

# TTK4215 System Identification and Adaptive Control

## Solution 1

### Non-parametric Methods

#### Problem 1 (Impulse-Response Analysis)

a) Since  $u(t) = 0$  for  $t \neq 0$ , the only non-zero term in the sum is for  $k = t$ . Thus, we have

$$y(t) = \sum_{k=1}^{\infty} g_0(k)u(t-k) + v(t) = g_0(k)u(t-k)|_{k=t} + v(t) = g_0(t)u(0) + v(t) = ag_0(t) + v(t). \quad (1)$$

b) An estimate can be formed by removing the uncertain part  $v(t)$ . That is

$$\hat{g}_0(t) = \frac{y(t)}{a}. \quad (2)$$

c) The resulting estimation error is

$$g_0(t) - \hat{g}_0(t) = \frac{y(t) - v(t)}{a} - \frac{y(t)}{a} = -\frac{v(t)}{a}. \quad (3)$$

In order to obtain an estimation error that is small,  $a$  has to be large compared to  $v(t)$ . This may be impossible due to saturation in the input (a valve, for instance, restricts  $u(t)$  to take values in  $[0, 1]$ ). Furthermore, since systems in practice are nonlinear, large perturbations will give nonlinear effects, and possibly as severe as instability.

#### Problem 2 (Step-Response Analysis)

a) In this case the terms of the sum are non-zero when  $k \leq t$ , so we have

$$y(t) = \sum_{k=1}^{\infty} g_0(k)u(t-k) + v(t) = a \sum_{k=1}^t g_0(k) + v(t). \quad (4)$$

b) From a), we have that

$$\begin{aligned} y(t) - y(t-1) &= a \sum_{k=1}^t g_0(k) + v(t) - a \sum_{k=1}^{t-1} g_0(k) - v(t-1) \\ &= ag_0(t) + v(t) - v(t-1). \end{aligned} \quad (5)$$

Removing the uncertain terms  $v(t)$  and  $v(t-1)$ , an estimate can be found using

$$y(t) - y(t-1) = a\hat{g}_0(t),$$

giving

$$\hat{g}_0(t) = \frac{y(t) - y(t-1)}{a}.$$

c) The estimation error is obtained as follows.

$$\begin{aligned} g_0(t) - \hat{g}_0(t) &= \frac{y(t) - y(t-1)}{a} - \frac{v(t) - v(t-1)}{a} - \frac{y(t) - y(t-1)}{a} \\ &= \frac{v(t-1) - v(t)}{a}. \end{aligned} \quad (6)$$

Again,  $a$  has to be large compared to the noise, and one will have the same practical problems as for the impulse-response analysis.

d) A first order system with time delay has transfer function

$$h(s) = \frac{k}{Ts + 1} e^{-\tau s},$$

where  $k$  is the process gain,  $T$  is the time constant, and  $\tau$  is the time delay. These parameters can be read directly from a single step response graph.

### Problem 3 (Correlation Analysis)

a) A stationary signal  $\{v(t)\}$  has  $Ev(t) = c$ , for some constant  $c$ , so  $m_s(t)$  can be taken as  $c$  in  $i)$ . Since  $Ev(t)v(t-\tau) = R_v(\tau)$ ,  $\check{R}_v(t, r)$  in the sum in  $ii)$  only depends on  $t - r = \tau$  and thus is independent of the summation variable  $t$ .

b) We have

$$\bar{E}s(t)s(t-\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{t=1}^N Es(t)s(t-\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{t=1}^N \check{R}_s(t, t-\tau) = R_s(\tau). \quad (7)$$

c) We have that

$$\begin{aligned} R_{yu}(\tau) &= \bar{E}y(t)u(t-\tau) = \bar{E}[G_0(q)u(t) + v(t)]u(t-\tau) \\ &= \bar{E}G_0(q)u(t)u(t-\tau) + \bar{E}v(t)u(t-\tau). \end{aligned}$$

Since  $v$  and  $u$  are uncorrelated, the last term is identically zero. Therefore, we can view the system as  $y(t) = G_0(q)u(t)$  for the purpose of this computation and exploit the fact that

$$\Phi_{yu}(\omega) = G_0(e^{i\omega})\Phi_u(\omega).$$

We have

$$\begin{aligned} R_{yu}(\tau) &= \frac{1}{2\pi} \int_{-\pi}^{\pi} \Phi_{yu}(\omega) e^{i\tau\omega} d\omega = \frac{1}{2\pi} \int_{-\pi}^{\pi} G_0(e^{i\omega}) \Phi_u(\omega) e^{i\tau\omega} d\omega \\ &= \frac{1}{2\pi} \int_{-\pi}^{\pi} \sum_{k=1}^{\infty} g_0(k) e^{-ik\omega} \Phi_u(\omega) e^{i\tau\omega} d\omega = \frac{1}{2\pi} \int_{-\pi}^{\pi} \sum_{k=1}^{\infty} g_0(k) \Phi_u(\omega) e^{i(\tau-k)\omega} d\omega \\ &= \sum_{k=1}^{\infty} g_0(k) \left( \frac{1}{2\pi} \int_{-\pi}^{\pi} \Phi_u(\omega) e^{i(\tau-k)\omega} d\omega \right) = \sum_{k=1}^{\infty} g_0(k) R_u(\tau - k). \end{aligned} \quad (8)$$

d) We can replace  $R_u(\tau)$  and  $R_{yu}(\tau)$  with their estimates to obtain

$$\hat{R}_{yu}^N(\tau) = \sum_{k=1}^{\infty} g_0(k) \hat{R}_u^N(\tau - k). \quad (9)$$

Next, we have to truncate the sum, which we can since the coefficients  $g_0(k)$  decay quickly, to obtain

$$\hat{R}_{yu}^N(\tau) = \sum_{k=1}^M g_0(k) \hat{R}_u^N(\tau - k). \quad (10)$$

Equation (10) can be solved for the coefficients  $g_0(k)$ .

#### **Problem 4 (Fourier Analysis)**

a) Since  $\rho_1(N)$  approaches zero for large  $N$ ,  $\hat{G}_N(e^{i\omega})$  is an unbiased estimate of  $G_0(e^{i\omega})$ . Since  $\rho_2(N)$  approaches zero for large  $N$ , the variance is given by the noise/signal ratio, which does not decrease with increasing  $N$ , and the estimates at different frequencies are uncorrelated (for large  $N$ ).