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Body biasing fault injection: modeling

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Abstract [2023-09-16 12:54:23+02:00](#)

Résumé de la thèse [2023-09-16 12:54:23+02:00](#)

Acknowledgements 2023-09-16 12:54:23+02:00

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Contents

| | |
|--|-------------|
| List of Figures | ix |
| List of Tables | xi |
| List of algorithms JAAJ | xiii |
| List of Acronyms | xv |
| Publications | xvi |
| General introduction | xvii |
| 1 Introduction and state of the art <small>2023-09-16 12:54:13+02:00</small> | 1 |
| 1.1 Summary <small>2023-09-16 12:54:13+02:00</small> | 2 |
| 1.2 Introduction <small>2023-09-16 12:54:13+02:00</small> | 2 |
| 1.3 Side-channel attacks <small>2023-09-16 12:54:13+02:00</small> | 5 |
| 1.3.1 Timing attacks <small>2023-09-16 12:54:13+02:00</small> | 5 |
| 1.3.2 Power analysis and electromagnetic analysis attacks <small>2023-09-16 12:54:13+02:00</small> | 5 |
| 1.4 Fault-injection attacks <small>2023-09-16 12:54:13+02:00</small> | 7 |
| 1.4.1 Giraud's differential fault attack <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5 Fault-injection techniques <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5.1 Glitch fault injection <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5.2 Laser fault injection <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5.3 Electromagnetic fault injection <small>2023-09-16 12:54:13+02:00</small> | 9 |
| 1.5.4 Body biasing injection <small>2023-09-16 12:54:13+02:00</small> | 9 |
| 2 Body Biasing Injection platforms and good practices <small>2023-09-16 12:54:13+02:00</small> | 11 |
| 2.1 Summary <small>NEW 2023-09-16 12:54:13+02:00</small> | 12 |
| 2.2 Introduction <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 12 |
| 2.3 BBI platforms in the state-of-the-art <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 13 |
| 2.3.1 Initial BBI platforms <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 13 |
| 2.3.2 C. O'Flynn BBI platform <small>NO CHANGES 2023-09-16 12:54:13+02:00</small> | 13 |
| 2.3.3 Commercial platforms <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 14 |
| 2.3.4 An overview about BBI platforms <small>NEW 2023-09-16 12:54:13+02:00</small> | 18 |
| 2.4 Our BBI platform <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 19 |
| 2.4.1 The probe <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 19 |

| | | |
|----------|--|-----------|
| 2.4.2 | The generator <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 20 |
| 2.5 | BBI in practice <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 21 |
| 2.5.1 | Typical BBI platform model <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 21 |
| 2.5.2 | Platforms evaluation criteria <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 21 |
| 2.5.3 | Raw results <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 22 |
| 2.5.4 | Analysis conclusions <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 22 |
| 2.6 | Enhanced BBI platform model and simulation <small>2023-09-16 12:54:13+02:00</small> | 24 |
| 2.6.1 | Matching the generator output impedance <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 24 |
| 2.6.2 | Improving the grounding installation <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 25 |
| 2.6.3 | Simulation results <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 25 |
| 2.6.4 | Simulation conclusions <small>NO CHANGES 2023-09-16 12:54:13+02:00</small> | 26 |
| 2.7 | Actual enhanced BBI platform <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 26 |
| 2.7.1 | Generator impedance matching in practice <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 27 |
| 2.7.2 | Grounding installation bypass in practice <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 27 |
| 2.7.3 | Practical analysis <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 27 |
| 2.8 | Enhanced BBI platform in a fault attack context <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 29 |
| 2.8.1 | Giraud's DFA detailed description <small>NO CHANGES 2023-09-16 12:54:13+02:00</small> | 29 |
| 2.8.2 | Integrated circuits target characteristics <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 31 |
| 2.8.3 | Preliminary attack experiments <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 32 |
| 2.8.4 | Attack results and analysis <small>NEW 2023-09-16 12:54:13+02:00</small> | 33 |
| 2.9 | Conclusion <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 34 |
| 3 | Integrated circuits modeling <small>2023-09-16 12:54:13+02:00</small> | 37 |
| 3.1 | Summary <small>2023-09-16 12:54:13+02:00</small> | 38 |
| 3.2 | Introduction <small>2023-09-16 12:54:13+02:00</small> | 38 |
| 3.3 | Electrical models <small>2023-09-16 12:54:13+02:00</small> | 39 |
| 3.3.1 | Standard-cell segment models <small>2023-09-16 12:54:13+02:00</small> | 42 |
| 3.4 | Preliminary model validation <small>2023-09-16 12:54:13+02:00</small> | 45 |
| 3.5 | Voltage pulse generator model and further validation <small>2023-09-16 12:54:13+02:00</small> | 46 |
| 3.5.1 | Early generator models <small>2023-09-16 12:54:13+02:00</small> | 47 |
| 3.5.2 | Further generator models and verification <small>2023-09-16 12:54:13+02:00</small> | 47 |
| 3.6 | Experimental comparisons <small>2023-09-16 12:54:13+02:00</small> | 48 |
| 3.7 | Conclusion <small>2023-09-16 12:54:13+02:00</small> | 48 |
| 4 | Substrate thinning analysis <small>2023-09-16 12:54:13+02:00</small> | 51 |
| 4.1 | Summary <small>2023-09-16 12:54:13+02:00</small> | 52 |
| 4.2 | Introduction <small>2023-09-16 12:54:13+02:00</small> | 52 |
| 4.3 | Geometric and electrical modeling <small>2023-09-16 12:54:13+02:00</small> | 53 |
| 4.3.1 | Geometric modeling <small>2023-09-16 12:54:13+02:00</small> | 53 |
| 4.3.2 | Electrical approach <small>2023-09-16 12:54:13+02:00</small> | 56 |
| 4.4 | Models validation <small>2023-09-16 12:54:13+02:00</small> | 58 |
| 4.4.1 | IC substrate thinning quick look <small>2023-09-16 12:54:13+02:00</small> | 58 |

| | | |
|----------|---|-----------|
| 4.4.2 | Experiments with thinned circuits 2023-09-16 12:54:13+02:00 | 59 |
| 4.5 | Conclusion 2023-09-16 12:54:13+02:00 | 60 |
| 5 | Fault model 2023-09-16 12:54:13+02:00 | 63 |
| 5.1 | Summary 2023-09-16 12:54:13+02:00 | 64 |
| 5.2 | Introduction 2023-09-16 12:54:13+02:00 | 64 |
| 5.3 | Charge extortion 2023-09-16 12:54:13+02:00 | 64 |
| 5.3.1 | Sequential logic operation and simple fault model 2023-09-16 12:54:13+02:00 | 65 |
| 5.4 | Silicon substrate charges propagation 2023-09-16 12:54:13+02:00 | 65 |
| 5.5 | Logic gates simulation under BBI 2023-09-16 12:54:13+02:00 | 65 |
| 6 | Conclusion | 67 |
| | Bibliography | 69 |

List of Figures

| | | |
|------|--|----|
| 2.1 | Schematic extracted from C. O'Flynn [1]: BBI injection device proposed by C. O'Flynn [1], using a transformer to produce high voltage pulses from a low voltage power supply. | 14 |
| 2.2 | BBI probe proposed by the company Langer EMV-Technik GmbH. | 15 |
| 2.3 | BBI probe proposed by the company Riscure BV. | 16 |
| 2.4 | Pulse generator for EMFI and BBI proposed by NewAE Technology Inc. | 17 |
| 2.5 | PicoEMP: a low-cost pulse generator from NewAE Technology Inc. It provides much less instantaneous power than a typical generator, has a long recovery time (from 1 to 4 seconds), has a lower maximum amplitude (250 V), is not pre-calibrated, and has no controllable pulse width. However, it costs 94 % less than a typical generator, giving it a considerable advantage when building low-cost BBI platforms. | 17 |
| 2.6 | Custom BBI probes photographs | 19 |
| 2.7 | Front side of the Avtech Electrosystems Ltd. AVRK-4-B High Voltage Pulser, used during all my thesis experiments. | 20 |
| 2.8 | BBI platform electrical model developed for my thesis to quickly evaluate various platform's parameters, alongside the model simulation results. | 21 |
| 2.9 | Platform simulation results with different IC load values. | 23 |
| 2.10 | BBI platform enhanced electrical model developed for my thesis to quickly evaluate various platform parameters, alongside the model simulation results. | 24 |
| 2.11 | Simulation results of the enhanced platform with a 250Ω IC load (2.11a) and a $2 k\Omega$ IC load (2.11b). The current increase in 2.11a is natural due to the load impedance reduction. However, the effective pulse amplitude relative to the set point has only a -7 % error, which is a drastic improvement over the previous -30 %. The set point is met. Then, in 2.11b, the current decrease is logical given the higher impedance value. The effective pulse amplitude relative to the set point has only a 7 % error, which is a drastic improvement over the previous 40 %. The ringing almost disappeared in every case. It is because the generator is not only loaded by the IC, but by the equivalent load composed of the IC and the compensation load, which reduces the effective load variation when changing the IC load value. | 26 |

| | |
|---|----|
| 2.12 BBI platforms comparison: state-of-the-art (S1P and S1G) versus the proposed enhanced platform (S2P and S2G). The ideal voltage pulse is -140 V ample and 20 ns wide, with rise and fall times of 4 ns. S1P shows a -108 % negative percentage overshoot. PW is 275 % too high with a 75 ns value. The fall time is 4 times higher than requested, and the rise time is more than 15 times higher. S1G highlights the ringing, seen on S1P on a lesser extent. On S2P, the voltage set point negative PO measures -31 %. PW now perfectly matches the set point of 20 ns. Rise and fall times are 4 times higher than they should be, despite both being consistent. S2G shows significant ringing reduction, while maintaining the same amount of transferred energy into the IC. | 28 |
| 2.13 The two last rounds of an AES-128 | 30 |
| 2.14 Fault analysis mapping | 32 |
| 3.1 Dual-well and triple-well inverter silicon sectional view | 39 |
| 3.2 Surface subdivision improvement. | 40 |
| 3.3 Three-dimensional Dual-Well and Triple-Well IC comprehensive standard-cell electrical schematic. | 41 |
| 3.4 Elementary substrate 3D netlist | 43 |
| 3.5 Elementary substrate SPICE netlist | 44 |
| 3.6 SCS substrate layer SPICE netlist | 44 |
| 3.7 Three-dimensional standard-cell segments interconnection example. | 45 |
| 3.8 Mixed substrates operating point. | 46 |
| 3.9 Dual-well and triple-well cross-sectional current distribution view at the apex of the voltage pulse | 48 |
| 4.1 BBI susceptibility area cross-sectional 2D view | 54 |
| 4.2 Simulated non-thinned IC (140 μm) substrate voltage distribution: peak of the first voltage pulse edge | 56 |
| 4.3 Simulated thinned IC (60 μm) substrate voltage distribution: peak of the first voltage pulse edge | 57 |
| 4.4 Fault susceptibility maps | 59 |
| 4.5 Susceptibility area spreading | 59 |
| 4.6 Fault susceptibility maps couples | 59 |
| 5.1 Sequential logic operation and BBI sampling fault susceptibility | 65 |

List of Tables

| | | |
|-----|---|----|
| 2.1 | FAM faults description | 32 |
| 2.2 | Giraud's DFA results. In yellow are indicated the bytes retrieved with a brute-force method instead of the Giraud's bit fault attack. | 34 |
| 3.1 | Dual-well, triple-well and mixed substrates SCS operating point. | 46 |

List of Algorithms

| | | |
|---|--|----|
| 1 | Integrated circuit SPICE netlist generation algorithm. | 50 |
|---|--|----|

List of Acronyms

| | |
|--------------|------------------------------------|
| AES | Advanced Encryption Standard |
| BBI | Body Biasing Injection |
| BSIM | Berkeley Short-channel IGFET Model |
| CPS | Cyber-Physical System |
| DES | Data Encryption Standard |
| DoM | Difference of Means |
| DFA | Differential Fault Analysis |
| DPA | Differential Power Analysis |
| ECC | Elliptic-Curve Cryptography |
| EMFI | Electro-Magnetic Fault Injection |
| FAM | Fault Analysis Mapping |
| FIB | Focused Ion Beam |
| FSA | Fault Sensibility Analysis |
| FSM | Fault Susceptibility Map |
| GFI | Glitch Fault Injection |
| HFI | Hardware Fault Injection |
| IoT | Internet of Things |
| LFI | Laser Fault Injection |
| PCC | Pearson Correlation Coefficient |
| PLL | Phase Locked Loop |
| RAM | Random Access Memory |
| RSA | Rivest Shamir Adleman |
| SCA | Side Channel Attack |
| | |
| SCS | Standard Cell Segment |
| SMA | SubMiniature version A |
| SPA | Simple Power Analysis |
| WLCSP | Wafer-Level Chip-Scale Packaging |

Publications

2023-09-16 12:54:23+02:00

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General introduction

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Over the past years, various fault injection methods, representing a significant threat for secure integrated circuits, have been extensively studied, like laser fault injection (LFI), or more recently electromagnetic fault injection (EMFI). The purpose of these studies is to propose efficient countermeasures to the right cost. They have had multiple objectives, such as understanding the various phenomena at the origin of fault creation, or being able to simulate fault propagation over multiple abstraction levels...

Voltage pulse substrate fault injection, commonly called Body Biasing Injection (BBI), while being contemporary to EMFI, led to very few researches and studies in comparison. Up to the best of our knowledge, three scientific papers existed at the beginning of my thesis, back in 2020.

The LIRMM (Laboratoire d’Informatique, de Robotique et de Microélectronique de Montpellier: Computer Sciences, Robotics and Microelectronics Laboratory of Montpellier), inventor of this technique in 2011, proposed this thesis to answer various questions such as:

- What are the phenomena at work leading to fault injection?
- What kind of spatial resolution does BBI offer?
- What is the time resolution of this method?
- Is it relevant to thin the silicon substrate of BBI target ICs?
- Can constraining fault attacks be performed with this method?

These questions have guided my thesis work through the last three years. These works have led me to propose CMOS integrated circuits simulation models in a BBI context, in addition to proposing improvements for the practice of BBI. My thesis manuscript is structured in five chapters. Each one of them attempt to provide answers to the preceding interrogations.

The **first chapter** of this manuscript provides an overview of the existing fault injection techniques, with a particular emphasis on BBI.

The **second chapter** describes improvements for the practice of BBI. These improvements have been conceived and obtained through my studies concerning BBI resolution and accuracy, both in time and space. Additionally, this **chapter** describes the practical results of a differential fault attack performed thanks to BBI and requiring single-bit faults.

The **third chapter** is dedicated to CMOS integrated circuits modeling under BBI. It introduces the established simulation models, in addition the designed algorithms allowing to simulate circuits subjected to BBI. The models and methods introduced allow us to simulate circuit behavior in reasonable duration, which allows us to perform parametric analysis of BBI effects.

The **fourth chapter** discusses a common practice in fault injection methods: the thinning of integrated circuits' substrate. While this topic has been extensively addressed concerning LFI, it is not the case for BBI. It relates to studying IC behavioral differences and BBI efficiency on different substrate thicknesses circuits. Various models are introduced to get different approaches, allowing to predict differently electrical and physical phenomena at work. Mathematical models are also derived from the previous models, enabling the calculation of optimal experimental parameters, in addition to predicting circuit behavior.

The **fifth** is dedicated to the understanding of fault creation in circuits subjected to BBI. It allows deriving a fault model from the simulations.

Eventually, the **last chapter** presents a general conclusion of my thesis work. In addition to this, outlooks are provided. The latter are interrogations remaining unanswered by my thesis works, mostly concerning more specific BBI effects on integrated circuits.

I

Introduction and state of the art 2023-09-16

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chap:1_stateOfTheArt

Contents

| | | |
|-------|--|---|
| 1.1 | Summary <small>2023-09-16 12:54:13+02:00</small> | 2 |
| 1.2 | Introduction <small>2023-09-16 12:54:13+02:00</small> | 2 |
| 1.3 | Side-channel attacks <small>2023-09-16 12:54:13+02:00</small> | 5 |
| 1.3.1 | Timing attacks <small>2023-09-16 12:54:13+02:00</small> | 5 |
| 1.3.2 | Power analysis and electromagnetic analysis attacks <small>2023-09-16 12:54:13+02:00</small> | 5 |
| 1.4 | Fault-injection attacks <small>2023-09-16 12:54:13+02:00</small> | 7 |
| 1.4.1 | Giraud's differential fault attack <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5 | Fault-injection techniques <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5.1 | Glitch fault injection <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5.2 | Laser fault injection <small>2023-09-16 12:54:13+02:00</small> | 8 |
| 1.5.3 | Electromagnetic fault injection <small>2023-09-16 12:54:13+02:00</small> | 9 |
| 1.5.4 | Body biasing injection <small>2023-09-16 12:54:13+02:00</small> | 9 |

1.1 Summary 2023-09-16 12:54:23+02:00

chap:1; sect:summary

This chapter reviews the state-of-the-art concerning fault injection methods. It first defines the interest of studying fault injection and its context. Then, various fault injection techniques are presented and their differences, advantages and disadvantages are analyzed. Specifically, platforms equipment across all methods is described alongside the different techniques employed to perform such fault injection. Eventually, body biasing injection is introduced, and we will study its interests in a fault injection context.

1.2 Introduction 2023-09-16 12:54:23+02:00

chap:1; sect:intro

In our time, almost every business sector and every part of our surroundings, directly or indirectly, use integrated electronics circuits. It ranges from smart-cards to supercomputers, through military devices, cell-phones, Cyber-Physical Systems (CPS) and Internet-of-Things (IoT) objects to name but a few.

Traditionally, integrated circuits design mainly focused on performance upgrades over the generations. Performance was measured thanks to two factors: computation speed and silicon surface. Within this context, power consumption was not a design constraint, therefore, integrated circuits became more and more energy-consuming. However, with the advent of portable devices, power consumption became a predominant design factor over speed, and space and got included into the former design flows. Nevertheless, less space and more speed does not physically equate with less energy. Alongside, new systems have emerged and have massively grown these past decades: IoT and CPS. On one hand, CPS are often systems where hardware and software are interlaced and thought together, and can be drastically different from one application to another. On the other hand, IoT systems have often less coordination between hardware and software, but are commonly more flexible. Whatsoever, both of these systems have something strong in common: their security is fundamental. Therefore, in this context, as it has been proposed in [3], and because security had been adopted as a counter-measure after the design flow, it has to enter as a fourth design rule when creating integrated circuits. This is required because a secure system has to ensure that every data going in and out of it are subject to the following criteria:

- Authenticity: data received have to come from the sender
- Integrity: data cannot be altered in any way
- Confidentiality: data cannot be accessed (read or written) by third-parties

Therefore, it is imperative to study and comprehend the strategies for enhancing IC security in order to develop future integrated circuits that are designed with security in mind from the

initial stages of development to its completion.

Currently, electronic devices implement security in two distinct ways, namely from a software or hardware standpoint. To accomplish this objective, encryption algorithms have been integrated. It is possible to distinguish two distinct categories of encryption algorithms, namely symmetric and asymmetric algorithms.

In short, symmetric cryptographic techniques use a unique key for encrypting and decrypting messages. The most popular algorithms are the AES (Advanced Encryption Standard), DES (Data Encryption Standard), IDEA (International Data Encryption Algorithm), RC5 (Rivest Cipher 5), and TDES (Triple DES) not to cite them all. The key must be kept confidential and only shared among parties in order to maintain a confidential connection between them. The requirement for a single key is the main drawback of symmetric encryption methods. As a result, every possible step must be taken to safeguard key secrecy, such as avoiding key exchanges on public networks. However, symmetric encryption has a clear advantage over asymmetric encryption. As a result of utilizing a single key, symmetric algorithms are typically simpler than asymmetric algorithms, resulting in a reduction in computing power required for encryption. It is therefore possible to encrypt a large amount of data in a short amount of time.

In contrast, when it comes to symmetric cryptographic techniques, commonly referred to as public key cryptography techniques, a pair of keys is employed. The keys are usually referred to as public-key and private-key. The public key is used to encrypt a message, and anyone can use it. The private-key is, however, kept confidential to ensure that only authorized parties can decrypt a message that has been encrypted with the public-key. The primary motivation behind having two keys is that it is impracticable to reconstruct the public-key from the private-key. The most commonly employed asymmetric algorithms include the RSA (Rivest–Shamir–Adleman) algorithm, the ElGamal encryption system, the ECC (Elliptic-curve cryptography), and the Cramer-Shoup system, to name a few. The main drawback of symmetrical algorithms is that they involve large mathematical calculations, which implies a higher time complexity. Hence, these techniques are capable of encrypting a limited quantity of data. Therefore, to achieve this objective, in the majority of systems, a hybrid approach is employed to employ both encryption methods, thereby ensuring optimal security and a brief calculation time.

On the one hand, if all the previously mentioned algorithms are mathematically reliable, their reliability will decrease when they are implemented on actual integrated circuits. Indeed, every integrated circuit uses electrical energy to function. Therefore, when an electric current appears in a conductor, there is inevitably an electromagnetic field associated with this current. Moreover, every measurable physical quantity concerning the IC could be a point of information leakage. This is particularly true when considering the fact that these quantities will exhibit varying variations based on the calculations performed by the IC. When evaluating these quantities, it is possible to retrieve confidential information. We described what is called a "**side-channel attack**" (SCA) when considering cybersecurity.

On the other hand, physical quantity measurement is not the only flaw in actual algorithm implementations. In fact, every physical IC has specifications under which it can execute its functions properly. It includes temperature, clock frequency, power supply voltage, and the electromagnetic environment. When pushed beyond its specifications, any integrated circuit will exhibit unpredictable behavior. However, it is still possible to control an IC's behavior outside its specifications with a certain degree of success. By doing so, it allows running the IC calculation incorrectly by finely controlling how much time and by which amount the IC is outside its specifications, thus enabling, with specific mathematical algorithms, to retrieve hidden data manipulated by the IC. This process is commonly referred to as a "**fault injection attack**".

We have identified two potential attacks on robust algorithms that have been implemented into actual integrated circuits. However, it is customary to categorize cyberattacks into three distinct categories based on their execution methods.

Despite being technically advanced, noninvasive attacks are the most materially trivial. SCA are included in this set, which do not require any hardware modification to the targeted ICs, even if there is no physical contact. It is a delicate task to detect them; hence, they are deemed to be highly dangerous and are commonly considered in the initial stages of designing integrated circuits.

It is then possible to distinguish semi-invasive attacks. Systematically, they are accompanied by device physical preparation, which is entirely devoid of noninvasive attacks, but they are not accompanied by device physical modification. ICs integrity is therefore theoretically preserved. A typical IC modification involves the removal of the chip package. It enables access to either the front or back side of the integrated circuit, thereby facilitating micro-probing, laser injection, or substrate pulse injection. Furthermore, substrate thinning is also commonly considered and used, as it facilitates the fine-tuning of certain fault injection techniques, such as laser fault injection (LFI). These attacks necessitate specialized hardware, tools, and expertise and are frequently challenging to establish and execute.

Eventually, there are invasive attacks. They imply further physical modifications to integrated circuits. For instance, it is common to eliminate the layers of a chip, thereby enabling the photographing of the various layers and the reverse engineering of the target. A focused ion beam (FIB) can also be used to change the IC target internally by making electric connections that did not exist before. Contrary to semi-invasive attacks, invasive attacks frequently involve the definitive destruction of the target, primarily due to the absence of physical integrity during the process.

This doctoral thesis is dedicated to the study of a specific fault injection method: Body Biasing Injection (BBI). In this particular context, we will examine in this chapter the current state of the art in relation to side-channel attacks and fault injection techniques as outlined in the literature. This allows us to explain the interests of the current work regarding hardware

security.

In the first place, we will briefly discuss side-channel attacks. We will then examine the various fault injection platforms commonly described. Eventually, we will ponder the interests of BBI in this context.

1.3 Side-channel attacks 2023-09-16 12:54:23+02:00

chap:1;sect:sca

1.3.1 Timing attacks 2023-09-16 12:54:23+02:00

chap:1;sect:sca;subsect:timingAttacks

The most fundamental side-channel attack was initially introduced in 1996 [4]. This attack involves determining the duration required to execute cryptographic computations. By executing this method, the adversaries were able to obtain a variety of algorithmic keys, specifically for the RSA algorithm. The computation cost of this attack is low, thereby enabling it to execute swift attacks. Indeed, as per the RSA algorithm, as outlined in [5], the encryption of a message necessitates the calculation of the following relationship:

$$C \equiv E(M) \equiv M^e \pmod{n} \quad \text{eqn:rsa (1.1)}$$

M denotes the message to be encrypted, while C is the ciphertext and (e, n) the encryption key pair. The objective of the attack outlined in [4] is to retrieve e. To achieve this objective, the integrated circuit must perform multiple computations of the equation 1.1 for varying values of M, while maintaining identical values of e. Subsequently, the attacker must evaluate the duration of each computation. If the value of e differs for each operation, the attack cannot be executed. After the demonstration of this attack, countermeasures were implemented, including the implementation of constant-time cryptographic algorithms allowing the elimination of leaks through the utilization of timing analysis. More recently, other, more advanced countermeasures have also been proposed [6].

1.3.2 Power analysis and electromagnetic analysis attacks 2023-09-16 12:54:23+02:00

chap:1;sect:sca;subsect:powerAttack

Subsequently, more elaborated side-channel attacks were explained in 1999, as documented in [7]. This paper presents the concepts of simple power analysis (SPA) and differential power analysis (DPA).

On the one hand, SPA entails the measurement and direct interpretation of power consumption traces of a cryptographic integrated circuit. For instance, it enables the counting of DES or AES rounds to gain insights into the utilized implementation. Furthermore, it allows for the observation of power consumption variations depending on the executed instruction. A proposal has been made to prevent the utilization of secret keys or information during conditional

branching logic, with the objective of preventing simple power analysis.

On the other hand, DPA is a more elaborate approach that aims to identify the effects and variations associated with data processed by ICs. The aforementioned variations are more subtle and frequently obscured by noise. Therefore, DPA proposes to use statistics tools to reveal hidden system information, specifically by computing the difference of means (DoM) between traces. Therefore, preventing DPA is more complicated than preventing SPA. One of the simplest methods is to add electrical noise. Another technique is to reduce measurable signal amplitude. It is done first by optimizing code execution, by finely choosing which operation is performed to reduce electromagnetic leakage. Second, it is also possible to shield the device, but it increases the IC's cost significantly.

In addition to these attacks, there is also another attack which is commonly studied: correlation power analysis (CPA) [8]. As well as DPA, CPA uses statistical tools. However, as opposite to computing the difference of means, it involves calculating the Pearson correlation coefficient (PCC), allowing to measure the linear correlation between different power consumption traces.

It is important to note that SPA, DPA and CPA are historically performed using traces directly measured from the ICs power consumption. However, these attacks can also be performed thanks to IC electromagnetic radiation analysis [9]. Because electric charges are circulating into the IC, they inevitably generate electromagnetic waves. Therefore, it is possible to pick up these waves, and similar to power consumption, their shape depends on the data being processed. There has been numerous active research concerning this method for twenty years. It can be explained thanks to its advantages compared to bare power consumption analysis. Indeed, when measuring the entire power consumption of an IC, it is not possible to target a specific area. It leads, especially with complex ICs and countermeasures, to an impossibility to perform such attacks. On the contrary, electromagnetic analysis attacks have multiple advantages over power consumption analysis attacks:

- No sample preparation required
- No physical contact with the target
- It requires only little equipment: probe and voltage amplifier

As we stated previously, power consumption analysis attacks target an entire IC, whereas electromagnetic analysis attacks allow having fine resolutions. Indeed, small probes with a size down to 50 µm have been proposed [10]. Such small probes allow focusing the measurement on the cryptographic area of the IC, while excluding from the measurement, with a certain amount, any undesirable electromagnetic emission which could potentially harm the attack efficiency. In addition to that, electromagnetic probes, depending on their design, can have very high cutoff frequency. Therefore, it allows analyzing ICs running at high frequencies, enabling attacks on recent devices such as smartphones [11].

1.4 Fault-injection attacks 2023-09-16 12:54:23+02:00

chap:1;sect:fattack

Fault injections are widely described in the literature and can be utilized for a variety of purposes. For instance, during integrated circuits testing, it is common to find fault injection susceptibility tests, allowing for engineers to test fault detection circuits, recovery capabilities and reconfiguration possibilities of ICs. In this work, we are going to take a closer look at hardware fault injections (HFI) techniques solely, which fall in two distinct categories, similar to side-channel attacks:

- HFI with physical contact
- Contactless HFI

For each kind of HFI, multiple outcomes are aimed. On the one hand, the HFI can produce, in the targeted IC, branching errors leading secret codes to be revealed or protected rights to be acquired by an attacker. On the other hand, HFI can produce incorrect behaviors, allowing to retrieve hidden and protected data thanks to mathematical tools. In that case, HFI targets are mostly cryptographic algorithms, and can be segmented in non-comprehensive set of categories.

One of the most performed HFI is called differential fault attack/analysis (DFA). The principle of DFA lies in inducing computation errors during the decryption process of cryptographic algorithm thanks to fault injection. Several DFA were proposed on different algorithms [12, 13, 14, 15, 16]. Every DFA implies that the attacker has access to at least two ciphertexts, a correct one, denoted C , and a faulty one, denoted C_F . In addition to that, the attacker must also know the characteristics of the induced faults, such as the amount of faulted bits, in which operation they are faulted, etc. Eventually, it is needed to be able to induce the expected faults depending on the fault model required for the DFA.

Another common HFI is the fault sensitivity analysis (FSA) [17]. As every HFI, it is still required to have physical access to the device. FSA usefulness comes from the fact that alongside fault characteristics, other information can be used by attackers, in that case: the IC sensitivity to faults. As defined in [17], fault sensitivity is a condition where the faulty output begins to show specific characteristics. Specifically, this work defines a critical condition, similar to the PLL capture ranges (lock-in, hold-in, pull-in, etc.), where the IC starts to exhibit a faulty behavior or when it stops this behavior. Then, to perform an attack with this information, the attacker has to know the relationship between the fault sensitivity and the computed data, without knowing the insights of the cryptographic algorithm at work. It states that the algorithm will inevitably exhibit data-dependency of fault sensitivity. Hence, it allows using the IC as an almost black box.

In the next paragraph, we are going to analyze deeper a specific fault attack and its impli-

cations

1.4.1 Giraud's differential fault attack 2023-09-16 12:54:23+02:00

chap:1; sect:fattack; subsect:giraud

1.5 Fault-injection techniques 2023-09-16 12:54:23+02:00

chap:1; sect:fInjTech

1.5.1 Glitch fault injection 2023-09-16 12:54:23+02:00

chap:1; sect:fInjTech; subsect:glitch

Glitch fault injection (GFI) are one of the first historical documented fault injection attacks. They are simple and require little equipment. For the most part, they are non-invasive, which means that they are reversible, physically speaking. Various physical quantities can be disturbed, but the power supply voltages (VDD or GND), and the IC clock are the most common. Each physical quantity can be modified at the attacker's discretion, with a certain amount. However, the disturbances have to be short enough to avoid IC shutdown concerning power supply glitches, but also not powerful enough to avoid the IC destruction. On the one hand, the main advantage of such attack is its easiness to set up compared to other methods. On the other hand, their main disadvantage is the complete lack of locality with the injection effects. Indeed, disturbing IC's macro-parameters interfere with the entire chip and does not guarantee a useful faulty behavior. In addition to that, every modern IC is prepared to detect such attacks and thus protect itself by resetting its electronics.

1.5.2 Laser fault injection 2023-09-16 12:54:23+02:00

chap:1; sect:fInjTech; subsect:lfi

Laser fault injection (LFI), sometimes called optical fault injection, has been introduced in 2002 [18] and is a more complex technique than GFI. However, its precision is immensely better, at the cost of being semi-invasive, and sometimes invasive. LFI consists in targeting specific regions of the IC with laser beams of specific wavelengths. Several other parameters are involved for this method to succeed, such as the light emission duration, the area/volume of the targeted region, the IC substrate thickness, etc. Although LFI requires chip preparation, it is often minimal. LFI works thanks to the fact that every silicon semiconductor device (diode, transistor...) is intrinsically sensitive to light, typically with wavelengths ranging from 400 nm to 1000 nm. Therefore, if the light conveys enough energy, it is possible to change the state of some transistors, thus affecting logical values. The main shortcoming of LFI is the platform price. [Add more details.](#)

1.5.3 Electromagnetic fault injection 2023-09-16 12:54:23+02:00

chap:1; sect:fInjTech; subsect:emfi

Electromagnetic fault injection (EMFI) is a more recent and more studied technique, introduced in 2002 [19]. Its principle is basic: an electric current in a wire (probe) near an IC creates a corresponding electric current in the IC power delivery network, similar to an electric transformer. Similar to GFI, the attack can be non-invasive, although this method yields better results while being semi-invasive. Indeed, the closer the probe to the IC, the better the coupling and the mutual inductance, which often required to remove the IC's plastic package. This injection technique efficiency greatly varies depending on the probe's characteristics, the IC transistors size, the targeted location, the field duration, etc. Over the time, electromagnetic probes were constantly improved, and it is common to find probes with a ferrite core, allowing for better injection locality. In 2020, a modeling workflow was proposed [20], allowing to explain how EM probe can couple to IC power delivery networks. [Add more details.](#)

1.5.4 Body biasing injection 2023-09-16 12:54:23+02:00

chap:1; sect:fInjTech; subsect:bbi

Eventually, there is another fault injection method, less studied and more recent than the others, commonly called Body Biasing Injection (BBI), which is the research topic of this thesis. This technique has been introduced in 2012 [21], and further studied in 2013 [22] and 2016 [23]. At the beginning of this thesis, a fourth article was published [1], studying the interests of BBI concerning Wafer-Level Chip-Scale Packaging (WLCSP). The principle behind BBI is fairly simple: applying voltage pulses directly onto the backside of IC targets, thanks to a metallic probe. On the one hand, despite this simple premise, in the vast majority of cases, BBI is a semi-invasive method. Indeed, as most IC are encapsulated in a ceramic or plastic package, it is required, to access to the substrate, to partially remove a piece of the package. On the other hand, building a BBI platform is not expensive and technically easier when compared to LFI or EMFI. Indeed, a metallic probe with a custom armature costs around 10 euros at worst, and is easy to build at hand, while manufacturing a precise EMFI probe requires more knowledge to achieve good results. Considering that EMFI and BBI both require similar voltage pulse generator, which is often the most expensive piece of equipment, the overall platform cost is lower concerning BBI.

II

Body Biasing Injection platforms and good practices 2023-09-16 12:54:23+02:00

Contents

| | | |
|-------|--|----|
| 2.1 | Summary <small>NEW 2023-09-16 12:54:13+02:00</small> | 12 |
| 2.2 | Introduction <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 12 |
| 2.3 | BBI platforms in the state-of-the-art <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 13 |
| 2.3.1 | Initial BBI platforms <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 13 |
| 2.3.2 | C. O'Flynn BBI platform <small>NO CHANGES 2023-09-16 12:54:13+02:00</small> | 13 |
| 2.3.3 | Commercial platforms <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 14 |
| 2.3.4 | An overview about BBI platforms <small>NEW 2023-09-16 12:54:13+02:00</small> | 18 |
| 2.4 | Our BBI platform <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 19 |
| 2.4.1 | The probe <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 19 |
| 2.4.2 | The generator <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 20 |
| 2.5 | BBI in practice <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 21 |
| 2.5.1 | Typical BBI platform model <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 21 |
| 2.5.2 | Platforms evaluation criteria <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 21 |
| 2.5.3 | Raw results <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 22 |
| 2.5.4 | Analysis conclusions <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 22 |
| 2.6 | Enhanced BBI platform model and simulation <small>2023-09-16 12:54:13+02:00</small> | 24 |
| 2.6.1 | Matching the generator output impedance <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 24 |
| 2.6.2 | Improving the grounding installation <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 25 |
| 2.6.3 | Simulation results <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 25 |
| 2.6.4 | Simulation conclusions <small>NO CHANGES 2023-09-16 12:54:13+02:00</small> | 26 |
| 2.7 | Actual enhanced BBI platform <small>PARTIALLY UPDATED 2023-09-16 12:54:13+02:00</small> | 26 |
| 2.7.1 | Generator impedance matching in practice <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 27 |
| 2.7.2 | Grounding installation bypass in practice <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 27 |
| 2.7.3 | Practical analysis <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 27 |
| 2.8 | Enhanced BBI platform in a fault attack context <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 29 |
| 2.8.1 | Giraud's DFA detailed description <small>NO CHANGES 2023-09-16 12:54:13+02:00</small> | 29 |
| 2.8.2 | Integrated circuits target characteristics <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 31 |
| 2.8.3 | Preliminary attack experiments <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 32 |
| 2.8.4 | Attack results and analysis <small>NEW 2023-09-16 12:54:13+02:00</small> | 33 |
| 2.9 | Conclusion <small>UPDATED 2023-09-16 12:54:13+02:00</small> | 34 |

2.1 Summary NEW 2023-09-16 12:54:23+02:00

This chapter first presents the various existing BBI platforms in the state-of-the-art, in addition to introducing our BBI platform. Then, I introduce improvements over the default platform used, allowing for better reproducibility and control over BBI parameters when compared to state-of-the-art platforms. At the beginning of this work, I was working using a state-of-the-art like platform, which led me to elaborating the enhancements as experiments were not reproducible due to great variations in every platform's parameter. Thanks to these improvements, I was able to draw better experimental results and to compare them to state-of-the-art platforms to verify the soundness of such platform modifications. These results are presented in the last part of this chapter thanks to elementary electrical experiments, followed by a differential fault attack, that I managed to perform thanks to the enhancements on a hardware AES coprocessor. Parts of this work were published in FDTC 2022 [24] and FDTC 2023. ([Add reference, quand on l'aura.](#))

2.2 Introduction UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:summaryIntro

In the first place, we are going to introduce Body Biasing Injection platforms:

- What exists in the state-of-the-art
- What I am using for my experiments

Afterward, I present a general BBI platform with its electrical model, in addition to evaluating the platform characteristics. Thanks to the model, I can perform electric simulations, allowing me to study and highlight its inherent flaws, such as:

- Poor control over the characteristics of the platform
- Obvious ringing leading to poor temporal accuracy
- Platform dependent parameters such as the ground installation quality
- Main physical quantities, such as the voltage and the pulse width, set points not met

Thereafter, I propose enhancements to overcome the previous platform shortcomings, which are:

- Matching the output impedance of the generator to reduce the ringing and bring the measurements closer to the specifications and the set points
- Bypassing the grounding installation to minimize platform dependency

After that, I present a deeper analysis of these enhancements, including ringing, set points accuracy, and load and transmission line dependency. Then, I discuss various techniques allowing to match the generator output impedance, in addition to introducing practical grounding installation bypass. Next, I perform actual experiments with our BBI platform, including measurements of such platform, illustrating the enhancements in practice. Eventually, I introduce a constraining differential fault attack set-up with our platform. It includes the attack description, followed by a thorough description of the IC target, sustained with experiments allowing me to perform the attack with more ease, with a comparison of a state-of-the-art platform with our enhanced platform, ended up by the attack results.

2.3 BBI platforms in the state-of-the-art PARTIALLY UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiPlatforms

2.3.1 Initial BBI platforms UPDATED 2023-09-16 12:54:23+02:00

First introduced in 2012 by P. Maurine et al. [21], further studied in 2013 by K. Tobich et al. [22], the proposed BBI platform in both papers is fairly simple, similar to EMFI platforms, composed of:

- A decapped IC, with its backside accessible;
- An independent voltage pulse generator able to generate positive and negative voltage pulses up to 100 V, with a maximum current of 2 A. The generator is DC-coupled with the load;
- A passive custom-made probe, consisting of an SMA connector and a standard needle soldered to it;
- A positioning system to place the probe precisely onto the IC backside;
- An acquisition system, measuring various voltages.

It is important to remark that the probe is connected through a relatively long interconnection, acting as a transmission line.

2.3.2 C. O'Flynn BBI platform NO CHANGES 2023-09-16 12:54:23+02:00

The original platform had stayed identical in the literature [23], until C. O'Flynn published in 2020 [1] practical examples of BBI attacks on WLCSP integrated circuits. In this work, the platform is structured differently. There are common elements, such as:

- An IC target with an accessible backside, in that case thanks to the WLCSP;
- A positioning system;

- Various acquisition tools.

The structural differences concern the voltage pulse generation. Instead of an independent voltage pulse generator, connected to a passive probe through a transmission line, the proposed solution consists in implementing an active probe with a separate pulse trigger generator.

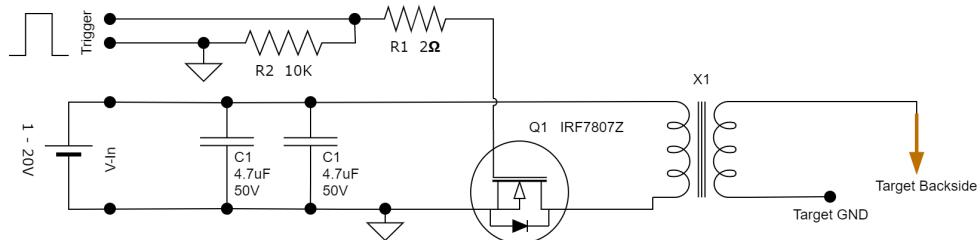


Figure 2.1: Schematic extracted from C. O'Flynn [1]: BBI injection device proposed by C. O'Flynn [1], using a transformer to produce high voltage pulses from a low voltage power supply. Fig: colinBBIsonde

Fig. 2.1 shows the design extracted from C. O'Flynn work [1]. The transformer allows creating high voltage pulses from a low voltage power supply. The transformer is controlled through the transistor Q1. Because the output is the secondary of a transformer, it is AC-coupled to the load, thus, no DC current can be transferred to the load. The transformer is custom-made and allows for ten times voltage multiplication, therefore enabling 300 V pulses with a 30 V power supply unit (PSU), which is fairly common for a lab PSU. The transistor is controlled thanks to an external trigger pulse, generated by another piece of equipment on this platform. It is on this point that O'Flynn's platform greatly differs from Maurine's initial platform.

The pulse generator used in this paper is a ChipWhisperer-Lite, an open-source tool created by NewAE Technology Inc. This tool can perform various tasks, such as pulse generation (as it is currently done), analog signals capture, or clock generation, enabling clock glitch fault injection. In addition to that, it can act as a simultaneous capture and target board, which is of great use in a BBI context.

2.3.3 Commercial platforms PARTIALLY UPDATED 2023-09-16 12:54:23+02:00

In addition to documented research BBI platforms, there are multiple commercially available solutions. We are going to address the most noteworthy in the current section.

2.3.3.1 Langer EMV-Technik GmbH BBI platform UPDATED 2023-09-16 12:54:23+02:00



Figure 2.2: BBI probe proposed by the company Langer EMV-Technik GmbH. Fig: langerBBI

The German society "Langer EMV-Technik GmbH" proposes a ready-to-use BBI platform. It is composed of two main hardware components:

- A BBI current pulse generator, illustrated in Fig. 2.2;
- A "Burst Power Station", which is the combination of a power supply and a controller allowing to control and monitor every probe sold by the company, with a provided software.

The core design is similar to the state-of-the-art platform, the main difference being that the system commercialized by Langer is marketed as being a current source instead of a voltage source. However, in practical operation, it does not represent a significant difference, since the major difference between a current source and a voltage source is their output impedance. Thus, one can either perform the BBI experiments with both electrical sources without much distinction, as long as the attacker is aware of these characteristics. The probe is specified with the following characteristics:

- A maximum allowable current of 4 A in a 1Ω load;
- A rise time inferior to 2 ns;
- A maximum pulse repetition frequency of 20 kHz;
- Positive and negative polarities;
- The possibility to delay the pulse command thanks to their control module;
- A jitter of ± 1 ns;
- A pulse width of 2 ns at full power, and of 4 ns at minimum power;
- A trigger delay ranging from 70 ns to 420 ns.

According to the product's datasheet, containing actual measurements of the probe, the minimal intensity allows injecting at peak approximately 2.4 A in 1Ω . However, contrary to the

open-source ChipWhisperer-Lite, there is very little official documentation about their products, thus reducing the available knowledge.

2.3.3.2 Riscure BBI platform UPDATED 2023-09-16 12:54:23+02:00

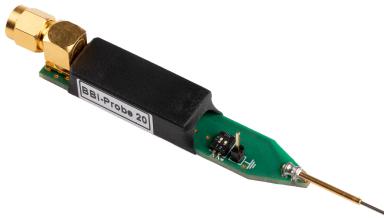


Figure 2.3: BBI probe proposed by the company Riscure BV. fig:riscureBBI

Similar to Ledge, Riscure proposes a quite complete BBI platform. It is composed, as before, of two major tools: a pulse generator and a metal probe. In that case however, the probes are passive ones. The generator, called "EM-FI Transient Probe", originally designed to be used in conjunction with EMFI probes, has the following characteristics:

- A maximum output voltage of $450 \text{ V} \pm 45 \text{ V}$;
- A maximum probe current (with 0 Ohm impedance) of 64 A ;
- A pulse width at half maximum output of 50 ns at full power (there is no mention of a controllable width);
- A trigger latency of 50 ns .

On the other hand, they propose four different BBI probes, one of them being illustrated in 2.3 which, in an odd way, are specified for different polarity and voltage amplitude depending on the model:

- A positive $200 \text{ V} \pm 40 \text{ V}$ with 15 ns pulse width;
- A positive $33 \text{ V} \pm 6.6 \text{ V}$ with 12 ns pulse width;
- A negative $37 \text{ V} \pm 7.4 \text{ V}$ with 20 ns pulse width;
- A negative $200 \text{ V} \pm 40 \text{ V}$ with 23 ns pulse width.

They include an SCS connector and a spring-loaded metal tip to avoid damage to the IC back-side. These BBI probes are meant to be used with the "EM-FI Transient Probe" pulse generator. Eventually, they provide a software to control their equipment.

2.3.3.3 NewAE Technology Inc. generators UPDATED 2023-09-16 12:54:23+02:00



Figure 2.4: Pulse generator for EMFI and BBI proposed by NewAE Technology Inc. fig:chipshouter

Eventually, NewAE Technology Inc. proposes various products for the practice of EMFI and BBI. Most of them can be used with one or the other fault injection method. I am going to cover two of them in this subsection.

The first one being the ChipSHOUTER®, with the pulse generator having the following characteristics:

- A voltage range comprised between 150 V to 500 V;
- A pulse width ranging from 15 ns to 480 ns depending on the connected load;
- A charge rate of 35 V/ms;
- An input jitter of 220 ps;
- A trigger latency of 50 ns;
- Python libraries allowing to interface and control the device;
- Monitor outputs allowing the user to probe internal signals.

This product costs around €4000 and the electrical schematics are available for free. It is a medium cost alternative compared to other equivalent pulse generator suh as the AVTECH AVRZ-5W-B from Avtech Electrosystems Ltd., the base model costing around \$15000.



Figure 2.5: PicoEMP: a low-cost pulse generator from NewAE Technology Inc. It provides much less instantaneous power than a typical generator, has a long recovery time (from 1 to 4 seconds), has a lower maximum amplitude (250 V), is not pre-calibrated, and has no controllable pulse width. However, it costs 94 % less than a typical generator, giving it a considerable advantage when building low-cost BBI platforms. fig:newAeChipShouter

The second product from NewAE is a very low-cost device: the PicoEMP. It is an open-source device, where safety and cost where the two main design rules. The tool is community maintained, and while originally designed for EMFI in mind, it was very recently studied concerning BBI in 2023 [25] by one of its contributors. A photograph of the device is shown in Fig. 2.5. Thanks to the low-cost design approach, the bill-of-materials for this tool is roughly equal to 50 \$., which makes it very accessible for anyone to build it from scratch. Its main characteristics and drawbacks are the following:

- It uses a transformer to generate high voltages, therefore no DC voltage option is available at its output;
- The output transformer is low-power, around up to 200 mW;
- The recovery time is slow, measured between 1 to 4 seconds depending on operating conditions;
- The maximum voltage pulse is of approximately 250 V;
- A pulse width of about 85 ns in $50\ \Omega$;
- There is no pre-calibration;
- It does not allow pulse width control by default. However, it is possible through drive signal control, even though being less accurate.

2.3.4 An overview about BBI platforms NEW 2023-09-16 12:54:23+02:00

From what I described previously, there are many different platforms and tools available for the practice of BBI. Their characteristics greatly vary from one platform to another, but they share a common ground, allowing to distinguish many tools and equipment constituting a typical BBI platform, which are the following:

- A metallic probe, allowing to make an electrical contact with the target backside, preferably spring-loaded;
- A voltage pulse generator capable of generating very high, short and precise pulses;
- A 3D positioning table, with a precision high enough for the application, to move the probe precisely with correct pressure on the backside;
- A preferably vibration-proof table to minimize probe physical jitter due to vibration caused by other equipment or natural vibration;
- A high precision oscilloscope to measure various physical quantities that might help to practice BBI.

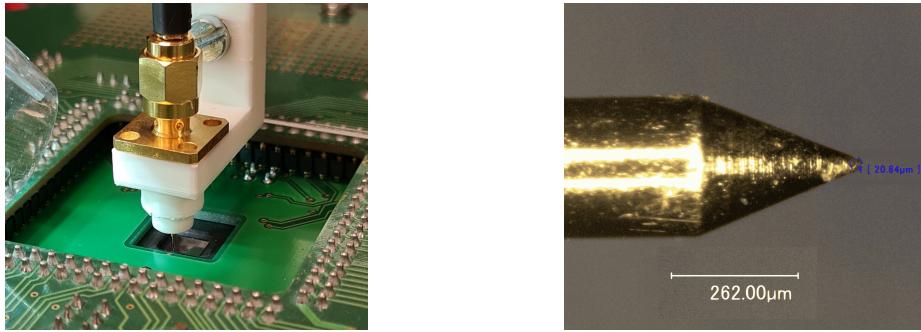
Some of these tools are not necessary to constitute a BBI platform, such as the positioning table, but they greatly simplify the platform reliability and reproducibility.

2.4 Our BBI platform PARTIALLY UPDATED 2023-09-16 12:54:23+02:00

With these tools in mind, we are describing in this section the platform we are using in our lab in detail.

2.4.1 The probe UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiPlatforms; subsect:probes



(a) Custom BBI probe in mechanical contact with the IC backside, seen through the perforated PCB

(b) Custom BBI probe microscopy physical measurements

Figure 2.6: Custom BBI probes photographs fig:sondePointeBBI

The most distinctive piece of equipment when working with BBI compared to other fault injection methods is the electrical probe. As we have seen before, it is commonly made with a metal tip, a connector of any sort and a mechanical support to hold the structure together. Some can be active, while others are passive, and therefore less expensive. However, it is very easy to build one, and any needle size available on the market can be used depending on the needs. In the case of BBI, the probe is used to establish the electrical contact with the substrate of integrated circuits, the latter being poorly conductive, but not isolating. For this work, we designed a custom probe, allowing us to control its characteristics, around three simple parts:

- An SMA connector, to have a low-cost, small and standard interconnection available with almost every high-speed equipment;
- A spring-loaded metallic tip soldered onto the SMA connector providing a better control over the applied pressure onto the backside;
- A custom 3D-printed support holding the parts together, shaped to fit with our other tools.

Fig. 2.6 shows detailed pictures of the probe we designed, with a photograph in operation in Fig. 2.6a, and a photograph under a microscope of the probe tip-end in Fig. 2.6b, allowing to measure its actual size before its first usage. The metallic probe we had chosen has a 0.635 mm diameter and is 16.35 mm long. The specified maximum nominal current of the probe is of 1.5 A, and the electrical contact resistance measures approximately 70 mΩ. The tip has a diameter

roughly equal to 20 μm , and it is important to note that this value tends to increase when the probe is utilized, due to the physical contact and the pressure with the IC backside. The bill-of-materials cost for our custom probe tool is roughly equal to 20 \$, ignoring manual labor to assemble everything together.

2.4.2 The generator UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiPlatforms; subsect:generator

The other fundamental piece of equipment when practicing BBI is the voltage pulse generator. It is, generally, one of the most expensive platform tool, similar to EMFI. Indeed, because BBI relies on voltage pulses to disturb an IC, it is necessary to provide a precise control over the pulse parameters to the user, such as the voltage set point, the pulse duration, etc.



Figure 2.7: Front side of the Avtech Electrosystems Ltd. AVRK-4-B High Voltage Pulser, used during all my thesis experiments.

fig:avrk4b

For my thesis, I am using a precise high speed and high voltage pulse generator to be able to finely study the voltage pulse characteristics effects on BBI, more specifically the AVRK-4-B from Avtech Electrosystems Ltd. It is shown in Fig. 2.7, and costs around \$14500 in its most basic configuration. Similar to the low-cost generator described previously, it is commonly used for EMFI, but is also suitable for BBI. Its main specifications are the following:

- The voltage pulse amplitude is specified between 150 V and 750 V with positive and negative polarities. The generator can go below and above these thresholds, however, there is no guarantee of the set point value correctness;
- The pulse width is specified between 6 ns and 20 ns. Similar to the voltage, the generator can go down from 4.5 ns, up to 22 ns, but is not specified out of the default range;
- Rise time (resp. fall time) for positive (resp. negative) pulses is specified to be precisely of 4 ns. Fall time (resp. rise time) for positive (resp. negative) pulses is not specified and depends on the generator load characteristics;
- The recovery time is inferior to 1 ms, allowing a pulse repetition frequency up to 1 kHz;
- The minimal propagation delay measures 150 ns, and can be raised up to 1 s;
- The jitter measures $\pm 100 \text{ os} \pm 0.03\%$ of the propagation delay;
- The output is DC-coupled, allowing the generator to continue providing energy to the load (if resistive or inductive) during the pulse plateau;
- All the specifications presuppose that the generator is loaded precisely with 50Ω .

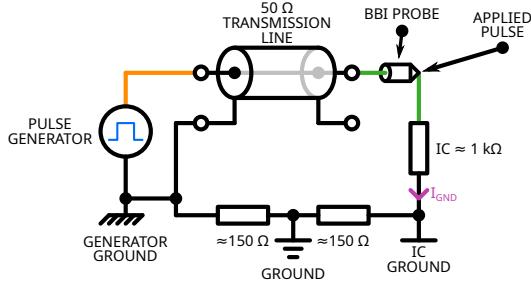
2.5 BBI in practice PARTIALLY UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiInPractice

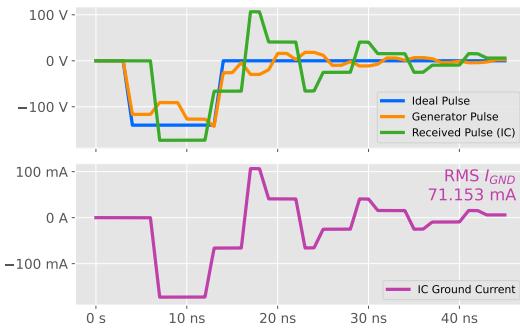
With actual BBI platform in mind, let me introduce a typical BBI platform model that we are going to study in details. These models allow us to concisely understand, evaluate and simulate BBI platforms behavior, limitations and room for improvement. We will therefore analyze the platform's performance and point out its weaknesses.

2.5.1 Typical BBI platform model UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiInPractice; subsect:bbiPlatformModel



(a) Model of a state-of-the-art BBI setup. It consists of the voltage pulse generator, the BBI metal probe, the transmission line, the IC ($1\text{ k}\Omega$ resistor), and the platform grounding (two $150\text{ }\Omega$ resistors). This model allows for fast evaluation and prediction of the BBI platform macro-behavior.



(b) Simulation results of the BBI model. Blue: ideal voltage pulse (-140 V, 10 ns). Green: effective signal applied on the IC backside. Orange: generator output. Purple: IC ground current. These results highlight the platform limitations: ringing (impedance mismatch) and high ground impedance, leading to higher voltage.

Figure 2.8: BBI platform electrical model developed for my thesis to quickly evaluate various platform's parameters, alongside the model simulation results.

fig:bbiBadGndGlobalFig

To be able to quickly predict and analyze BBI platforms, I developed a very simple electrical model, illustrated in Fig. 2.8a. This model represents the key components of a BBI platform, which are:

- The voltage pulse generator;
- The transmission line, used to connect the probe to the generator;
- The BBI probe;
- The targeted IC, modeled by an electrical resistance;
- The grounding installation, consisting of electrical resistances connected between equipment grounding.

2.5.2 Platforms evaluation criteria UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiInPractice; subsect:platformEvalCrit

For the purpose of evaluating BBI platforms, we decided to focus on two important criteria, allowing to represent the platform quality:

- The characteristics of the voltage pulse measured at the generator output, allowing to observe how the generator behave when loaded with the transmission line and the IC;
- The characteristics of the target ground current waveform, allowing to monitor exactly what is actually injected into the IC.

2.5.3 Raw results UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiInPractice; subsect:rawRes

To that end, we will deeply analyze the platform's simulation results shown in Fig. 2.8b. Four signals are displayed, with their colors matching the colors in Fig. 2.8a for greater clarity. There are three voltage waveforms and a current waveform. The blue waveform is the ideal voltage pulse an attacker want to apply to the backside of an IC during a body biasing injection. Its characteristics are the following: a voltage set point of -140 V and a pulse width set point of 10 ns. It is a steep, fast and precise pulse with controlled rise and fall times, pulse width and voltage. However, when performing real experiments, which the model allow us to evaluate, this ideal pulse falls apart. It can be seen thanks to the orange and green waveforms, representing respectively the pulse observer at the generator output and the pulse effectively applied onto the backside of the IC target. There are multiple obvious observations that can be made concerning the received pulse (green) signal:

- The voltage set point is not respected, with a 23.5 % negative percentage overshoot (PO) on the falling edge, and a 107 % positive percentage overshoot (PO);
- There is obvious ringing, causing the pulse width to be longer than expected in addition to damped oscillations

These effects can also be observed on the IC ground current waveform (**purple**), as it is a mirror of the applied pulse due to the pure resistive nature of the IC in that model.

2.5.4 Analysis conclusions UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:bbiInPractice; subsect:analysConcl

In order to understand the implications of such observations, let us analyze each one of them.

The first important thing to note is that the various model numeric values are extracted from our actual platform. Therefore, the $150\ \Omega$ grounding and the $1\ k\Omega$ IC are average measured values of actual devices. Thus, these parameters, in addition to the transmission line characteristics, will inevitably vary with a certain amount from one platform to another.

Indeed, the backside surface of an IC does not equal to a constant load. In addition to this, if the IC substrate is thinned, these values will change even more. Therefore, depending on the probe location and the IC substrate thickness, the generator might not see the exact same load. To illustrate the induced effects of such differences, I performed simulations with various IC

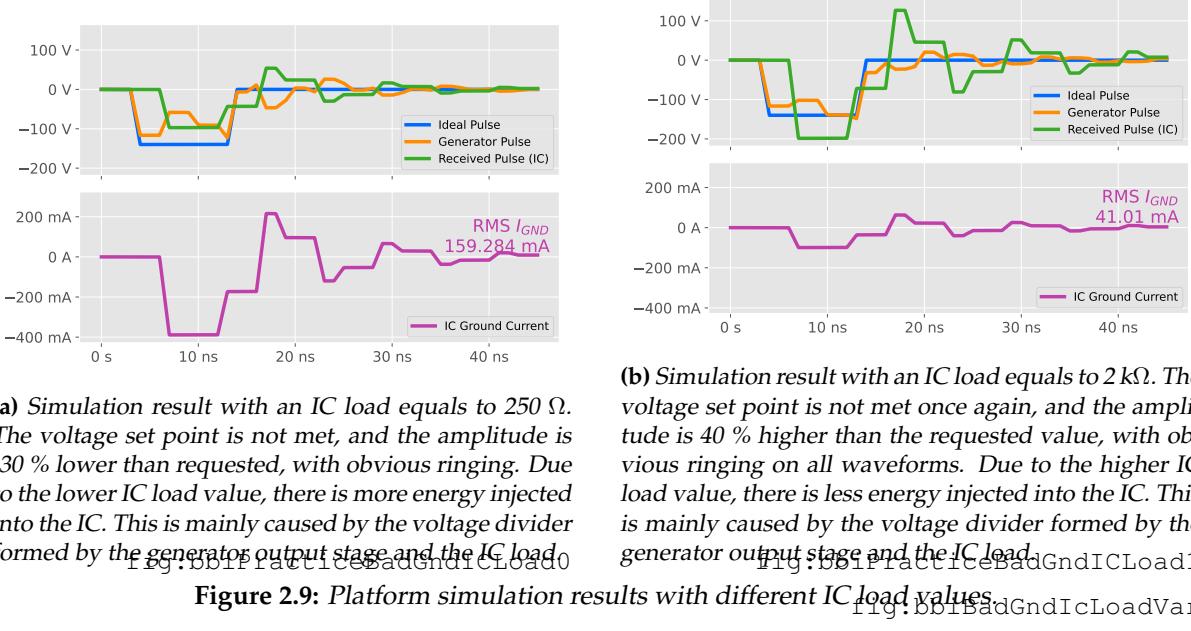


Figure 2.9: Platform simulation results with different IC load values.

values, representing typical measured values for my IC target when thinned down to $50 \mu\text{m}$, up to more than $700 \mu\text{m}$, and the results are shown in Fig. 2.9, both for a 250Ω load (Fig. 2.9a), and a $2 k\Omega$ load (Fig. 2.9b). In both cases, due to the non-zero generator output impedance, the latter forms a voltage divider with the IC load. On the one hand, with an IC load value one quarter lower, there is more current in it, while the applied pulse amplitude is 30% lower. On the other hand, with an IC load value two times higher, there is less current in it, while the applied pulse amplitude is 40% higher. It represents a 70 % range around the set point value, which is excessively high. However, in both cases, the ringing is still present with the same amount relative to the pulse amplitude.

Eventually, all of these observations allow us to spot three major flaws of such platform:

- The platform parameters are difficult to control, leading to unknown values concerning pulse width, voltage set point, etc.;
- It leads to a poor temporal accuracy, thus minimizing the chances to perform a precise and repeatable fault injection;
- At last, all parameters are platform dependent, leading to a low reproducibility rate, thus lowering the credibility of experiments performed on such platforms.

In this context, I present in the next section various simple improvements to the BBI state-of-the-art platform.

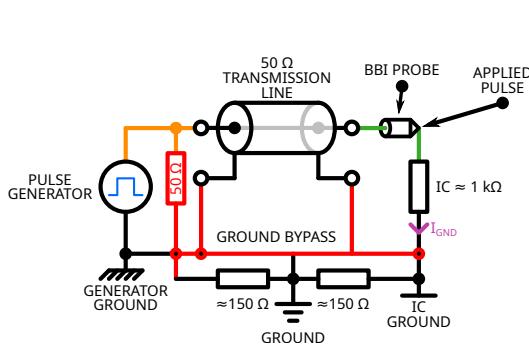
2.6 Enhanced BBI platform model and simulation 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:enhancedBBIPatterns

In this section, I propose platform enhancements over the state-of-the-art BBI platform previously introduced. These improvements aim at being low-cost, fast and easy to set up, to represent an interesting addition without drastically increasing the platform financial cost. Eventually, I am able to draw conclusions on such improvements thanks to simulation results.

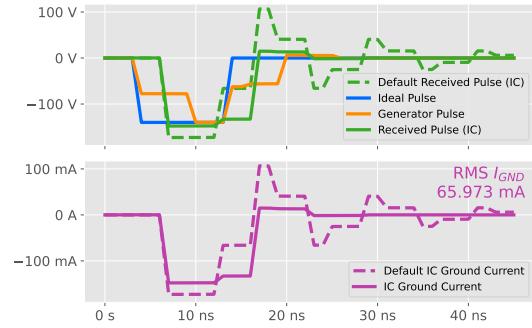
2.6.1 Matching the generator output impedance UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:enhancedBBIPatterns; subsect:bbiGenImpMatch



(a) Enhanced BBI platform model. It describes the generator, the BBI probe, the transmission line, the IC ($1\text{ k}\Omega$ resistor), the default platform grounding (both $150\text{ }\Omega$ resistors), and the enhancements highlighted in red, which are: creating an approximate impedance matching for the generator, and bypassing the poor grounding with low impedance copper wires.

fig:bbiPracticeImpGnd



(b) Simulation results of the enhanced BBI model. Blue: ideal voltage pulse (-140 V, 10 ns). Green: effective signal applied on the IC backside. Orange: generator output. Purple: IC ground current. The dotted waveforms are those observed in Fig. 2.8b. The most obvious observed improvements concern the set points, which are fully respected, in addition to the drastic ringing reduction, leading to better temporal control.

fig:bbiPracticeImpGndSignals

Figure 2.10: BBI platform enhanced electrical model developed for my thesis to quickly evaluate various platform parameters, alongside the model simulation results.

fig:bbiImpGndGlobalFig

The first proposed improvement concerns the generated voltage pulse characteristics. As we observed previously, the various parameters set points were not met. In a fault injection context, it is an undesirable behavior, as it is required to finely control the generated pulse to produce controlled disturbances into ICs. Therefore, and because most high speed high voltage pulse generator are specified to be loaded with a precise impedance, I simply propose to connect a known load directly at the output of the generator model. In my model, a $50\text{ }\Omega$ resistor is loaded at the generator output, as illustrated in red in Fig. 2.10a. Thus, the generator sees the impedance network formed by the compensation load, the IC, the transmission line, and the grounding installation. However, because the grounding installation is platform dependent, it is required, in order to perform a better impedance matching of the generator output, to improve the grounding, which leads to the other platform enhancement described in the following section.

2.6.2 Improving the grounding installation UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:enhancedBBIPlatforms; subsect:bbiGndBetter

In many platforms, the grounding installation might be perfectly fine, and the following section may not apply to them. However, with our platform, we quickly observed that the grounding impedance was far from negligible. Indeed, with an average IC impedance around $1\text{ k}\Omega$, and inter-equipment ground impedance around $150\text{ }\Omega$, it represents a 15 % increase in the total impedance seen by the generator. Therefore, in order to transfer a maximum amount of energy into the IC, especially in areas where the IC impedance might be closer to the grounding impedance, it is required to cancel as much as possible the latter.

To that end, I propose a very simple setup modification. It consists in keeping the platform as is, and adding short copper wires between equipment grounds. Therefore, they shunt the platform ground and creates a low-impedance path for electric charges, thus allowing the previous section approximate impedance matching to perform better.

2.6.3 Simulation results UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:enhancedBBIPlatforms; subsect:simRes

To verify the soundness of the previously proposed enhancements, I performed simulations thanks to the model presented in Fig. 2.10a. The simulation results are shown in Fig. 2.10b.

In that case, unlike in the state-of-the-art platform, the voltage set point is almost met concerning the received pulse (green waveform), with a slight undershoot of 6%. It is mirrored on the IC ground current waveform, where the ringing is drastically reduced, which leads to a steeper and more accurate pulse. It is especially noticeable when directly comparing the state-of-the-art waveforms in dotted lines. Concerning the generator pulse (orange waveform), it is still distorted as the ringing has not disappeared, but is less of a concern since the waveform of interest is the one effectively applied to the IC backside.

2.6.3.1 Load dependency NO CHANGES 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:enhancedBBIPlatforms; subsect:simRes; subsubsect:loadDep

To further analyze the benefits of the proposed improvements, I performed, as for the state-of-the-art platform, additional simulations with various loads. As before, $250\text{ }\Omega$ and $2\text{ k}\Omega$ were chosen to have a common point of comparison. As I stated previously, these values are chosen to match the average typical value of my IC target when thinned down to $50\text{ }\mu$, up to $700\text{ }\mu\text{m}$.

Fig. 2.11 presents the simulation results for such loads. For both loads, the measured voltage moves away from the set point by around 7 % in each case. It represents a 14 % range around the -140 V set point, which is immensely better than in the previous platform. It is still not perfect, but the platform is overall less dependent to the IC load, which is desirable in order to have repeatable voltage pulse across the entire IC backside.

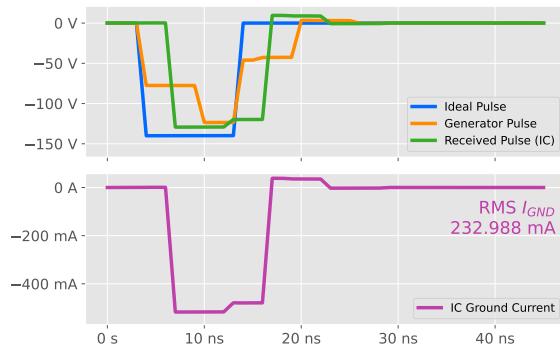


fig:bbiPracticeImpGndICLoad0

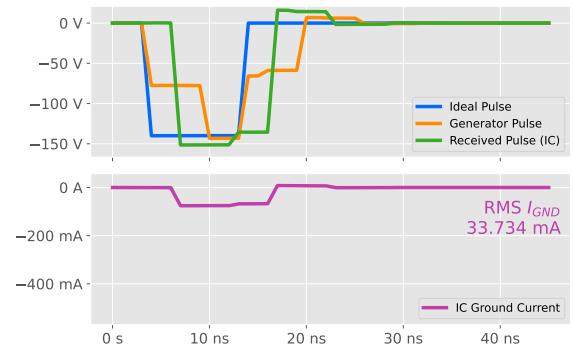


fig:bbiPracticeImpGndICLoad1

Figure 2.11: Simulation results of the enhanced platform with a 250Ω IC load (2.11a) and a $2 \text{ k}\Omega$ IC load (2.11b). The current increase in 2.11a is natural due to the load impedance reduction. However, the effective pulse amplitude relative to the set point has only a -7 % error, which is a drastic improvement over the previous -30 %. The set point is met. Then, in 2.11b, the current decrease is logical given the higher impedance value. The effective pulse amplitude relative to the set point has only a 7 % error, which is a drastic improvement over the previous 40 %. The ringing almost disappeared in every case. It is because the generator is not only loaded by the IC, but by the equivalent load composed of the IC and the compensation load, which reduces the effective load variation when changing the IC load value.

Then, quite naturally, for the 250Ω load, the current is higher than for the $1 \text{ k}\Omega$, and with the $2 \text{ k}\Omega$, it is lower. In addition to that, thanks to the 50Ω resistor placed at the generator output, it reduces the range in which the effective load (the compensation load in parallel with the IC) changes. Indeed, it goes from around 42Ω to about 49Ω , instead of going from 250Ω to $2 \text{ k}\Omega$ in the previous case. Eventually, in addition to all of the above, these enhancements have also drastically reduced ringing, which contributes to the applied pulse amplitude being closer to the set point.

2.6.4 Simulation conclusions NO CHANGES 2023-09-16 12:54:23+02:00

All of this leads to better control over the various platform parameters, allowing for more accurate and shorter pulses, closer to the expectations. In addition to that, the platform is less design dependent thanks to the minimization of impedance mismatch and poor grounding installation. It leads to a better time accuracy, enabling potentially more controllable fault injections.

2.7 Actual enhanced BBI platform PARTIALLY UPDATED 2023-09-16 12:54:23+02:00

The previous models being a useful tool to draw quick conclusions and predictions, it does not represent the reality. To that end, I set up the various presented enhancements in an actual BBI platform in order to verify the soundness of all the outcomes. In the first place, we are going to discuss how to perform the approximate impedance matching. Then, I will explain how to set up an efficient grounding bypass. After that, we will take a look at actual measurements

allowing to spot the improvements.

2.7.1 Generator impedance matching in practice UPDATED 2023-09-16 12:54:23+02:00

Add pictures of real platform impedance matching. An ideal impedance matching implementation should be adaptive and vary the impedance seen by the generator to perfectly match 50 Ω in every case. It would require a system with feedback, capable of measuring in real time the impedance presented by the IC target, in addition to the transmission line characteristics, to be able to adapt the compensation load impedance value. However, this is not the approach I have chosen. Indeed, the goal here is to minimize financial cost and platform modification, while allowing for better control over the platform parameters.

Another possibility would be to first measure the average IC backside impedance over its entire area or only the targeted area (such as the cryptographic core for instance). Then, thanks to the average value, the compensation load impedance could be chosen to better match the required 50 Ω .

Eventually, the selected solution is the simplest one. It consists in connecting a compensation load at the generator output, consisting in a 50 Ω SMA terminator. It is far from ideal, as this solution does not consider the transmission line nor the IC effective load nor the capacitive and/or inductive nature of the IC in addition to its resistive nature. However, it is a solution requiring little to no change to an existing platform and has proven to be good enough thanks to the previous models.

2.7.2 Grounding installation bypass in practice UPDATED 2023-09-16 12:54:23+02:00

Add pictures of real GND bypass. As we discussed previously, the grounding installation can drastically vary from one platform to another. Its effective impedance can be very high, such as in our platform, where equipment is grounded thanks to the platform earthing, with inter-equipment ground of around 150 Ω . To alleviate the effects of such ground impedance, I simply decided to shunt the existing earthing with short low-resistance copper wires. To that end, I chose an arbitrary piece of equipment as the reference, and connected every other piece of equipment local ground to the reference. It allowed reducing the effective platform ground impedance to a value close to 0 Ω .

2.7.3 Practical analysis UPDATED 2023-09-16 12:54:23+02:00

Now that I presented how to practically set up the enhancements, let us analyze actual measurements on the platform. We will compare before and after results, allowing us to analyze each evaluation criterion. As it was done for the simulations, we will observe the voltage pulse

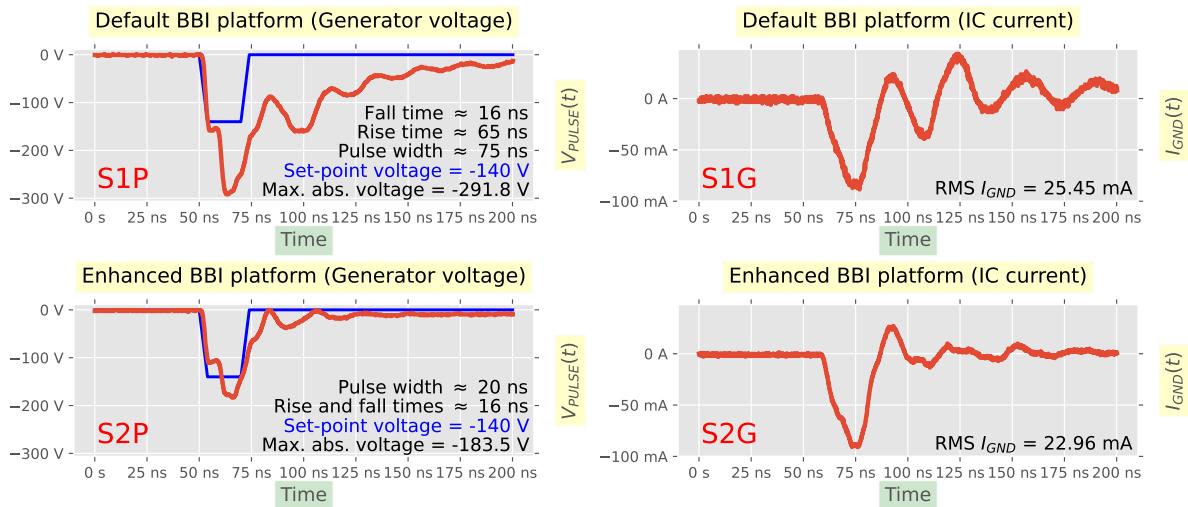


Figure 2.12: BBI platforms comparison: state-of-the-art (*S1P* and *S1G*) versus the proposed enhanced platform (*S2P* and *S2G*). The ideal voltage pulse is -140 V ample and 20 ns wide, with rise and fall times of 4 ns. *S1P* shows a -108 % negative percentage overshoot. PW is 275 % too high with a 75 ns value. The fall time is 4 times higher than requested, and the rise time is more than 15 times higher. *S1G* highlights the ringing, seen on *S1P* on a lesser extent. On *S2P*, the voltage set point negative PO measures -31 %. PW now perfectly matches the set point of 20 ns. Rise and fall times are 4 times higher than they should be, despite both being consistent. *S2G* shows significant ringing reduction, while maintaining the same amount of transferred energy into the IC.

fig:bbiRealXp

and the IC ground current.

Fig. 2.12 presents the various waveform results. The voltage pulse was measured at the IC backside during the injection, and the IC ground current was measured using a current probe thanks to the IC PCB ground interconnection. Therefore, the measured current is precisely the IC ground current, excluding any other equipment. The four waveforms displayed in Fig. 2.12 are code named using three characters for clarity. The first character is common to all waveforms, denoted "S" for "setup". Then, the number indicates which platform is concerned, "1" being the default platform, "2" being the enhanced one. Eventually, the last letter indicates which waveform is observed, "P" being the voltage pulse, "G" being the IC ground current. Therefore, the default platform contains *S1P* and *S1G* waveforms, while the enhanced one contains *S2P* and *S2G* signals. Fig. 2.12 also displays the waveforms characteristics for more clarity. The ideal voltage pulse applied has a maximum negative amplitude of 140 V, a pulse width of 20 ns, and 4 ns rise and fall times.

S1P shows a clear undershoot of -108 % under the set point. It is a clearly non-negligible value, which is far from desirable when performing fault injection, as most of the time, the voltage value has a great importance concerning efficiency and repeatability. In addition to this, the pulse width is 275 % higher than its set point. It is an additional undesirable behavior, especially when one wants to inject precise disturbances into an IC under test. Then, fall time is four times higher than requested, and rise time is more than fifteen times higher. Put with the longer pulse width, it worsens the pulse accuracy.

S1G brings to light the obvious ringing issue, also observable to a lesser extent on S1P, which leads to longer than expected disturbance inside the IC. Considering that the ringing is mainly caused by impedance mismatch between the generator and the IC, it will drastically change from one location to another, further reducing repeatability.

S2P, on the other hand, shows a better voltage amplitude, with a -31 % undershoot. It is far from perfect, but given the approximate nature of the proposed impedance matching, it was to be expected. Concerning the pulse width, the set point value is perfectly respected, which is very important for precise disturbance duration. However, rise and fall times are now consistent, but still four times higher than requested. It can easily be explained by the fact that the transmission line, the probe, the IC and the power installation are not a purely resistive load. Therefore, any capacitive element in the chain will inevitably reduce the system response time, thus elongating rise and fall times, leading to a shorter pulse plateau.

Concerning S2G, the approximate impedance matching shows a clear ringing reduction, with a steep current pulse, leading to a precise disturbance.

2.8 Enhanced BBI platform in a fault attack context UPDATED 2023-09-16

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chap:2_goodPractices; sect:enhancedBBIGiraudAttack

Now that we have seen with simple actual experiments the benefits of the proposed enhanced BBI platform, let us linger on further experiments to verify more thoroughly the soundness of these enhancements. To that end, I performed a differential fault attack on our IC target. More specifically, a constraining fault attack requiring single bit faults on one or more bytes working on an AES cryptographic core, introduced by C. Giraud [16] in 2002, submitted in April 2002 to CHES'02. In the first place, we are going to discuss in details the core of the attack. Afterward, I will describe the IC target, its characteristics, and its operating conditions for the experiments. Then, I will introduce experiments we developed to perform preliminary measurements to the attack, accelerating the search of points of interests on the IC. Next, we will discuss the practical attack results. Eventually, we will draw conclusions on the various observations.

2.8.1 Giraud's DFA detailed description NO CHANGES 2023-09-16 12:54:23+02:00

When Giraud's paper [16] was published in 2002, no existing DFA was capable of attacking an AES algorithm. In this context, they proposed two types of DFA on AES, in order to cover various fault types one can induce on secured ICs. In this thesis, I focused on the first fault model, consisting in inducing single bit faults, therefore, this is the one we are going to discuss and describe in details in this section. It is interesting to note that Piret and Quisquater published another DFA one year after Giraud to CHES'03 [26], but I focused on Giraud's DFA for my thesis.

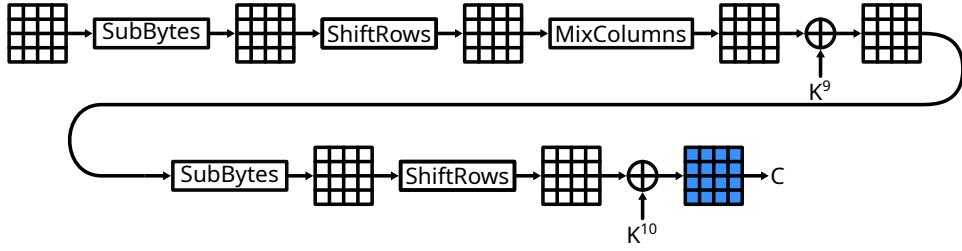


Figure 2.13: The two last rounds of an AES-128 fig:aesLastRounds

As we said before, the attack requires single bit faults on AES computation. More specifically, the fault has to appear at the beginning of the final AES round. Because we are using an AES-128, we will describe everything with this in mind. In addition to this, the various notations we will be using are the following:

- P is the AES plaintext and K the AES secret key
- P^i stands for the intermediate cipher result after the i^{th} AES round
- P_j^i is the j^{th} byte of P^i
- K^i represents the i^{th} AES round key
- As for P , K_j^i is the j^{th} byte of K^i
- C is the correct ciphertext, C_j is the j^{th} byte of C
- Eventually, CF stands for the faulty ciphertext, CF_j is the j^{th} byte of CF

Although the attack requires single bit faults on the final round, the attack is fairly simple and quick to perform with the right data at hand. I will not describe how AES operates, as it is well described in [16, 27]. The final ciphertext is given thanks to the following equation:

$$C = ShiftRows(SubBytes(P^9)) \oplus K^{10} \quad \text{cipherGiraud1} \quad (2.1)$$

With $SubBytes(P_j^i)$ being the substitution table (S-box) result calculated on M_j^i byte, and $ShiftRow(j)$ being the j^{th} byte position of the temporary result of the $ShiftRows$ transform. Thanks to eqn. 2.1, we can then deduce:

$$C_{ShiftRow(i)} = SubByte(P_i^9) \oplus K_{ShiftRow(i)}^{10}, \forall i \in [0, 15] \quad \text{cipherGiraud2} \quad (2.2)$$

If an attacker manages to induce a fault e_j on a single bit of the j^{th} byte of the intermediate cipher P^9 before the AES final round, we have the following faulty ciphertext CF :

$$CF_{ShiftRow(j)} = SubByte(P_j^9 \oplus e_j) \oplus K_{ShiftRow(j)}^{10} \quad \text{faultyCipherGiraud1} \quad (2.3)$$

Which then gives us as before:

$$CF_{ShiftRow(i)} = SubByte(P_i^9 \oplus e_i) \oplus K_{ShiftRow(i)}^{10}, \forall i \in [0, 15] \quad \text{faultyCipherGiraud2} \quad (2.4)$$

If there is no fault on the i^{th} byte of P^9 , thanks to eqns. 2.2 and 2.4, we have the following relation:

$$C_{ShiftRow(i)} \oplus CF_{ShiftRow(i)} = 0 \quad \text{griaudNoByteFault_ith} \quad (2.5)$$

If there is a fault on P_j^9 , we have, thanks to eqns. 2.2 and 2.3:

$$C_{ShiftRow(j)} \oplus CF_{ShiftRow(j)} = SubByte(P_j^9) \oplus SubByte(P_j^9 \oplus e_j) \quad \text{griaudFault} \quad (2.6)$$

Eventually, we have to first calculate ShiftRow(j), which gives us the location of the only non-zero byte of $C \oplus CF$, which in return gives us j . We then need to find P_j^9 : we look for the single bit fault e_j , and identify an ensemble of values of P_j^9 satisfying eqn. 2.6. For each correct value, we increase a counter by 1. Then, by taking another faulty ciphertext CF , and the correct value for P_j^9 should be counter more often than another incorrect value. Therefore, we can identify the correct value thanks to that affirmation. This process shall be repeated as much as needed to find every bytes of P^9 .

Thanks to eqn. 2.1, it is possible to retrieve the last round key K^{10} , which can be then converted to the AES secret key thanks to the inverse Key Scheduling applied on K^{10} . **To finish.**

2.8.2 Integrated circuits target characteristics UPDATED 2023-09-16 12:54:23+02:00

For the purpose of understanding clearly how we set up the previous attack, it is required to describe thoroughly the integrated circuit targeted. The model is an STM32F439VIT6 32-bits ARM Cortex-M4 microcontroller from STMicroelectronics, available in a LQFP100 package. The IC is manufactured using a 90 nm bulk technology. Its main characteristics are the following:

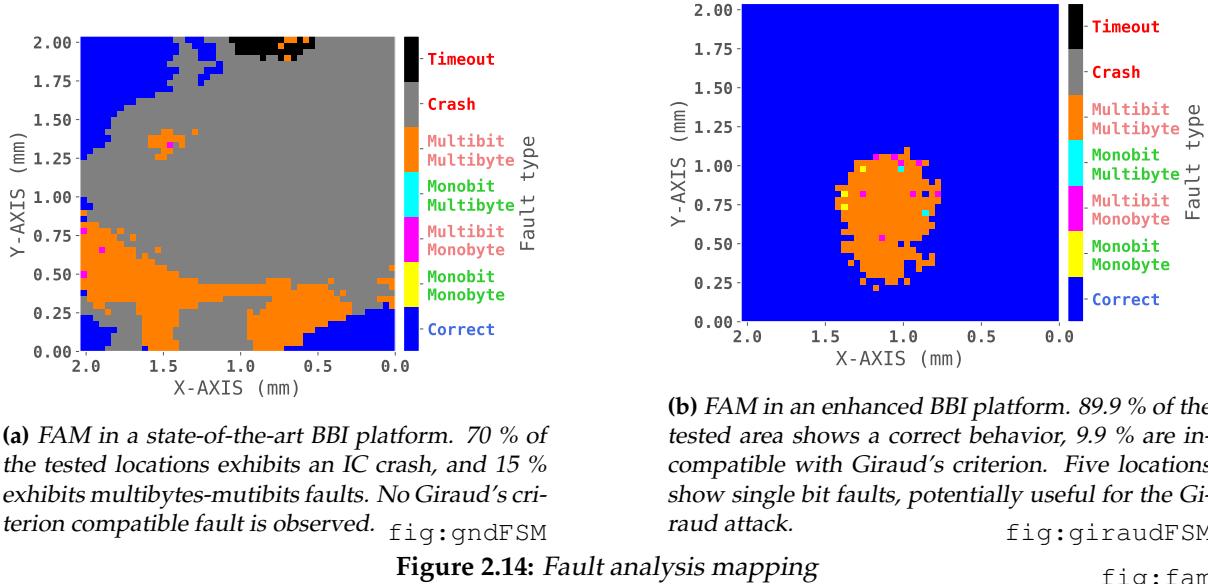
- A core clock up to 180 MHz;
- Two 1 MB FLASH memory banks;
- 256 kB of RAM;
- Voltage supply allowed from 1.7 V to 3.6 V;
- A True Random Number Generator (TRNG);
- A dedicated hardware cryptographic coprocessor, embedding AES (128, 192 and 256 bits), triple DES, and various HASH algorithms;
- A 700 μ m substrate thickness.

For the purpose of every other experiment, the IC is clocked at 40 MHz thanks to an external 8 MHz crystal oscillator.

2.8.3 Preliminary attack experiments UPDATED 2023-09-16 12:54:23+02:00

2.8.3.1 Fault analysis mapping description UPDATED 2023-09-16 12:54:23+02:00

For the purpose of accelerating and simplifying the attack process, especially because creating single bit faults is a troublesome process, I designed experiments to be conducted on the IC target, allowing me to spot interesting IC areas to perform the attack on. Because the attack targets the AES coprocessor, all the experiments described here are performed specifically on the AES core area.



These experiments are called "Fault Analysis Mapping" (FAM), and two results are shown in Fig.2.14. An FAM consists in performing BBI on the cryptographic core of the IC and trying to inject faults while identifying its behavior. We separated seven fault cases, described in Table 2.1.

| Fault type | Description |
|--------------------|--|
| Correct | The AES outputs a correct result |
| Monobit Monobyte | The fault is located on a single bit on a single byte |
| Multibit Monobyte | The faults are located multiple bits on a single byte |
| Monobit Multibyte | The faults are located multiple bytes and are single bit |
| Multibit Multibyte | The faults are located multiple bytes and multiple bits |
| Crash | The microcontroller did not respond correctly |
| Timeout | The microcontroller was unresponsive |

Table 2.1: FAM faults description

`table:faultType`

Over the seven outcomes, only two of them can lead to potential exploitable fault according to Giraud's criterion: Monobit Monobyte and Monobit Multibyte. We performed these exper-

iments on a state-of-the-art (default) platform and on our enhanced platform, with the exact same equipment on both platforms.

2.8.3.2 Fault analysis mapping comparison NEW 2023-09-16 12:54:23+02:00

The FAMs I performed have the following parameters:

- A voltage pulse amplitude ranging from -150 V to -400 V with -5 V steps;
- A fixed pulse width of 4.5 ns;
- A fixed pulse delay of 150 ns + 553 ns allowing to target the penultimate AES round;
- The mapping measures 2 mm by 2 mm, with an isotropic displacement step of 40 μm .

These experiments take from 16 hours at best, up to 36 hours at worst to perform. It is quite long, however, compared to blindly looking for the correct location to perform the Giraud's attack, it is statistically much faster, especially when the AES approximate location is known to the user. I performed two FAMs, on the same IC target, for a state-of-the-art platform and for the proposed enhanced platform. FAM results are shown for the default platform in Fig. 2.14a and for the enhanced platform in Fig. 2.14b.

On the one hand, concerning the state-of-the-art platform, where the FAM is shown in Fig. 2.14a, we can spot numerous locations where a microcontroller crash was observed, more specifically 70 % of the tested locations. It is problematic as this behavior cannot lead to any meaningful data to perform a fault attack. Despite trying numerous experiment parameters, I was never able to obtain a single bit fault on any physical location on the AES core, even considering the ringing and reducing the voltage down to -20 V, to a point where the generator is not specified anymore to deliver consistent amplitudes.

On the other hand, without any tweaking, the FAM results show five single-bit faults. In addition to this, the IC did not crash at any given moment, and eight multi-bit faults can be spotted. It gives valuable information related to potentially interesting areas where the Giraud's DFA could be performed. It does not mean that the attack can be performed entirely on a single location, but it is a great way to guide the attack process, knowing that the set of parameters used is sound.

2.8.4 Attack results and analysis NEW 2023-09-16 12:54:23+02:00

Thanks to the previous FAM results, I decided to perform the attack on every location candidate using the enhanced platform. For each location above the AES core, a parameter sweep was performed, consisting in finding for each set of parameters, as much single bit faults as possible. The test settings are the following:

- The voltage pulse set point ranging from -300 V to -600 V;
- The pulse width ranging from 4.5 ns to 5.5 ns;
- The injection delay ranging from ± 10 ns around the penultimate AES round.

For each set of parameter, I set a limit of 100 single bit faults. However, this is an optimistic goal which, in some cases, can take a very long time to be achieved, and in other cases, cannot be achieved at all. Therefore, I decided to limit the number of trials to 10000, allowing the test algorithm to be finite and quick to perform. Then, with these results, I was able to perform the attack, where the result are shown in Table 2.2.

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
|-----|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| K10 | 0xFF | 0x1F | 0x42 | 0xE8 | 0xEF | 0x44 | 0xA5 | 0x6A | 0xCA | 0xE7 | 0x55 | 0x3C | 0xFD | 0x65 | 0x39 | 0x26 |
| KEY | 0x01 | 0x23 | 0x45 | 0x67 | 0x89 | 0xAB | 0xCD | 0xEF | 0xDE | 0xAD | 0xBE | 0xEF | 0x12 | 0x34 | 0x43 | 0x21 |

Table 2.2: Giraud's DFA results. In yellow are indicated the bytes retrieved with a brute-force method instead of the Giraud's bit fault attack.

table:dfaResults

What is obvious at first glance is that I was not able to retrieve the 16 bytes of K^{10} . Indeed, without further search for valid locations above the AES core, I was able to retrieve 14 out of 16 bytes. It is a great result, as the attack took about 20 hours to perform, including the FAM, which was the longest experiment to set up the attack. However, to retrieve the secret key, it is required to find all 16 bytes of K^{10} . Because there are 16 bits left, it is not particularly relevant to try to find interesting locations to perform Giraud's DFA, as there are only 65536 combinations to blindly test at worst to find the correct last round key. Considering the platform computer is able to perform approximately $188 \cdot 10^3$ encryptions per second, it would take $\frac{2^{16}}{188 \cdot 10^3} \approx 349 \cdot 10^{-3}$ seconds to perform the required calculation in the worst scenario. I then blindly tested every possibility to find the last two bytes, and I was able to retrieve them, thus allowing me to retrieve the AES secret key. These brute-forced bytes are shown in yellow in Table 2.2.

To finish.

2.9 Conclusion UPDATED 2023-09-16 12:54:23+02:00

chap:2_goodPractices; sect:conclusion

In this chapter, I first introduced existing BBI platforms both in the state-of-the-art and commercially available. We have seen that multiples solutions ranging from low prices to very high prices exist, each one having its own advantages and disadvantages concerning their characteristics. Thanks to this platform overview, I was able to enumerate the fundamental building block of a typical BBI platform. After that, I presented the platform used during my thesis experiments, from the custom probe to the generator. Afterward, I introduced electrical models I designed to quickly compare and evaluate BBI platforms. We studied the simulation results of such models, which allowed me to introduce enhancements to existing BBI platforms, allowing for better accuracy and reproducibility. Thereafter, I presented experiments performed to verify

the soundness of such models, comparing state-of-the-art platforms to the enhanced platform I propose. Eventually, to go further in the model validation, I described and performed a constraining differential fault attack on a hardware AES coprocessor, sustaining the usefulness of the proposed enhancements.

III

Integrated circuits modeling 2023-09-16 12:54:23+02:00

chap:3icModeling

Contents

| | | |
|-------|---|----|
| 3.1 | Summary <small>2023-09-16 12:54:13+02:00</small> | 38 |
| 3.2 | Introduction <small>2023-09-16 12:54:13+02:00</small> | 38 |
| 3.3 | Electrical models <small>2023-09-16 12:54:13+02:00</small> | 39 |
| 3.3.1 | Standard-cell segment models <small>2023-09-16 12:54:13+02:00</small> | 42 |
| 3.4 | Preliminary model validation <small>2023-09-16 12:54:13+02:00</small> | 45 |
| 3.5 | Voltage pulse generator model and further validation <small>2023-09-16 12:54:13+02:00</small> | 46 |
| 3.5.1 | Early generator models <small>2023-09-16 12:54:13+02:00</small> | 47 |
| 3.5.2 | Further generator models and verification <small>2023-09-16 12:54:13+02:00</small> | 47 |
| 3.6 | Experimental comparisons <small>2023-09-16 12:54:13+02:00</small> | 48 |
| 3.7 | Conclusion <small>2023-09-16 12:54:13+02:00</small> | 48 |

3.1 Summary 2023-09-16 12:54:23+02:00

This chapter presents the work carried out concerning the modeling and simulation of integrated circuits and platforms in a body biasing fault injection context. The presented work focused on elaborating electrical models allowing to evaluate with simulations the behaviors of ICs subjected to BBI. The chapter introduces the elaborated models and the algorithms used to create them, and then goes on to present various validation steps to check the meaningfulness of the models. Parts of this work have been published both in [2] and [24].

3.2 Introduction 2023-09-16 12:54:23+02:00

When evaluating and studying ICs under BBI, it is important to be able to fully predict and understand the underlying mechanisms at work in order to set up reproducible and reliable experiments, as well as being able to set up efficient countermeasures. However, to model and simulate integrated circuit behavior subject to fault injection is not an easy task. Specifically, simulating an entire IC at a transistor level under fault injection is unrealistic with current resources and technology. It is especially true when considering time cost, as current digital ICs are composed of about a million of transistors for standard microcontrollers. Furthermore, no software nor algorithm is currently dedicated to simulate the functional, electrical behavior of millions of transistors at the same time while some of them are disrupted by strong and transient disturbances. In addition to that, to be able to set up a reliable model, one should have access to the detailed architecture of each considered IC, which is almost never the case, as most studied architectures are proprietary. Therefore, it is required to find alternative workarounds in order to be able to study IC behavior and their various responses to fault injection techniques.

This has been first proposed in 2019 concerning Electromagnetic Fault Injection (EMFI) [28], and further extended in 2021 [20]. Especially in the latest work [20], the proposed solution consisted in establishing an equivalent non-logical model of the section of an IC. Instead of modeling each logic gate with as many transistors as required, in addition to the power delivery network and the silicon substrate, it was chosen to represent a hundred of logic gates in an average way, solely with a few resistors and capacitors. This results in a transistor-less model, achieved using manufacturing data for the studied IC. The authors assumed that the first half of the transistors are conducting while the other half are blocking. Then, two levels of power delivery network were added, simply modeled with electrical resistances. Eventually, and because the modeled IC was manufactured using a dual-well substrate type, the silicon substrate and the P-N junction respectively are modeled by six resistors going in every direction in addition to a diode and its capacitance respectively. This clever design allows to drastically reduce the computing work required to analyze and predict behaviors of ICs subject to EMFI. Indeed, simulating the average behavior of a hundred of logic gates only with four resistors and four capacitors is immensely lighter than simulating the equivalent with BSIM (Berkeley

Short-channel IGFET Model) transistors. However, the main shortcoming being the lack of functionality with the produced ICs, it is therefore impossible to evaluate their functional or logical behavior.

Body biasing injection being less documented than EMFI, no distributed model has yet been proposed to simulate ICs under BBI. In this context, our motivations were to set up and evaluate electrical models being able to reliably predict both in time and space IC behavior in order to understand how BBI induced disturbances propagate and create faults inside ICs. The current work main goal being to model and simulate BBI similarly to EMFI, we decided to start from the model proposed in [20], to improve and adapt it in order to be able to implement it in a BBI context.

This chapter begins with a general presentation of the enhanced models, followed by a closer look at each model and its specific features. Eventually, various model validation are studied in order to verify their soundness.

3.3 Electrical models 2023-09-16 12:54:23+02:00

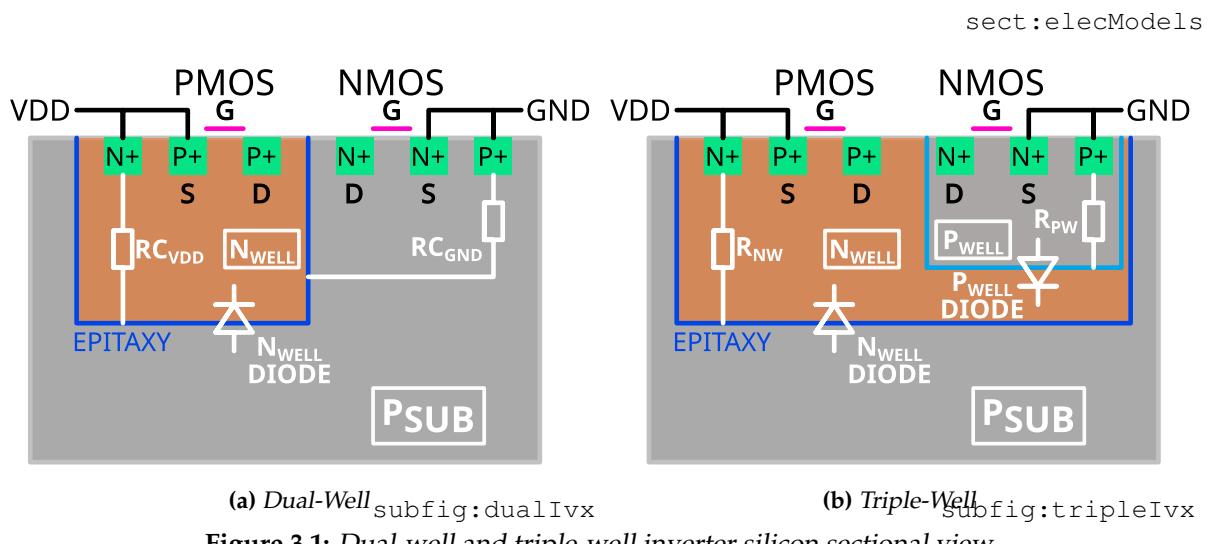


Figure 3.1: Dual-well and triple-well inverter silicon sectional view

On one hand, when performing EMFI (usually on the front side of the IC), air is the physical support to convey energy through electromagnetic waves. It is achieved by coupling the loop wire probe to the power delivery network loops. On the other hand, when working with BBI, the context is different. Indeed, the energy is conveyed through electrical charges through the silicon substrate. Therefore, the carriers have to go through the metallic probe and the whole substrate to reach the logic gates and the power delivery network in order to disturb the IC operation. Thus, the substrate type and design could have a significant impact on BBI efficiency. As a result, we explored and studied BBI in two specific scenarios depending on the substrate types: dual-well and triple-well. Fig. 3.1 shows the sectional views of two inverters manufactured in a dual-well and a triple-well substrate respectively. These simple schematics are helpful in understanding the reasoning behind the design of the electrical models.

Fig. 3.1a depicts the cross-sectional view of a dual-well CMOS inverter. The P-doped silicon substrate is colored in gray, with RC_{GND} being the access resistance from the epitaxy layer to the NMOS bulk. This physical environment is the conducting support of electrical charges which flow up to the NMOS transistor. The orange region is the N-doped silicon well, located inside the P-substrate to manufacture the PMOS transistors. RC_{VDD} is the access resistance from the epitaxy to the PMOS bulk inside the N_{WELL} . In addition to the P-substrate, the N-well is the last environment electrical charges have to go through before reaching the PMOS transistor.

Fig. 3.1b shows the cross-sectional view of a triple-well CMOS inverter. As before, gray areas represent P-doped silicon, and orange areas N-doped silicon. R_{NW} is the N_{WELL} access resistance from the epitaxy to the PMOS bulk, and R_{PW} is the P_{WELL} access resistance from the $N_{WELL} - P_{WELL}$ junction to the NMOS bulk. In this case, two silicon junctions are present, represented by two independent diodes. In order to reach the PMOS transistors, charges have to go through the exact same environments as before. However, concerning NMOS transistors, they have to pass through two silicon junctions instead of none. As discussed in Chapter 5, this has a significant impact on BBI induced effects. However, these schematics are incomplete and do not allow simulating ICs behaviors under BBI.

Therefore, as it has been done in [20], ICs are spatially split in elementary sections called standard-cells segments (SCS). However, in addition to the improvement of the dual-well proposed model proposed in [20], we also introduce a triple-well model in order to fully appreciate the behavioral differences of BBI applied to both substrate types.

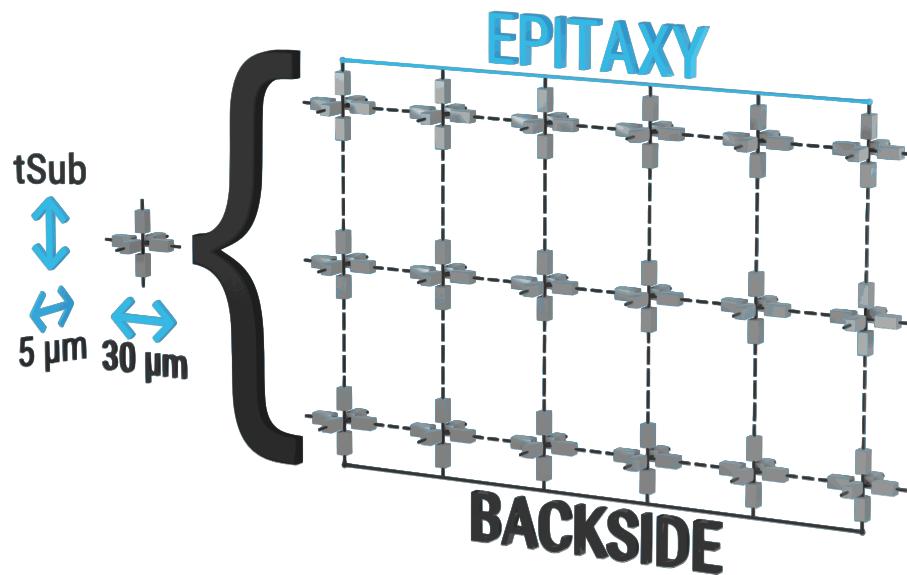
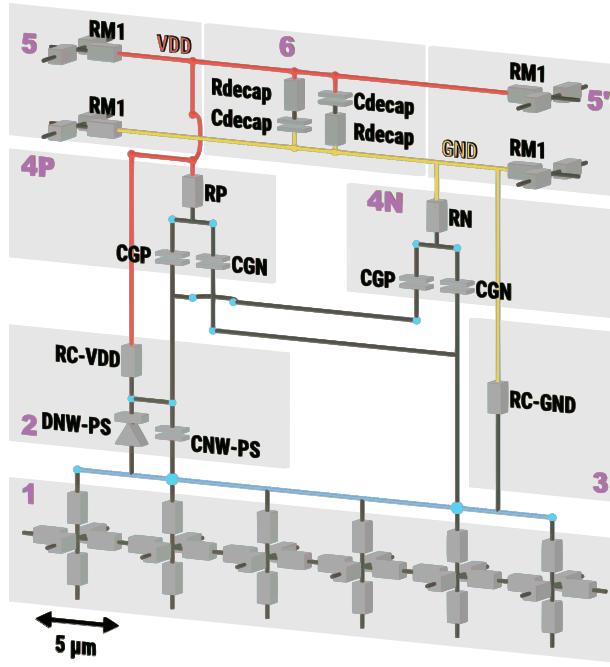
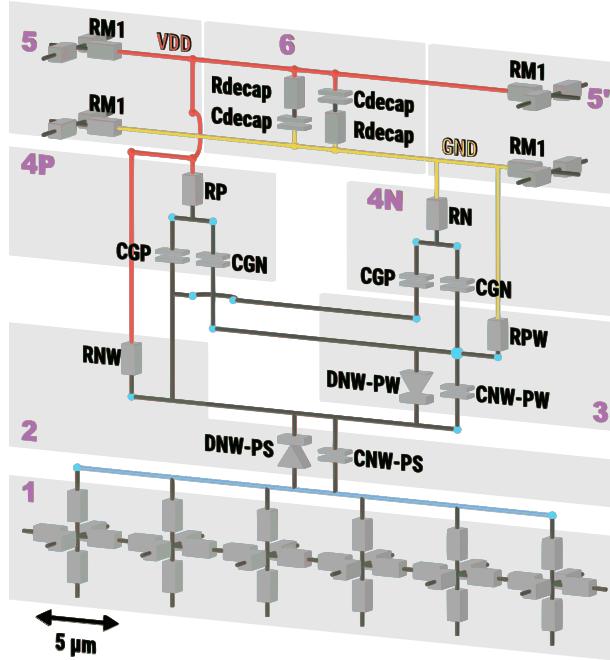


Figure 3.2: Surface subdivision improvement. fig:surfaceSubDivid

The main improvement over the dual-well model proposed in [20] concerns the substrate resistive network, as shown in Fig. 3.2. In [20], the substrate network is coarse and only consists of six electrical resistances for each SCS. It means that they represent the entire SCS substrate thickness, width, and height (on the left in Fig 3.2). Even though it is sufficient to appreciate



(a) Dual-Well subfig:dualScs



(b) Triple-Well subfig:tripleScs

Figure 3.3: Three-dimensional Dual-Well and Triple-Well IC comprehensive standard-cell electrical schematic.

the injection method effects while studying EMFI, mainly because the substrate is almost transparent when it comes to electromagnetic waves, but also because EMFI is mostly performed at the IC front side, it is not precise enough to model the spreading of the voltage pulse from the IC backside to the transistors.

To that end, we decided to split as much as possible these resistors, as shown in Fig. 3.2, to provide a precise enough substrate sub-model while keeping realistic computational workload. For the final models, it was decided to use an editable elementary thickness of $10 \mu\text{m}$, and fixed width and depth of $5 \mu\text{m}$ for each elementary six-resistors substrate models, according to the footprint of an SCS on the XY plane ($5 \mu\text{m} \times (6 \mu\text{m} \times 5 \mu\text{m})$), resulting in a $30 \mu\text{m}$ wide and $5 \mu\text{m}$ deep SCS. One can remark that in Fig 3.3, no number is given concerning the substrate thickness, as similar to LFI, it is an important parameter which does not have a fixed value. Indeed, an attacker may want to thin the substrate or not before performing BBI.

Furthermore, as shown in Fig. 3.3, both SCS models contain various electrical components describing the IC structure, roughly composed of:

- Its substrate
- Its silicon junction(s)
- Its logic gates
- Its power supply rails

These two models, while being close to each other, allow, thanks to their subtle differences, to properly consider the different behaviors each substrate type exhibits. In the next section, dual-well SCS model and triple-well SCS model are consecutively considered and analyzed.

3.3.1 Standard-cell segment models 2023-09-16 12:54:23+02:00

subSect : dualTripleWellScs

Historically, IC substrate was manufactured using an exclusive dual-well structure. However, nowadays, it is common to find on relatively modern ICs a mix of dual-well and triple-well structures on a monolithic die. Triple-well substrate structures bring significant advantages over dual-well substrates. In digital ICs, it is mainly used to body bias transistors to optimize their performance under power constraints. When used in analog or mixed designs, it gives two main advantages: substrate cross-talk and noise reduction, in addition to power supply decoupling thanks to the additional P-N junction capacitance [29]. This is why we decided to cover dual-well and triple-well structures in our models.

Fig. 3.3a depicts an SCS dual-well model. Each significant section of the SCS is gray-framed and numbered:

- The section 1 represents the substrate environment: resistive and isotropic.
- The section 2 is the $P - N$ silicon junction between the P-substrate and the N-well, represented by a diode and its junction capacitance, in addition to an access resistance $RC - VDD$, being the N-well electrical resistance.

- The section [3] is the substrate access resistance.
- The sections [4P] and [4N] contain the average non-logical model of a hundred of logic gates.
- The sections [5] and [5'] are the two levels of the power delivery network, which are low resistive metals.
- The section [6] is the decoupling between both GND and V_{DD} power networks.

Fig. 3.3b depicts the SCS triple-well model as follows:

- The section [2] is the $P - N$ silicon junction between the P-substrate and the N-well, represented by a diode and its junction capacitance, in addition to an access resistance R_{NW} , being the N-well electrical resistance.
- The section [3] is the $N - P$ silicon junction between the N-well and the P-well, represented once again by a diode and its junction capacitance, in addition to an access resistance R_{PW} , being the P-well electrical resistance.
- The sections [1], [4P], [4N], [5'] and [6] being the same as before.

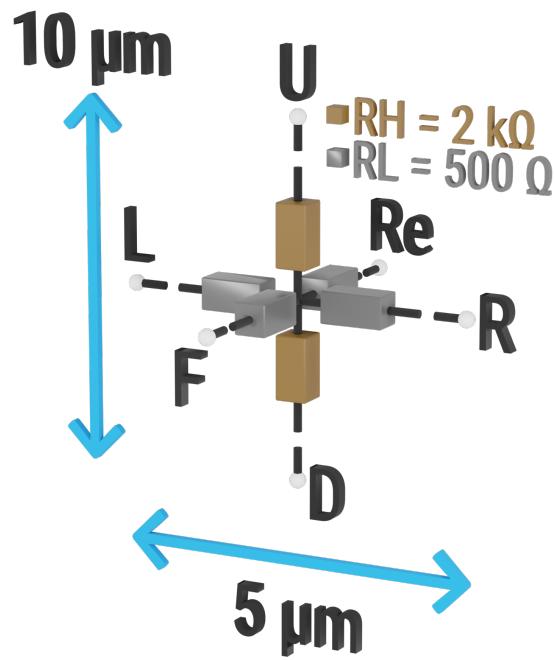


Figure 3.4: Elementary substrate 3D netlist

fig:algo

Each area of the elementary SCS models were automatically generated using a custom algorithm, shown in Alg. 1. It was mainly designed in order to reduce as much as possible any human intervention to limit difficult to debug errors and inconsistencies. Furthermore, it provides a degree of flexibility due to the ease of user modifications directly into the generation

```
.subckt elementary_bloc D F L R Re U
R1 U N001 RH
R2 N001 D RH
R3 Re N001 RL
R4 N001 F RL
R5 N001 L RL
R6 R N001 RL
.ends elementary_bloc
```

Figure 3.5: Elementary substrate SPICE netlist fig:subSpiceNetlist

```
.subckt elementary_blocx6 D1 D2 D3 D4 D5 D6
+F1 F2 F3 F4 F5 F6 L R RE1 RE2 RE3 RE4 RE5 RE6
+U1 U2 U3 U4 U5 U6 VSUBCintC
XX1 D1 F1 L VSUBCintL2 RE1 U1 elementary_bloc
XX2 D2 F2 VSUBCintL2 VSUBCintL1 RE2 U2 elementary_bloc
XX3 D3 F3 VSUBCintL1 VSUBCintC RE3 U3 elementary_bloc
XX4 D4 F4 VSUBCintC VSUBCintR1 RE4 U4 elementary_bloc
XX5 D5 F5 VSUBCintR1 VSUBCintR2 RE5 U5 elementary_bloc
XX6 D6 F6 VSUBCintR2 R RE6 U6 elementary_bloc
.ends elementary_blocx6
```

Figure 3.6: SCS substrate layer SPICE netlist fig:subSpiceSCS

algorithm parameters, as opposed to netlist editing, thereby reducing errors further. These models only represent a section of an integrated circuit. For effective use and verification, it is necessary to replicate and interconnect these models spatially as much as possible. This was accomplished by utilizing customized Python scripts coupled with procedural generation. The IC generation algorithm enables the modification of multiple settings to produce the desired outcomes, albeit with certain inherent structural limitations. Two of the main limitations are the fixed width and depth of the elementary SCS models, and the fixed number of metal levels in the power delivery network. On the contrary, the following is a non-exhaustive list of user-modifiable settings:

- Global IC size.
- Probe position.
- IC global substrate thickness.
- IC elementary substrate thickness.
- Substrate type (dual-well, triple-well, or mixed).
- Voltage pulse amplitude.
- Voltage pulse width.

- Voltage pulse rise and fall times.
- Simulation time and step.

Eventually, the generator script incorporates a visual inspection tool in order to quickly verify the correctness of the generated netlist. Alg. 1 shows the IC generation algorithm main function, which is to create the coordinates for every net in the netlist.

3.4 Preliminary model validation 2023-09-16 12:54:23+02:00

Because validating such models is a complex task, we chose to trim validation into elementary steps. As these models aim at modeling and report back average IC behaviors, it is required to verify their soundness in trivial scenarios. Specifically, two class of measurements are going to be discussed in this section:

- Global quiescent leakage current evaluation
- Quiescent power network IR drop verification

These are important parameters to verify before going any further because any inconsistent or unrealistic value would result in meaningless models and simulations.

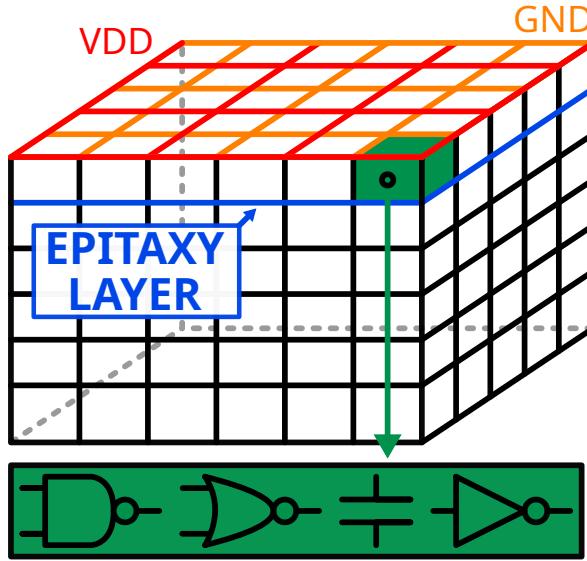


Figure 3.7: Three-dimensional standard-cell segments interconnection example

To that end, we decided, as stated previously, to create an IC composed of several SCS. Fig. 3.7 depicts in a general way how the various SCS required are spatially connected to each other. In blue is indicated the epitaxy layer, which is the junction between the highest substrate level and the top of the SCS. All SCS share the power delivery network at their top and the silicon substrate at their bottom. As mentioned earlier, each SCS represent the average behavior of

about a hundred of logic gates. The resulting IC measurements are the following: a width of $550 \mu\text{m}$, a depth of $450 \mu\text{m}$, and a thickness of $140 \mu\text{m}$. First, we will present the global leakage current, then, we will analyze mappings of the simulated ICs power distribution networks. Dual-well, triple-well and mixed substrates models are analyzed, and most importantly, the simulated circuits do not include the voltage pulse generator nor any other external component required to work with BBI as what we present here is the first validation step. They are proposed as is, and Table 3.1 presents the operating point results for each substrate type.

Table 3.1: Dual-well, triple-well and mixed substrates SCS operating point.

tab:basicOpPointScs

| Measurement | Description | Dual-well | Triple-well | Mixed substrates |
|-------------|--------------------------|-----------|-------------|------------------|
| I_{GND} | IC global ground current | 1.92 nA | 1.94 nA | 3.4 nA |
| I_{VDD} | IC global VDD current | -1.96 nA | -5.8 nA | -3.5 nA |
| GND_{AVG} | Average GND voltage | 1 nV | 1 nV | 1.75 nV |
| VDD_{AVG} | Average VDD Voltage | 1.2 V | 1.2 V | 1.2 V |

Looking at Table 3.1 indicates the absence of any significant leakage current and power supply voltage drop. However, to check the models relevance further and in a more reliable way, it is interesting to look at voltage mappings of the power delivery networks (VDD and GND), as shown in Fig. 3.8.

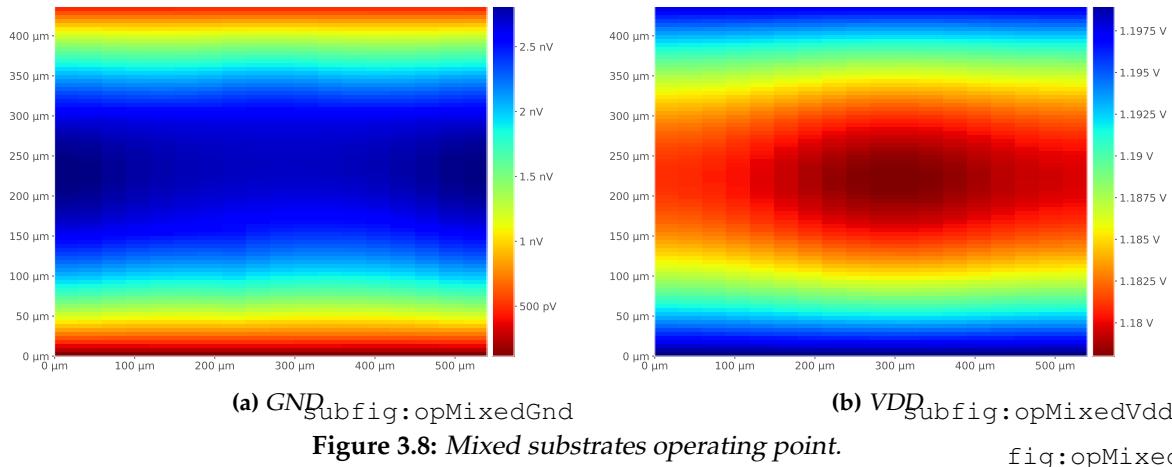


Figure 3.8: Mixed substrates operating point.

fig:opMixed

Concerning both GND and VDD operating point maps, there is no significant voltage drop across both maps, which indicates further the absence of significant leakage current in the simulated IC. With this in mind, we then introduced the generator into the model.

3.5 Voltage pulse generator model and further validation 2023-09-16 12:54:23+02:00

section:genModel

Introducing the generator did not come without major problems. Indeed, the latter inevitably interacts with the target IC, and depending on the real generator output stage architecture, this interaction can drastically vary from one to another.

For example, when using ESD guns as in [30, 31], their output stages are usually AC-coupled, while on our works, we mostly use DC-coupled generators. These subtle differences in practice become major issues in simulation when not treated correctly. Indeed, even considering the transmission line as it has been recommended in Chapter ??, most DC-coupled high voltage generators use a high-impedance mode to disconnect the load from the generator before and after the generated pulses. Therefore, one has to consider this specific aspect when designing a proper BBI electrical model, as we will explain in this section.

3.5.1 Early generator models 2023-09-16 12:54:23+02:00

subsection:earlyGenModel

The first models consisted in a PWL voltage source directly connected to the substrate of the IC, and we quickly observed abnormal operating point values. **Je dois rajouter des valeurs chiffrées.** Indeed, in this setup, at rest, the generator is equivalent a DC voltage source applying 0 V to the backside of the simulated IC. Therefore, it applies an undesired bias to the substrate and thus changes the operating point, inducing a high amount of charges flowing between power sources, thus disturbing the power delivery network. To circumvent this issue, we chose to mimic the behavior of an actual high voltage pulse generator and to switch between a high impedance mode and a voltage pulse mode as a function of the pulse time. This allowed to observe correct operating points with the generator connected, as it is the case in a real experiment. **Je rajouterais les figures.**

3.5.2 Further generator models and verification 2023-09-16 12:54:23+02:00

subsection:furtherGenModel

Because the previously explained generator model is electrically perfect and does not include any impedance mismatching effects, we extended the model to include the generator output impedance and the transmission line. **Peut-être faire un schéma ?** It allowed us to observe impedance mismatch effects, which are of great importance when performing BBI (Chapter ??), as the injected pulses are very fast and of high amplitude. Thus, impedance mismatch greatly changes the effective applied voltage pulse and injected currents, while also modifying unpredictably the induced disturbances, as we will observe further in this manuscript.

In order to verify more thoroughly the soundness of the proposed models, a circuit under BBI is simulated in order to analyze the current distribution and amplitude, specifically at the peak of the voltage pulse. Fig. 3.9 presents the results for both dual-well and triple-well ICs. The substrate being a resistive environment, it is natural to observe isotropic hemispheric current distributions. However, it is interesting to notice that the results show a lower amount of current concerning the triple-well IC compared to the dual-well one. It can be explained thanks to the coupling between the probe/substrate and the logic gates. On one hand, as shown in Fig. 3.1, in the dual-well IC, the charges do not have to cross any silicon junction in order to reach the NMOS transistors, while there is one junction between the probe and the

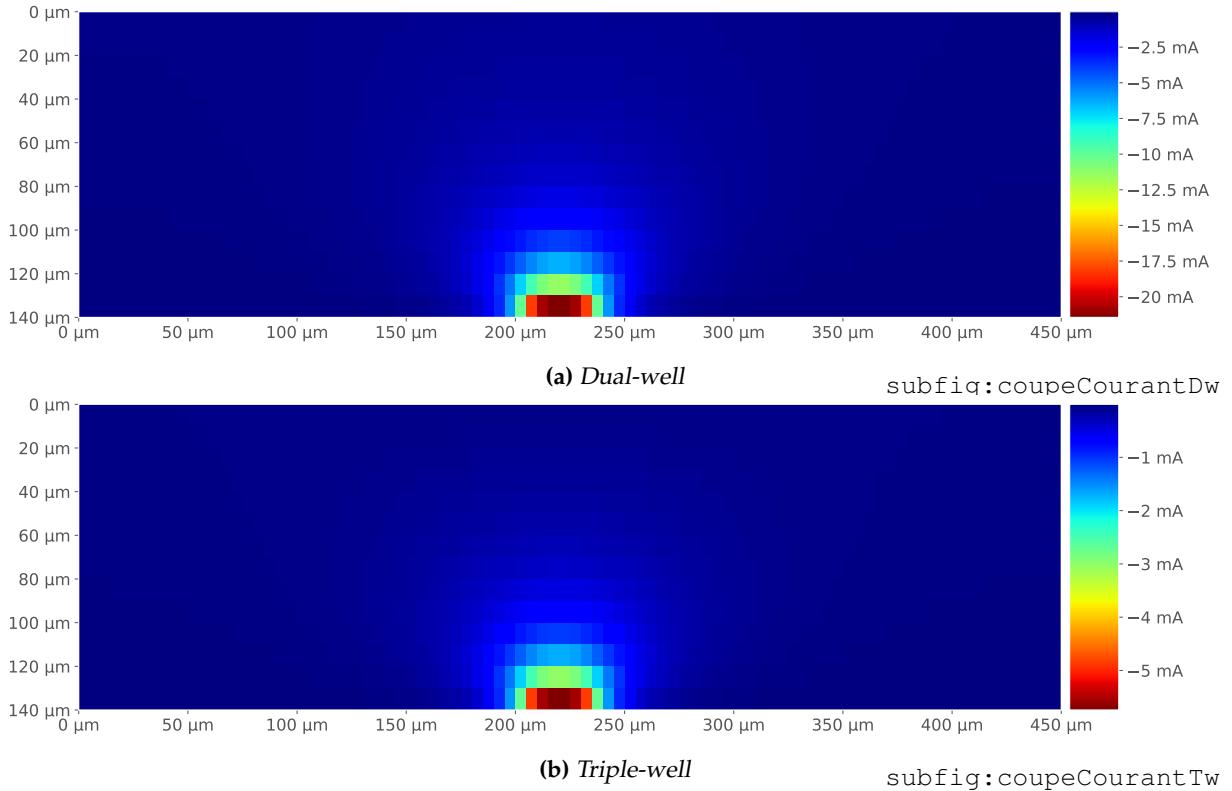


Figure 3.9: Dual-well and triple-well cross-sectional current distribution view at the apex of the voltage pulse
 subfig:coupeCourantDw
 subfig:coupeCourantTw

PMOS transistors. On the other hand, concerning the triple-well IC, there is always at least one silicon junction to cross in order to reach the transistors. Because of this, and because the voltage pulse will inevitably bias the diode, it will change the coupling whether the diode is conducting or blocking. When the diode is conducting, the transistors are DC-coupled to the probe, whereas when the diode is blocking, the transistors are AC-coupled. In the second case, it means that charges can flow only on the edge of the pulse. Thus, during the pulse's plateau, there is no charge flow.

3.6 Experimental comparisons 2023-09-16 12:54:23+02:00

CREUSER PLUS EN DÉTAILS DANS LES SECTIONS PRÉCÉDENTES LES DIFFÉRENCES DUAL/TRIPLE, PARCE QUE C'EST IMPORTANT DANS LE MODÈLE ! In order to complete this chapter, we are going to analyze, in this last section, experimental results highlighting the differences between dual-well and triple-well substrates.

3.7 Conclusion 2023-09-16 12:54:23+02:00

In this chapter, we presented enhanced electrical models which can be utilized to simulate integrated circuits under body biasing fault injection. These models, supported by older ones

originally designed for ICs under EMFI, cover two substrate types commonly found in commercial ICs: dual-well and triple-well substrates. The substrate type is of great importance when considering BBI as it is the only physical environment where charges can circulate. Each sub-models contain:

- The power delivery network
- The average electrical model of a hundred of logic gates
- The various silicon junctions
- The silicon substrate

Standard-cells segments models representing a portion of an IC, they need to be replicated and connected with each other in order to be meaningful. In addition to this, they propose refined substrate sub-models in order to improve the model spatial accuracy over their predecessors. The main advantage of these models is their relative lightness, computationally speaking. Indeed, they are only composed of passives components, in order to be able to simulate large resulting ICs. However, their main advantage is also their main shortcoming, they do not represent any function of the modeled IC, but its average electrical behavior.

Algorithm 1 Integrated circuit SPICE netlist generation algorithm.

Require: SUBTYPE ▷ IC substrate type: Dual-well, Triple-well, Mixed
alg: ieGen

Require: TSUB ▷ IC substrate thickness

Require: ESUB ▷ Elementary substrate block thickness

Require: VPUU ▷ Voltage pulse amplitude

Require: PW ▷ Voltage pulse width

Require: TFR ▷ Voltage pulse rise and fall times

Require: SIMTIME ▷ Simulation duration

Require: SIMSTEP ▷ Simulation time step

Require: TEX ▷ Desired X size (μm)

Require: TEY ▷ Desired Y size (μm)

Require: prbX ▷ BBI probe X coordinate

Require: prbY ▷ BBI probe Y coordinate

$RH \leftarrow 2000$ ▷ Elementary substrate up-down/front-rear resistor value

$RL \leftarrow 500$ ▷ Elementary substrate left-right resistor value

$WSEG \leftarrow 30$

$HSEG \leftarrow 5$

$W6SEG \leftarrow 30 \div 6$

$nC \leftarrow TEX \div WSEG$ ▷ Number of column

$nL \leftarrow TEY \div HSEG$ ▷ Number of lines

$nH \leftarrow TSUB \div ESUB$ ▷ Number of substrate layers

Ensure: nC, nL and nH are integers

var SCS[nL, nH] ▷ Array containing each standard-cell properties

$RH \leftarrow RH \times (ESUB \div 10)$ ▷ Adjust RH value according to user defined variable

$RL \leftarrow RL \times (ESUB \div 10)$ ▷ Adjust RL value according to user defined variable

for all cY in $\llbracket 0 ; nL \rrbracket$ **do**

for all cX in $\llbracket 0 ; nH \rrbracket$ **do**

$\vec{X} \leftarrow \begin{bmatrix} cX \times WSEG \\ cX \times WSEG + 1 \times (W6SEG \div 2) \\ cX \times WSEG + 3 \times (W6SEG \div 2) \\ cX \times WSEG + 5 \times (W6SEG \div 2) \\ cX \times WSEG + 7 \times (W6SEG \div 2) \\ cX \times WSEG + 9 \times (W6SEG \div 2) \\ cX \times WSEG + 11 \times (W6SEG \div 2) \\ cX \times WSEG + 12 \times (W6SEG \div 2) \end{bmatrix}; \vec{Y} \leftarrow \begin{bmatrix} cY \times HSEG \\ (cY + \frac{1}{2}) \times HSEG \\ (cY + 1) \times HSEG \end{bmatrix}$

if $\vec{Y}[0] = 0 \vee \vec{Y}[0] = TEY$ **then** ▷ Determines if SCS has external power

SCS[cY, cX].power = True

else

SCS[cY, cX].power = False

end if

if $\vec{X}[0] = prbX \wedge \vec{X}[2] = prbX \wedge \vec{Y}[0] \leqslant (prbY + 15) \wedge \vec{Y}[0] \geqslant (prbY - 15)$ **then**

SCS[cY, cX].probe = True

else

SCS[cY, cX].probe = False

end if

end for

end for

IV

Substrate thinning analysis 2023-09-16 12:54:23+02:00

chap:4thinning

Contents

| | | |
|-------|--|----|
| 4.1 | Summary <small>2023-09-16 12:54:13+02:00</small> | 52 |
| 4.2 | Introduction <small>2023-09-16 12:54:13+02:00</small> | 52 |
| 4.3 | Geometric and electrical modeling <small>2023-09-16 12:54:13+02:00</small> | 53 |
| 4.3.1 | Geometric modeling <small>2023-09-16 12:54:13+02:00</small> | 53 |
| 4.3.2 | Electrical approach <small>2023-09-16 12:54:13+02:00</small> | 56 |
| 4.4 | Models validation <small>2023-09-16 12:54:13+02:00</small> | 58 |
| 4.4.1 | IC substrate thinning quick look <small>2023-09-16 12:54:13+02:00</small> | 58 |
| 4.4.2 | Experiments with thinned circuits <small>2023-09-16 12:54:13+02:00</small> | 59 |
| 4.5 | Conclusion <small>2023-09-16 12:54:13+02:00</small> | 60 |

4.1 Summary 2023-09-16 12:54:23+02:00

This chapter proposes to study the interests of thinning the substrate of integrated circuits with the aim to enhance Body Biasing Injection efficiency. First, we are going to present a geometrical approach in order to appreciate with a certain abstraction from electronics the effects of substrate thinning on ICs behaviors. Second, thanks to the models presented in Chapter 3, in addition to the geometrical approach, we are going to theoretically analyze the effects of substrate thinning from an electrical point of view. Eventually, in order to verify the soundness of the geometric approach and the simulation results, experiments are going to be studied thanks to an actual analysis of substrate thinning on identical IC targets behavior.

4.2 Introduction 2023-09-16 12:54:23+02:00

When working with integrated circuits in a fault injection context, several physical parameters of the considered IC are of great importance. For example, as we have seen in the previous Chapter, the type of substrate used to manufacture the IC has a significant impact on BBI efficiency and behavior. In addition to this, the transistors' size, power supply voltage, the IC package or the IC substrate thickness can drastically change fault injections results. Among these examples, one of great interest for body biasing injection is the substrate thickness.

Indeed, as there are different manufacturing processes depending on the purpose of each manufactured IC, it is common to find various substrate thicknesses depending on the IC targeted application. On one hand, it is not rare to find 700 μm thick wafers with 300 mm diameters for generic applications. On the other hand, in other specific applications like SoCs, where vertical stacking is commonly used, or in Smart-cards and ID cards, the typical substrate thickness value is lower, around 200 μm . In addition to these differences one can find in commercial products, the practice of thinning the substrate of ICs is not uncommon in a context of fault injection. More specifically, substrate thinning has been thoroughly studied concerning Laser Fault Injection (LFI) [32, 33], and has proven to greatly enhance LFI efficiency, in addition to drastically reducing the power required to create faults. However, it had not been studied for Body Biasing Injection at the beginning of this work.

In this context, this work was first done in order to assess whether substrate thinning has similar effects on BBI as it has on LFI. Second, because thin ICs commonly found in smart-cards have unavoidable security constraints, third because BBI is performed using the silicon substrate as the physical environment to carry energy through electrical charges. Therefore, this Chapter will evaluate the interests of substrate thinning on BBI efficiency. In other words, we will analyze the electrical and behavioral differences between identical ICs with different substrate thicknesses. This analysis will take place using multiple approaches. In the first place, we will address the question using a geometric approach to appreciate the effects of substrate

thinning on voltage propagation inside the substrate while taking a step back from electrical modeling. Then, the geometric approach will be completed with an electrical simulation analysis of two identical ICs with different substrate thicknesses, created thanks to the models proposed in Chapter 3. Eventually, experimental results will be analyzed in order to verify the correctness of the previous approaches, in addition to studying the actual effects of substrate thinning concerning faults creation.

4.3 Geometric and electrical modeling 2023-09-16 12:54:23+02:00

chap4 : sect : geomModel

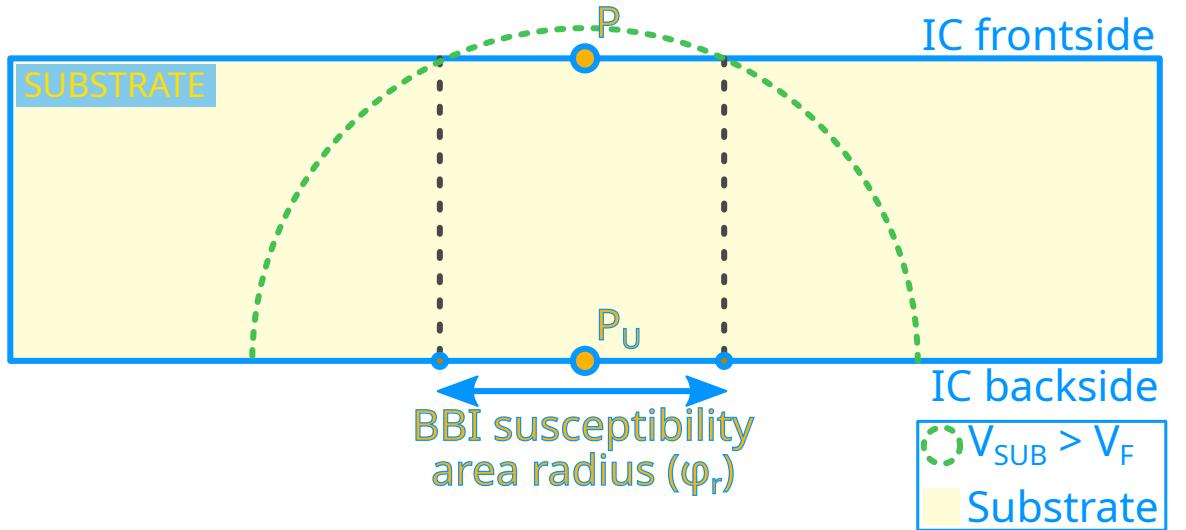
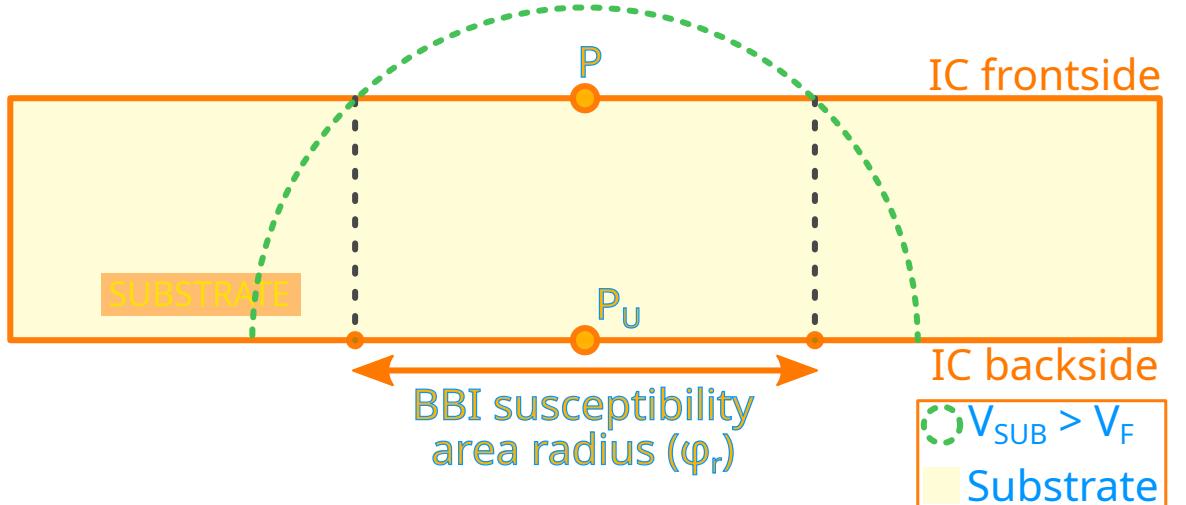
To begin with, we will address the geometric approach. It has been chosen thanks to the advantages it brings forward, such as the abstraction from electronics it enables, thus allowing easier and faster modeling. However, because this approach alone is insufficient, we will then study an analogous electrical one.

4.3.1 Geometric modeling 2023-09-16 12:54:23+02:00

chap4 : sect : geomModel : subsect : geomModel

For the purpose of geometric modeling, let us consider two identical ICs. A commercial one, with an arbitrary standard substrate thickness, and another one with its substrate thinned by a certain amount in order to perform fault injection. Fig. 4.1 illustrates the two-dimensional cross-sectional views of the considered ICs substrates during an arbitrary BBI voltage pulse. The silicon substrate being an isotropic resistive environment, it is quite natural to expect the electrical charges to flow and spread evenly when injected into it at any given time. Therefore, equipotentials form half-sphere surfaces inside the substrate volume. These surfaces are highlighted in two-dimensions as green half-circles in Fig. 4.1.

In this scenario, an attacker wants to induce a fault in the logic gates, located at the top of each IC. To that end, they need to change the voltage enough at point P , called V_P , in order to disturb the transistors and change the logic gates behavior. In addition to that, and for the sake of simplicity, let us assume that P is the only location in the considered IC where faults can be injected. However, in order to observe faults at point P , V_P needs to reach a minimal threshold voltage, called V_F . Because the attacker is working with BBI, a metallic probe is connected onto the backside of the IC, at point P_U , in order to inject energy into the IC. Depending on the amount of injected energy, in other words, the maximum amplitude of the voltage pulse because the substrate effective resistance is static, the voltage at P might never reach V_F , therefore, no faults will be observed. Let us consider that the attacker chose an amplitude V_{PU} big enough such that at a moment in the injection, V_P reaches V_F or more in each considered IC. In that scenario, the area on the IC front side where $V > V_F$ is a disk of radius ϕ , centered in P , called the BBI susceptibility area radius. It means that the attacker can position the probe anywhere on the backside within this disk to reach V_F at P , and therefore induce a fault at P .

(a) Normal IC_{fig:geomCrossView; subfig:geomThick}(b) Thinned IC_{fig:geomCrossView; subfig:geomThin}**Figure 4.1:** BBI susceptibility area cross-sectional 2D view_{fig:geomCrossView}

The half-sphere equipotential radius relative to time can be determined thanks to the following formula:

$$r(t) = \frac{\rho_{SUB}}{\sqrt{2}} \cdot \frac{|I_G(t)|}{|V_{PU}(t) + V_F|} \quad (4.1)$$

with ρ_{SUB} the resistivity of the silicon substrate, $I_G(t)$ the instantaneous sum of the current distribution contained in the half-sphere, and $V_{PU}(t)$ the instantaneous voltage pulse applied on the backside of the IC. Then, logically, the BBI susceptibility area radius, denoted ϕ_r , is described by:

$$\phi_r(t) = 2 \cdot \sqrt{r(t)^2 - t_{SUB}^2} \quad (4.2)$$

with t_{SUB} being the IC substrate thickness.

As it is illustrated in Fig. 4.1, thinning the substrate inevitably increases the size of the susceptibility area if the experimental conditions are constant. It means that the susceptibility

evolution ratio is always greater than 1 when thinning the substrate:

$$\frac{\phi_r^{THIN}}{\phi_r^{THICK}} = \sqrt{\frac{r^2 - t_{THIN}^2}{r^2 - t_{THICK}^2}} > 1 \quad (4.3)$$

Therefore, in order to obtain the same susceptibility area with a thinner IC, it is required to reduce the voltage pulse amplitude, thanks to the following relation:

$$V_{PU}^* = \frac{t_{THIN}}{t_{THICK}} \cdot V_{PU} + V_F \cdot \left(1 - \frac{d_{gapA} \cdot \text{sect : geomModel : eqnVpu*}}{t_{THICK}}\right) \quad (4.4)$$

Eventually, this geometrical approach allows deducing three conclusions:

1. Thinning the substrate allows reducing the minimal voltage pulse amplitude required to induce a fault while keeping a constant susceptibility area.
2. The BBI susceptibility area increases while the substrate thickness decreases while working at a constant voltage pulse V_{PU} .
3. Thinning the substrate alone does not have an influence on BBI spatial resolution, as the susceptibility area depends on the couple (t_{SUB}, V_{PU}) . Thus, similar spatial resolution could be obtained with different substrate thicknesses by changing V_{PU} .

4.3.2 Electrical approach 2023-09-16 12:54:23+02:00

chap4:sect:geomModel:subsect:elecApproach

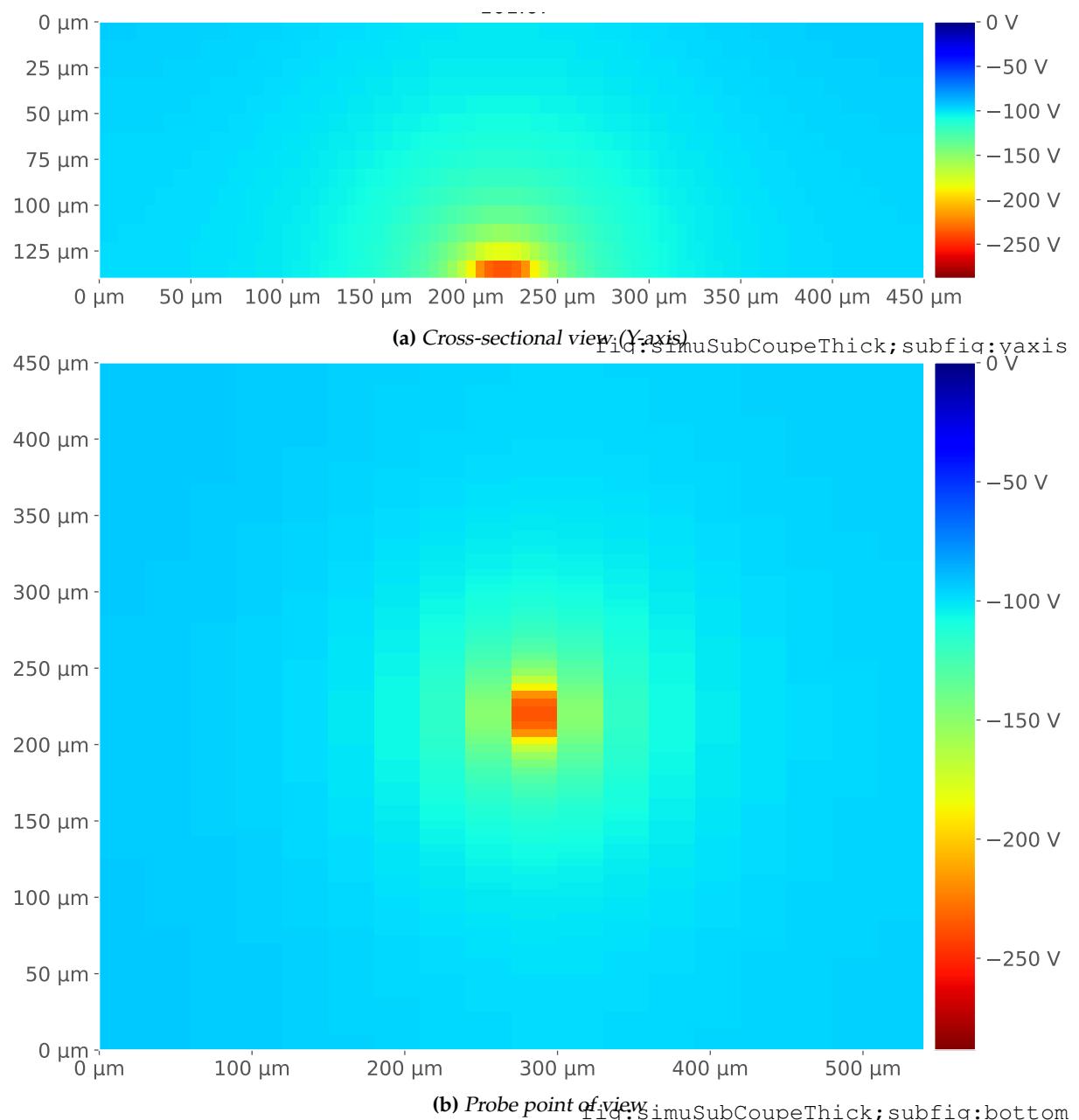


Figure 4.2: Simulated non-thinned IC (140 μm) substrate voltage distribution: peak of the first voltage pulse edge
fig:simuSubCoupeThick

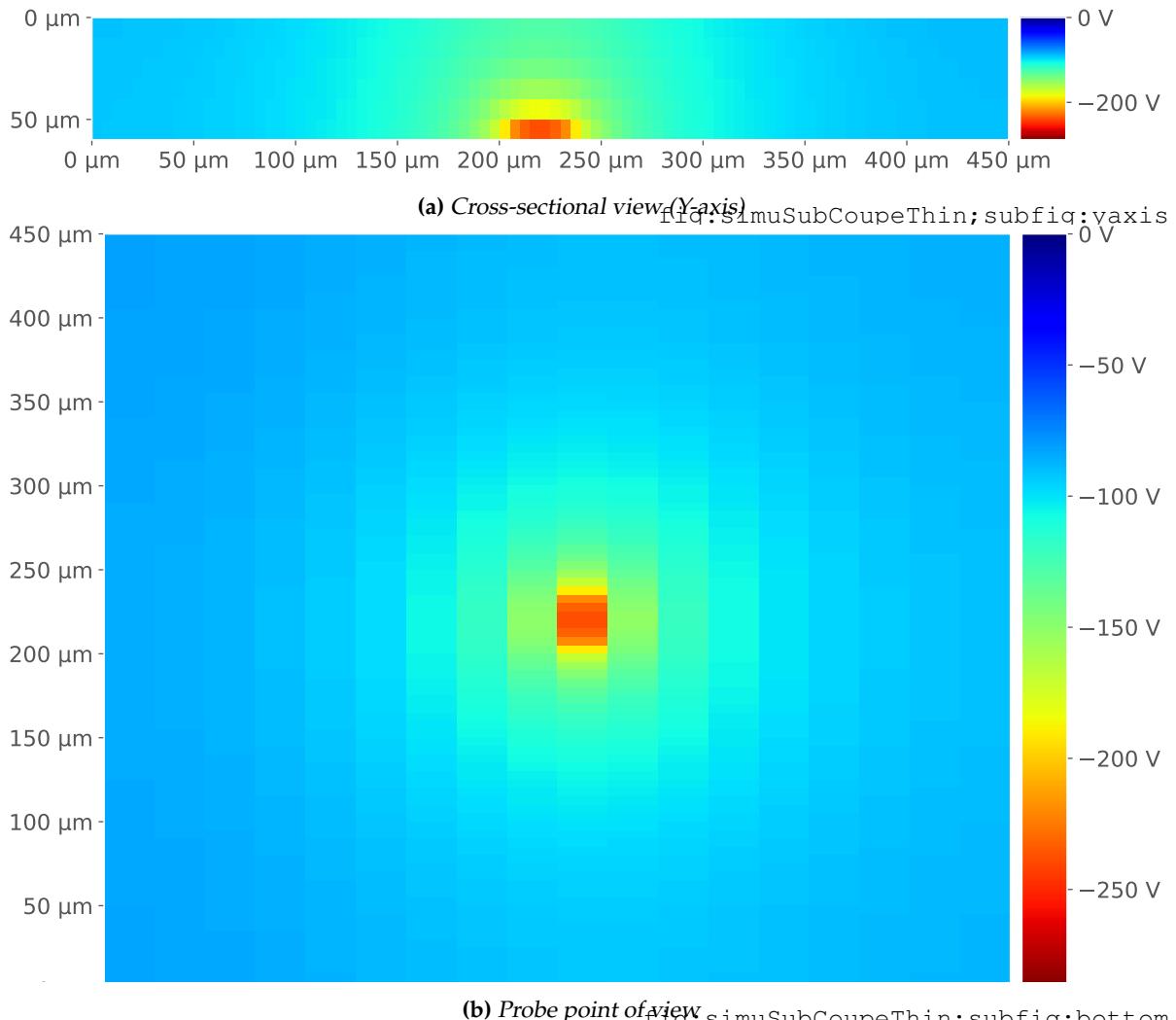


Figure 4.3: Simulated thinned IC (60 μm) substrate voltage distribution: peak of the first voltage pulse edge
 fig: simuSubCoupeThin

As stated previously, in order to verify the meaningfulness of the geometrical approach, we will complete it with an electrical modeling approach. For this purpose, the models introduced in Chapter 3 are reused. The electrical approach consists in generating ICs with different substrate thicknesses and simulating them during BBI. The considered ICs are 550 μm wide and 450 μm deep. Two substrate thicknesses are analyzed, 60 μm and 140 μm . The simulation parameters are the following:

- Triple-well substrate
- Required voltage pulse: -300 V
- Required pulse width: 20 ns
- Required rise and fall times: 8 ns

Fig. 4.2 and Fig. 4.3 show, for each simulated IC, the voltage bias across the substrate through different point of view at the apex of the voltage pulse first edge. For simplicity, results

are shown in two dimensions and from two point of views: a cross-sectional view and a bottom view. The first interesting thing to note is that, as predicted thanks to the geometric model and as shown in Fig. 4.2 and 4.3, equipotentials effectively form half-circles into the substrate (half-spheres in 3D). They can be first observed from the bottom, where the voltage is spreading across the backside surface of the IC. Second, in the cross-sectional view, as it was illustrated previously with the geometrical model..... **IL Y A BEAUCOUP DE CHOSES À DIRE MAIS JE MANQUE D'INSPIRATION POUR CETTE PARTIE, JE REVIENDRAI PLUS TARD DESSUS.**

4.4 Models validation 2023-09-16 12:54:23+02:00

chap4:sect:modelValid

This section presents the conducted experiments allowing to validate the previously presented models.

4.4.1 IC substrate thinning quick look 2023-09-16 12:54:23+02:00

chap4:sect:modelValid:subsect:thinQuick

As substrate thinning is quite widespread when performing fault injection, let us have a quick look on how it is performed. Commonly, It is done using Selected Area Preparation (SAP) or Focused Ion Beams (FIB) milling. SAP milling consists in a very precise mechanical milling tool, generally able to remove material with a precision down to a few micrometers. However, it can often lead to uneven surfaces. FIB milling consists in a physical milling which does not imply a mechanical contact with the material to be removed, and allows nanometer-level precision. For that purpose, FIB is commonly used in combination with SAP [34] to produce even substrate surfaces. In addition to substrate thinning, SAP milling machines allow removing the plastic package and eventual internal metallic heat-sinks of ICs prior to substrate thinning. It has the advantage of providing low damage to thinned ICs, thanks to low spindle speed and low temperature rise compared to traditional high speed milling.

4.4.2 Experiments with thinned circuits 2023-09-16 12:54:23+02:00

chap4 : sect : modelValid : subsect : XpThinning

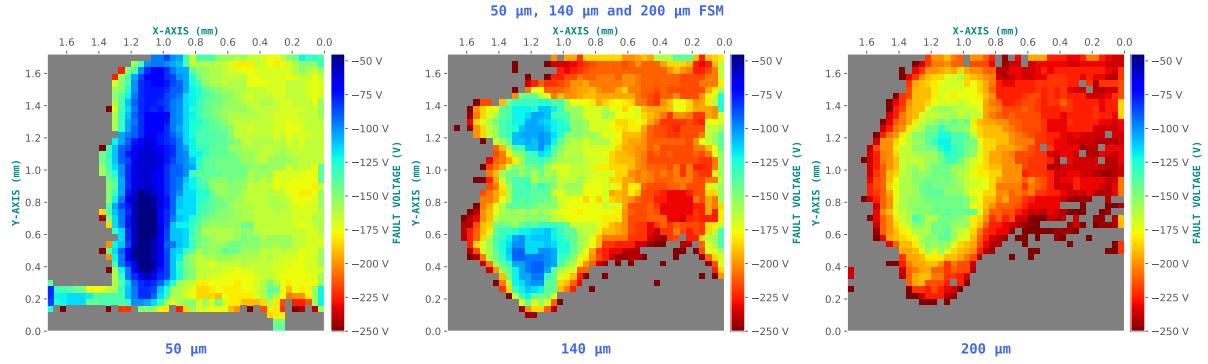


Figure 4.4: Fault susceptibility maps

fig: fsm1

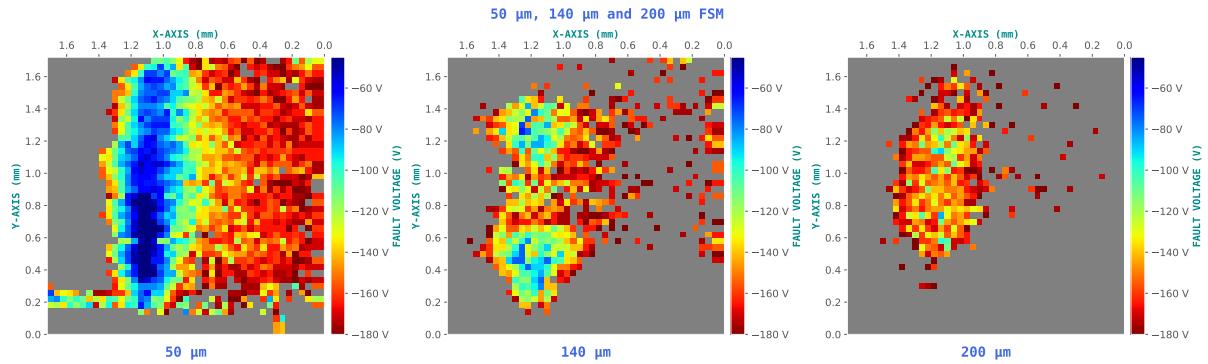


Figure 4.5: Susceptibility area spreading

fig: fsm1spread

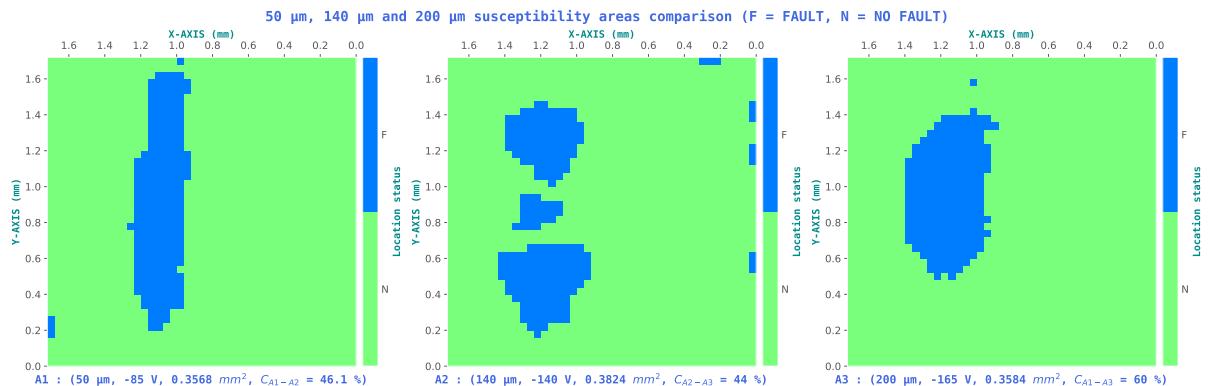


Figure 4.6: Fault susceptibility maps couples

fig: fsm1couple

With geometric and electrical modeling complete, it is now possible to conduct actual experiments in order to verify the meaningfulness of the previous approaches. In this context, three identical targets were thinned to three different levels, from 750 μm to respectively 200 μm , 140 μm and 50 μm , respectively named ST200, ST140 and ST50 for the rest of this Chapter. In order to verify the three conclusions extracted from the modeling section, three experiments are conducted for each target.

The first experiment aims at measuring the minimal voltage pulse amplitude V_{PU}^{MIN} re-

quired to induce a faulty behavior on an IC performing computations. These experiments are called Fault Susceptibility Maps (FSM). They allow spotting the region where the IC is sensitive to BBI, no matter which type of induced fault. Therefore, when mapping an entire IC, it is common to spot various areas not directly involved in the targeted calculation, like the analog voltage regulator or the FLASH memory logic control logic not to cite them all. As a result, and because in a fault injection context the cryptographic core is very often targeted, it was decided to focus the maps above the STM32 AES core only. Fig. 4.4 presents the three performed FSM. From left to right, t_{SUB} goes from 50 μm , then to 140 μm , finally to 200 μm . As stated before, the maps are performed above the hardware AES core of the IC, temporally aiming the penultimate AES round. The scanned area measures 1.7 mm by 1.7 mm, with a displacement step of 40 μm between each point. V_{PU} was limited to the following range: [30 V ; 280 V], with 5 V steps and a negative polarity. The pulse width was fixed at 6 ns. The first important thing to note here is that, as predicted with the geometric and electrical modelings, a thinner substrate allows a lower fault induction threshold. It is mainly shown thanks to the measurement of the average voltage required to induce a fault across the entire map, annotated at the top of each map. All of this sustains the first conclusion made in section 4.3.

Then, the second experiment, whose results are shown in Fig. 4.5, consist in analyzing the spreading of the BBI susceptibility area. The core of the experiment is identical as before. However, in order to highlight the spreading effect, it was required to set a lower maximum voltage amplitude (in absolute value). The value of 180 V was chosen as it is the average voltage of the medium-thinned IC. What is interesting here is that, for the ST200 target, because the voltage at the epitaxy level cannot reach the threshold value V_F in most cases, the fault area is tiny compared to the other targets, and focused on the AES core. Then, concerning the ST140 target, thanks to the thinner substrate, the voltage at the epitaxy level can reach a higher value, and thus can cause more logic gates or further logic gates from the probe to have a faulty behavior. Eventually, the ST50 target shows the largest fault area. These experiments help to sustain the second conclusion of section 4.3.

Eventually, the last experiment consisted in finding, whenever possible, (t_{SUB}, V_{PU}) couples for which the susceptibility area is identical across all targets. The search for the couples of values was done by first choosing an arbitrary couple for ST200 target, and then calculating the correlation for each couple between the other two susceptibility areas and finding the highest correlation. Then, to confront the geometric modeling predictions, we calculated, thanks to equation 4.4, couples corresponding to

4.5 Conclusion 2023-09-16 12:54:23+02:00

This chapter introduced the interest of thinning the substrate of integrated circuits on Body Biasing Injection efficiency. In the first place, we studied thanks to a geometrical approach the potential benefits of this practice, further completed with electrical simulations. The geomet-

ric approach brought mathematical relations allowing to evaluate preliminary the effects of thinning the substrate of a target IC.

À FINIR.

V

Fault model 2023-09-16 12:54:23+02:00

chap:5faultModel

Contents

| | | |
|-------|--|----|
| 5.1 | Summary <small>2023-09-16 12:54:13+02:00</small> | 64 |
| 5.2 | Introduction <small>2023-09-16 12:54:13+02:00</small> | 64 |
| 5.3 | Charge extortion <small>2023-09-16 12:54:13+02:00</small> | 64 |
| 5.3.1 | Sequential logic operation and simple fault model <small>2023-09-16 12:54:13+02:00</small> | 65 |
| 5.4 | Silicon substrate charges propagation <small>2023-09-16 12:54:13+02:00</small> | 65 |
| 5.5 | Logic gates simulation under BBI <small>2023-09-16 12:54:13+02:00</small> | 65 |

5.1 Summary 2023-09-16 12:54:23+02:00

chap5:sect:summary

In this chapter, we present a fault model for BBI, extrapolated from a fault model used for EMFI. The objective of this chapter is to provide an explanation of the mechanisms and causes of faults in integrated circuits that are subjected to body biasing injection. Electrical models presented in the chapter 3 can be used to explain how electrical charge displacement in the IC during a BBI pulse allows changing some logic gates output values. Targeting an IC via BBI forces electric charges to be injected (resp. absorbed) with positive pulses (resp. negative). Therefore, it is possible to target a critical time in the IC calculation thanks to the ability to finely control the induced disturbances. Eventually, to verify the correctness of the proposed analysis, both substrate charge propagation and logic gate behavior studies will be conducted in parallel.

5.2 Introduction 2023-09-16 12:54:23+02:00

chap5:sect:intro

To further complete the understanding of BBI, in addition to having a reliable model to predict IC behavior, it is of great importance of having a precise fault model, in order to be able to set up countermeasures. Indeed, the main objective of studying fault injection techniques is to protect further secured ICs in order to consider during the design of new ICs, the implications and impacts of such countermeasures on the design. As it has been said in Chapter 3, simulating at a transistor level an entire IC is unrealistic, at least computationally speaking. Therefore, and because the previous models do not represent the logical functions of the considered ICs, we propose an additional step to the simulation workflow proposed in Chapter 3. This addition consists in extracting the propagated disturbances from standard-cell segments models, and injecting them into functioning logic gates. This method allows appreciating logic gates behavior under BBI in order to get a deeper and more precise understanding of both electrical and functional fault creation mechanisms. All of this is part of the required steps to set up efficient countermeasures, as we need to understand precisely the insights of fault creation.

5.3 Charge extortion 2023-09-16 12:54:23+02:00

chap5:sect:chargeExtortion

This section explains the charge extortion mechanism at work during BBI which allows fault creation. The voltage pulse generator, at each edge of its pulse, injects and then extorts electrical charges into and out of the IC.

5.3.1 Sequential logic operation and simple fault model 2023-09-16 12:54:23+02:00

chap5:sect:chargeExtortion:subsect:seqLogic

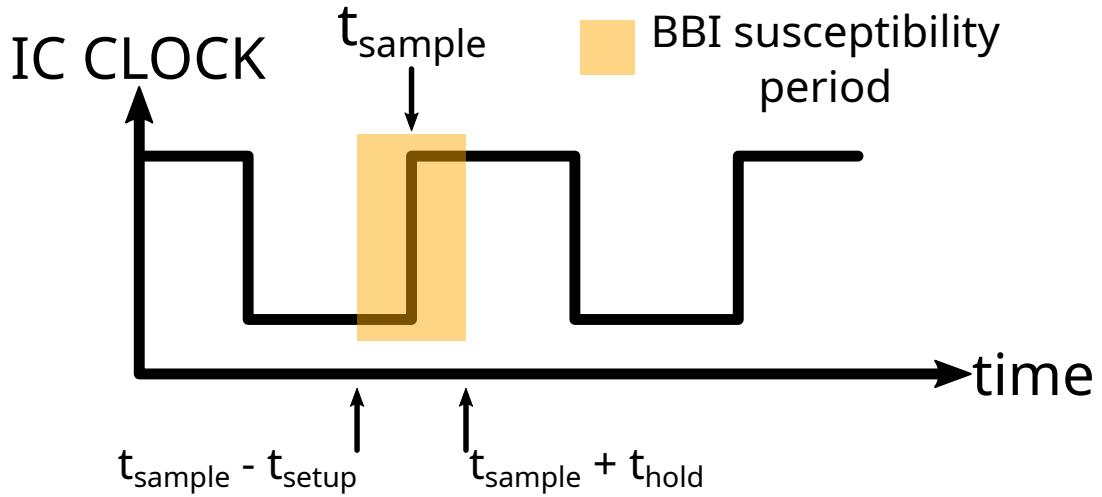


Figure 5.1: Sequential logic operation and BBI sampling fault susceptibility
chap5:fig:bbisusc

As sequential logic is ubiquitous in contemporary integrated circuits, we shall examine its fundamental workings in greater detail. Sequential logic relies on a core element: the edge-triggered D flip-flop (DFF). They are a memory component that is governed by a clock. At each rising-edge or falling-edge (depending on the design) of the clock, DFFs sample their input and replicate it at their output. Between DFFs are placed the logic gates, which fulfill a specific logical function. Because of this, values in sequential logic circuits can only be changed at the clock edges. Hence, in the event that an adversary is able to alter a logical value for an extended period of time at the input of a DFF, the subsequent combinatorial logic will yield an incorrect value, which will propagate to the subsequent DFFs.

We are going to use this fault model, depicted in short in Fig. 5.1, for the rest of this chapter. It is important to note that this model was first introduced for EMFI [35].

5.4 Silicon substrate charges propagation 2023-09-16 12:54:23+02:00

chap5:sect:subEpiCurr

On a déjà montré ces cartes dans des parties précédentes.

5.5 Logic gates simulation under BBI 2023-09-16 12:54:23+02:00

chap5:sect:simuLogic

VI

Conclusion

chap:6conclusion

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