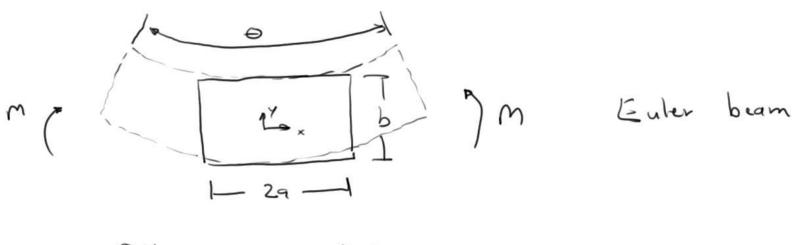
dof 
$$1 \Rightarrow 1, 2$$
  
 $2 \Rightarrow 3, 4$   
 $3 \Rightarrow 5, 6$ 



$$\varepsilon_{xx} = \frac{-\Theta \gamma}{2q}$$
,  $\varepsilon_{yy} = \lambda \frac{\Theta \gamma}{2q}$ ,  $\varepsilon_{xy} = 0$ 

$$m_z$$
 $m_z$ 
 $m_z$ 

Elastic strain energy

M = Me under plane stress [C] > plane stress

$$\frac{\Theta_e}{\Theta} = \frac{1-\frac{1}{2}}{1+\frac{1-\frac{1}{2}}{2}(\frac{9}{2})^2}$$

when the term ( ) is present due to parasitic shear

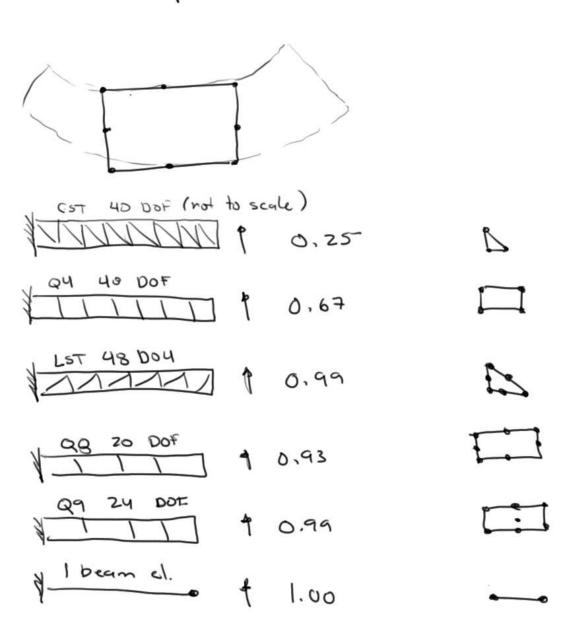
$$\lim_{\frac{a}{b} \to \infty} \frac{1 - 3^2}{1 + \frac{1 - 3}{2} \left(\frac{a}{b}\right)^2} = 0 \qquad \frac{\Theta e}{\Theta} \ge 0 \qquad as \quad \frac{a}{b} \to \infty$$
The mash "locks"

Consider Volumetric strain

Under plain strain conditions, the pressure  $P = \frac{E_{y} \otimes (y-v)}{2g(1+v)(2v-1)}$ 

volumetric locking

For example (Q0)



Define "Full integration" = quadratur rule & sufficient accuracy to exactly integrat all coefficients of ke of the undistorted element

R = Sre BT [C] B J; he dr => O(5. 1/2) for QY 2x2 144

## Under integration

DKA "reduced integration"

- Use a rule that is less than exact
- Reduces computation time
- Can offset parasitic shear
- Introduce a defet i.e. spurious moder, singular moder, zero-energy moder hourglass modes.

