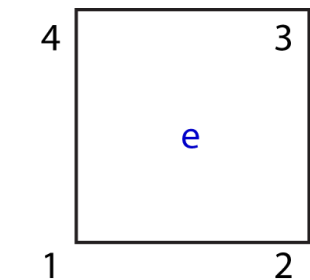
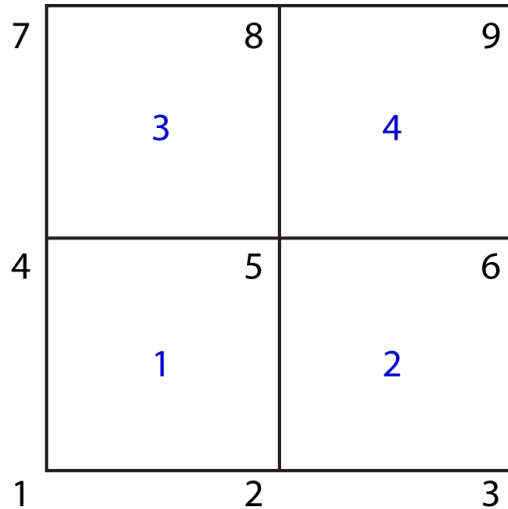


Multidimensional elastic solutions: FEM Implementation

MAE 404/598 – Oswald

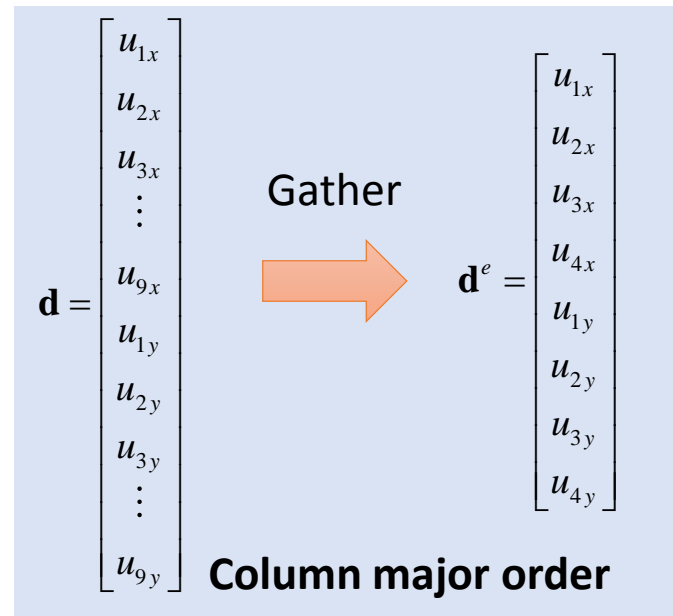
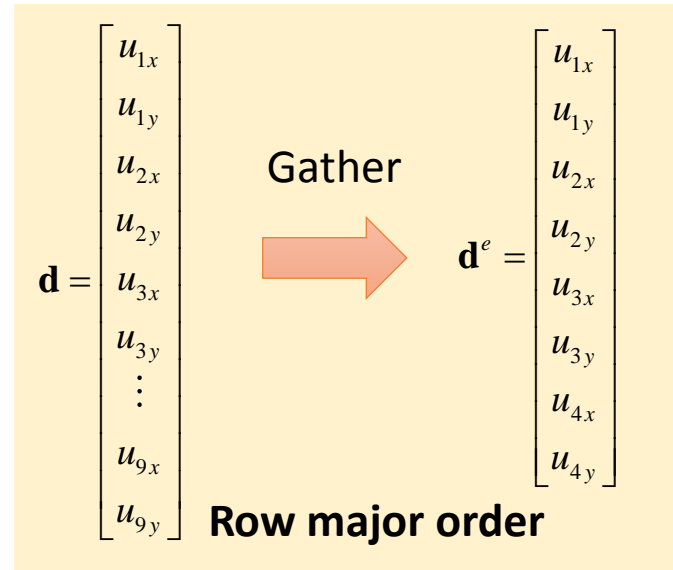
3/26/2015

Organization of nodal degrees of freedom



$$\mathbf{d} = \begin{bmatrix} u_{1x} & u_{1y} \\ u_{1y} & u_{2y} \\ u_{2x} & u_{3y} \\ \vdots & \vdots \\ u_{9x} & u_{9y} \end{bmatrix}$$

Nodal displacement matrix



Weak form and discretization

$$\int_{\Omega} \nabla_s \mathbf{w} : \mathbf{C}^e : \nabla_s \mathbf{u} d\Omega = \int_{\Omega} \mathbf{w} \cdot \mathbf{b} d\Omega + \int_{\Gamma_t} \mathbf{w} \cdot \bar{\mathbf{t}} d\Gamma$$

$$\nabla_s = \begin{bmatrix} \frac{\partial}{\partial x} & 0 \\ 0 & \frac{\partial}{\partial y} \\ \frac{\partial}{\partial y} & \frac{\partial}{\partial x} \end{bmatrix}$$

$$\mathbf{w} = N_I \mathbf{w}_I \quad \nabla_s \mathbf{w} = \mathbf{B}_I \mathbf{w}_I$$

$$\mathbf{u} = N_I \mathbf{u}_I \quad \nabla_s \mathbf{u} = \mathbf{B}_I \mathbf{u}_I$$

Symmetric gradient operator

$$\mathbf{B}_I = \begin{bmatrix} \frac{\partial N_I}{\partial x} & 0 \\ 0 & \frac{\partial N_I}{\partial y} \\ \frac{\partial N_I}{\partial y} & \frac{\partial N_I}{\partial x} \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} \frac{\partial N_1}{\partial x} & 0 & \frac{\partial N_2}{\partial x} & 0 & \frac{\partial N_3}{\partial x} & 0 & \frac{\partial N_4}{\partial x} & 0 \\ 0 & \frac{\partial N_1}{\partial y} & 0 & \frac{\partial N_2}{\partial y} & 0 & \frac{\partial N_3}{\partial y} & 0 & \frac{\partial N_4}{\partial y} \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_1}{\partial x} & \frac{\partial N_2}{\partial y} & \frac{\partial N_2}{\partial x} & \frac{\partial N_3}{\partial y} & \frac{\partial N_3}{\partial x} & \frac{\partial N_4}{\partial y} & \frac{\partial N_4}{\partial x} \end{bmatrix}$$

General 2D B-matrix

B-Matrix for a 4-node element.

Weak form – stiffness matrix

$$\int_{\Omega} \nabla_s \mathbf{w} : \mathbf{C}^e : \nabla_s \mathbf{u} d\Omega = \int_{\Omega} \mathbf{w} \cdot \mathbf{b} d\Omega + \int_{\Gamma_t} \mathbf{w} \cdot \bar{\mathbf{t}} d\Gamma$$

$$\int_{\Omega} \nabla_s \mathbf{w} : \mathbf{C}^e : \nabla_s \mathbf{u} d\Omega \Rightarrow \mathbf{w}^T \mathbf{K} \mathbf{d}$$

LHS of weak form

$$\mathbf{K} = \sum_e \mathbf{L}^{eT} \mathbf{K}^e \mathbf{L}^e$$

Stiffness matrix assembly

$$\mathbf{K}^e = \int_{\Omega} \mathbf{B}^{eT} \mathbf{C}^e \mathbf{B}^e d\Omega$$

Element stiffness matrix

```
for c = mesh.conn
    xe = mesh.x(:,c);
    Ke = zeros(8);
    for q = quadrature_points
        dNdp = grad_shape(q);
        J = xe * dNdp;
        dNdx = dNdp / J;
        B = zeros(3,8);
        B(1,1:2:end) = dNdx(:,1);
        B(2,2:2:end) = dNdx(:,2);
        B(3,1:1:end) = dNdx(:,2);
        B(3,2:2:end) = dNdx(:,1);
        Ke = Ke + B'*C*B * det(J)*q(3);
    end
    % scatter operation goes here...
end
```

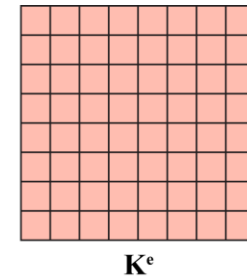
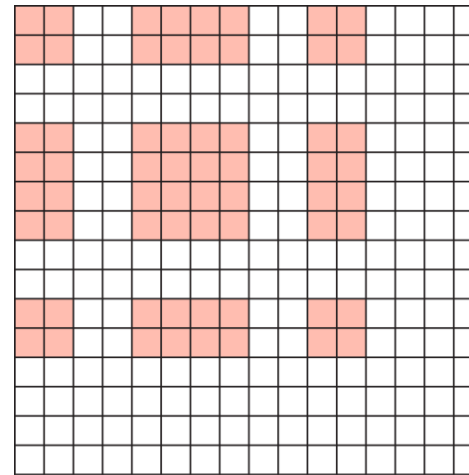
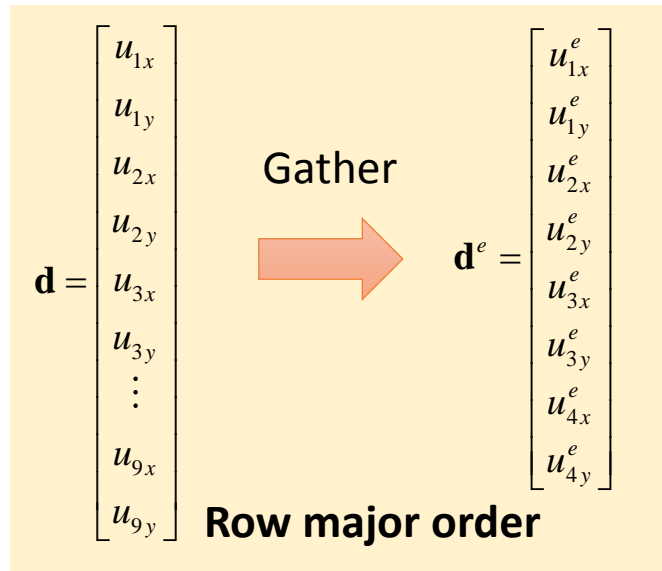
*% [3xNQ] matrix, each column gives [ξ;η;wt]
 % compute gradient of shape functions
 % J_{ij} = dx_i/dξ_j; J is not generally symmetric.*

*% assigns dNdx to odd columns in first row
 % assigns dNdx to even columns in second row
 % assigns dNdy to odd columns in third row
 % assigns dNdx to even columns in third row*

Scattering of element stiffness matrix

$$K_{IJ} \Leftarrow K_{ij}^e$$

What is the relationship between (i,j) and (I,J)?



```
cc = [2*conn-1; 2*conn];
% e.g. c=[1;2;3;4]; becomes
% cc = [1;2;3;4;5;6;7;8];
K(cc,cc) = K(cc,cc) + Ke;
```

Procedure for row-major ordering (2D)

```
cc = [3*conn-2; 3*conn-1; e*conn];
K(cc,cc) = K(cc,cc) + Ke;
```

Procedure for row-major ordering (3D)

Vector operations vs for loops (scatter in 3D)

Where *c* is an array of the nodes within an element.

METHOD 1

```
cc = [3*c-2; 3*c-1; 3*c];  
K(cc,cc) = K(cc,cc) + Ke;
```

METHOD 2

```
for i = 1:4  
    for di = 1:3  
        for j = 1:4  
            for dj = 1:3  
                I = 3*(c[i]-1) + di;  
                J = 3*(c[j]-1) + dj;  
                ii = 3*(i-1) + di;  
                jj = 3*(j-1) + dj;  
                K(I,J) = K(I,J) + Ke(ii,jj);  
            end  
        end  
    end  
end
```

Timing for 1000 elements

METHOD 1: 15 ms

METHOD 2: 850 ms

METHOD 2 is 60X slower!

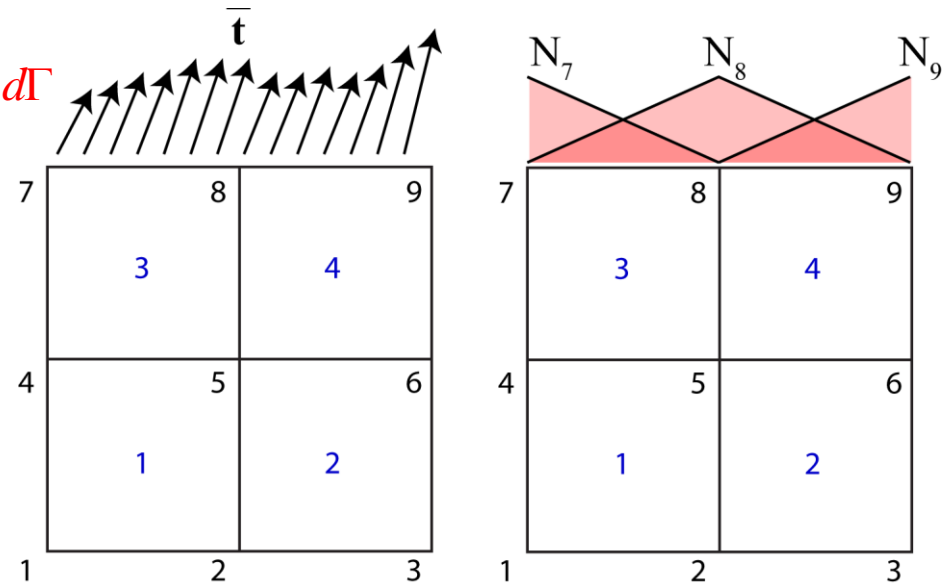
Integration of applied traction

$$\int_{\Omega} \nabla_S \mathbf{w} : \mathbf{C}^e : \nabla_S \mathbf{u} d\Omega = \int_{\Omega} \mathbf{w} \cdot \mathbf{b} d\Omega + \int_{\Gamma_t} \mathbf{w} \cdot \bar{\mathbf{t}} d\Gamma$$

$$\int_{\Gamma_t} \mathbf{w} \cdot \bar{\mathbf{t}} d\Gamma = \mathbf{w}_I \sum_e \mathbf{L}^{eT} \int_{\Gamma_t^e} \mathbf{N}_I^e \cdot \bar{\mathbf{t}} d\Gamma = \mathbf{w}_I \mathbf{f}_I^t$$

$$\int_{\Gamma_t^e} \mathbf{N}_I^e \cdot \bar{\mathbf{t}} d\Gamma = \int_{-1}^1 \mathbf{N}_I^e(\xi) \cdot \bar{\mathbf{t}}(\mathbf{x}(\xi)) \left\| \frac{\partial \mathbf{x}}{\partial \xi} \right\| d\xi$$

$$J^{edge} = \left\| \frac{\partial \mathbf{x}}{\partial \xi} \right\| = \frac{\text{length on element edge}}{\text{length on parent element edge}}$$



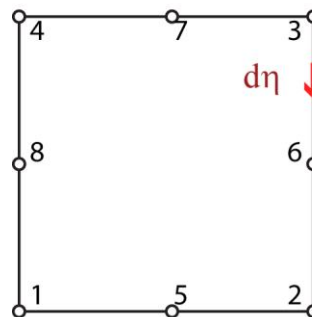
Simple case

When the element edge is straight (and nodes I, J are the corner nodes on the edge)

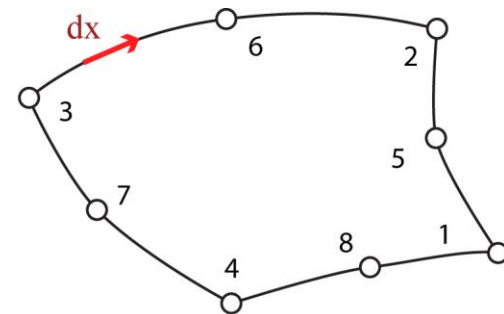
$$\left\| \frac{\partial \mathbf{x}}{\partial \xi} \right\| = \frac{\|\mathbf{x}_I^e - \mathbf{x}_J^e\|}{2}$$

General case (where c are the nodes on the edge)

```
dNdp = shape1D(ξ); % 1D edge shape function
J_edge = norm(xe(:,c) * dNdp);
```



parent coordinates



global coordinates