s+1);
W_a = G_true - G_n
W_a_realizable = tf(pade(W_a,1))
bode(W_a_realizable)
```



(b) Assume we have derived the following detailed model:

$$G_{\text{actual}}(s) = \frac{10(-0.5s+1)}{(6s+1)(0.2s+1)(20s+1)}$$

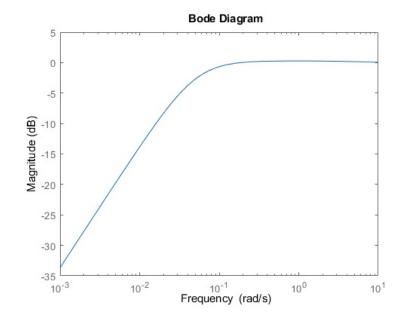
and we want to use the simplified nominal model  $G(s) = \frac{10}{6s+1}$  with multiplicative uncertainty. Find an appropriate weighting function  $w_I(s)$ .

$$G = G_{N}(1 + W; \Delta)$$

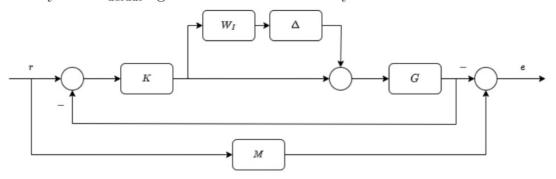
$$W; \Delta = \frac{G}{G_{N}} - 1$$

$$W; \Delta = \frac{-0.5 + 1}{(0.25 + 1)(205 + 1)} - 1$$

```
%Problem 1b  
G_actual = 10*(-0.5*s+1)/(6*s+1)/(0.2*s+1)/(20*s+1);  
G_n = 10/(6*s+1);  
W_i = (G_actual/G_n) - 1  
bodemag(W_i)
```



(c) Now using the results from Part b you will design a model matching controller for uncertain plant based on the block diagram below. In this case we would like to match the critically damped model  $M = \frac{1}{(s+1)^2}$ . Setup and solve the  $H_{\infty}$  optimal control problem and plot the step response of the system  $G_{actual}$  against the model M. Did you achieve RS?

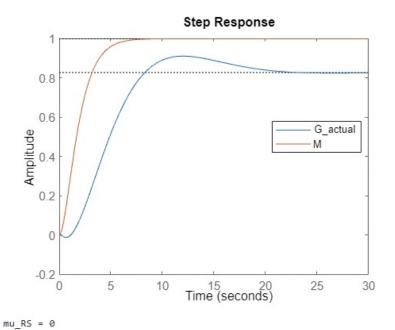


```
%Problem 1c
M = 1/(s+1)^2;

P = [0 0 W_i; -G_actual M -G_actual; -G_actual 1 -G_actual];
[K,CL,GAM] = hinfsyn(P,1,1);
G_CL = feedback(G_actual*K,1);

step(G_CL,M)
legend('G_actual','M',location='best')
[stabmarg,~] = robstab(lft(P,K));
mu_RS = 1/stabmarg.LowerBound
```

```
\begin{bmatrix} Y_D \\ z \\ v \end{bmatrix} = P \begin{bmatrix} u_B \\ w \\ u \end{bmatrix}
V = w - G(u + u_A)
Z = Nw - G(u + u_A)
V_B = u w;
\begin{bmatrix} Y_A \\ z \\ v \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 \\ -G & M & -G \\ -G & 1 & -G \end{bmatrix} \begin{bmatrix} u_B \\ w \\ n \end{bmatrix}
```



As mu-Rs is oct, we can see that this system is robustly stable.

### **2:** 30 points

Disk Drive Control Application

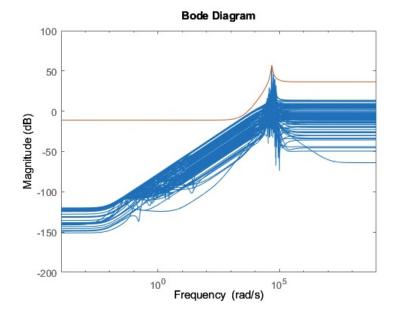
The file HDDModel\_DS\_Uncertain.m contains a dual-stage HDD model that includes uncertainty from various sources.

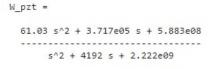
(a) The file contains 2 uncertain models - VCM and PZT. Use Matlab to fit a 2nd order multiplicative uncertainty weight that best approximates the uncertainty for each model. Report the final weight for each, and plot  $\frac{G_P-G}{G}$  for various perturbed plants  $G_p$  vs. the uncertainty weight for each plant.

```
%Problem 2a
HDDModel_DS_Uncertain;

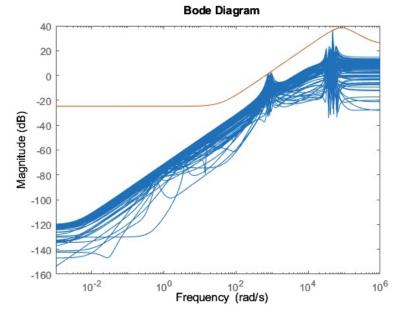
PZT_samples = usample(PZT,100);
[PZT_p,PZT_info] = ucover(PZT_samples,PZT.NominalValue,2);
W_pzt = tf(PZT_info.W1)
bodemag((PZT_samples-PZT.NominalValue)/PZT.NominalValue,W_pzt);

VCM_samples = usample(VCM,100);
[VCM_p,VCM_info] = ucover(VCM_samples,VCM.NominalValue,2);
W_vcm = tf(VCM_info.W1)
bodemag((VCM_samples-VCM.NominalValue)/VCM.NominalValue,W_vcm);
```





Continuous-time transfer function.



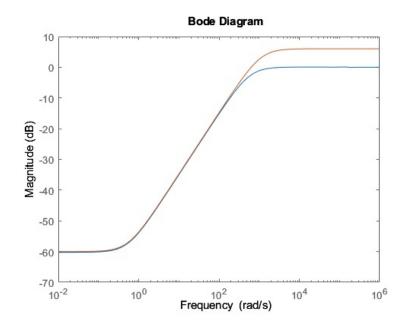
W\_vcm = 17.48 s^2 + 1.068e07 s + 4.009e08 s^2 + 1.301e05 s + 6.962e09

Continuous-time transfer function.

(b) Perform single stage robust controller design for the VCM plant using *mixsyn*. Maximize the crossover frequency such that the low frequency disturbances are rejected by a factor of 1000, the sensitivity peak is below 2, and  $\gamma < 1$ . A first order performance weight is fine. Compute

 $\|\begin{bmatrix} W_P S \\ W_T T \end{bmatrix}\|_{\infty}$  for your final design and plot the Bode magnitude plot of the uncertain sensitivity function vs. the performance weight.

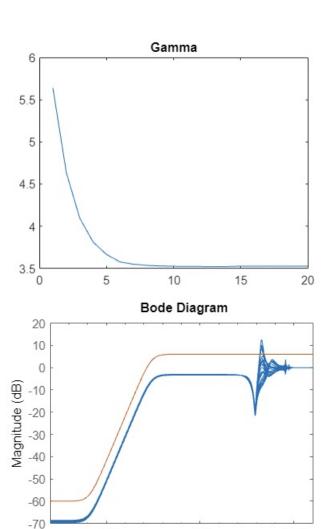
```
%Problem 2b
%Used class exxample for robust control
wh = 1500;
w1 = 0;
w_{try} = wh;
w_{new} = 1/2*(wh+w1);
while(abs(w_new - w_try)>.001)
    w_try = w_new;
    Wp = makeweight(1000, w_{try}, 1/2);
    [K,CL,GAM] = mixsyn(VCM.NominalValue, Wp, [], W vcm);
    wl = w_try;
    else
    wh = w_try; %
    end
    w_{new} = 1/2*(wh+w1);
S = 1/(1 + VCM.NominalValue*K);
bodemag(S,1/Wp)
```



(c) Perform dual stage robust controller design for the dual stage system  $G = \begin{bmatrix} VCM & PZT \end{bmatrix}$ . Use the same performance criteria from part b, and again maximize the crossover frequency such that  $\gamma < 3.5$ . For each step of your iteration, capture  $\gamma$ . Plot the value of  $\gamma$  vs. iteration count and plot the Bode magnitude plot of the uncertain sensitivity function vs. the performance weight for the final design. Does your final design satisfy robust performance?

# The final design fails to satisfy robust performance as GAM >1

```
%Problem 2c
G_nom = [VCM.NominalValue PZT.NominalValue];
G_mult = [VCM_p PZT_p];
G = [VCM PZT];
G_v = VCM.NominalValue;
G_p = PZT.NominalValue;
wh = 1500;
w1 = 0;
w_{try} = wh;
w_new = 1/2*(wh+w1);
gam_arr = [];
while(abs(w_new-w_try)>.001)
    systemnames = 'G_v G_p W_vcm W_pzt Wp';
    inputvar = '[ud1;ud2;d;u1;u2]';
    outputvar = '[W_vcm;W_pzt;Wp;-G_v-G_p-d]';
    input_to_G_v = '[u1+ud1]';
    input_to_G_p = '[u2+ud2]';
    input_to_W_vcm = '[u1]';
    input_to_W_pzt = '[u2]';
    input_to_Wp = '[G_v + G_p + d]';
    w_try = w_new;
    Wp = makeweight(1000, w_try, 1/2);
    P = sysic;
    [K,CL,GAM] = hinfsyn(P,1,2);
    gam_arr = [gam_arr GAM];
    if GAM<3.5
    wl = w_try;
    else
    wh = w_try;
    end
    w_{new} = 1/2*(wh+w1);
end
plot(1:length(gam_arr),gam_arr)
title("Gamma")
bodemag(1/(1+G_mult*K),1/Wp)
```



Frequency (rad/s)

 $10^{5}$ 

10<sup>-5</sup>

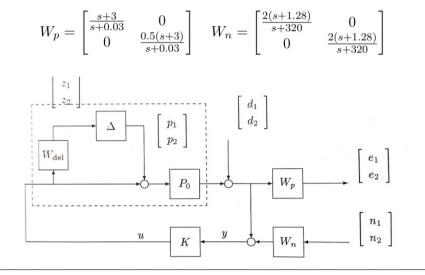
#### **3:** 20 points

### Aircraft Control Application

The nominal plant model for a highly maneuverable aircraft is given by

$$A = \begin{bmatrix} -0.0226 & -36.6 & -18.9 & -32.1 \\ 0 & -1.9 & 0.983 & 0 \\ 0.0123 & -11.7 & -2.63 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \quad B = \begin{bmatrix} 0 & 0 \\ -0.414 & 0 \\ -77.8 & 22.4 \\ 0 & 0 \end{bmatrix}$$
$$C = \begin{bmatrix} 0 & 57.3 & 0 & 0 \\ 0 & 0 & 0 & 57.3 \end{bmatrix} \quad D = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

Consider the block diagram below with

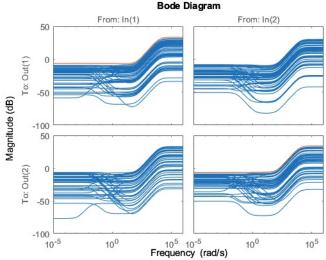


(a) The file responses.mat gives a vector of responses for the system. Fit a multiplicative uncertainty weight  $W_{del}$  to the response. Create a Bode magnitude plot that shows the quality of your fit.

```
%Problem 3a
clear;clc
load("responses.mat");
s = tf('s');
A = [-0.0226 -36.6 -18.9 -32.1;0 -1.9 0.983 0;0.0123 -11.7 -2.63 0;0 0 1 0];
B = [0 0;-0.414 0;-77.8 22.4;0 0];
C = [0 57.3 0 0;0 0 0 57.3];
D = [0 0;0 0];

W_p = [(s+3)/(s+0.03) 0; 0 0.5*(s+3)/(s+0.03)];
W_n = 2*(s+1.28)/(s+320)*eye(2);
G = ss(A,B,C,D);

[G_uncertain,G_info] = ucover(Gp_samples, G, [2,2]);
W_del = G_info.W1;
actual = (G_uncertain - G) / G;
bodemag(inv(G)*Gp_samples-eye(2), W_del)
```



(b) Design an  $H_{\infty}$  optimal controller considering the uncertainty. Plot the Bode magnitude of the sensitivity function for 10 samples of the uncertain plant. Do you meet robust performance specs? What about robust stability?

# System is robustly stable System does not have robust performance

```
%Problem 3b
W_del = G_info.W1;
systemnames = 'G W_p W_n W_del';
inputvar = '[p{2};n{2};d{2};u{2}]';
outputvar = '[W_del;W_p;W_n-G-d]';
input_to_G = '[u+p]';
input_to_W_p = '[d+G]';
input_to_W_n = '[n]';
input_to_W_del = '[u]';
cleanupsysic = 'yes';
P = sysic;
[K,CL,GAM] = hinfsyn(P,2,2);
GAM

S = eye(2)-feedback(G_uncertain*K,eye(2));
bodemag(S,inv(W_p))
[stabmarg,~,~,info] = robuststab(S)
```

