



M.Tech thesis  
**Doppler-Resilient 802.11ad-Based  
Ultra-Short Range Automotive Radar**

By

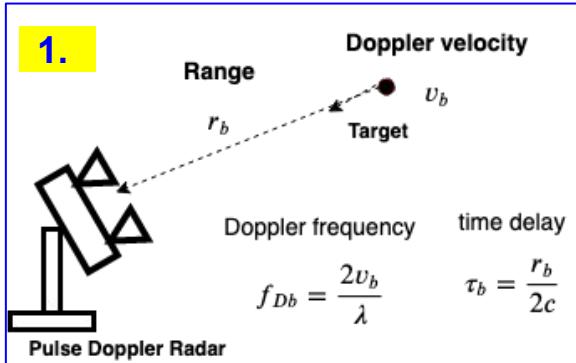
Gaurav Duggal (MT17091)

Supervisor: Shobha Sundar Ram

# Organisation

1. Pulse Doppler Radar working
2. Literature Survey and introduction to 802.11ad
3. Methodology
4. Radar Signal Model
5. Target Models and Radar Signatures
6. Radar Operating Curves
7. Conclusion

# 1.1 Pulse-Doppler Radar



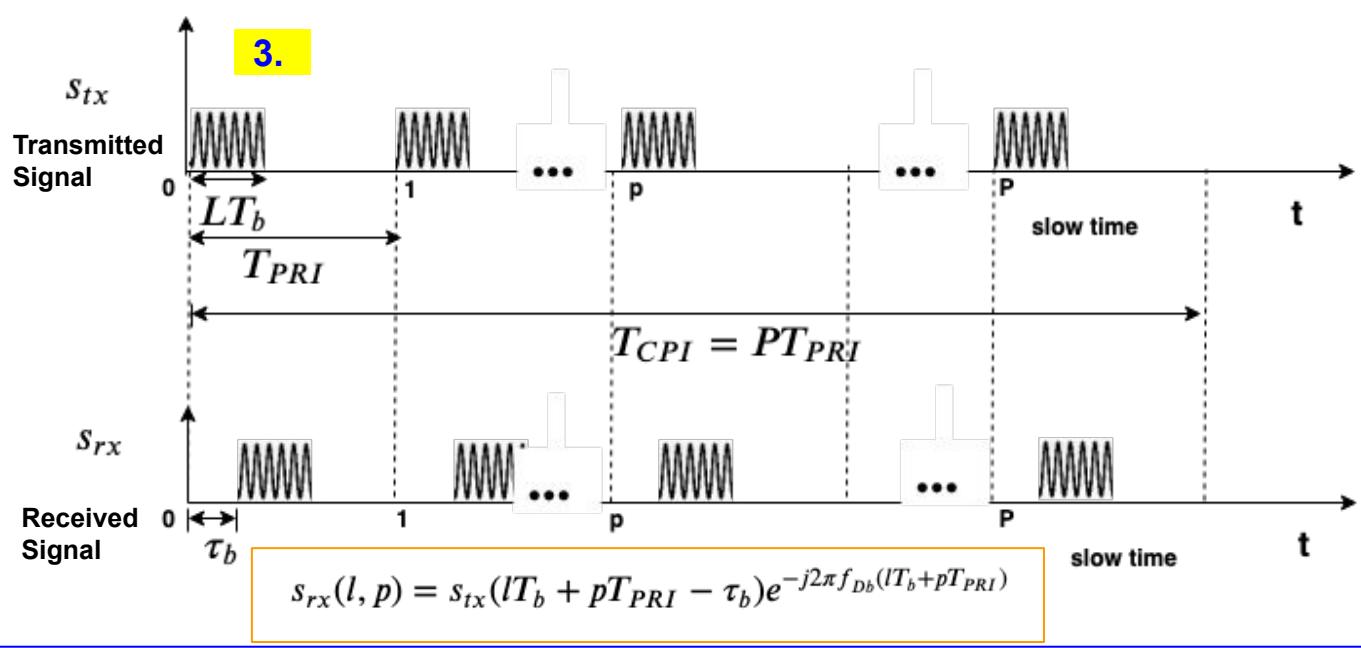
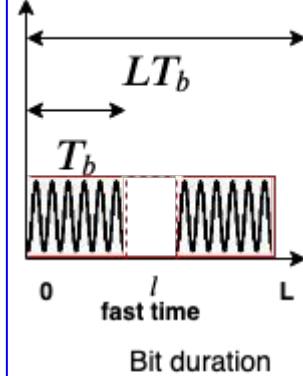
$T_{CPI}$  – Coherent Processing Interval

$T_{PRI}$  – Pulse Repetition Interval

$T_b$  – Bit duration

2.

$L$  bits in 1 Sequence

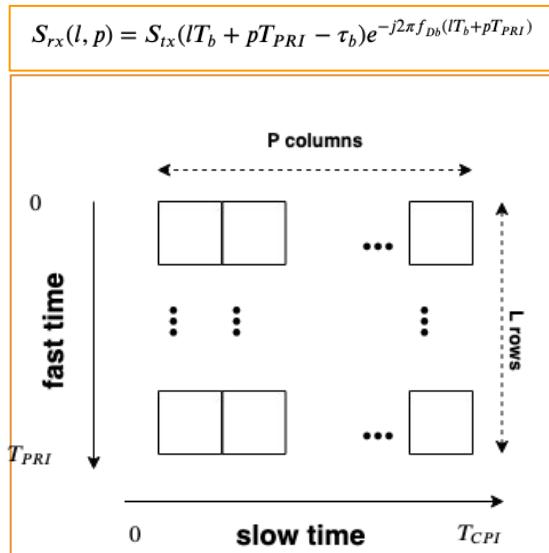


# 1.2 Pulse - Doppler Radar Signal Processing

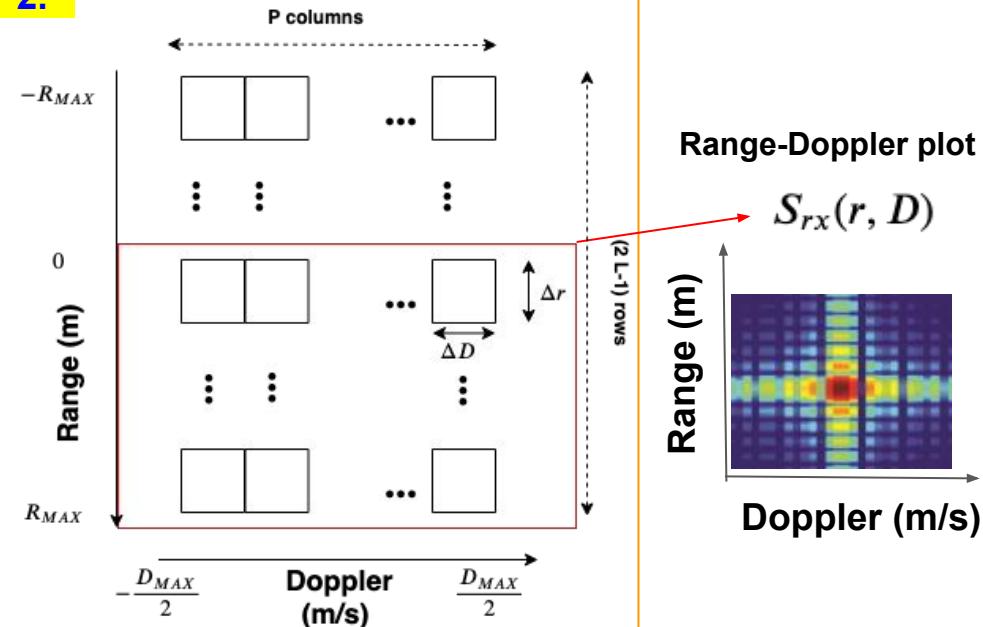
1.

Received baseband signal

$$S_{rx}(l, p) = S_{tx}(lT_b + pT_{PRI} - \tau_b)e^{-j2\pi f_{db}(lT_b + pT_{PRI})}$$



2.



Range Resolution

$$\Delta r = \frac{cT_b}{2}$$

Max. Range

$$R_{max} = \frac{cLT_b}{2}$$

Doppler velocity resolution

$$\Delta D = \frac{\lambda}{2T_{CPI}}$$

Max. Doppler velocity

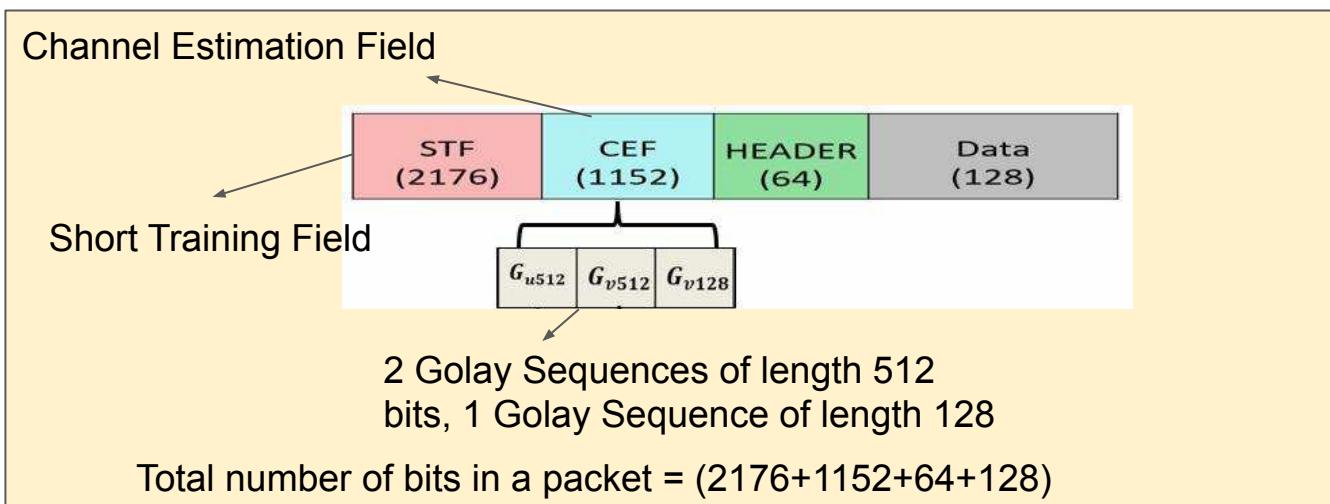
$$D_{max} = \frac{\lambda}{4T_{PRI}}$$

## 2.1 Introduction to the IEEE 802.11ad

1. 60 GHz wireless link for 5G communications between autonomous vehicles
2. Signal bandwidth: 1.76 GHz - significantly more than 802.11ac (20/40MHz)
3. Joint radar and communication framework

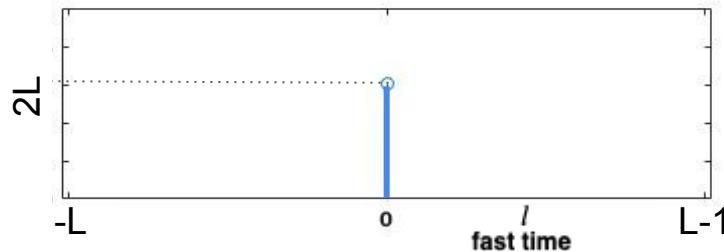
Range Resolution

$$\Delta r = \frac{cT_b}{2}$$



Protocol	Range Resolution
802.11ad	0.085 m
802.11ac	0.9 m
802.11n	3.75 m
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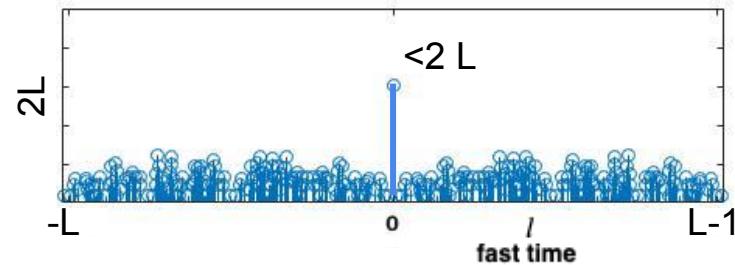
## 2.2 Golay Perfect Autocorrelation Property



1. This is the received signal for a static target at zero delay and we see there are zero sidelobes

$$(G_{a,L}[l] * G_{a,L}[l]) + (G_{b,L}[l] * G_{b,L}[l]) = 6L\delta[l], l = -L, \dots, 0, \dots, L-1$$

2. This is the received signal for a moving target at zero delay and we see there are sidelobes present



$$(G_{a,L}[l] * G_{a,L}[l]) + (G_{b,L}[l] * G_{b,L}[l])e^{j\theta} \neq 6L\delta[l], l = -L, \dots, 0, \dots, L-1$$

## 2.3 Literature Survey

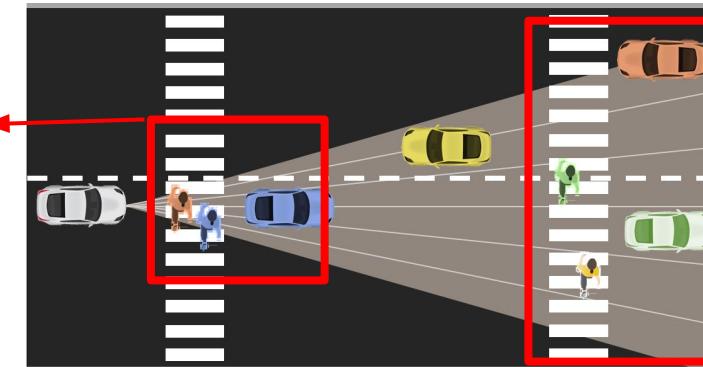
Parameters	Current Literature	Shortcomings
Range	Long Range (~200m)	Attenuation is high ( <b>20 dB/km at sea level</b> ) for 60 GHz
Target Model	Simple point targets	For short range radar, targets are closer, we hypothesize simple point target model isn't accurate
Type of target	Static	Automotive scenario has moving targets

1. P. Kumari et.al “IEEE 802.11ad-based radar:An approach to joint vehicular communication-radar system,” *IEEE Transactions on Vehicular Technology*, 2018. (**UT Austin**)
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## 3.1 Methodology

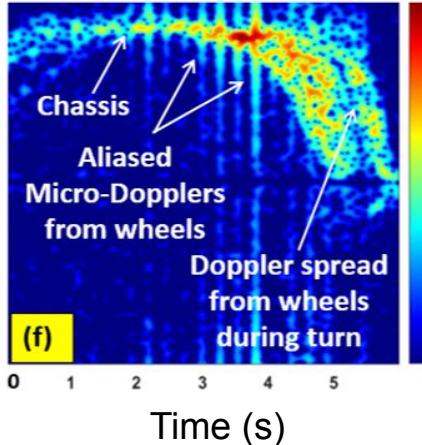
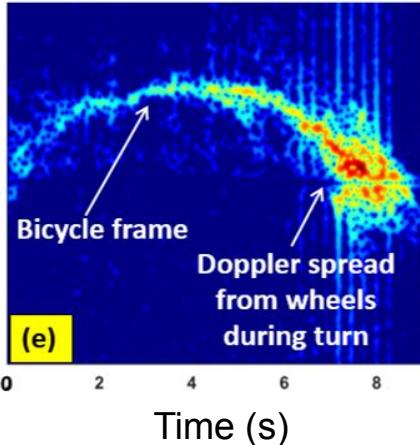
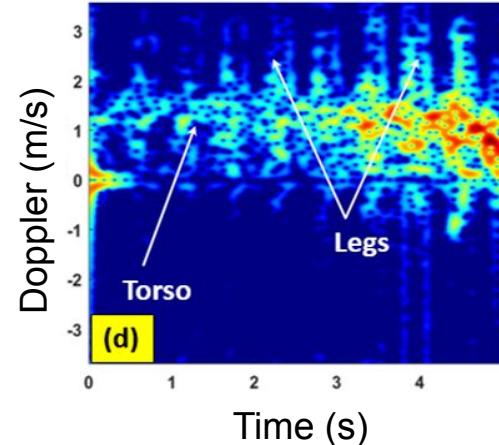
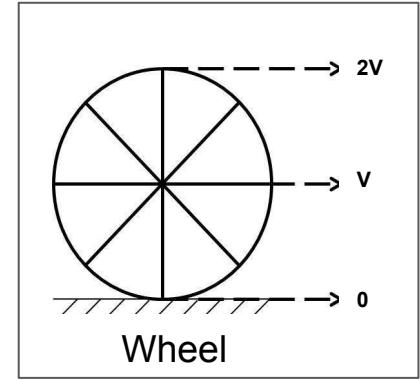
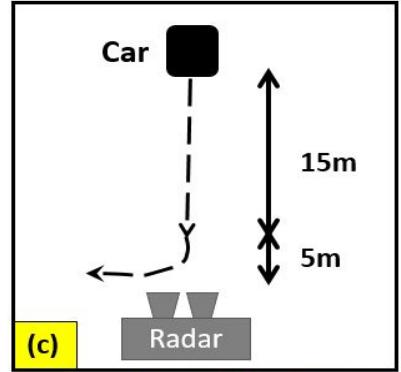
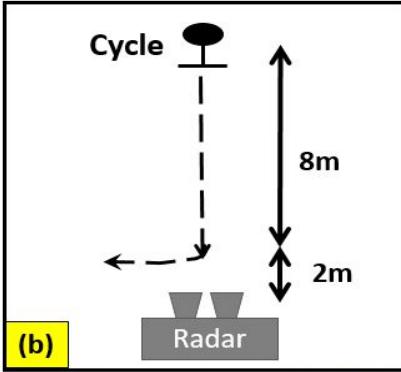
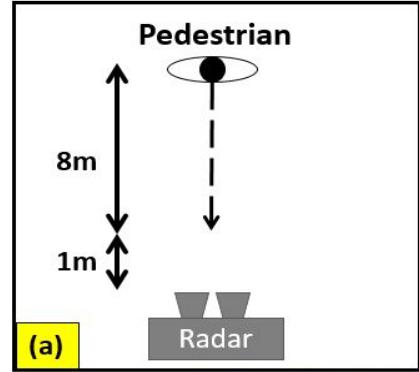
1.	Test extended target model hypothesis
2.	Implement Standard Golay (SG) Processing and Modified Golay (MG) Processing to test range-sidelobe level reduction for simple point scatterer
3.	Generate realistic Electromagnetic target models for the automotive scenario
4.	Generate radar receiver operating curves to quantify the improvement in an objective manner

Short range targets fit in multiple bins and need to be modelled as extended targets



Long range targets fit in 1 bin and should appear as point targets

## 3.2 Short Range Automotive Scenario Experiment

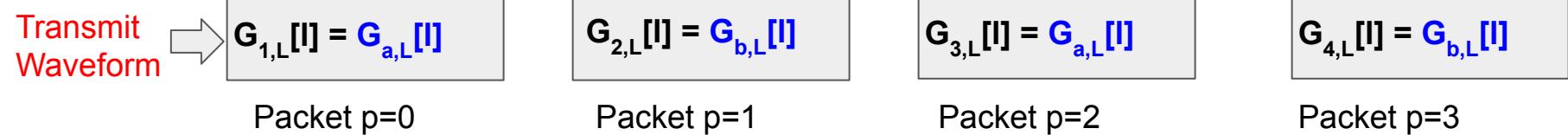


Test Setup

# 4.1 Standard Golay (SG) waveform Example, L=512

## Example for 4 packets

1. Consider a Golay Pair  $\{\mathbf{G}_{a,L}[n], \mathbf{G}_{b,L}[n]\}$  of length 512 bits each.



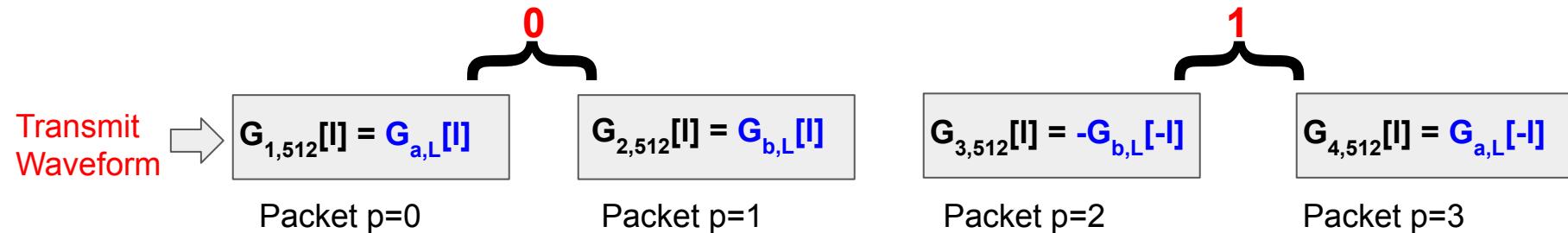
Receiver matched filter processing

$$\sum_{p=0}^3 e^{jp\theta} (G_{p,L}[l] * G_{p,L}[l]) \neq 6L\delta[l], \quad l = -L, \dots, (L-1)$$

## 4.2 Modified Golay (MG) waveform, L=512

### Example for 4 packets

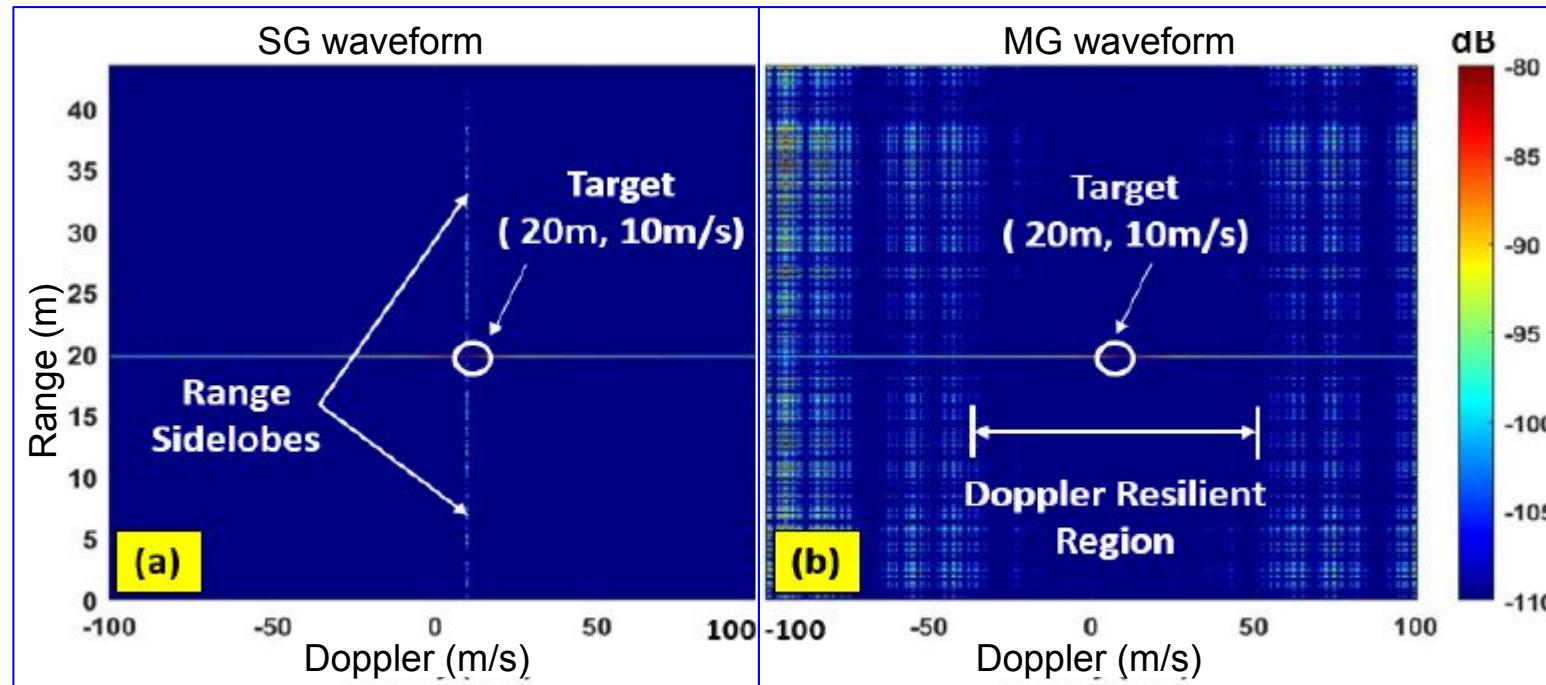
1. Generate Prou-Thue-Morse (PTM) sequence of length 2 bits - {0,1}
2. In PTM sequence replace all 0's with Golay Pair  $\{G_{a,L}[l], G_{b,L}[l]\}$  and 1's with Golay Pair  $\{-G_{b,L}[-l], G_{a,L}[-l]\}$



### Receiver matched filter processing

$$\begin{aligned} \sum_{p=0}^3 e^{j p \theta} (G_{p,L}[l] * G_{p,L}[l]) &\approx 1(G_{1,L}[l] * G_{1,L}[l]) + 2(G_{2,L}[l] * G_{2,L}[l]) + 3(G_{3,L}[l] * G_{3,L}[l]) \\ &= 1((G_{b,L}[l] * G_{b,L}[l]) + (G_{a,L}[-l] * G_{a,L}[-l])) + 2((-G_{b,L}[-l] * -G_{b,L}[-l]) + (G_{a,L}[-l] * G_{a,L}[-l])) \\ &= (2L + 2(2L))\delta[l] \\ &= 6L\delta[l] \end{aligned}$$

## 4.3 MG vs SG for a moving point target, P=2048 packets



Range sidelobes have been suppressed by 20 dB

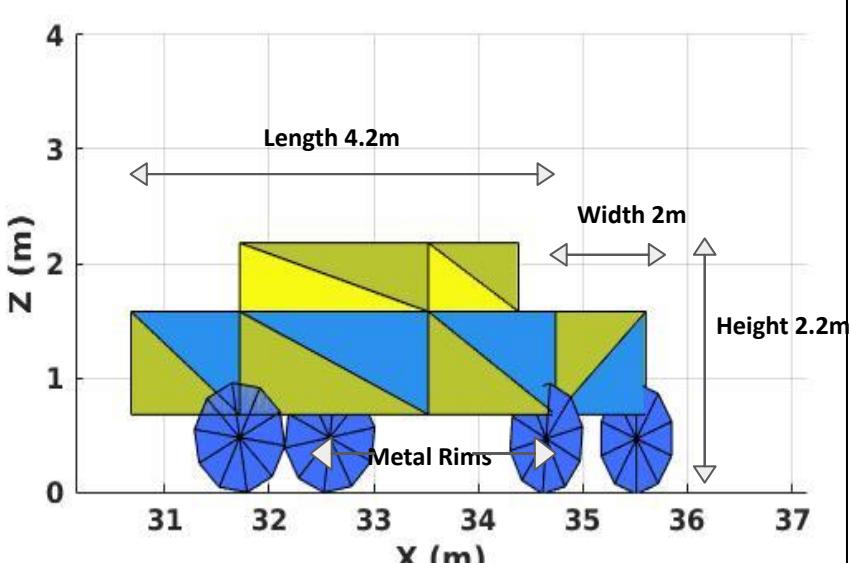
## 4.4 Ultra Short Range Radar

Parameter	Proposed Radar	Commercial SRR
Carrier Frequency	60 GHz	77 GHz
Bandwidth	1.76 GHz	2 GHz
Range resolution	0.085 m	0.075 m
Maximum unambiguous range	44 m	40 m
Pulse repetition interval	2 us	1.67 us
Velocity resolution	0.6 m/s	0.27 m/s
Maximum unambiguous velocity	625 m/s	111 m/s
Coherent Processing interval	0.0041 s (P=2048)	0.007 s

Ultra short range automotive radars have the following usage scenarios:

1. Parking assistance
2. Lane change assistance
3. Object detection and tracking

## 5.1 Extended target model of a car



Radar cross section of a triangular plate

$$\sigma_b[n] = \frac{4\pi A_b^2 \cos^2 \theta_b[n]}{\lambda^2} \left( \frac{\sin \left( kd_b \sin \frac{\theta_b[n]}{2} \right)}{kd_b \sin \frac{\theta_b[n]}{2}} \right)^4$$

$A_b$  = area of the plate

$\theta_b$  = aspect angle

$d_b$  = dimension along aspect angle

$k$  = propagation constant

$\lambda$  = wavelength

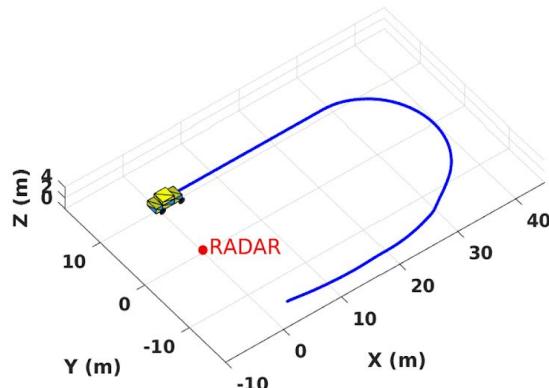
**Primitive** chosen for a car is a triangular plate and can be represented in 3D space by its centroid

Received signal

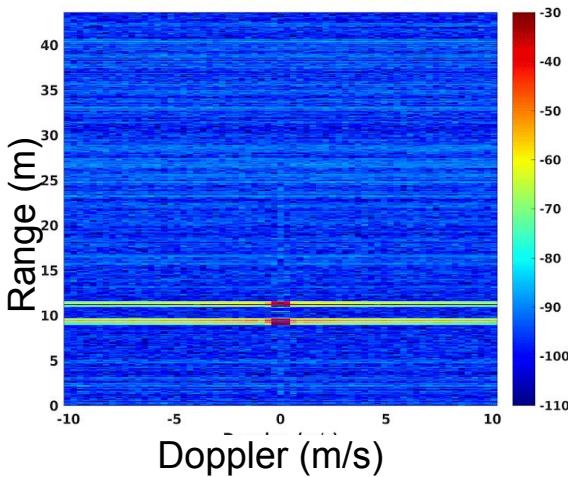
$$x_R(t) = \sum_{b=0}^B A \frac{\sqrt{\sigma_b(\theta)}}{r_b(t)^2} x_T \left( t - \frac{2r_b(t)}{c} \right) + \eta$$

## 5.2 Car range-Doppler MG waveform vs SG waveform

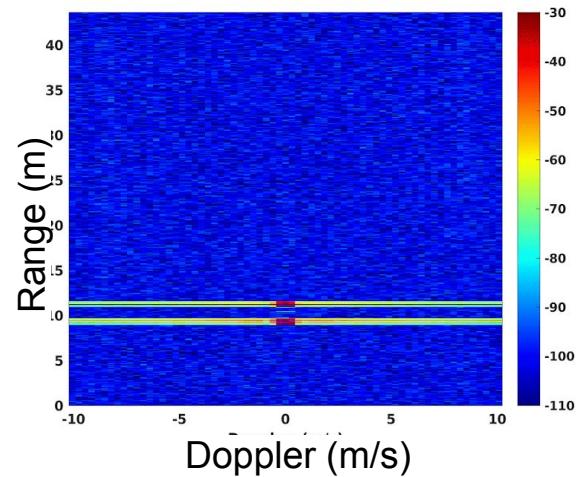
Scene View



SG waveform



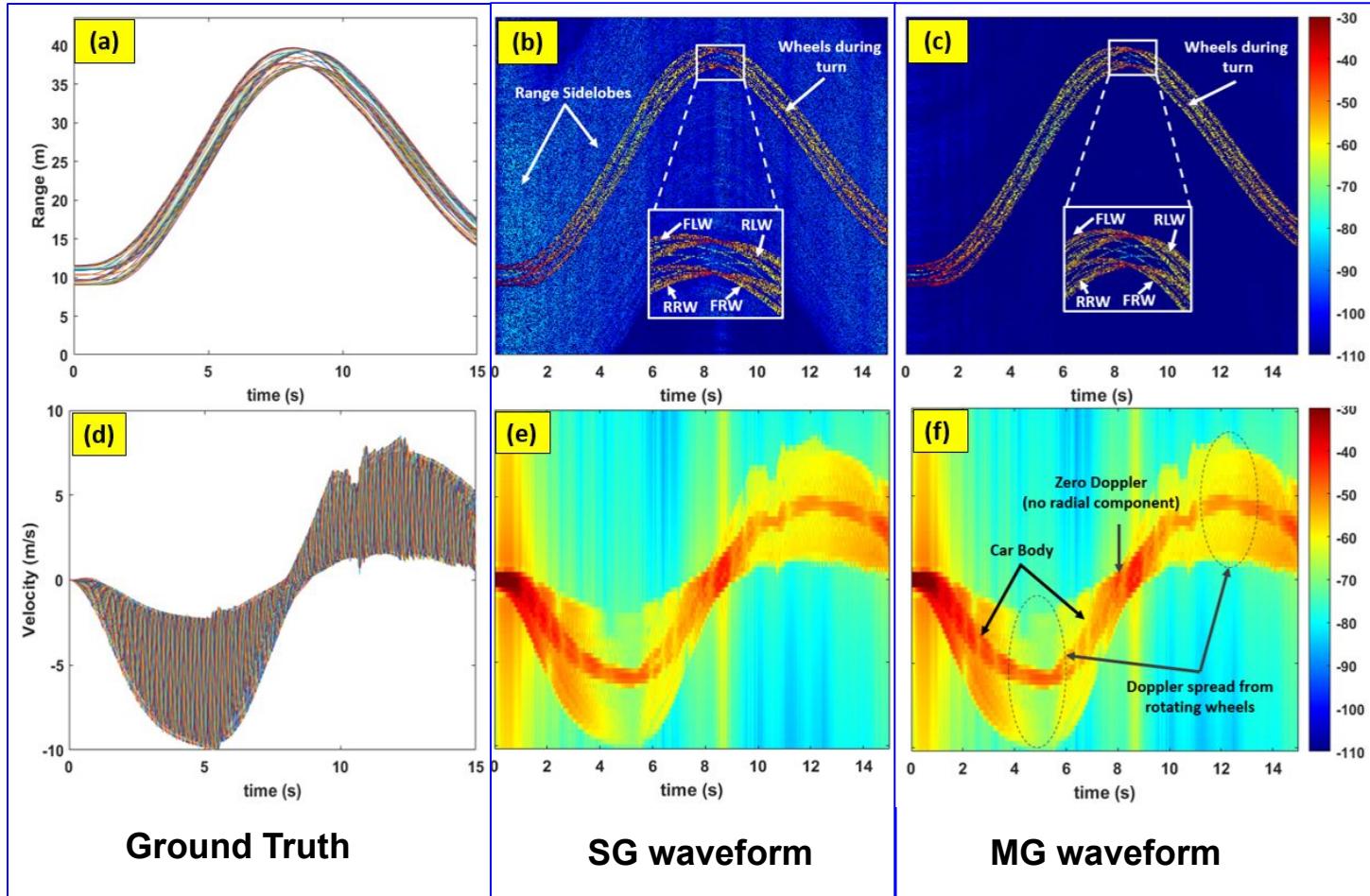
MG waveform



### Key Observations:

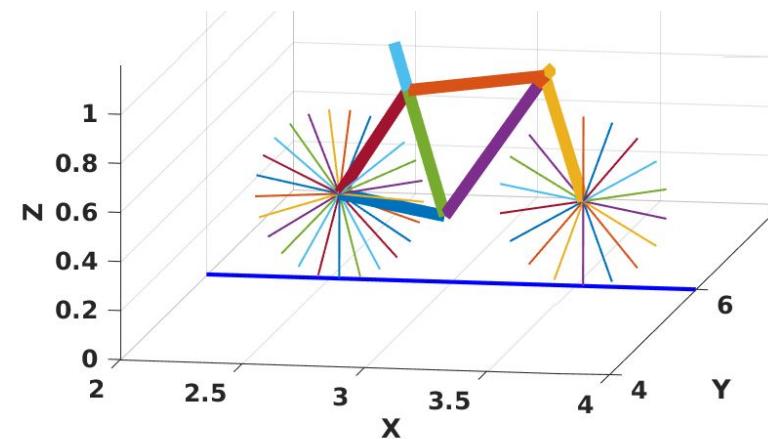
1. The extended target model of the car manifests itself over multiple range-Doppler bins.
2. The power of the reflected signal from the car causes the fluctuations in colour in the range-Doppler plot.
3. Range sidelobes are suppressed in the MG waveform making it Doppler resilient.

# 5.3 Car Radar Signatures



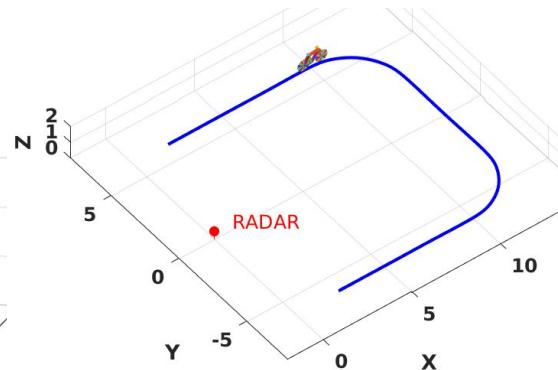
# 5.4 Extended target model of a bicycle

Primitives are rods

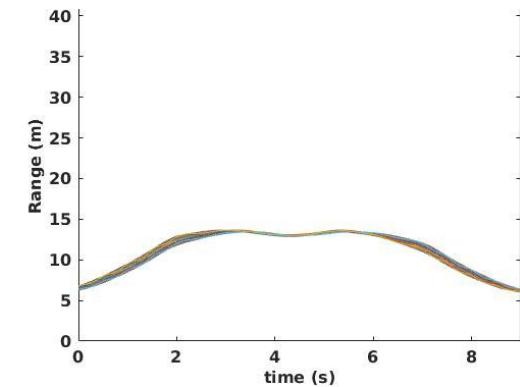


$$\sigma_b[n] = \frac{2\pi a_b L_b^2}{\lambda} \cos^2(\theta_b[n]) \left( \frac{\sin(kL_b \sin \theta_b[n])}{kL_b \sin \theta_b[n]} \right)^2$$

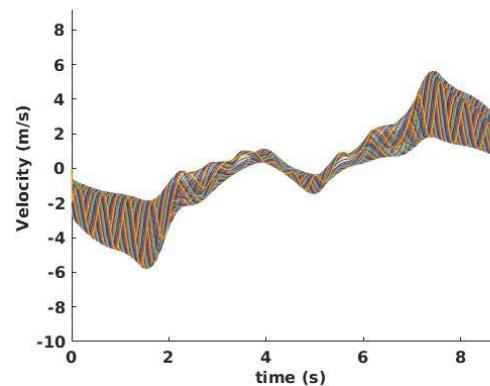
The metal rods of the frame and the metal rods of the spokes are modelled in this electromagnetic model



Range-time ground truth



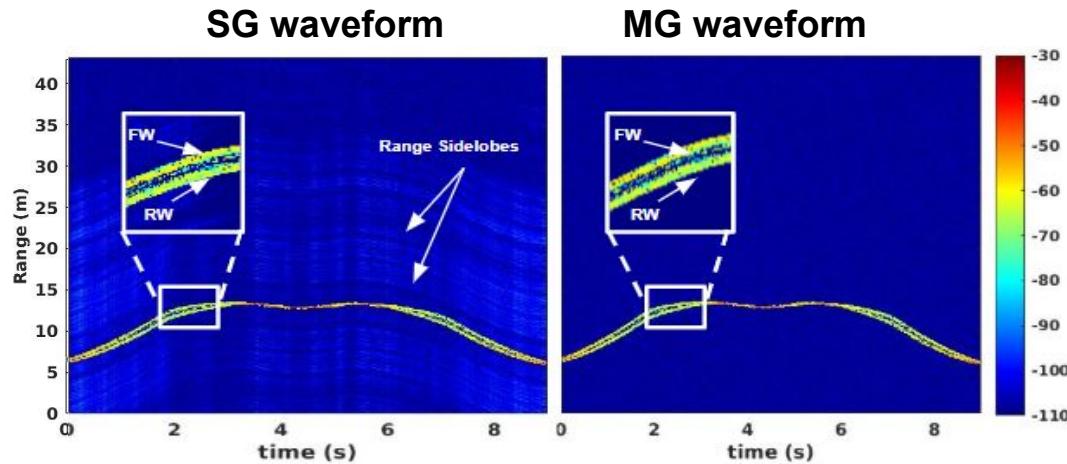
Doppler-time ground truth



# 5.5 Extended Target Model: Bicycle radar signatures

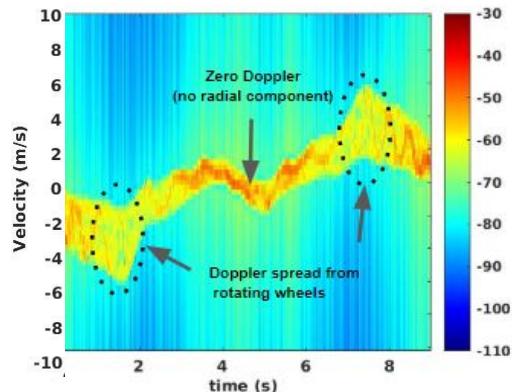
## Range-time plot

1. Range-sidelobes are suppressed in the MG waveform
2. Micro-range information from the wheels is visible

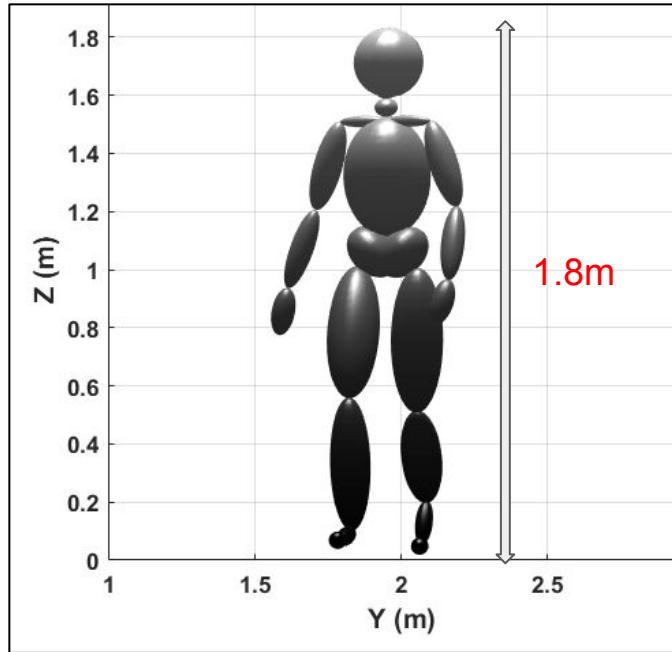


## Doppler-time plot

1. The aspect angle variation manifests itself in the variation of the received power and we can see it on the colour bar
2. When the bicycle is directly in front of the radar, it is moving in the transverse direction hence there is zero Doppler in the received signal



## 5.6 Extended target model of a pedestrian



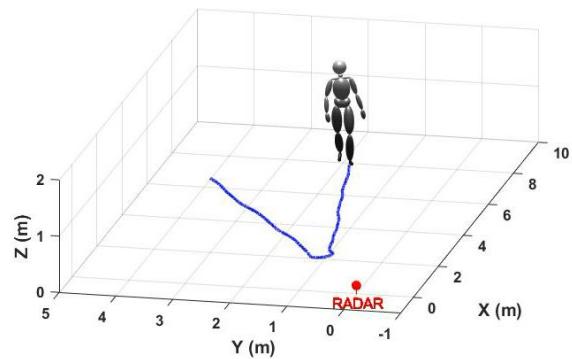
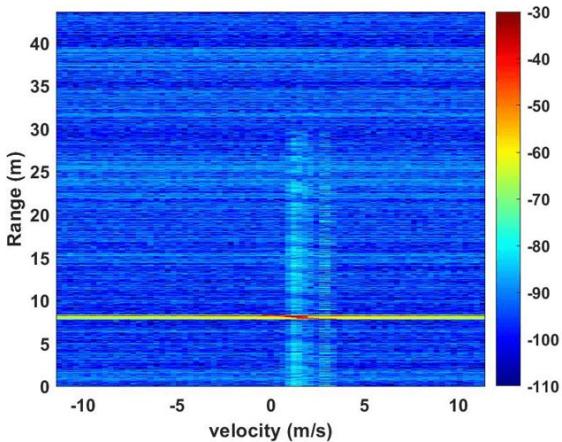
Radar cross section of an ellipsoid

$$\sigma_b[n] = \frac{\frac{1}{4} R_b^4 H_b^2}{R_b^2 \sin^2 \theta_b[n] + \frac{1}{4} H_b^2 \cos^2 \theta_b[n]}$$

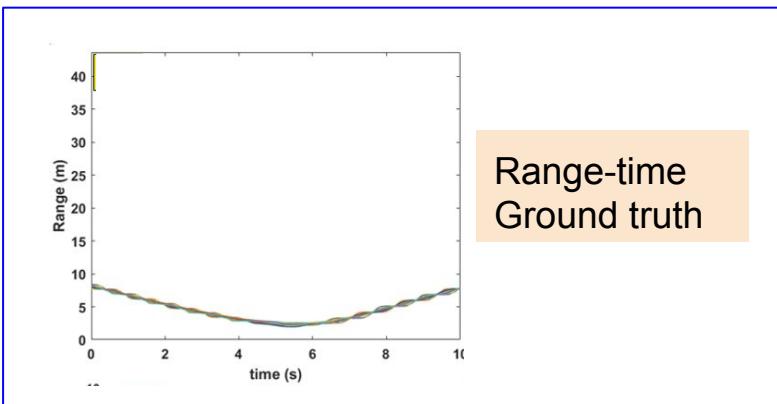
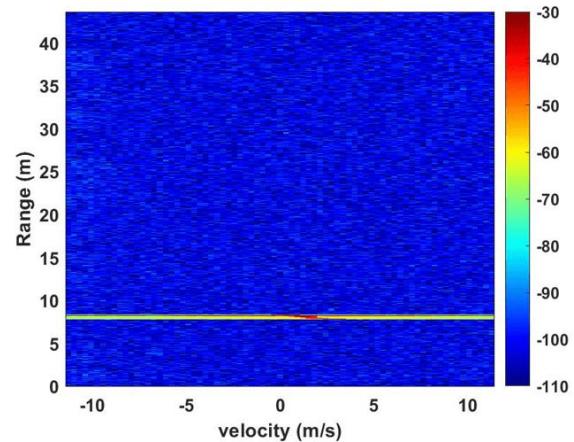
$H_b$  = length of the ellipsoid  
 $R_b$  = radius of the ellipsoid

# 5.7 Pedestrian MG waveform vs SG waveform

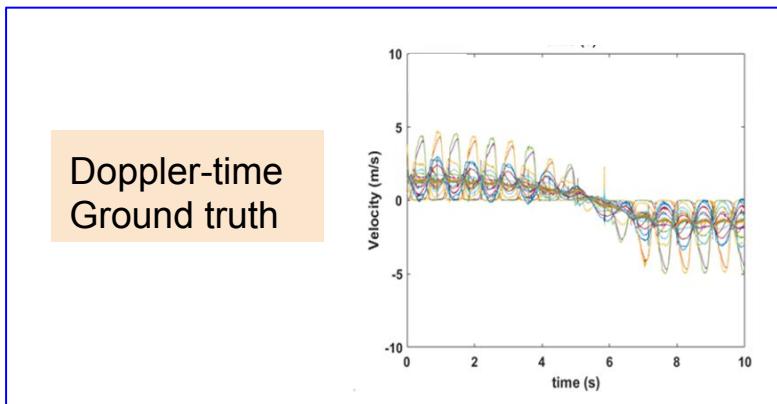
SG Waveform



MG Waveform



Range-time  
Ground truth



Doppler-time  
Ground truth



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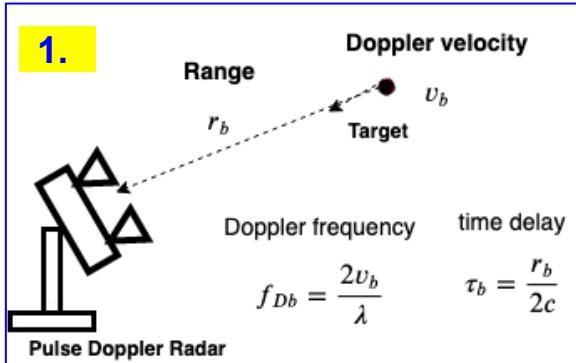
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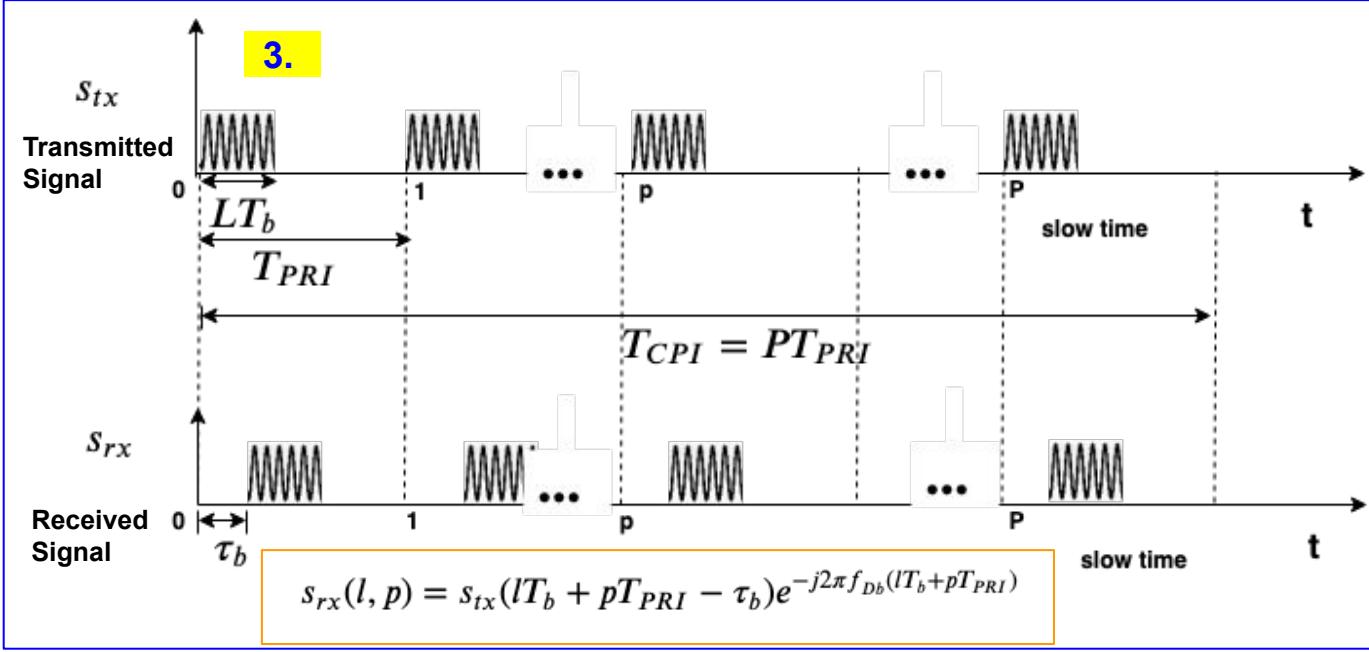
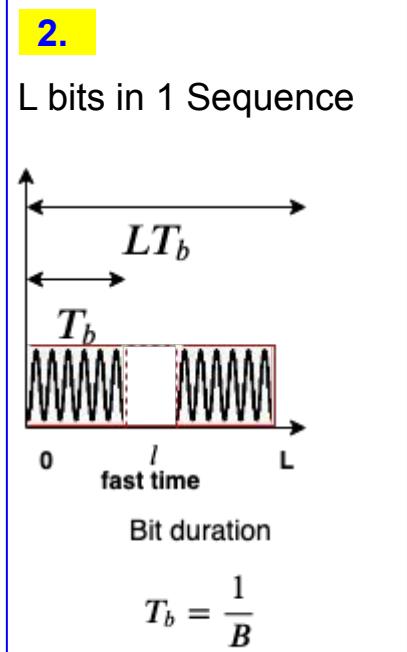
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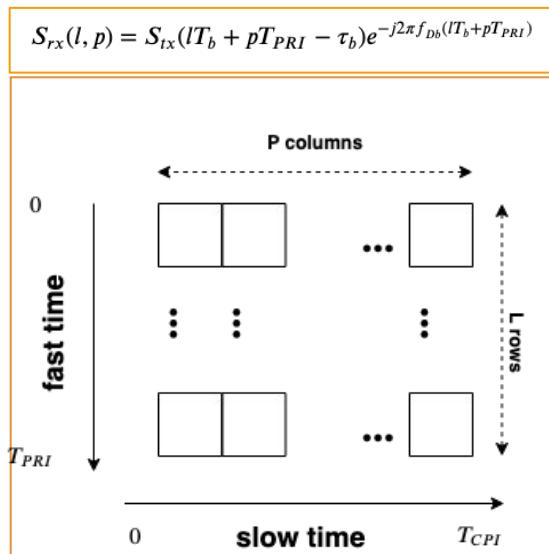


# 1.2 Pulse - Doppler Radar Signal Processing

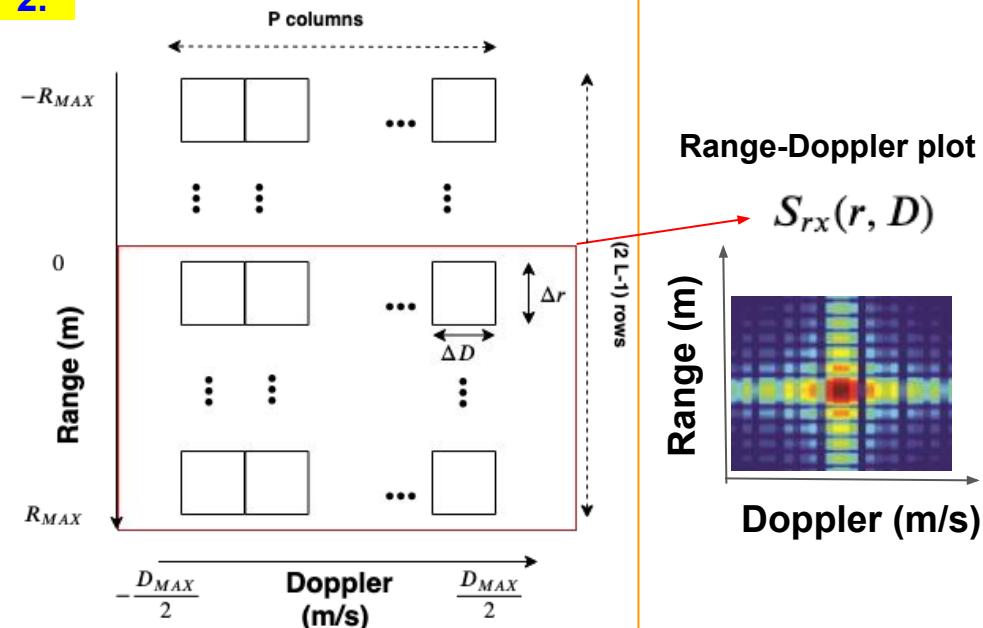
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Received baseband signal

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2.



Range Resolution

$$\Delta r = \frac{cT_b}{2}$$

Max. Range

$$R_{max} = \frac{cLT_b}{2}$$

Doppler velocity resolution

$$\Delta D = \frac{\lambda}{2T_{CPI}}$$

Max. Doppler velocity

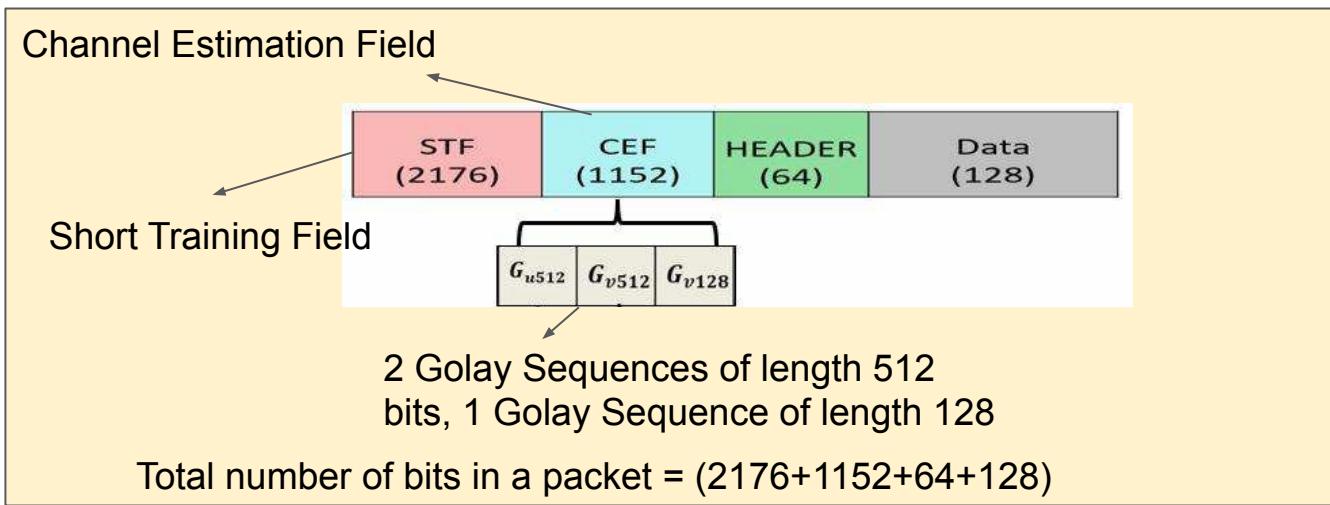
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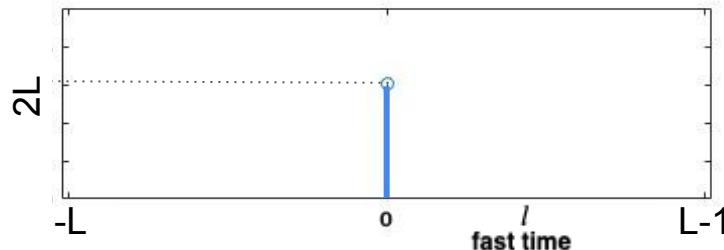
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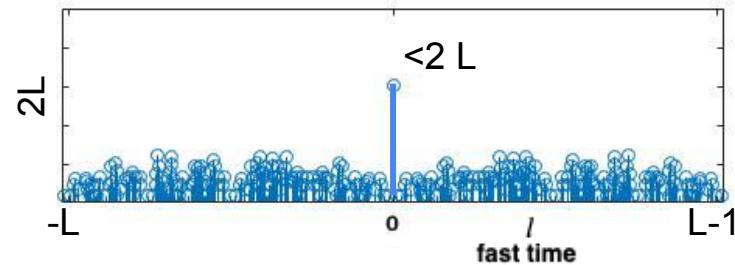
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2. This is the received signal for a moving target at zero delay and we see there are sidelobes present



$$(G_{a,L}[l] * G_{a,L}[l]) + (G_{b,L}[l] * G_{b,L}[l])e^{j\theta} \neq 6L\delta[l], l = -L, \dots, 0, \dots, L-1$$

## 2.3 Literature Survey

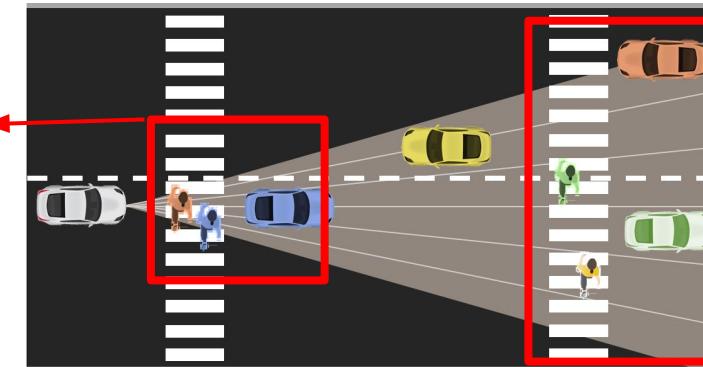
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## 3.1 Methodology

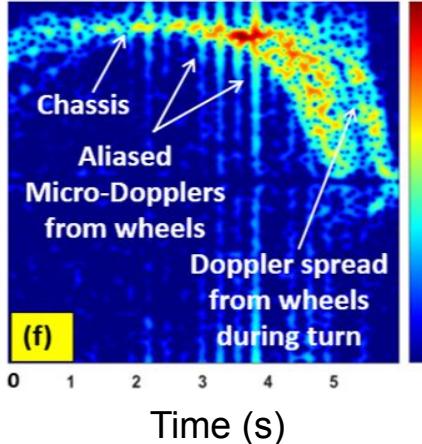
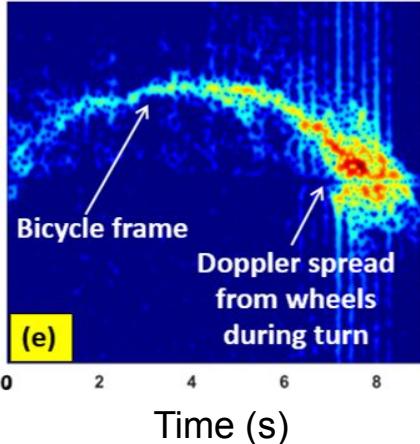
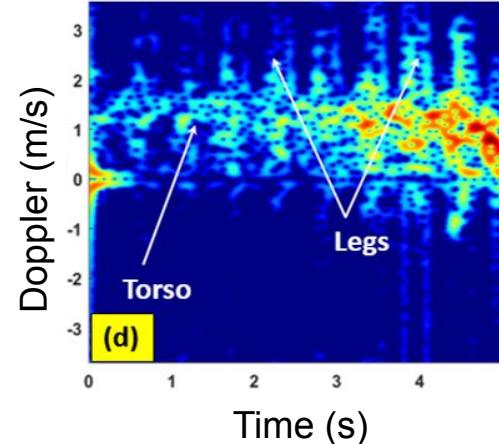
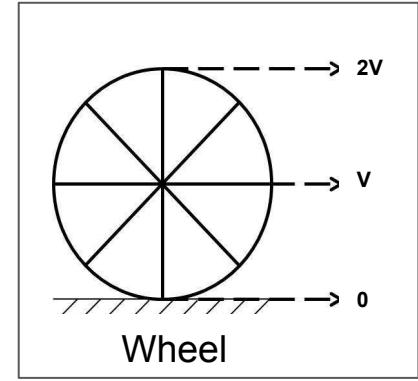
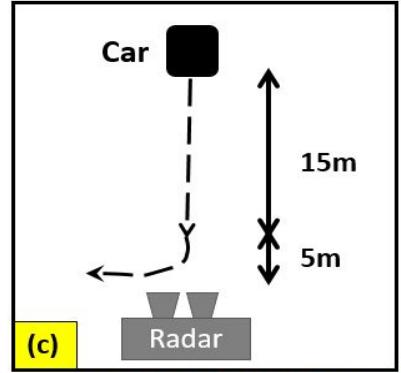
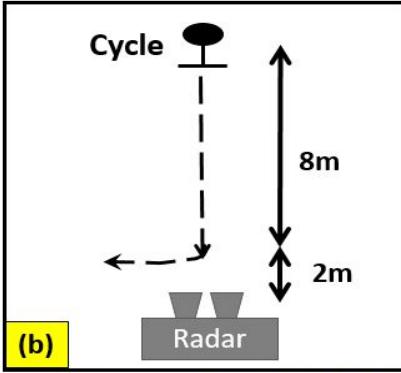
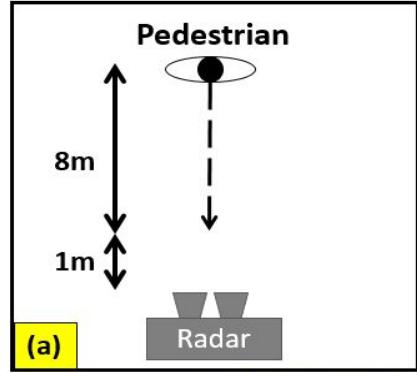
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## 3.2 Short Range Automotive Scenario Experiment



# 4.1 Standard Golay (SG) waveform Example, L=512

## Example for 4 packets

1. Consider a Golay Pair  $\{\mathbf{G}_{a,L}[n], \mathbf{G}_{b,L}[n]\}$  of length 512 bits each.

Transmit Waveform  $\rightarrow$

$\mathbf{G}_{1,L}[l] = \mathbf{G}_{a,L}[l]$	$\mathbf{G}_{2,L}[l] = \mathbf{G}_{b,L}[l]$	$\mathbf{G}_{3,L}[l] = \mathbf{G}_{a,L}[l]$	$\mathbf{G}_{4,L}[l] = \mathbf{G}_{b,L}[l]$
Packet p=0	Packet p=1	Packet p=2	Packet p=3

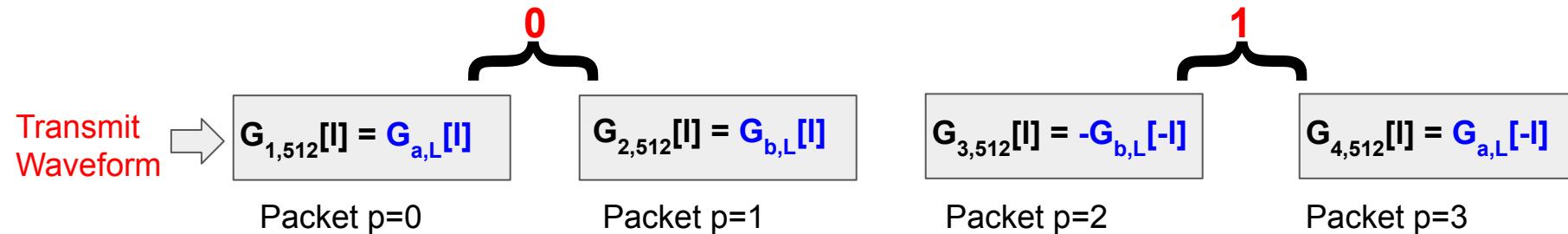
Receiver matched filter processing

$$\sum_{p=0}^3 e^{jp\theta} (G_{p,L}[l] * G_{p,L}[l]) \neq 6L\delta[l], \quad l = -L, \dots, (L-1)$$

## 4.2 Modified Golay (MG) waveform, L=512

### Example for 4 packets

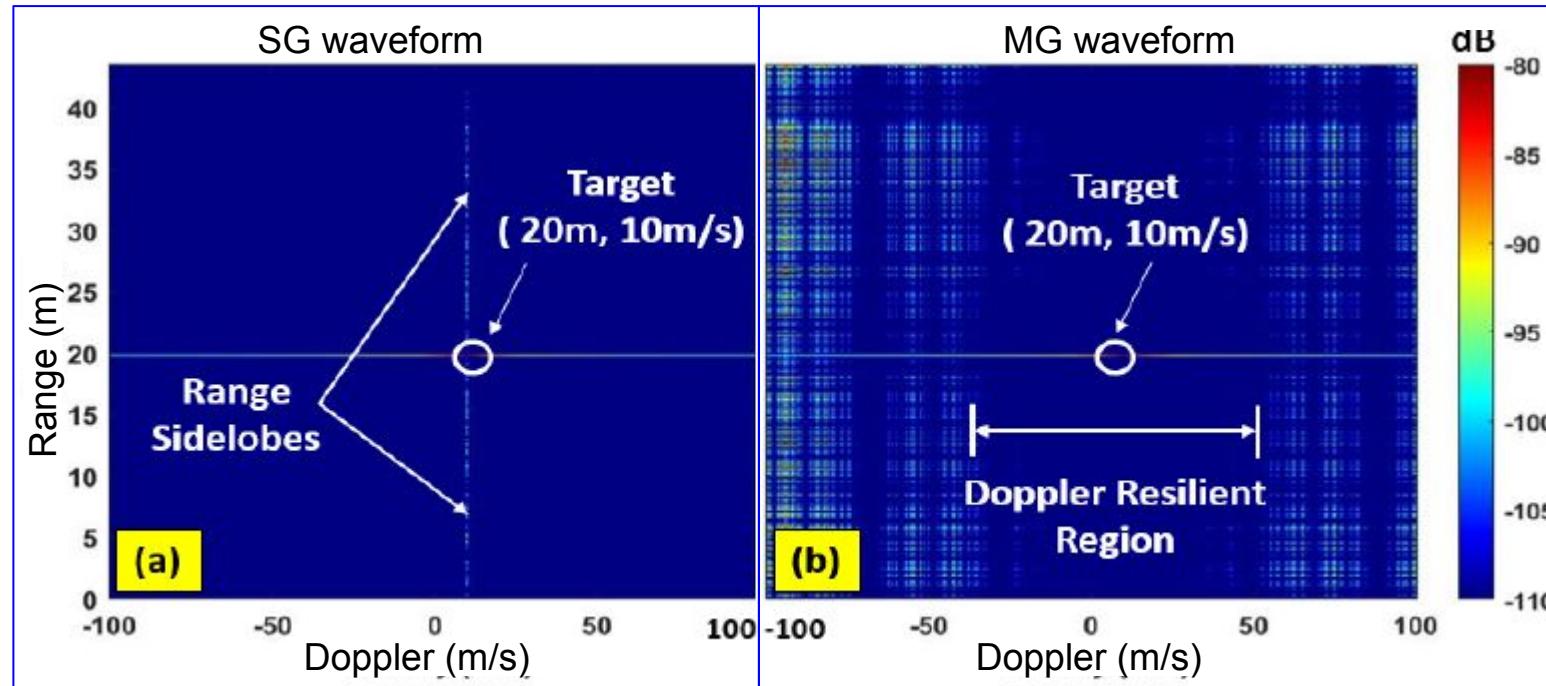
1. Generate Prou-Thue-Morse (PTM) sequence of length 2 bits - {0,1}
2. In PTM sequence replace all 0's with Golay Pair  $\{G_{a,L}[l], G_{b,L}[l]\}$  and 1's with Golay Pair  $\{-G_{b,L}[-l], G_{a,L}[-l]\}$



### Receiver matched filter processing

$$\begin{aligned} \sum_{p=0}^3 e^{j p \theta} (G_{p,L}[l] * G_{p,L}[l]) &\approx 1(G_{1,L}[l] * G_{1,L}[l]) + 2(G_{2,L}[l] * G_{2,L}[l]) + 3(G_{3,L}[l] * G_{3,L}[l]) \\ &= 1((G_{b,L}[l] * G_{b,L}[l]) + (G_{a,L}[-l] * G_{a,L}[-l])) + 2((-G_{b,L}[-l] * -G_{b,L}[-l]) + (G_{a,L}[-l] * G_{a,L}[-l])) \\ &= (2L + 2(2L))\delta[l] \\ &= 6L\delta[l] \end{aligned}$$

## 4.3 MG vs SG for a moving point target, P=2048 packets



Range sidelobes have been suppressed by 20 dB

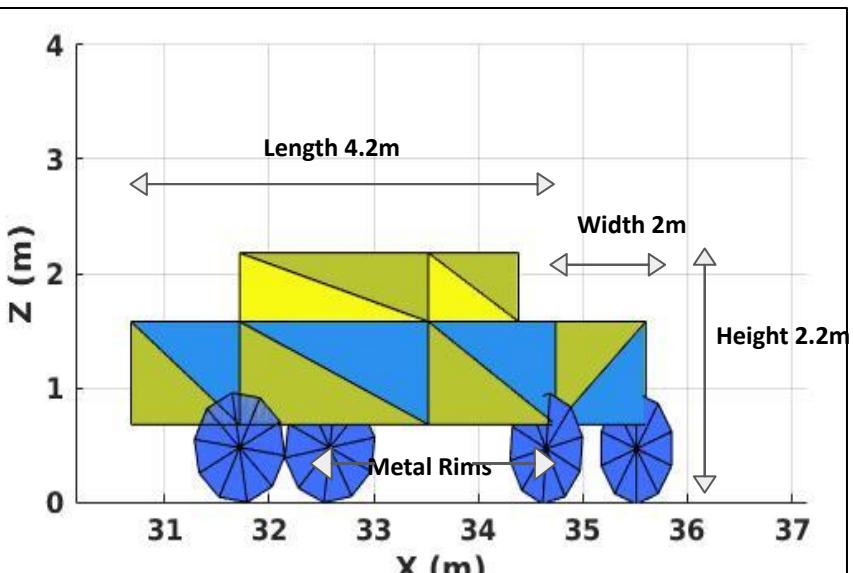
## 4.4 Ultra Short Range Radar

Parameter	Proposed Radar	Commercial SRR
Carrier Frequency	60 GHz	77 GHz
Bandwidth	1.76 GHz	2 GHz
Range resolution	0.085 m	0.075 m
Maximum unambiguous range	44 m	40 m
Pulse repetition interval	2 us	1.67 us
Velocity resolution	0.6 m/s	0.27 m/s
Maximum unambiguous velocity	625 m/s	111 m/s
Coherent Processing interval	0.0041 s (P=2048)	0.007 s

Ultra short range automotive radars have the following usage scenarios:

1. Parking assistance
2. Lane change assistance
3. Object detection and tracking

## 5.1 Extended target model of a car



**Primitive** chosen for a car is a triangular plate and can be represented in 3D space by its centroid

Radar cross section of a triangular plate

$$\sigma_b[n] = \frac{4\pi A_b^2 \cos^2 \theta_b[n]}{\lambda^2} \left( \frac{\sin \left( kd_b \sin \frac{\theta_b[n]}{2} \right)}{kd_b \sin \frac{\theta_b[n]}{2}} \right)^4$$

$A_b$  = area of the plate

$\theta_b$  = aspect angle

$d_b$  = dimension along aspect angle

$k$  = propagation constant

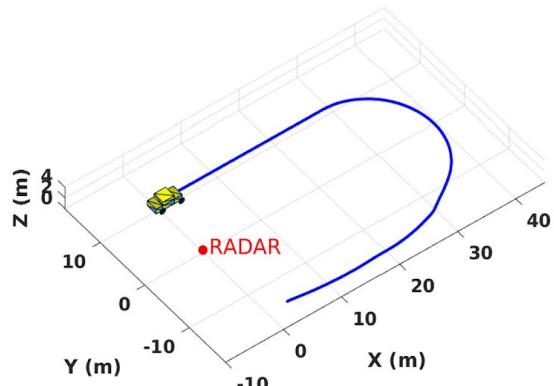
$\lambda$  = wavelength

Received signal

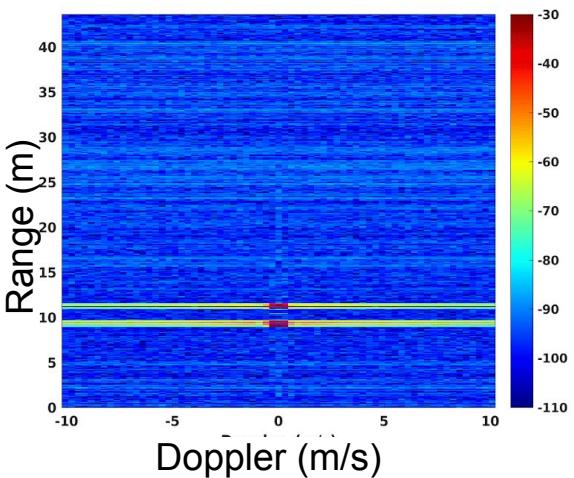
$$x_R(t) = \sum_{b=0}^B A \frac{\sqrt{\sigma_b(\theta)}}{r_b(t)^2} x_T \left( t - \frac{2r_b(t)}{c} \right) + \eta$$

## 5.2 Car range-Doppler MG waveform vs SG waveform

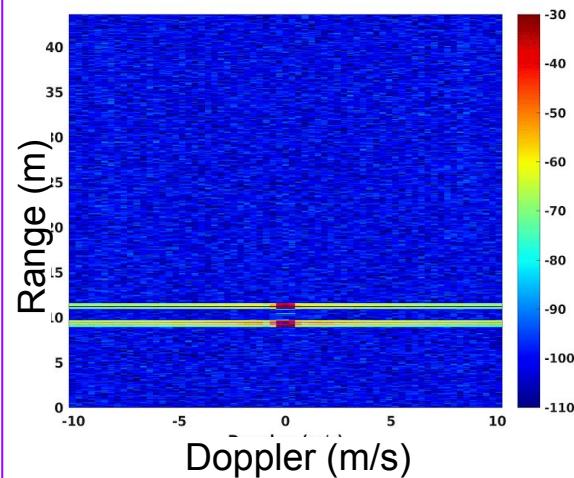
Scene View



SG waveform



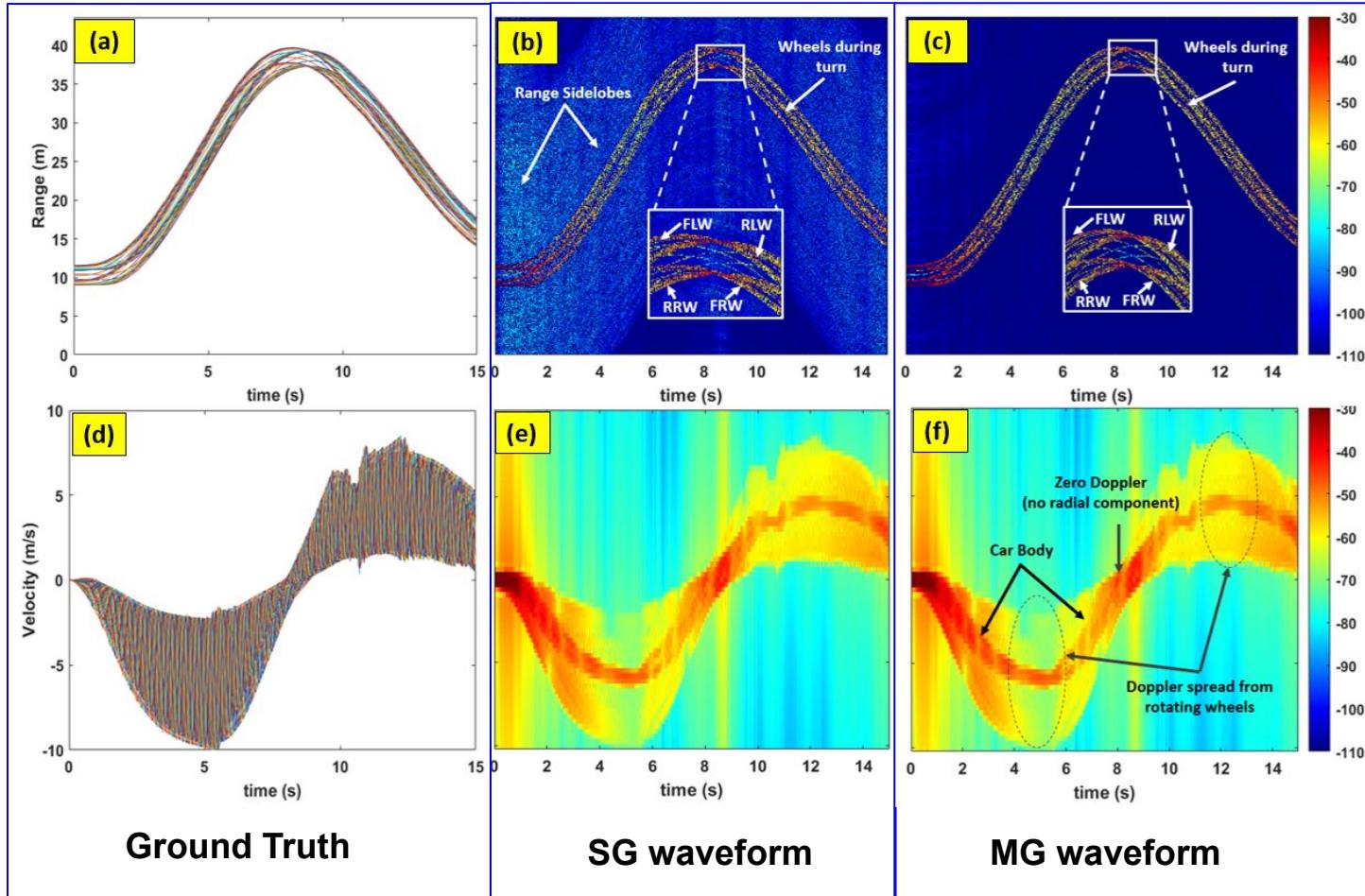
MG waveform



### Key Observations:

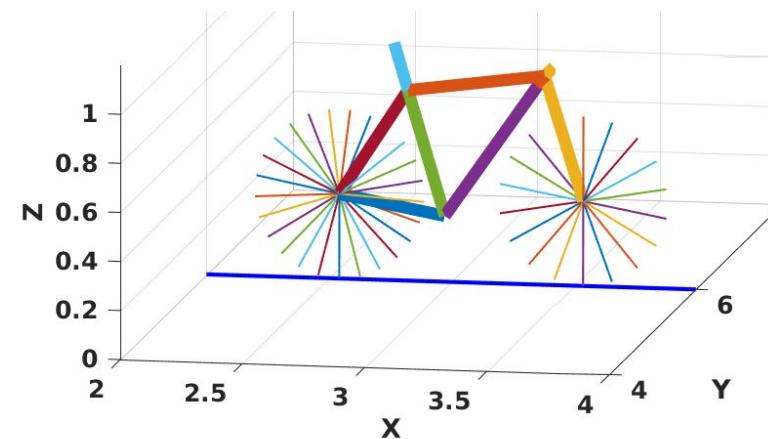
1. The extended target model of the car manifests itself over multiple range-Doppler bins.
2. The power of the reflected signal from the car causes the fluctuations in colour in the range-Doppler plot.
3. Range sidelobes are suppressed in the MG waveform making it Doppler resilient.

# 5.3 Car Radar Signatures



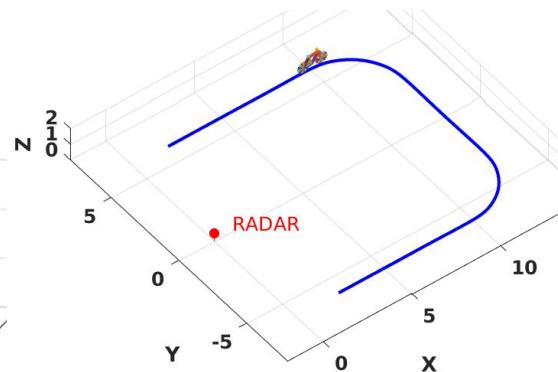
# 5.4 Extended target model of a bicycle

Primitives are rods

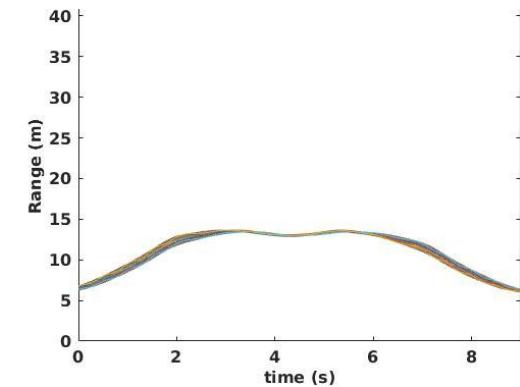


$$\sigma_b[n] = \frac{2\pi a_b L_b^2}{\lambda} \cos^2(\theta_b[n]) \left( \frac{\sin(kL_b \sin \theta_b[n])}{kL_b \sin \theta_b[n]} \right)^2$$

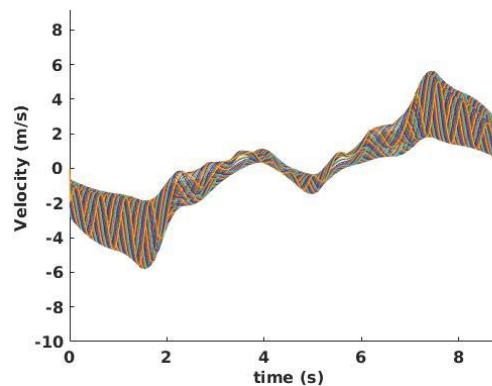
The metal rods of the frame and the metal rods of the spokes are modelled in this electromagnetic model



Range-time ground truth



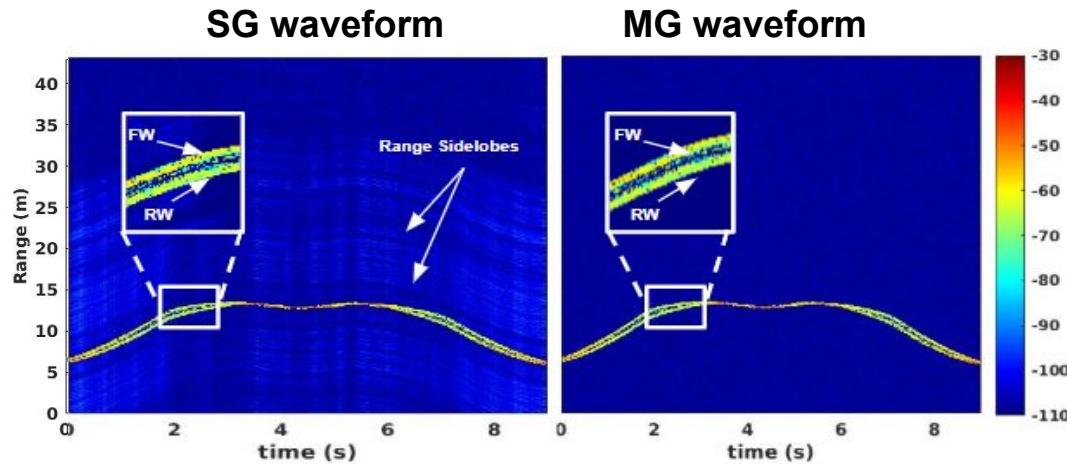
Doppler-time ground truth



# 5.5 Extended Target Model: Bicycle radar signatures

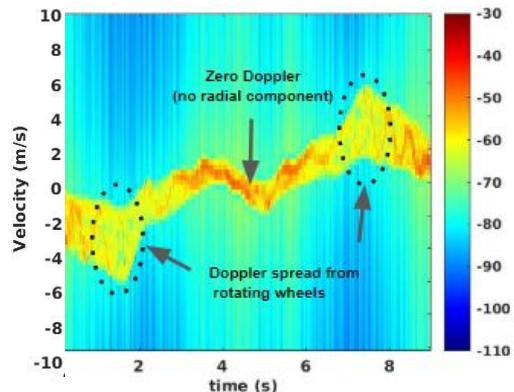
## Range-time plot

1. Range-sidelobes are suppressed in the MG waveform
2. Micro-range information from the wheels is visible

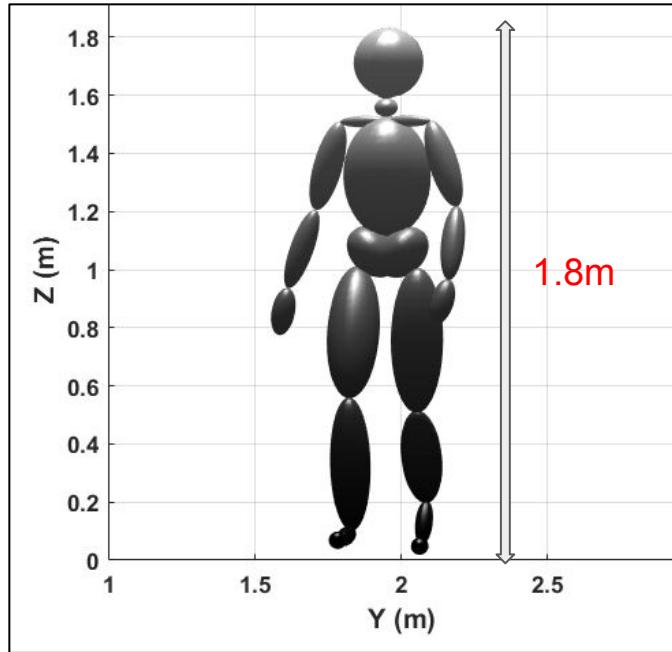


## Doppler-time plot

1. The aspect angle variation manifests itself in the variation of the received power and we can see it on the colour bar
2. When the bicycle is directly in front of the radar, it is moving in the transverse direction hence there is zero Doppler in the received signal



## 5.6 Extended target model of a pedestrian



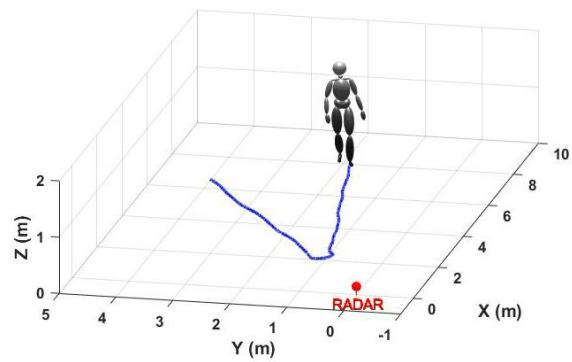
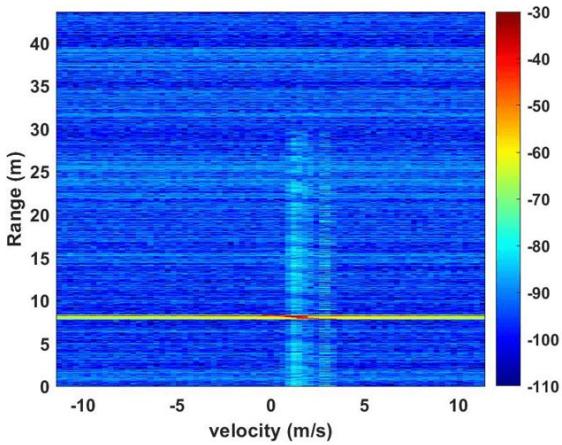
Radar cross section of an ellipsoid

$$\sigma_b[n] = \frac{\frac{1}{4}R_b^4H_b^2}{R_b^2 \sin^2 \theta_b[n] + \frac{1}{4}H_b^2 \cos^2 \theta_b[n]}$$

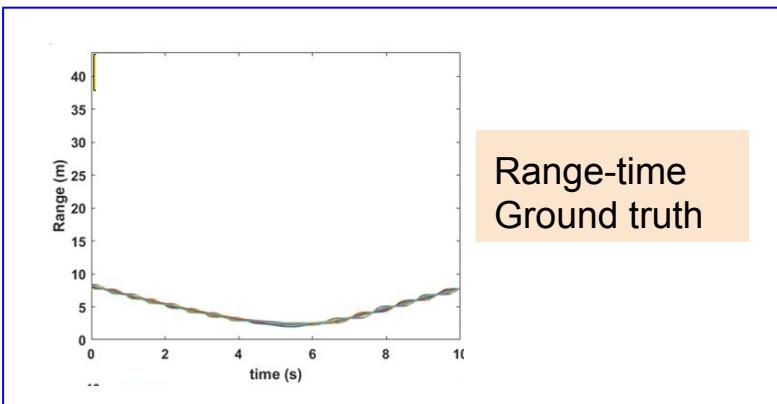
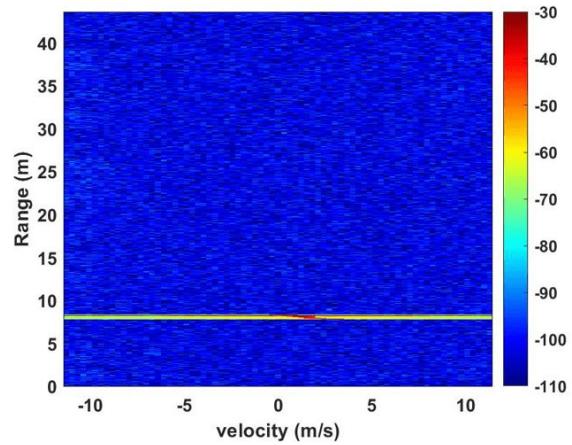
$H_b$  = length of the ellipsoid  
 $R_b$  = radius of the ellipsoid

# 5.7 Pedestrian MG waveform vs SG waveform

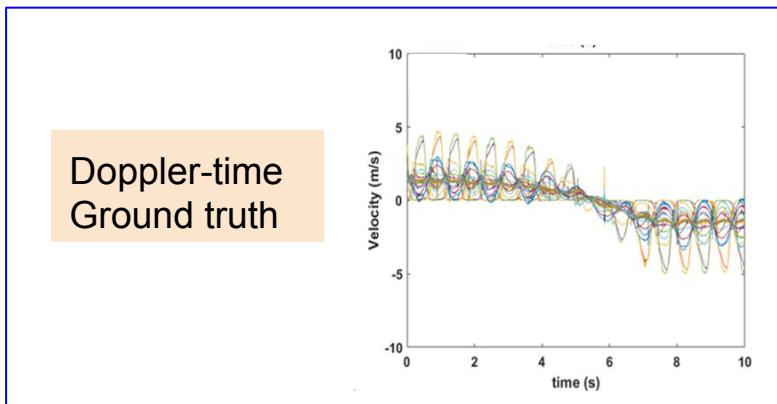
SG Waveform



MG Waveform



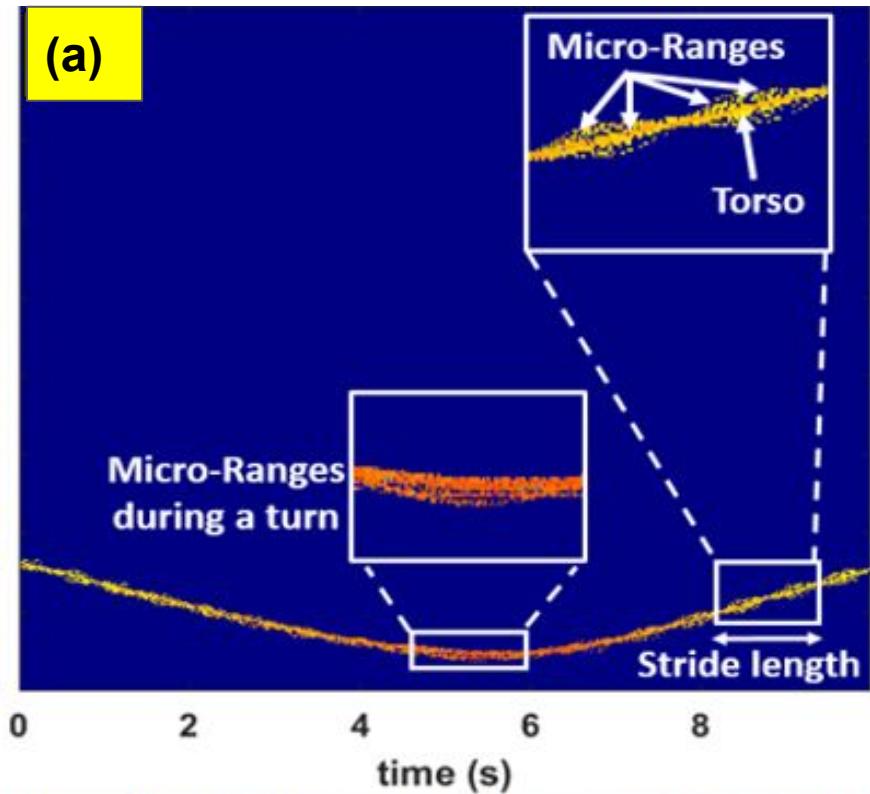
Range-time  
Ground truth



Doppler-time  
Ground truth

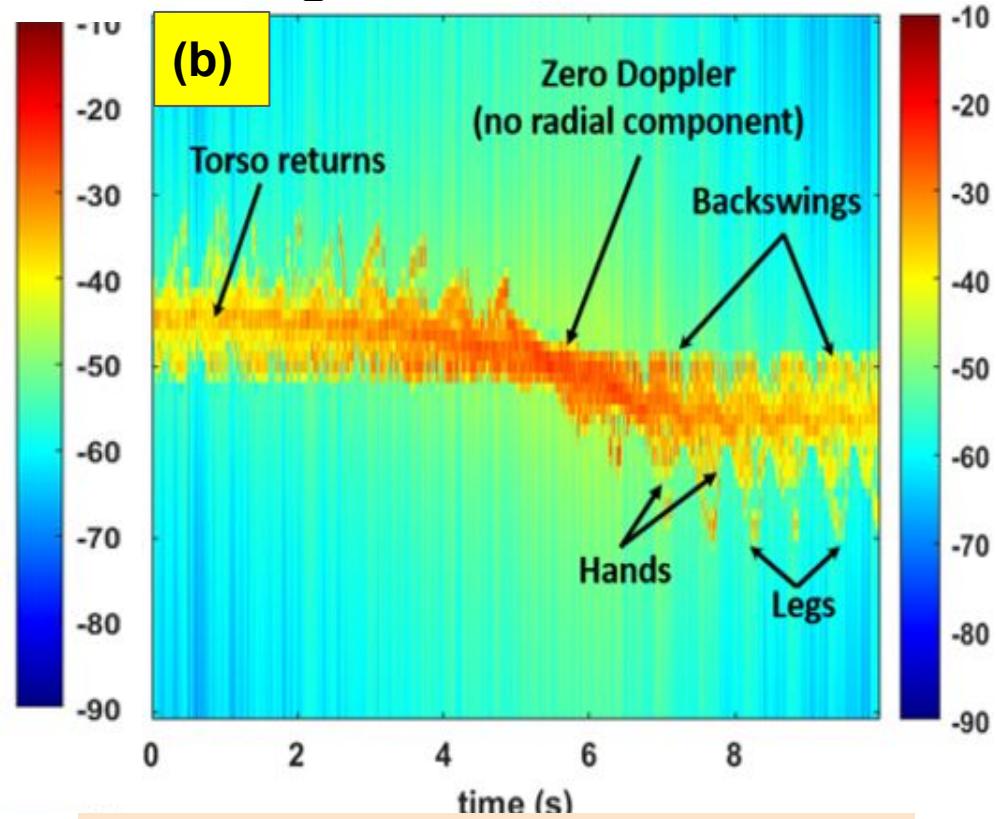
# 5.8 Pedestrian Radar Signatures

(a)



In the range-time plot We can see the stride length of the pedestrian.

(b)

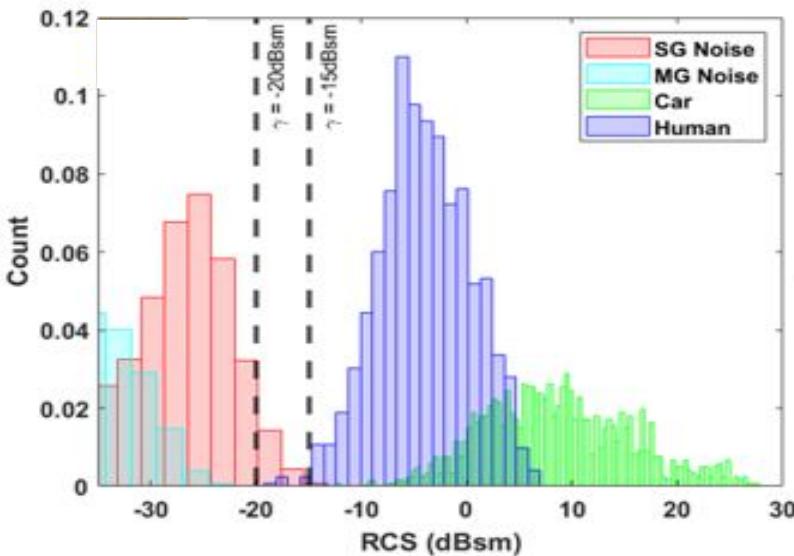


In the Doppler time plot, we can see the swing of the arms and legs of the pedestrian

# 6.1 Detection Methodology

## RCS calculation after range compensation

$$\sigma_{\text{target}}(m) = \left\| \sum_{b=1}^B \chi_{RT}[m, r_b] r_b^2 e^{j2\frac{2\pi}{\lambda}r_b} \right\|^2$$



Generate range-time plot for a car and a pedestrian moving simultaneously in front of radar

Range compensate the radar range-time plot

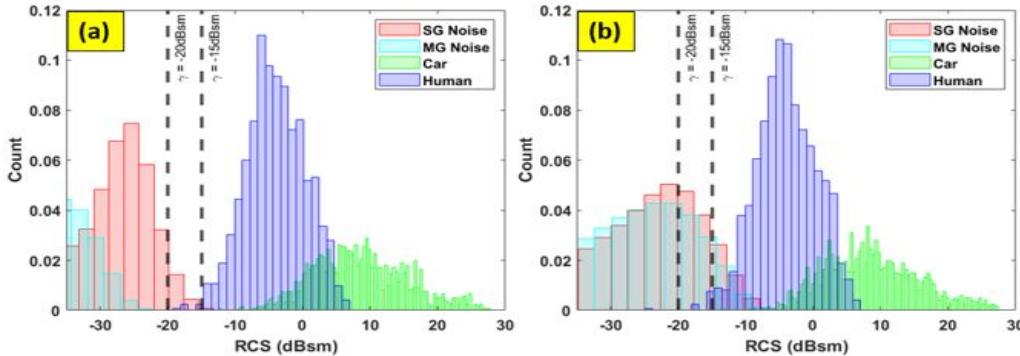
Using ground truth range-time positions of each target and the radar range-time plot

The target locations in the radar range-time plot are time samples of the target radar cross section

The non target locations in the radar range-time are a time samples of the noise.

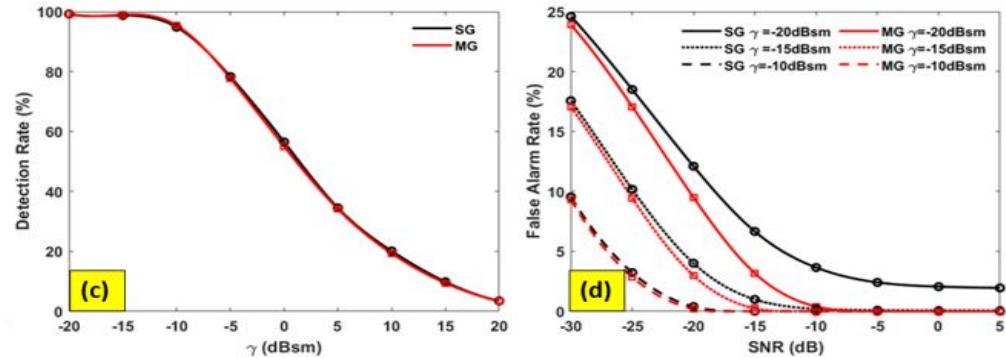
Using the time samples generate histograms of the noise and targets

## 6.2 Radar Operating Curves



- (a) Radar cross section histogram at an SNR of -20 dB
- (b) Radar cross section histogram at an SNR of +5 dB

- (c) Detection threshold vs probability of detection
- (d) False alarm probability vs SNR for three different detection thresholds.



# 7.1 Conclusion

## What we did:

1. Designed an ultra short range Automotive Radar based on the 802.11ad protocol
2. Changed the transmit waveform to improve the detection on radar signatures for dynamic targets
3. Constructed an extended target model and processed high resolution radar signatures for typical automotive targets

## What we found:

4. The MG radar, on comparing with the SG radar, was observed to be performing better on the following metrics:
  - a. Suppressed range-sidelobes by 20 dB for point targets
  - b. Reduced probability of false alarms by 2.5% at low SNR (-20dB to 0dB)
5. Interesting micro-Doppler and micro-range features for different automotive targets

# Questions?

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# Conclusion

1. We designed an ultra short range Radar based on the 802.11ad protocol
2. The transmit waveform was changed slightly to improve the detection on radar signatures for dynamic targets
3. An extended target model was constructed and high resolution radar signatures for typical automotive targets were processed
4. The MG radar was tested with the SG radar and shown to be better using performance metrics

# Detection Methodology

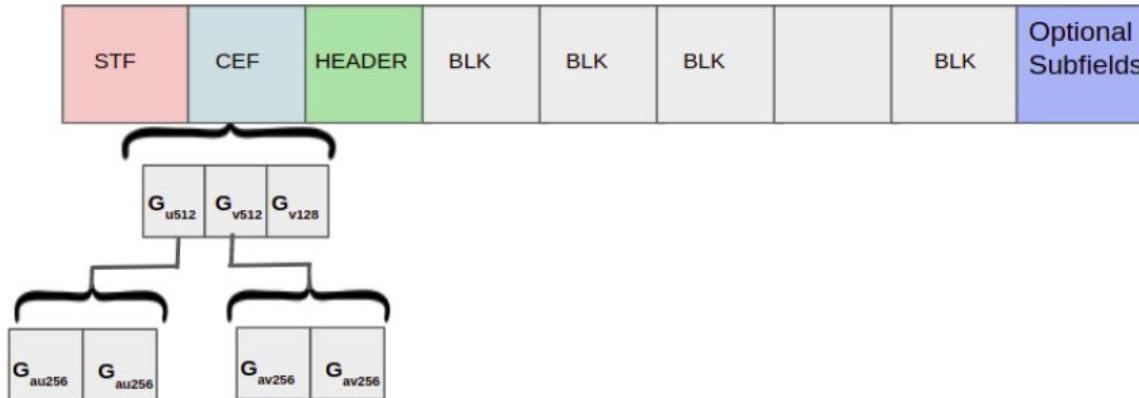
1. For two targets - a car and a pedestrian moving in front of the Radar, we generate a range-time signature
2. Range compensate the range-time signature.
3. From the ground truth range values of each target calculate the radar cross section by doing a coherent sum of all the point scatterers of each individual target

$$\sigma_{\text{target}}(m) = \left\| \sum_{b=1}^B \chi_{RT}[m, r_b] r_b^2 e^{j2\frac{2\pi}{\lambda}r_b} \right\|^2$$

4. The range compensated range-time signature also gives us the virtual noise radar cross section values at all points in time.
5. Plot a histogram of the radar cross section and the virtual noise cross section
6. Use thresholding for detection

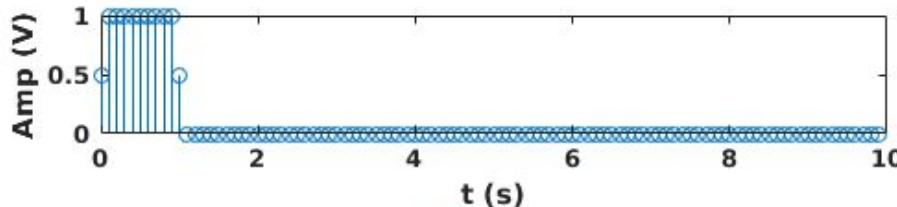
# IEEE802.11AD

- ① 60GHz wireless link for 5G communications between autonomous vehicles
- ② Modes: Control (CPHY), Single Carrier (SCPHY), Orthogonal Frequency Division Multiplexing (OFDM)
- ③ Chip rates: 1.76 GHz / 2.64GHz
- ④ Joint radar and communication framework

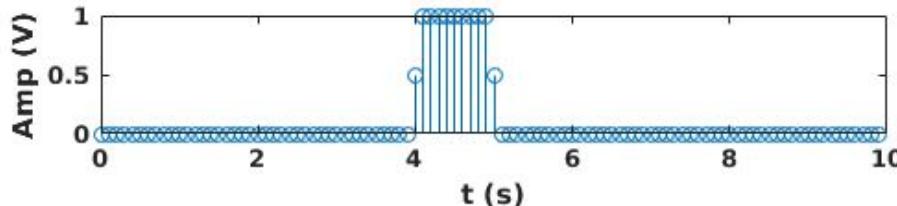


# Pulse - Doppler Radar Operation

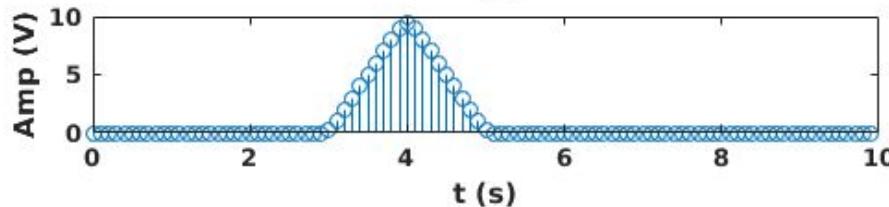
TX Pulse



RX Pulse



Matched Filter

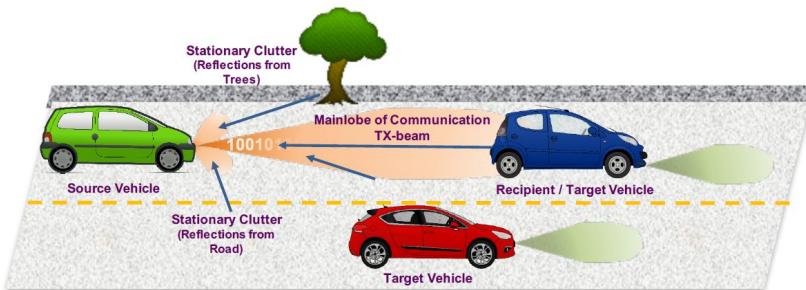


- IEEE 802.11.ad based radar transmits a Golay Coded waveform and the received signal is delayed in time and Doppler shifted
- The received signal after signal processing results in a range-Doppler plot

The last plot gives us the delay at which the target is located

# Previous work

- Preeti Kumari used the CEF in the SC mode in IEEE 802.11.AD to create a Long Range Radar (~200m) and assumed targets as point targets



\*Taken from: P. Kumari et.al IEEE 802.11ad-based radar: An approach to joint vehicular communication-radar system, IEEE Transactions on Vehicular Technology, 2018.

# 802.11.ad based radar

## Perfect Autocorrelation Property

$$G_{a,N}[n] * G_{a,N}[-n] + G_{b,N}[n] * G_{b,N}[-n] = 2N\delta[n].$$

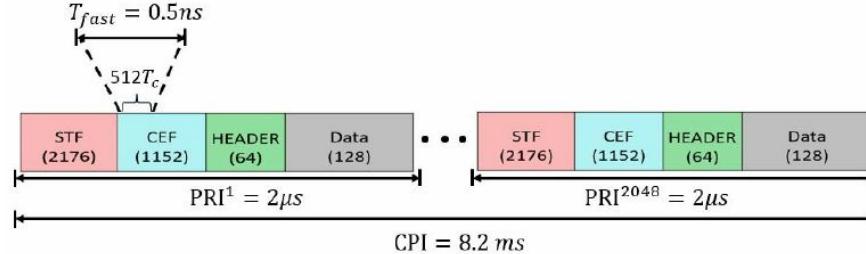
$$(G_{a,N}[n] * G_{a,N}[-n]) + (G_{b,N}[n] * G_{b,N}[-n]) e^{-j\theta} \neq 2N\delta[n],$$

- In case of Non Stationary targets, the perfect autocorrelation property is not valid and creates range sidelobes due to Doppler in received signal
- Put main plots of above equations here

# Our objectives

1. Create a Short range radar as attenuation is high for 60 GHz radio waves and we are looking for 2 way propagation
2. Solve the range side-lobes due to Doppler problem
3. Since we have a high radar resolution and close range to targets, our targets are modelled as extended targets

# Radar Signal Model and Parameters

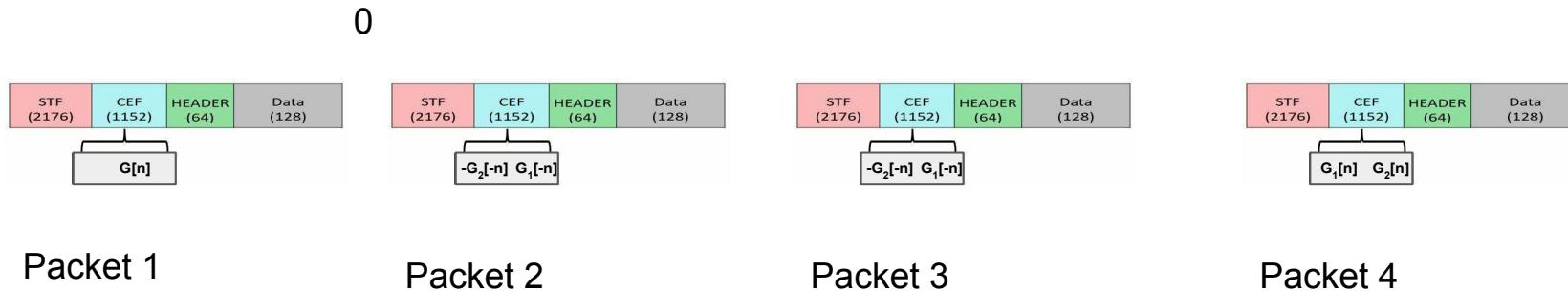


Parameter	Proposed Radar	Commercial SRR
Carrier frequency	60 GHz	77 GHz
Bandwidth	1.76 GHz	2 GHz
Range resolution	0.085 m	0.075 m
Maximum unambiguous range	44m	40m
Pulse repetition interval	$2\mu s$	$1.67\mu s$
Velocity resolution	0.05 m/s	0.3 m/s
Maximum unambiguous velocity	111 m/s	625 m/s

## 2. Modified Golay (MG) signal model

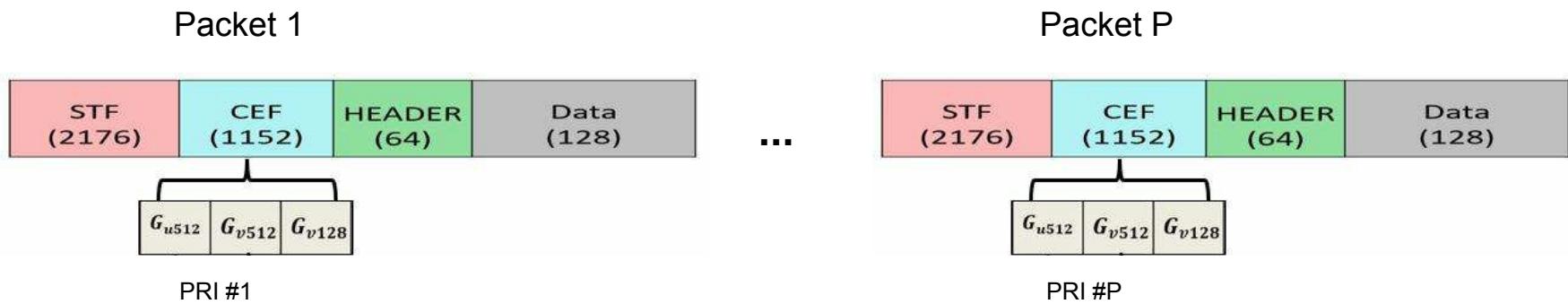
Example for 4 packets

1. Generate PTM sequence of length 2 bits -  $\{0,1\}$
2. In PTM sequence replace all 0's with Golay Pair  $\{G_1[n], G_2[n]\}$  and 1's with Golay Pair  $\{-G_2[-n], G_1[-n]\}$



\*Pezeshki reference

## 2. Standard Golay (SG) signal model



The received signal for P packets after reflection from a point target

$$S_{rx}[n] = \sum_{p=0}^{P-1} \sum_{b=1}^B a_b[n] S_{tx}(nt_s - \tau_b - pT_{PRI}) e^{-j2\pi f_{D_b} p T_{PRI}} + z[n]$$

$\tau_b$  = delay for  $b^{th}$  point scatterer

$a_b$  = reflectivity for  $b^{th}$  point scatterer

$f_{D_b}$  = Doppler for  $b^{th}$  point scatterer

# Modified Golay: Doppler Resilience

$$\Theta = 2\pi f_d \text{PRI}$$

For P packets at the receiver the matched filter looks like this

$$\sum_{p=0}^{P-1} e^{jn\theta} (G_{p,N}[n] * G_{p,N}[n]) \approx 0(G_{0,N}[n] * G_{0,N}[n]) + 1(G_{1,N}[n] * G_{1,N}[n]) + 2(G_{2,N}[n] * G_{2,N}[n]) + \dots + (P-1)(G_{P-1,N}[n] * G_{P-1,N}[n]).$$

- Using the first order Taylor Expansion about 0 for small theta i.e. small Doppler, we make RHS as close to the original perfect autocorrelation property as possible.

# Modified Golay: PTM sequence

Pezeshki et.al, *Doppler resilient Golay complementary waveforms* Trans. Information Theory 2008

Prouhet-Thue-Morse (PTM)  
Sequence

Modified Golay sequence

$$q_p = \begin{cases} 0, & \text{if } p = 0 \\ q_{\frac{p}{2}}, & \text{if } (p \text{ modulo } 2) = 0 \\ \overline{q_{\frac{p-1}{2}}}, & \text{if } (p \text{ modulo } 2) = 1, \end{cases}$$

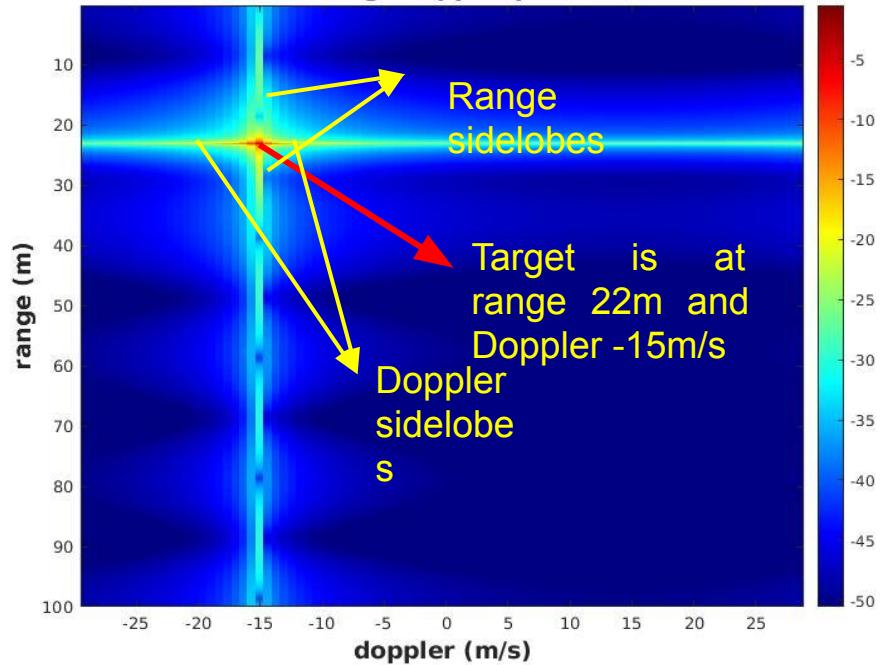
if  $q_p = 0, \{G_{a,N}[n], G_{b,N}[n]\}$   
if  $q_p = 1, \{-G_{b,N}[-n], G_{a,N}[-n]\}$

Example

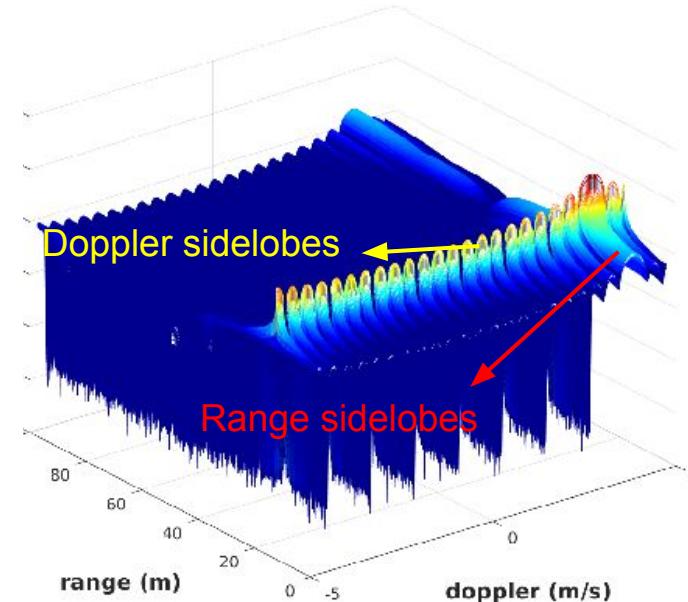
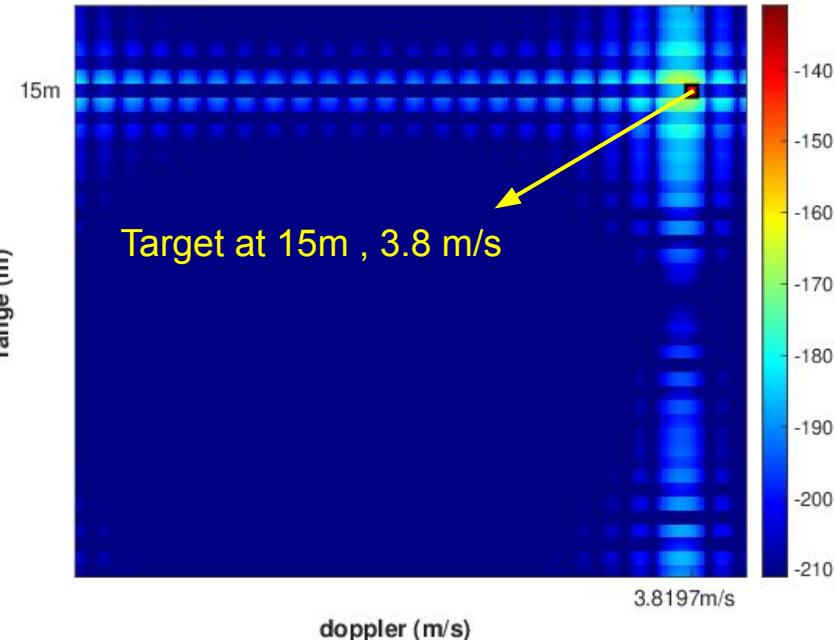
PTM Sequence: [01] :  $G_{a,N}[n], G_{b,N}[n], -G_{b,N}[-n], G_{a,N}[-n]$ :

$$\begin{aligned} \sum_{p=0}^3 e^{-jp\theta} (G_{p,N}[n] * G_{p,N}[-n]) &\approx 1((G_{1,N}[n] * G_{1,N}[-n]) + (G_{3,N}[n] * G_{3,N}[-n])) \\ &\quad + 2((G_{2,N}[n] * G_{2,N}[-n]) + (G_{3,N}[n] * G_{3,N}[-n])) \\ &= (2N + 2(2N))\delta[n] = 6N\delta[n]. \end{aligned}$$

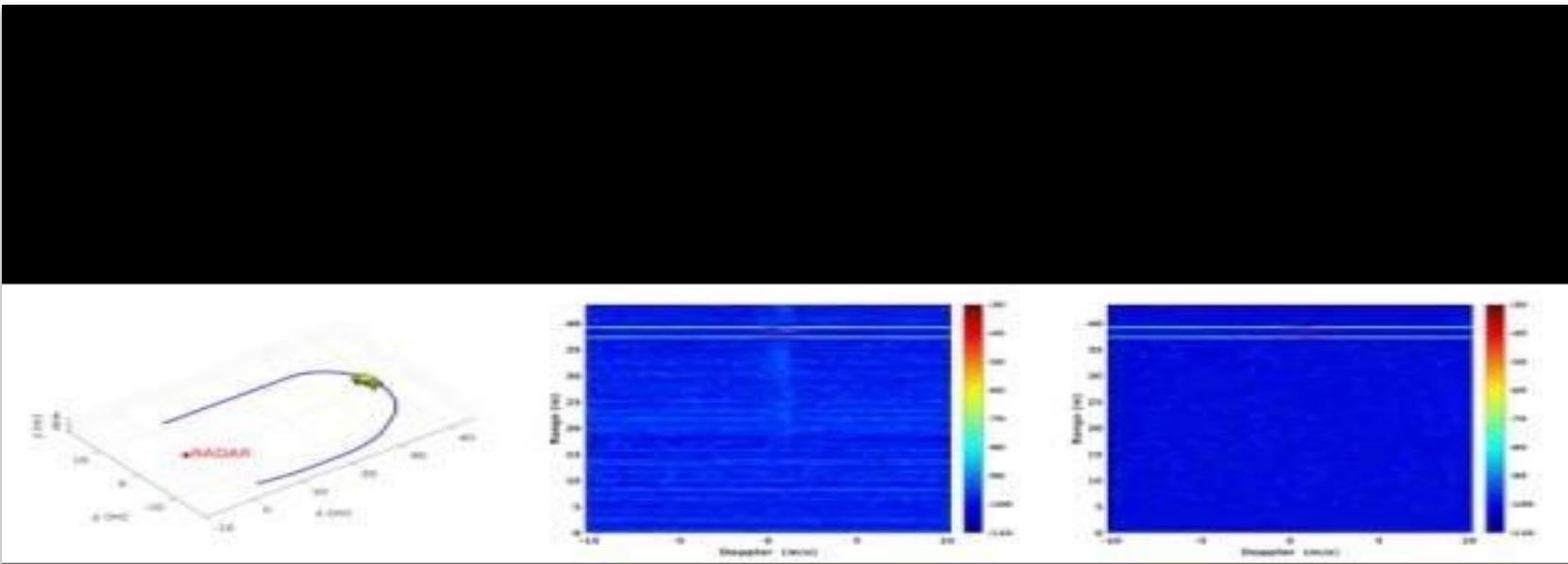
range doppler plot



# An example of a range-Doppler plot



### 3. Car MG vs SG radar

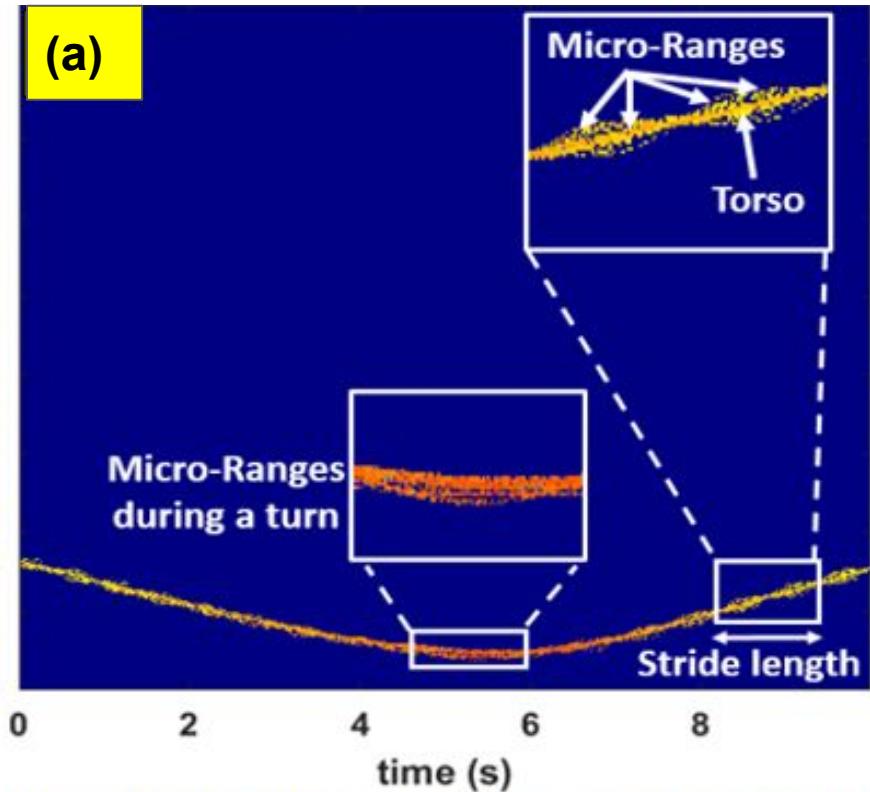


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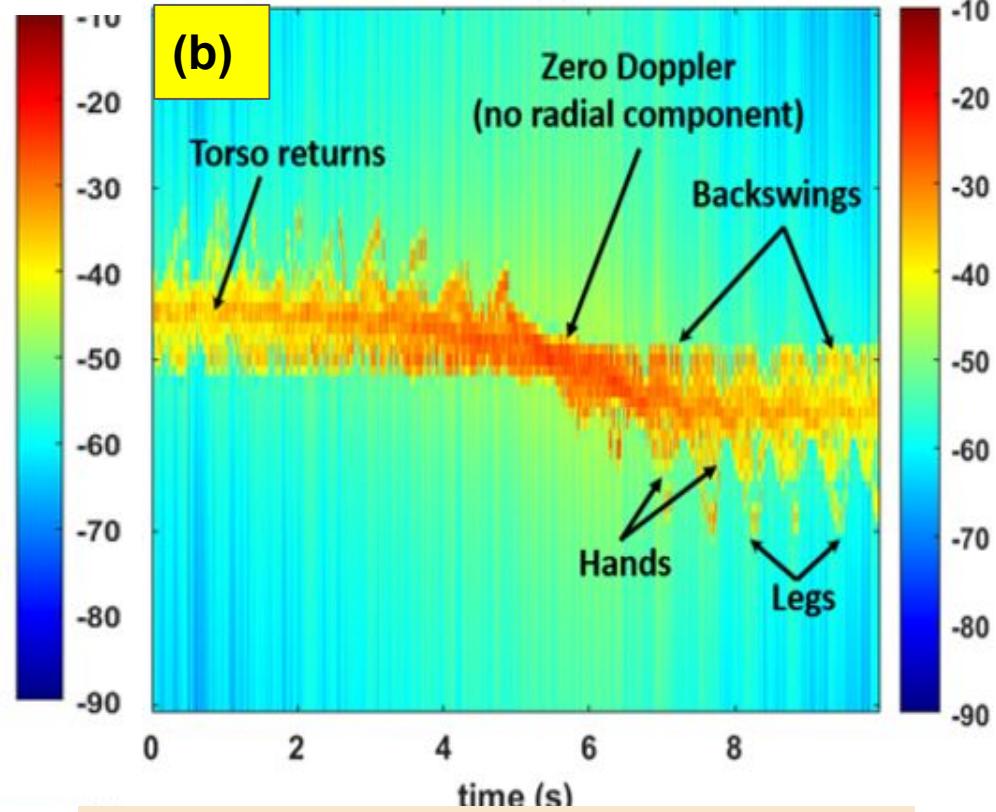
# 5.8 Pedestrian Radar Signatures

(a)



In the range-time plot We can see the stride length of the pedestrian.

(b)

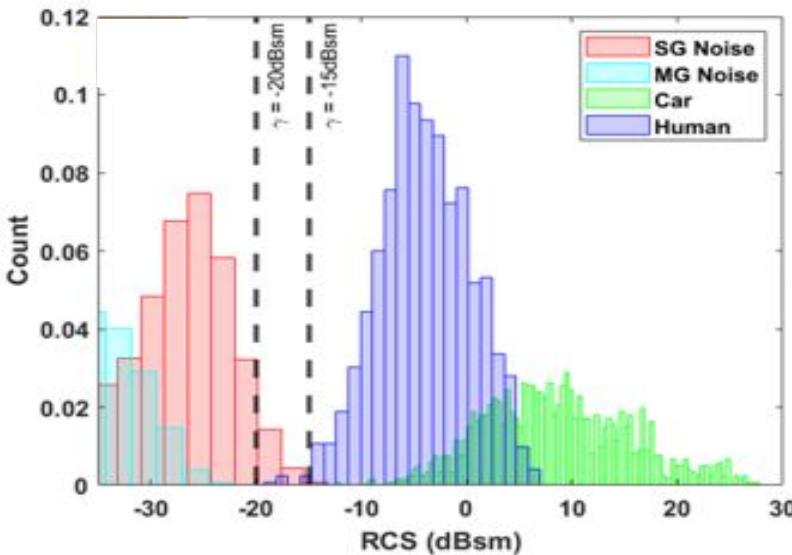


In the Doppler time plot, we can see the swing of the arms and legs of the pedestrian

# 6.1 Detection Methodology

## RCS calculation after range compensation

$$\sigma_{\text{target}}(m) = \left\| \sum_{b=1}^B \chi_{RT}[m, r_b] r_b^2 e^{j2\frac{2\pi}{\lambda}r_b} \right\|^2$$



Generate range-time plot for a car and a pedestrian moving simultaneously in front of radar

Range compensate the radar range-time plot

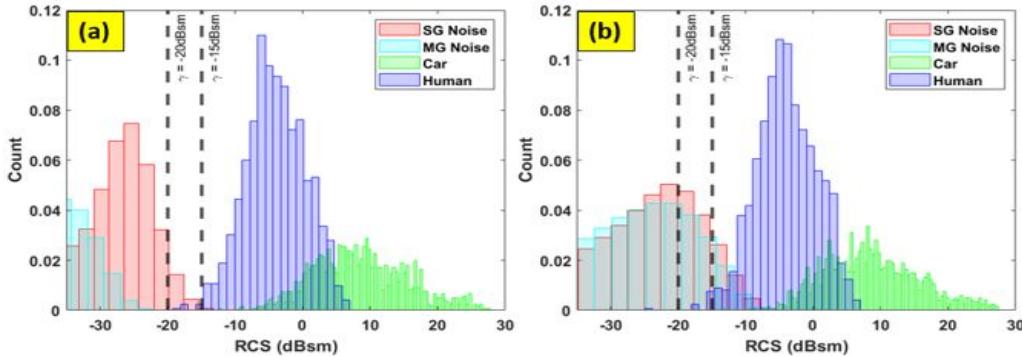
Using ground truth range-time positions of each target and the radar range-time plot

The target locations in the radar range-time plot are time samples of the target radar cross section

The non target locations in the radar range-time are a time samples of the noise.

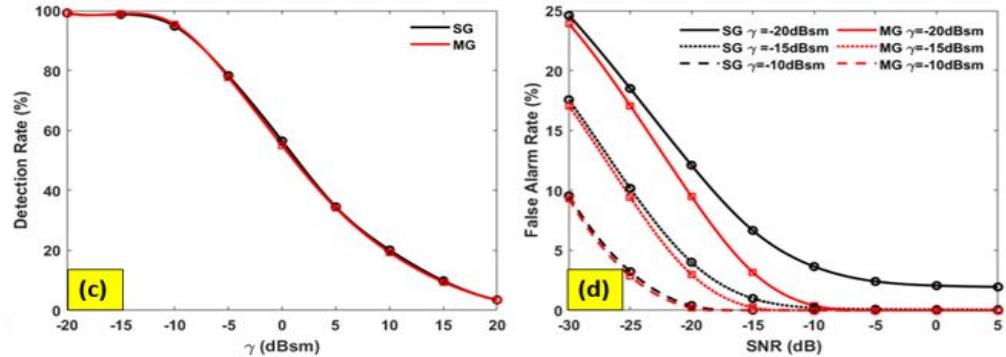
Using the time samples generate histograms of the noise and targets

## 6.2 Radar Operating Curves



- (a) Radar cross section histogram at an SNR of -20 dB
- (b) Radar cross section histogram at an SNR of +5 dB

- (c) Detection threshold vs probability of detection
- (d) False alarm probability vs SNR for three different detection thresholds.



# 7.1 Conclusion

## What we did:

1. Designed an ultra short range Automotive Radar based on the 802.11ad protocol
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1. We designed an ultra short range Radar based on the 802.11ad protocol
2. The transmit waveform was changed slightly to improve the detection on radar signatures for dynamic targets
3. An extended target model was constructed and high resolution radar signatures for typical automotive targets were processed
4. The MG radar was tested with the SG radar and shown to be better using performance metrics

# Detection Methodology

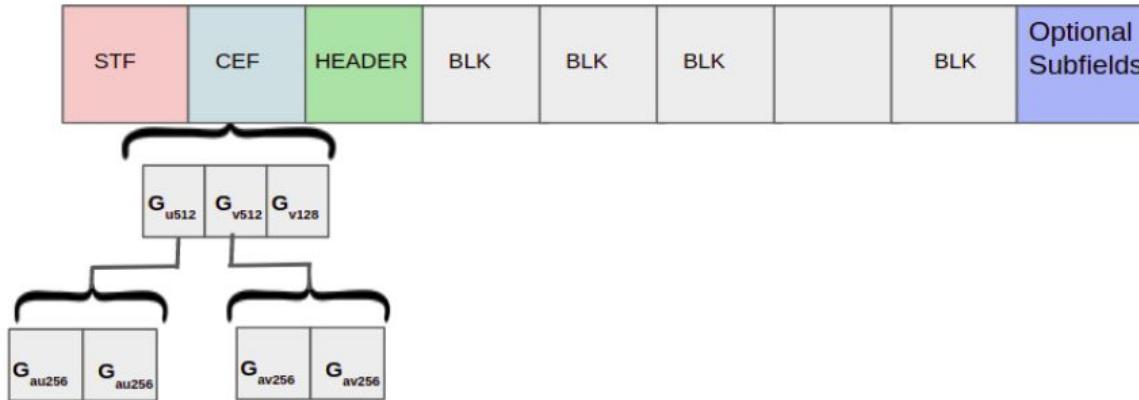
1. For two targets - a car and a pedestrian moving in front of the Radar, we generate a range-time signature
2. Range compensate the range-time signature.
3. From the ground truth range values of each target calculate the radar cross section by doing a coherent sum of all the point scatterers of each individual target

$$\sigma_{\text{target}}(m) = \left\| \sum_{b=1}^B \chi_{RT}[m, r_b] r_b^2 e^{j2\frac{2\pi}{\lambda}r_b} \right\|^2$$

4. The range compensated range-time signature also gives us the virtual noise radar cross section values at all points in time.
5. Plot a histogram of the radar cross section and the virtual noise cross section
6. Use thresholding for detection

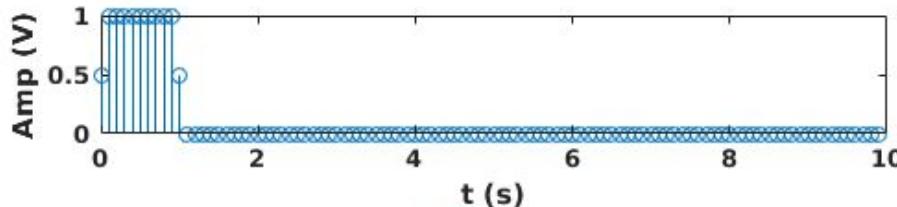
# IEEE802.11AD

- ① 60GHz wireless link for 5G communications between autonomous vehicles
- ② Modes: Control (CPHY), Single Carrier (SCPHY), Orthogonal Frequency Division Multiplexing (OFDM)
- ③ Chip rates: 1.76 GHz / 2.64GHz
- ④ Joint radar and communication framework

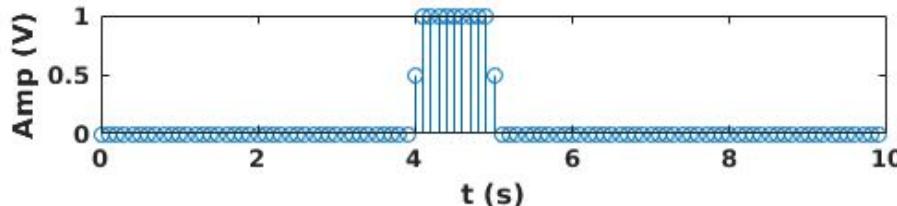


# Pulse - Doppler Radar Operation

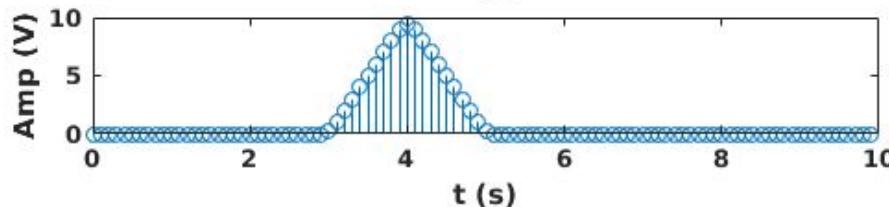
TX Pulse



RX Pulse



Matched Filter

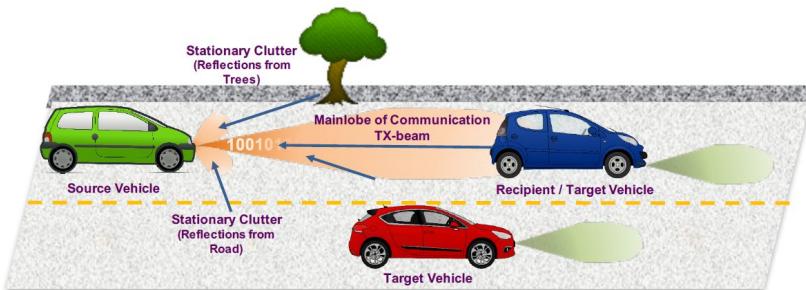


- IEEE 802.11.ad based radar transmits a Golay Coded waveform and the received signal is delayed in time and Doppler shifted
- The received signal after signal processing results in a range-Doppler plot

The last plot gives us the delay at which the target is located

# Previous work

- Preeti Kumari used the CEF in the SC mode in IEEE 802.11.AD to create a Long Range Radar (~200m) and assumed targets as point targets



\*Taken from: P. Kumari et.al IEEE 802.11ad-based radar: An approach to joint vehicular communication-radar system, IEEE Transactions on Vehicular Technology, 2018.

# 802.11.ad based radar

## Perfect Autocorrelation Property

$$G_{a,N}[n] * G_{a,N}[-n] + G_{b,N}[n] * G_{b,N}[-n] = 2N\delta[n].$$

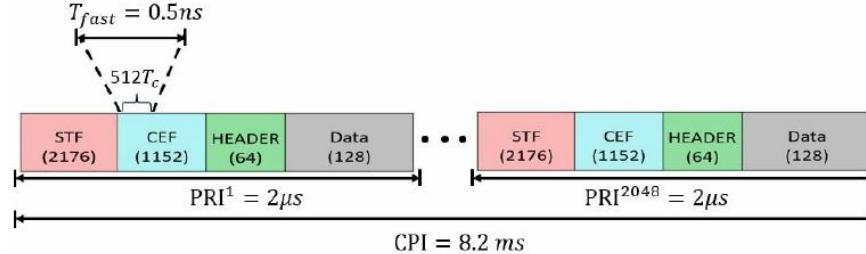
$$(G_{a,N}[n] * G_{a,N}[-n]) + (G_{b,N}[n] * G_{b,N}[-n]) e^{-j\theta} \neq 2N\delta[n],$$

- In case of Non Stationary targets, the perfect autocorrelation property is not valid and creates range sidelobes due to Doppler in received signal
- Put main plots of above equations here

# Our objectives

1. Create a Short range radar as attenuation is high for 60 GHz radio waves and we are looking for 2 way propagation
2. Solve the range side-lobes due to Doppler problem
3. Since we have a high radar resolution and close range to targets, our targets are modelled as extended targets

# Radar Signal Model and Parameters

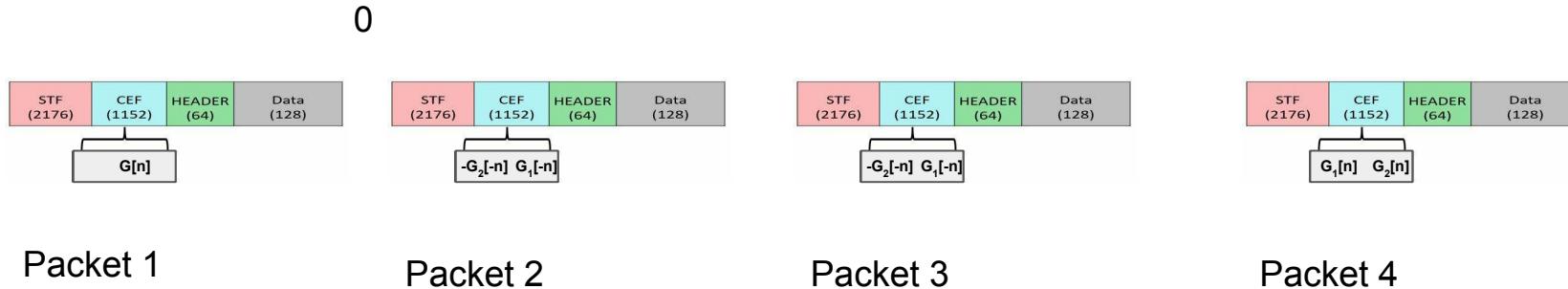


Parameter	Proposed Radar	Commercial SRR
Carrier frequency	60 GHz	77 GHz
Bandwidth	1.76 GHz	2 GHz
Range resolution	0.085 m	0.075 m
Maximum unambiguous range	44m	40m
Pulse repetition interval	$2\mu\text{s}$	$1.67\mu\text{s}$
Velocity resolution	0.05 m/s	0.3 m/s
Maximum unambiguous velocity	111 m/s	625 m/s

## 2. Modified Golay (MG) signal model

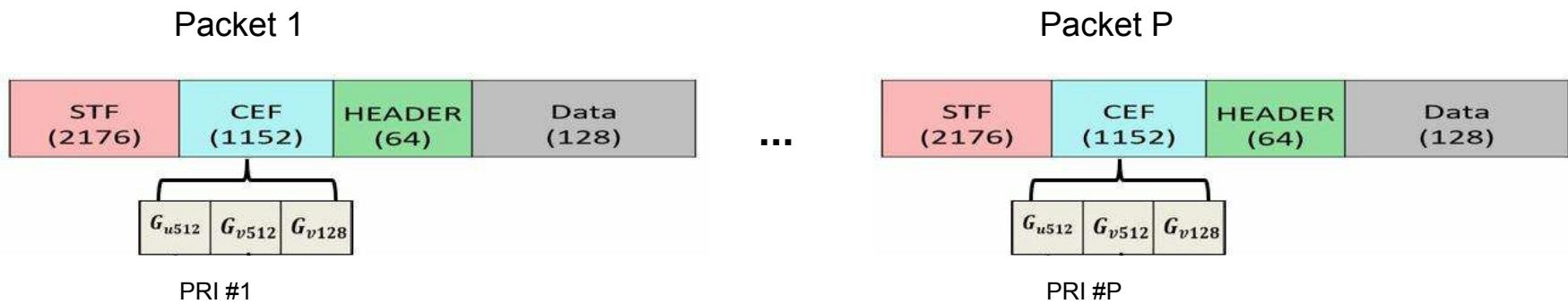
Example for 4 packets

1. Generate PTM sequence of length 2 bits -  $\{0,1\}$
2. In PTM sequence replace all 0's with Golay Pair  $\{G_1[n], G_2[n]\}$  and 1's with Golay Pair  $\{-G_2[-n], G_1[-n]\}$



\*Pezeshki reference

## 2. Standard Golay (SG) signal model



The received signal for P packets after reflection from a point target

$$S_{rx}[n] = \sum_{p=0}^{P-1} \sum_{b=1}^B a_b[n] S_{tx}(nt_s - \tau_b - pT_{PRI}) e^{-j2\pi f_{D_b} p T_{PRI}} + z[n]$$

$\tau_b$  = delay for  $b^{th}$  point scatterer

$a_b$  = reflectivity for  $b^{th}$  point scatterer

$f_{D_b}$  = Doppler for  $b^{th}$  point scatterer

# Modified Golay: Doppler Resilience

$$\Theta = 2\pi f_d \text{PRI}$$

For  $P$  packets at the receiver the matched filter looks like this

$$\sum_{p=0}^{P-1} e^{jn\theta} (G_{p,N}[n] * G_{p,N}[n]) \approx 0(G_{0,N}[n] * G_{0,N}[n]) + 1(G_{1,N}[n] * G_{1,N}[n]) + 2(G_{2,N}[n] * G_{2,N}[n]) + \dots + (P-1)(G_{P-1,N}[n] * G_{P-1,N}[n]).$$

- Using the first order Taylor Expansion about 0 for small theta i.e. small Doppler, we make RHS as close to the original perfect autocorrelation property as possible.

# Modified Golay: PTM sequence

Pezeshki et.al, *Doppler resilient Golay complementary waveforms* Trans. Information Theory 2008

Prouhet-Thue-Morse (PTM)  
Sequence

Modified Golay sequence

$$q_p = \begin{cases} 0, & \text{if } p = 0 \\ q_{\frac{p}{2}}, & \text{if } (p \text{ modulo } 2) = 0 \\ \overline{q_{\frac{p-1}{2}}}, & \text{if } (p \text{ modulo } 2) = 1, \end{cases}$$

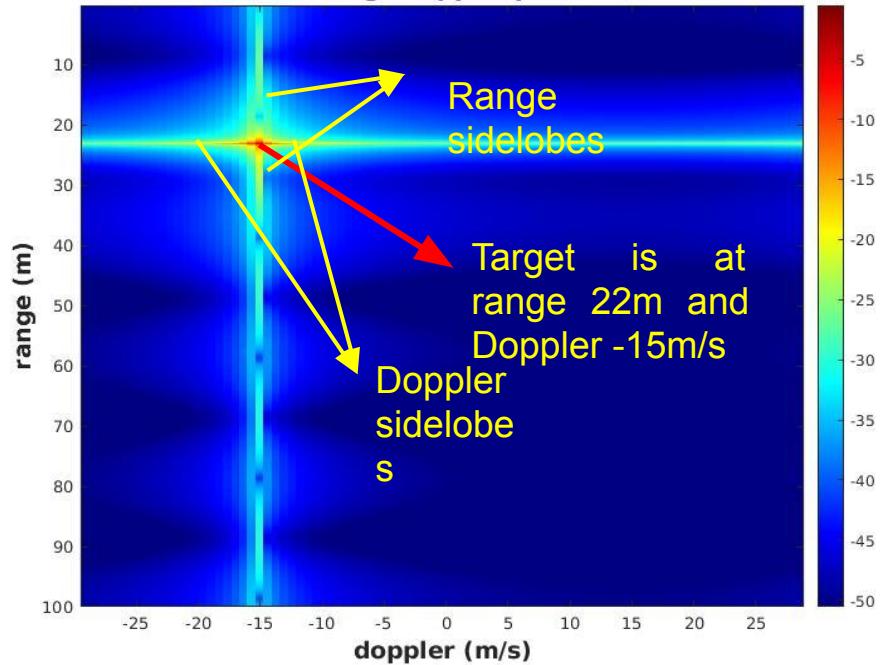
if  $q_p = 0, \{G_{a,N}[n], G_{b,N}[n]\}$   
if  $q_p = 1, \{-G_{b,N}[-n], G_{a,N}[-n]\}$

Example

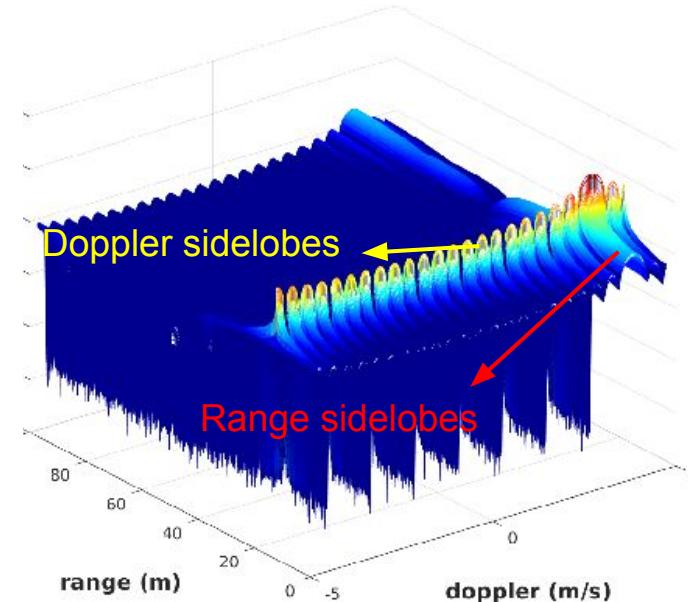
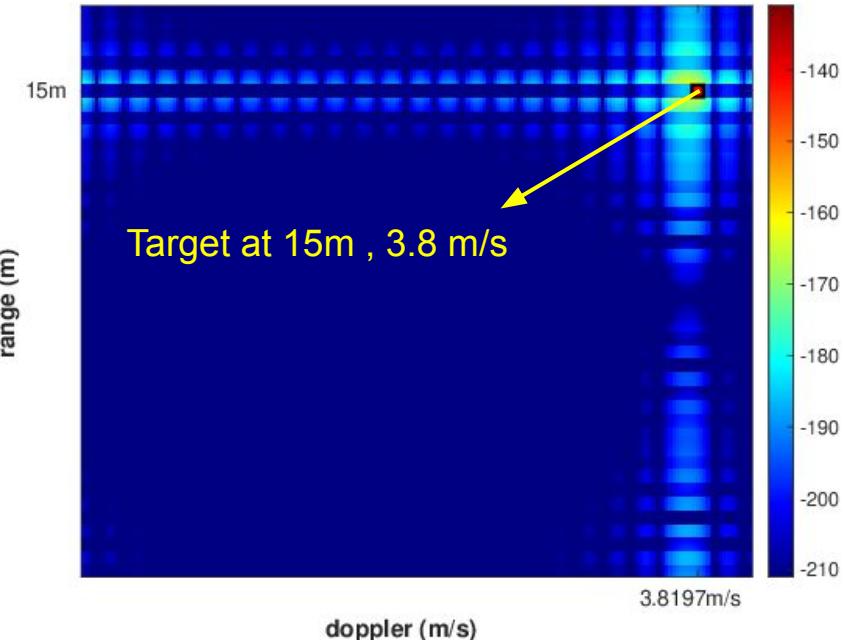
PTM Sequence: [01] :  $G_{a,N}[n], G_{b,N}[n], -G_{b,N}[-n], G_{a,N}[-n]$ :

$$\begin{aligned} \sum_{p=0}^3 e^{-jp\theta} (G_{p,N}[n] * G_{p,N}[-n]) &\approx 1((G_{1,N}[n] * G_{1,N}[-n]) + (G_{3,N}[n] * G_{3,N}[-n])) \\ &\quad + 2((G_{2,N}[n] * G_{2,N}[-n]) + (G_{3,N}[n] * G_{3,N}[-n])) \\ &= (2N + 2(2N))\delta[n] = 6N\delta[n]. \end{aligned}$$

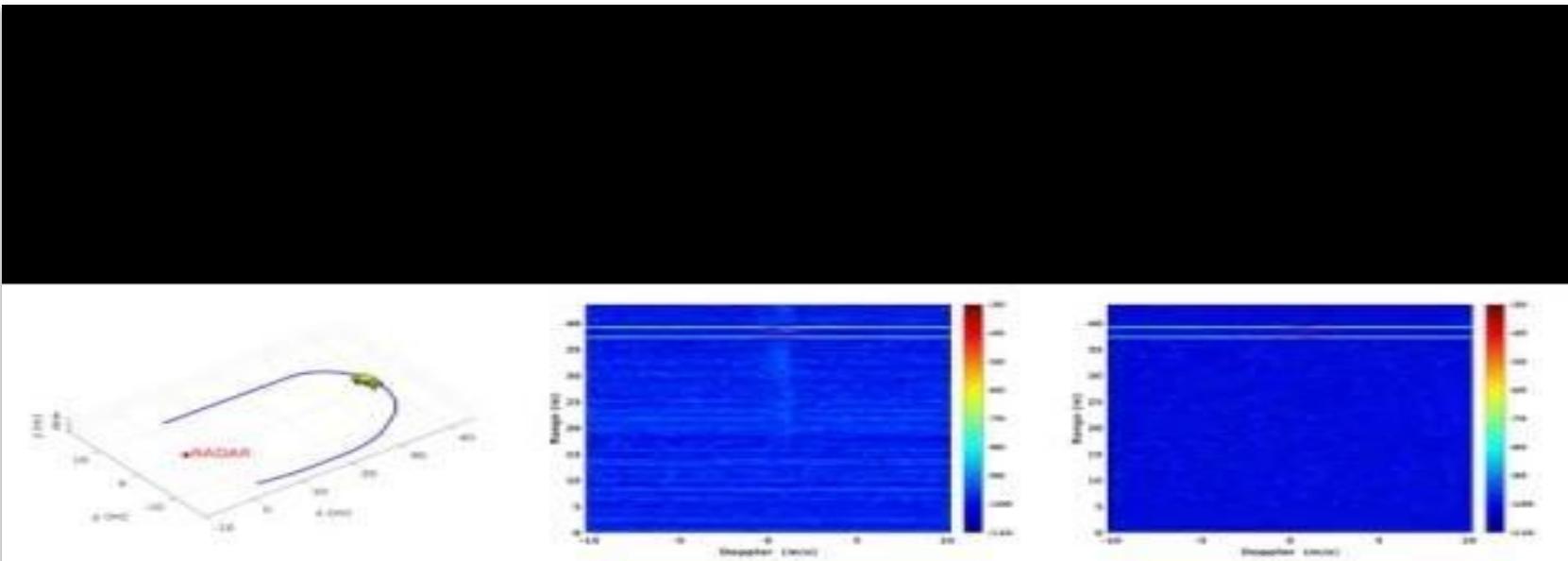
range doppler plot



# An example of a range-Doppler plot



### 3. Car MG vs SG radar



# Acknowledgement

I would like to thank my supervisor Dr. Shobha Sunder Ram for guiding me during this thesis. I would also like to thank Dr. Vijay mishra without whose technical inputs these thesis would not have been possible. Mrs. Shelly Vishwakarma for helping with the data collection and performance metrics. Lastly I'd like to thank Dr. Aditya Jaganathan and Dr. Vivek Bohara for being part of the thesis committee.