$$\varepsilon_{11}^{Q} = \frac{\sigma_{11}}{E} - \frac{\Im}{E} \left(\frac{\Im}{\sigma_{22}} + \frac{\Im}{\sigma_{83}} \right) = \frac{\Upsilon}{E}$$

$$\varepsilon_{22} = \frac{\Im}{E} \sigma_{11} = -\frac{\Im}{E}$$

$$\mathcal{E}_{33} = \frac{3}{E} \sigma_{11} = -\frac{34}{E}$$

$$\frac{\mathcal{E}^{\rho} = \lambda}{\partial \mathcal{E}^{\rho}} = \frac{\partial f}{\partial \sigma_{ij}}$$

$$\frac{\partial \mathcal{E}^{\rho}}{\partial \mathcal{E}^{\rho}} = \frac{\partial \lambda}{\partial \sigma_{ij}}$$

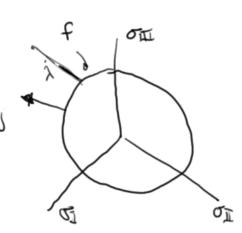
$$\frac{\partial \mathcal{E}^{\rho}}{\partial \sigma_{ij}} = \frac{\partial \lambda}{\partial \sigma_{ij}}$$

$$\frac{\partial \alpha_i^2}{\partial t} = \frac{\partial \alpha_i^2}{\partial t} (25) = 2i$$

$$= 25 - \frac{3}{13} = 0$$

$$= 25 - \frac{3}{13} = 0$$

$$= 25i$$



associated flow rule

$$\frac{\partial f}{\partial f} = \frac{1}{3} \frac{\partial \sigma_{ij}}{\partial f} = \frac{1}{3} \frac{\partial \sigma_{ij}}{\partial f}$$

$$\dot{\varepsilon}^{\rho} = \dot{\lambda} \frac{\partial \dot{\varphi}_{ij}}{\partial \dot{\varphi}_{ij}} = \dot{\lambda} \frac{\dot{S}_{ij}}{\dot{S}_{ij}}$$

$$d\varepsilon^{P_{5}} d\widetilde{\lambda} \begin{bmatrix} \frac{2y}{3} & 0 & 0 \\ 0 & -\frac{y}{3} & 0 \end{bmatrix}$$

$$\varepsilon_{\parallel} = \frac{\gamma}{E} + \varepsilon_{\parallel}^{P} \Rightarrow \varepsilon_{\parallel}^{P} = \varepsilon_{\parallel} - \frac{\gamma}{E}$$

$$\mathcal{E}_{zz} = -\frac{\mathcal{Y}}{\mathcal{E}} Y - \frac{1}{2} \left(\mathcal{E}_{\parallel}^{\rho} \right) = \frac{-\mathcal{Y}}{\mathcal{E}} Y - \frac{1}{2} \left(\mathcal{E}_{\parallel} - \frac{\mathcal{Y}}{\mathcal{E}} \right)$$

like E33

$$f = \sqrt{37_2} - y(\xi^{\beta}) = 0$$

= $\sqrt{37_2} - y - H\xi^{\beta} = 0$

equivalent plastic strain-
$$\xi P = \sqrt{\frac{2}{3}} \xi_{ij}^{p} \xi_{ij}^{p} = \sqrt{\frac{2}{3}} \lambda$$

Flow
$$\Rightarrow$$
 $\dot{\mathcal{E}}_{ij}^{g} = \dot{\lambda} \left(\frac{S_{ij}}{|S_{ij}|} \right)^{Q_{ij}} = \left(\dot{\lambda} Q_{ij} \right)^{Q_{ij}}$

$$\varepsilon_{ij}^{4} = \varepsilon_{ij} - \frac{1}{3} \varepsilon_{kk} \delta_{ij}$$

$$\dot{\varepsilon}_{ij}^{d} = \dot{\varepsilon}_{ij}^{de} + \dot{\varepsilon}_{ij}^{de} \Rightarrow \dot{\varepsilon}_{ij}^{d} - \dot{\varepsilon}_{ij}^{de} - \dot{\varepsilon}_{ij}^{de} = 0$$

$$\dot{\varepsilon}_{ij}^{i} Q_{ij} - \dot{\varepsilon}_{ij}^{de} Q_{ij} - \dot{\varepsilon}_{ij}^{de} Q_{ij} = 0$$

$$\begin{aligned}
\sigma_{ij} &= \lambda \, \mathcal{E}_{ux} \, \delta_{ij} + 2\mu \, \mathcal{E}_{ij} \\
&= \lambda \, \mathcal{E}_{ux} \, \delta_{ij} + 2\mu \left(\mathcal{E}_{ij}^{d} + \frac{1}{3} \mathcal{E}_{ux} \delta_{ij}^{c} \right) \\
&= \lambda \, \mathcal{E}_{ux} \, \delta_{ij} + 2\mu \left(\mathcal{E}_{ij}^{d} + \frac{1}{3} \mathcal{E}_{ux} \delta_{ij}^{c} \right) \\
&= \mathcal{E}_{ij}^{d} + \mathcal{E}_{ux} \, \delta_{ij}^{c} \\
&= \mathcal{E}_{ij}^{d}$$

$$O = \dot{\varepsilon}_{ij}^{i} Q_{ij} - \dot{\varepsilon}_{ij}^{de} Q_{ij} - (\dot{\varepsilon}_{ij}^{de})Q_{ij}$$

$$S_{ij} = 2\mu \dot{\epsilon}_{ij}^{ide} \Rightarrow (\dot{\epsilon}_{ij}^{ide}) = \frac{S_{ij}}{2\mu}$$

$$O = \dot{\varepsilon}_{ij}^{\lambda} O_{ij} - \frac{\dot{S}_{ij}}{Z_{P}} Q_{ij} - \dot{\lambda}$$

$$\dot{\epsilon}_{ij}^{d} Q_{ij} - \frac{\dot{5}}{2\mu} - \dot{\lambda} = 0$$

Kuhn-Tucker constrait eggs. kinematic hardening

$$S = \frac{2}{3} H \lambda$$

$$\dot{\lambda} = \varepsilon_{ij}^{d} Q_{ij} \left(\frac{H}{3m} + 1 \right)^{-1}$$

$$\dot{\varepsilon}_{ij}^{de} = \dot{\varepsilon}_{ij}^{d} - \dot{\varepsilon}_{ij}^{d} + \dot{\varepsilon}_{ij}^{d} = \dot{\varepsilon}_{ij}^{d} \left(1 - \left(\frac{H}{3m} + 1 \right)^{-1} \right)$$

$$\dot{\sigma}_{ij} = \begin{cases}
\frac{2H\mu}{H+3m} \dot{\varepsilon}_{ij}^{d} + K \dot{\varepsilon}_{im} S_{ij} & \text{if } f=0 \\
2\mu \dot{\varepsilon}_{ij}^{d} + K \dot{\varepsilon}_{im} S_{ij} & \text{if } f<0
\end{cases}$$

