

# PPML - RCWA

## (Periodically Patterned Multi Layer – Rigorous Coupled Wave Analysis)

### User manual



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**WARNING! PPML 3.0 is a major release, that includes conducting interfaces between the layers. The software interface of all the functions is changed with respect to previous versions. Compatibility is however fully guaranteed. Look at the end of this Manual for details.**

INCLUDED FOLDERS:

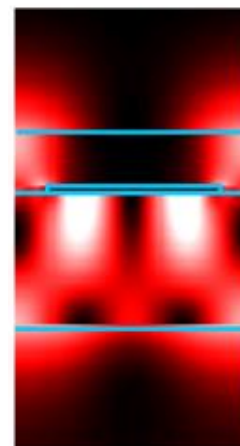
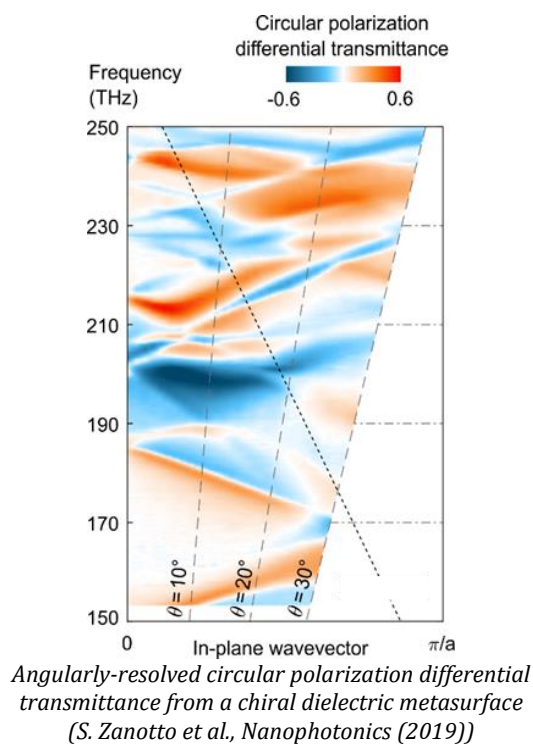
**general** ----- utility functions (scattering matrix propagation, complex square root)

**1d\_tm** ----- functions for 1d patterned multilayers, TM polarization

**1d** ----- functions for anisotropic 1d patterned multilayers

**2d\_rect; 2d\_Lshape** ---- functions for 2d patterned multilayers (rectangular & L-shaped inclusions)

**examples** ----- some examples



Intracavity field in a patterned membrane  
(S. Zanotto and A. Tredicucci, Scientific Reports 2016;  
6: 24592)

## Contents of the 1d\_tm folder:

**RTA\_1d\_tm** - calculates reflectance, transmittance, and layer-by-layer absorbance

**SM\_1d\_tm** - calculates the 2x2 scattering matrix

**field\_1d\_tm** - calculates some components of the E and S fields inside the structure

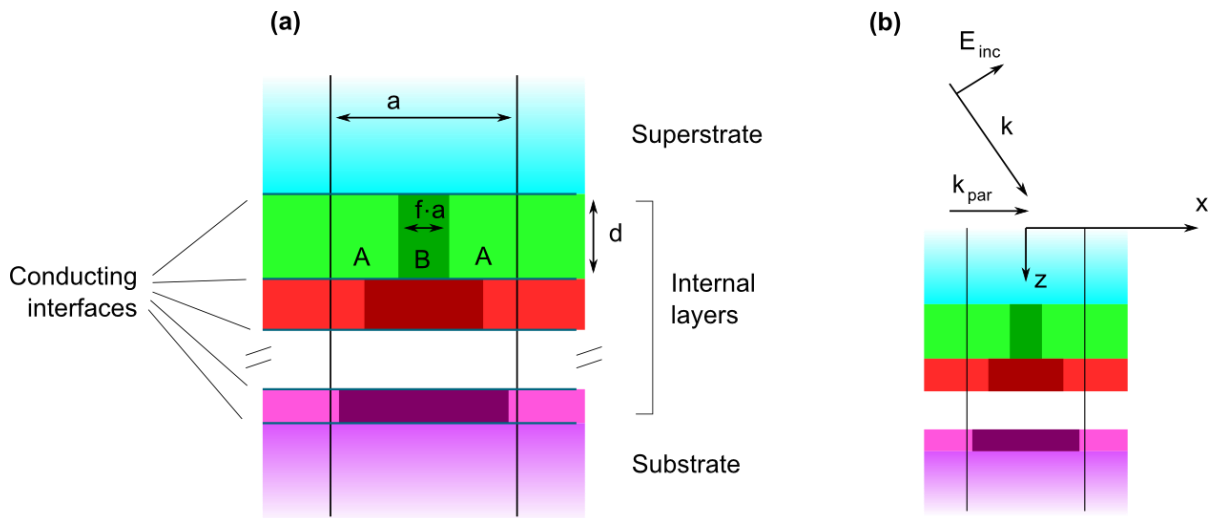
The “1d\_tm” functions solve the periodically patterned multilayer problem in the 1-d geometry (fig. 1a). Only TM-polarization is considered, i.e., the H-field has the sole  $y$  component. This corresponds to  $p$ -polarized plane waves incident on a plane orthogonal to the 1d pattern (see fig. 1b). Their wavevector has modulus  $k (=k_0 \cdot \sqrt{\epsilon_{sup}})$ , being  $k_0$  the vacuum wavevector and  $\epsilon_{sup}$  the superstrate permittivity; moreover, the incident wavevector has a projection  $k_{par}$  along the  $x$  axis.

The template structure comprises a superstrate, a substrate, and a number of internal layers. Super- and substrate are not patterned, while the internal layers can be. The unit cell geometry consists of a centered stripe of material B surrounded by material A. Super- and substrate have isotropic permittivity, while internal layers can have anisotropic permittivity of the form

$$\begin{pmatrix} \epsilon_x & 0 & 0 \\ 0 & \epsilon_y & 0 \\ 0 & 0 & \epsilon_z \end{pmatrix} ; \quad \epsilon_x = \epsilon_y$$

Complex-valued permittivities are allowed. The method works well also for strongly negative epsilons (metals), but care has to be taken in choosing the convergence parameter (**halfnpw**, see below). The layers are separated by zero-thickness, two-dimensional conducting interfaces, whose 2d-conductivity can be specified as a complex number. Notice that setting the conductivity to zero is equivalent to assuming the direct contact between the dielectric materials of adjacent layers.

All the geometrical parameters are input as arguments of the function. See the comments below for the requirements specific to each function.



**Figure 1**



### INPUT VARIABLES

Here follows a commented list of the input variables. This is the same for **RTA\_1d\_tm** and **SM\_1d\_tm**

NAME	DESCRIPTION	TYPE
a	period	real > 0
L	number of layers excluded superstrate and substrate	integer > 0
epssup, epssub	super-and sub-strate permittivities	complex
epsxA	in-plane component of dielectric tensor for material A in the internal layers	1xL complex
epsxB	idem, for material B	1xL complex
epszA, epszB	idem, out-of-plane components	1xL complex
sigma	conductivity of the interfaces	1x(L+1) complex
f	duty cycle in the internal layers	1xL real, each component in [0,1]
d	thicknesses of the layers, including super- and sub-strate	1x (L+2) complex
halfnpw	half number of harmonic waves used in calculation [see below]	integer >= 0
k0	wavevector in vacuum ( $= 2\pi/\lambda_0$ )	real > 0
kpar	x-projection of the incident wavevector	real

The function **field\_1d\_tm** also asks for two more inputs:

NAME	DESCRIPTION	TYPE
nx	number of points along x for field display	integer > 0
nz	number of points along z for field display, specified for each layer	1x (L+2) integer > 0

## OUTPUT VARIABLES & NOTES TO EACH FUNCTION

### RTA\_1d\_tm

NAME	DESCRIPTION	TYPE
RR	Reflectance (total reflected flux/input flux)	real
TT	Transmittance (total transmitted flux/input flux)	real
AA	Layer-by-layer absorbance (power absorbed in the layer/input flux)	1xL real

#### Notes:

- $\epsilon_{\text{ssup}}$  must be real (otherwise the incident waves are ill-defined)  
 $\epsilon_{\text{ssub}}$  can be either real or complex.  
In the first case,  $TT$  has the meaning of transmittance towards the far field.  
In the second case,  $TT$  has the meaning of absorbance in the substrate.
- Above diffraction thresholds,  $RR$  and  $TT$  contain also the contribution of diffracted beams.
- Thickness of superstrate and substrate do not influence the output of **RTA\_1d\_tm**. In this calculation, super- and substrate are at all effects semi-infinite.
- Layer-by-layer absorbance includes also the energy absorbed by some conducting surfaces. Specifically,  $AA(l)$  is the absorbance of internal layer number  $l$  plus the absorbance of the interface that separates layer  $l$  from layer  $l+1$ . (Here,  $l=1$  is the first internal layer).

### SM\_1d\_tm

NAME	DESCRIPTION	TYPE
rl	reflection coefficient from superstrate to superstrate ("left reflectance")	complex
rr	reflection coefficient from substrate to substrate ("right reflectance")	complex
tlr	transmission coefficient from superstrate to substrate ("left to right")	complex
trl	transmission coefficient from substrate to superstrate ("right to left")	complex

#### Notes:

- The coefficients connect the amplitudes of the  $H_y$  fields, calculated at the interface between superstrate and first layer, or substrate and last layer.
- Has been tested extensively only when superstrate and substrate have equal epsilon and thickness
- Why "left" and "right" and not "up" and "down"? ...for historical reasons!



### **field\_1d\_tm**

<b>NAME</b>	<b>DESCRIPTION</b>	<b>TYPE</b>
x	vectors of x points where field is computed	1x (nx) real
z	vectors of z points where field is computed	1x [sum (nz) ] real
Ex, Ez	E field x- and z-components , calculated on the x-y grid	(nx) x [sum (nz) ] complex
Sz	Poynting vector z-component averaged over the unit cell, calculated on the z-grid	1x [sum (nz) ] complex

#### **Notes:**

- `epssup` must be real (otherwise the incident waves are ill-defined)
- E fields are complex. The real, time-dependent fields are  $\text{Re}(E \cdot \exp(-i \omega t))$  [ $\omega = c \cdot k_0$ ]

#### **NOTES COMMON TO ALL FUNCTIONS**

- the lengths (`a`, `d`) and inverse lengths (`k0`, `kpar`) must be set in the same units (for instance microns and inverse microns, or meters and inverse meters)
- the units of `sigma` must be inverse Ohms.

#### **The setting of `halfnpw`**

- As well known, the RCWA has a single convergence parameter which is the truncation order for the plane wave basis. Here, this is ruled by `halfnpw`, which is such that the complete basis is  $(-\text{halfnpw}, \dots, 0, \dots, +\text{halfnpw})$ .  
Always pay attention that the selected value for `halfnpw` guarantees a satisfactory convergence for the problem under analysis.
- `halfnpw = 0` sets the number of harmonic waves to 1, e.g. the scattering matrix reduces to the ordinary 2x2 formalism for unpatterned multilayers



## Contents of the 1d folder:

**epar\_1d** - calculates the vector containing the Fourier amplitudes of the electric field vector in-plane (“parallel”) components

The “1d” functions solve the periodically patterned multilayer problem with 1-d pattern (fig. 2a). Plane waves are incident according to the scheme in fig. 2a. Their wavevector has modulus  $k (=k_0 \cdot \sqrt{\epsilon_{sup}})$ , being  $k_0$  the vacuum wavevector and  $\epsilon_{sup}$  the superstrate permittivity; moreover, the incident wavevector has a projection  $k_{par}$  along on the x-y plane.

The template structure comprises a superstrate, a substrate, and a number of internal layers. Super- and substrate are not patterned, while the internal layers can be. The unit cell geometry consists of a centered stripe of material B surrounded by material A (fig. 1a). Super- and substrate have isotropic permittivity. In the internal layers, material A is isotropic, while material B has an anisotropic permittivity of the form

$$\begin{pmatrix} \epsilon_{xx} & \epsilon_{xy} & 0 \\ \epsilon_{xy} & \epsilon_{yy} & 0 \\ 0 & 0 & \epsilon_z \end{pmatrix}$$

Complex-valued permittivities are allowed. The method works well also for strongly negative epsilons (metals), but care has to be taken in choosing the convergence parameter (**halfnpw**, see below). The layers are separated by zero-thickness, two-dimensional conducting interfaces, whose 2d-conductivity can be specified as a complex number (see also Fig. 1a). Notice that setting the conductivity to zero is equivalent to assuming the direct contact between the dielectric materials of adjacent layers.

All the geometrical parameters are input as arguments of the function. See the comments below for the requirements specific to each function.

## INPUT VARIABLES

Here follows a commented list of the input variables for **epar\_1d**

NAME	DESCRIPTION	TYPE
a	period	real > 0
L	number of layers excluded superstrate and substrate	integer > 0
epssup, epssub	super-and sub-strate permittivities	complex
epsA	permittivity of material A in the internal layers	1xL complex
epsxxB	dielectric tensor xx-component for material B in the internal layers	1xL complex
epsxyB	idem, xy-component	1xL complex
epsyyB	idem, yy-component	1xL complex
epszB	idem, z-component	1xL complex



<code>sigma</code>	conductivity of the interfaces	$1 \times (L+1)$ complex
<code>f</code>	duty cycle in the internal layers	$1 \times L$ real, each component in $[0,1]$
<code>d</code>	thicknesses of the layers, including super- and sub-strate	$1 \times (L+2)$ complex
<code>halfnpw</code>	half number of harmonic waves used in calculation [see below]	integer $\geq 0$
<code>k0</code>	wavevector in vacuum ( $= 2\pi/\lambda_0$ )	real $> 0$
<code>kparx</code>	x-projection of the incident wavevector	real
<code>kpary</code>	y-projection of the incident wavevector	real
<code>pol</code>	polarization state of the incident light	's' or 'p'

## OUTPUT VARIABLES & NOTES TO EACH FUNCTION

### `epar_1d`

NAME	DESCRIPTION	TYPE
<code>epar</code>	Fourier amplitudes of the electric field vector in-plane components	complex, $2 \times (2 \times \text{halfnpw} + 1)$

#### Notes:

- `epssup` must be real (otherwise the incident waves are ill-defined)
- `epssub` can be complex or real. If it is real, and the periodicity is such that diffraction is allowed (i.e. the wavelength is shorter than the diffraction threshold), the meaning of `epar` is the following:

`index`            1,        ...,     $h-1$ ,                     $h$ ,                     $h+1$ ,        ...,     $2 \times h+1$ ,  
`epar(index)`    ...,    ...,     $-E_y(D-1)$ ,    $-E_y(D0)$ ,    $-E_y(D+1)$ ,   ...,        ...,

`index`             $2 \times h+2$ ,    ...,     $2 \times h+1+h-1$ ,    $2 \times h+1+h$ ,    $2 \times h+1+h+1$ ,   ...,     $2 \times h+1+2 \times h+1$ ,  
`epar(index)`        ...,    ...,         $E_x(D-1)$ ,     $E_x(D0)$ ,         $E_x(D+1)$ ,    ...,                    ...,

where  $h$  is a shorthand for `halfnpw`. Here,  $E_x$  or  $E_y$  are the electric field  $x$ - and  $y$ - components of a diffracted wave. Please be careful since  $E_y$  have a minus sign. The diffracted order is identified by ...  $D-1$ ,  $D0$ ,  $D+1$ , ..., according to Fig. 2b.

For further details please refer to [1].

- the lengths ( $a$ ,  $d$ ) and inverse lengths ( $k0$ ,  $kpar$ ) must be set in the same units (for instance microns and inverse microns, or meters and inverse meters)
- the units of `sigma` must be inverse Ohms.

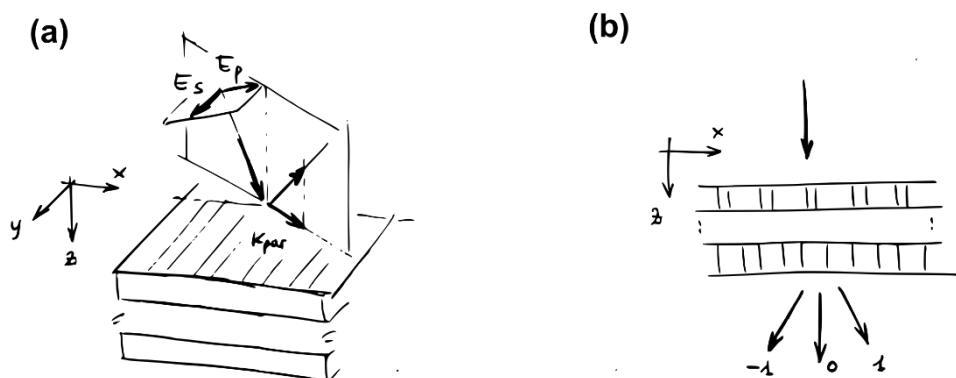


Figure 2



## ***Contents of the 2d\_ folders:***

**ZSM\_2d\_rect** - calculates the zero-order scattering matrix for a layer stack comprising rectangle-shaped inclusions

**ZSM\_2d\_Lshape** - calculates the zero-order scattering matrix for a layer stack comprising L-shaped inclusions

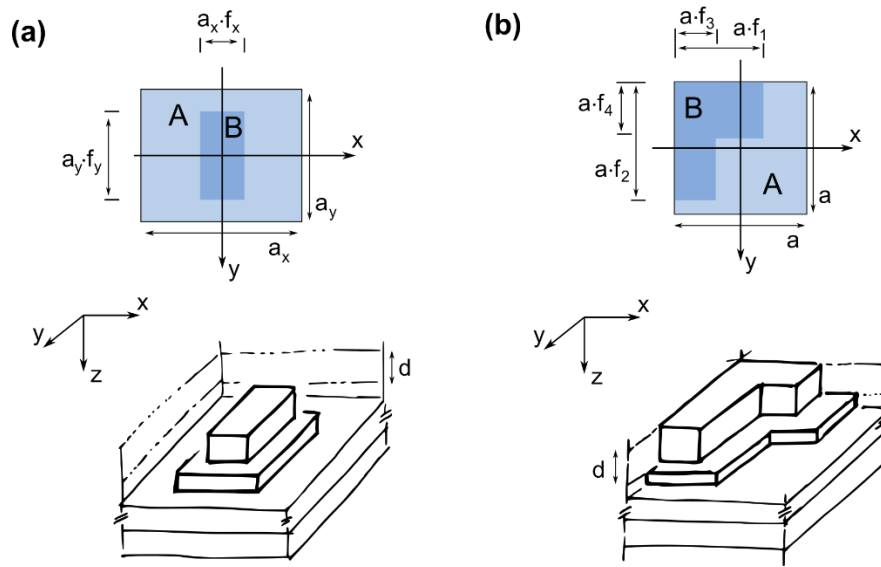
The “2d” functions solve the periodically patterned multilayer problem in the 2-d geometry for two selected geometries (fig. 3 a-b), calculating the scattering matrix for the zero-order diffracted waves. The zero-order scattering matrix **S** is defined as following:

$$\begin{pmatrix} s_{\text{sup}}^- \\ p_{\text{sup}}^- \\ s_{\text{sub}}^- \\ p_{\text{sub}}^- \end{pmatrix} = \mathbf{S} \begin{pmatrix} s_{\text{sup}}^+ \\ p_{\text{sup}}^+ \\ s_{\text{sub}}^+ \\ p_{\text{sub}}^+ \end{pmatrix}$$

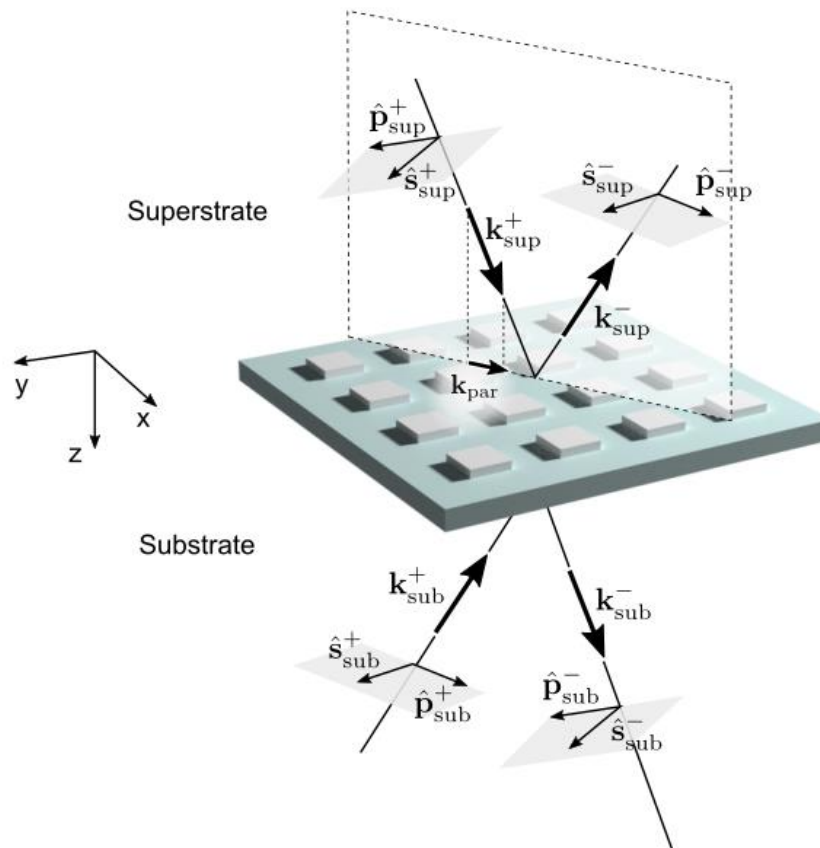
Polarizations are defined according to fig. 4. Incident and reflected wavevectors have modulus  $k_0 \cdot \varepsilon$ , being  $k_0$  the vacuum wavevector and  $\varepsilon$  the permittivity of superstrate or substrate. The wavevector projection is  $\mathbf{k}_{\text{par}} = (k_{\text{par},x}, k_{\text{par},y})$

The unit cell geometry consists of an inclusion of material B within a region of material A. For **ZSM\_2d\_rect** the unit cell is a rectangle; for **ZSM\_2d\_Lshape** the unit cell is a square. All the layers have isotropic permittivity. Complex-valued permittivities are allowed. The method works well also for strongly negative epsilons (metals), but care has to be taken in choosing the convergence parameter (**halfnpw**, see below). This convergence property follows from the implementation of the factorization rules by L. Li (see the webpage for the reference), here implemented in terms of crossed mixed Fourier transforms. The layers are separated by zero-thickness, two-dimensional conducting interfaces, whose 2d-conductivity can be specified as a complex number (see also Fig. 1a). Notice that setting the conductivity to zero is equivalent to assuming the direct contact between the dielectric materials of adjacent layers.

All the geometrical parameters are input as arguments of the function. See the comments below for the requirements specific to each function.



**Figure 3**



**Figure 4**

**WARNING!** The convention for the polarization vectors are different with respect to those for epar\_1d (Fig. 2), and from those of rxx\_functions found in PPML versions older than 2.0.



## INPUT VARIABLES

Here follows a commented list of the input variables which are shared between **ZSM\_2d\_rect** and **ZSM\_2d\_Lshape**.

NAME	DESCRIPTION	TYPE
L	number of layers excluded superstrate and substrate	integer > 0
epssup, epssub	super-and sub-strate permittivities	real complex
epsA	permittivity of material A in the internal layers	1xL complex
epsB	permittivity of material B in the internal layers	1xL complex
sigma	conductivity of the interfaces	1x (L+1) complex
d	thicknesses of the layers, including super- and sub-strate	1x (L+2) real
halfnpw	truncation order [see below]	integer >= 0
k0	wavevector in vacuum ( $= 2\pi/\lambda_0$ )	real > 0
kparx	x-projection of the incident wavevector	real
kpary	y-projection of the incident wavevector	real

Here the input variables specific for **ZSM\_2d\_rect**

NAME	DESCRIPTION	TYPE
ax	x-period	real > 0
ay	y-period	real > 0
fx	x-length of inclusion (relative to ax)	real in [0,1]
fy	y-length of inclusion (relative to ay)	real in [0,1]

Here the input variables specific for **ZSM\_2d\_Lshape**

NAME	DESCRIPTION	TYPE
a	period	real > 0
f1	see figure	real in [f3,1]
f2	see figure	real in [f4,1]
f3	see figure	real in [0,1]
f4	see figure	real in [0,1]

## OUTPUT VARIABLES & NOTES

NAME	DESCRIPTION	TYPE
S	zero-order scattering matrix	4x4 complex

Notes:

- Coefficients are determined assuming that the fields are evaluated at the interface between superstrate and first internal layer. In the case there are no internal layers ( $L = 0$ ), the fields are evaluated at the interface between superstrate and substrate.



## NOTES COMMON TO ALL FUNCTIONS

- the lengths ( $a, a_x, a_y, d$ ) and inverse lengths ( $k_0, k_{parx}, k_{pary}$ ) must be set in the same units (for instance microns and inverse microns, or meters and inverse meters)
  - the units of `sigma` must be inverse Ohms.
  - thickness of superstrate and substrate do not influence the result.
- The electromagnetic problem is solved de facto assuming semi-infinite super- and substrate boundary conditions. You find them in view of further development (field profile calculation).

### The setting of `halfnpw`

- As well known, in two-dimensional RCWA a proper spatial harmonics basis must be chosen. Here we chose a square truncation scheme. This is ruled by `halfnpw`, which is such that the complete basis is built by the direct product of  $(-\text{halfnpw}, \dots, 0, \dots, +\text{halfnpw})$  partial harmonics along x- and y- directions.  
Always pay attention that the selected value for `halfnpw` guarantees a satisfactory convergence for the problem under analysis.
- `halfnpw = 0` sets the number of harmonic waves to 1, e.g. the scattering matrix reduces to the ordinary 4x4 formalism for unpatterned multilayers.

#### Note on the compatibility between PPML 3.0 and older versions:

All the calculations possible in older versions of PPML can be done in PPML 3.0 with a very simple setting. Since a conducting interface with zero conductivity can always be included anywhere without affecting the electromagnetic response, one can adapt the old codes by simply setting `sigma = zeros(L+1)`, where  $L$  is the number of internal layers.

## Bibliography

- [1] D. Whittaker and I. Culshaw, Phys. Rev. B **60**, 2610 (1999).