

# Experiment Results and Analysis

## Table of Contents

Section 2.....	1
Section 3.....	4
Section 4.....	6
Theoretical Model Analysis.....	10
Section 5.....	13
<i>Modifications to code</i> .....	17
Appendix .....	18
Erlang B Blocking Performance (Experimental) .....	18
Erlang B Blocking Performance (Theoretical) .....	20
Multiplexing Gain ( $P_b=1\%$ ).....	21
Probability of Hangup vs. Offered Load.....	22
Mean Waiting Time vs. Offered Load (Hangup included).....	23
Mean Waiting Time vs. Offered Load (Hangup excluded).....	23
$W(t)$ Experimental 1 trunk .....	24
$W(t)$ Theoretical 1 trunk .....	26
$W(t)$ Experimental 2 trunks.....	28
$W(t)$ Theoretical 2 trunks.....	31

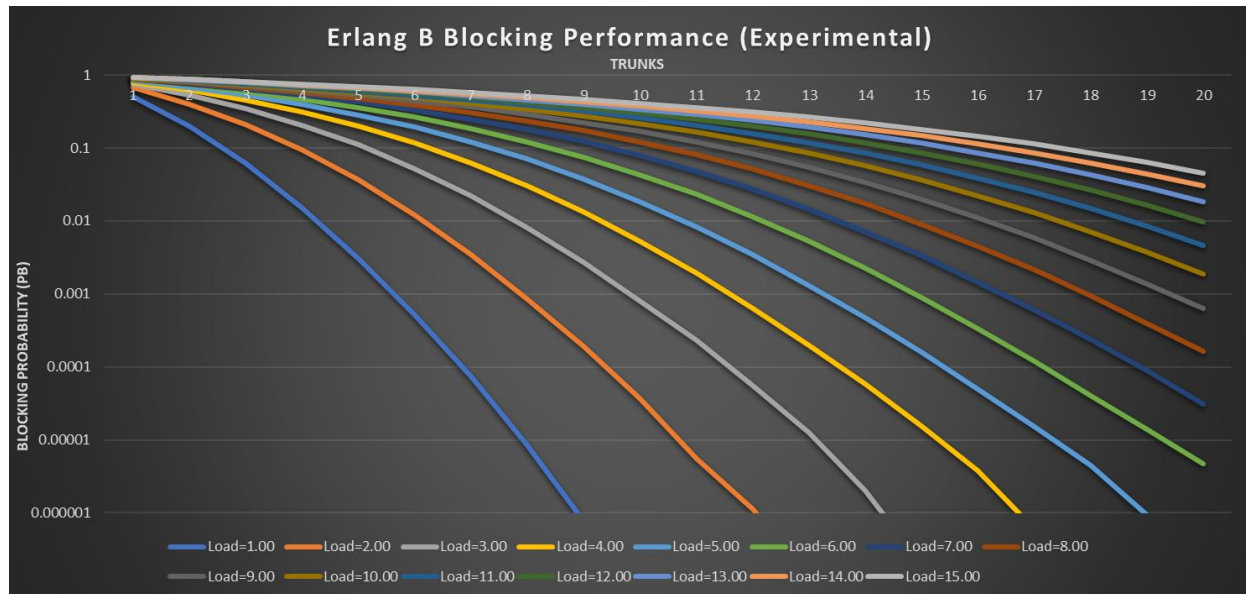
## Section 2

I've generated two plots, displayed below. The first demonstrates the experimental results of Erlang B Blocking Performance, and the second displays the theoretical results. The raw data for both sets will be available in the appendix.

To compute the experimental results, I ran simulations of 10 million calls, with a mean call length ( $E[X]$ ) of 3 minutes. By changing the arrival rate ( $\lambda$ ) in each simulation, I was able to change the offered load ( $A$ ), because  $A = \lambda E[X]$ .

I ran the simulation through a range of arrival rate =  $[1,15]$ , and number of trunks =  $[1,20]$ . I chose to run on 3 different seeds and average the results.

The offered load (A) is displayed through a variety of series plotted on the graph. The horizontal axis is in the blocking probability, and the horizontal axis is the number of trunks used.



Data is in the appendix at Erlang B Blocking Performance (Experimental)

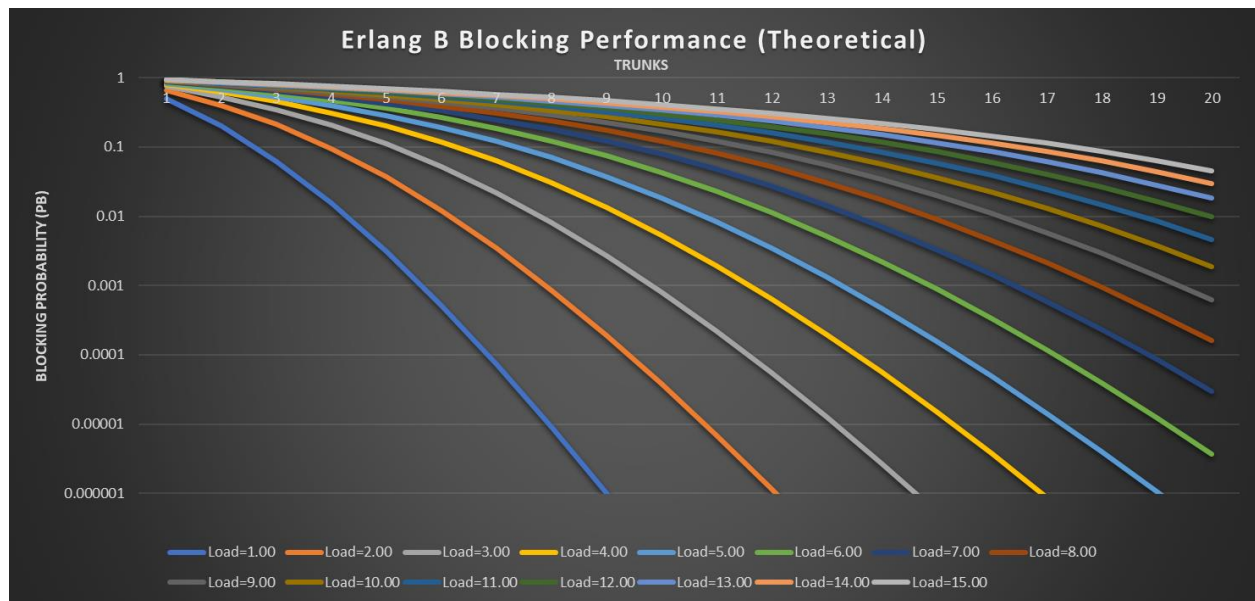
We can see that as the load increases, it requires more trunks to maintain the same blocking probability. The effects of **Trunking Efficiency** are also visible, as the difference in trunks required to maintain a given blocking probability becomes smaller as the load increases.

The theoretical results were calculated alongside each run in C, using the following code:

```
157 //theoretical_erlang_B
158 double accum = 0;
159 for (int i = 0; i <= data.trunk_count; i++) {
160     accum += (double)pow(offered_load, i) / fact2(i);
161 }
162 double theoretical_erlang_B = ((double)pow(offered_load, data.trunk_count) / fact2(data.trunk_count)) / accum;
163
```

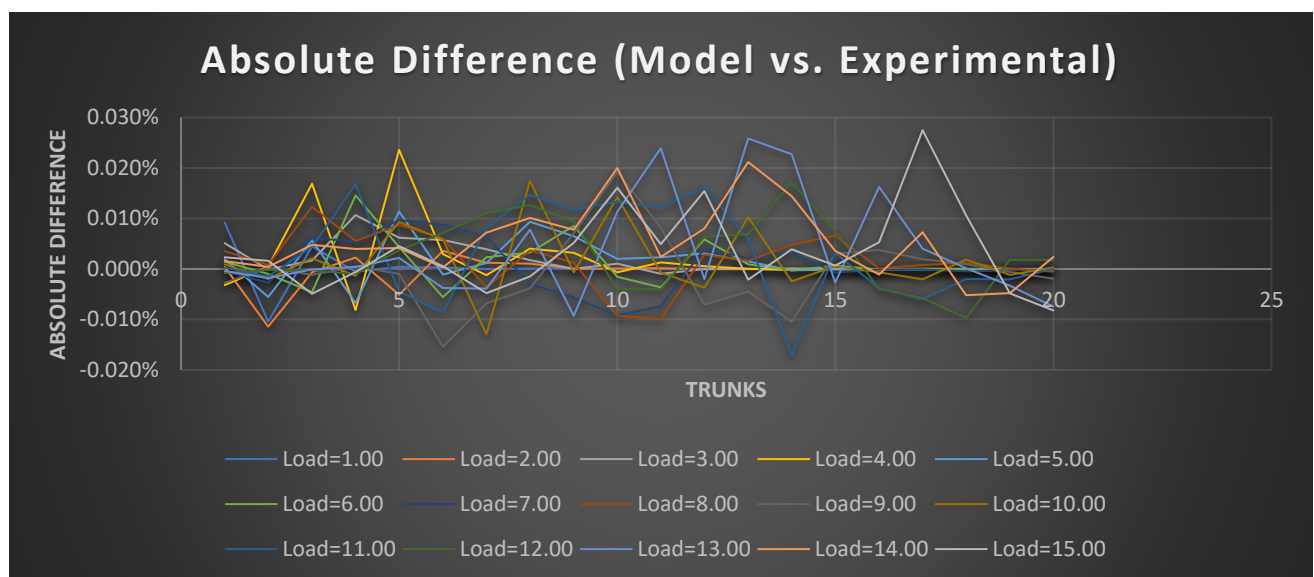
The results were verified using the erlang B online calculator at Westbay Engineers, Erlang and call center software (<https://www.erlang.com/calculator/erlb/>).

The theoretical results were plotted in the same style as the experimental, and the results are as follows.



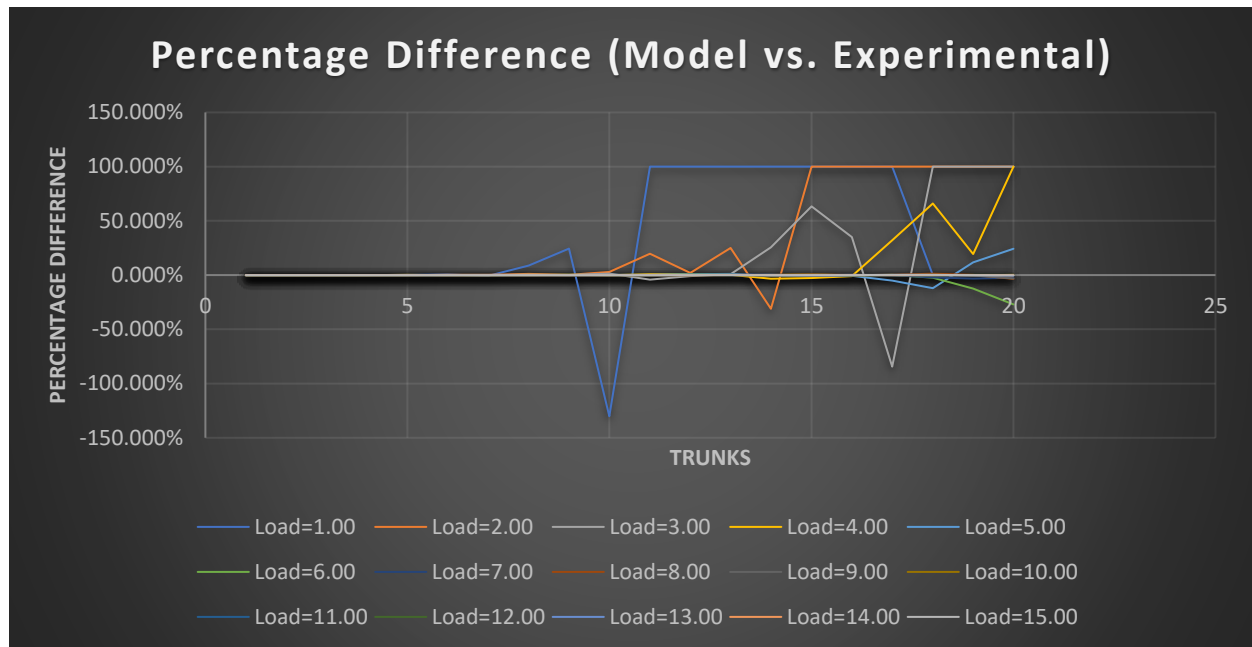
Data is in the appendix at Erlang B Blocking Performance (Theoretical)

The absolute difference between the theoretical and experimental model doesn't exceed  $\pm 0.03\%$ .



This small **absolute difference** tells us that the accuracy of the model is quite high at predicting the observed behaviour.

The relative difference between the experimental and theoretical values increases as the blocking probability becomes smaller (more trunks and smaller load lead to a smaller blocking probability).



This is because of the finite precision in floating point values, the relative change between two small numbers becomes increasingly large. These floating-point precision differences would be resolved by increasing the number of calls processed in the simulation due to the law of large numbers, however due to the small **absolute difference** the model is already very accurate.

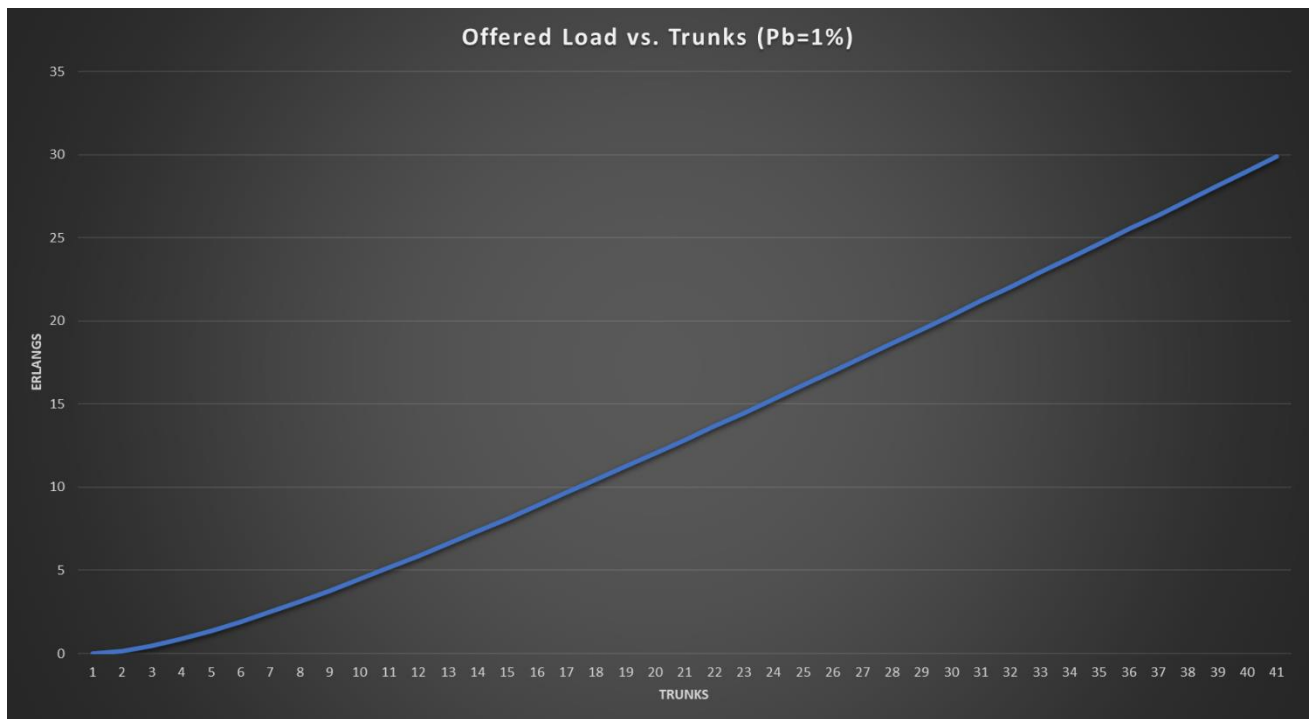
### Section 3

To find the offered load vs. trunk count with a blocking probability of 1% (using the **theoretical** Erlang B formula to calculate the blocking probability), I used nested loops in order to iterate through a fine range of arrival rates, for each trunk value.

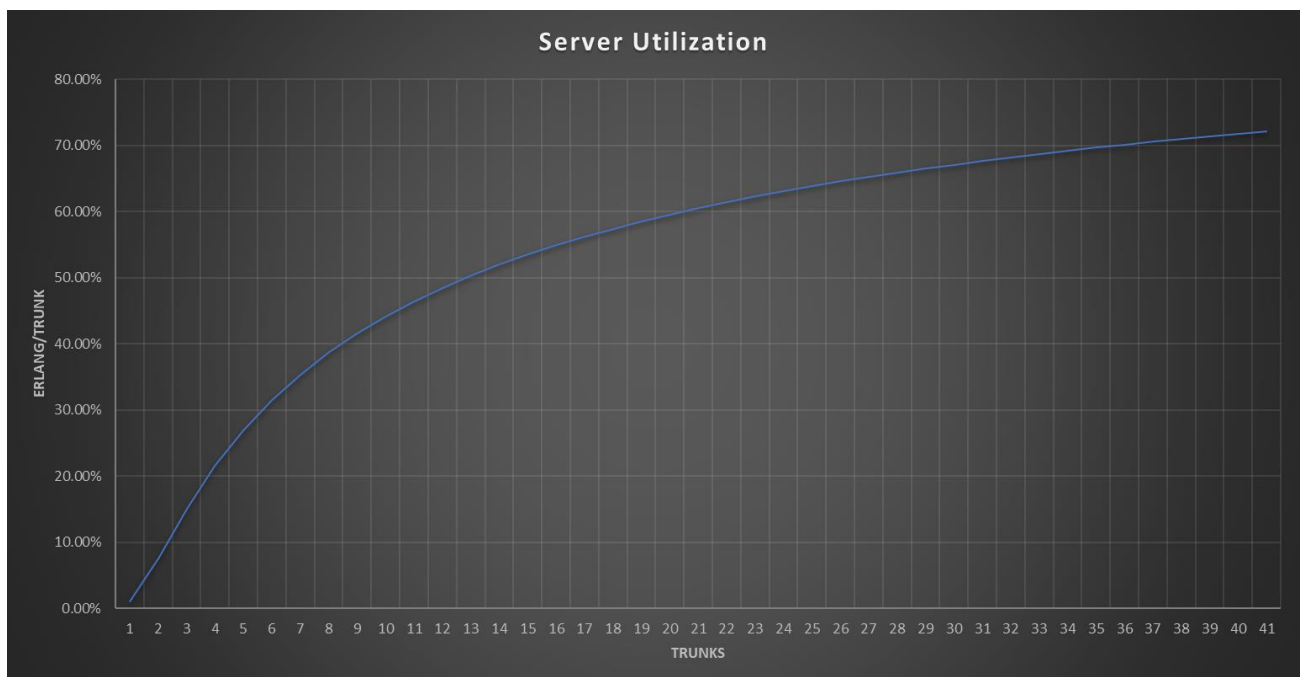
If I detected a blocking probability was greater than 1% (by using the erlang B formula on the offered load and trunk count), I would exit the loop and write the value to a file.

I ran this program with an arrival rate resolution of  $\pm 0.3$  *mErlangs*, in a range between [0.003,10] Erlangs.

The results are below.

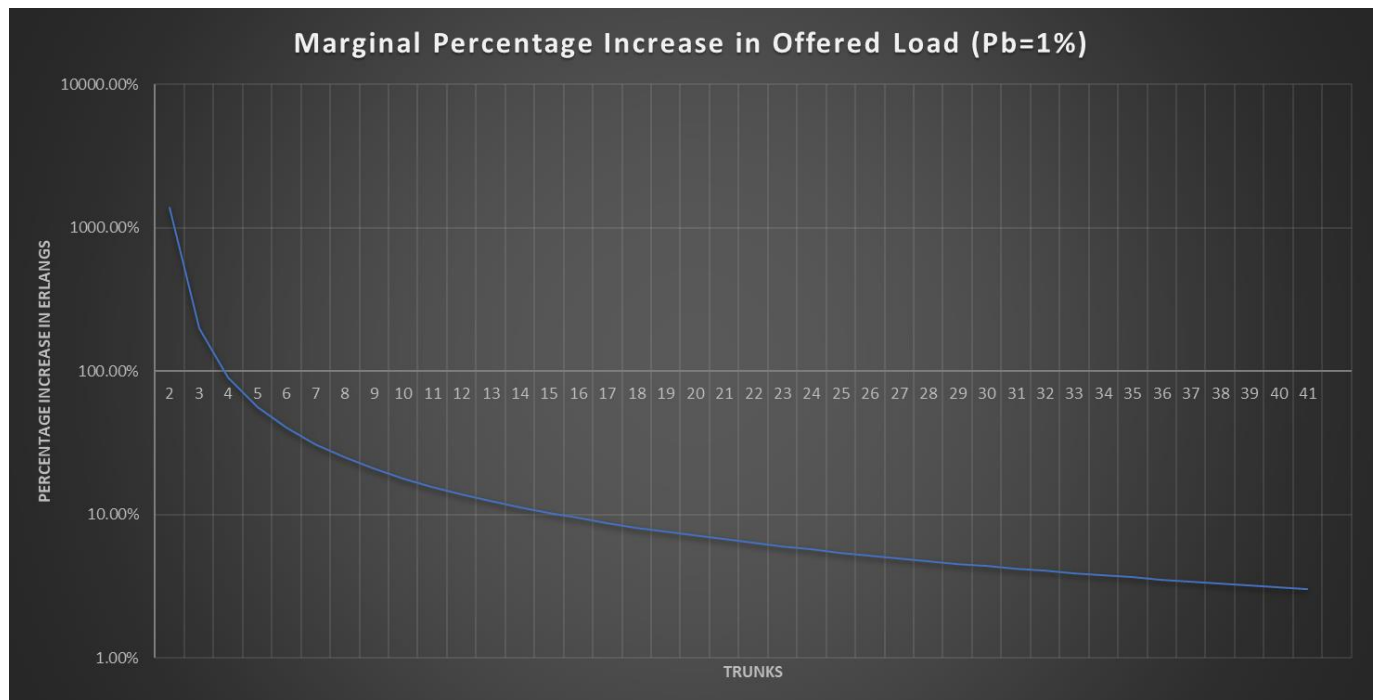


The maximum offered erlangs that achieve  $P_b=1\%$  increase as the number of trunks increase. This increase is **not linear**, due to multiplexing gain (trunking efficiency). The ratio of trunks to erlangs decreases as the number of trunks increases.



The server utilization is calculated using  $\frac{(1-P_b)A}{c}$ . The utilization increases as the number of trunks increases. This is multiplexing gain.

When looking at the marginal increase in utilization, we can see number of new Erlangs that can be serviced with the addition of new trunks is marginally decreasing, however it does not reach 0.

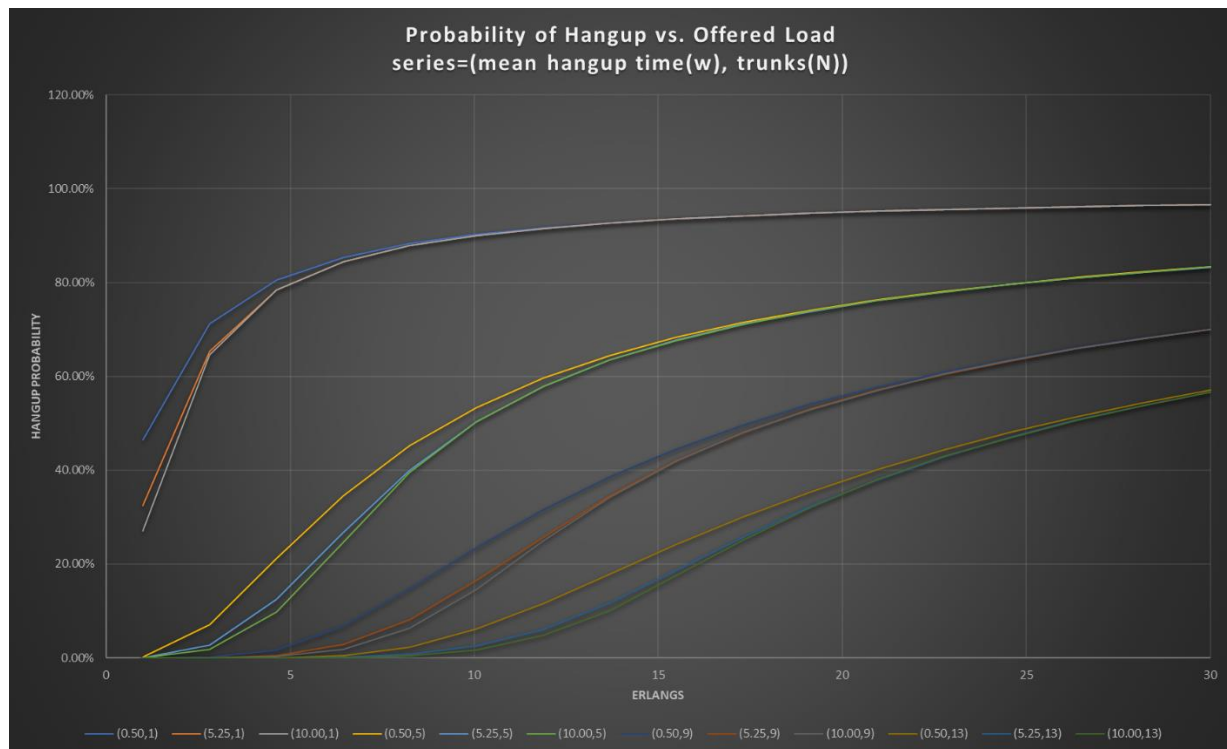


We can see that multiplexing gain is much higher at smaller trunk values, but the effect is still present even at larger trunk values.

Data for the above graphs is in the appendix at [Multiplexing Gain \(Pb=1%\)](#).

## Section 4

I have used a Fifo queue to hold customers that arrive when all servers are busy. When a server becomes free, the queue is checked and if a customer is waiting then they are put into service. If the customer hangup, then we increment a counter. At the end of the simulation, I calculate the hangup probability by taking the ration of customers that hang up against all arriving calls. I plot this probability against the arrival rate. I use separate series represented on the same graph to demonstrate the effect of the mean hangup time ( $w$ ) and the number of trunks ( $N$ ) on the hangup probability. I ran the simulation over 10 million processed calls, to apply the law of large numbers.



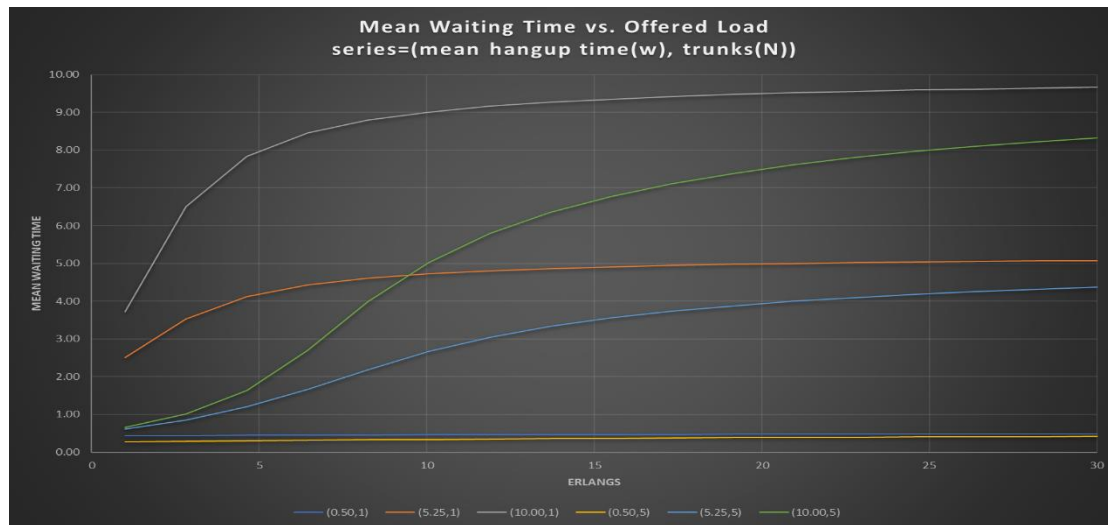
Data is in the appendix at Probability of Hangup vs. Offered Load

As the **arrival rate (offered load)** increases, the buffer will backfill, and the probability of a call being blocked will increase. As the number of **trunks** increases, the effect of the arrival rate is diminished as the utilization ( $A/N$ ) decreases, and the probability of a hangup decreases. As the **mean hangup time** increases, the hangup probability decreases. This is because the customers will be willing to wait for a longer period in the buffer before they hang up. This effect is more noticeable when the server is **stable**, as the buffer has not begun to drastically backfill.

System Parameter	Effect on Hangup Probability
Offered load	Increase
Number of Trunks	Decrease
Mean hangup time	Decrease

When calculating the **mean waiting time**, I decided to make two independent observations. I wanted to explore the mean waiting time of **all customers who call**, and **all customers who are served**. I think that from an industry standpoint, the waiting time of all customers who call can provide insight to identify the **mean hangup time** of a system, while the waiting time of all customers who are served provides insight into the **throughput** or performance of a system.

I plotted first a graph of the mean waiting time, including customers who have hung up (1).



Data is in the appendix at [Mean Waiting Time vs. Offered Load \(Hangup included\)](#)

The **mean waiting time ( $h$ )** trends towards the **mean hangup time ( $w$ )** as the offered load increases. This is because as the system becomes **unstable** and the buffer begins to **backfill**, most calls will hang up after the mean hangup time.

As the number of **trunks** increases, the system instability point increases, and therefore the mean waiting time **decreases** for a constant value of offered load.

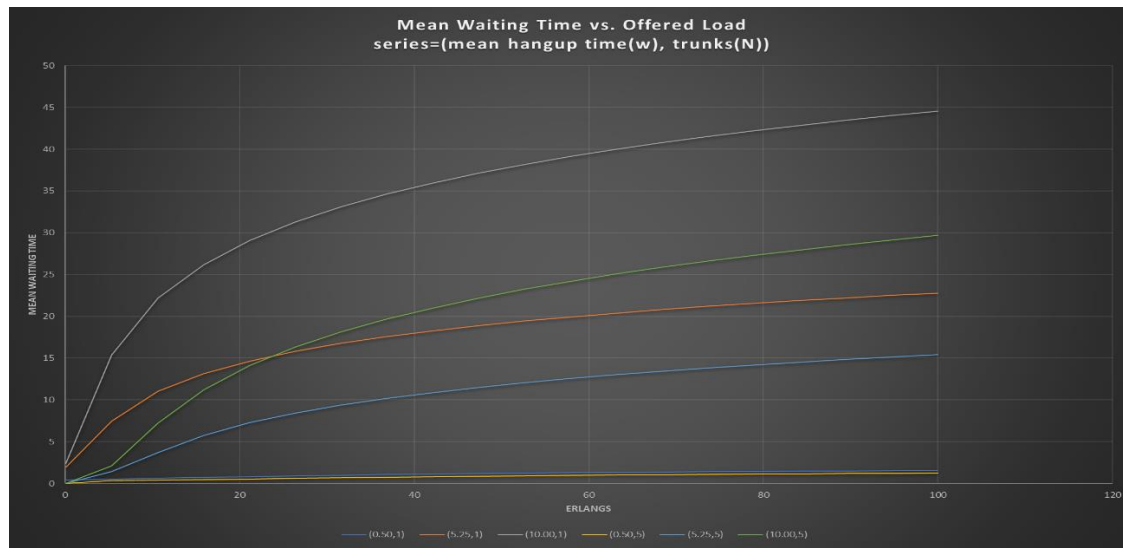
The mean waiting time **decreases** as the mean hangup time **decreases**, even for non-asymptotic behaviour.

- This is because as more customers hangup, there is a decreased chance that other customers will have to continue to wait, as they have effectively moved up a spot in the FIFO.

This plot exposes that a technique to analyze the **mean hangup time** of a system is to drive a high utilization, and measure the average time that users stay in the queue.



I plotted second a graph of the mean waiting time, not including customers who have hung up (2).



Data is in the appendix at Mean Waiting Time vs. Offered Load (Hangup excluded)

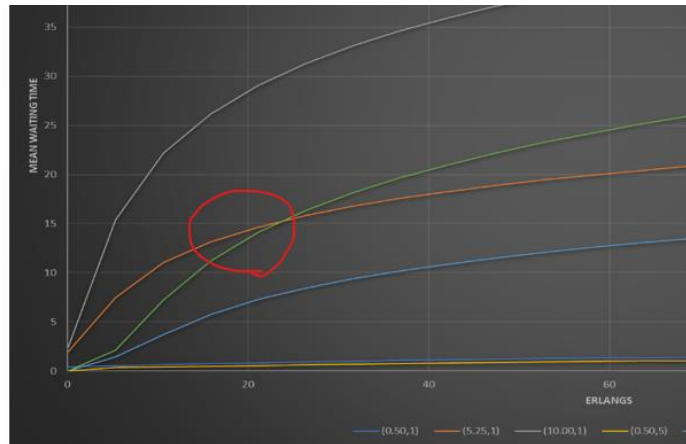
The **mean waiting time** trends towards **infinity**, as the queue continues to backfill when the system is unstable. This graph only includes customers who do not hang up, so the waiting time can now exceed the mean waiting time. The customers who do not hang up will still see a decrease in wait time as the number of trunks increase, and a decrease in wait time as mean hangup time decreases.

Both graphs (1 and 2) see the following relationships.

System Parameter	Effect on mean waiting time
Offered load	Increase
Number of Trunks	Decrease
Mean hangup time	Increase

The first graph sees a **horizontal asymptote** when the mean waiting time equals the mean hangup time. The second graph is unbounded, and customers who are served will see their mean waiting time increase to **infinity**.

It is **worth noting** that for non-asymptotic behaviour, when the system is stable, the number of trunks will have a greater impact on the mean waiting time than the mean hangup time will.



This is because a stable system will have a low mean waiting time, due to the servers being capable of handling the majority of arrivals. Once the system becomes unstable, the mean hangup time will have a greater impact than the number of trunks. This is because an unstable system will be unbounded, and the buffer will begin to **backfill**. The mean hangup time will then have a greater impact on whether customers will spend more or less time in the unstable system. As the hangup time **increases**, they will spend more time in the queue.

### Theoretical Model Analysis

As discussed in Section 5, the mean waiting time is proportional to the probability of waiting in a queue.

When customers hang up, the **Erlang A** formula will calculate the probability of waiting in the queue.

We see the same properties as above graphs, as the Erlang A formula

(<https://help.calabrio.com/doc/Content/user-guides/schedules/about-erlang-formula.htm>).

$$P_w = \frac{A\left(\frac{n\mu}{\theta}, \frac{\lambda}{\theta}\right) \cdot E_{1,n}}{1 + \left(A\left(\frac{n\mu}{\theta}, \frac{\lambda}{\theta}\right) - 1\right) \cdot E_{1,n}}$$

where

$$A(x, y) = 1 + \sum_{j=1}^{\infty} \frac{y^j}{\prod_{k=1}^j (x + k)}$$

and

$$E_{1,0} = 1$$

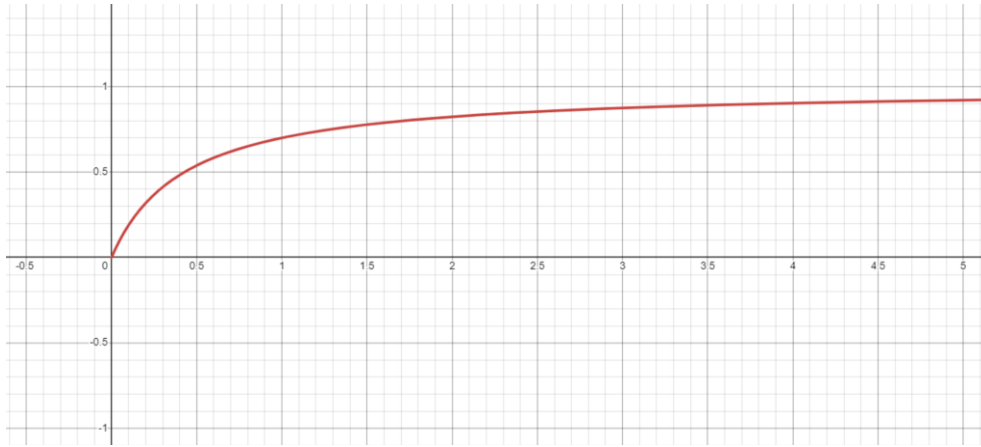
$$E_{1,n} = \frac{\rho E_{1,n-1}}{1 + \rho E_{1,n-1}}$$

and

$$\rho = \frac{\lambda}{n\mu}$$

We can see that  $E_{1,n}$  must be  $< 1$ , as the  $\frac{\rho}{1+\rho}$  will always be  $< 1$ .

Therefore, if  $A\left(\frac{n\mu}{\theta}, \frac{\lambda}{\theta}\right) = x$ ,  $f(x) \cong$  the below graph (plotted using <https://www.desmos.com/calculator>).



This shows us that as  $A\left(\frac{nu}{\theta}, \frac{\lambda}{\theta}\right)$  increases, the probability of waiting increases.

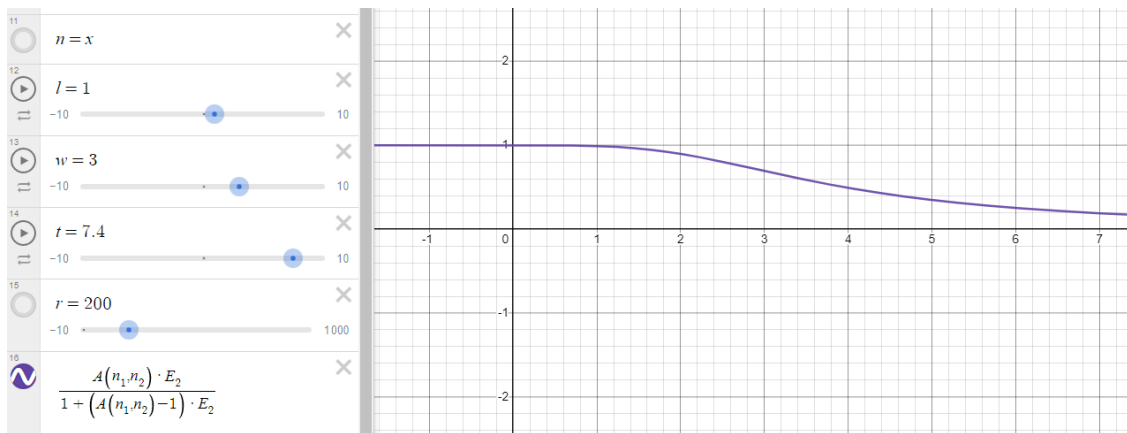
### Erlang A Model Analysis

I implemented the Erlang A model using an online graphing calculator tool, to quickly observe the effects of changing different system parameters (plotted using [desmos.com/calculator \(Erlang A\)](https://www.desmos.com/calculator/ErlangA)).

To observe the effects of different parameters, I hold all parameters constant, and then plot one parameter against the queuing probability.

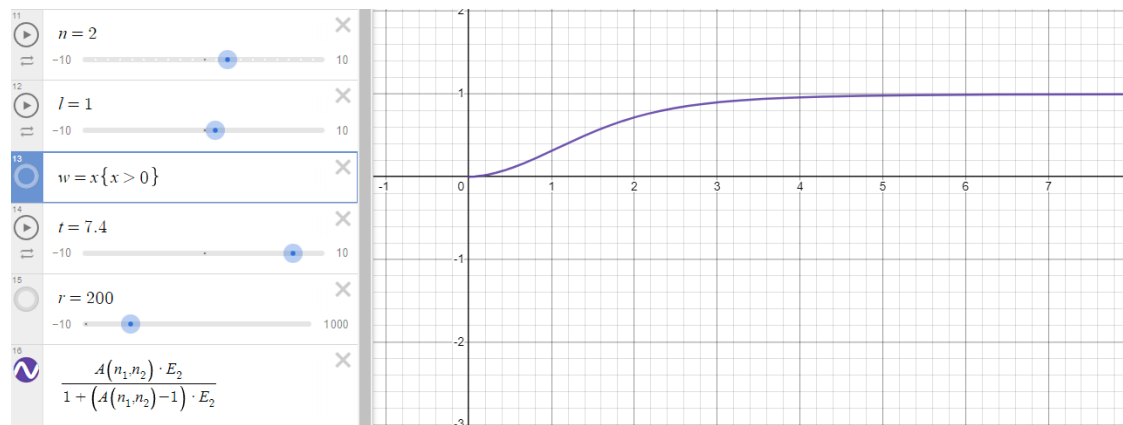
#### Trunks

We can see that as the **number of trunks** increases, the queuing probability decreases:



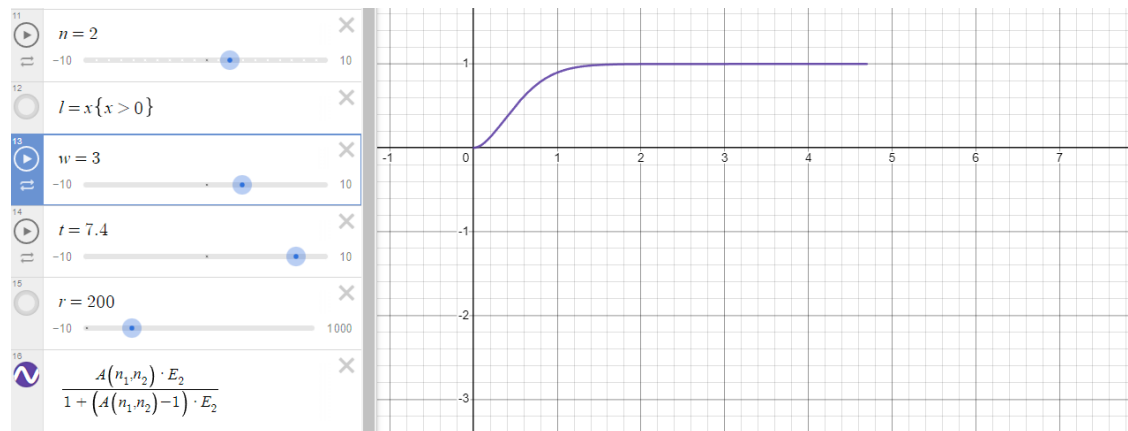
#### Call Length

We can see that as the **call length** increases, the queuing probability increases.



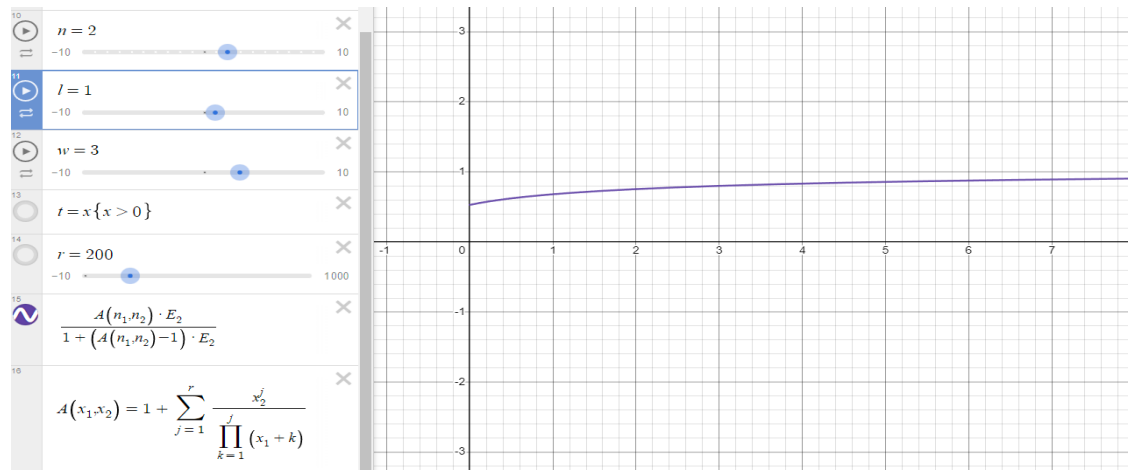
## Arrival Rate

We can see that as the **arrival rate** increases, the queuing probability increases.



## Mean Abandonment Time

We can see that as the **abandonment time** increases, the queuing probability increases.



## Theoretical

System Parameter	Effect on queuing probability
Offered load	Increase
Number of Trunks	Decrease
Mean hangup (abandonment) time	Increase

## Experimental

System Parameter	Effect on mean waiting time
Offered load	Increase
Number of Trunks	Decrease
Mean hangup time	Increase

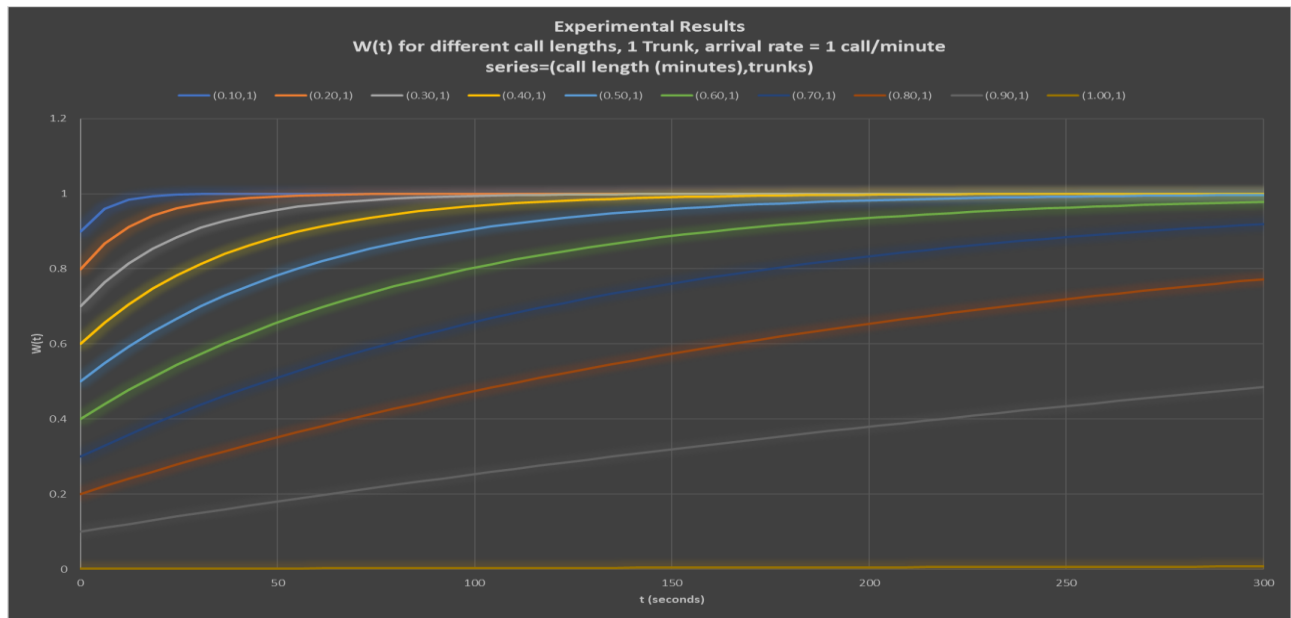
These theoretical analyses of the Erlang A formula align with the experimental results observed in the C simulation. The probability of being placed in the queue is shown to be proportional to the mean waiting time in Section 5.

### *Note on Erlang A*

The results obtained by the erlang A formula are held with some controversy when used in isolation to derive plans for call centers. This is because it has a tendency to predict lower trunk requirements than the Erlang B and C, by expecting customers to abandon their calls. The controversy is that it is good practice not to plan for customers to abandon their calls, as during busy periods this can lead to poor system performance (<https://www.callcentrehelper.com/a-beginners-guide-to-the-erlang-a-formula-140998.htm>).

## Section 5

I removed the hang-up functionality from the code, and ran the simulations over a range of different  $t$  values, collecting the number of callers that had to queue for less than  $t$  minutes. I have converted that values to *seconds* to align with the lab requirements, in the following graph.



Data is in the appendix at [W\(t\) Experimental 1 trunk](#).

As the **mean call length** increases, the probability of a caller waiting in the queue less than  $t$  seconds **decreases**. This makes sense, as the calls will take longer to be serviced, and therefore the queue will take longer to empty.

We can see that when the system becomes **unstable** (series (1.00,1)), the probability of any call waiting less than any value of  $t$  becomes 0. This is because the buffer will **backfill** to infinity, and the mean queuing time will explode to infinity.

Using the **Erlang C** formula:

$$P_w = \frac{A^N / N!}{A^N / N! + (1 - \rho) \sum_{i=0}^{N-1} A^i / i!}$$

We can calculate the probability that a customer will have to wait in the queue.

It can be shown that the average waiting time is therefore:

$$T_w = \frac{P_w h}{N(1 - A/N)}$$

We can see that the probability of waiting in the queue is proportional to the time spent waiting in the queue. The proportionality factor, is then equal to the average service time, multiplied by the mean number of calls in the queue.

$$\rho = A/N$$

$$N(1 - \rho) = \text{Mean Free Servers}$$

$$\frac{h}{N(1-\rho)} = \text{Mean time until free server} = T_f$$

The **mean time until free server** multiplied by the probability of being placed in a queue, is the **average queueing time**.

Given the arrivals follow an exponential distribution, we know that PDF of the waiting time will be:

$$P(T_f, t) = e^{-\lambda t}$$

Given  $\lambda$  is the average rate of server clearing events. From this we can derive:

$$\lambda = \frac{1}{T_f}$$

$$\lambda = \frac{1}{\frac{h}{N(1-\rho)}}$$

$$\lambda = \frac{N(1-\rho)}{h}$$

$$\lambda = \frac{N(1 - A/N)}{h}$$

$$\lambda = \frac{(N - A)}{h}$$

Given that waiting will only occur if a customer enters the queue, and the probability of waiting and the server clearing are independent events, we can show that:

$$P(T_w, t) = P[P_w \cup P(T_f, t)] = P_w \cdot e^{-\lambda t}$$

From the exponential distribution CDF, we can derive that:

$$P(T_w < t) = 1 - P_w \cdot e^{-\lambda t}$$

This is the equation posed in the lab, to calculate theoretical values of:

$$W(t) = P(T_w < t)$$

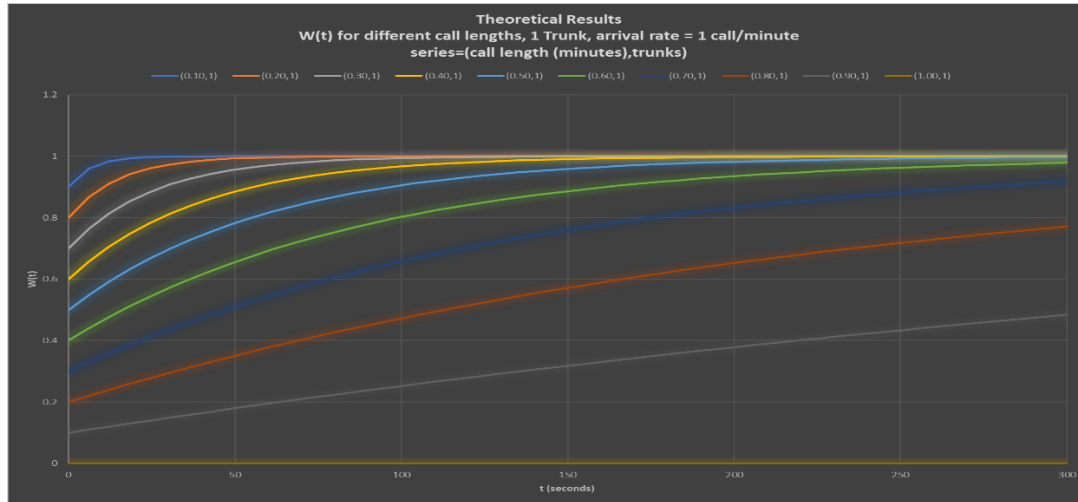
$$W(t) = 1 - P_w e^{-(N-A)t/h}.$$

I used a modified version of my erlang B C-code to calculate the theoretical  $W(t)$  values as my simulation ran.

```
//theoretical_erlang.c
double accum = 0;
for (int i = 0; i <= data.trunk_count-1; i++) {
    accum += (double)pow(offered_load, i) / fact2(i);
}
double theoretical_erlang_C = (((double)pow(offered_load, data.trunk_count) / fact2(data.trunk_count)) / (((double)pow(offered_load, data.trunk_count) / fact2(data.trunk_count)) + (1-(offered_load / data.trunk_count))*accum);
double theoretical_waiting_time = theoretical_erlang_C * (data.mean_call_time / (data.trunk_count * (1 - (offered_load / data.trunk_count))));
double Wt = 1-theoretical_erlang_C * exp( (-1 * (data.trunk_count - offered_load) * data.t_val) / data.mean_call_time);
```

The theoretical results are quite close to the experimental values. The only variance can likely be attributed to the law of large numbers.

The largest **discrepancy** in relative terms between the model and the experiment was on the order of 0.5%. The average relative difference is 0.05%.

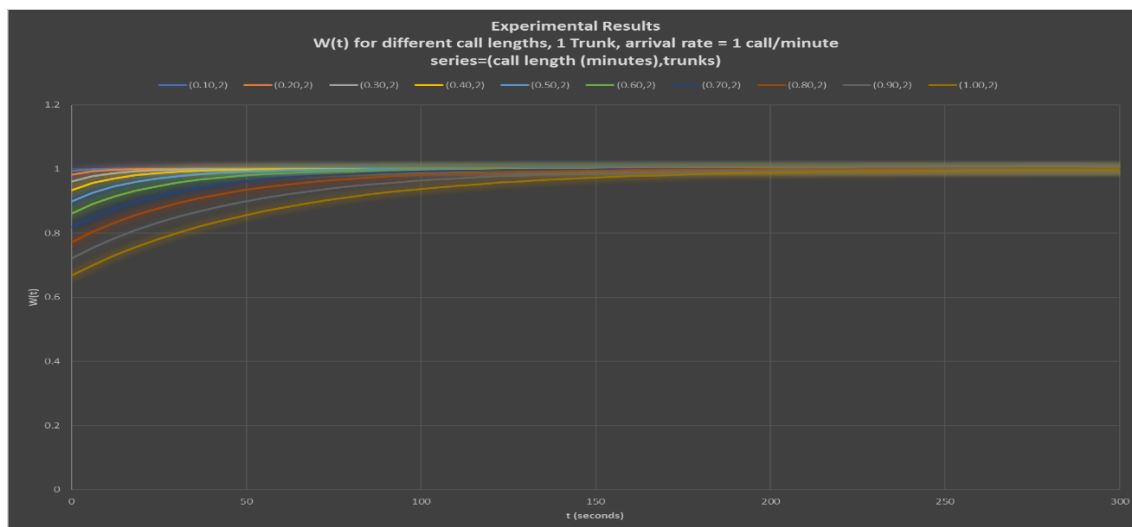


Data is in the appendix at W(t) Theoretical 1 trunk.

The results are visually similar to the experimental results, and show that as the **mean call time** increases, the probability of waiting less than  $t$  seconds will decrease.

I also simulated the effect of changing the **trunk** count on the waiting probability.

The experimental results below are for 2 trunks, an **increase** in trunk count.

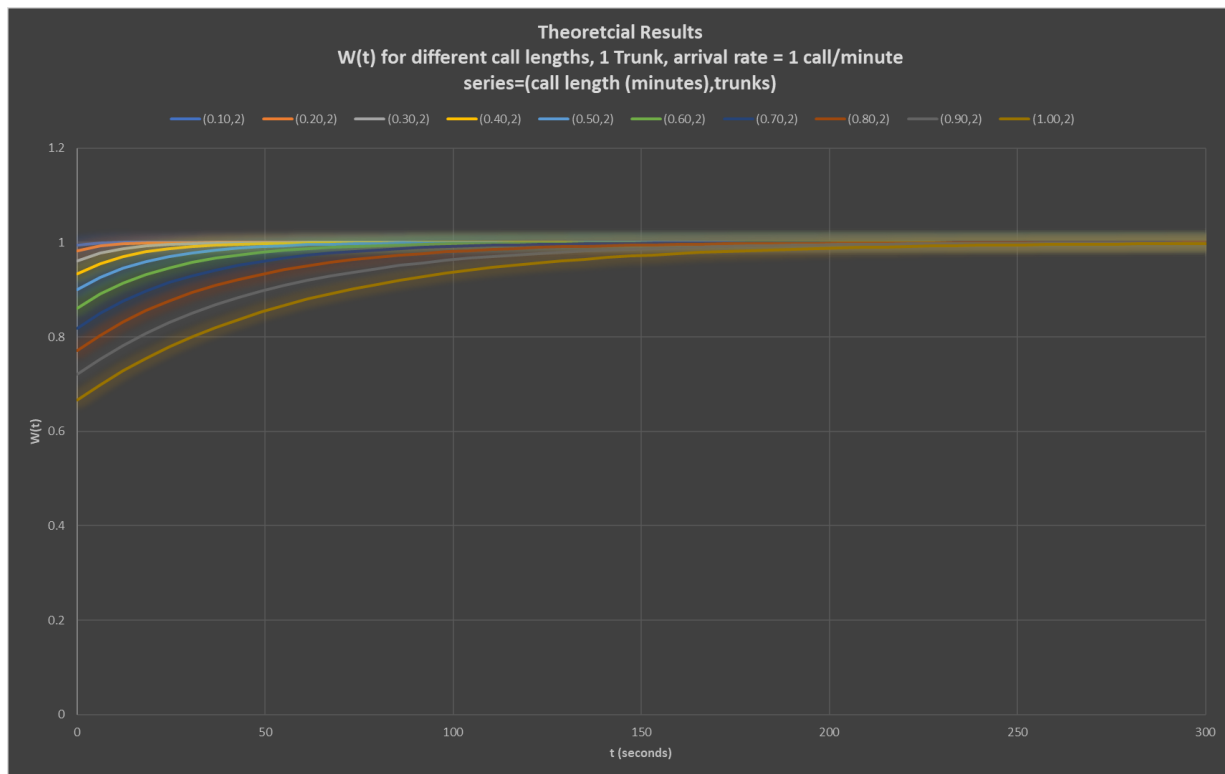


Data is in the appendix at W(t) Experimental 2 trunks.

We can see that **increasing** the number of trunks leads to an **increase** in the probability of having to wait less than  $t$  seconds.



I have calculated the theoretical values as well and see the same accuracy as with 1 trunk.



Data is in the appendix at [W\(t\) Theoretical 2 trunks](#).

### *Modifications to code*

For-loops were used to allow a range of arrival rates, seeds, trunks,  $t/W(t)$  values to be generated: to collect a fine range of data.

Data was exported en-masse to a .csv file, where the data was manipulated in excel to create the plots.

The code was modified throughout the lab to enable:

- Counters were used to track how many callers were blocked, had to queue, or abandoned their calls.
- The theoretical Erlang B and C models were implemented in C (code snippet is shown in report).
- Variables were used to store the amount of time spent in the queue, which is divided by the number of customers who enter the queue to determine the average time spent in the queue.
- To simulate customer *hangups* (abandonment), a conditional was added to check whether a customer has hung up before starting service. When a free server checks the FIFO, it checks whether the customer at the front has been in the queue for longer than their "hangup\_time" (a structural variable). If the customer has been in the queue for longer than their hangup\_time, they are discarded, and the server tries to grab another customer from the queue.

- The  $W(t)$  function was implemented in C, to generate theoretical results in section 5. Conditionals were used to detect customers who queue for less than  $t$  seconds, and a counter was incremented. This counter was divided by the number of customers serviced, in order to calculate the probability of queuing for less than  $t$  seconds.

## Appendix

### Erlang B Blocking Performance (Experimental)

Seed	trunks	Load=1.00	Load=2.00	Load=3.00	Load=4.00	Load=5.00	Load=6.00	Load=7.00	Load=8.00	Load=9.00	Load=10.00	Load=11.00	Load=12.00	Load=13.00	Load=14.00	Load=15.00
4001 3727 1	1	0.499 759	0.666 586	0.749 936	0.800 121	0.833 272	0.857 061	0.874 978	0.888 858	0.899 994	0.909 085	0.916 652	0.923 091	0.928 608	0.933 338	0.937 496
4001 3727 1	2	0.199 949	0.399 963	0.529 31	0.615 297	0.675 502	0.719 974	0.753 866	0.780 503	0.801 979	0.819 689	0.834 499	0.847 011	0.857 853	0.867 265	0.875 459
4001 3727 1	3	0.062 547	0.210 56	0.346 132	0.450 464	0.529 591	0.590 419	0.637 505	0.675 223	0.706 528	0.732 092	0.753 539	0.772 174	0.788 036	0.801 824	0.814 1
4001 3727 1	4	0.015 365	0.095 14	0.206 01	0.310 932	0.398 462	0.469 215	0.527 251	0.574 603	0.613 865	0.646 683	0.674 425	0.698 439	0.719 122	0.737 279	0.753 356
4001 3727 1	5	0.003 054	0.036 732	0.109 932	0.198 78	0.284 735	0.360 225	0.424 452	0.479 004	0.524 828	0.563 853	0.597 456	0.626 366	0.651 491	0.673 561	0.693 234
4001 3727 1	6	0.000 51	0.012 05	0.051 929	0.117 171	0.191 889	0.264 946	0.331 148	0.389 685	0.440 64	0.484 524	0.522 932	0.555 943	0.585 394	0.611 29	0.634 109
4001 3727 1	7	7.04E-05	0.003 41	0.021 824	0.062 682	0.120 321	0.185 03	0.248 873	0.307 993	0.361 528	0.409 273	0.451 084	0.487 799	0.520 706	0.550 049	0.575 895
4001 3727 1	8	8.5E-06	0.000 825	0.008 098	0.030 399	0.070 007	0.121 88	0.178 855	0.235 312	0.289 151	0.338 107	0.382 728	0.422 525	0.458 429	0.490 415	0.519 283
4001 3727 1	9	8E-07	0.000 189	0.002 702	0.013 393	0.037 388	0.075 017	0.122 108	0.172 875	0.224 226	0.273 167	0.318 814	0.360 076	0.398 371	0.432 483	0.463 825
4001 3727 1	10	1E-07	3.96E-05	0.000 799	0.005 318	0.018 404	0.043 194	0.078 753	0.121 744	0.167 55	0.214 481	0.259 365	0.302 04	0.341 089	0.376 699	0.410 12
4001 3727 1	11	0	5.9E-06	0.000 238	0.001 92	0.008 224	0.022 934	0.047 715	0.081 227	0.120 805	0.163 277	0.206 136	0.247 651	0.287 043	0.324 337	0.358 523
4001 3727 1	12	0	8E-07	5.56E-05	0.000 649	0.003 387	0.011 368	0.027 062	0.051 387	0.083 268	0.119 693	0.158 749	0.198 451	0.237 453	0.274 269	0.309 174
4001 3727 1	13	0	1E-07	1.25E-05	0.000 204	0.001 321	0.005 269	0.014 457	0.030 637	0.054 405	0.084 124	0.118 257	0.154 709	0.191 363	0.227 779	0.263 396
4001 3727 1	14	0	1E-07	1.8E-06	6.07E-05	0.000 488	0.002 237	0.007 119	0.017 313	0.033 831	0.056 868	0.085 213	0.116 899	0.151 008	0.185 833	0.219 837
4001 3727 1	15	0	0	3E-07	1.51E-05	0.000 168	0.000 891	0.003 344	0.009 028	0.019 854	0.036 409	0.058 81	0.085 693	0.115 754	0.147 744	0.180 142
4001 3727 1	16	0	0	1E-07	3E-06	5.15E-05	0.000 343	0.001 449	0.004 549	0.011 053	0.022 311	0.038 855	0.060 342	0.085 76	0.114 344	0.144 593
4001 3727 1	17	0	0	0	6E-07	1.53E-05	0.000 12	0.000 608	0.002 13	0.005 842	0.012 973	0.024 586	0.040 981	0.061 639	0.085 886	0.112 718
4001 3727 1	18	0	0	0	0	5.4E-06	4.29E-05	0.000 238	0.000 936	0.002 909	0.007 114	0.014 827	0.026 75	0.042 692	0.062 955	0.086 012
4001 3727 1	19	0	0	0	0	8E-07	1.43E-05	8.99E-05	0.000 406	0.001 366	0.003 755	0.008 574	0.016 503	0.028 53	0.044 32	0.063 648

4001 3727 1	20	0	0	0	0	2E-07	5.3E-06	2.99E-05	0.00017	0.000639	0.001848	0.004706	0.009853	0.018236	0.029968	0.045608
333	1	0.500074	0.666724	0.750021	0.799976	0.833325	0.85716	0.875006	0.888834	0.900042	0.909095	0.916656	0.923074	0.928564	0.933296	0.937452
333	2	0.200237	0.400244	0.529426	0.615344	0.675818	0.7199	0.753861	0.780532	0.802005	0.819658	0.834479	0.847056	0.857898	0.867278	0.875503
333	3	0.062517	0.210463	0.346006	0.450635	0.529697	0.590139	0.637604	0.675399	0.706277	0.731935	0.753606	0.772083	0.788083	0.801812	0.814122
333	4	0.015395	0.09532	0.206167	0.310708	0.398527	0.469603	0.527325	0.574534	0.6138	0.646584	0.6744	0.698405	0.719146	0.737252	0.753184
333	5	0.003076	0.03676	0.109994	0.198801	0.284577	0.360386	0.424627	0.47878	0.524986	0.563905	0.597489	0.626188	0.651629	0.673605	0.693125
333	6	0.000504	0.012068	0.052232	0.117034	0.191816	0.265098	0.331358	0.389797	0.440594	0.484532	0.52267	0.556015	0.585377	0.611183	0.634046
333	7	7.09E-05	0.003434	0.021817	0.062939	0.120737	0.18488	0.248733	0.308278	0.361725	0.409158	0.450765	0.488023	0.521041	0.550064	0.576254
333	8	7.5E-06	0.000852	0.00814	0.030384	0.070027	0.121947	0.178746	0.235821	0.289158	0.338233	0.382499	0.422653	0.45821	0.490291	0.519057
333	9	9E-07	0.000185	0.002712	0.013254	0.037357	0.075061	0.122343	0.173372	0.224067	0.273206	0.318415	0.360379	0.398291	0.432707	0.464012
333	10	5E-07	3.78E-05	0.000811	0.005338	0.018342	0.043115	0.078868	0.121781	0.167815	0.214567	0.259259	0.301755	0.341066	0.377271	0.41023
333	11	0	5.9E-06	0.000237	0.001921	0.008287	0.023024	0.04791	0.081513	0.120772	0.163005	0.206105	0.247849	0.287147	0.324375	0.358859
333	12	0	1.5E-06	5.79E-05	0.00063	0.003414	0.011261	0.026994	0.051353	0.083044	0.119728	0.158752	0.1985	0.23753	0.274663	0.309703
333	13	0	1E-07	1.21E-05	0.000193	0.001305	0.00516	0.01428	0.030701	0.054432	0.084313	0.118642	0.154914	0.191718	0.227981	0.263102
333	14	0	0	1.6E-06	5.83E-05	0.00047	0.002192	0.007059	0.017043	0.033948	0.056917	0.085528	0.117255	0.150783	0.18537	0.219925
333	15	0	0	1E-07	1.49E-05	0.000159	0.000884	0.003321	0.009052	0.019801	0.036478	0.058693	0.085781	0.116064	0.147956	0.180615
333	16	0	0	0	4.3E-06	5.27E-05	0.000321	0.001463	0.004512	0.010938	0.022284	0.038964	0.060646	0.085996	0.114558	0.144524
333	17	0	0	0	6E-07	1.49E-05	0.000115	0.000602	0.002121	0.005739	0.012851	0.024502	0.041006	0.061819	0.086139	0.113001
333	18	0	0	0	1E-07	4.1E-06	3.95E-05	0.000241	0.000926	0.002844	0.007072	0.014723	0.026433	0.042567	0.062818	0.086234
333	19	0	0	0	1E-07	7E-07	1.43E-05	8.81E-05	0.000392	0.001389	0.003769	0.008388	0.016428	0.028257	0.044219	0.063913
333	20	0	0	0	0	1E-07	3.7E-06	3.39E-05	0.000164	0.000645	0.001878	0.004582	0.009701	0.018042	0.029928	0.045688
4444	1	0.499891	0.666677	0.74989	0.799999	0.833345	0.857165	0.875028	0.888868	0.900047	0.909064	0.916683	0.92309	0.928553	0.933319	0.937482
4444	2	0.200126	0.400135	0.529502	0.615498	0.675874	0.720155	0.753894	0.780405	0.801947	0.81973	0.834516	0.847117	0.857908	0.867215	0.875449
4444	3	0.062301	0.210575	0.346272	0.450507	0.529525	0.59007	0.637347	0.675394	0.706416	0.732102	0.753765	0.772103	0.787944	0.801831	0.814038
4444	4	0.015409	0.095187	0.205823	0.310643	0.398241	0.46944	0.527293	0.574602	0.613745	0.646763	0.674307	0.698578	0.719274	0.737234	0.753219
4444	5	0.00306	0.036753	0.110051	0.198912	0.28495	0.36046	0.424789	0.478979	0.52494	0.563819	0.59746	0.62639	0.651476	0.673732	0.693187
4444	6	0.000511	0.012028	0.052139	0.117193	0.191869	0.26489	0.331224	0.389591	0.440776	0.484313	0.522863	0.556094	0.585407	0.61107	0.634162
4444	7	7.9E-05	0.003441	0.021834	0.062663	0.120463	0.185184	0.248815	0.308332	0.361705	0.409079	0.45086	0.487977	0.52096	0.549759	0.576165
4444	8	9E-06	0.000871	0.008107	0.030356	0.069828	0.121701	0.178953	0.235468	0.289282	0.338091	0.382599	0.422408	0.458346	0.490368	0.519472
4444	9	6E-07	0.000196	0.002696	0.013276	0.037434	0.075102	0.122022	0.173139	0.224395	0.273272	0.318561	0.36054	0.398717	0.432871	0.463796
4444	10	1E-07	3.37E-05	0.000789	0.005287	0.018347	0.043164	0.078878	0.121737	0.167947	0.214273	0.259717	0.302099	0.341061	0.377284	0.41019
4444	11	0	4.9E-06	0.000216	0.001898	0.00828	0.023124	0.047747	0.081421	0.12064	0.163437	0.205651	0.247918	0.287151	0.324436	0.358844
4444	12	0	1.1E-06	5.37E-05	0.00063	0.003429	0.01129	0.027067	0.051395	0.083159	0.119907	0.158692	0.19856	0.237269	0.274508	0.309537
4444	13	0	2E-07	1.33E-05	0.000193	0.001294	0.005198	0.014316	0.030608	0.054475	0.084272	0.118466	0.154872	0.1917	0.228219	0.26323
4444	14	0	0	2.7E-06	5.59E-05	0.000465	0.002274	0.00713	0.017162	0.033892	0.056745	0.08533	0.116962	0.151159	0.185774	0.22007
4444	15	0	0	2E-07	1.64E-05	0.000147	0.00088	0.003313	0.009025	0.019861	0.036588	0.058794	0.08549	0.115856	0.147557	0.180173

4444	16	0	0	1E-07	4.1E-06	4.41E-05	0.000341	0.001441	0.004526	0.011055	0.022331	0.03885	0.060367	0.085877	0.114652	0.144531
4444	17	0	0	1E-07	6E-07	1.53E-05	0.000118	0.000584	0.002108	0.005812	0.013085	0.024662	0.040884	0.061623	0.08628	0.112914
4444	18	0	0	0	1E-07	4E-06	3.85E-05	0.000231	0.000934	0.002921	0.007184	0.014804	0.026738	0.042784	0.062824	0.085942
4444	19	0	0	0	0	1.3E-06	1.33E-05	8.67E-05	0.000393	0.001378	0.003747	0.008526	0.016478	0.028438	0.044313	0.063669
4444	20	0	0	0	0	3E-07	5.2E-06	2.8E-05	0.00016	0.000623	0.001871	0.004631	0.009779	0.018275	0.03014	0.04573
MEA N	1	0.499908	0.666663	0.749949	0.800032	0.833314	0.857129	0.875004	0.888853	0.900027	0.909081	0.916664	0.923085	0.928575	0.933318	0.937477
MEA N	2	0.200104	0.400114	0.529413	0.61538	0.675731	0.72001	0.753874	0.78048	0.801977	0.819692	0.834498	0.847061	0.857186	0.867253	0.87547
MEA N	3	0.062455	0.210533	0.346137	0.450535	0.529604	0.59021	0.637485	0.675338	0.706407	0.732043	0.753637	0.77212	0.788021	0.801822	0.814087
MEA N	4	0.01539	0.095215	0.206	0.310761	0.39841	0.469419	0.52729	0.57458	0.613803	0.646677	0.674377	0.698474	0.719181	0.737255	0.753253
MEA N	5	0.003063	0.036748	0.109993	0.198831	0.284754	0.360357	0.424623	0.478921	0.524918	0.563859	0.597468	0.626315	0.651532	0.673633	0.693182
MEA N	6	0.000508	0.012049	0.0521	0.117133	0.191858	0.264978	0.331243	0.389691	0.44067	0.484456	0.522822	0.556017	0.585392	0.611181	0.634106
MEA N	7	7.34E-05	0.003428	0.021825	0.062761	0.120507	0.185031	0.248807	0.308201	0.361653	0.40917	0.450903	0.487933	0.520902	0.549957	0.576105
MEA N	8	8.33E-06	0.000849	0.008115	0.03038	0.069954	0.121843	0.178851	0.235534	0.289197	0.338144	0.382609	0.422529	0.458328	0.490358	0.519271
MEA N	9	7.67E-07	0.00019	0.002703	0.013308	0.037393	0.07506	0.122158	0.173129	0.22423	0.273215	0.318597	0.360332	0.39846	0.432687	0.463877
MEA N	10	2.33E-07	3.7E-05	0.0008	0.005314	0.018364	0.043158	0.078833	0.121754	0.167771	0.21444	0.259447	0.301965	0.341072	0.377085	0.41018
MEA N	11	0	5.57E-06	0.00023	0.001913	0.008264	0.023027	0.047791	0.081387	0.120739	0.16324	0.205964	0.247806	0.287113	0.324383	0.358742
MEA N	12	0	1.13E-06	5.57E-05	0.000636	0.00341	0.011306	0.027041	0.051378	0.083157	0.119776	0.158731	0.198503	0.237417	0.27448	0.309471
MEA N	13	0	1.33E-07	1.26E-05	0.000197	0.001307	0.005209	0.014351	0.030648	0.054437	0.084236	0.118455	0.154832	0.191594	0.227993	0.263243
MEA N	14	0	3.33E-08	2.03E-06	5.83E-05	0.000475	0.002234	0.007103	0.017173	0.03389	0.056843	0.085357	0.117039	0.150983	0.185659	0.219944
MEA N	15	0	0	2E-07	1.55E-05	0.000158	0.000885	0.003326	0.009035	0.019838	0.036492	0.058766	0.085654	0.115892	0.147752	0.18031
MEA N	16	0	0	6.67E-08	3.8E-06	4.94E-05	0.000335	0.001451	0.004529	0.011015	0.022309	0.03889	0.060452	0.085878	0.114518	0.144549
MEA N	17	0	0	3.33E-08	6E-07	1.52E-05	0.000118	0.000598	0.002119	0.005798	0.01297	0.024583	0.040957	0.061693	0.086101	0.112878
MEA N	18	0	0	0	6.67E-08	4.5E-06	4.03E-05	0.000237	0.000932	0.002891	0.007124	0.014785	0.02664	0.042681	0.062866	0.086063
MEA N	19	0	0	0	3.33E-08	9.33E-05	1.4E-05	8.82E-05	0.000397	0.001378	0.003757	0.008496	0.01647	0.028408	0.044284	0.063743
MEA N	20	0	0	0	0	2E-07	4.73E-06	3.06E-05	0.000165	0.000636	0.001866	0.00464	0.009777	0.018184	0.030012	0.045675

## Erlang B Blocking Performance (Theoretical)

trunks	Load=1.00	Load=2.00	Load=3.00	Load=4.00	Load=5.00	Load=6.00	Load=7.00	Load=8.00	Load=9.00	Load=10.00	Load=11.00	Load=12.00	Load=13.00	Load=14.00	Load=15.00
1	0.5	0.666667	0.75	0.8	0.833333	0.857143	0.875	0.888889	0.9	0.909091	0.916667	0.923077	0.928571	0.933333	0.9375
2	0.2	0.4	0.529412	0.615385	0.675676	0.72	0.753846	0.780488	0.80198	0.819672	0.834483	0.847059	0.857868	0.867257	0.875486
3	0.0625	0.210526	0.346154	0.450704	0.529661	0.590164	0.637546	0.675462	0.706395	0.732064	0.753681	0.772118	0.78802	0.80187	0.814038
4	0.015385	0.095238	0.206107	0.31068	0.398343	0.469565	0.527345	0.574635	0.613809	0.646663	0.674545	0.698464	0.719185	0.737295	0.753247
5	0.003067	0.036697	0.110054	0.199067	0.284868	0.3604	0.424719	0.479008	0.524908	0.563952	0.597423	0.626352	0.651554	0.673675	0.693227
6	0.000511	0.012085	0.052157	0.117162	0.191847	0.264922	0.33133	0.389752	0.440516	0.484515	0.522736	0.556089	0.585355	0.611183	0.634111
7	7.3E-05	0.003441	0.021864	0.062749	0.120519	0.185055	0.248871	0.308165	0.361585	0.409041	0.450984	0.488045	0.520863	0.550029	0.576057

8	9.12E-06	0.000859	0.008132	0.03042	0.070048	0.121876	0.178822	0.23557	0.289158	0.338318	0.382756	0.422655	0.458406	0.490459	0.519256
9	1.01E-06	0.000191	0.002703	0.01334	0.037458	0.075145	0.122101	0.173141	0.2243	0.273208	0.318714	0.360426	0.398367	0.432765	0.463929
10	1.01E-07	3.82E-05	0.00081	0.005308	0.018385	0.043142	0.078741	0.121661	0.167963	0.214582	0.25958	0.301925	0.341185	0.377285	0.410341
11	9.22E-09	6.94E-06	0.000221	0.001926	0.008287	0.022991	0.047717	0.081288	0.120821	0.163232	0.206085	0.247766	0.287353	0.324407	0.358792
12	7.68E-10	1.16E-06	5.52E-05	0.000642	0.003441	0.011365	0.027081	0.051406	0.083087	0.119739	0.158894	0.198567	0.237397	0.27456	0.309626
13	5.91E-11	1.78E-07	1.27E-05	0.000197	0.001322	0.005218	0.014373	0.030665	0.054393	0.084339	0.118515	0.154901	0.191852	0.228205	0.263222
14	4.22E-12	2.54E-08	2.73E-06	5.64E-05	0.000472	0.002231	0.007135	0.017221	0.033785	0.056819	0.085186	0.11721	0.15121	0.185804	0.219983
15	2.81E-13	3.39E-09	5.46E-07	1.5E-05	0.000157	0.000892	0.003319	0.009101	0.019868	0.036497	0.058797	0.085729	0.115865	0.147788	0.180316
16	1.8E-14	4.24E-10	1.02E-07	3.76E-06	4.91E-05	0.000334	0.00145	0.00453	0.011052	0.022302	0.038852	0.060413	0.08604	0.114507	0.144602
17	1E-15	4.99E-11	1.81E-08	8.85E-07	1.45E-05	0.000118	0.000597	0.002127	0.005817	0.012949	0.024523	0.040934	0.061734	0.086174	0.113153
18	0	5.54E-12	3.01E-09	1.97E-06	4.01E-05	3.93E-05	0.000232	0.000945	0.0029	0.007142	0.014765	0.026543	0.042683	0.062814	0.086169
19	0	5.83E-13	4.76E-10	4.14E-08	1.06E-06	1.24E-05	8.55E-05	0.000398	0.001372	0.003745	0.008476	0.016488	0.028375	0.044236	0.063695
20	0	5.8E-14	7.14E-11	8.28E-09	2.64E-07	3.73E-06	2.99E-05	0.000159	0.000617	0.001869	0.00464	0.009796	0.01811	0.030035	0.045593

### Multiplexing Gain (Pb=1%)

trunks	load	pb0.1	Marginal increase in Load	Utilization
1	0.0103	0.010195		0.010195
2	0.152796	0.010025	13.83492011	0.075632
3	0.455489	0.01	1.98102064	0.150311
4	0.86948	0.010002	0.908891282	0.215196
5	1.360868	0.010002	0.565152371	0.269451
6	1.909255	0.010005	0.402968617	0.315026
7	2.501142	0.010004	0.3100089	0.353732
8	3.127827	0.010004	0.250559729	0.387067
9	3.782712	0.010002	0.2093737	0.416097
10	4.461296	0.010001	0.179390926	0.441668
11	5.15998	0.010001	0.156610032	0.464398
12	5.876063	0.010001	0.13877638	0.484775
13	6.607446	0.010003	0.124468193	0.503181
14	7.351728	0.01	0.112643017	0.519872
15	8.108311	0.010002	0.102912172	0.535147
16	8.875093	0.010001	0.094567429	0.549146
17	9.651775	0.010001	0.087512535	0.562073
18	10.43716	0.010002	0.081371736	0.574042
19	11.23034	0.010002	0.075995938	0.585159
20	12.03072	0.010001	0.071269567	0.59552
21	12.838	0.010001	0.067101654	0.605219
22	13.65128	0.01	0.063349509	0.614308
23	14.47056	0.010001	0.060014943	0.622863
24	15.29524	0.010001	0.056990235	0.630928

25	16.12472	0.010001	0.054231282	0.638538
26	16.959	0.010001	0.051739214	0.645746
27	17.79748	0.01	0.049441608	0.652574
28	18.64047	0.010001	0.047365139	0.659073
29	19.48705	0.010001	0.045416262	0.665247
30	20.33753	0.010001	0.043643361	0.671138
31	21.19131	0.010001	0.041980529	0.676754
32	22.04839	0.01	0.040444889	0.682122
33	22.90877	0.010001	0.039022355	0.687263
34	23.77215	0.010001	0.037687751	0.692188
35	24.63823	0.01	0.036432547	0.69691
36	25.5073	0.010001	0.035273633	0.70145
37	26.37878	0.010001	0.034165886	0.70581
38	27.25266	0.010001	0.033128123	0.710003
39	28.12894	0.010001	0.032153904	0.714042
40	29.00762	0.010001	0.031237558	0.717938
41	29.8884	0.010001	0.030363723	0.721695

## Probability of Hangup vs. Offered Load

Seed	Arrival Rate	(0.50,1)	(5.25,1)	(10.00,1)	(0.50,5)	(5.25,5)	(10.00,5)	(0.50,9)	(5.25,9)	(10.00,9)	(0.50,13)	(5.25,13)	(10.00,13)	(0.50,17)	(5.25,17)	(10.00,17)
4E+08	1	0.396454	0.48502	0.491833	0.000909	0.002456	0.002709	0	6E-07	6E-07	0	0	0	0	0	0
4E+08	2	0.586011	0.653476	0.659469	0.014237	0.030904	0.033229	4.12E-05	0.000139	0.000161	2E-07	2E-07	2E-07	0	0	0
4E+08	3	0.692711	0.739188	0.743998	0.053656	0.096745	0.102422	0.000675	0.002001	0.002278	2.2E-06	6.2E-06	8.4E-06	0	0	0
4E+08	4	0.759269	0.790986	0.794962	0.116973	0.180594	0.188332	0.003941	0.010252	0.011421	3.86E-05	0.000135	0.000155	0	8E-07	0.000001
4E+08	5	0.803363	0.825917	0.829105	0.192146	0.263734	0.272885	0.013525	0.030255	0.033056	0.000272	0.000865	0.001021	2.4E-06	8.8E-06	1E-05
4E+08	6	0.834643	0.850699	0.853492	0.269048	0.338897	0.348063	0.032626	0.063285	0.068077	0.001312	0.003765	0.004327	1.88E-05	7.54E-05	8.96E-05
4E+08	7	0.857762	0.869325	0.871784	0.340679	0.403502	0.412162	0.062113	0.105671	0.112325	0.004153	0.010694	0.012014	0.000103	0.000374	0.000445
4E+08	8	0.875363	0.883949	0.886053	0.404005	0.459424	0.467336	0.100448	0.154038	0.161993	0.010471	0.023989	0.026549	0.000435	0.001438	0.001633
4E+08	9	0.88905	0.895517	0.897333	0.460463	0.506924	0.514124	0.144371	0.203019	0.211447	0.021422	0.043901	0.047711	0.001401	0.004092	0.004707
4E+08	10	0.900062	0.905221	0.906734	0.508486	0.546971	0.553347	0.192079	0.251525	0.260366	0.038298	0.070228	0.075502	0.003642	0.009406	0.010679
4E+08	11	0.909085	0.913166	0.914569	0.550292	0.581454	0.587892	0.239903	0.296502	0.305066	0.060819	0.101498	0.107993	0.007868	0.018628	0.020682
4E+08	12	0.916712	0.919885	0.921112	0.586088	0.611503	0.617266	0.286419	0.338659	0.347205	0.089577	0.136246	0.143357	0.014837	0.032086	0.035566
4E+08	13	0.923067	0.925688	0.926756	0.6171	0.637786	0.642857	0.330454	0.377317	0.385461	0.121073	0.17132	0.179446	0.02568	0.049901	0.054184
4E+08	14	0.928526	0.930666	0.931644	0.643605	0.660965	0.665641	0.371558	0.413184	0.420484	0.1554	0.206848	0.215238	0.040231	0.071764	0.076718
4E+08	15	0.933304	0.935114	0.935954	0.666844	0.681624	0.685743	0.408464	0.445374	0.451961	0.191071	0.241984	0.249964	0.059206	0.096456	0.102371
4E+08	16	0.937444	0.938967	0.939723	0.68772	0.699666	0.703525	0.443066	0.474651	0.48082	0.226593	0.275067	0.283091	0.081018	0.122875	0.130025
4E+08	17	0.94119	0.942425	0.943135	0.706179	0.715801	0.719558	0.474238	0.501044	0.506956	0.261783	0.306674	0.314784	0.105591	0.151319	0.158439
4E+08	18	0.944468	0.945488	0.946078	0.72256	0.730646	0.733905	0.502073	0.525132	0.530764	0.295761	0.336877	0.343835	0.132661	0.178775	0.187268
4E+08	19	0.947372	0.948235	0.948816	0.73682	0.744038	0.747102	0.527952	0.547414	0.552906	0.327845	0.364496	0.372001	0.160771	0.206657	0.215267
4E+08	20	0.949982	0.950722	0.951271	0.750195	0.756066	0.758802	0.550736	0.567473	0.572968	0.357977	0.39096	0.397691	0.189918	0.234657	0.242148
4E+08	21	0.952357	0.952992	0.953478	0.762094	0.767014	0.769627	0.572109	0.586328	0.590998	0.386309	0.415626	0.421936	0.218792	0.261117	0.268617
4E+08	22	0.954526	0.955073	0.955583	0.772819	0.777172	0.779642	0.591408	0.603501	0.608084	0.412367	0.43809	0.444359	0.247819	0.28705	0.294082

4E+08	23	0.95650 9	0.95699 1	0.95741 7	0.78246 6	0.78630 9	0.78874 7	0.60886 3	0.61974 6	0.62380 1	0.43704 1	0.45977 7	0.46603 1	0.27468 6	0.31089 6	0.31862 2
4E+08	24	0.95834 4	0.95875	0.95910 4	0.79176	0.79473 1	0.79711 8	0.62540 2	0.63416 3	0.63810 6	0.45944 4	0.47971 7	0.48521 6	0.30172 8	0.33443 3	0.34179 2
4E+08	25	0.95998	0.96030 8	0.96063	0.80003 7	0.80274	0.80472	0.64002 9	0.64801 8	0.65148 7	0.48148 7	0.49825 4	0.50336 8	0.32693 8	0.35683 4	0.36308 4
4E+08	26	0.96153	0.96184 9	0.96217 4	0.80776 8	0.81019 2	0.81195 4	0.65400 2	0.66055 4	0.66422	0.50051 6	0.51558 2	0.52064 7	0.35106 8	0.37772	0.38448 7
4E+08	27	0.96297 3	0.96318 7	0.96354 7	0.81482 5	0.81704 4	0.81856 3	0.66664 8	0.67289 6	0.67621 8	0.51901 7	0.53208 9	0.53717 4	0.37392 5	0.39772 3	0.40420 2
4E+08	28	0.96428 4	0.96450 5	0.96479 5	0.82134 8	0.82324 7	0.82497 3	0.67859 9	0.68390	0.68676 8	0.53621 2	0.54754	0.55215 2	0.39550 7	0.41707 5	0.42189 1
4E+08	29	0.96552 8	0.96573	0.96596 8	0.82756 9	0.82928 4	0.83084	0.68978 9	0.69436 1	0.69728 8	0.55194 4	0.56214 1	0.56603 9	0.416	0.43414 2	0.43978 6
4E+08	30	0.96667 8	0.96683 7	0.96709	0.83330 1	0.83477 6	0.83612 7	0.70009 4	0.70409 1	0.70678 8	0.56706 1	0.57576 5	0.57973 2	0.4346	0.45106 8	0.45663 5

### Mean Waiting Time vs. Offered Load (Hangup included)

Seed	Arrival Rate	(0.50,1)	(5.25,1)	(10.00,1)	(0.50,5)	(5.25,5)	(10.00,5)
400137271	1	0.432541	2.513186	3.71647	0.273998	0.612214	0.664184
400137271	2.8125	0.440585	3.522256	6.500271	0.293485	0.853104	1.009854
400137271	4.625	0.446756	4.126904	7.839841	0.305131	1.199313	1.634535
400137271	6.4375	0.452344	4.434954	8.451386	0.317285	1.668165	2.699274
400137271	8.25	0.457248	4.612863	8.790845	0.32876	2.183479	3.989996
400137271	10.0625	0.461504	4.72847	9.008089	0.33997	2.665122	5.023887
400137271	11.875	0.464881	4.809188	9.160069	0.350232	3.042522	5.786986
400137271	13.6875	0.46807	4.866978	9.270363	0.359574	3.340141	6.350637
400137271	15.5	0.470875	4.909358	9.351956	0.368925	3.559953	6.763991
400137271	17.3125	0.473093	4.945771	9.420024	0.376969	3.73504	7.107797
400137271	19.125	0.475223	4.974008	9.474302	0.384942	3.876179	7.381766
400137271	20.9375	0.47701	4.997856	9.519457	0.392034	3.995367	7.610212
400137271	22.75	0.478731	5.018081	9.557549	0.398438	4.094062	7.800806
400137271	24.5625	0.480113	5.035048	9.590589	0.403887	4.178897	7.961703
400137271	26.375	0.481256	5.049424	9.618047	0.409498	4.251963	8.09961
400137271	28.1875	0.482273	5.061938	9.641882	0.414285	4.315815	8.221663
400137271	30	0.483563	5.073084	9.662985	0.418631	4.371999	8.329315

### Mean Waiting Time vs. Offered Load (Hangup excluded)

Seed	Arrival Rate	(0.50,1)	(5.25,1)	(10.00,1)	(0.50,5)	(5.25,5)	(10.00,5)
400137271	0.1	0.430035	1.966593	2.421104	0	0	0
400137271	5.357895	0.528005	7.482443	15.35921	0.332558	1.454913	2.115227
400137271	10.61579	0.632899	11.03972	22.20315	0.400437	3.706833	7.223741
400137271	15.87368	0.736947	13.14312	26.192	0.473285	5.780974	11.23556
400137271	21.13158	0.832971	14.64723	29.06318	0.549774	7.273492	14.11843
400137271	26.38947	0.923953	15.81426	31.29093	0.624645	8.434711	16.33392
400137271	31.64737	1.005073	16.76726	33.10579	0.696417	9.389281	18.15099
400137271	36.90526	1.076913	17.57178	34.63315	0.763859	10.19753	19.68637
400137271	42.16316	1.141418	18.26435	35.96934	0.824296	10.8981	21.02071

400137271	47.42105	1.200027	18.88441	37.14256	0.880113	11.50917	22.18474
400137271	52.67895	1.25122	19.43786	38.19131	0.93222	12.07218	23.25556
400137271	57.93684	1.297545	19.93376	39.14246	0.979214	12.56695	24.20796
400137271	63.19474	1.34256	20.39991	40.02047	1.02376	13.02525	25.07524
400137271	68.45263	1.381749	20.81456	40.81123	1.062071	13.44184	25.87079
400137271	73.71053	1.41945	21.20131	41.55289	1.100384	13.83366	26.60848
400137271	78.96842	1.452802	21.55361	42.23183	1.134648	14.19988	27.30842
400137271	84.22632	1.485098	21.89745	42.86953	1.165658	14.53971	27.95008
400137271	89.48421	1.515648	22.21099	43.46912	1.196892	14.85609	28.55822
400137271	94.74211	1.542728	22.50983	44.03233	1.225157	15.15547	29.1266
400137271	100	1.569718	22.78836	44.57668	1.252918	15.44426	29.67939

### W(t) Experimental 1 trunk

Seed	t (min) (	t (sec)	(0.10 ,1)	(0.20 ,1)	(0.30 ,1)	(0.40 ,1)	(0.50 ,1)	(0.60 ,1)	(0.70 ,1)	(0.80 ,1)	(0.90 ,1)	(1.00 ,1)
40013 7271	0	0	0.89 9811	0.79 9886	0.70 0241	0.59 9988	0.50 0303	0.40 07	0.29 9827	0.20 0989	0.10 0289	0.00 1185
40013 7271	0.10 2041	6.12 2449	0.96 0114	0.86 6762	0.76 373	0.65 6507	0.54 862	0.44 0267	0.32 9892	0.22 1251	0.11 0464	0.00 1309
40013 7271	0.20 4082	12.2 449	0.98 4173	0.91 1597	0.81 407	0.70 5173	0.59 2504	0.47 7163	0.35 8542	0.24 0857	0.12 0515	0.00 1448
40013 7271	0.30 6122	18.3 6735	0.99 3671	0.94 1162	0.85 3536	0.74 706	0.63 2054	0.51 1786	0.38 6039	0.25 9962	0.13 05	0.00 1573
40013 7271	0.40 8163	24.4 898	0.99 7445	0.96 1046	0.88 4624	0.78 2784	0.66 7998	0.54 3877	0.41 2345	0.27 86	0.14 0504	0.00 1692
40013 7271	0.51 0204	30.6 1224	0.99 8968	0.97 4242	0.90 9131	0.81 3567	0.70 0163	0.57 3914	0.43 761	0.29 6811	0.15 0186	0.00 1811
40013 7271	0.61 2245	36.7 3469	0.99 9592	0.98 2832	0.92 8411	0.84 0059	0.72 9273	0.60 217	0.46 1871	0.31 4599	0.15 9746	0.00 1942
40013 7271	0.71 4286	42.8 5714	0.99 9834	0.98 8586	0.94 3775	0.86 2733	0.75 5671	0.62 8439	0.48 4961	0.33 1969	0.16 9265	0.00 2069
40013 7271	0.81 6327	48.9 7959	0.99 9938	0.99 243	0.95 5769	0.88 2229	0.77 9355	0.65 3062	0.50 7067	0.34 8966	0.17 8767	0.00 22
40013 7271	0.91 8367	55.1 0204	0.99 9974	0.99 5001	0.96 5355	0.89 8846	0.80 0853	0.67 5659	0.52 8336	0.36 539	0.18 8091	0.00 2334
40013 7271	1.02 0408	61.2 2449	0.99 999	0.99 668	0.97 2739	0.91 3123	0.82 0243	0.69 7039	0.54 8604	0.38 1454	0.19 7256	0.00 2459
40013 7271	1.12 2449	67.3 4694	0.99 9995	0.99 781	0.97 8532	0.92 5545	0.83 7742	0.71 6956	0.56 7991	0.39 7079	0.20 6302	0.00 2569
40013 7271	1.22 449	73.4 6939	0.99 9999	0.99 8535	0.98 3089	0.93 6221	0.85 3449	0.73 5651	0.58 6484	0.41 2462	0.21 538	0.00 2691
40013 7271	1.32 6531	79.5 9184	1	0.99 9017	0.98 6668	0.94 5344	0.86 7591	0.75 31	0.60 431	0.42 747	0.22 4294	0.00 281



40013 7271	1.42 8571	85.7 1429	1	0.99 9342	0.98 9556	0.95 3191	0.88 0475	0.76 937	0.62 1369	0.44 1988	0.23 3077	0.00 2922
40013 7271	1.53 0612	91.8 3673	1	0.99 9566	0.99 1807	0.95 9781	0.89 2134	0.78 4499	0.63 7697	0.45 6208	0.24 1845	0.00 3034
40013 7271	1.63 2653	97.9 5918	1	0.99 9712	0.99 3586	0.96 5379	0.90 2691	0.79 8549	0.65 3333	0.47 0065	0.25 0469	0.00 3158
40013 7271	1.73 4694	104. 0816	1	0.99 9811	0.99 4954	0.97 0263	0.91 2238	0.81 1896	0.66 8085	0.48 358	0.25 8936	0.00 3284
40013 7271	1.83 6735	110. 2041	1	0.99 9884	0.99 605	0.97 4461	0.92 0777	0.82 4258	0.68 2333	0.49 6615	0.26 7352	0.00 3403
40013 7271	1.93 8776	116. 3265	1	0.99 9919	0.99 6907	0.97 8121	0.92 8368	0.83 5825	0.69 5855	0.50 9511	0.27 5616	0.00 3523
40013 7271	2.04 0816	122. 449	1	0.99 9944	0.99 7553	0.98 1232	0.93 5299	0.84 6771	0.70 8743	0.52 1861	0.28 3807	0.00 3654
40013 7271	2.14 2857	128. 5714	1	0.99 9963	0.99 8044	0.98 3913	0.94 1635	0.85 7007	0.72 1313	0.53 393	0.29 1968	0.00 3766
40013 7271	2.24 4898	134. 6939	1	0.99 9975	0.99 8444	0.98 6243	0.94 7208	0.86 6401	0.73 3223	0.54 5672	0.29 9877	0.00 3906
40013 7271	2.34 6939	140. 8163	1	0.99 9981	0.99 8779	0.98 8136	0.95 2382	0.87 5256	0.74 4751	0.55 7048	0.30 7824	0.00 4023
40013 7271	2.44 898	146. 9388	1	0.99 9989	0.99 9032	0.98 9775	0.95 6993	0.88 3542	0.75 5674	0.56 8264	0.31 5637	0.00 414
40013 7271	2.55 102	153. 0612	1	0.99 9993	0.99 9236	0.99 1252	0.96 1149	0.89 112	0.76 6258	0.57 9225	0.32 3353	0.00 428
40013 7271	2.65 3061	159. 1837	1	0.99 9996	0.99 9399	0.99 2454	0.96 4888	0.89 8234	0.77 631	0.58 9793	0.33 1045	0.00 4409
40013 7271	2.75 5102	165. 3061	1	0.99 9998	0.99 9535	0.99 3536	0.96 8379	0.90 4979	0.78 6157	0.60 0099	0.33 8564	0.00 4535
40013 7271	2.85 7143	171. 4286	1	0.99 9999	0.99 9633	0.99 4432	0.97 1425	0.91 109	0.79 533	0.61 0255	0.34 6024	0.00 4655
40013 7271	2.95 9184	177. 551	1	1 9706	0.99 52	0.99 4203	0.97 6934	0.91 4206	0.80 4206	0.62 0051	0.35 3343	0.00 4762
40013 7271	3.06 1224	183. 6735	1	1 9766	0.99 5872	0.99 6681	0.97 2339	0.92 2683	0.81 9638	0.62 0728	0.36 4885	0.00
40013 7271	3.16 3265	189. 7959	1	1 9817	0.99 6461	0.99 8921	0.97 743	0.92 0725	0.82 9076	0.63 797	0.36 4994	0.00
40013 7271	3.26 5306	195. 9184	1	1 9859	0.99 6942	0.99 0942	0.98 2217	0.93 845	0.82 8113	0.64 4998	0.37 5121	0.00
40013 7271	3.36 7347	202. 0408	1	1 9891	0.99 7387	0.99 2759	0.98 6623	0.93 5844	0.83 6979	0.65 1951	0.38 5256	0.00
40013 7271	3.46 9388	208. 1633	1	1 9912	0.99 7745	0.99 4434	0.98 0786	0.94 2965	0.84 5591	0.66 8934	0.38 5392	0.00
40013 7271	3.57 1429	214. 2857	1	1 9924	0.99 8071	0.99 5888	0.98 4839	0.94 9832	0.84 4043	0.67 5793	0.39 5512	0.00
40013 7271	3.67 3469	220. 4082	1	1 9935	0.99 8354	0.99 7248	0.98 8493	0.94 6359	0.85 2324	0.68 2625	0.40 5637	0.00

40013 7271	3.77 551	226. 5306	1	1	0.99 9943	0.99 8589	0.98 8487	0.95 1862	0.86 2658	0.69 0331	0.40 9399	0.00 5768
40013 7271	3.87 7551	232. 6531	1	1	0.99 9956	0.99 8766	0.98 962	0.95 4968	0.86 8659	0.69 8189	0.41 6111	0.00 5898
40013 7271	3.97 9592	238. 7755	1	1	0.99 9964	0.99 893	0.99 0634	0.95 7969	0.87 4378	0.70 5836	0.42 2741	0.00 6031
40013 7271	4.08 1633	244. 898	1	1	0.99 9975	0.99 9085	0.99 1527	0.96 0765	0.87 9804	0.71 3313	0.42 929	0.00 6162
40013 7271	4.18 3673	251. 0204	1	1	0.99 9981	0.99 9206	0.99 2346	0.96 3395	0.88 4969	0.72 0514	0.43 5716	0.00 6274
40013 7271	4.28 5714	257. 1429	1	1	0.99 9987	0.99 9316	0.99 3093	0.96 5797	0.89 0002	0.72 7553	0.44 2097	0.00 6393
40013 7271	4.38 7755	263. 2653	1	1	0.99 999	0.99 9407	0.99 3738	0.96 8012	0.89 483	0.73 4523	0.44 844	0.00 6524
40013 7271	4.48 9796	269. 3878	1	1	0.99 9993	0.99 9494	0.99 4322	0.97 0083	0.89 9447	0.74 123	0.45 472	0.00 6645
40013 7271	4.59 1837	275. 5102	1	1	0.99 9994	0.99 9564	0.99 4863	0.97 2043	0.90 3799	0.74 7857	0.46 0883	0.00 6776
40013 7271	4.69 3878	281. 6327	1	1	0.99 9995	0.99 9626	0.99 5355	0.97 3875	0.90 797	0.75 4274	0.46 6879	0.00 6902
40013 7271	4.79 5918	287. 7551	1	1	0.99 9997	0.99 9672	0.99 5783	0.97 5575	0.91 2006	0.76 049	0.47 2893	0.00 7027
40013 7271	4.89 7959	293. 8776	1	1	0.99 9999	0.99 9716	0.99 6169	0.97 7207	0.91 5821	0.76 6611	0.47 884	0.00 7147
40013 7271	5	300	1	1	0.99 9999	0.99 9749	0.99 6516	0.97 8737	0.91 9547	0.77 2621	0.48 4604	0.00 727

#### W(t) Theoretical 1 trunk

Seed	t (min) (	t (sec)	(0.10 ,1)	(0.20 ,1)	(0.30 ,1)	(0.40 ,1)	(0.50 ,1)	(0.60 ,1)	(0.70 ,1)	(0.80 ,1)	(0.90 ,1)	(1.0 0,1)
400137 271	0	0	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.2	0.1	0
400137 271	0.10 2041	6.12 2449	0.96 0083	0.86 7026	0.76 3562	0.65 6769	0.54 8504	0.43 9459	0.32 9953	0.22 015	0.11 0146	0
400137 271	0.20 4082	12.2 449	0.98 4066	0.91 1589	0.81 3656	0.70 5481	0.59 2302	0.47 6323	0.35 8623	0.23 9793	0.12 0179	0
400137 271	0.30 6122	18.3 6735	0.99 364	0.94 1218	0.85 3138	0.74 728	0.63 1852	0.51 0763	0.38 6067	0.25 894	0.13 0097	0
400137 271	0.40 8163	24.4 898	0.99 7461	0.96 0918	0.88 4254	0.78 3147	0.66 7565	0.54 2937	0.41 2337	0.27 7606	0.13 9905	0
400137 271	0.51 0204	30.6 1224	0.99 8987	0.97 4015	0.90 8777	0.81 3923	0.69 9813	0.57 2996	0.43 7483	0.29 5801	0.14 9601	0
400137 271	0.61 2245	36.7 3469	0.99 9595	0.98 2724	0.92 8105	0.84 0332	0.72 8934	0.60 1078	0.46 1553	0.31 3538	0.15 9188	0

400137 271	0.71 4286	42.8 5714	0.99 9839	0.98 8513	0.94 3337	0.86 2992	0.75 5229	0.62 7313	0.48 4592	0.33 0829	0.16 8668	0
400137 271	0.81 6327	48.9 7959	0.99 9936	0.99 2363	0.95 5343	0.88 2437	0.77 8974	0.65 1823	0.50 6646	0.34 7683	0.17 804	0
400137 271	0.91 8367	55.1 0204	0.99 9974	0.99 4922	0.96 4804	0.89 9122	0.80 0415	0.67 4721	0.52 7757	0.36 4114	0.18 7307	0
400137 271	1.02 0408	61.2 2449	0.99 999	0.99 6624	0.97 2261	0.91 3439	0.81 9776	0.69 6113	0.54 7964	0.38 013	0.19 6469	0
400137 271	1.12 2449	67.3 4694	0.99 9996	0.99 7755	0.97 8138	0.92 5724	0.83 7259	0.71 6098	0.56 7306	0.39 5743	0.20 5528	0
400137 271	1.22 449	73.4 6939	0.99 9998	0.99 8508	0.98 277	0.93 6265	0.85 3046	0.73 4768	0.58 5821	0.41 0963	0.21 4484	0
400137 271	1.32 6531	79.5 9184	0.99 9999	0.99 9008	0.98 6421	0.94 5311	0.86 7302	0.75 2211	0.60 3543	0.42 5799	0.22 334	0
400137 271	1.42 8571	85.7 1429	1	0.99 934	0.98 9298	0.95 3072	0.88 0174	0.76 8507	0.62 0507	0.44 0262	0.23 2096	0
400137 271	1.53 0612	91.8 3673	1	0.99 9561	0.99 1565	0.95 9732	0.89 1798	0.78 3731	0.63 6746	0.45 436	0.24 0753	0
400137 271	1.63 2653	97.9 5918	1	0.99 9708	0.99 3352	0.96 5447	0.90 2295	0.79 7954	0.65 2289	0.46 8104	0.24 9313	0
400137 271	1.73 4694	104. 0816	1	0.99 9806	0.99 4761	0.97 0351	0.91 1773	0.81 1242	0.66 7167	0.48 1501	0.25 7776	0
400137 271	1.83 6735	110. 2041	1	0.99 9871	0.99 5871	0.97 4559	0.92 0332	0.82 3655	0.68 1409	0.49 4561	0.26 6144	0
400137 271	1.93 8776	116. 3265	1	0.99 9914	0.99 6746	0.97 817	0.92 806	0.83 5253	0.69 5041	0.50 7291	0.27 4417	0
400137 271	2.04 0816	122. 449	1	0.99 9943	0.99 7435	0.98 1268	0.93 5039	0.84 6087	0.70 809	0.51 9702	0.28 2597	0
400137 271	2.14 2857	128. 5714	1	0.99 9962	0.99 7979	0.98 3926	0.94 134	0.85 6209	0.72 0581	0.53 1799	0.29 0685	0
400137 271	2.24 4898	134. 6939	1	0.99 9975	0.99 8407	0.98 6208	0.94 7031	0.86 5666	0.73 2537	0.54 3592	0.29 8682	0
400137 271	2.34 6939	140. 8163	1	0.99 9983	0.99 8744	0.98 8165	0.95 2169	0.87 45	0.74 3982	0.55 5088	0.30 6588	0
400137 271	2.44 898	146. 9388	1	0.99 9989	0.99 901	0.98 9845	0.95 6809	0.88 2754	0.75 4936	0.56 6294	0.31 4406	0
400137 271	2.55 102	153. 0612	1	0.99 9993	0.99 922	0.99 1286	0.96 0999	0.89 0464	0.76 5423	0.57 7218	0.32 2135	0
400137 271	2.65 3061	159. 1837	1	0.99 9995	0.99 9385	0.99 2523	0.96 4782	0.89 7668	0.77 546	0.58 7867	0.32 9777	0
400137 271	2.75 5102	165. 3061	1	0.99 9997	0.99 9516	0.99 3584	0.96 8199	0.90 4398	0.78 5068	0.59 8248	0.33 7333	0
400137 271	2.85 7143	171. 4286	1	0.99 9998	0.99 9618	0.99 4494	0.97 1284	0.91 0685	0.79 4265	0.60 8367	0.34 4804	0
400137 271	2.95 9184	177. 551	1	0.99 9999	0.99 9699	0.99 5276	0.97 4069	0.91 6559	0.80 3068	0.61 8231	0.35 2191	0

400137 271	3.06 1224	183. 6735	1	0.99 9999	0.99 9763	0.99 5946	0.97 6585	0.92 2046	0.81 1495	0.62 7847	0.35 9494	0
400137 271	3.16 3265	189. 7959	1	0.99 9999	0.99 9813	0.99 6522	0.97 8856	0.92 7173	0.81 9561	0.63 722	0.36 6715	0
400137 271	3.26 5306	195. 9184	1	1	0.99 9853	0.99 7015	0.98 0907	0.93 1963	0.82 7281	0.64 6358	0.37 3854	0
400137 271	3.36 7347	202. 0408	1	1	0.99 9884	0.99 7439	0.98 276	0.93 6437	0.83 4672	0.65 5265	0.38 0913	0
400137 271	3.46 9388	208. 1633	1	1	0.99 9909	0.99 7802	0.98 4432	0.94 0617	0.84 1746	0.66 3948	0.38 7893	0
400137 271	3.57 1429	214. 2857	1	1	0.99 9928	0.99 8114	0.98 5942	0.94 4523	0.84 8518	0.67 2413	0.39 4794	0
400137 271	3.67 3469	220. 4082	1	1	0.99 9943	0.99 8382	0.98 7306	0.94 8171	0.85 5	0.68 0664	0.40 1617	0
400137 271	3.77 551	226. 5306	1	1	0.99 9955	0.99 8612	0.98 8537	0.95 158	0.86 1204	0.68 8707	0.40 8363	0
400137 271	3.87 7551	232. 6531	1	1	0.99 9965	0.99 8809	0.98 9649	0.95 4764	0.86 7143	0.69 6548	0.41 5033	0
400137 271	3.97 9592	238. 7755	1	1	0.99 9972	0.99 8978	0.99 0653	0.95 7739	0.87 2828	0.70 4191	0.42 1628	0
400137 271	4.08 1633	244. 898	1	1	0.99 9978	0.99 9123	0.99 156	0.96 0518	0.87 827	0.71 1642	0.42 8148	0
400137 271	4.18 3673	251. 0204	1	1	0.99 9983	0.99 9247	0.99 2379	0.96 3115	0.88 3478	0.71 8905	0.43 4595	0
400137 271	4.28 5714	257. 1429	1	1	0.99 9986	0.99 9354	0.99 3118	0.96 554	0.88 8464	0.72 5985	0.44 0969	0
400137 271	4.38 7755	263. 2653	1	1	0.99 9989	0.99 9446	0.99 3786	0.96 7807	0.89 3237	0.73 2887	0.44 7272	0
400137 271	4.48 9796	269. 3878	1	1	0.99 9992	0.99 9524	0.99 4389	0.96 9924	0.89 7805	0.73 9615	0.45 3503	0
400137 271	4.59 1837	275. 5102	1	1	0.99 9993	0.99 9592	0.99 4933	0.97 1902	0.90 2178	0.74 6173	0.45 9664	0
400137 271	4.69 3878	281. 6327	1	1	0.99 9995	0.99 965	0.99 5424	0.97 375	0.90 6364	0.75 2566	0.46 5756	0
400137 271	4.79 5918	287. 7551	1	1	0.99 9996	0.99 97	0.99 5868	0.97 5476	0.91 037	0.75 8799	0.47 1779	0
400137 271	4.89 7959	293. 8776	1	1	0.99 9997	0.99 9742	0.99 6269	0.97 7089	0.91 4205	0.76 4874	0.47 7734	0
400137 271	5	300	1	1	0.99 9997	0.99 9779	0.99 6631	0.97 8596	0.91 7877	0.77 0796	0.48 3622	0

#### W(t) Experimental 2 trunks

Seed	t (min)	t (sec)	(0.10 ,2)	(0.20 ,2)	(0.30 ,2)	(0.40 ,2)	(0.50 ,2)	(0.60 ,2)	(0.70 ,2)	(0.80 ,2)	(0.90 ,2)	(1.00 ,2)
------	------------	------------	--------------	--------------	--------------	--------------	--------------	--------------	--------------	--------------	--------------	--------------

40013 7271	0 0	0 0	0.99 5252	0.98 1752	0.96 049	0.93 3485	0.89 954	0.86 1341	0.81 853	0.77 16	0.72 1682	0.66 8276
40013 7271	0.10 2041	6.12 2449	0.99 9297	0.99 2756	0.97 7819	0.95 5889	0.92 6143	0.89 0724	0.85 0034	0.80 4118	0.75 4444	0.70 0545
40013 7271	0.20 4082	12.2 449	0.99 9905	0.99 7106	0.98 7549	0.97 0647	0.94 5663	0.91 3854	0.87 5884	0.83 2111	0.78 3382	0.72 979
40013 7271	0.30 6122	18.3 6735	0.99 9985	0.99 8893	0.99 2997	0.98 0468	0.96 0082	0.93 2023	0.89 744	0.85 6048	0.80 9008	0.75 6257
40013 7271	0.40 8163	24.4 898	0.99 9998	0.99 9563	0.99 6086	0.98 702	0.97 0642	0.94 6579	0.91 5053	0.87 6504	0.83 1388	0.78 0121
40013 7271	0.51 0204	30.6 1224	1 983	0.99 983	0.99 7806	0.99 1416	0.97 8351	0.95 7886	0.92 9675	0.89 4062	0.85 1123	0.80 1524
40013 7271	0.61 2245	36.7 3469	1 9935	0.99 9935	0.99 8792	0.99 4287	0.98 4083	0.96 6753	0.94 198	0.90 9118	0.86 8598	0.82 0833
40013 7271	0.71 4286	42.8 5714	1 9974	0.99 9974	0.99 9336	0.99 6234	0.98 8293	0.97 3759	0.95 1955	0.92 212	0.88 4025	0.83 8282
40013 7271	0.81 6327	48.9 7959	1 9989	0.99 9989	0.99 9635	0.99 755	0.99 134	0.97 923	0.96 0149	0.93 3283	0.89 7774	0.85 3923
40013 7271	0.91 8367	55.1 0204	1 9997	0.99 9997	0.99 9806	0.99 838	0.99 3651	0.98 3664	0.96 7087	0.94 2713	0.90 9806	0.86 8045
40013 7271	1.02 0408	61.2 2449	1 9999	0.99 9999	0.99 9895	0.99 8928	0.99 534	0.98 7183	0.97 2715	0.95 0878	0.92 0393	0.88 0939
40013 7271	1.12 2449	67.3 4694	1 9999	0.99 9999	0.99 9937	0.99 9302	0.99 6635	0.98 9906	0.97 7473	0.95 7827	0.92 9688	0.89 2516
40013 7271	1.22 449	73.4 6939	1 9962	1 9962	0.99 9962	0.99 9552	0.99 7536	0.99 1998	0.98 1409	0.96 3787	0.93 7976	0.90 2992
40013 7271	1.32 6531	79.5 9184	1 9978	1 9978	0.99 9978	0.99 9709	0.99 8197	0.99 3694	0.98 4645	0.96 8937	0.94 5225	0.91 2368
40013 7271	1.42 8571	85.7 1429	1 9988	1 9988	0.99 9988	0.99 9813	0.99 869	0.99 504	0.98 7295	0.97 3376	0.95 1512	0.92 1006
40013 7271	1.53 0612	91.8 3673	1 9991	1 9991	0.99 9991	0.99 9874	0.99 9037	0.99 6109	0.98 947	0.97 7198	0.95 7295	0.92 8766
40013 7271	1.63 2653	97.9 5918	1 9995	1 9995	0.99 9995	0.99 9919	0.99 9299	0.99 6944	0.99 1248	0.98 04	0.96 2348	0.93 5707
40013 7271	1.73 4694	104. 0816	1 9998	1 9998	0.99 9998	0.99 9957	0.99 9487	0.99 7617	0.99 2756	0.98 3238	0.96 6823	0.94 1898
40013 7271	1.83 6735	110. 2041	1 9999	1 9999	0.99 9999	0.99 9975	0.99 9624	0.99 814	0.99 3981	0.98 5649	0.97 071	0.94 7556
40013 7271	1.93 8776	116. 3265	1 9983	1 9983	1 9983	0.99 9983	0.99 9726	0.99 8547	0.99 5053	0.98 7661	0.97 4132	0.95 2664
40013 7271	2.04 0816	122. 449	1 9989	1 9989	1 9989	0.99 9989	0.99 9803	0.99 886	0.99 5923	0.98 9394	0.97 7129	0.95 731
40013 7271	2.14 2857	128. 5714	1 9994	1 9994	1 9994	0.99 9994	0.99 9856	0.99 9096	0.99 6623	0.99 0924	0.97 9794	0.96 1536
40013 7271	2.24 4898	134. 6939	1 9994	1 9994	1 9994	0.99 9994	0.99 9898	0.99 9295	0.99 7208	0.99 2233	0.98 2125	0.96 5306

40013 7271	2.34 6939	140. 8163	1	1	1	0.99 9998	0.99 9928	0.99 944	0.99 7695	0.99 3354	0.98 4172	0.96 8715
40013 7271	2.44 898	146. 9388	1	1	1	1	0.99 9947	0.99 9566	0.99 809	0.99 4313	0.98 6053	0.97 1789
40013 7271	2.55 102	153. 0612	1	1	1	1	0.99 9965	0.99 9657	0.99 842	0.99 5134	0.98 7712	0.97 4587
40013 7271	2.65 3061	159. 1837	1	1	1	1	0.99 9978	0.99 9738	0.99 8701	0.99 5827	0.98 912	0.97 7093
40013 7271	2.75 5102	165. 3061	1	1	1	1	0.99 9982	0.99 9793	0.99 8934	0.99 6427	0.99 0402	0.97 935
40013 7271	2.85 7143	171. 4286	1	1	1	1	0.99 9988	0.99 9845	0.99 9112	0.99 6912	0.99 1583	0.98 1364
40013 7271	2.95 9184	177. 551	1	1	1	1	0.99 9993	0.99 9885	0.99 9268	0.99 7363	0.99 2614	0.98 3188
40013 7271	3.06 1224	183. 6735	1	1	1	1	0.99 9995	0.99 9911	0.99 94	0.99 7733	0.99 3529	0.98 4795
40013 7271	3.16 3265	189. 7959	1	1	1	1	0.99 9997	0.99 9927	0.99 9488	0.99 8059	0.99 4303	0.98 6268
40013 7271	3.26 5306	195. 9184	1	1	1	1	0.99 9998	0.99 9943	0.99 9571	0.99 8343	0.99 4988	0.98 7619
40013 7271	3.36 7347	202. 0408	1	1	1	1	0.99 9999	0.99 9956	0.99 9648	0.99 8594	0.99 5565	0.98 8844
40013 7271	3.46 9388	208. 1633	1	1	1	1	1	0.99 9967	0.99 9707	0.99 8788	0.99 6082	0.98 9931
40013 7271	3.57 1429	214. 2857	1	1	1	1	1	0.99 9977	0.99 9771	0.99 8958	0.99 6552	0.99 0894
40013 7271	3.67 3469	220. 4082	1	1	1	1	1	0.99 9982	0.99 9807	0.99 9112	0.99 6953	0.99 1816
40013 7271	3.77 551	226. 5306	1	1	1	1	1	0.99 9985	0.99 9849	0.99 9245	0.99 7316	0.99 2604
40013 7271	3.87 7551	232. 6531	1	1	1	1	1	0.99 9987	0.99 9875	0.99 9357	0.99 7639	0.99 3327
40013 7271	3.97 9592	238. 7755	1	1	1	1	1	0.99 9991	0.99 9899	0.99 9449	0.99 7928	0.99 4024
40013 7271	4.08 1633	244. 898	1	1	1	1	1	0.99 9995	0.99 9915	0.99 9526	0.99 8173	0.99 4628
40013 7271	4.18 3673	251. 0204	1	1	1	1	1	0.99 9997	0.99 9934	0.99 959	0.99 8378	0.99 5167
40013 7271	4.28 5714	257. 1429	1	1	1	1	1	0.99 9998	0.99 9947	0.99 9636	0.99 8579	0.99 5675
40013 7271	4.38 7755	263. 2653	1	1	1	1	1	0.99 9999	0.99 9958	0.99 9689	0.99 8748	0.99 6109
40013 7271	4.48 9796	269. 3878	1	1	1	1	1	0.99 9999	0.99 9968	0.99 9729	0.99 8901	0.99 6485
40013 7271	4.59 1837	275. 5102	1	1	1	1	1	1	0.99 9973	0.99 9773	0.99 9045	0.99 6834

40013 7271	4.69 3878	281. 6327	1	1	1	1	1	1	0.99 9978	0.99 9805	0.99 9162	0.99 7153
40013 7271	4.79 5918	287. 7551	1	1	1	1	1	1	0.99 998	0.99 9837	0.99 9258	0.99 7441
40013 7271	4.89 7959	293. 8776	1	1	1	1	1	1	0.99 9985	0.99 9862	0.99 9357	0.99 769
40013 7271	5	300	1	1	1	1	1	1	0.99 9988	0.99 9881	0.99 944	0.99 7916

#### W(t) Theoretical 2 trunks

Seed	t (min) (	t (sec)	(0.10 ,2)	(0.20 ,2)	(0.30 ,2)	(0.40 ,2)	(0.50 ,2)	(0.60 ,2)	(0.70 ,2)	(0.80 ,2)	(0.90 ,2)	(1.00 ,2)
40013 7271	0	0	0.99 5238	0.98 1818	0.96 087	0.93 3333	0.9	0.86 1538	0.81 8519	0.77 1429	0.72 069	0.66 6667
40013 7271	0.10 2041	6.12 2449	0.99 9315	0.99 2742	0.97 8052	0.95 5675	0.92 637	0.89 0875	0.84 9848	0.80 3868	0.75 344	0.69 9002
40013 7271	0.20 4082	12.2 449	0.99 9901	0.99 7103	0.98 769	0.97 053	0.94 5787	0.91 3995	0.87 5769	0.83 1704	0.78 235	0.72 8201
40013 7271	0.30 6122	18.3 6735	0.99 9986	0.99 8844	0.99 3095	0.98 0406	0.96 0083	0.93 2217	0.89 7215	0.85 5589	0.80 787	0.75 4568
40013 7271	0.40 8163	24.4 898	0.99 9998	0.99 9538	0.99 6127	0.98 6973	0.97 0609	0.94 6579	0.91 4959	0.87 6084	0.83 0398	0.77 8377
40013 7271	0.51 0204	30.6 1224	1	0.99 9816	0.99 7828	0.99 1338	0.97 836	0.95 7897	0.92 964	0.89 3671	0.85 0284	0.79 9876
40013 7271	0.61 2245	36.7 3469	1	0.99 9926	0.99 8782	0.99 4241	0.98 4066	0.96 6818	0.94 1786	0.90 8761	0.86 7839	0.81 9289
40013 7271	0.71 4286	42.8 5714	1	0.99 9971	0.99 9317	0.99 6171	0.98 8268	0.97 3848	0.95 1835	0.92 171	0.88 3335	0.83 6819
40013 7271	0.81 6327	48.9 7959	1	0.99 9988	0.99 9617	0.99 7454	0.99 1362	0.97 9389	0.96 015	0.93 2821	0.89 7014	0.85 2649
40013 7271	0.91 8367	55.1 0204	1	0.99 9995	0.99 9785	0.99 8307	0.99 364	0.98 3756	0.96 7029	0.94 2355	0.90 909	0.86 6943
40013 7271	1.02 0408	61.2 2449	1	0.99 9998	0.99 9879	0.99 8875	0.99 5317	0.98 7198	0.97 2721	0.95 0536	0.91 9749	0.87 9851
40013 7271	1.12 2449	67.3 4694	1	0.99 9999	0.99 9932	0.99 9252	0.99 6552	0.98 991	0.97 743	0.95 7556	0.92 9159	0.89 1506
40013 7271	1.22 449	73.4 6939	1	1	0.99 9962	0.99 9503	0.99 7461	0.99 2048	0.98 1327	0.96 358	0.93 7465	0.90 2031
40013 7271	1.32 6531	79.5 9184	1	1	0.99 9979	0.99 9669	0.99 8131	0.99 3733	0.98 455	0.96 8749	0.94 4797	0.91 1535
40013 7271	1.42 8571	85.7 1429	1	1	0.99 9988	0.99 978	0.99 8624	0.99 5061	0.98 7217	0.97 3184	0.95 127	0.92 0116
40013 7271	1.53 0612	91.8 3673	1	1	0.99 9993	0.99 9854	0.99 8987	0.99 6107	0.98 9424	0.97 699	0.95 6984	0.92 7866

40013 7271	1.63 2653	97.9 5918	1	1	0.99 9996	0.99 9903	0.99 9254	0.99 6932	0.99 125	0.98 0256	0.96 2028	0.93 4863
40013 7271	1.73 4694	104. 0816	1	1	0.99 9998	0.99 9935	0.99 9451	0.99 7582	0.99 276	0.98 3058	0.96 648	0.94 1182
40013 7271	1.83 6735	110. 2041	1	1	0.99 9999	0.99 9957	0.99 9595	0.99 8094	0.99 401	0.98 5462	0.97 041	0.94 6888
40013 7271	1.93 8776	116. 3265	1	1	0.99 9999	0.99 9971	0.99 9702	0.99 8498	0.99 5044	0.98 7526	0.97 388	0.95 204
40013 7271	2.04 0816	122. 449	1	1	1	0.99 9981	0.99 9781	0.99 8816	0.99 59	0.98 9296	0.97 6942	0.95 6692
40013 7271	2.14 2857	128. 5714	1	1	1	0.99 9987	0.99 9839	0.99 9067	0.99 6608	0.99 0815	0.97 9646	0.96 0894
40013 7271	2.24 4898	134. 6939	1	1	1	0.99 9992	0.99 9881	0.99 9265	0.99 7193	0.99 2119	0.98 2033	0.96 4687
40013 7271	2.34 6939	140. 8163	1	1	1	0.99 9994	0.99 9912	0.99 9421	0.99 7678	0.99 3237	0.98 4139	0.96 8113
40013 7271	2.44 898	146. 9388	1	1	1	0.99 9996	0.99 9936	0.99 9543	0.99 8079	0.99 4197	0.98 5999	0.97 1206
40013 7271	2.55 102	153. 0612	1	1	1	0.99 9998	0.99 9953	0.99 964	0.99 841	0.99 5021	0.98 7641	0.97 3999
40013 7271	2.65 3061	159. 1837	1	1	1	0.99 9998	0.99 9965	0.99 9716	0.99 8685	0.99 5727	0.98 909	0.97 6522
40013 7271	2.75 5102	165. 3061	1	1	1	0.99 9999	0.99 9974	0.99 9776	0.99 8912	0.99 6334	0.99 0369	0.97 8799
40013 7271	2.85 7143	171. 4286	1	1	1	0.99 9999	0.99 9981	0.99 9824	0.99 91	0.99 6854	0.99 1498	0.98 0856
40013 7271	2.95 9184	177. 551	1	1	1	1	0.99 9986	0.99 9861	0.99 9255	0.99 73	0.99 2495	0.98 2713
40013 7271	3.06 1224	183. 6735	1	1	1	1	0.99 999	0.99 9891	0.99 9384	0.99 7684	0.99 3375	0.98 439
40013 7271	3.16 3265	189. 7959	1	1	1	1	0.99 9992	0.99 9914	0.99 949	0.99 8012	0.99 4152	0.98 5904
40013 7271	3.26 5306	195. 9184	1	1	1	1	0.99 9994	0.99 9932	0.99 9578	0.99 8294	0.99 4838	0.98 7272
40013 7271	3.36 7347	202. 0408	1	1	1	1	0.99 9996	0.99 9946	0.99 9651	0.99 8537	0.99 5443	0.98 8506
40013 7271	3.46 9388	208. 1633	1	1	1	1	0.99 9997	0.99 9958	0.99 9711	0.99 8744	0.99 5977	0.98 9621
40013 7271	3.57 1429	214. 2857	1	1	1	1	0.99 9998	0.99 9967	0.99 9761	0.99 8922	0.99 6449	0.99 0628
40013 7271	3.67 3469	220. 4082	1	1	1	1	0.99 9998	0.99 9974	0.99 9802	0.99 9075	0.99 6865	0.99 1537
40013 7271	3.77 551	226. 5306	1	1	1	1	0.99 9999	0.99 9979	0.99 9836	0.99 9207	0.99 7233	0.99 2358
40013 7271	3.87 7551	232. 6531	1	1	1	1	0.99 9999	0.99 9984	0.99 9865	0.99 9319	0.99 7557	0.99 31



40013 7271	3.97 9592	238. 7755	1	1	1	1	0.99 9999	0.99 9987	0.99 9888	0.99 9416	0.99 7844	0.99 3769
40013 7271	4.08 1633	244. 898	1	1	1	1	1	0.99 999	0.99 9907	0.99 9499	0.99 8097	0.99 4373
40013 7271	4.18 3673	251. 0204	1	1	1	1	1	0.99 9992	0.99 9923	0.99 957	0.99 832	0.99 4919
40013 7271	4.28 5714	257. 1429	1	1	1	1	1	0.99 9994	0.99 9937	0.99 9631	0.99 8517	0.99 5412
40013 7271	4.38 7755	263. 2653	1	1	1	1	1	0.99 9995	0.99 9948	0.99 9683	0.99 8691	0.99 5857
40013 7271	4.48 9796	269. 3878	1	1	1	1	1	0.99 9996	0.99 9957	0.99 9728	0.99 8844	0.99 6259
40013 7271	4.59 1837	275. 5102	1	1	1	1	1	0.99 9997	0.99 9964	0.99 9767	0.99 898	0.99 6622
40013 7271	4.69 3878	281. 6327	1	1	1	1	1	0.99 9998	0.99 997	0.99 98	0.99 9099	0.99 695
40013 7271	4.79 5918	287. 7551	1	1	1	1	1	0.99 9998	0.99 9975	0.99 9828	0.99 9205	0.99 7246
40013 7271	4.89 7959	293. 8776	1	1	1	1	1	0.99 9998	0.99 998	0.99 9853	0.99 9298	0.99 7513
40013 7271	5	300	1	1	1	1	1	0.99 9999	0.99 9983	0.99 9874	0.99 938	0.99 7754