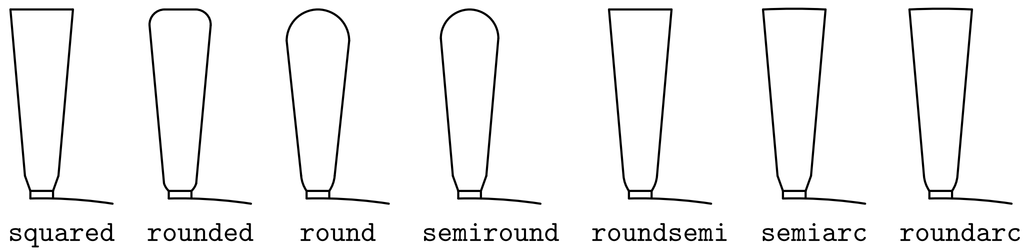
3F — Framework for FEMM

Contents

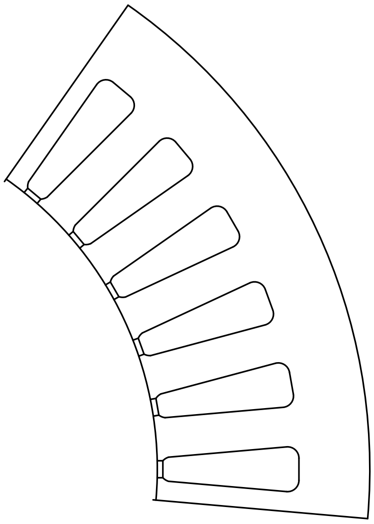
Chapter 1

Geometry

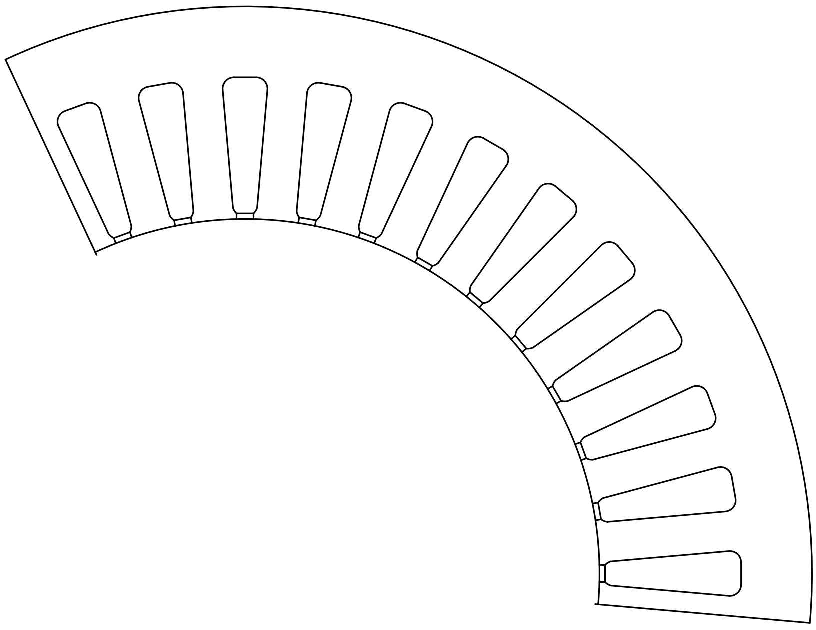
1.1 Slots



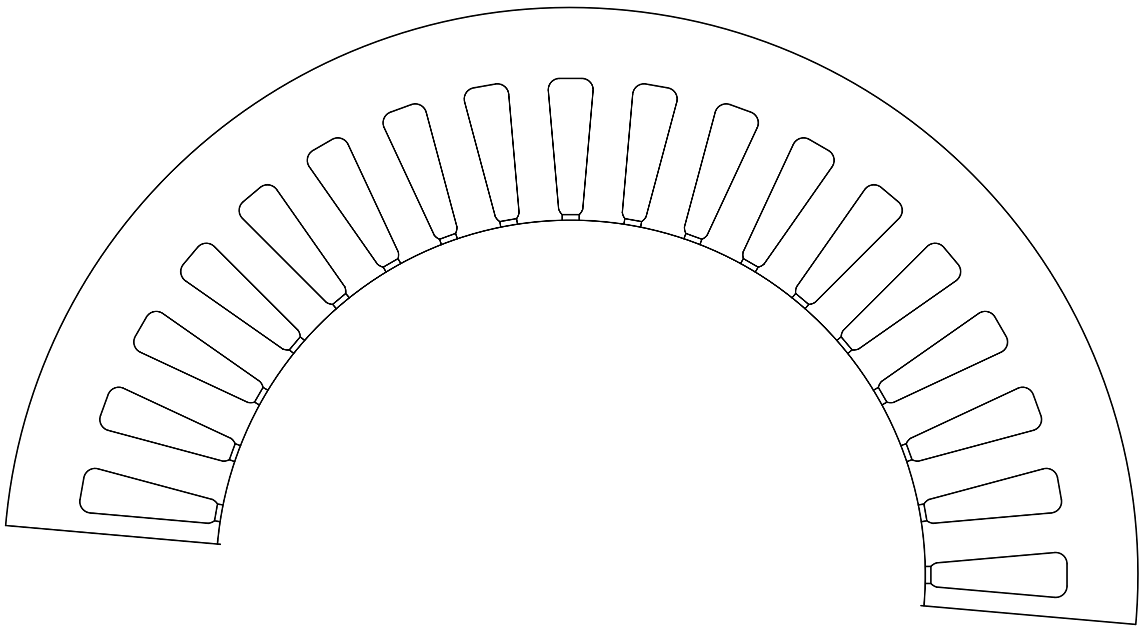
1.2 Stators



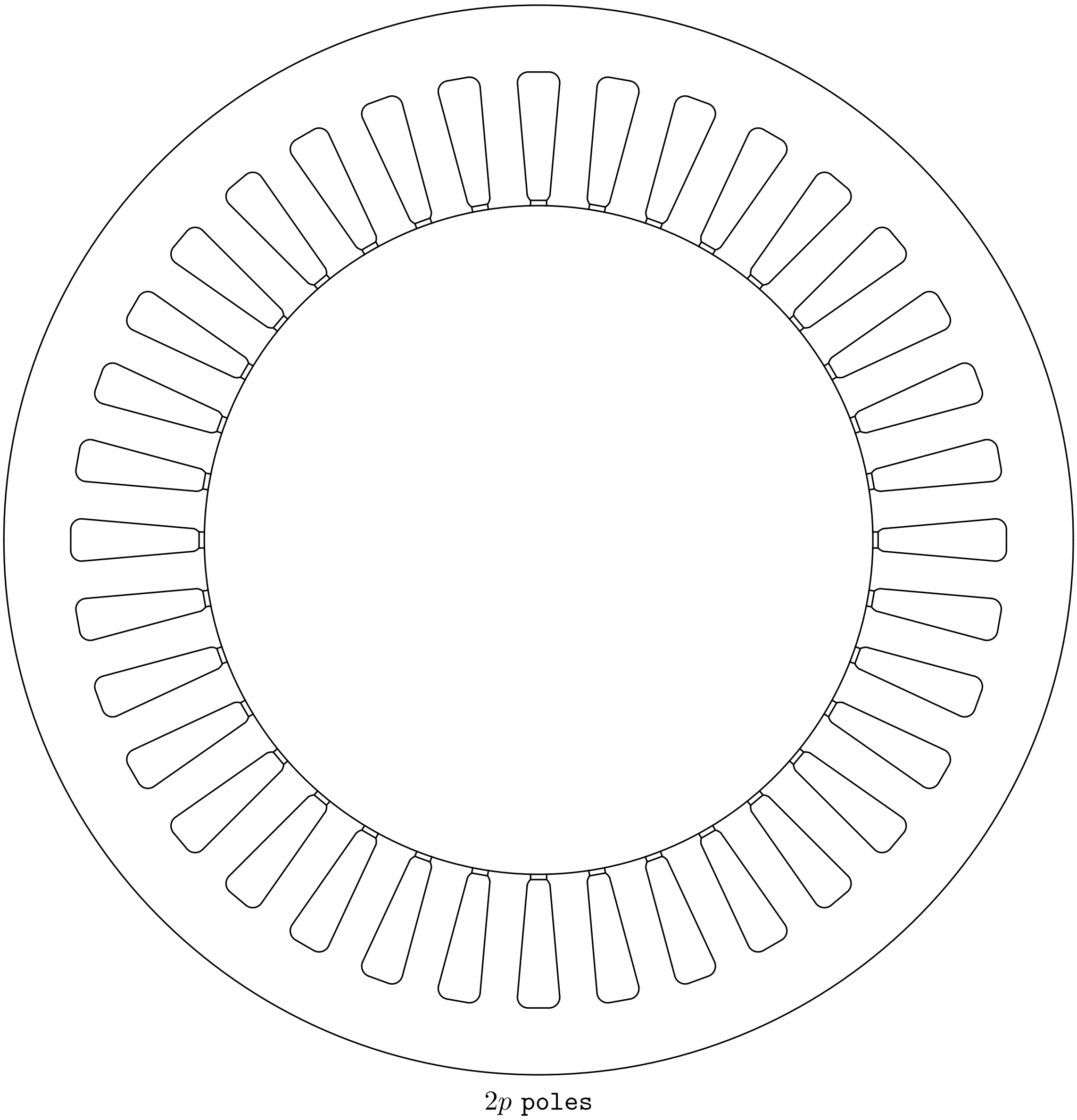
1 pole



2 poles

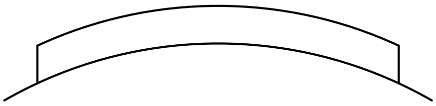


p `poles`

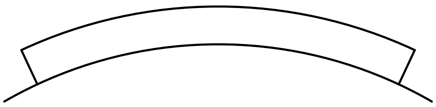


$2p$ `poles`

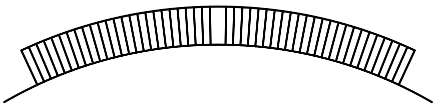
1.3 SPM Magnets



`parallel + rect`

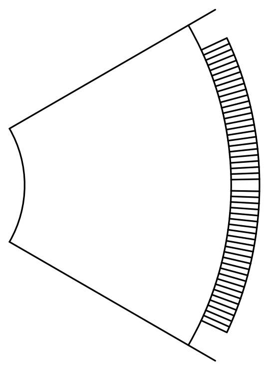


`parallel + trapz`

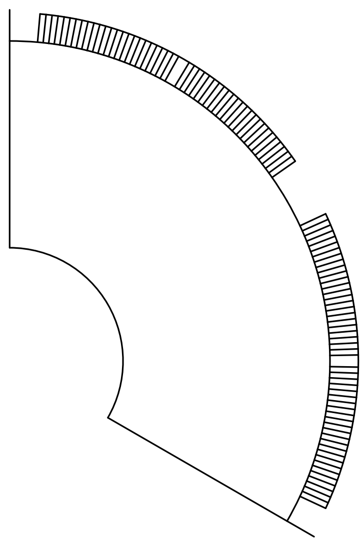


`radial (+ trapz)`

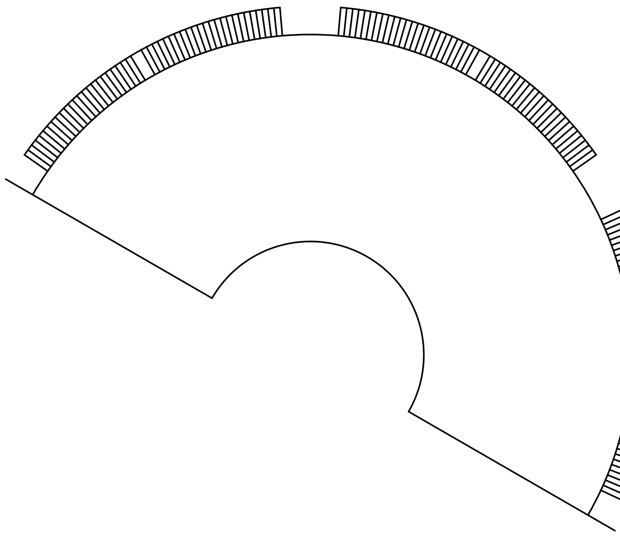
1.4 SPM Rotors



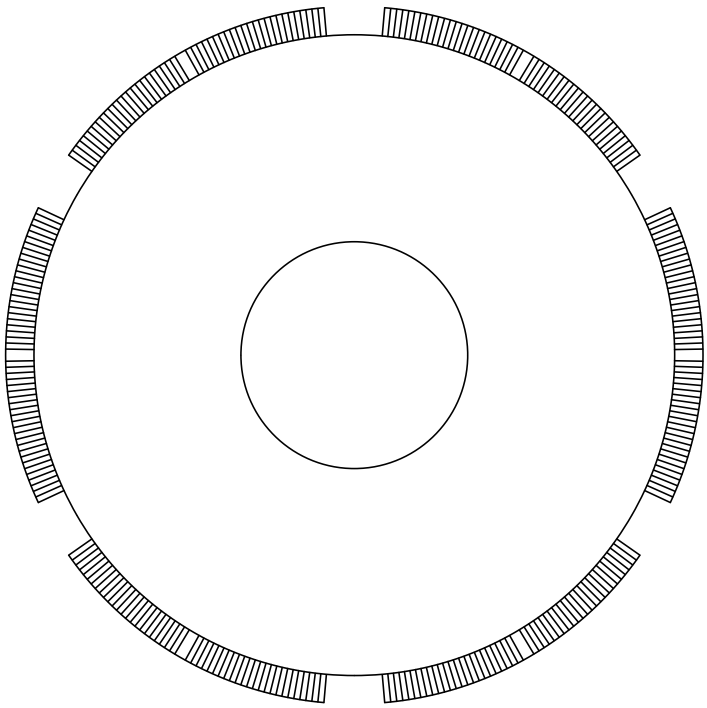
1 pole



2 poles



p poles



$2p$ poles

Chapter 2

Winding

We will characterise a winding through

Name	Math symbol	Code symbol
N. of phases	m	`m`
N. of coils	N_{coils}	`coils`
N. of turns per coil	N_{turns}	`turns`
N. of layers	N_{layers}	`layers`
N. of parallel paths	n_{pp}	`ppath`
N. of conductors in slot	n_{c}	`nc`

Typically, given a lamination stack with Q slots

$$N_{\mathrm{coils}} = \frac{Q}{2} N_{\mathrm{layers}}$$

so if the number of layers is one, the number of coils is half the number of slots, given the fact that a coil side occupies a full slot.

$$n_{\mathrm{c}} = N_{\mathrm{layers}} N_{\mathrm{turns}}$$

This equation means that in each slot there are n_{c} conductors of any phase due to the turns in each coil side in each layer. We bring this number to the equivalent series-connected machine, through the number of parallel paths:

$$n_{\mathrm{cs}} = \frac{n_{\mathrm{c}}}{n_{\mathrm{pp}}}$$

This number, n_{cs}, is related to the complete set of slots, while the previous n_{c} was related only to a part of them, due to the parallel connection of the winding. Thanks to this fact, we can compute the whole number of conductors for each phase, through

$$N_{\mathrm{c}} = \frac{Q\, n_{\mathrm{cs}}}{m}$$

Therefore the full number of turns for each phase, which will appear in the flux linkage, is $N_\mathrm{c}/2$. This number is valid for both the real machine and the equivalent series-connected one.

Another equivalence that we will use is the wye-equivalence. For both the wye and the delta connection of the windings, we will refer to the wye equivalent winding. Each winding sustains either the line(-to-line) voltage in the wye (delta) connection. Therefore

$$U_\mathrm{w} = \frac{U_\mathrm{N}}{\sqrt{3}} \quad [\mathrm{V}] \qquad \text{delta connection}$$

$$U_\mathrm{w} = U_\mathrm{N} \quad [\mathrm{V}] \qquad \text{wye connection}$$

In this way we can obtain the winding current directly from the power

$$I_\mathrm{w} = \frac{P}{3U_\mathrm{w}\cos\varphi} \quad [\mathrm{A}]$$

and use it as the design current for the winding itself. In fact, if each turn is made by some wires with a full section S_c, we will refer to the equivalent turn section

$$S_\mathrm{c,eq} = n_\mathrm{pp} S_\mathrm{c} \quad [\mathrm{mm}^2]$$

which sees the complete winding current, giving the current density

$$J = \frac{I_\mathrm{w}}{S_\mathrm{c,eq}} \quad [\mathrm{A/mm}^2]$$

It is important to highlight that this current density is the conductor's one, while the slot current density is given by

$$J_\mathrm{slot} = k_\mathrm{fill} J \quad [\mathrm{A/mm}^2]$$

where the fill factor, k_fill, represents the ratio between the actual conductor area in the slot and the slot section. Depending on the starting point, one can find the rms current in the slot through

$$I_\mathrm{slot} = J_\mathrm{slot} S_\mathrm{slot} = n_\mathrm{cs} I_\mathrm{w} \quad [\mathrm{A}]$$

2.1 Space vectors

2.2 Sinusoidal dq control

2.3 Trapezoidal control