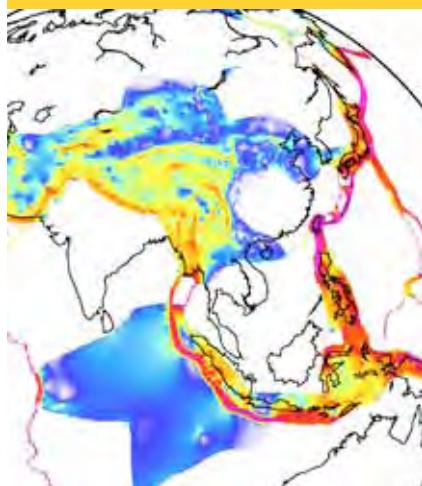


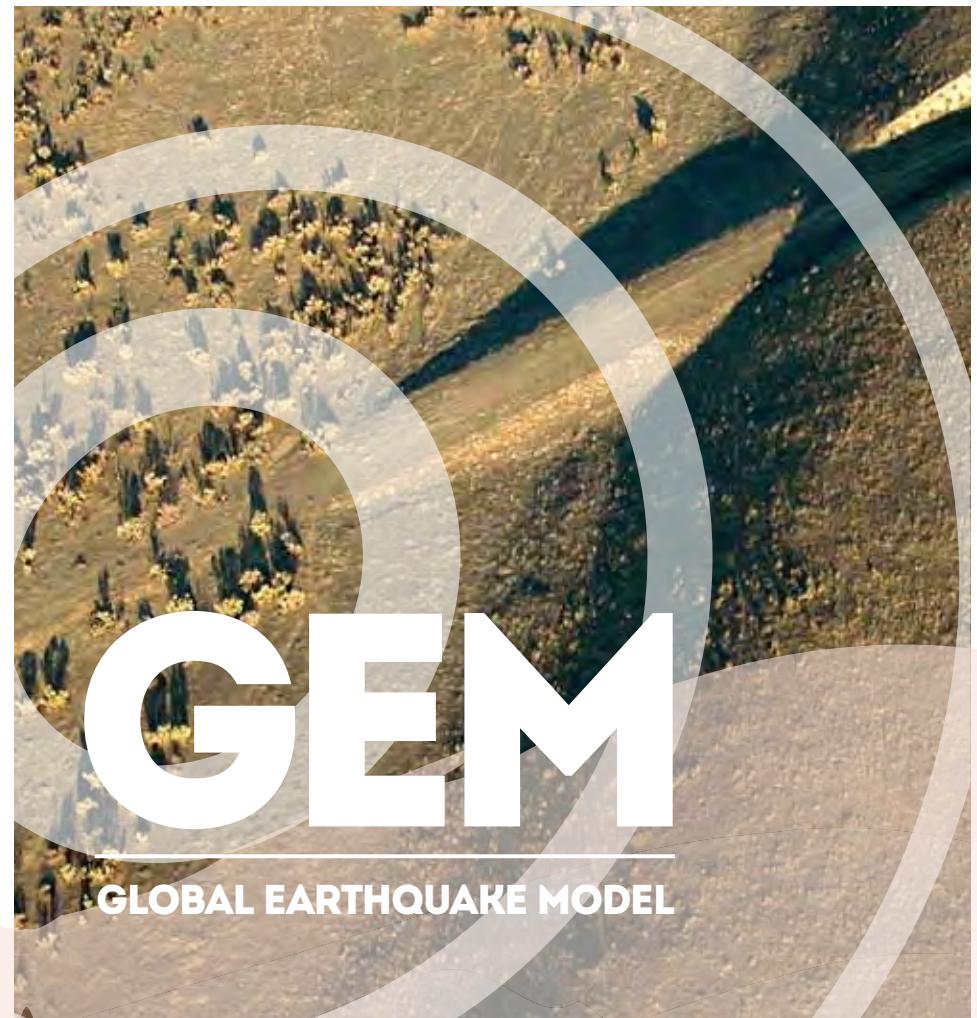
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GEOLOGICAL,
EARTHQUAKE AND
GEOPHYSICAL DATA

Global geodetic strain rate model

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Note on this release

This report details the data, model assumptions, and results for GSRM v.2.0. Since the writing of this report, a new version of GSRM (v.2.1) has been created and is now being released. Below are the details of how GSRM v.2.1 differs from v.2.0:

- + The UNR analysis produced 6739 velocities, all but 34 of those are used in the strain rate analysis.
- + We included 233 studies, from which 15,772 velocities were taken, and all but 62 were used in the strain rate analysis.
- + This makes a total of 22,415 velocities, at 18,336 locations, used in the analysis.
- + 17,567 data points are in the deforming zones, 4848 on rigid plates.
- + There are a total of 145,086 deforming grid cells. This increase is due to the inclusion of the Tyrrhenian Sea in the deforming zones.
- + The width of the zone along the creeping portion of the San Andreas Fault in which we exclude data was extended from 5 to 22 km. This explains the total of 96 excluded velocities, mentioned in the first two points above.
- + The definition of the motion of the Indian plate was changed to that using data from after (instead of prior) the 2004 Sumatra earthquake. This change minimizes any strain incompatibilities along the edges of the plate.
- + The a priori strain rate value for the Colorado Plateau area is now set to $3 \times 10^{-9}/\text{yr}$.
- + In the new model all grid cells use an a priori strain rate value taken from the result of an initial damped inversion, not just the cells that are constrained by GPS

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ABSTRACT

This is the final report produced in the context of the GEM Strain Rate Project, one of the global components of the GEM Foundation. The project was charged to analyse and synthesize all available geodetic data in order to create a global data set of geodetic velocities that can be used to model plate motions and strain rates in plate boundary zones. To this end, we estimated 6533 velocities from position time-series that we derived from the analysis of RINEX data that was either freely available or made available to us specifically for this project. All but 15 of these velocities were used in the modelling. In a separate analysis, we also re-analysed all RINEX data in China and effectively added 1143 velocities to the data set. Finally, we added 13,318 velocities from 216 studies in the published literature (or from personal communications) to achieve a grand total of 20,979 velocities at 17,491 unique locations used in the modelling. Of all velocities, 16,325 are in plate boundary zones (as defined by us) and the remaining 4654 velocities are for points on, predefined, rigid tectonic plates or blocks. We created a global mesh that has 144,827 deforming cells of 0.2° (latitudinal) by 0.25° (longitudinal) dimension covering the plate boundary zones, with the remaining cells covering 50 rigid plates and blocks. For 36 of these plates, we estimated the rigid-body rotation from our data set, and the rotations of the remaining plates are taken from the literature. The rigid-body rotations are used as boundary conditions in the strain rate calculations. The strain rate field is modelled using the Haines and Holt method, which uses splines to obtain an interpolated velocity gradient tensor field, from which strain rates, vorticity rates, and expected velocities are derived. We also estimated model uncertainties, specific for this high-resolution mesh, which indicates that there still are many areas with large strain rate uncertainties where the data spacing is often much larger than the cell dimensions. Nevertheless, the model and data input are a tremendous improvement to the previous global strain rate model from 2004. All results are transferred to GEM and are also archived and displayed by a dedicated server hosted by UNAVCO (gsrm2.unavco.org), one of the project's partners. In addition, we created a kmz-layer of contour's of the second invariant of the model strain rates, and we created an online tool that would allow a user to upload his own velocities and plot them with the velocities in the GEM dataset in 53 different reference frames.

Keywords

strain rate, geodetic velocities, GPS, plate boundaries

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1 Introduction

In 2009, the GEM foundation solicited proposals to create a geodetic strain rate model. The project presented here successfully proposed to update the Global Strain Rate Model (GSRM) v.1.2 of 2004 [Kreemer *et al.*, 2000, 2003; Holt *et al.*, 2005]. The new model, named GEM Strain Rate Model (GSRM v.2), is a large improvement on its predecessor, mostly because of the enormous increase in data. The data increase is large enough that the new model is almost exclusively based on the geodetic data alone, whereas the older model used faulting information and earthquake focal mechanisms as additional constraints. The data increase is due to two reasons: 1) we benefited from the proliferation of continuous GPS (CGPS) stations around the world and analysed all available raw data ourselves to obtain a unique consistent set of horizontal velocities, and 2) a large number of studies with geodetic velocities have been published since 2004.

2 GPS Data Analysis

The GPS analysis consisted of two components: 1) Analysis of all raw GPS data available to the University of Nevada, Reno (UNR) (section 2.1), and 2) Analysis of all raw GPS data in China (section 2.2). The two resulting velocity fields are combined by transforming the Chinese velocity field into the global solutions by inverting for, and applying, a translation rate and rotation rate that would minimize velocity differences at 36 collocated stations (i.e., IGS stations). We only maintain the UNR velocities for the collocated stations. The combined velocity field will be referred to as the “core solution”.

2.1 Analysis of Global Data

The analysis of all available GPS data (i.e., daily RINEX files) from around the world is performed at the University of Nevada, Reno. Most data come from public ftp/http sites, but some come from archives for which we have been given specific access (see Acknowledgements). Most data come from GPS stations that are operating continuously (CGPS), but we also analyse data for stations for which data are recorded intermittently but at a stable monument (e.g., MAGNET in Nevada, USA [Blewitt *et al.*, 2009; Hammond *et al.*, 2011], CBN network, Canada [Henton *et al.*, 2006], and Jura, France [Walpersdorf *et al.*, 2006]). Furthermore, some data come from CGPS stations for which only data for a few days per year are available (e.g., APRGP [Dawson *et al.*, 2004]).

We use GIPSY-OASIS II software for the data analysis package from the Jet Propulsion Laboratory (JPL) as well as JPL’s final fiducial-free GPS orbit products. Station coordinates were estimated every 24 hours by applying the Precise Point Positioning method to ionospheric-free carrier phase and pseudorange data [Zumberge *et al.*, 1997]. Data initially at the 15 or 30 second data intervals were automatically edited using the TurboEdit algorithm, and carrier phase data were decimated and pseudorange carrier-smoothed to obtain the ionosphere-free combinations of carrier phase and pseudorange every 5 minutes [Blewitt, 1990]. The observable model includes 1) ocean tidal loading and companion tides [Scherneck, 1991] using the FES2004 ocean tidal model [Lyard *et al.*, 2006], 2) estimation of wet zenith troposphere and two gradient parameters every 5 minutes as a random walk process [Bar-Sever *et al.*, 1998] using the Global Mapping Function (GMF) [Boehm *et al.*, 2006], 3) antenna calibrations for ground receivers and satellite transmitters [Schmid *et al.*, 2007], and 4) estimation of station clocks as a white-noise process. Finally, ambiguity resolution was applied to double differences of the estimated one-way bias parameters [Blewitt, 1989], using the wide lane and phase bias (WLPB) method, which phase-connects individual stations to IGS stations in common view [Bertiger *et al.*, 2010]. Resolving ambiguities significantly reduces the scatter in the East component time-series. Satellite orbit and clock parameters were provided by JPL, who determine them in a global fiducial-free analysis using a subset of the available IGS core stations as tracking sites. The fiducial-free daily GPS solutions are aligned to IGS08 [Rebischung *et al.*, 2012] by applying a daily 7-parameter Helmert transformation (3 rotations, 3 translations and a scale component) obtained from JPL [Bertiger *et al.*, 2010]. IGS08 is a frame that is derived from ITRF2008 and consists of 232 globally distributed IGS stations. The data processing system includes quality control, such as iterative outlier detection of the input observations, and rejecting output coordinates if the data fail to meet certain criteria such as number of unresolved cycle slips, fraction of the day spanned by the data, and formal errors.

We consider all data between January 01, 1996, and July 01, 2013, but only derive velocities from time-series that are at least 2.5 years long, so as to best account for seasonal cycles [Blewitt and Lavallée, 2002]. In some cases, time-series for (near) collocated stations are concatenated to extend their length and/or to derive a single velocity for two stations that operated consecutively. Because we are interested in capturing the “secular”, or interseismic, velocity, we exclude parts of the time-series that show significant transient motion. These transients are often due to postseismic deformation or slow-slip events (where the excluded part of the time-series is replaced with an offset). In the extreme, the exclusion could be for periods >10 years, sometimes at stations as far as several thousands kilometres from the largest earthquakes [Baek et al., 2012; Tregoning et al., 2013]. We model the time-series as an offset + trend (i.e., velocity) + annual cycle + semi-annual cycle + offsets. Offsets could come from equipment changes, earthquakes, or unknown reasons discovered in the analysis. Some stations only have intermittent data limiting our ability to model the seasonal terms, which could bias the velocity estimate. We therefore obtain the model parameters in a damped inversion, which ensures that the amplitude of the seasonal cycles remains small in those cases where data are only available for short periods year(s) apart. The velocities uncertainties are not adopted from this inversion, because it is well-known that those are too small due to the time-correlation of the errors. Instead we use the CATS software to calculate velocity uncertainties under the assumption that the error model consists of flicker-noise plus white-noise. We then multiplied the standard deviations with a factor of 2.0 so that the reduced chi-squared for fitting rigid-body rotations to velocities on stable plates is closer to 1.0.

Stations for which the time-series indicated rapid subsidence, unexplained transients, or for which the velocities were significantly different than nearby stations, were excluded. We also excluded any station near volcanic activity.

For the strain rate modelling we removed 15 velocities for stations within 5 km of the creeping section of the San Andreas Fault . The reason for this that the velocity profile across this fault is a step-function, which causes artefacts in the model, i.e., the spline function that we fit to the data will contain “overshoots” [Kreemer et al., 2012]. Removal of the data points close to the fault allows us to model the step-function as close as possible without creating “overshoots”.

2.2 Analysis of Chinese Data

We have processed GPS data to obtain a most updated velocity field in China. These data are not available outside China. The dataset includes mainly the campaign-mode field observations from the Crustal Motion Observation Network of China (CMONOC) sites in China, surveyed in 1999, 2001, 2004, 2007, 2009, and 2011, plus data from some other regional projects. Regional data are processed daily, and the solutions are subsequently combined with global daily solutions to tie the final solutions to the global ITRF2008 reference frame. Secular velocities, co-seismic offsets, and post-seismic logarithmic relaxations are incorporated in modelling GPS position changes. The final solution includes 1154 regional station velocities whose horizontal uncertainties are 1.5 mm/yr or less.

To produce this set of solution we have overcome numerous obstacles, such as properly modelling the antenna phase centre offset of the TOPCON antennas, removing biases introduced by using different geophysical models and satellite phase centre models employed by different GAMIT versions, and adequately modelling of the co-seismic and post-seismic displacements of the 2008 M7.9 Wenchuan earthquake, as well as some other large earthquakes occurred during the 1999–2011 period.

The handling of the data errors mostly follows Shen et al. [2011]. Gaussian errors are assumed for the GPS phase data during data processing to obtain the daily solutions. A priori uncertainty of 10 mm is assigned for the phase data, which are subsequently reweighted by a function associated with the observation elevation angle. Because GPS data are known to be correlated in time, a random-walk error model is assumed in time series modelling, with a set of constant perturbations of 1.0, 1.0, and 2.0 mm²/yr assigned for the variances of east, north, and up components of station positions, respectively. We also inspect the station position time series for outliers, and remove a few extreme outlier points and downweight a few others.

The resulting velocity field is shown in Figure 2.1

Because of Chinese regulations, station coordinates of the final results are given with only two decimal places, as opposed to three decimal places for the station coordinates of all other data analysed.

This velocity solution replaces previously published results [Shen et al., 2000, 2001, 2005; Wang et al., 2001; Zhang et al., 2004; Gan et al., 2007].

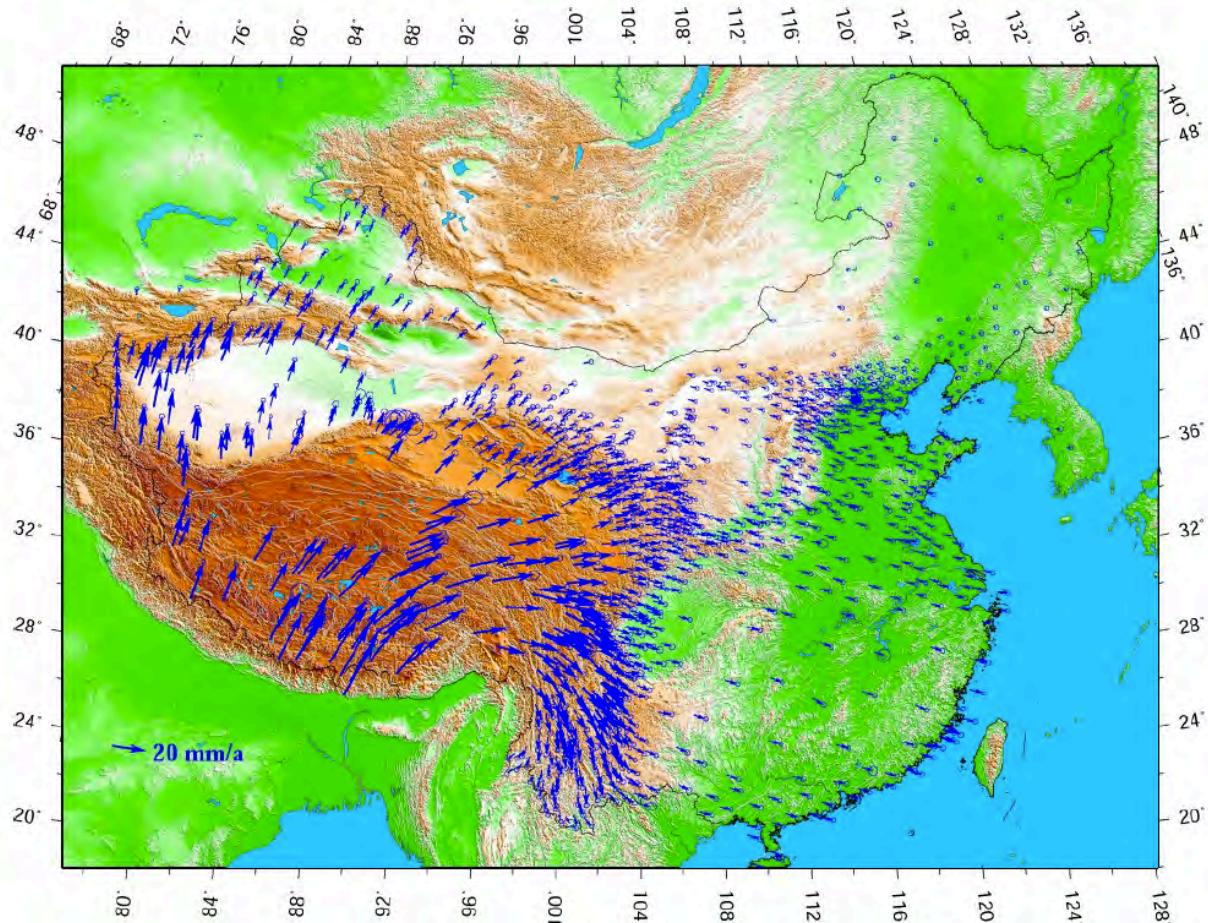


Figure 2.1 Velocity field for China relative to Eurasia

3 Synthesis of Published Velocities

The majority of geodetic velocities are derived from campaign-style measurements and are typically published in the literature. In other cases, publications report velocities for CGPS stations for which data is not publicly available. A very small minority of publications also report velocities derived from non-GPS techniques, such as DORIS [Bettinelli *et al.*, 2006; Saria *et al.*, 2013], VLBI [Shen *et al.*, 2011], or trilateration [Shen *et al.*, 2011; Weber *et al.*, 2011]. For several studies did researchers supply us with additional information such as station coordinates or velocities at nearby IGS sites. Six investigators sent us unpublished results (see Acknowledgements). All 210 publications from which data were used are listed in Appendix A. (For comparison, the previous model used data from 86 studies). For the first time, we included a handful of velocity estimates from submarine markers, off shore Peru [Gagnon *et al.*, 2005; used through the compilation Chlieh *et al.*, 2011] and Japan [Tadokoro *et al.*, 2012; Sato *et al.*, 2013].

In the synthesis, we included several studies focused exclusively on intraplate areas even though we do not solve for the strain rates there. The reason for this is that these studies could provide useful data in the future, when strain rates in plate interior will be modelled, and it would be sensible to already have them in the velocity compilation. We considered studies that put constraints on either the strain rates due to Glacial Isostatic Adjustment (GIA) [Mazzotti *et al.*, 2005; Lidberg *et al.*, 2010; Kierulf *et al.*, 2013] or on a known seismically active intraplate area such as the Carpathian Mountains [van der Hoeven *et al.*, 2005].

Where strain rates due to GIA interferes with tectonic strain rates, such as in southeast Alaska, we include GPS velocities that have been corrected for GIA by the original studies [Elliott *et al.*, 2010, 2013].

We applied the following criteria to decide whether data should be included:

1. studies were excluded when the velocity field was entirely based on publicly available data from (semi-)CGPS stations already analysed for the core solution [some examples since 2004 are: Prawirodirdjo and Bock, 2004; Wdowinski *et al.*, 2004; Wernicke *et al.*, 2004; Walpersdorf *et al.*, 2006; Calais *et al.*, 2006a; Hill and Blewitt, 2006; Kogan and Steblow, 2008; Teferle *et al.*, 2009; Argus *et al.*, 2010; Kreemer *et al.*, 2010a, 2010b; Hammond *et al.*, 2011; Asensio *et al.*, 2012; ten Brink and López-Venegas, 2012; Berglund *et al.*, 2012; de Lis Mancilla *et al.*, 2013; Ganas *et al.*, 2013].
2. if study a clearly superseded study b, then only results from study a were used. When in doubt both were included;
3. clear outlier velocities were removed, including those affected by volcanic deformation;
4. results reflecting postseismic deformation were not included;
5. velocities derived from <2.5 year (or sometimes just <2 year) time-series were excluded;
6. any station that was also excluded from the core solution;
7. velocities for 21 stations near the creeping portion of the San Andreas Fault (see section 2.1), but only after all data are combined (see below).

Next, we performed one large inversion in which we solve for, and apply, a translation rate and rotation rate that transform that would transform all results into the IGS08 reference frame of our core solution. The model parameters are obtained by minimizing velocity differences at collocated sites (within ~1km, short enough to avoid combining stations on opposite sides of the creeping section of the San Andreas Fault). We do this analysis for all studies simultaneously, because study *a* may, for example, not have any collocated

sites with the core solution, but has them with study *b*, which does have collocated sites with the core solution. Any velocity for a site collocated with the core solution will be removed, under the assumption that the velocity of the core solution is superior (e.g., it is typically derived from longer time-series and we checked offsets ourselves). At least three collocated sites are needed to solve for a translation and rotation rate. If only two collocated sites are present, we only solve for a rotation rate. To avoid solving for a large translation rate when the geographic footprint is small (in which case there may be a trade-off between translation and rotation rate), we down-weight the translation rate parameters in the inversion. In the few cases where study *a* mostly supersedes study *b*, but some velocities from study *b* are not in study *a*, we first translate study *b* onto study *a* before we perform the global transformation. In those cases we do not duplicate the velocities at the collocated sites. Fifteen studies could not directly be transformed, because they had less than two data points collocated with the other studies [Duquesnoy *et al.*, 1994; Antonelis *et al.*, 1999; Genrich *et al.*, 2000; Bacolcol *et al.*, 2005; Medak and Pribicevic, 2006; Rodriguez, 2007; Matson, 2007; Mullick *et al.*, 2009; Meng *et al.*, 2009; Ashurkov *et al.*, 2011; Tadokoro *et al.*, 2012; Miranda *et al.*, 2012; Sato *et al.*, 2013; Tserolas *et al.*, 2013; Mendes *et al.*, 2013], where we should note that only part of velocities presented by Genrich *et al.* [2000] could not be transformed and also that the results in Rodriguez [2007] seemed partly in difference reference frames. Six of these studies were presented in an ITRF-flavor reference frame, and we assumed that those were similar to our IGS08 frame. In addition, 2 studies were relative to a stable plate, and we fixed those velocities relative to the respective plates in our model. This leaves six studies which were then rotated into the model reference frame (i.e., Pacific) as part of modelling the velocity gradient tensor field while minimizing misfits between observed and model velocities. Although Mullick *et al.* [2009] was presented in an ITRF and plate-fixed fame, and has velocities at regional IGS stations, we solved for the transformation parameters in the strain rate model, because of notable problems with the velocity field if transformed or adopted as described above.

The procedure described above is an improvement on that followed in the previous GSRM when the transformation (i.e., rotation) of each study was determined in the modelling of the strain rates. The new approach is superior in that (except for the few exceptions mentioned above) the data is independent of the model.

In the end, we included 13,318 velocities from the literature. Together with the core solution, there are 20,979 velocity data at 17,491 unique locations available for the modelling. The sites are shown in Figure 3.1. For comparison, the previous model used 5170 velocities.

We show in Appendix A the GPS velocity field for many, well-covered, areas.

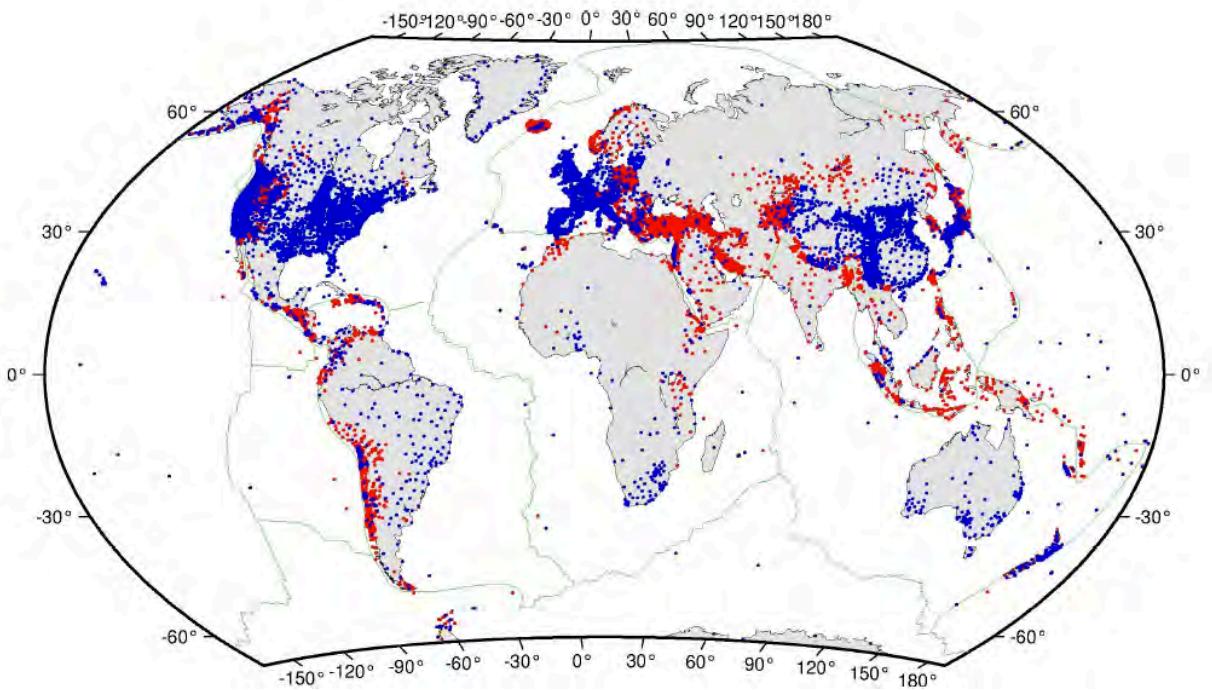


Figure 3.1 Locations for all 7661 GPS velocities for which we derived and used velocities (blue) and all 13,318 velocities we synthesized from the literature (red)

4 Strain Rate Modelling

4.1 Mesh Definition

We completely redefined the mesh for the modelling compared to what was used for the previous model. We consider the whole globe between 87.5°S and 87.5°N, which includes all data points, and the mesh is continuous in longitudinal direction. Individual grid cells are 0.2° (latitudinal) by 0.25° (longitudinal) in dimension. For comparison, the cells in the previous model were 0.5° by 0.6°. To determine which cells should be allowed to deform (i.e., cover the plate boundaries) and which not (i.e., move with a rigid plate), we started with the plate definitions of the PB2002 model of *Bird* [2003]. For each node of the mesh it was determined if it was within the polygon of a plate (and which plate) or not. As a result, for plate boundary zones that are defined by a single “line”, such as oceanic ridge-transform systems, the boundary consist of a single grid cell, which four corner nodes are typically divided over two plates. The definition of the diffuse zones in PB2002 was augmented by the boundary definitions of *Chamot-Rooke and Rabaute* [2006]. We made numerous adjustments to these definitions, mostly guided by the information from the GPS data. In total, the model contains 144,827 deforming cells, compared to 22,310 cells in the previous model. The deforming cells are shown in Figure 4.1 Of the total 20,979 velocities, 16,325 are inside the deforming cells (Figure 4.2).

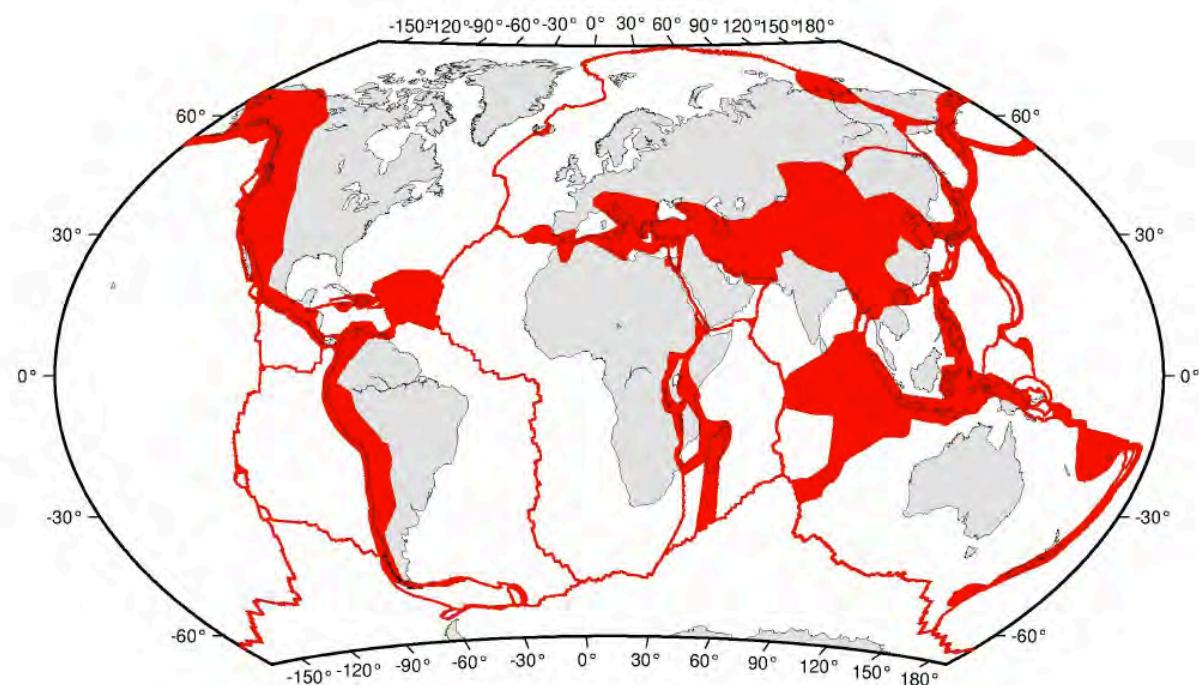


Figure 4.1 Red areas comprise the deforming grid cells, each 0.2° (latitudinal) by 0.25° (longitudinal) in dimension

A number of blocks defined in PB2002 were allowed to deform in our model, typically in areas of diffuse deformation such as Southeast Asia or the Andes. The rationale for this is that these blocks are typically in areas of large and complex deformation. If the blocks are covered by GPS stations, their velocities do often not reflect long-term motion because of elastic strain build-up along its margin (e.g., the Altiplano block) or, if they have no GPS coverage, the motion defined in PB2002 may not be compatible with nearby GPS data, causing spurious strain rates along the blocks' edges. This is not to say that no rigid blocks exist in continental back-arcs [Brooks *et al.*, 2003; Wallace *et al.*, 2004; Chlieh *et al.*, 2011; McCaffrey *et al.*, 2013], but that it is not possible to properly model the surface deformation (i.e., rigid block motion with localized high strain rates along its edges) without correcting/modelling for elastic strain accumulation.

Our model contains 50 rigid plates and blocks, compared to the 25 plates assumed in the previous model. We added a number of blocks that were not in PB2002. All these additional blocks have been shown to exist in the literature and, with two exceptions (Capricorn and Lwandle), we were able to constrain their rigid-body rotations by the GPS data (see Section 4.2). The new blocks are listed below with references arguing for their existence:

- Bering [e.g., Mackey *et al.*, 1997; Cross and Freymueller, 2008]
- Baja California [e.g., Umhoefer and Dorsey, 1997; Plattner *et al.*, 2007]
- Capricorn [e.g., Royer and Gordon, 1997; Conder and Forsyth, 2001]
- Danakil [McClusky *et al.*, 2010]
- Gônave [e.g., Mann *et al.*, 1995; Benford *et al.*, 2012]
- Lwandle [e.g., Hartnady, 2002; Horner-Johnson *et al.*, 2007]
- Puerto Rico [e.g., McCann, 1985; Jansma *et al.*, 2000; Manaker *et al.*, 2008]
- Rovuma [e.g., Hartnady, 2002; Calais *et al.*, 2006b]
- Sakishima [Nishimura *et al.*, 2004]
- Satunam [Nishimura *et al.*, 2004]
- Sinai [e.g., Salamon *et al.*, 2003; Mahmoud *et al.*, 2005]
- Victoria [e.g., Hartnady, 2002; Calais *et al.*, 2006b]

The Sakishima and Satunam blocks are sub-blocks of PB2002's Okinawa block and named here for the first time. In our model the Okinawa block is limited to only the central portion of the block defined in PB2002, with Sakishima to its south and Satunam to its north.

The Bering, Capricorn, Lwandle are part of the MORVEL plate motion model [DeMets *et al.*, 2010], although MORVEL did not have a rotation rate for Bering, which we estimated from the GPS data.

Compared to the previous strain rate model, other new plates and blocks in the model are (from PB2002): Aegean Sea, Burma, Easter, Galapagos, Juan Fernandez, Mariana, Niuafou, North Bismarck, Okinawa, Panama, Shetland, Sandwich, Solomon Sea, South Bismarck, Tonga, Woodlark

For some of these blocks (Aegean Sea, Mariana, Okinawa, Panama, Shetland, South Bismarck, Tonga, Woodlark) we were able to estimate the rigid-body rotation from the GPS data (see section 4.2) and thus replace the rotation given by PB2002.

Two plates that existed in the previous model are now part of a deforming zone. One is the Anatolia micro-plate, which also exists in PB2002. While it has long been considered as a rigid micro-plate [McKenzie, 1970; McClusky *et al.*, 2000], it is now evident from a new dense GPS network that there is significant internal deformation within Anatolia [Aktuğ *et al.*, 2013]. The other plate is Tarim. While it may indeed be a rigid micro-plate [Avouac *et al.*, 1993; Shen *et al.*, 2001; Meade, 2007; Zhang and Gan, 2008], there is now significant GPS coverage to constrain the Tarim area as having low strain rates within the greater India-

Eurasia subduction zone. Following the same argument, we do not consider, for example, a central Iranian block [Jackson and McKenzie, 1984; Vernant et al., 2004], a rigid Sierra Nevada-Great Valley block in the western United States [Argus and Gordon, 1991; Dixon et al., 2000; McCaffrey, 2005], or an Adria and/or Apulia block(s) between Italy and the Balkans [e.g., Anderson and Jackson, 1987; Ward, 1994; Battaglia et al., 2004; D'Agostino et al., 2008].

Polygon coordinates of all 50 plates/blocks are available upon request.

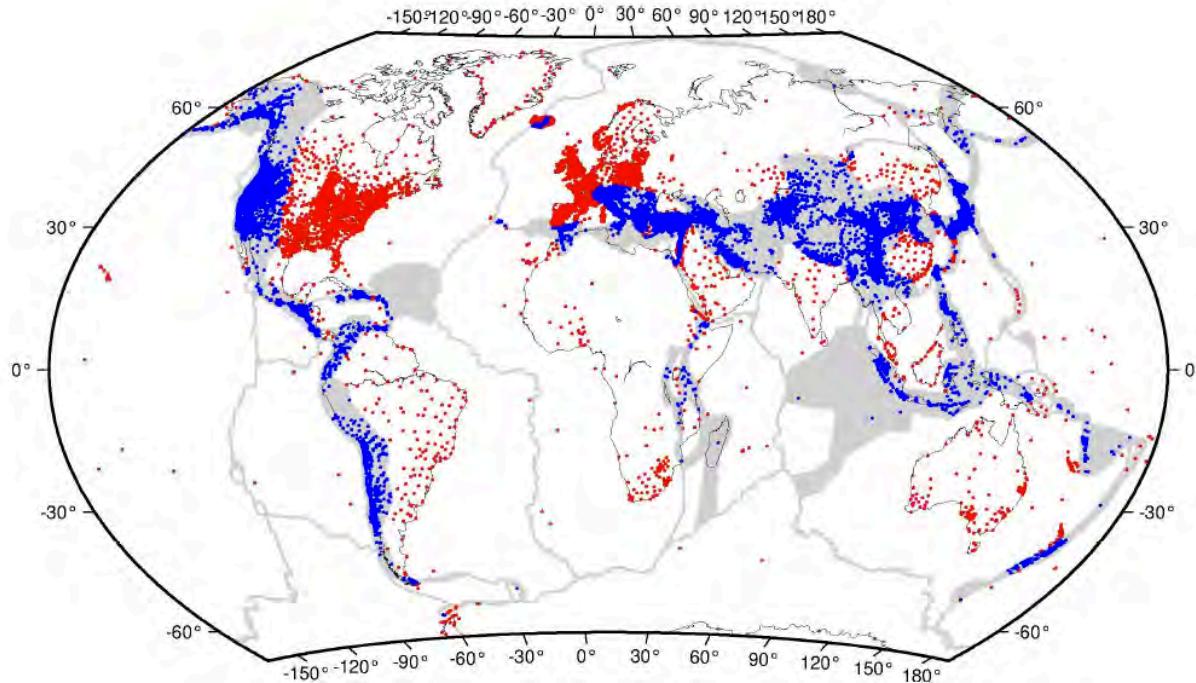


Figure 4.2 Deforming zones (in grey), locations of data points inside deforming grid (blue circles) and location on rigid plates (red circles). 16,326 velocities are used inside the deforming areas.

4.2 Rigid Body Rotations

In Table 4.1 we list the angular velocities (in terms of the corresponding Euler pole and rotation rate) for all assumed rigid plates and blocks included in the model. They are listed relative to the Pacific plate, which is the model's reference plate. Of the 50 plates, 36 angular velocities were estimated from the GPS velocities by this project, 6 were taken from PB2002 [Bird, 2003] and 8 were taken from MORVEL [DeMets et al., 2010].

Appendix C lists the IGS08-velocities used to constrain the plate motions, their residuals, and the study from which the velocity was taken.

Table 4.1 Euler pole location and rate, relative to Pacific, for all rigid plates/blocks in model. All results are derived by us, except * is from Bird [2003] and # is from DeMets et al. [2010]

Latitude ($^{\circ}$ N)	Longitude ($^{\circ}$ E)	Rate ($^{\circ}$ Myr $^{-1}$)	Plate Abbreviation	Plate Name
59.14	-73.32	0.942	AF	Africa
63.16	-79.68	0.944	AM	Amur
64.09	-83.73	0.882	AN	Antarctica
60.52	-45.39	1.112	AR	Arabia
73.68	-37.71	0.808	AS	Aegean Sea
60.56	3.64	1.082	AU	Australia
37.75	-8.22	0.037	BC	Baja California
34.78	-63.17	0.665	BG	Bering Sea
8.89	-75.51	2.667	BU	Burma*
56.03	-81.68	0.928	CA	Caribbean
10.13	-45.57	0.309	CL	Caroline#
42.20	-112.80	1.676	CO	Cocos#
62.30	-10.10	1.139	CP	Capricorn#
33.05	29.51	2.864	DA	Danakil
28.30	66.40	11.400	EA	Easter*
61.38	-78.85	0.927	EU	Eurasia
9.40	79.69	5.275	GP	Galapagos*
47.07	-78.99	1.070	GV	Gôname
61.34	-39.20	1.133	IN	India
-0.60	37.80	0.625	JF	Juan de Fuca#
35.91	70.17	22.520	JZ	Juan Fernandez*
60.00	-66.90	0.932	LW	Lwandle#
28.24	147.84	2.143	MA	Mariana
49.29	-76.04	0.791	NA	North America
-0.66	144.60	0.743	NB	North Bismarck

Latitude (°N)	Longitude (°E)	Rate (° Myr ⁻¹)	Plate Abbreviation	Plate Name
6.87	-168.87	3.255	NI	Niuafou [*]
57.23	-88.59	1.252	NZ	Nazca
53.64	-76.91	0.831	OK	Okhotsk
62.40	163.77	1.561	ON	Okinawa
0.00	0.00	0.000	PA	Pacific
33.47	-82.09	1.743	PM	Panama
47.33	-76.68	1.135	PR	Puerto Rico
-3.96	-41.88	0.864	PS	Philippine Sea
25.70	-104.80	4.966	RI	Rivera [#]
59.74	-70.66	0.930	RO	Rovuma
55.14	-83.42	0.684	SA	South America
11.49	-33.95	6.996	SB	South Bismarck
57.80	-78.00	0.755	SC	Scotia [#]
62.92	-39.75	1.094	SI	Sinai
32.73	129.75	7.031	SK	Sakishima
78.23	149.12	2.240	SL	Shetland
58.85	-79.53	0.983	SO	Somalia
19.53	135.02	1.478	SS	Solomon Sea [*]
48.65	139.00	3.053	ST	Satunam
59.20	-79.26	1.004	SU	Sunda
-3.80	-42.40	1.444	SW	Sandwich [#]
29.42	2.23	9.229	TO	Tonga
57.96	-84.86	0.973	VI	Victoria
17.69	134.28	1.763	WL	Woodlark
65.16	-83.04	0.991	YA	Yangtze

We chose to not use every GPS velocity on each rigid plate to estimate the angular velocities. Typically we would only use the best-behaved, longest running stations from our own analysis. In some cases, there were insufficient stations from our own analysis (or a sufficient number was not well distributed across the plate) to estimate the angular velocity. In those cases we also used velocities from the literature synthesis. In general, we would omit stations near plate boundaries, as those may be affected by elastic strain accumulation. A more detailed discussion is warranted for a subset of the plates:

1. Baja California

We estimate an Euler pole for Baja California relative to the Pacific plate at almost 90° away from the block, suggesting a pure translational nature of its motion. The predicted motion relative to the Pacific plate is $\sim 4 \text{ mm yr}^{-1}$ to N40°W. A GPS station near Cabo San Lázaro [Plattner *et al.*, 2007], moves at $\sim 2 \text{ mm yr}^{-1}$ to the southeast, suggesting that the boundary between the Pacific plate and the Baja California block is likely accommodated across a broad zone along the western margin of the Baja Peninsula.

2. Caribbean

We estimate the angular velocity for the Caribbean plate by using our velocity estimates for San Andres Island and Grenada and the additional estimate for Aves Island from Weber *et al.* [2001]. Most studies have considered station CRO1 on Saint Croix, U.S. Virgin Islands, to be part of the Caribbean plate [e.g., Sella *et al.*, 2002; Prawirodirdjo and Bock, 2004; Altamimi *et al.*, 2012]. In our analysis, CRO1 and nearby station VIKH move to the SSW at $0.4\text{--}1.3 \text{ mm yr}^{-1}$ relative to the Caribbean plate, possibly suggesting that the Muertos Trough is active as far east as south of the U.S. Virgin Islands [McCann, 1985].

3. Eurasia

The station coverage for the Eurasian plate is highly biased towards western Europe. To estimate the angular velocity, we used our velocity estimates from ten long-running CGPS sites that are roughly equally distributed across the plate. We excluded stations in Scandinavia, where velocities are affected by GIA [Lidberg *et al.*, 2010; Kierulf *et al.*, 2013]. The areas in the far-field from the former Fennoscandian ice-sheet may be moving towards the ice-sheet, but by picking areas equally covered over the plate, that affect should be averaged (see discussion North American plate below).

4. India

We observe a change (i.e., speed-up) in the east velocity of the long-running station at Bangalore (IISC) at the time of the 26 December, 2004, Mw=9.15, Sumatra earthquake. Even though this station is $>2000\text{km}$ from the epicentre, it is likely that this velocity change is due to visco-elastic postseismic relaxation. Similar results are seen in stations in SE Australia after the 23 December, 2004, Mw=8.1, Macquarie Ridge earthquake [Tregoning *et al.*, 2013] and in Korea after the March 11, 2011, Mw=9.0 Tohoku-Oki event [Baek *et al.*, 2012]. However, we do not see a velocity change for the CGPS station in Hyderabad, 500 km north of Bangalore. We restricted the data for Bangalore to be before the 2004 earthquake. Many of the studies that we added in this area have velocities based on data (partially) from after the 2004 earthquake. This could have some effects in the strain rate estimates along the boundaries of the rigid plate. However, it is not really possible to avoid this subtle effect, unless we only consider studies based on data from before the event. Most studies present velocities based on similar time-span, which is most important in inferring reliable strain rates within the footprints of those studies.

5. Mariana

For the Mariana plate we used our CGPS velocity on Mariana Island (CNM0, formed by concatenating the time-series of CNMI and CNMR) and three additional velocities from *Kato et al.* [2003] along the central Mariana Islands. Like *Kato et al.* [2003], we don't correct for any possible elastic strain accumulation along the Marianas trench. We find a significant N-to-S increase in the back-arc spreading rate, but overall 3-8 mm yr⁻¹ slower than predicted by *Kato et al.* [2003].

6. Nazca

It has been shown that significant deformation near Easter Island affects the GPS station there [*Kendrick et al.*, 2003] (ISPO, formed by concatenating the time-series of EISL and ISPA). We therefore add to the single CGPS station on the Galapagos Islands (GLPO, formed by concatenating the time-series of GALA and GLPS), the two velocities on San Felix and Robinson Crusoe Islands originally presented by *Kendrick et al.* [2003], but taken from *Wang et al.* [2007]. ISPO moves 2.8 mm yr⁻¹ towards S52°E relative to our definition of stable Nazca.

7. North America

Most previous studies of the motion of the North American plate only considered stations south of the former ice-sheet [e.g., *Sella et al.*, 2007; *Argus et al.*, 2010; *Altamimi et al.*, 2012]. However, the predictions from the latest GIA models predict a far-field motion towards the former ice-sheet [*Peltier and Drummond*, 2008]. If we were only to choose GPS stations south of the ice-sheet to estimate the plate's angular velocity, the assumed rigid-body motion of the northern part of the plate will be biased. We therefore chose 10 long-running stations that covered the entire plate roughly uniformly. Unfortunately, this still causes a small problem; we find artificial elevated strain rates along the eastern edge of the Pacific-north America plate boundary in the western U.S., because of the northerly oriented velocities (1-1.5 mm yr⁻¹) of the numerous stations in the eastern end of the boundary (due to GIA) relative to the (artificially) fixed plate interior. For future models, to avoid this artefact, all of the North American plate should be allowed to deform. Then, the strain rates due to GIA would be correctly found around the former ice-sheet.

8. Okhotsk

It is difficult to estimate an angular velocity for the Okhotsk plate, because GPS can only be found along its margins, where velocities may be affected by elastic loading (for which we do not account). Nevertheless, we are fairly confident about our results, which predicts (relative to Amur plate) ~8 mm yr⁻¹ WSW directed shortening across the island of Sakhalin and ~2 mm yr⁻¹ NE directed motion relative to North America across the Chersky Range. Both results are, at least in direction, consistent with regional focal mechanisms, with the motion across the Chersky Range being partitioned between E-W directed left-lateral strike-slip and N-S shortening [e.g., *Cook et al.*, 1986; *Riegel et al.*, 1993].

9. Pacific

Our definition of a stable Pacific plate includes the first global use of velocities at two stations (Kiritimati (KRTM), Kiribati Islands, and Gambie Island (GAMB), French Polynesia) for which data were collected by the Asia Pacific Crustal Monitoring System [*Harada*, 2000; *Munekane and Fukuzaki*, 2006], which allows for a better geometric spread of stable stations. Although the station on Guadalupe Island (GUAX), southwest of Baja California, would provide an important geometric constrain in the rotation estimation, the suggestion of thermal contraction in the young oceanic lithosphere precludes us from using it [*Kumar and Gordon*, 2009; *Kreemer et al.*, 2010c]. Indeed, GUAX moves at ~1.2 mm yr⁻¹ towards S27°E.

10. Philippine Sea

There are a couple of islands with GPS stations on this oceanic plate. The data from station G140 on Okino Torishima (also called Parece Vela) near the centre of the Philippine Sea plate is noisy and are not used. To avoid a geometric bias, we used only one of the two velocities on the Daito Islands, namely on Kita Daito (J746), and combine it with the velocity for Koro, Palau Islands (PAL0, concatenated from PAL1 and PALA). In this definition G140 moves $\sim 0.8 \text{ mm yr}^{-1}$ towards the NNE.

11. Scotia

There are a few GPS sites located on the very western side of the plate, but this provides a very poor geometry to estimate the angular velocity. We therefore adopted the rotation from MORVEL [DeMets *et al.*, 2010].

12. Shetland

We combined data for various studies (table 4.2) to present the first angular velocity estimate for the small Shetland block, which is almost entirely surrounded by the Antarctic plate. The pole of rotation of the block relative to Antarctica is near Gibbs Island. The result predicts northward directed shortening across the South Shetland Trench, from 6 mm yr^{-1} in the east to 12 mm yr^{-1} in the west, and a maximum of 9 mm yr^{-1} NNE directed extension across the Bransfield Rift System near Deception Island.

13. Tonga

As for the Mariana block, we assume that the three velocities we use to estimate the angular velocity of the Tonga block are not affected by elastic loading along the subduction interface.

4.3 Strain Rate Model

We used the method of Haines and Holt [*e.g.*, Haines and Holt, 1993; Holt *et al.*, 2000; Beavan and Haines, 2001] to model the strain rate field. This method uses bi-cubic splines to obtain a continuous velocity gradient tensor field in the plate boundary zones. The rigid-body rotations listed above are applied as *a priori* boundary conditions, relative to the Pacific plate, which is the reference plate in the model.

4.3.1 Methodology

To model the strain rate field as a continuous model, we explicitly assume that the crustal thickness over which the strain rates apply is relatively small compared to the horizontal dimension. We actually model the velocity gradient tensor field, which comprises both strain rates and vorticity. For this, we relate the velocity gradient tensor field to a three-dimensional rotation rate vector $\dot{\mathcal{W}}$ (which intercepts the Earth's centre and surface). A continuous velocity field $v(\hat{x})$ can then be written as:

$$v(\hat{x}) = R[\dot{\mathcal{W}}(\hat{x}) \times \hat{x}] \quad (1)$$

where R is the Earth's radius, and \hat{x} is a 3-dimensional unit vector for any point on the Earth's surface with latitude θ and longitude φ :

$$\hat{x} = (\cos\theta\cos\varphi, \cos\theta\sin\varphi, \sin\theta) \quad (2)$$

If \dot{W} is constant over a given area, then (1) gives the well-known formulation for a rigid body rotation. In fact, we define a rigid block/plate by enforcing \dot{W} to be constant (i.e., its spatial derivatives are zero) for part of the grid. For the new GSRM, \dot{W} is set *a priori* for each plate/block, using the results in Table 4.1.

The horizontal strain rates on a sphere can be written using the spatial derivatives of \dot{W} :

$$\dot{\varepsilon}_{\varphi\varphi} = \frac{\hat{\theta}}{\cos\theta} \frac{\partial \hat{W}}{\partial \varphi} \quad (3)$$

$$\dot{\varepsilon}_{\theta\theta} = -\hat{\phi} \frac{\partial \hat{W}}{\partial \theta} \quad (4)$$

$$\dot{\varepsilon}_{\varphi\theta} = \frac{1}{2} \left(\hat{\theta} \frac{\partial \dot{W}}{\partial \theta} - \frac{\hat{\phi}}{\cos\theta} \frac{\partial \dot{W}}{\partial \varphi} \right) \quad (5)$$

where $\hat{\theta}$ and $\hat{\phi}$ are the unit vectors in the North and East directions, respectively. In these definitions the contribution of any gradient in vertical velocities is omitted, because it is small.

The rotation rate about a local vertical axis (i.e., vorticity) can be written as:

$$\omega_r = \hat{x} \cdot \dot{W} - \frac{1}{2} \left(\frac{\hat{\phi}}{\cos\theta} \frac{\partial \dot{W}}{\partial \varphi} + \hat{\theta} \frac{\partial \dot{W}}{\partial \theta} \right) \quad (6)$$

The rotation vector function (\dot{W}) is expanded spatially using bi-cubic Bessel functions.

The objective function that is minimized in the inversion is:

$$\sum_1^N (\dot{\varepsilon}_{ij}^{fit} - \dot{\varepsilon}_{ij}^{obs}) (\dot{\varepsilon}_{pq}^{fit} - \dot{\varepsilon}_{pq}^{obs}) V_{ij,pq}^{-1} + \sum_1^M (u_i^{fit} - u_i^{obs}) (u_j^{fit} - u_j^{obs}) C_{ij}^{-1} \quad (7)$$

where ij , and pq denote tensor components of the strain rate tensor. The above equation suggest that “observed” strain rates can also be input, as was done in the previous GSRM, but this option was not used for the current GSRM. In any case, the strain rate variance covariance matrix V needs to be set. One could set the off-diagonal components of V such that preferred strain rate direction/style is imposed (as was done in the previous GSRM using earthquake focal mechanisms). However, for the new GSRM we only set the

diagonal components of V , i.e., variances of the three strain rate components (see Section 4.3.2). The second part of (7) pertains to the fit of the M geodetic velocities, with the data covariance matrix given by C .

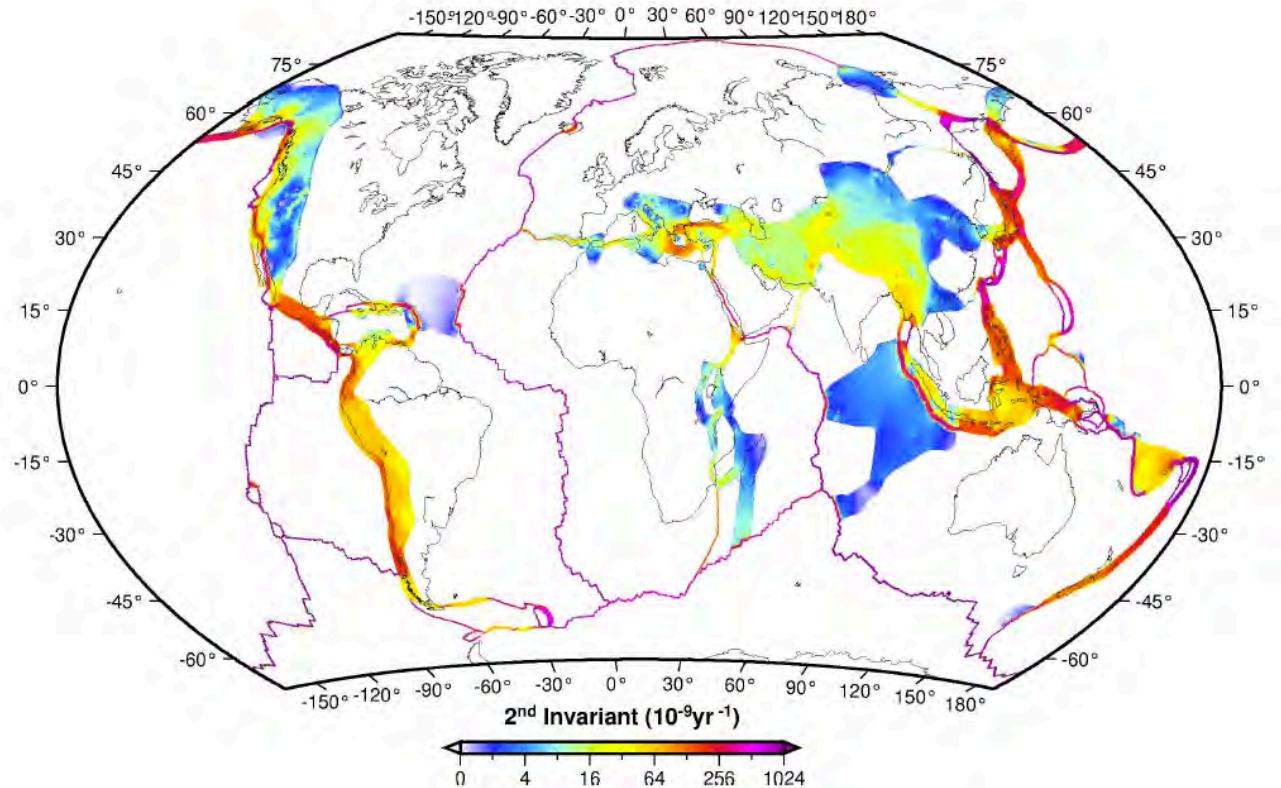


Figure 4.3 Second invariant of strain rates from step 1 (i.e., a spatially damped solution)

For the strain rate and velocity field to be self-consistent, St. Venant's compatibility relationships need to be satisfied everywhere. This strain rate compatibility equation for the horizontal strain rate tensor is (in Cartesian coordinates):

$$\frac{\partial^2 \varepsilon_{xx}}{\partial y^2} + \frac{\partial^2 \varepsilon_{yy}}{\partial x^2} - 2 \frac{\partial^2 \varepsilon_{xy}}{\partial x \partial y} = 0 \quad (8)$$

This constraint avoids having incompatible strain rates from spurious velocity data and ensures that the velocity gradient between points A and B is independent of the path one takes through the deforming area from A to B.

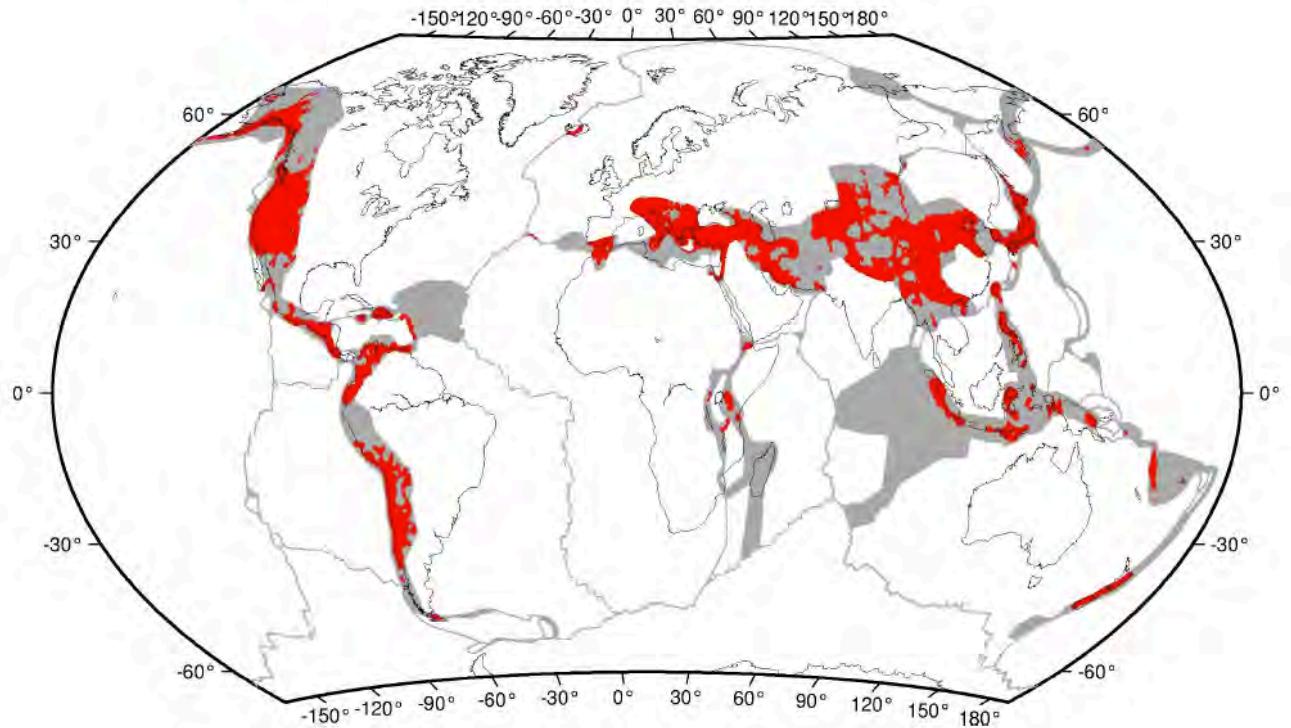


Figure 4.4 Red areas are parts of the plate boundary zone that are well constrained by GPS data (given our definition described in text), grey areas are not.

4.3.2 *A priori strain rate variances*

Following a Bayesian philosophy, the method requires us to assign *a priori* strain rate (co-)variances to each deforming grid cell. In order to properly fit the velocity gradient field in areas of high and low strain rates, and to avoid under- or over-fitting the geodetic velocities, respectively, we prefer to assign *a priori* variances that reflect the actual expected strain rates. To accomplish this, we decided on a two-step approach, modelling the strain rate field twice. In the first step, we assign the same standard deviations of $10^{-8}/\text{yr}$ for $\dot{\varepsilon}_{\varphi\varphi}$ and $\dot{\varepsilon}_{\theta\theta}$, and $1/\sqrt{2} 10^{-8}/\text{yr}$ for $\dot{\varepsilon}_{\varphi\theta}$ to each cell, with zero covariances (i.e., assumed isotropy). However, if we would assign the same *a priori* values to each grid cell, we would create some erroneous results in the diffuse oceanic areas, where GPS data are largely absent. For instance, we can safely assume that in the Indian Ocean most of the deformation occurs along the spreading centres and not in the diffuse zone between the India, Capricorn and Australian plates. If we assign the same *a priori* variances to all grid cells, relatively high strain rates due to the relative plate motions will spread into the diffuse zone. To remedy this, we give all cells with transform and ridge segments very large *a priori* values. We do the same for the part of the Sunda subduction zone that borders the Indian Ocean diffuse deformation area. We follow a similar approach for the diffuse oceanic areas between the New Hebrides and Fiji, the one between the North and South America plates, and in the “armpit” of the easternmost Aleutian/Alaska subduction zone. For the diffuse boundary between Africa and Eurasia, south west of Portugal (as defined by *Chamot-Rooke and Rabaut [2006]*), the PB2002 boundary segments run through the middle of the diffuse zone and we set very high variances for the cells containing the PB2002 boundary segments. Figure 4.3 shows the second invariant of the model resulting from step 1.

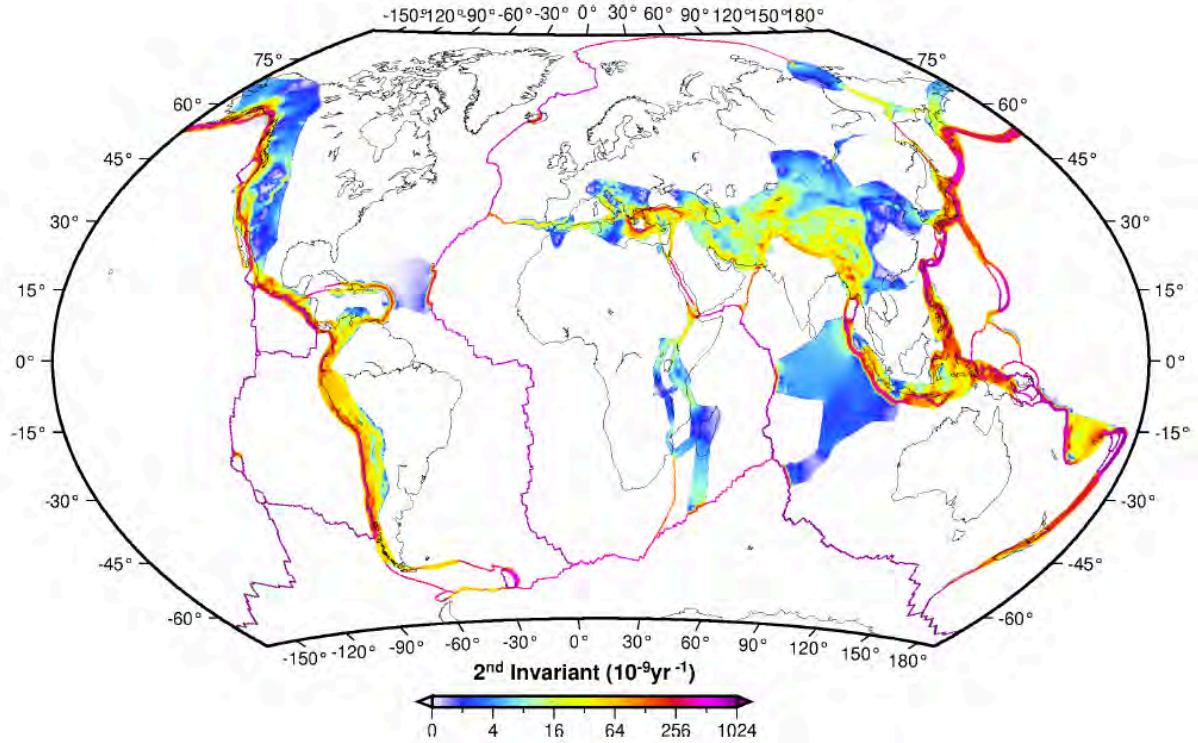


Figure 4.5 Contours of the second invariant of the strain rate tensor

In the second step, we take the modelled strain rate field from the first step and used it to constrain the *a priori* standard deviations. For this, we did not take-over the style or covariances but set the *a priori* standard deviation of $\dot{\varepsilon}_{\varphi\varphi}$ and $\dot{\varepsilon}_{\theta\theta}$ equal to the second invariant of the tensor modelled in step 1 ($\sqrt{\dot{\varepsilon}_{\varphi\varphi}^2 + \dot{\varepsilon}_{\theta\theta}^2 + 2\dot{\varepsilon}_{\varphi\theta}^2}$), and $\dot{\varepsilon}_{\varphi\theta}$ to the second invariant divided by the square-root of 2. However, we only want to apply these constraints to those cells that are reasonably well constrained by the GPS data so not to potentially “blow-up” the strain rates in areas where the data don't warrant it. We decided that a grid cell is constrained by the data if its midpoint lies within an ellipse defined by a pair of geodetic stations (within the deforming zones) less than 200 km apart with the data points situated at the endpoints of the major axis, and the length of the minor-axis being 3/4 of the major axis. Figure 4.4 shows the grid cells that we define as being well constrained by the data. All cells whose midpoints do not fall within any ellipse had their *a priori* standard deviations set to 0.35 times the second invariant of the tensor modelled in step 1 (to damp the model more where there are no data), unless that value is lower than the *a priori* standard deviations used in step 1 (i.e., $10^{-8}/\text{yr}$), in which case those *a priori* standard deviations values are used. The latter exception is to avoid large signal-to-noise values in slowly deforming ($<10^{-8}/\text{yr}$), unconstrained, areas. A final exception was given to the Colorado Plateau area in the western United States. Because of how we define stable North America, we would obtain a band of elevated strain rates on the eastern edge of the Pacific-North America plate boundary zone (see discussion on the definition of the North America rotation vector in section 4.2) when following the procedure above. To avoid most of this artefact, we set the *a priori* strain rates in the second step to $5 \times 10^{-9}/\text{yr}$ in order to damp the model there.

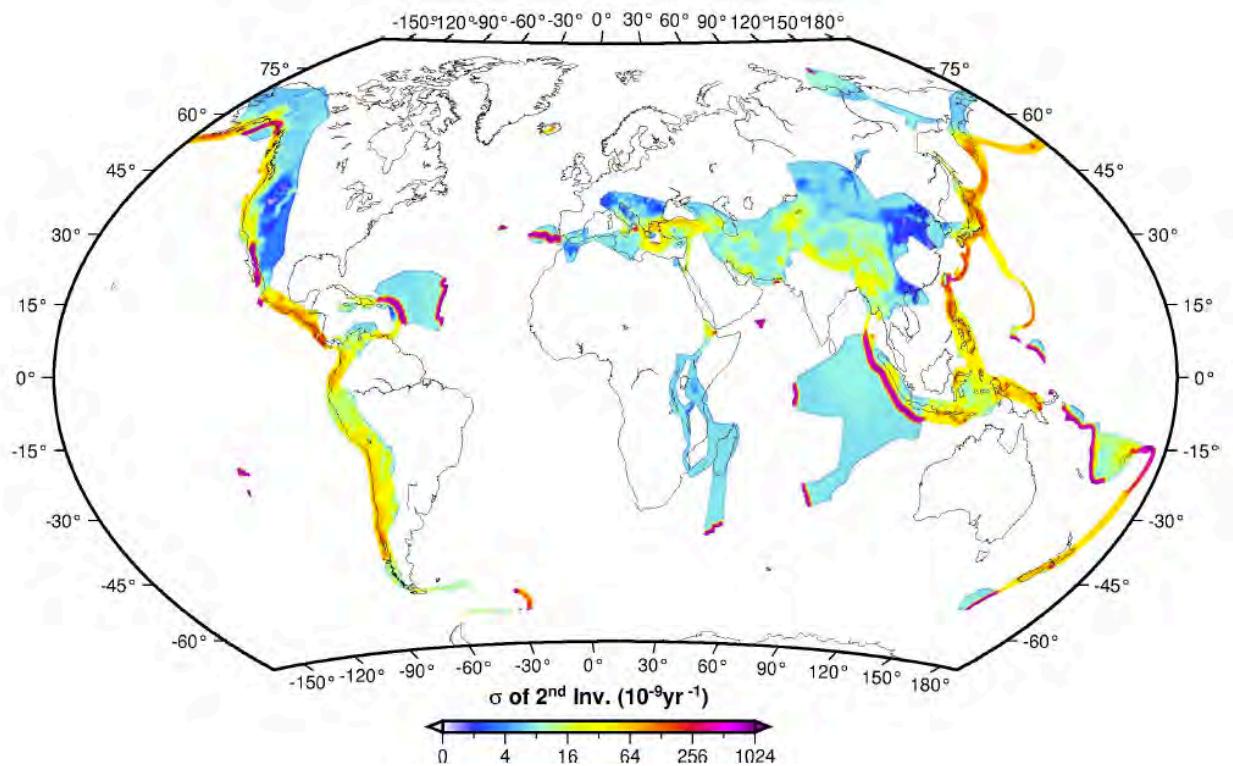


Figure 4.6 Contours of the standard deviation of the second invariant of the strain rate tensor

4.3.3 Results

The second invariant of strain rate of GSRM v.2 is shown in Figure 4.5. Note that the colour-scale is non-linear and that the high values are saturated. Strain rate contours for selected regions (where the model is well constrained by GPS data) are shown in Appendix A along with the input data.

A map with formal model uncertainties is shown in Figure 4.6 and a map with the signal-to-noise ratio in Figure 4.7. It is important to keep in mind that the shown uncertainties are indicative for uncertainty of the model at the scale of the 0.2° by 0.25° large cells. Because station spacing is for many areas (much) larger than the grid dimension, model uncertainties are correspondingly large. Also note that the strain rate uncertainties are zero for most spreading ridges and transform, because the deforming grid is only one grid cell wide, and thus the average model strain rates for those cells are exact.

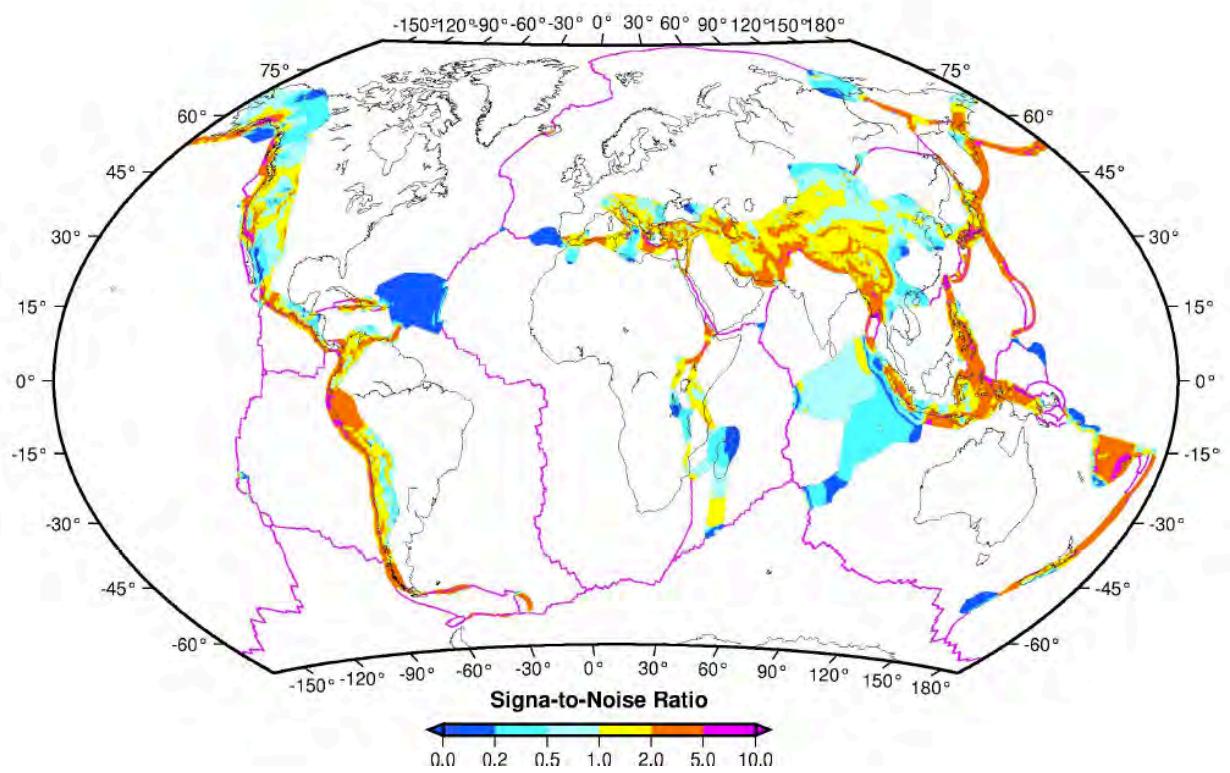


Figure 4.7 Contours of the signal-to-noise (results of Figure 4.5 divided by those in Figure 4.6)

5 Display and Archive of Data and Model

To dramatically show some of the GEM results around the globe, UNAVCO created and hosts a Google Earth representation of the GEM Strain Rate magnitude by images in a KMZ file, available online at http://gsrm2.unavco.org/images/GSRM_strain_magnitude.kmz (Figure 5.1). This Google Earth resource uses the tiling approach to show images of strain magnitude at progressively higher resolution as you zoom in towards the Earth surface. Images of GEM strain magnitude used in tiling, and the related logarithmic color scale, were created with UNAVCO's IDV visualization system (<http://facility.unavco.org/software/idv/idv.html>), which also made images for the GEM Strain Rate Model Project web site.

UNAVCO created, and hosts online, the "GEM GPS Velocity Viewer", available from the GEM SRM web site (Figure 5.2). This web tool shows the GPS velocity data and the user can control for map region and size, and for vector size, coloring , and decluttering. A user may also show the "error ellipses" for each station, a graphical depiction of data quality, and may show labels with information boxes for each station and its motion vector. GPS motion vectors can be defined relative to 53 reference frames, 50 of which are fixed plate reference frames, and additional frames are 1) a no-net-rotation reference frame, recomputed from the new model [after Kreemer and Holt, 2001; Kreemer *et al.*, 2006], 2) a frame that has the subasthenospheric mantle fixed [Kreemer, 2009], and IGS08 (the frame in which the original data was analysed).

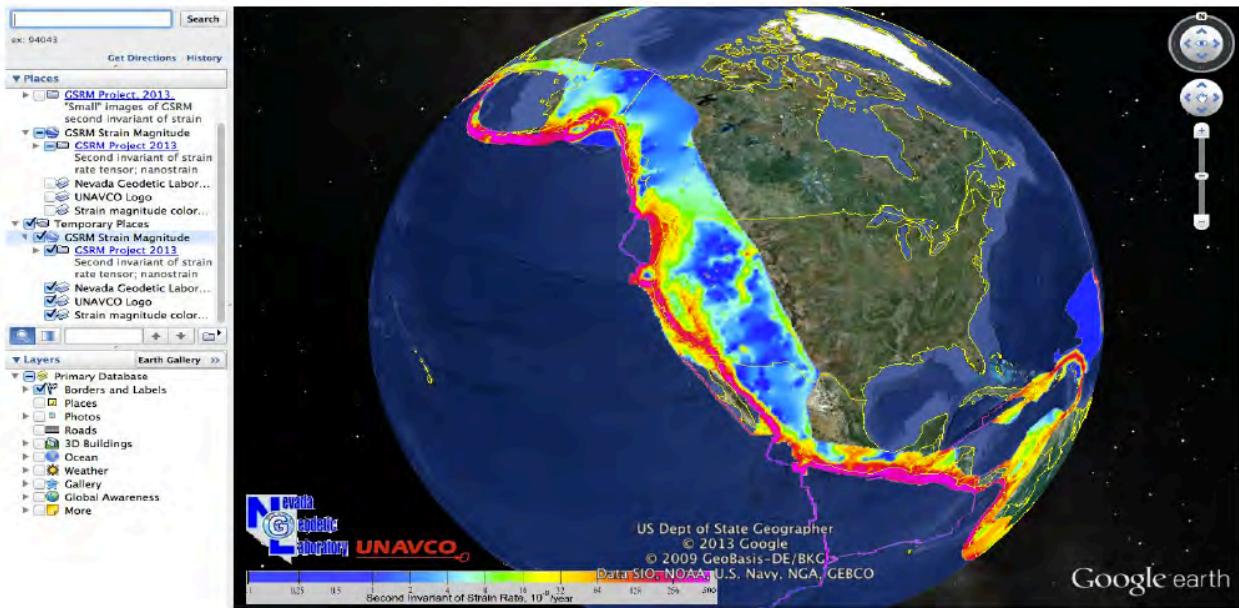


Figure 5.1 The GEM Strain Rate Model Project strain magnitude in Google Earth

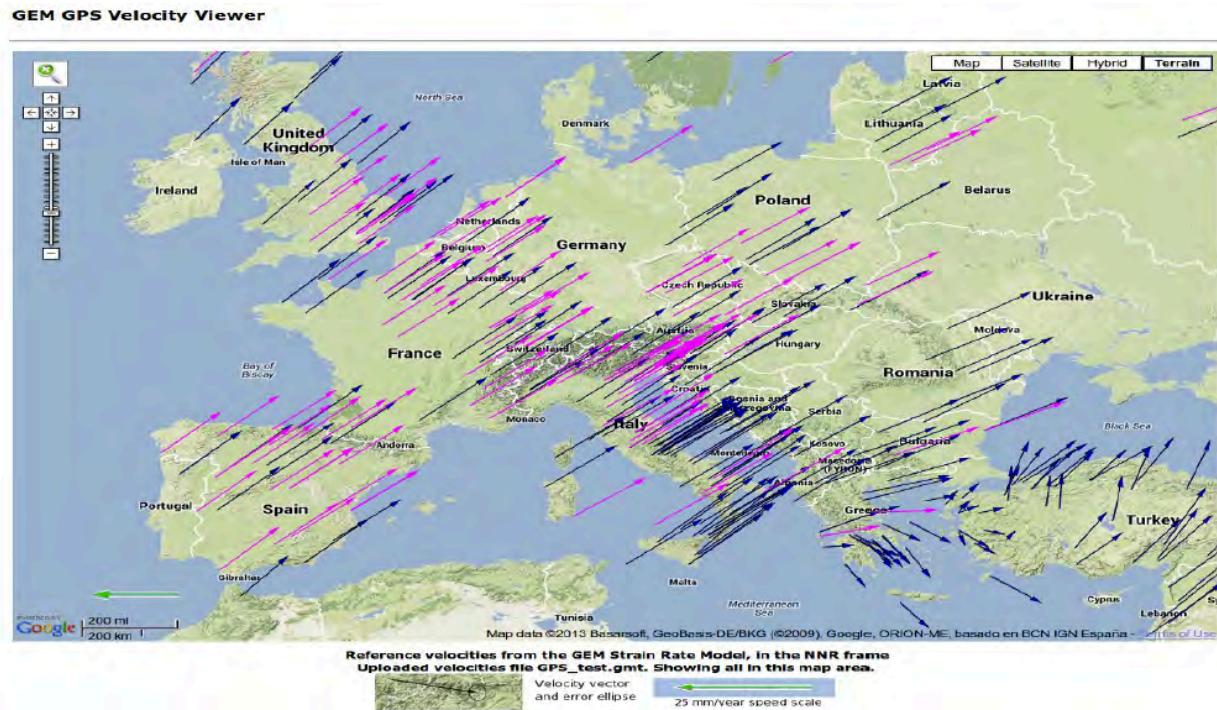


Figure 5.2 The GEM GPS velocity viewer map

The "GSRM GPS Velocity Viewer" also allows Earth scientists to upload a file with their own velocity data of station motions observations and plot vectors for them. This allows side by side comparison of their data with the GPS velocity data used in GSRM v.2. Users may optionally change their data from any of the 53 GEM Strain Rate project reference frames, to any other reference frame. This tool can quickly reveal important parallels of differing data sets, indicating either important Earth behaviour or detecting obvious errors in measurements of velocities.

The GSRM data and model files were reformatted for input to Generic Mapping Tools (GMT) routines, which constitute the underlying engine for map image creation for the Voyager tools. The GEM GSRM edition also required modification of the Voyager Java applet (which runs on the user's browser, if Java is allowed) and creation of the needed Perl modules on the UNAVCO jules servers needed to construct the proper GMT commands for map images, made on demand, which are sent back to the user's browser.

The options for the JVV GEM GSRM edition can be found here:
http://jules.unavco.org/Voyager/Docs/GEM_GSRM

For representation of the GSRM tensor field, the JVV GEM GSRM edition can display:

- the second-invariant of the strain rate tensor
- the principal strain axes
- the vertical strain rate, $E_{zz} = -E_{xx} - E_{yy}$
- the strain style; for key, see:
- http://jules.unavco.org/Voyager/Anc/GEM_GSRM/strain_rate_style
- a "scaled" strain style, weighted by the second-invariant of the strain rate

Note: Currently, the JVV interface is a Java applet requiring the user to be using Java 6, not Java 7.

6 Concluding Remarks

GSRM v.2 is a vast improvement over GSRM v.1.2 in terms of data input and model resolution. However, only at a few places is the data input sufficient to obtain well-constrained strain rates at the resolution of the underlying grid. In the future we hope to use a dynamic grid that has the grid size adjusted to the station spacing, so that no computational power is wasted and no high-resolution model is pretended at places where the data are insufficient. However, we also hope that the recent surge in GPS data densification continues. About half of all studies included in our compilation were published since 2010 and the time-series of thousands of CGPS stations will mature over the next few years.

Some areas with great data coverage (western Europe, central and eastern U.S.) are currently not modelled. The main reason being that the strain rates there are expected to be at or below the uncertainty in the GPS velocity data. Furthermore, adding those regions to the area for which strain rates are currently modelled would add a significant computational burden. Hopefully in a future iteration of the GSRM, we can include those areas.

There are still many areas with insufficient GPS coverage surrounding important seismogenic faults, let alone unknown faults. This situation may not change for a long time, yet knowledge of the strain accumulation rate across these faults is essential to assess their activity rate. A potential solution in improving the spatial resolution in areas with limited GPS coverage is the use of InSAR. Most recent developments have been on using GPS to help improve the resolution and usefulness of InSAR maps of strain accumulation [e.g., *Wei et al.*, 2010; *Tong et al.*, 2013], however these improvements really only lead to images of the deformation in the direction of the line-of-sight (LOS) of the satellite. The main problem lies in 1) the ambiguity in the 3D velocity vector that can explain the LOS velocity, and 2) the fact that the LOS is insensitive to velocities along the direction of the satellite track. Therefore, InSAR alone can never recover the velocity gradient tensor field needed to determine the strain rate. However, recent advances have shown strain rate fields from a combination of GPS and InSAR data [*Wang and Wright*, 2012].

It is our hope that GSRM will directly contribute to GEM's goals through the creation of earthquake activity rate maps. The previous GSRM was used to make such maps [*Bird et al.*, 2010], and new results based on the new GSRM are in development. Another contribution of the new GSRM is in assessing the correctness of the moment rate budget implied by GEM's Faulted Earth model. Indeed, we envision a future GSRM that is not only consistent with the GPS velocities, but also satisfies the geologic and seismologic data in terms of the spatial distribution of strain rate. This could be done by using the fault slip rates and earthquake rates as *a priori* estimates of the strain rate variances when inverting the GPS velocities.

Finally, some recommendations for those collecting GPS data and who would like to see their results included in future models:

For campaign measurements:

- Time-series length >3 years
- Each campaign several 24 hour sessions
- Each campaign held at approximately same time of year
- Velocity uncertainty should be “reasonable” and not the formal, white-noise, uncertainty
- Provide the time-span, useful to assess the possible effect of earthquakes

For continuous measurements:

- Time-series length >2.5 years
- Velocity uncertainty should be based on time-correlated noise model
- Also provide vertical velocity, which would help identify hydrologic effects
- Provide the time-span, useful to assess the possible effect of earthquakes

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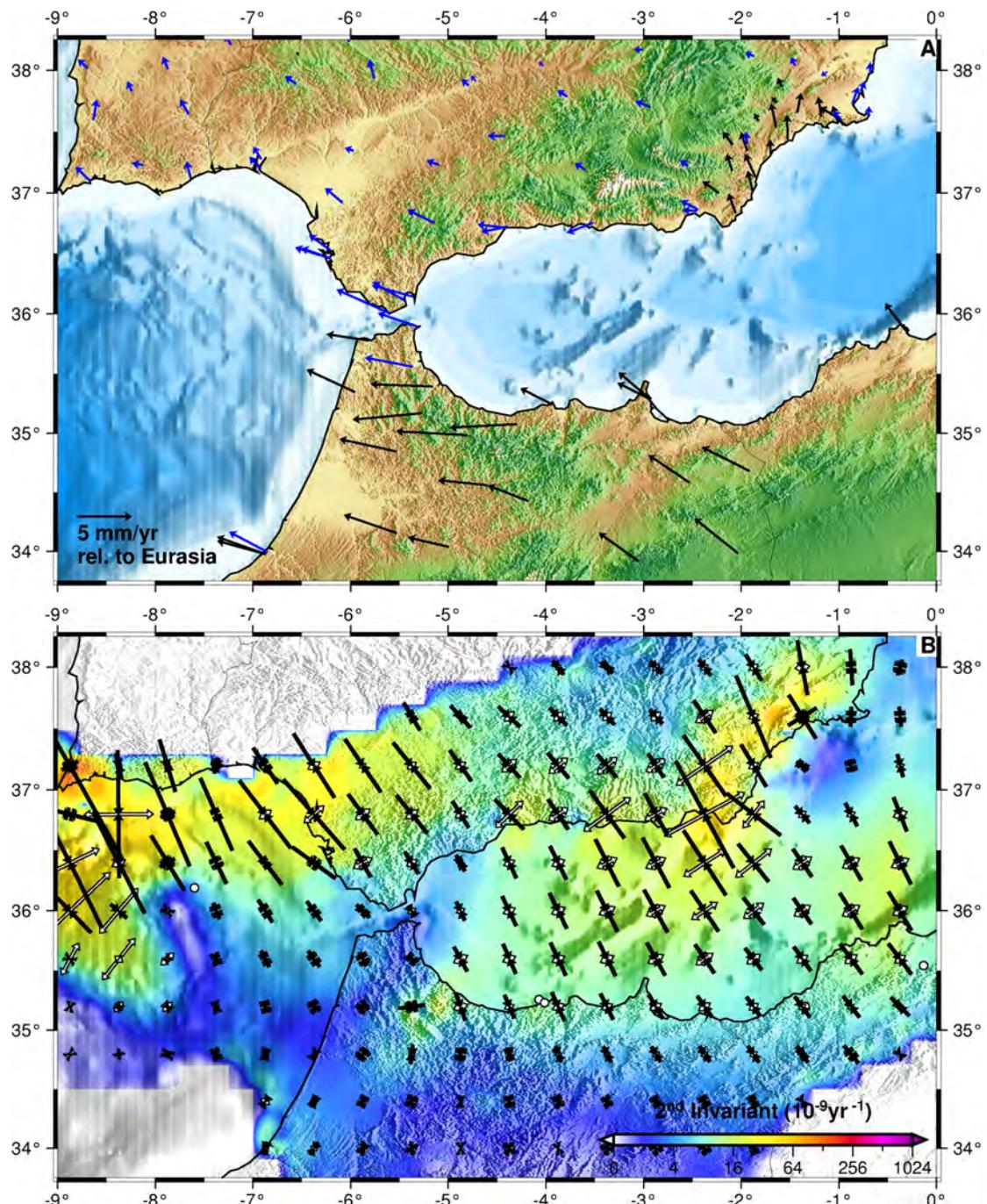
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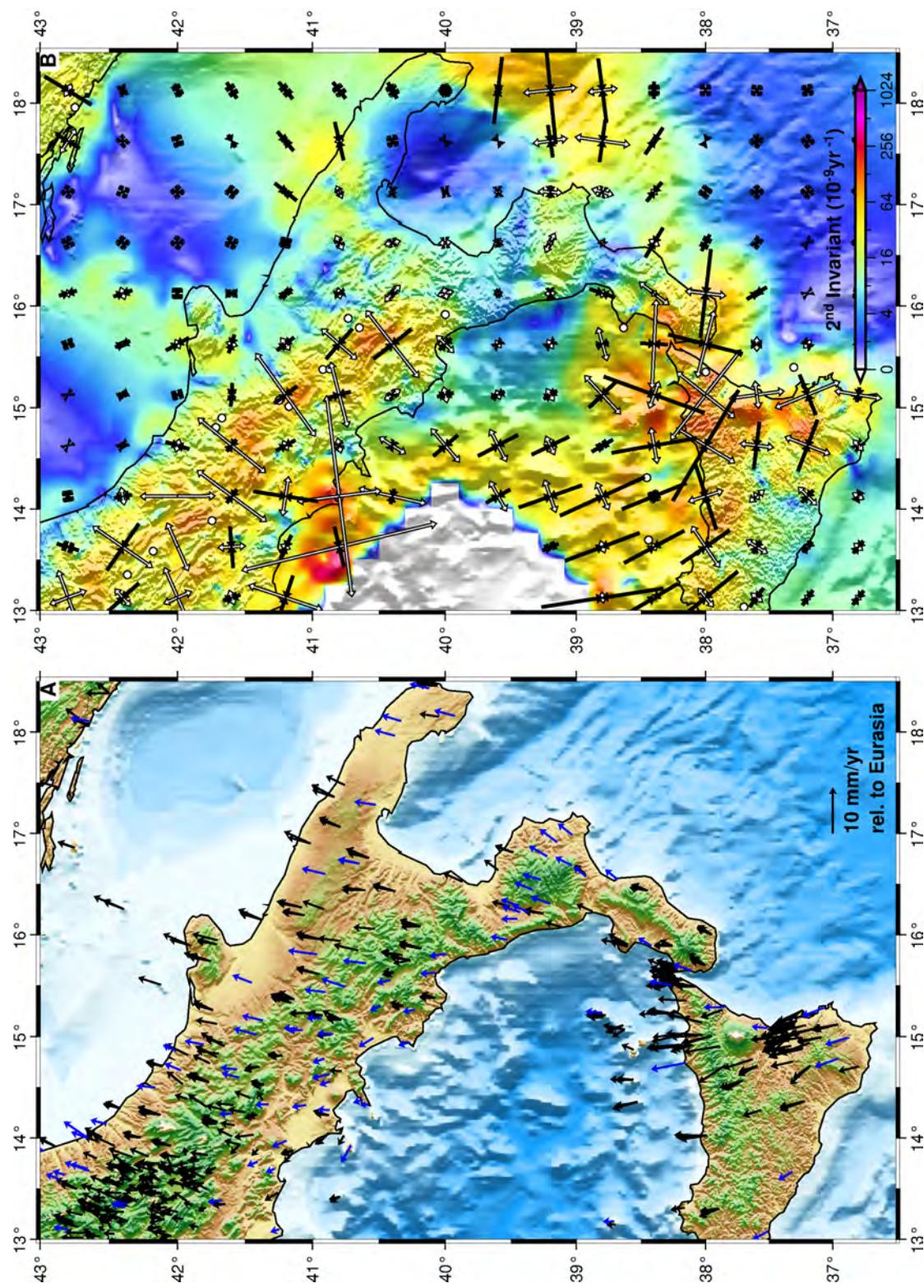
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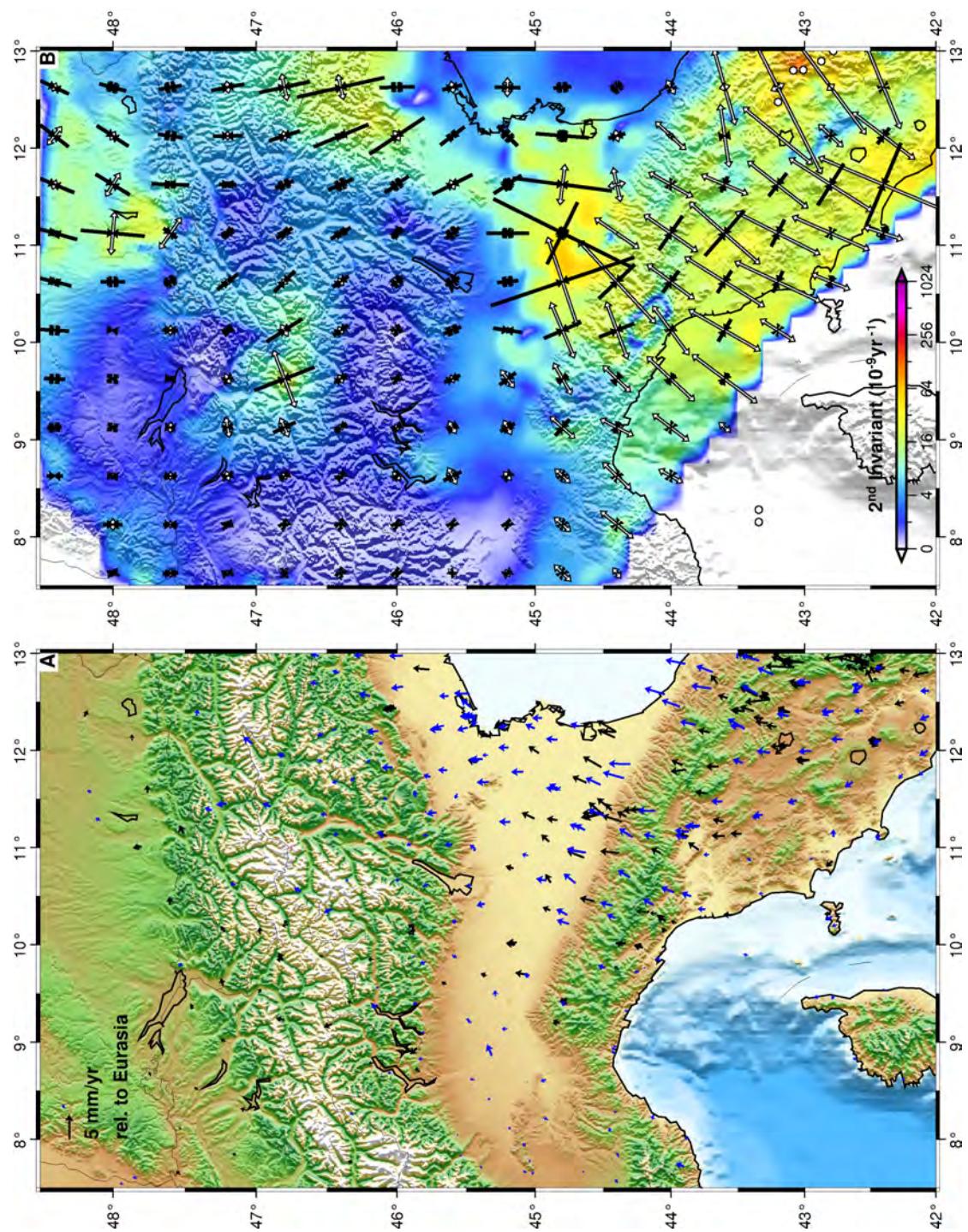
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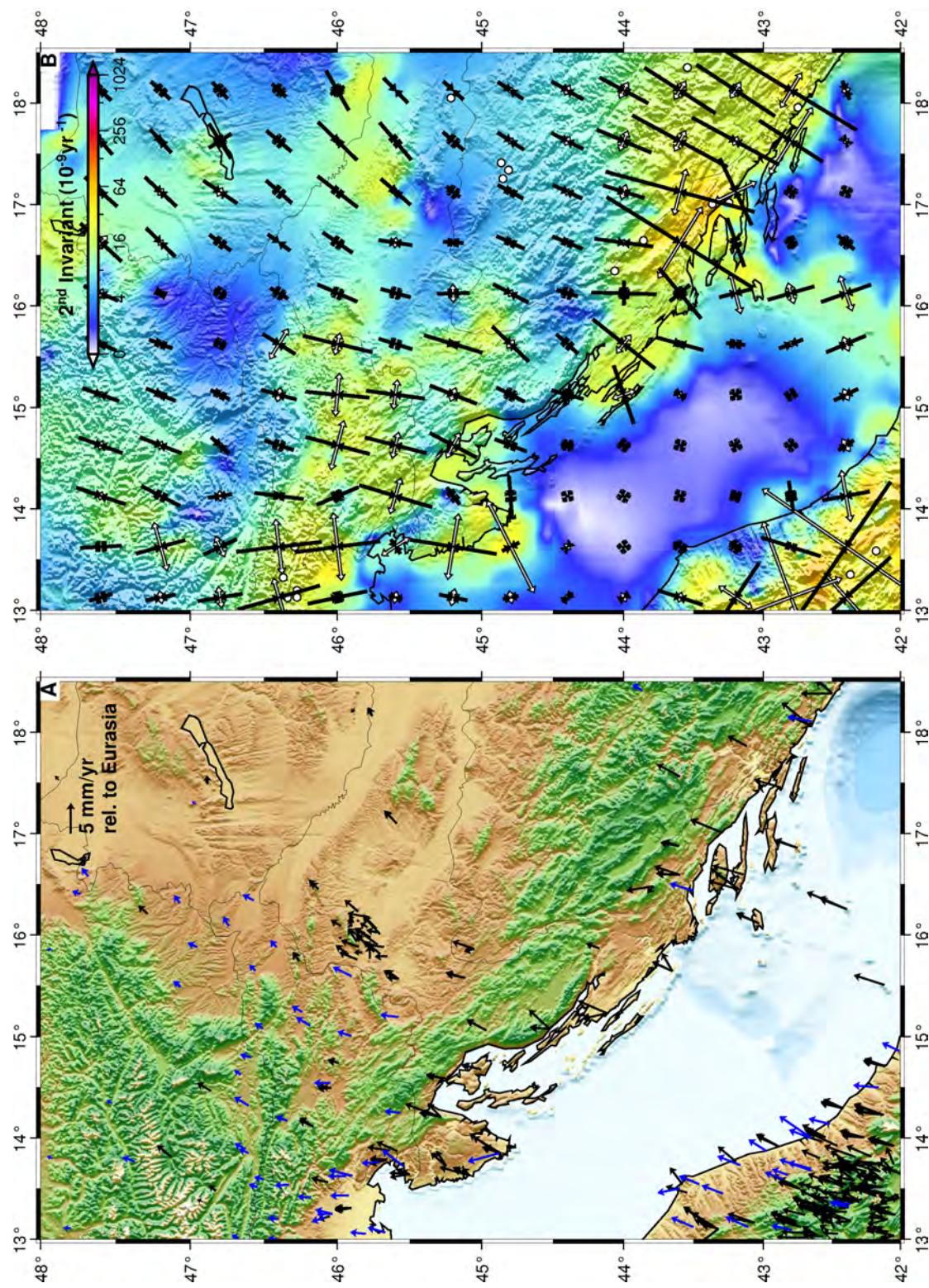
APPENDIX A Figures with Regional Results

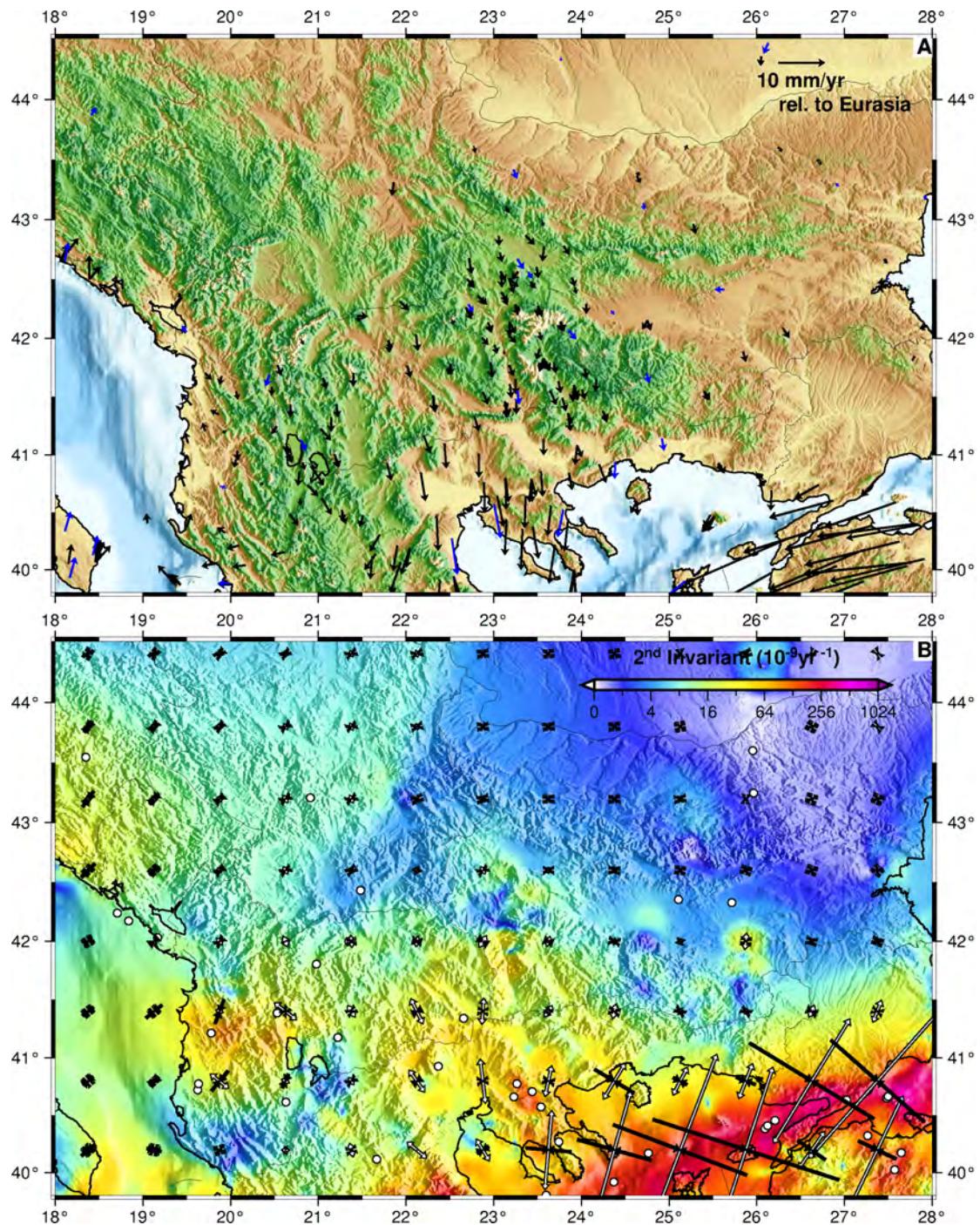
a) GPS velocities in regional reference frame (indicated in legend). Blue velocities are derived in this project, black velocities are from the literature. b) Contour of second invariant of modelled strain rates. Black and white vectors are the average contractional and extensional principal strain rate vectors, respectively, for sampled grid cells (scaled relatively to the highest principal values shown in plot). Open circles are epicentres for all events in ISC-GEM catalogue with depths ≤ 70 km [Storchak *et al.*, 2012].

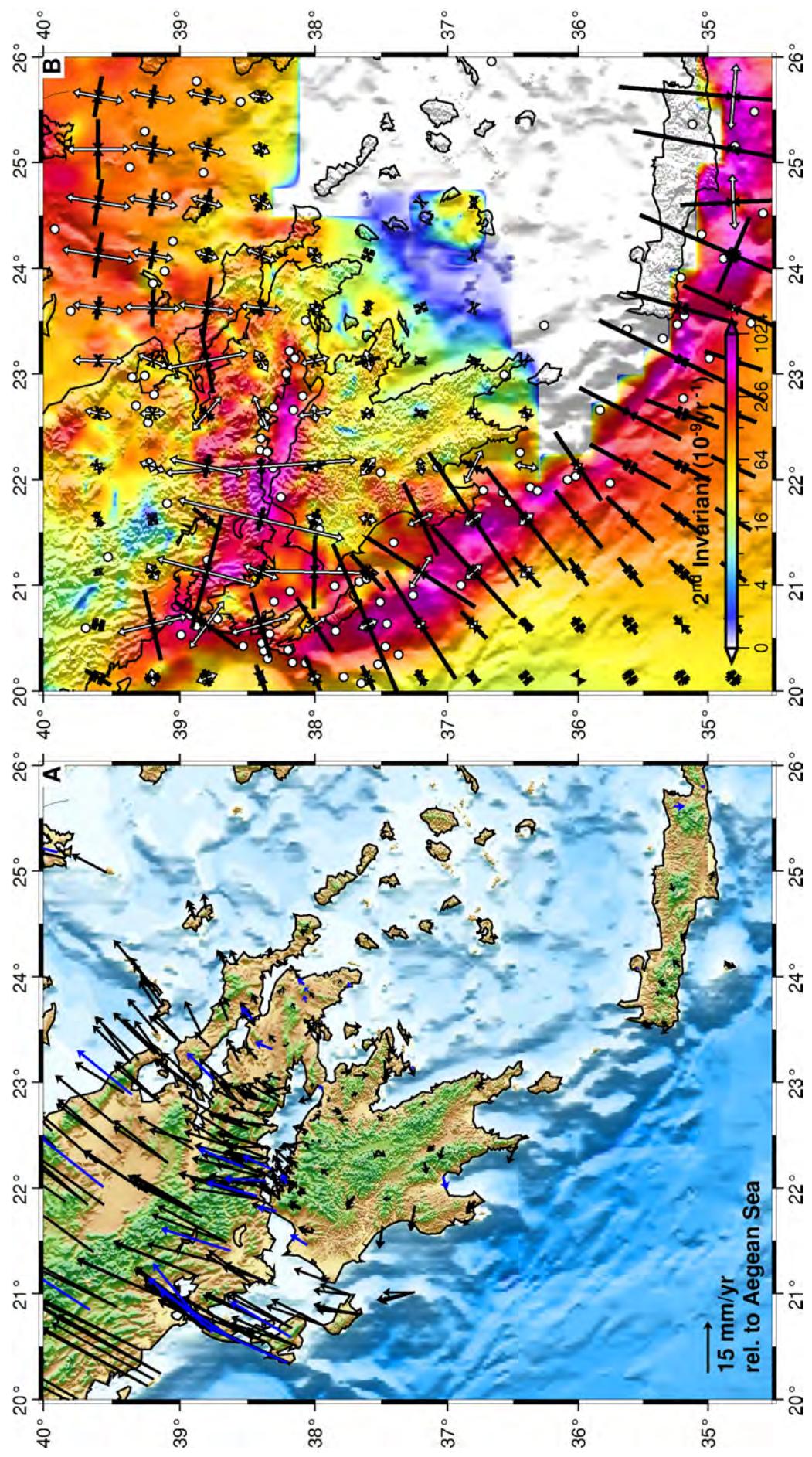


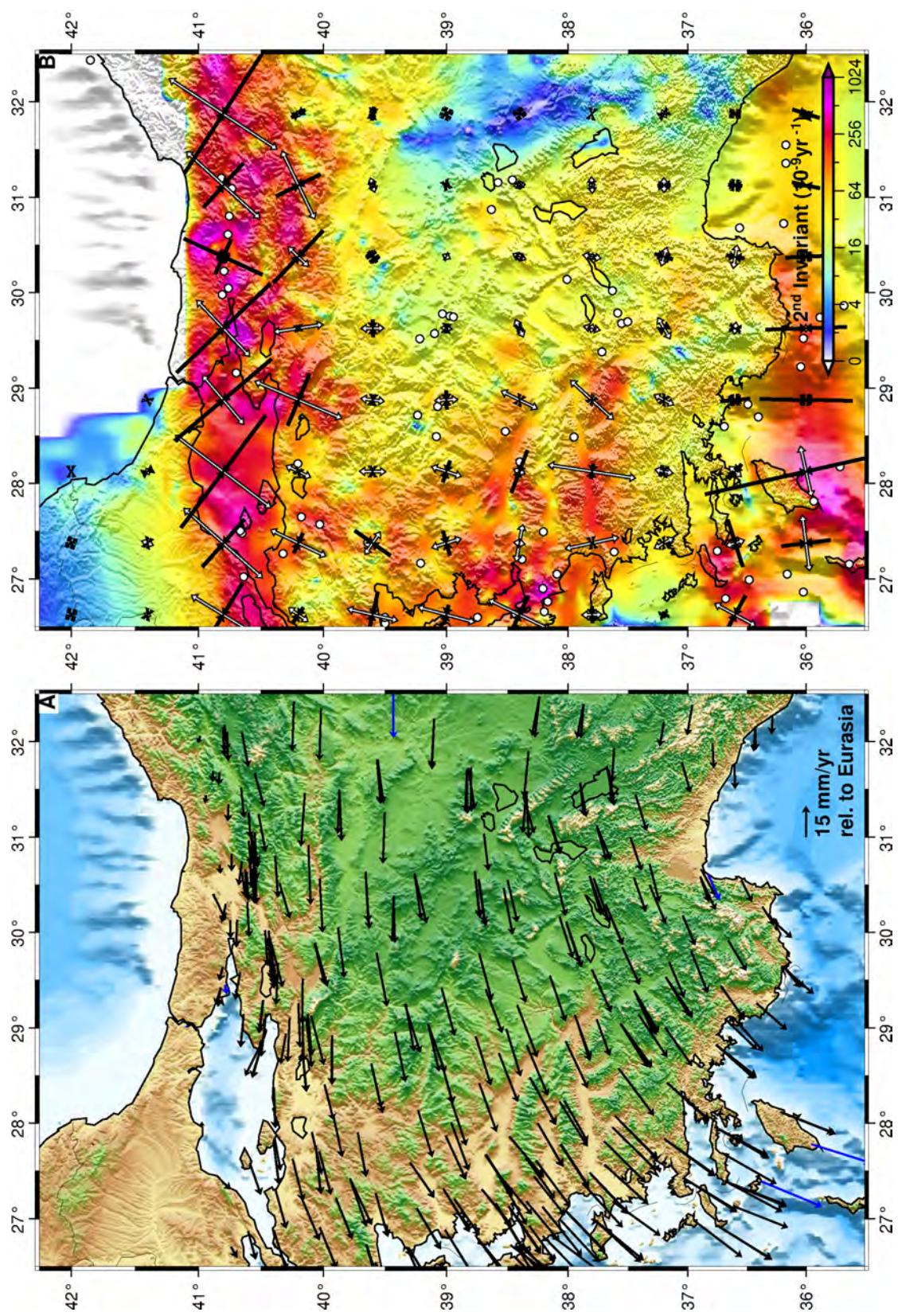


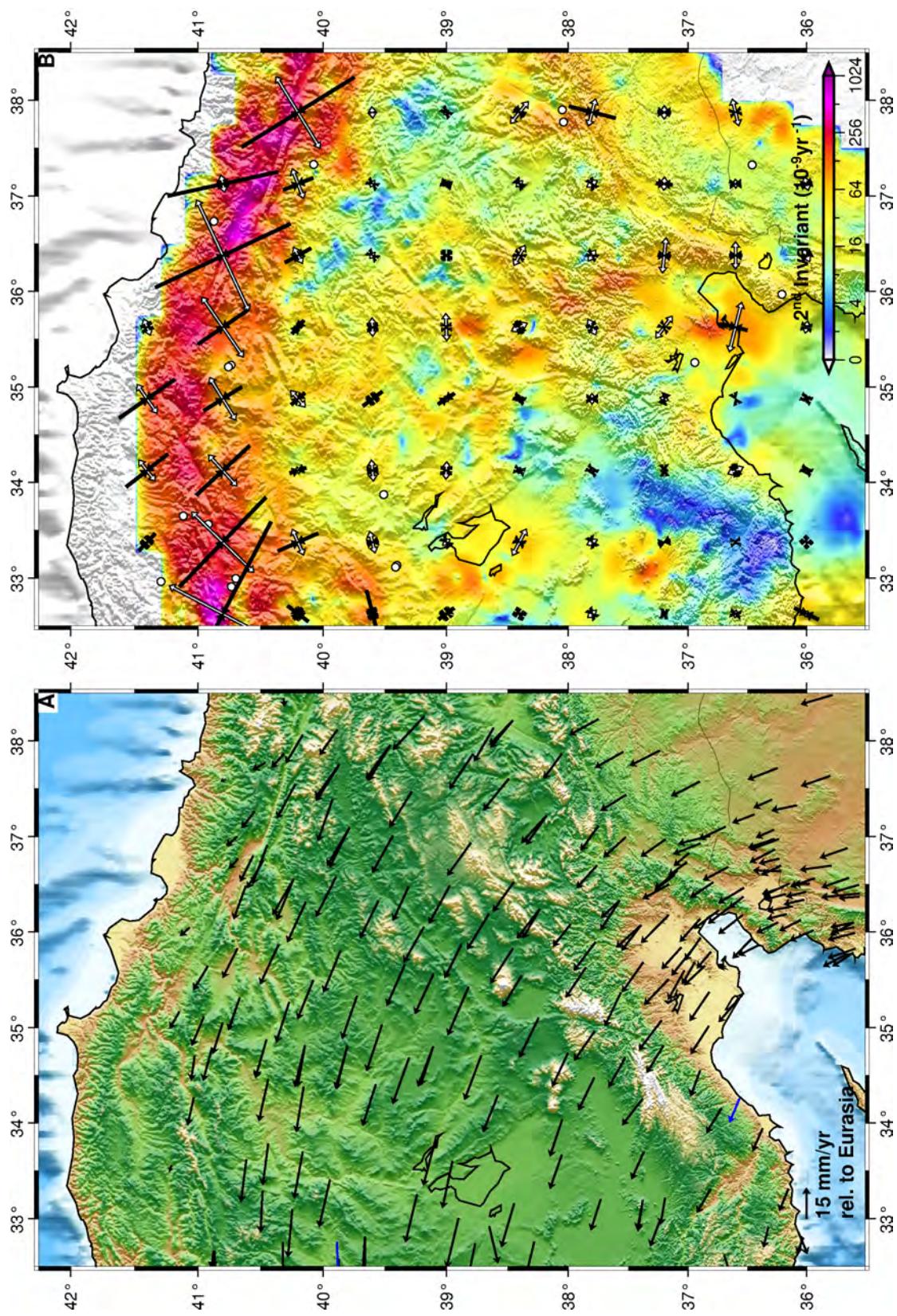


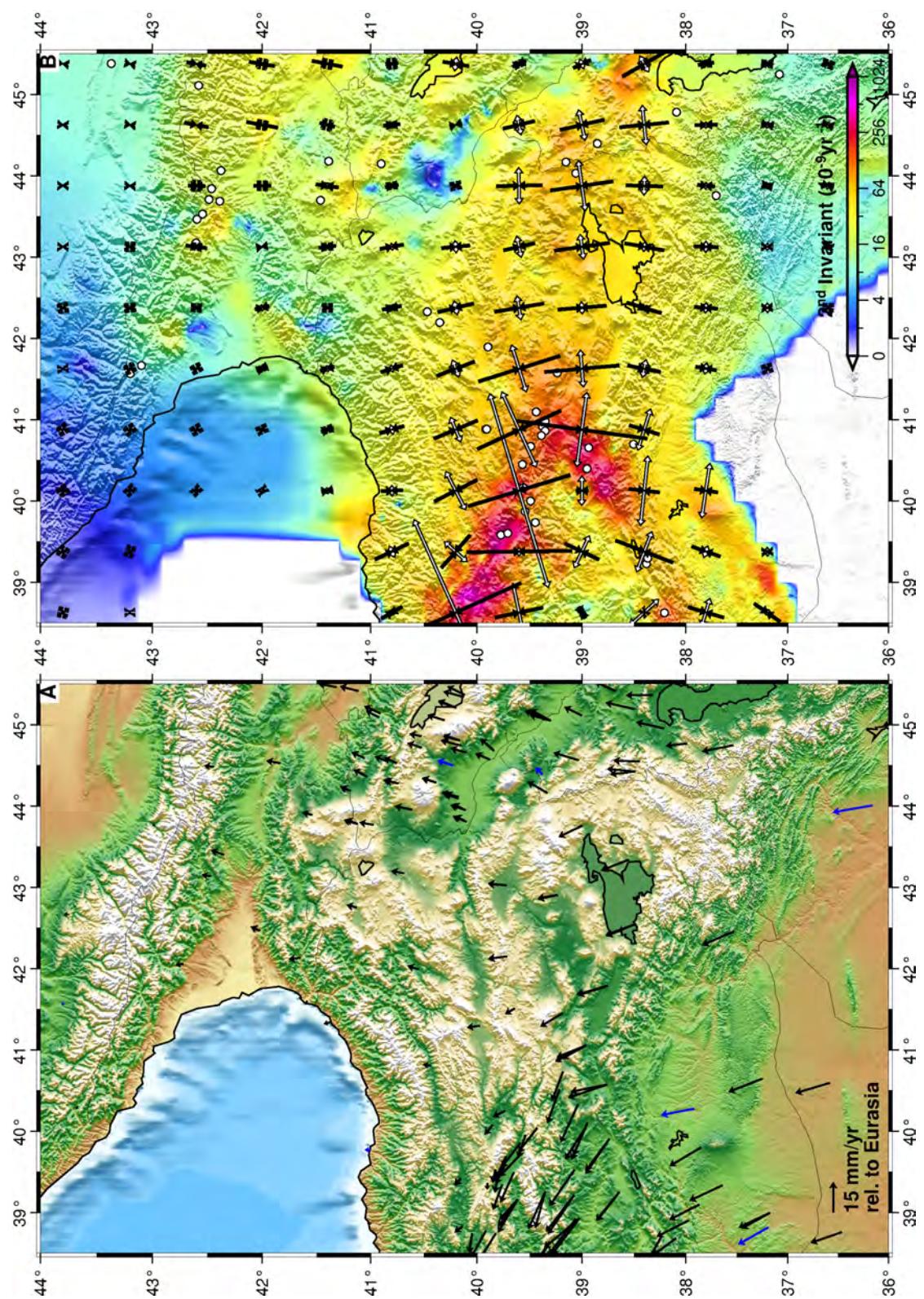


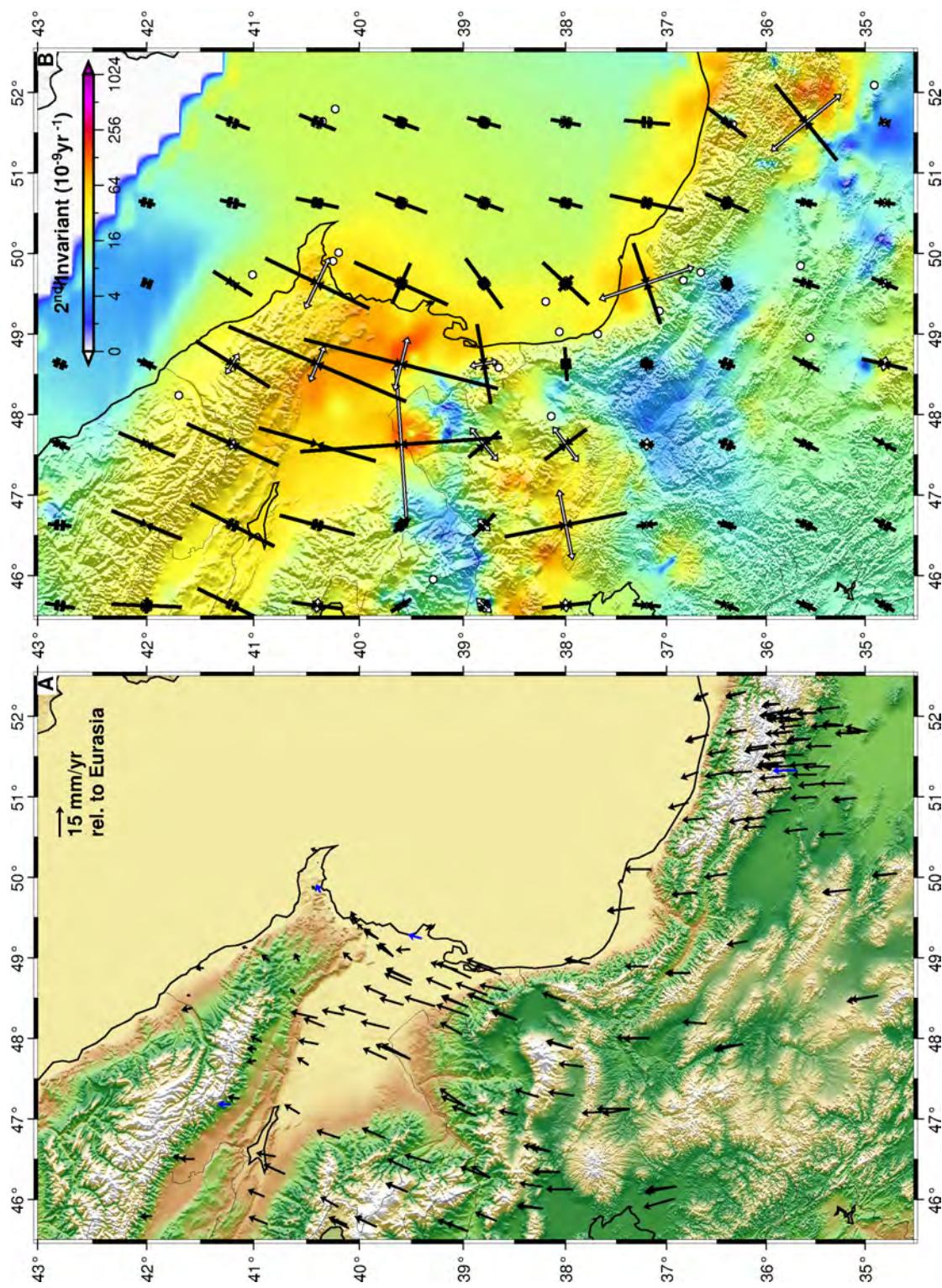


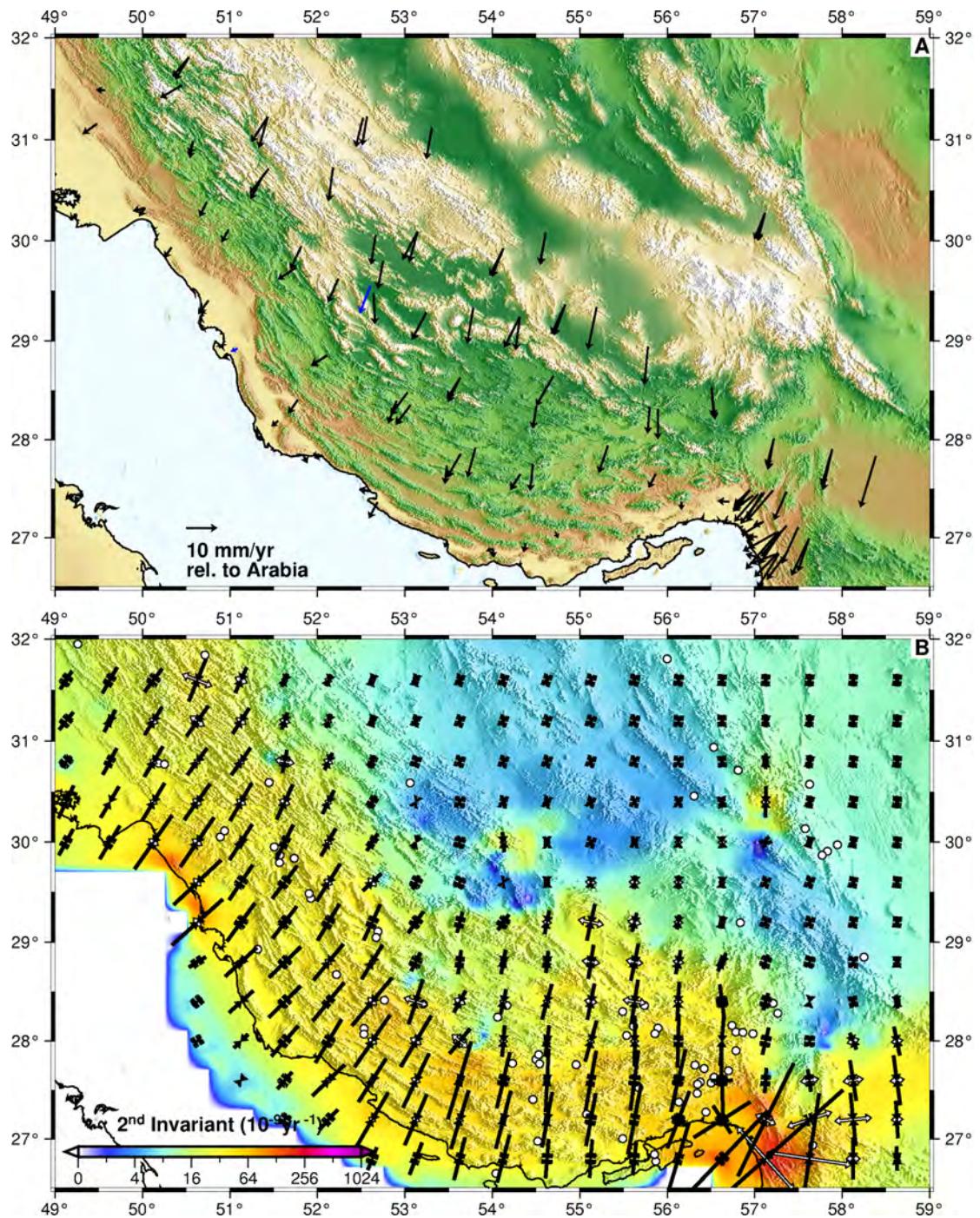


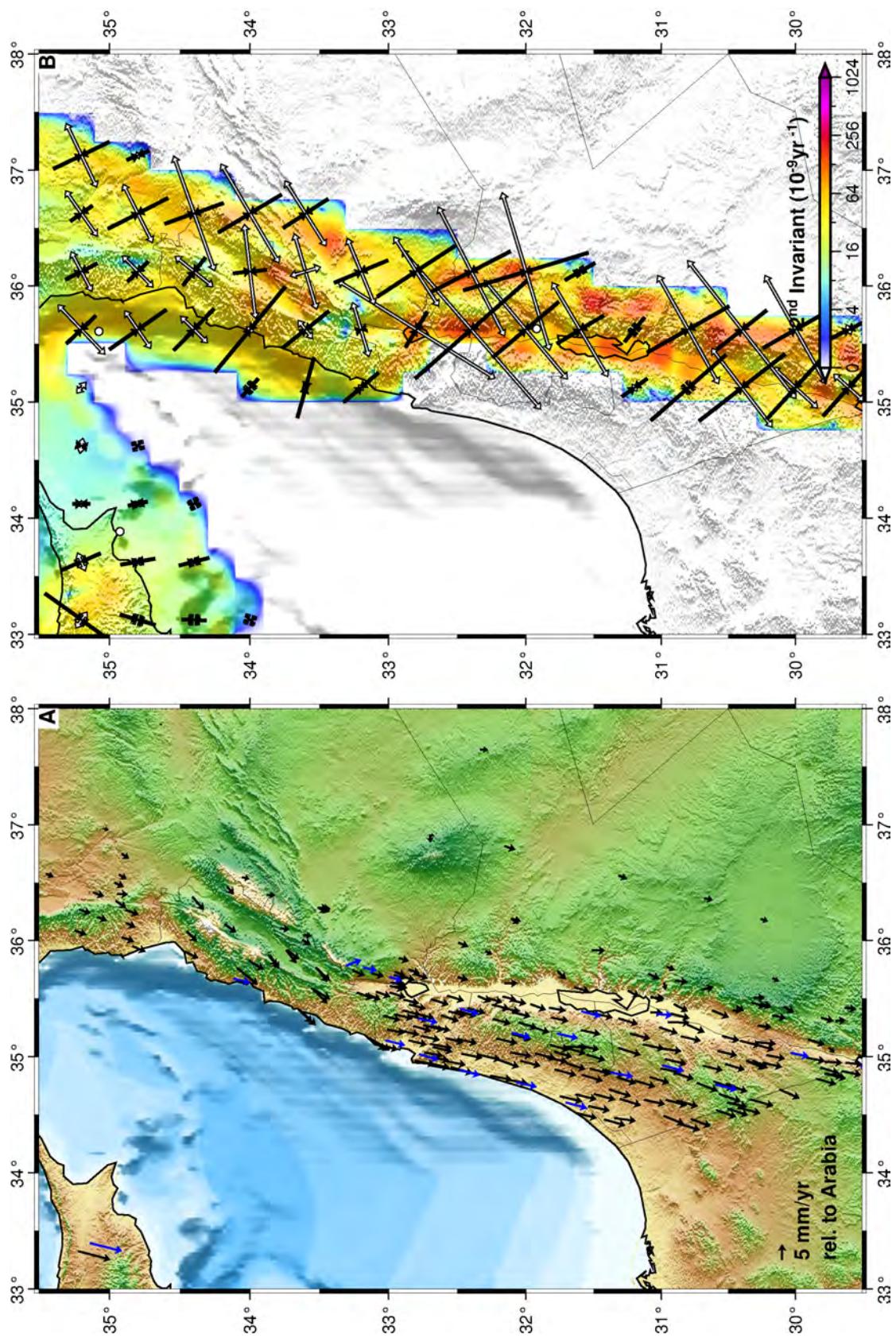


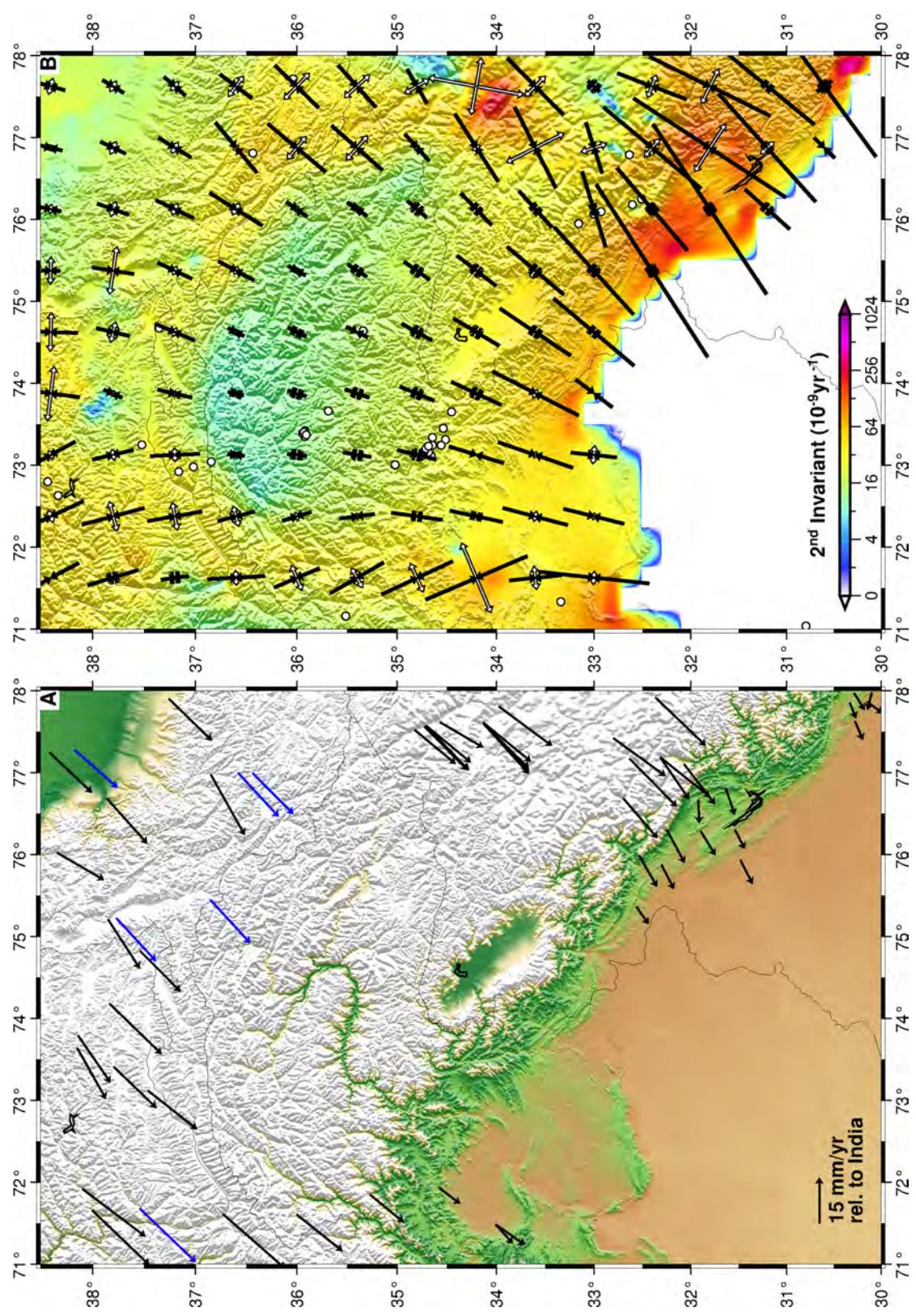


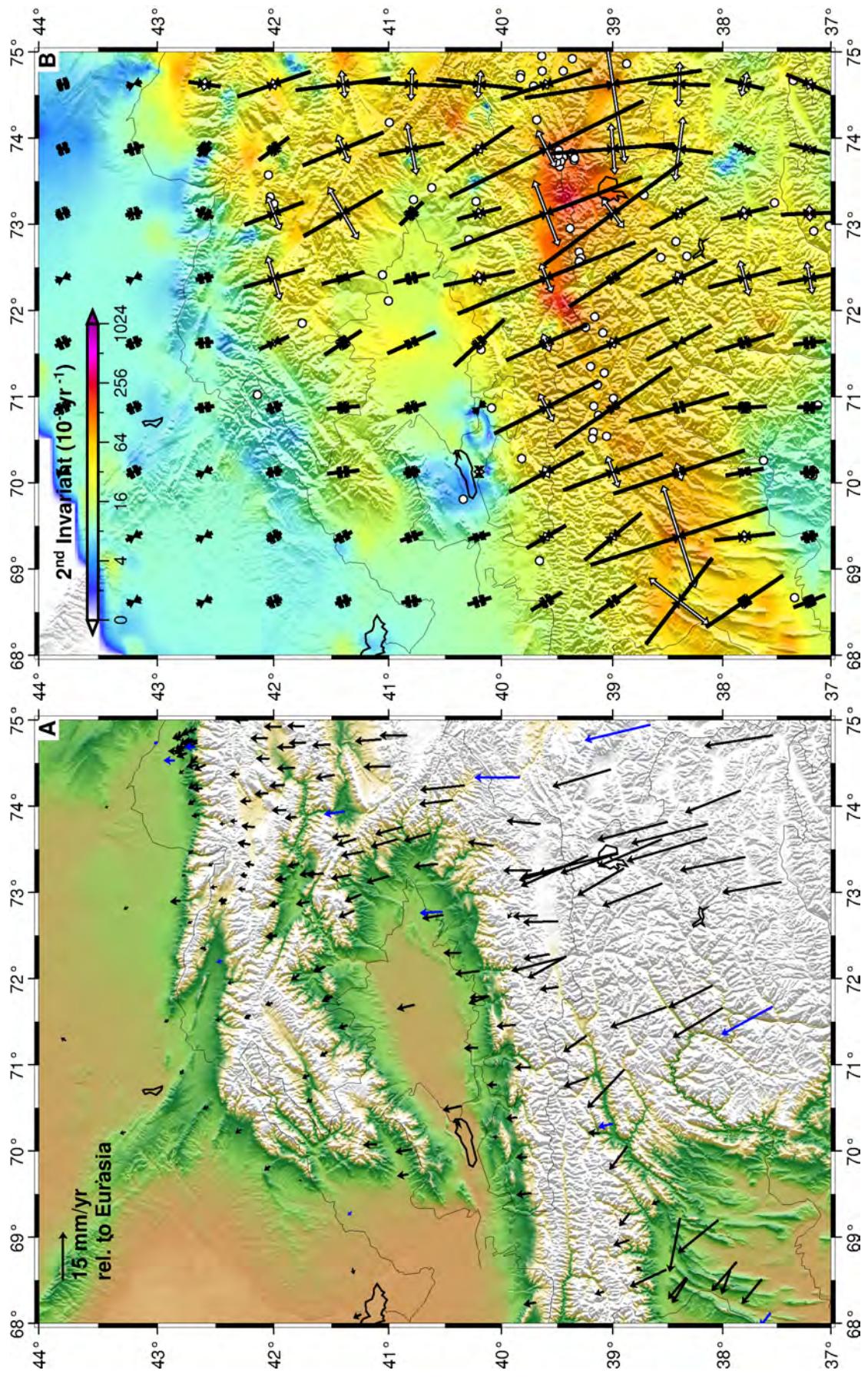


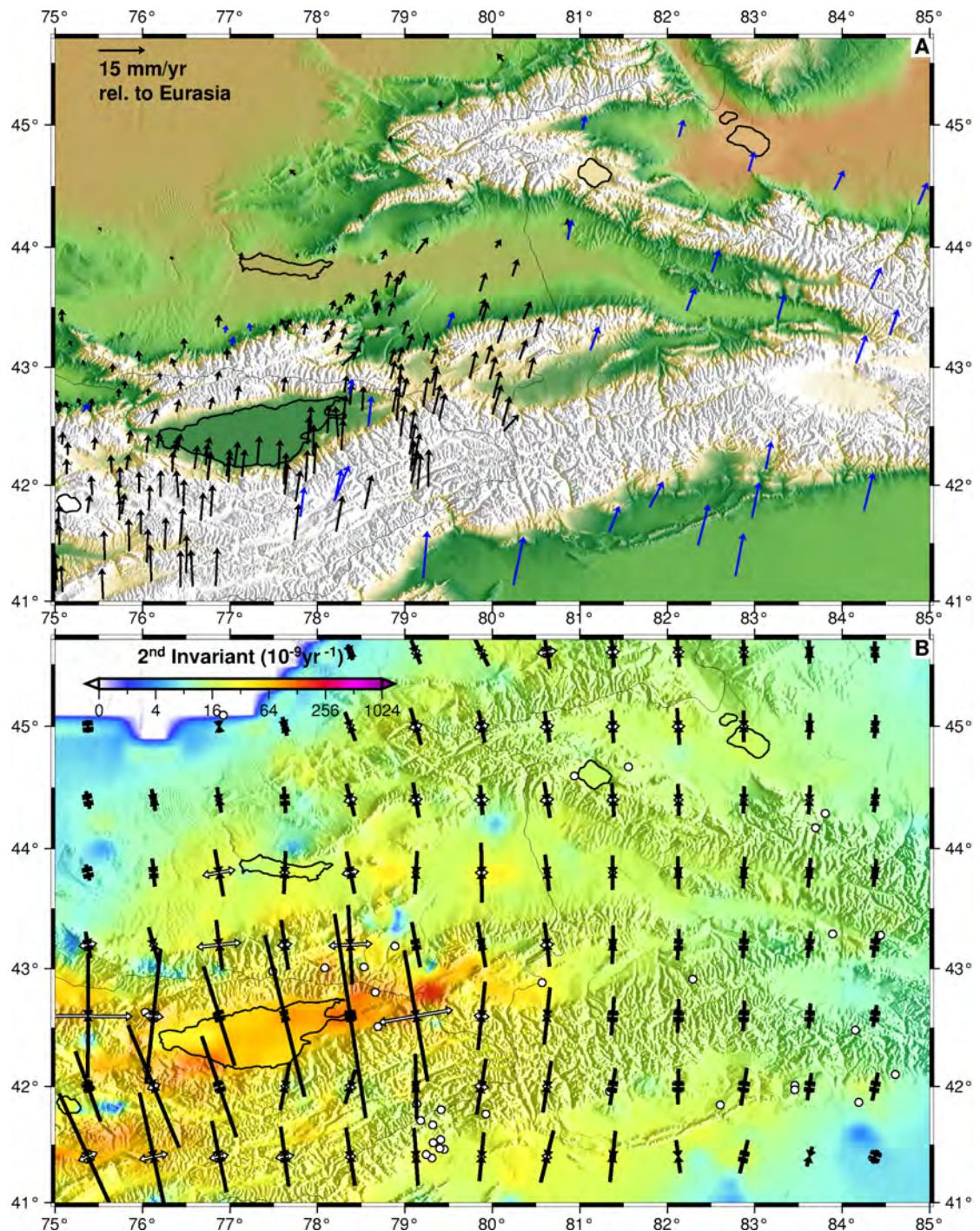


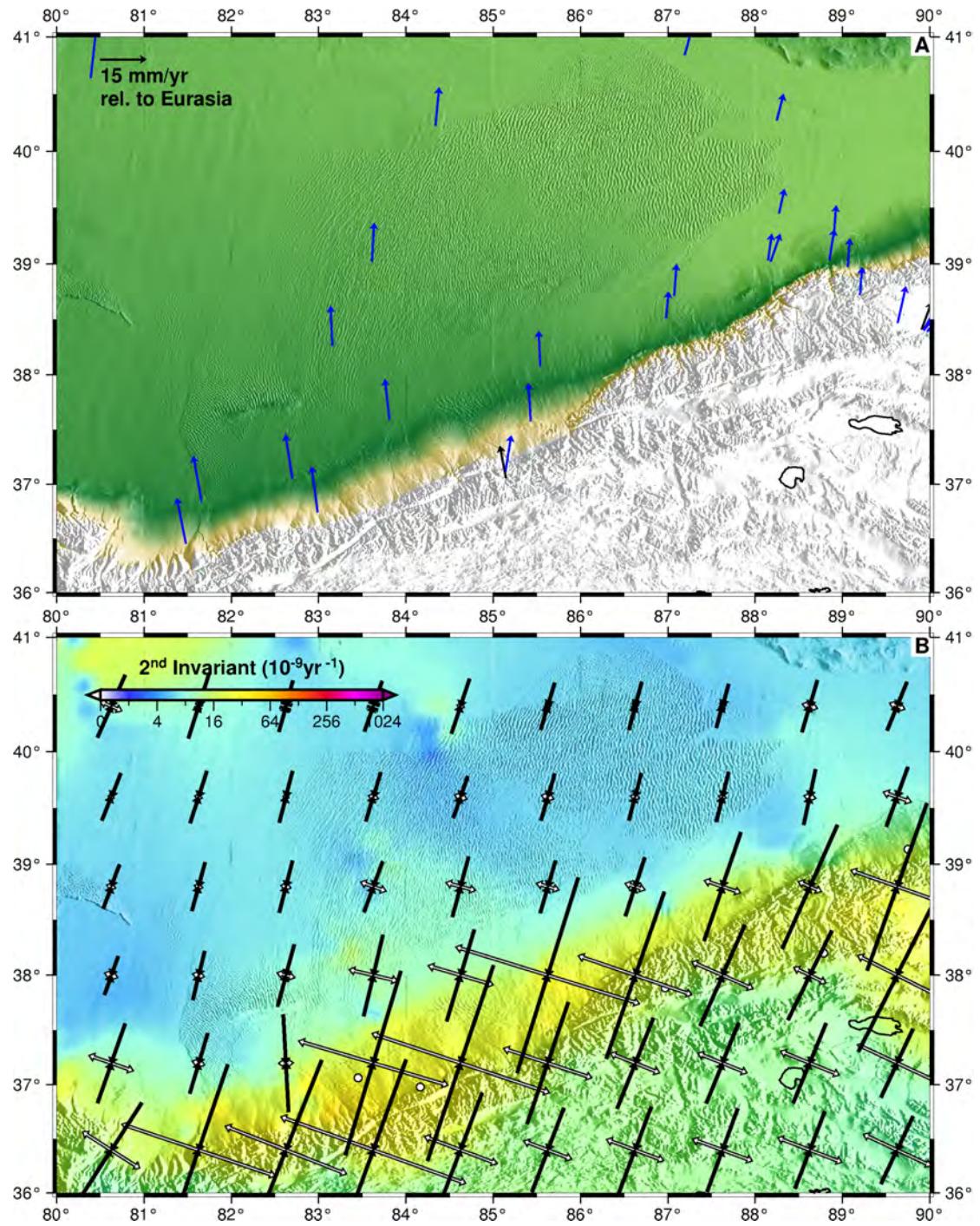


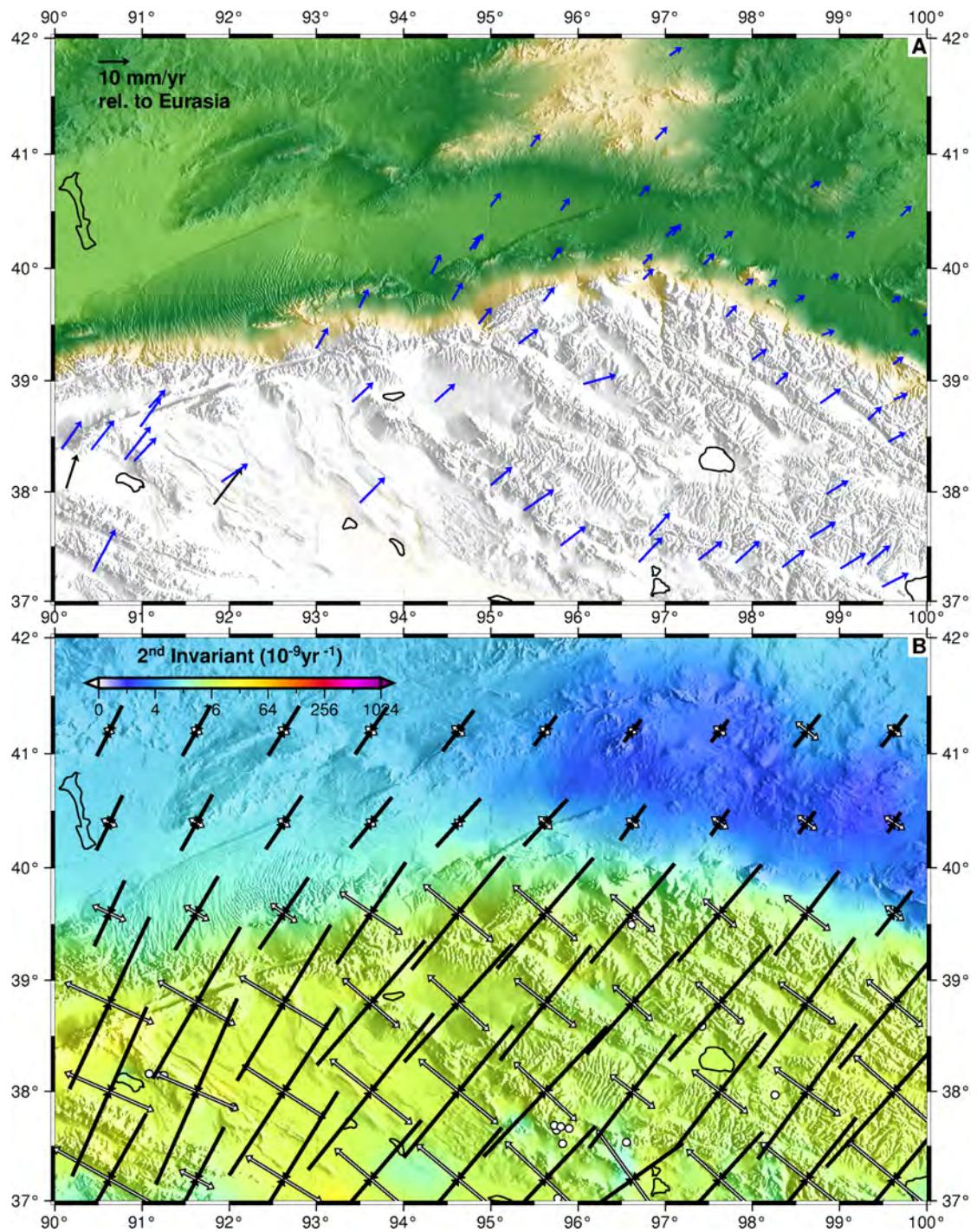


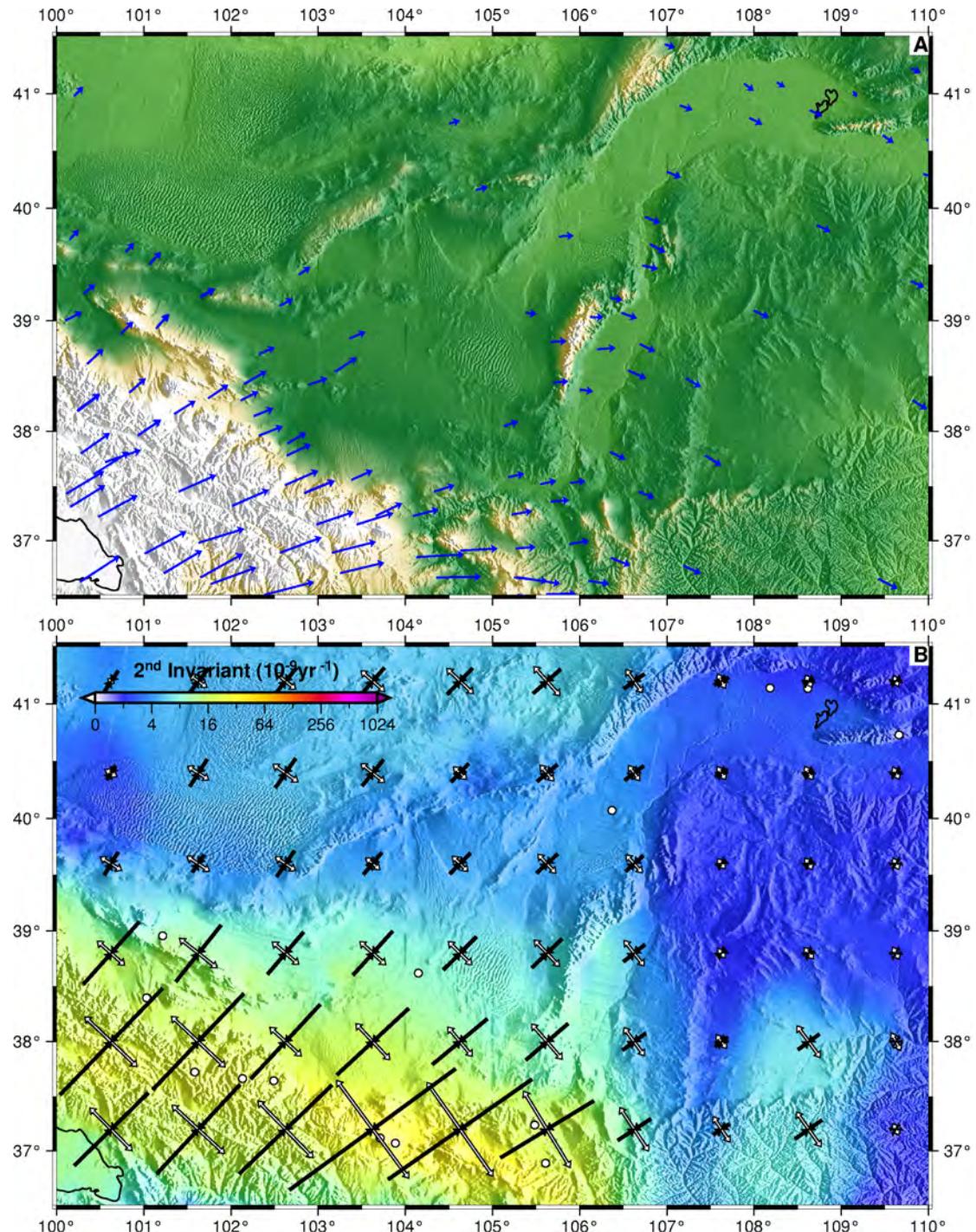


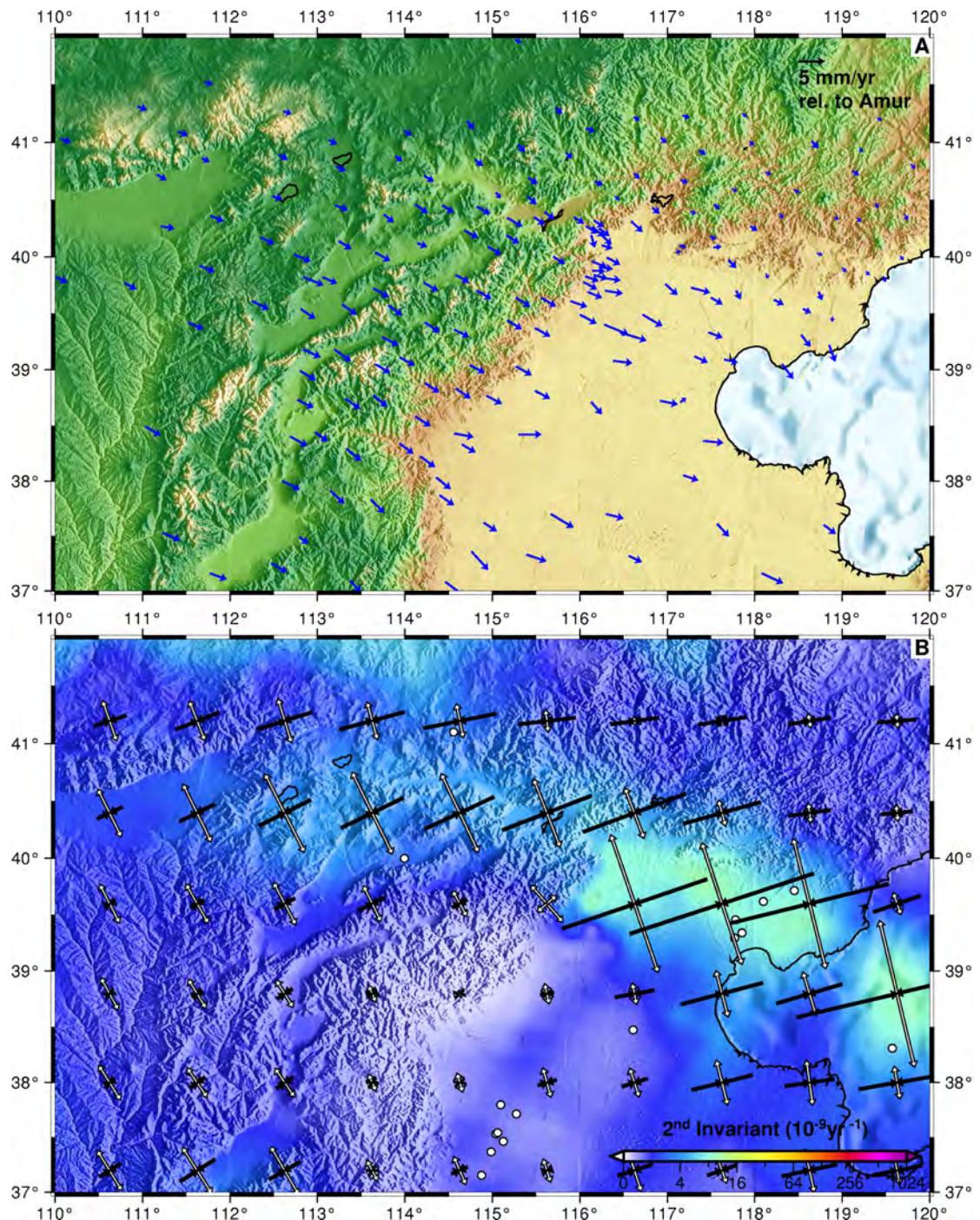


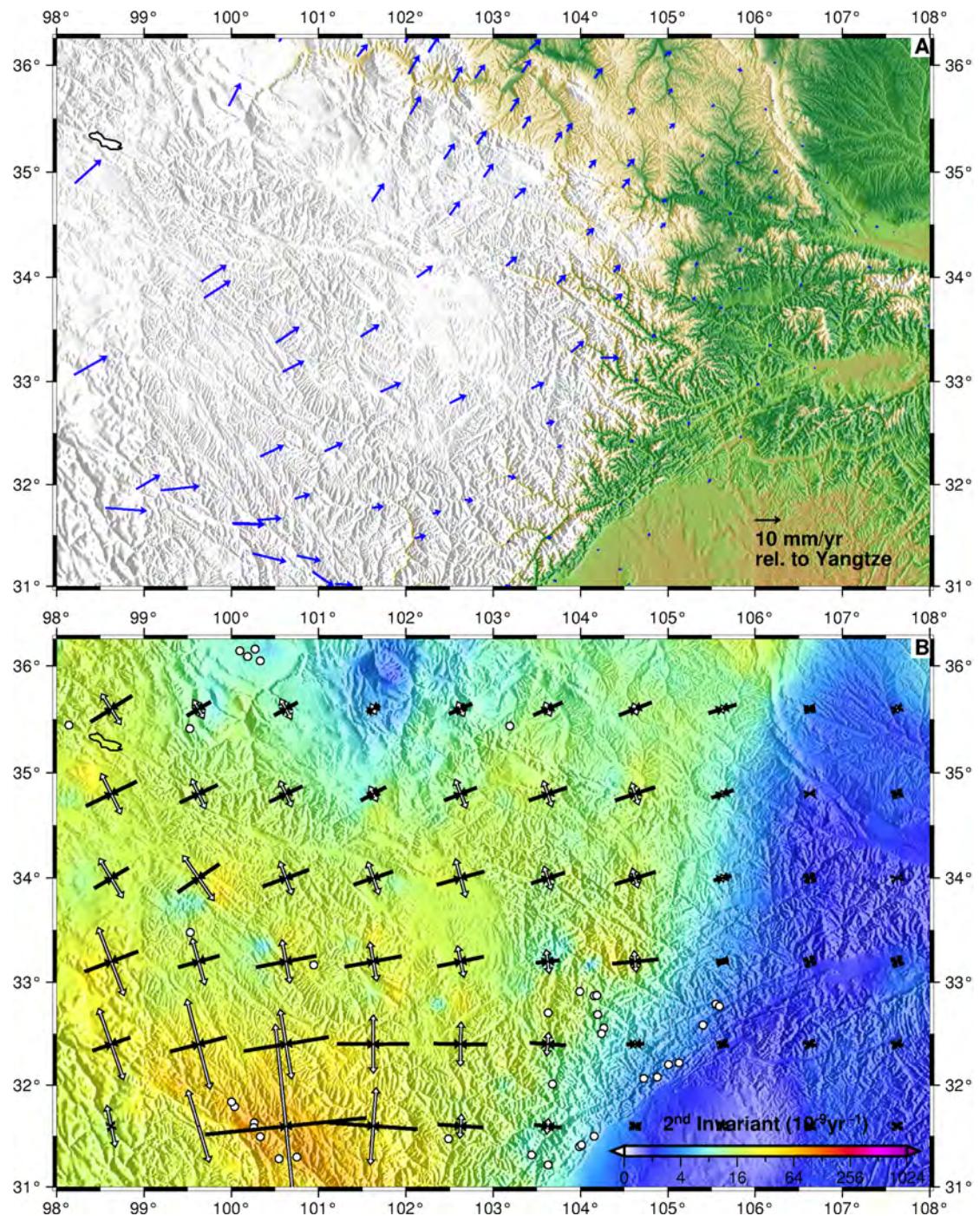


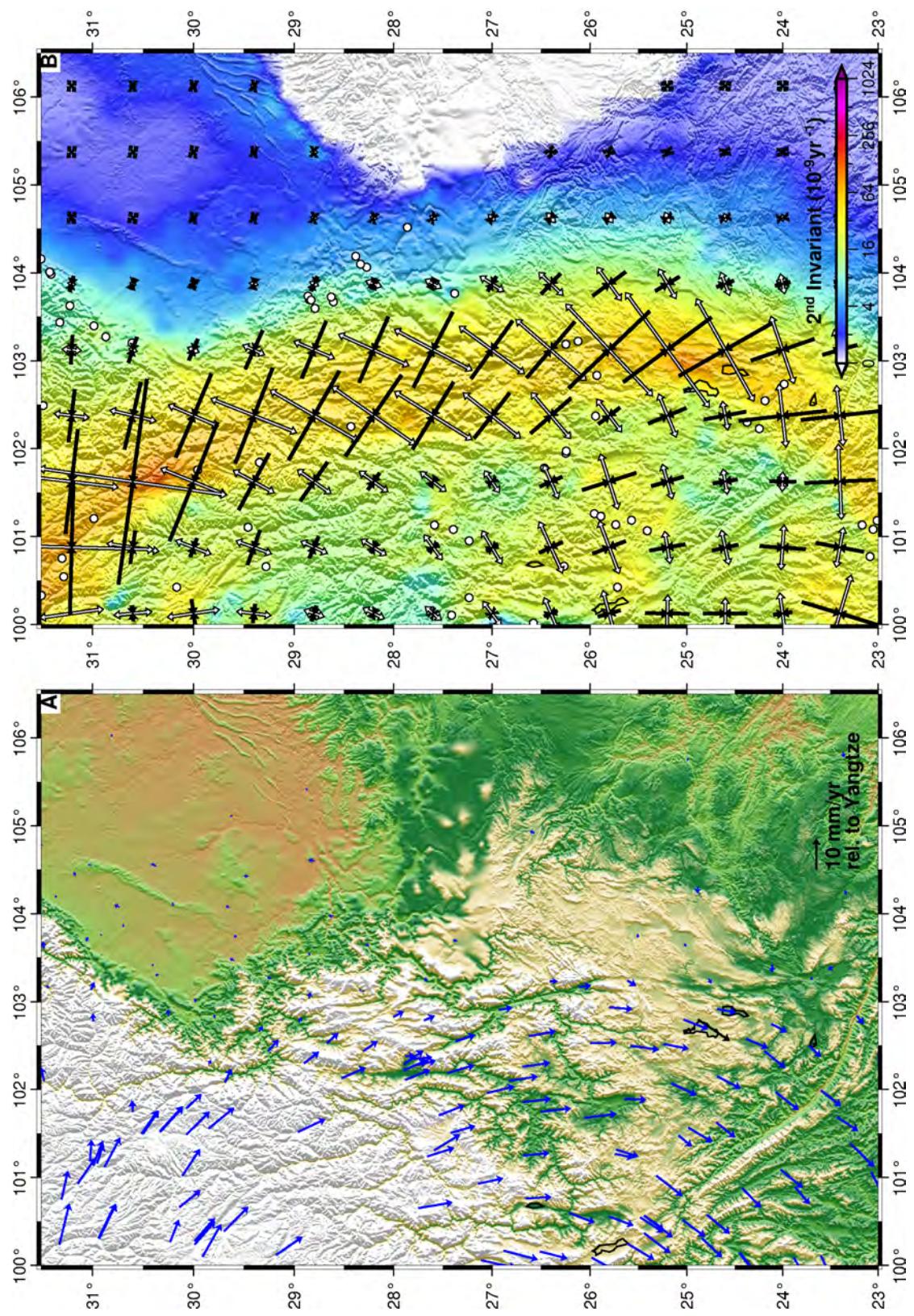


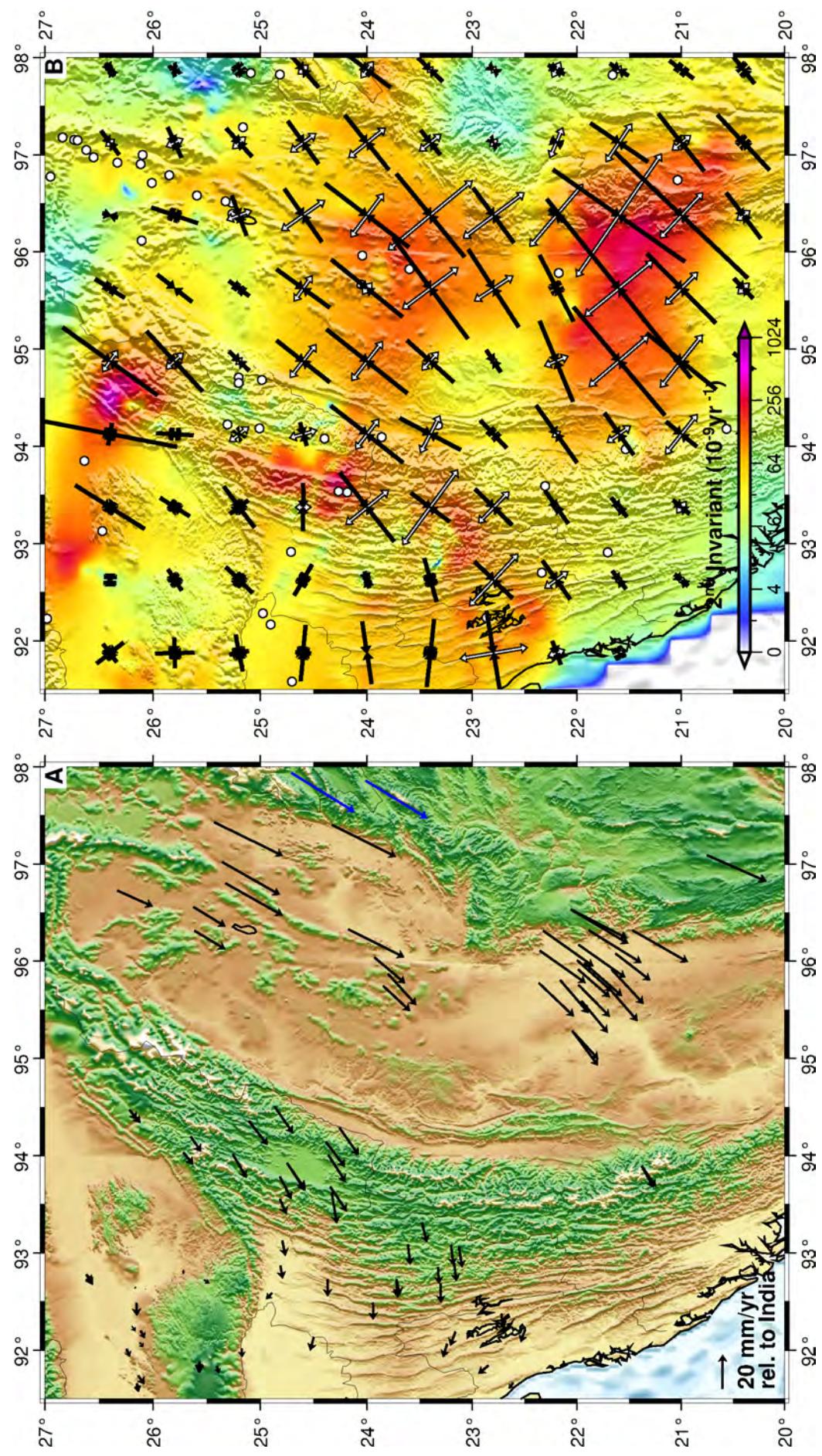


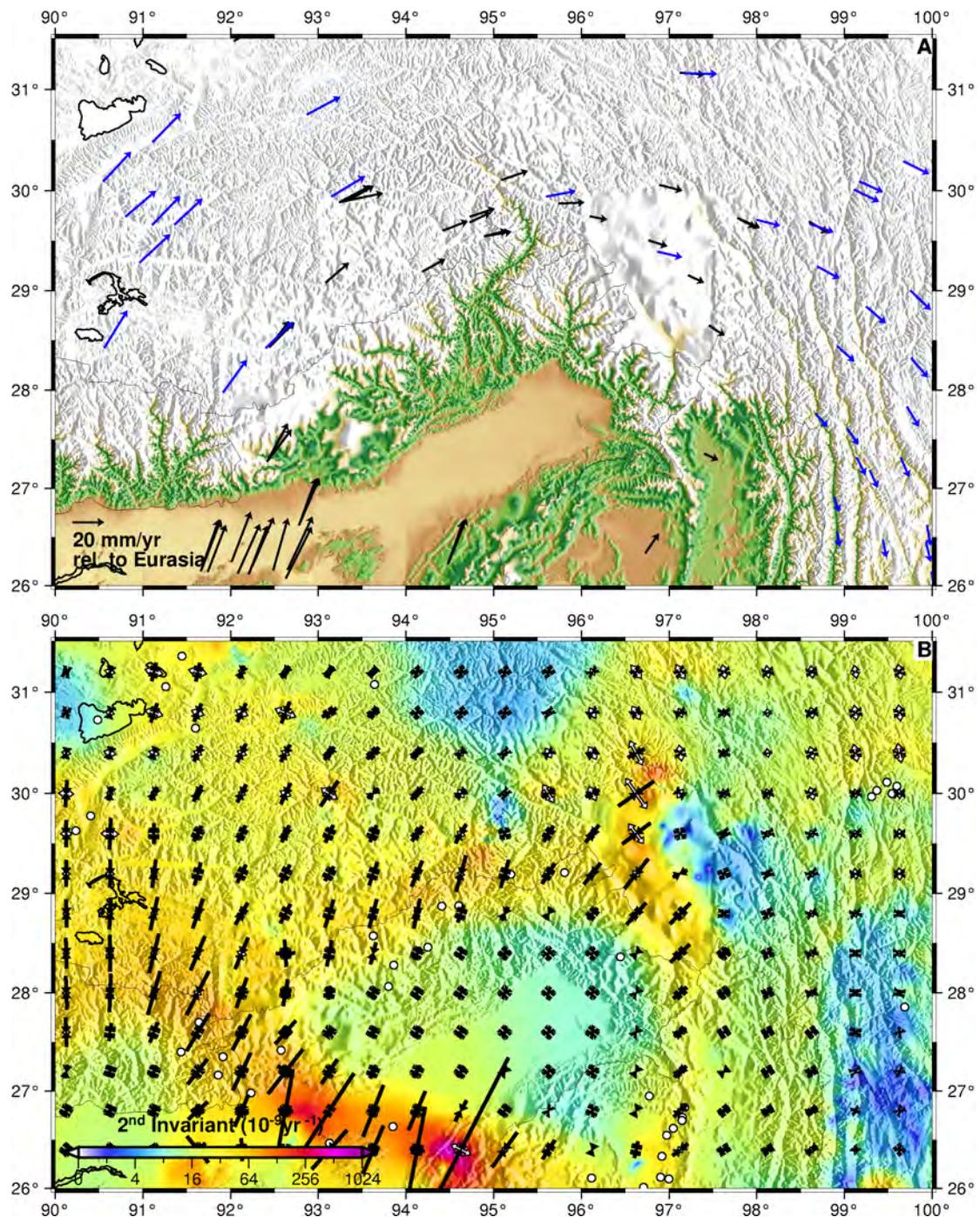


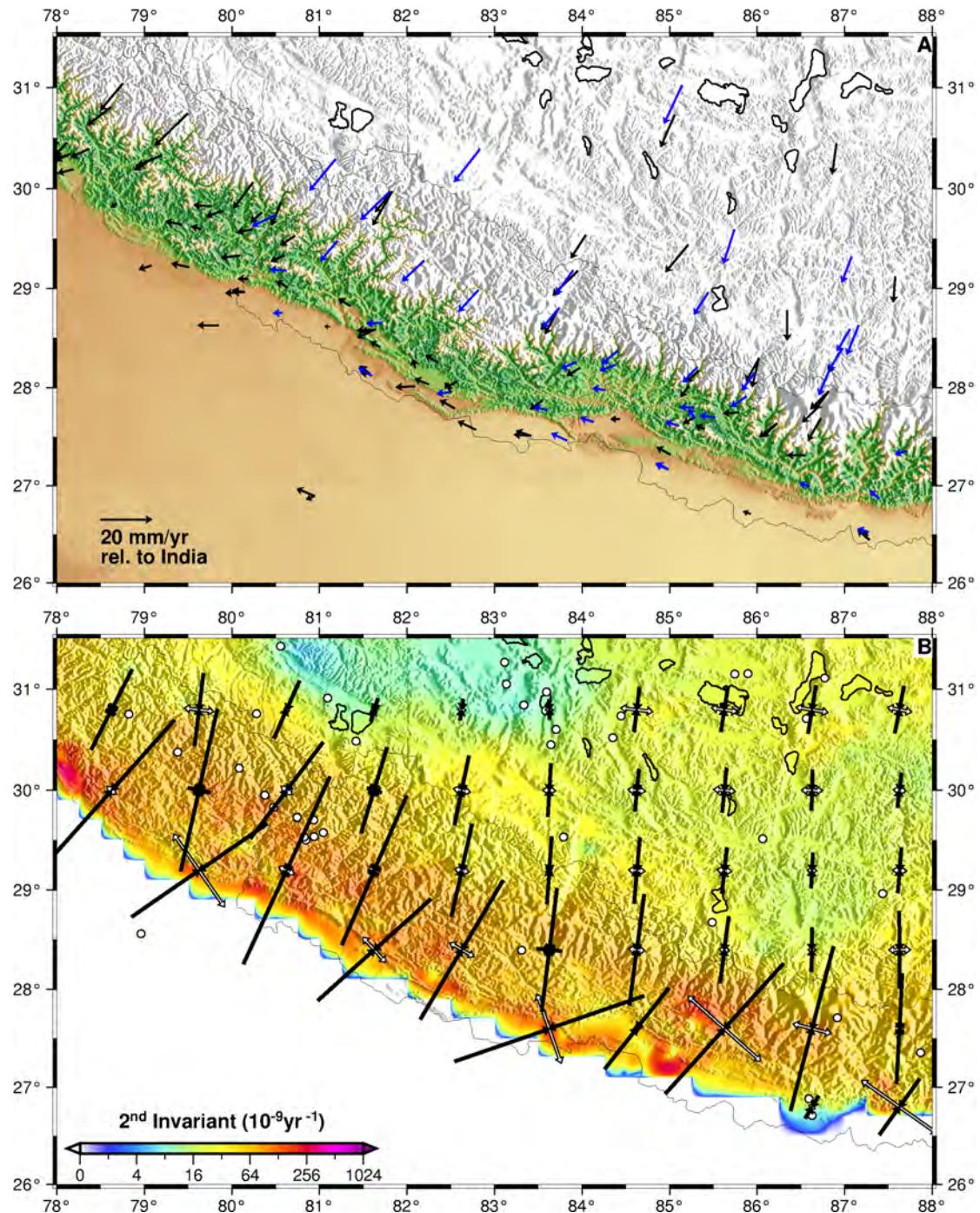


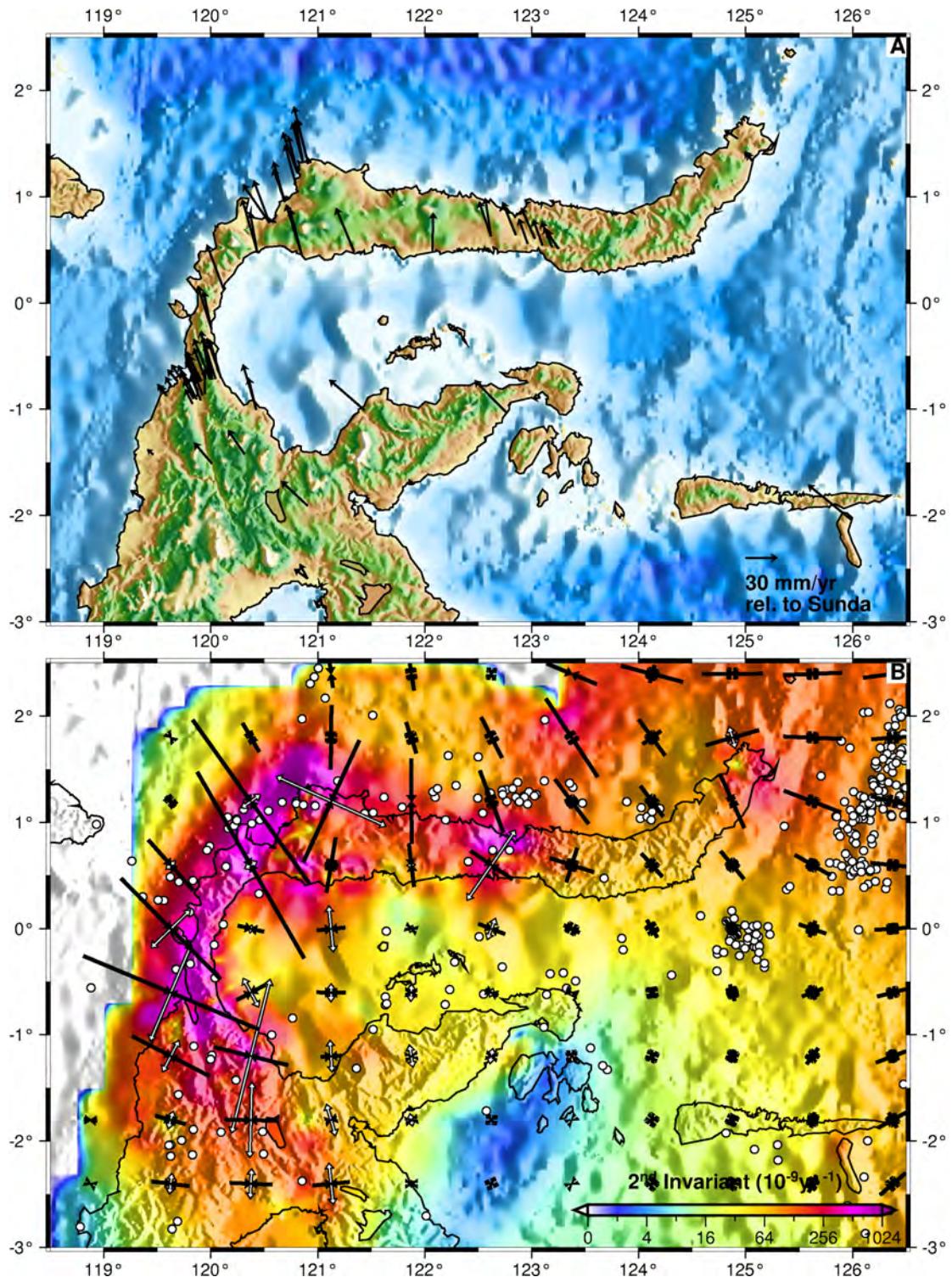


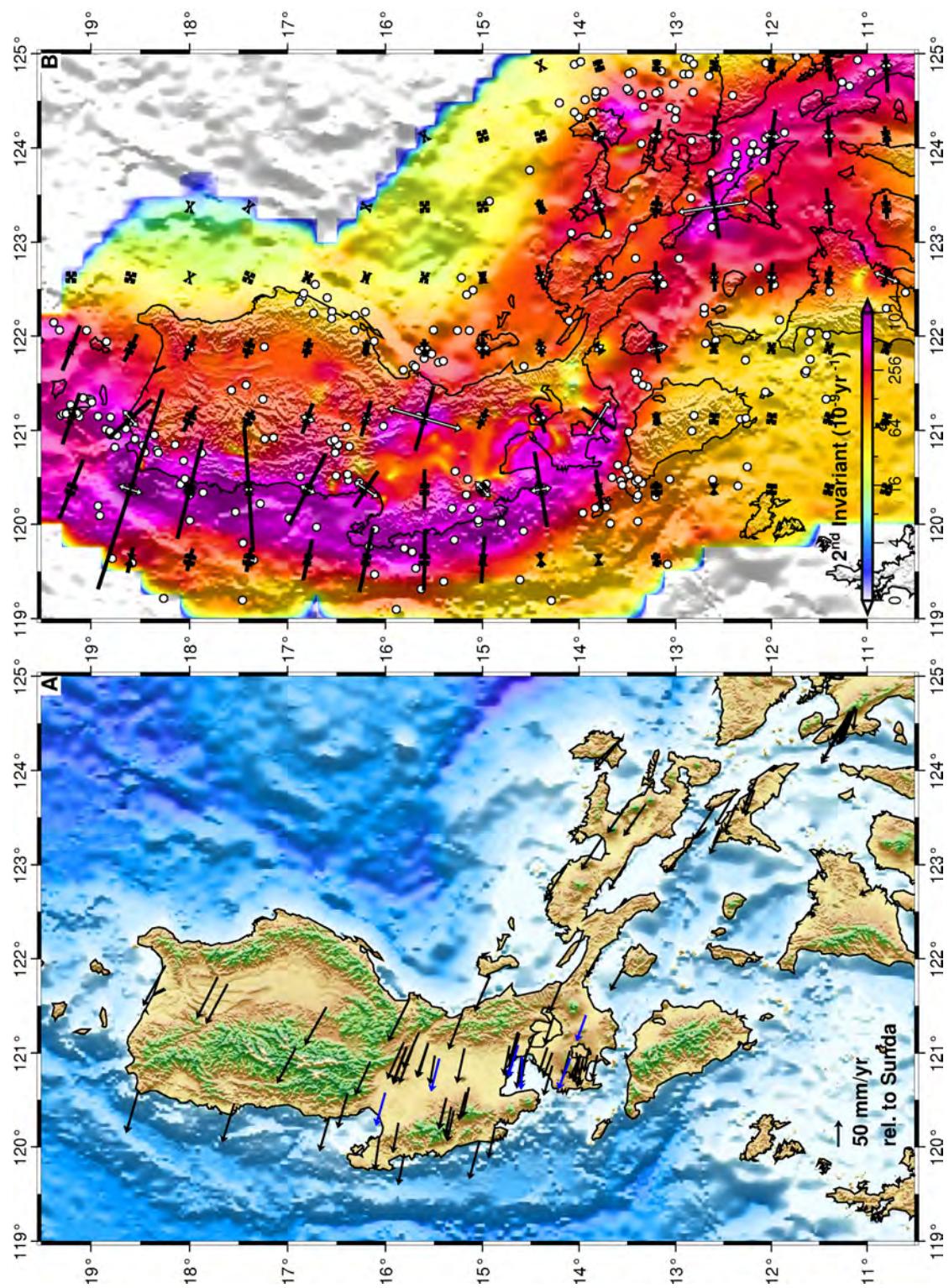


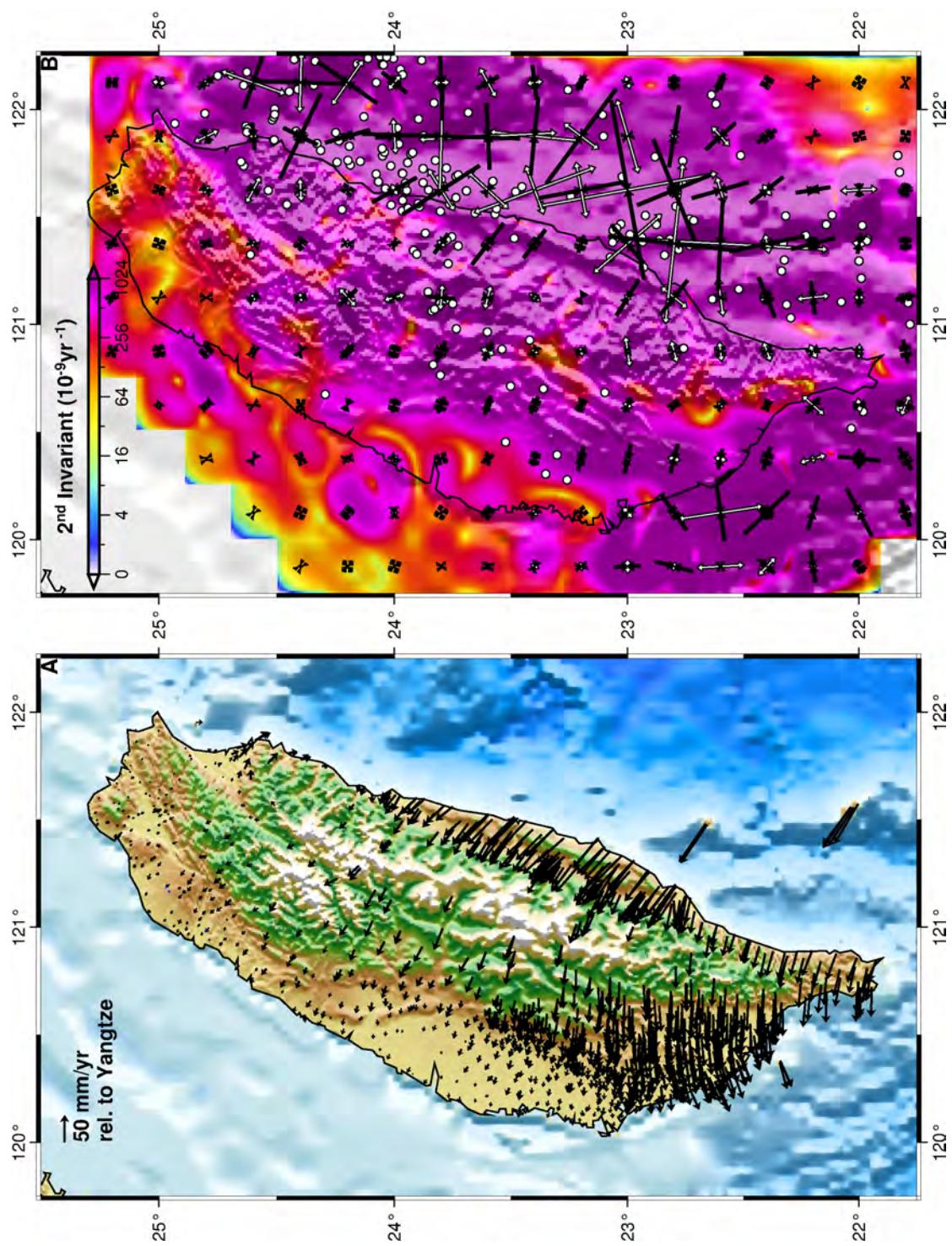


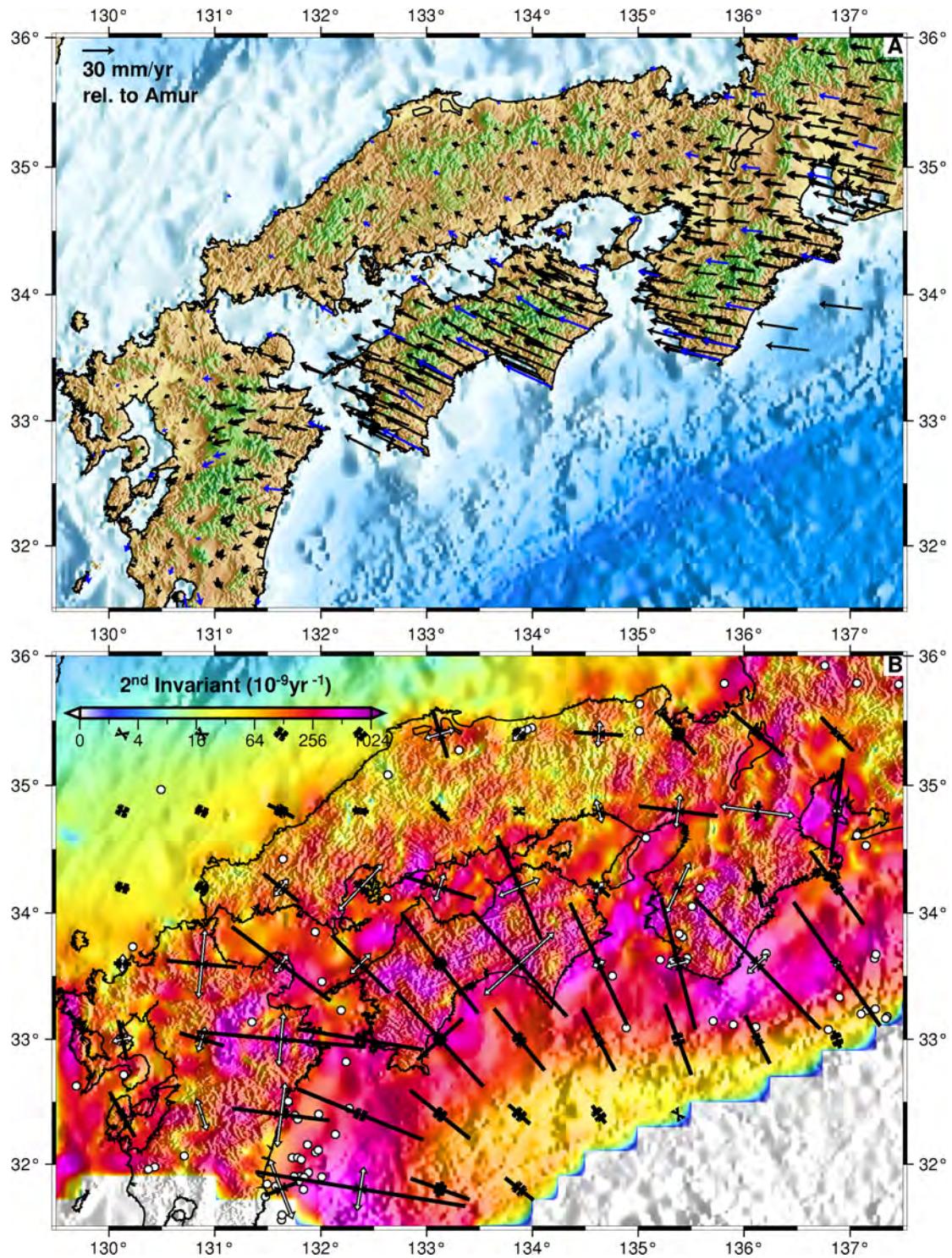


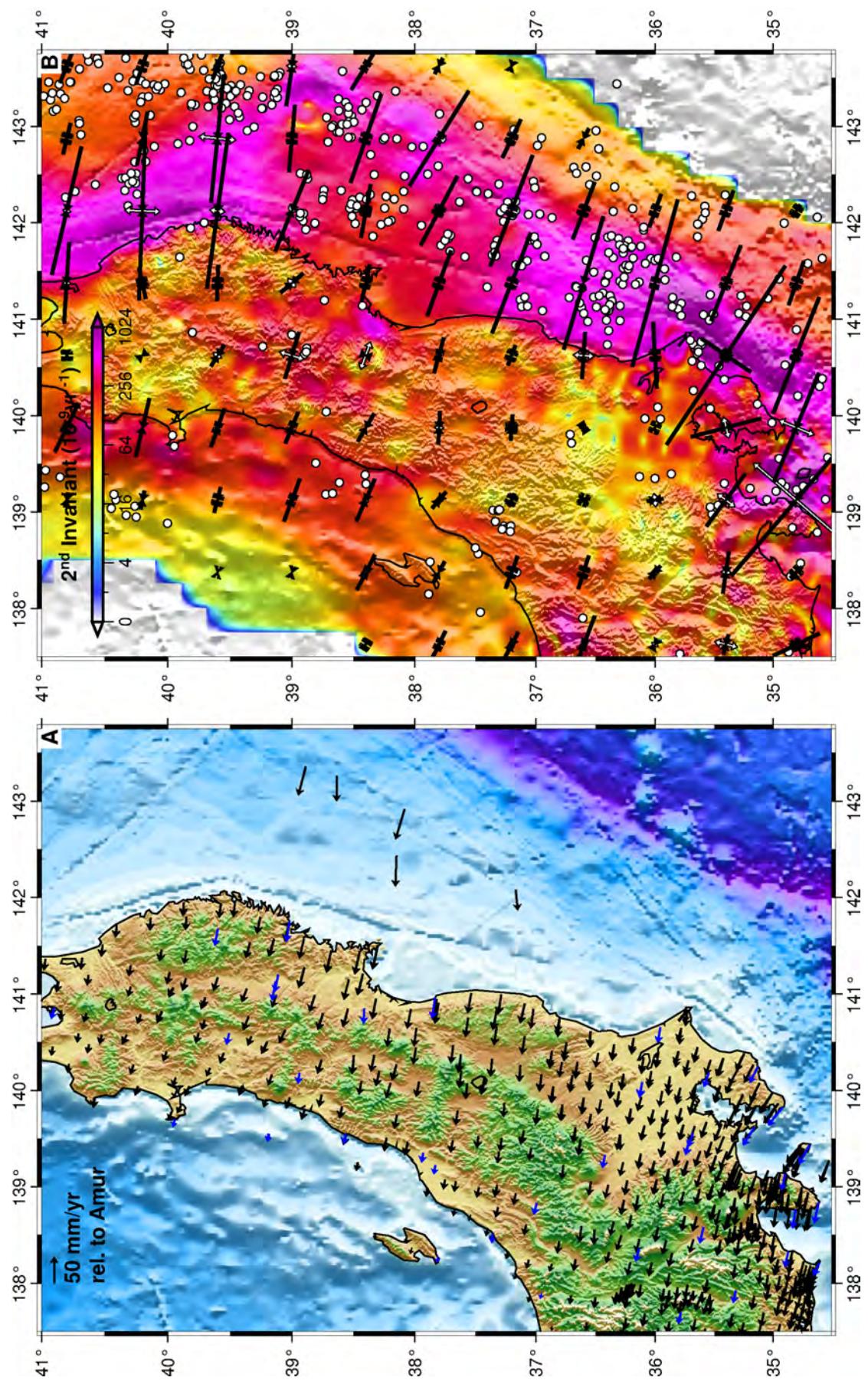


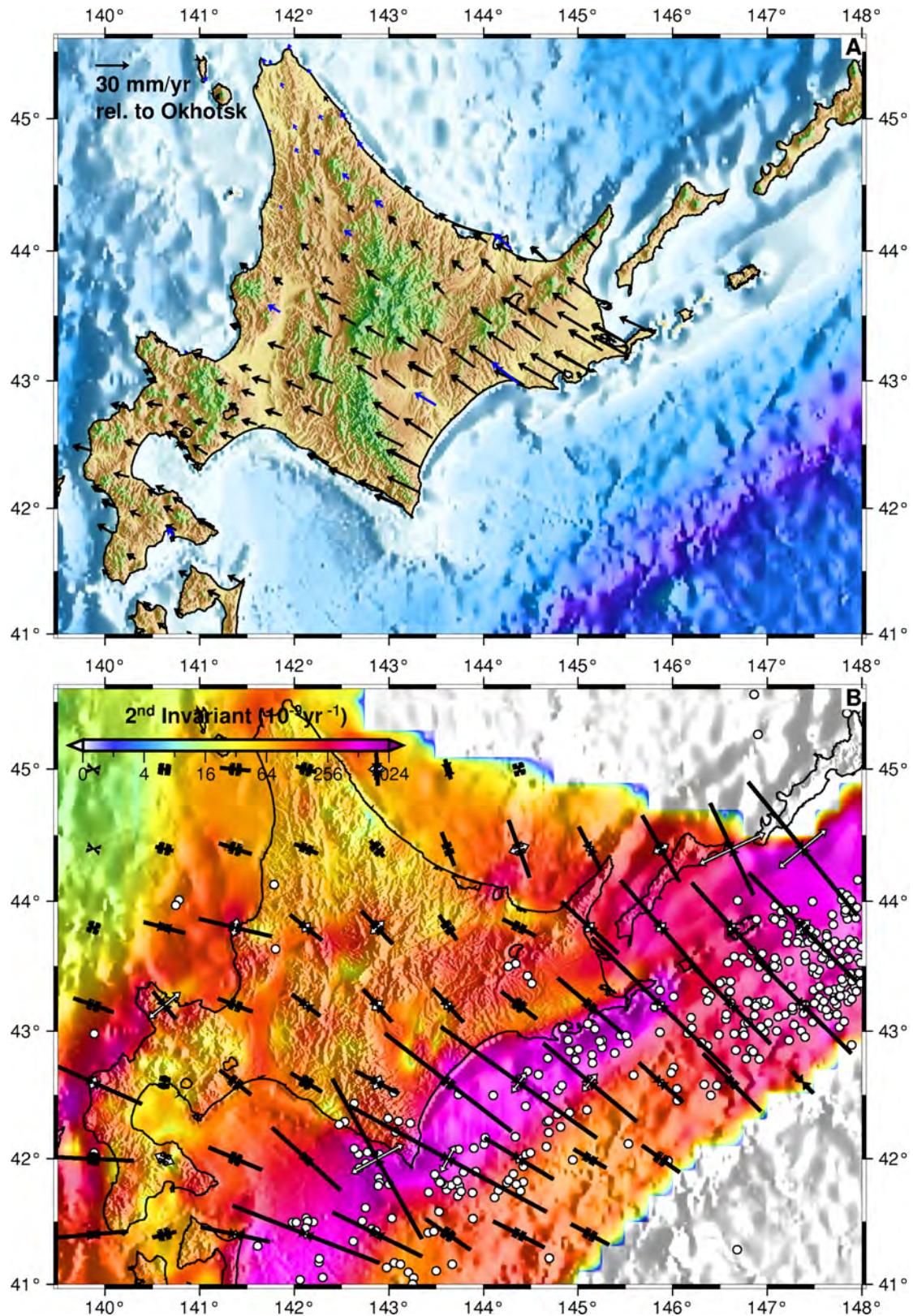


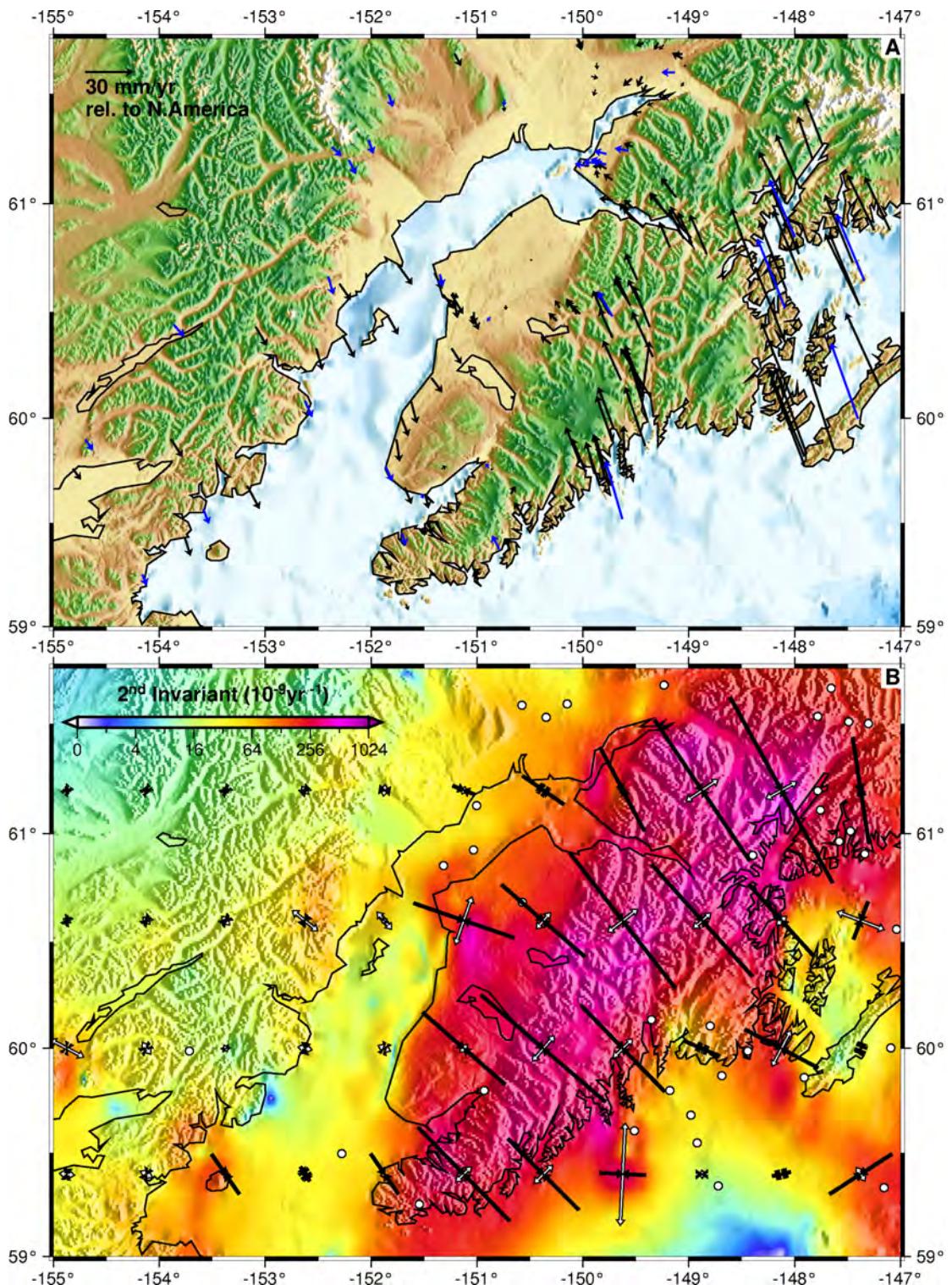


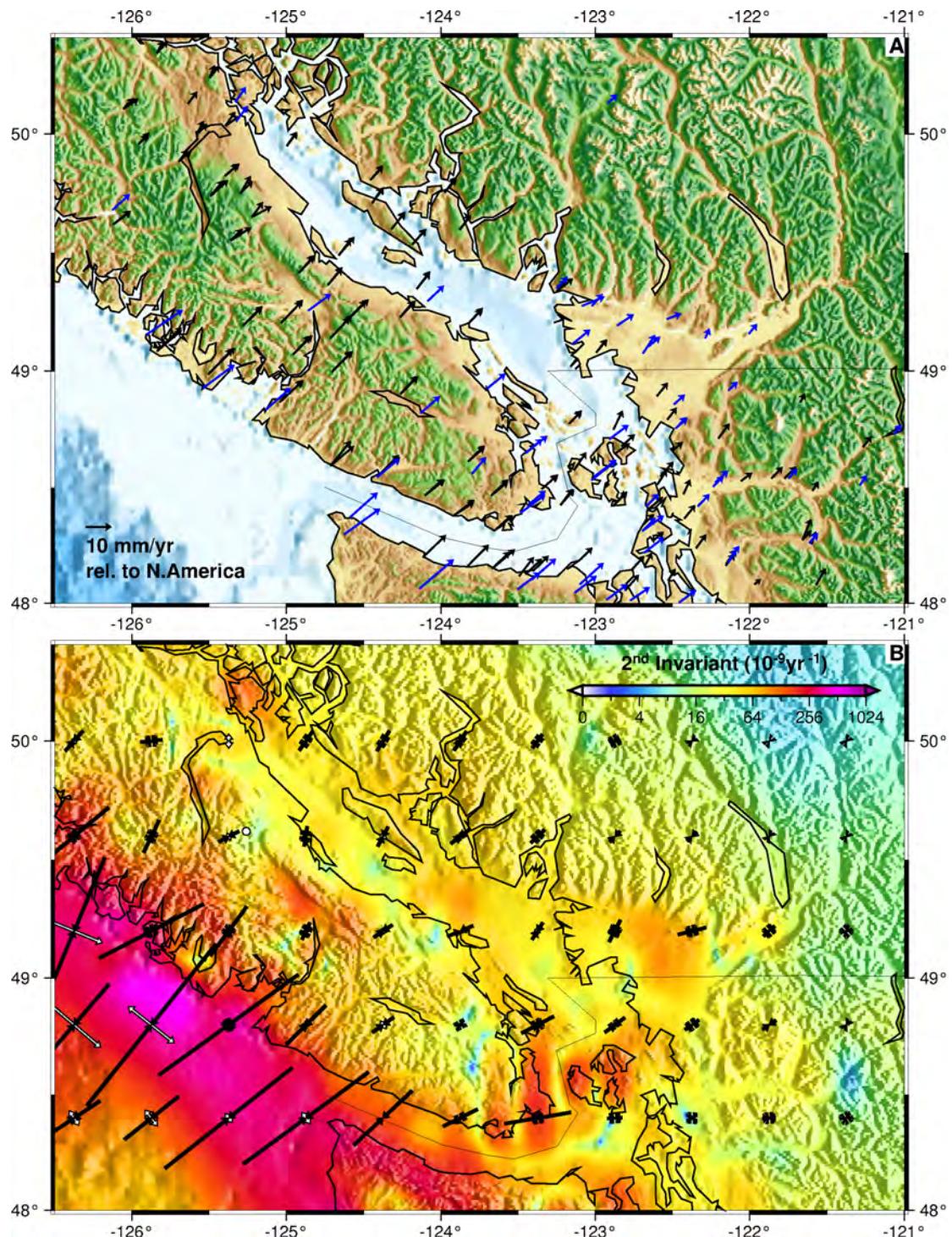


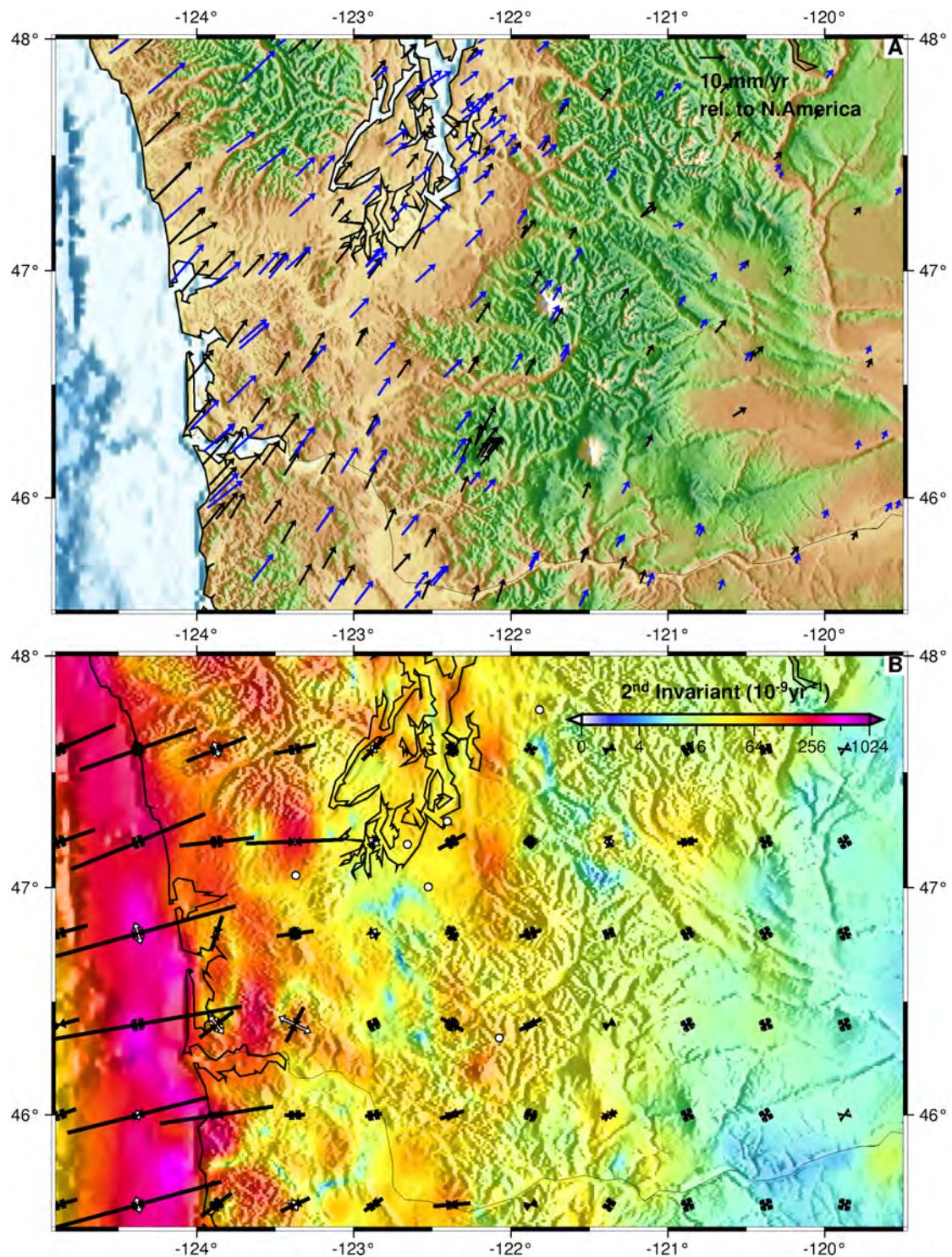


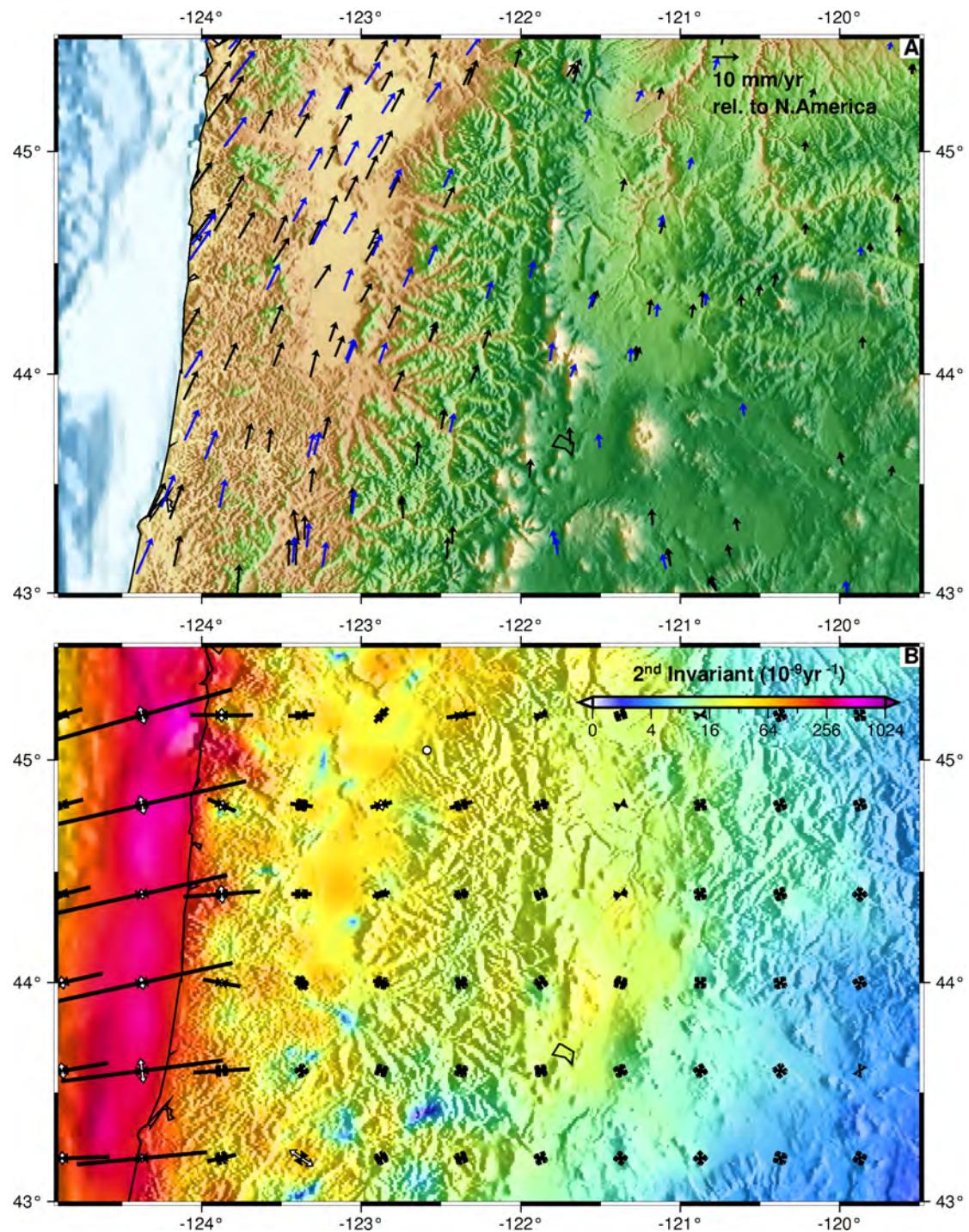


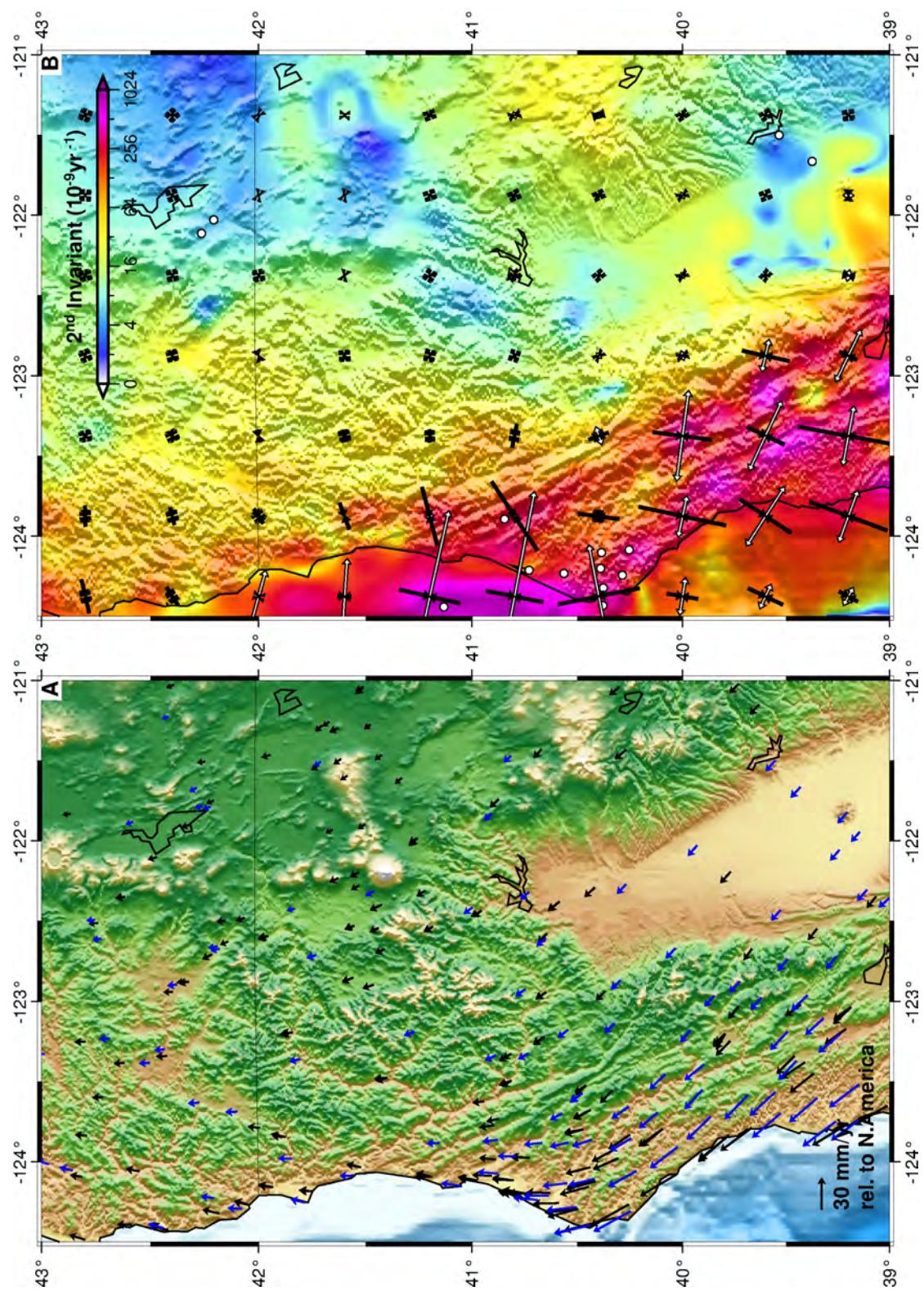


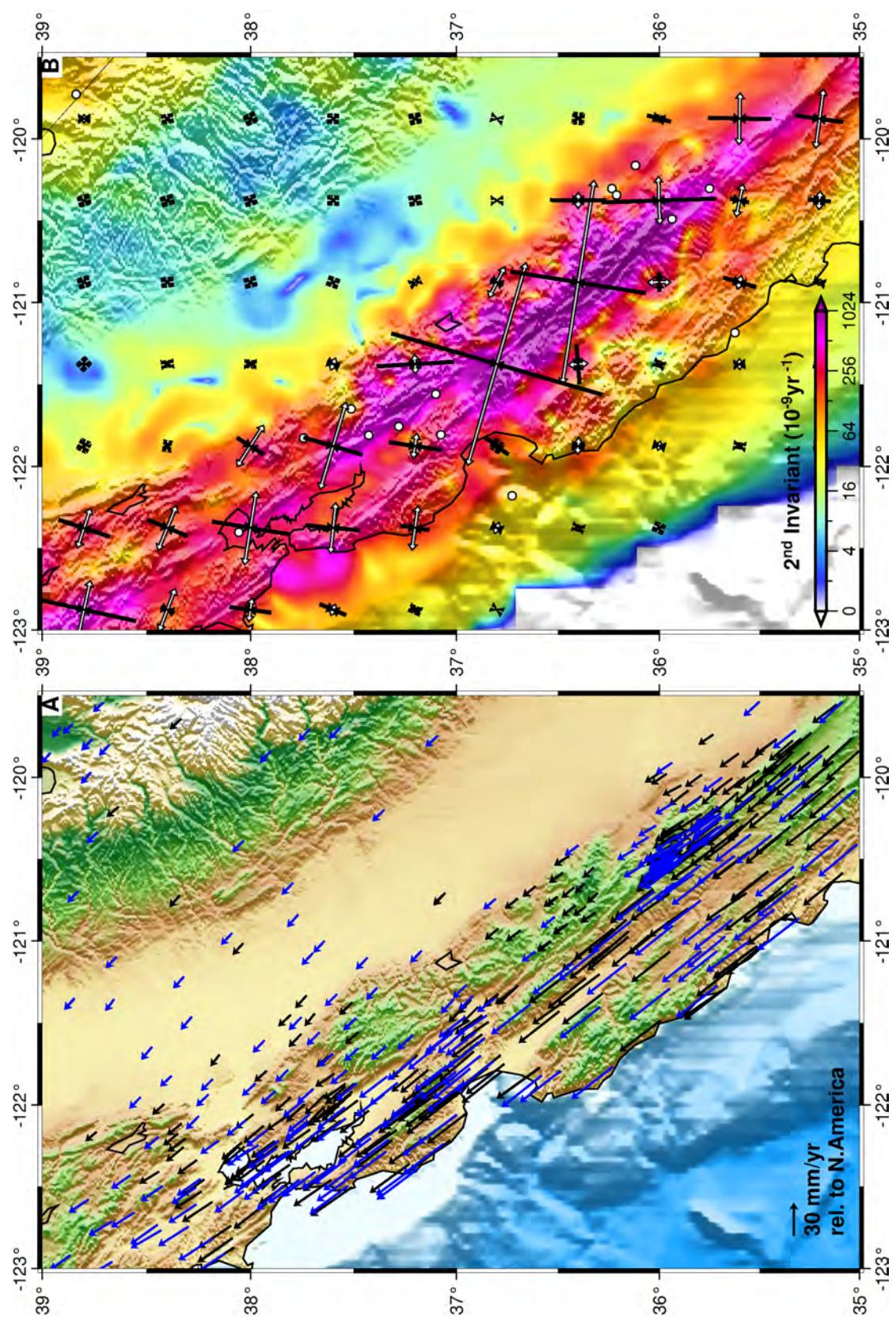


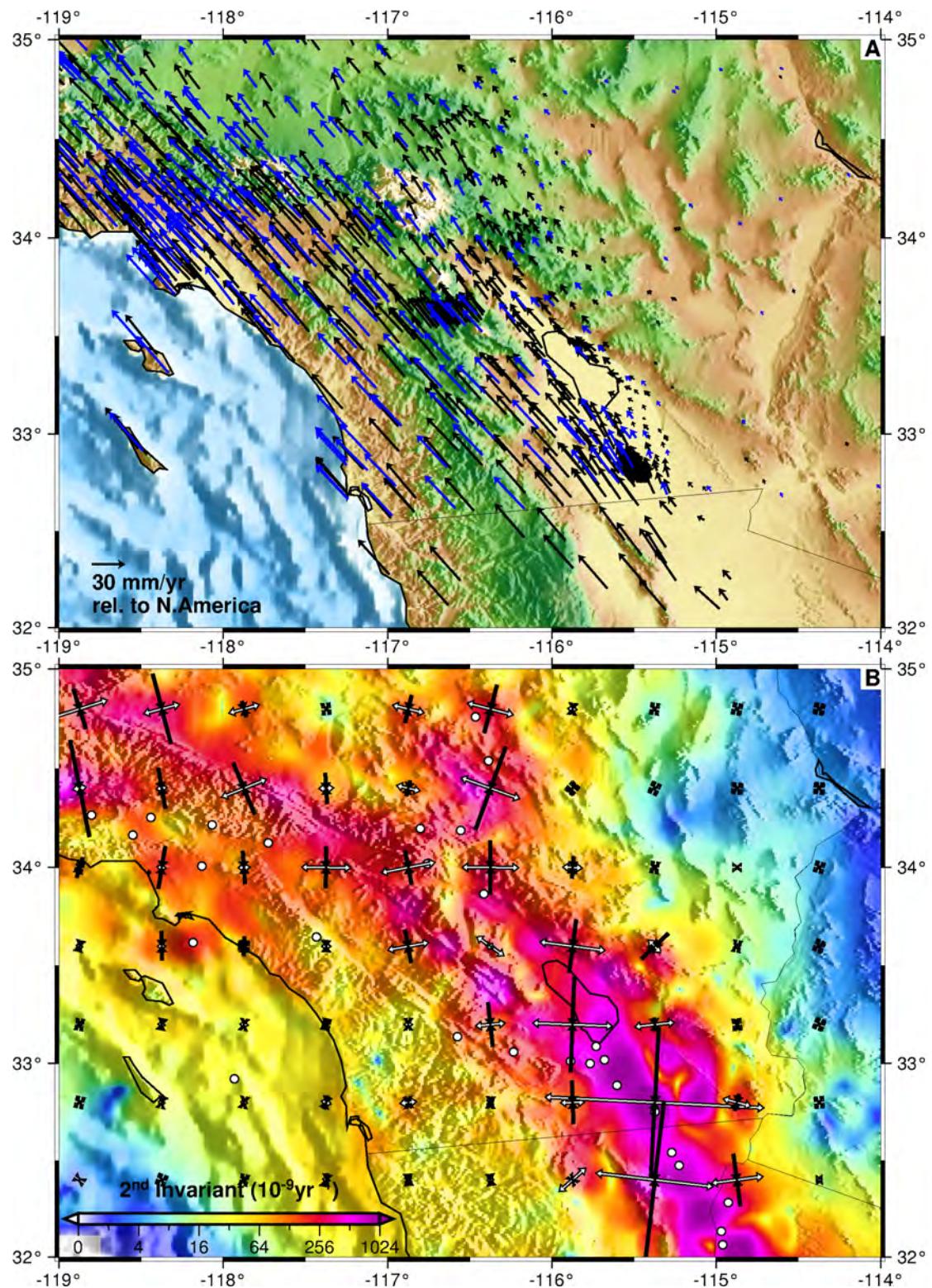


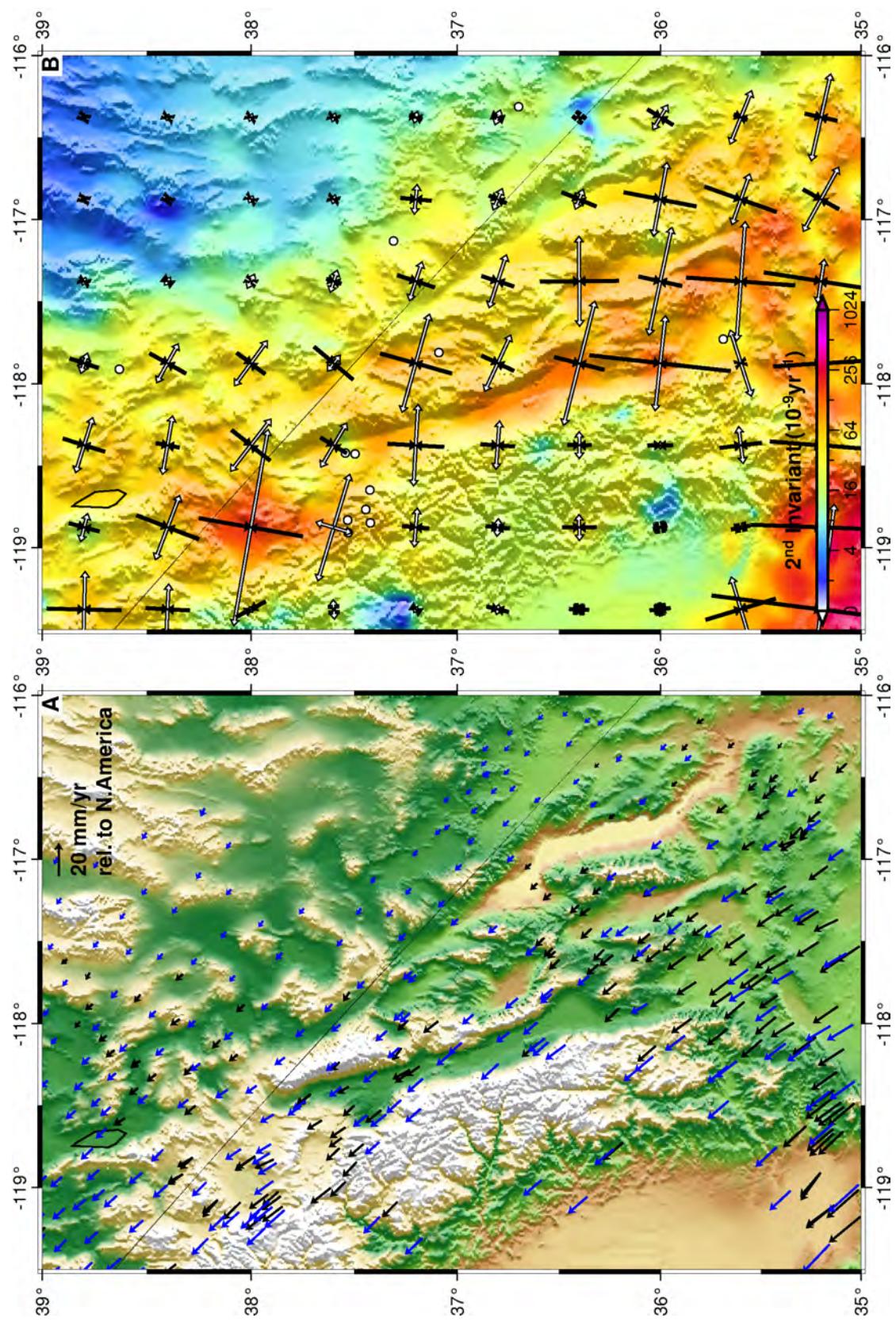


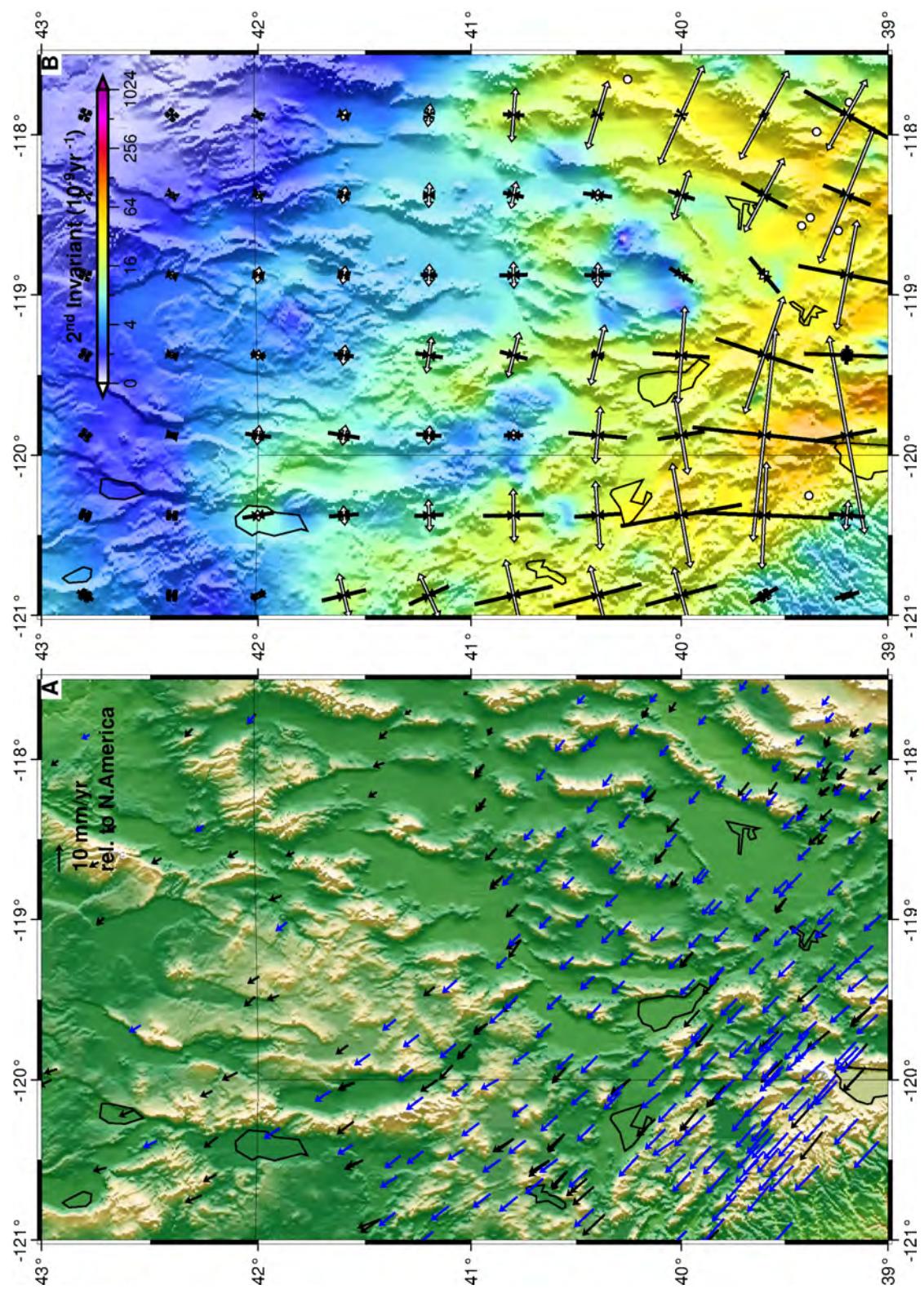


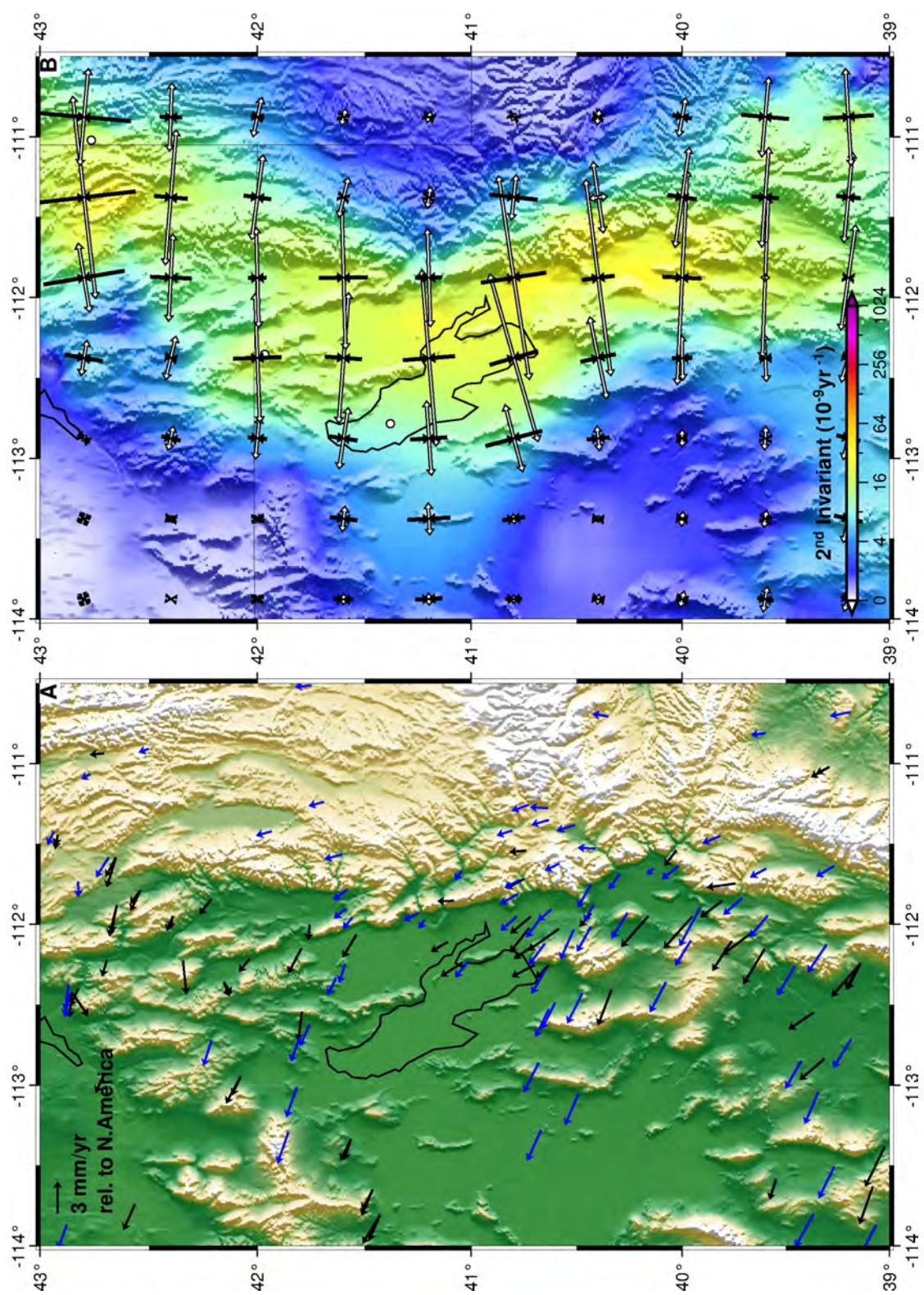


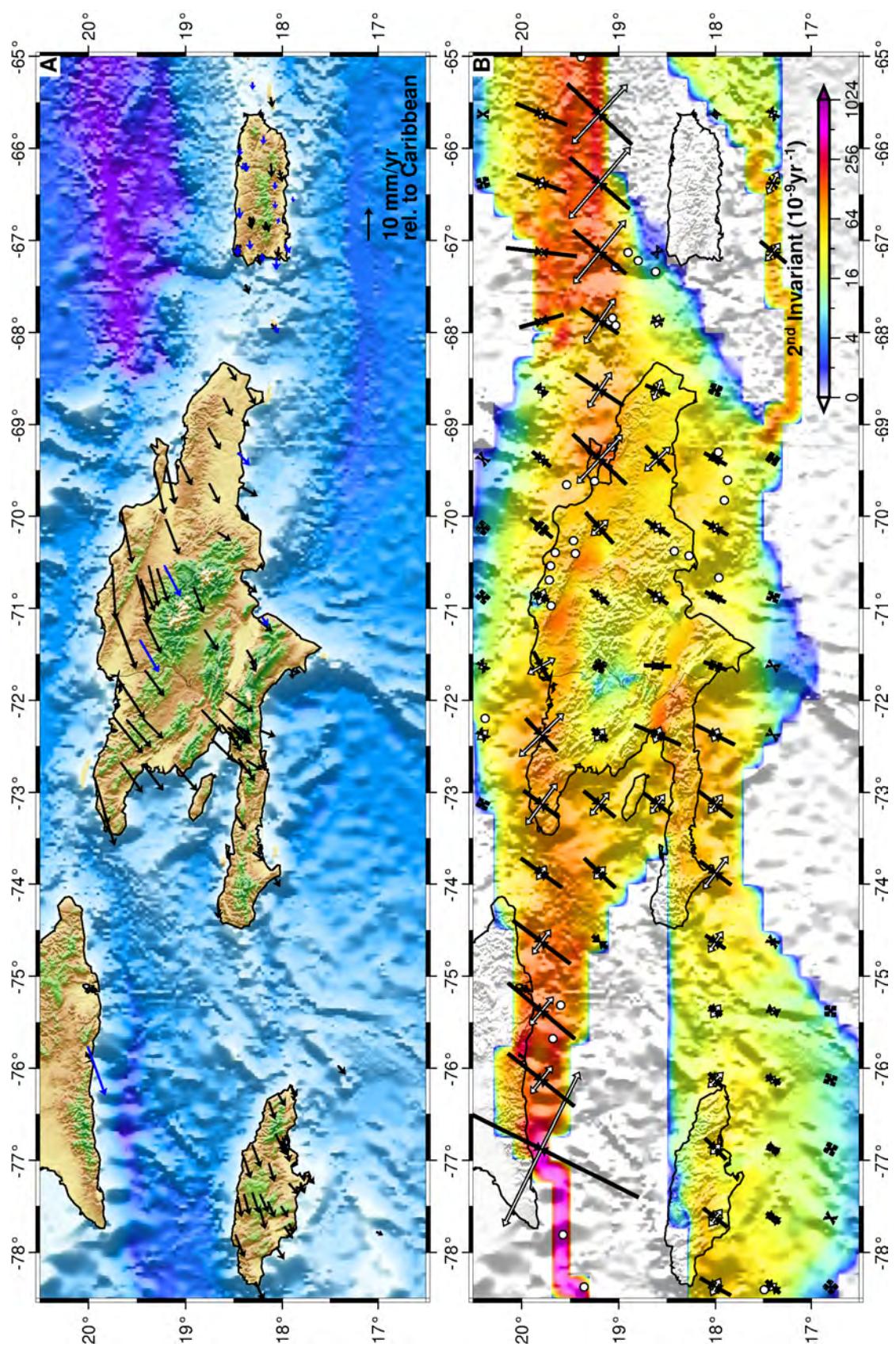


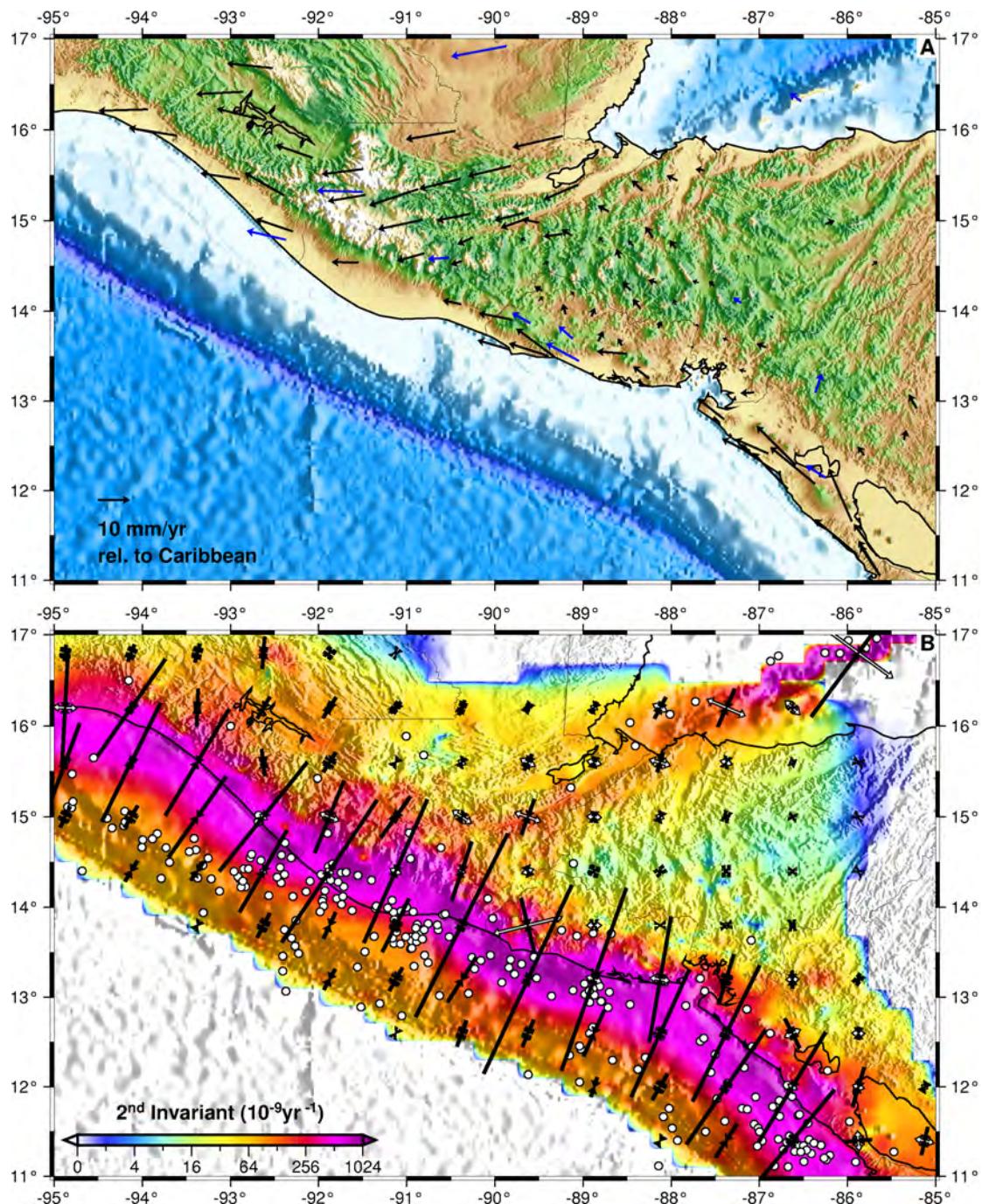


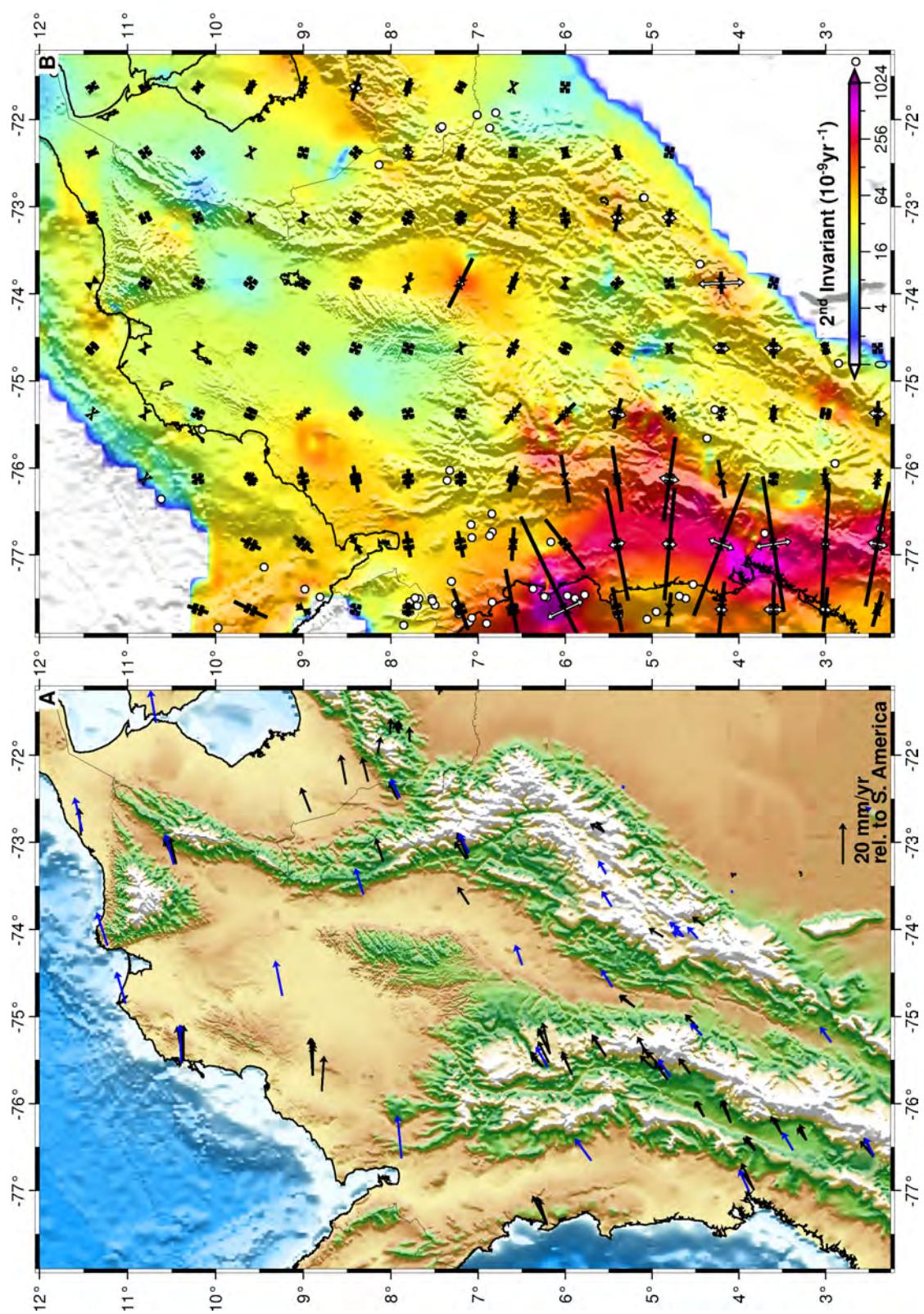


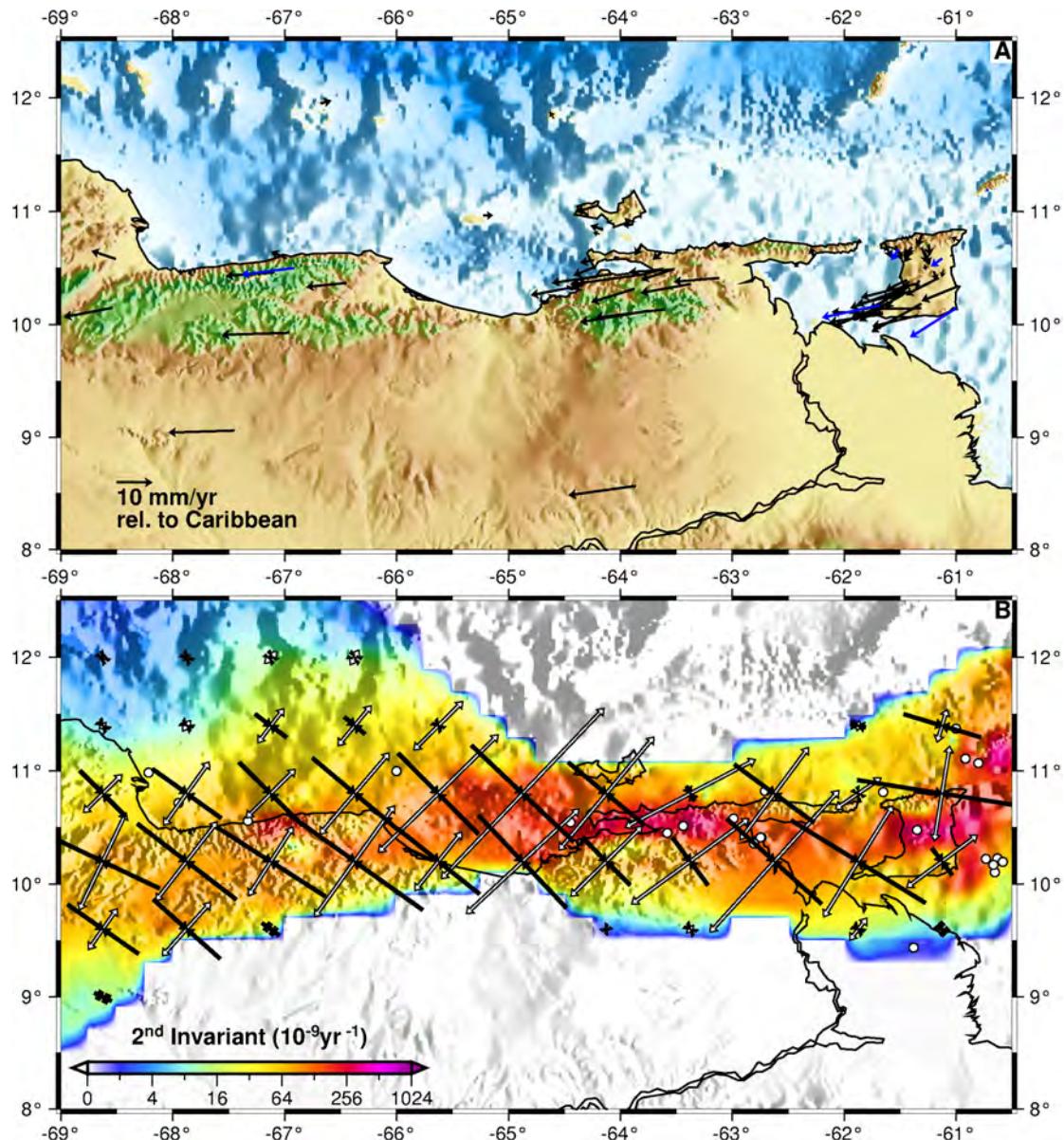


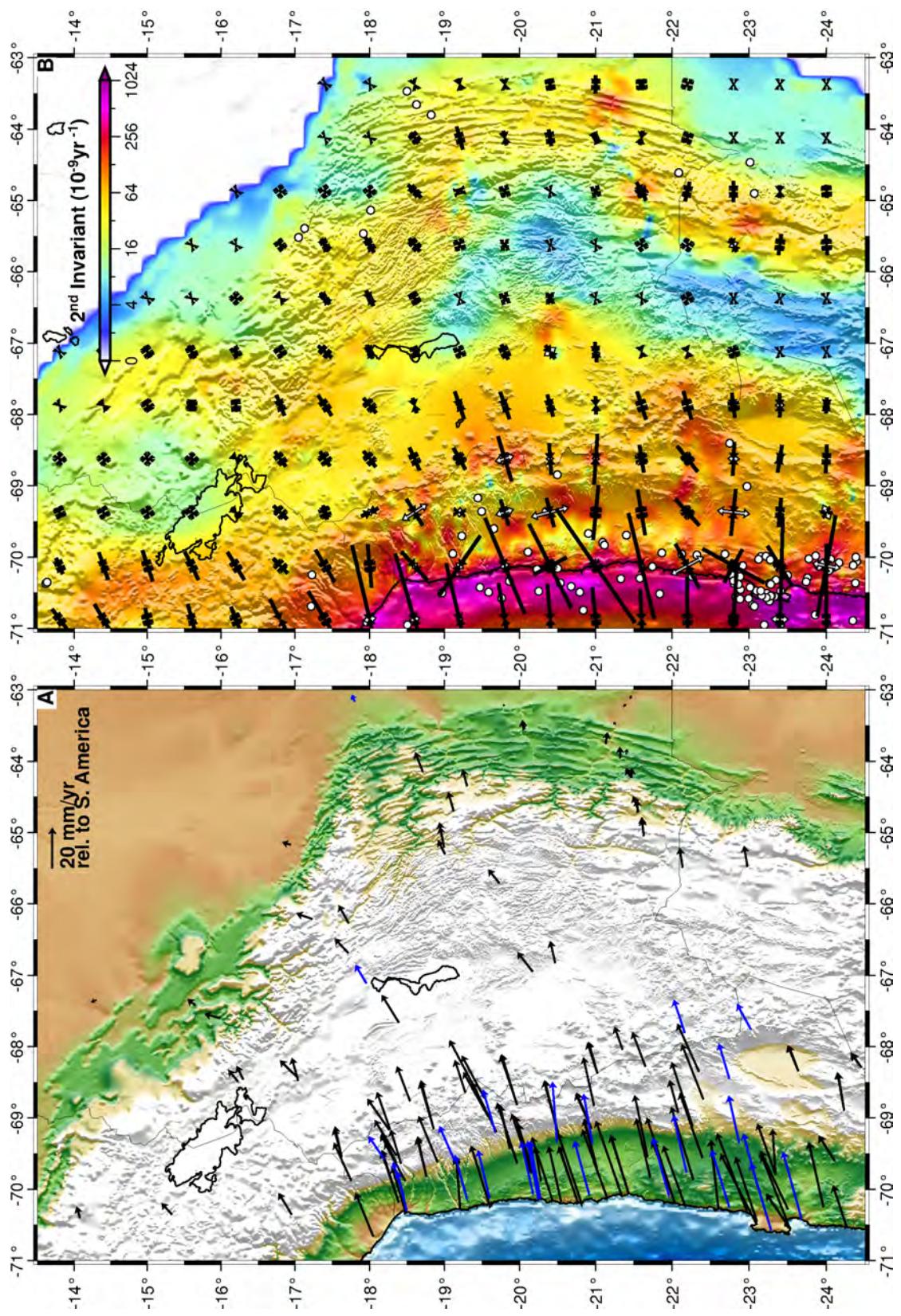


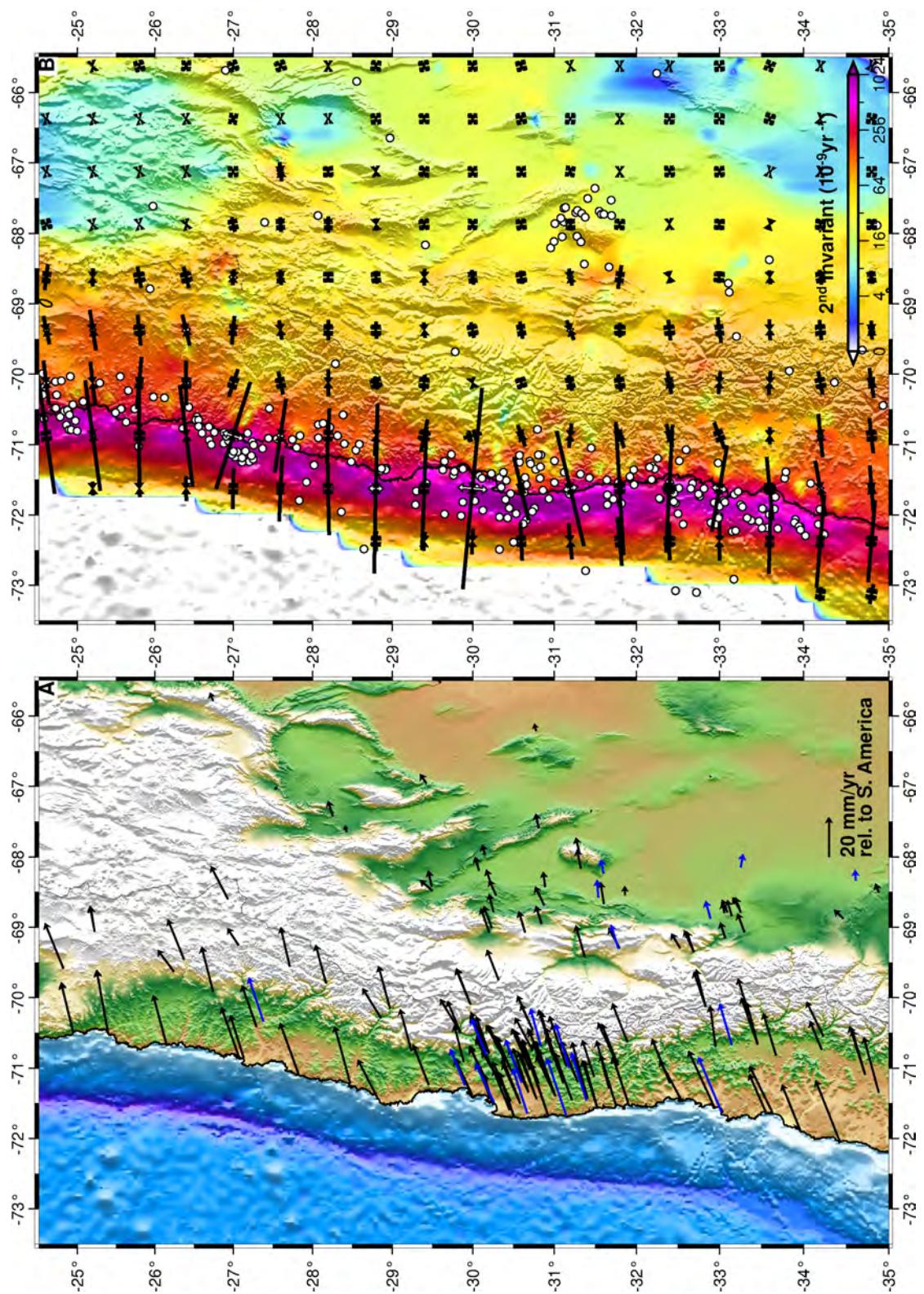


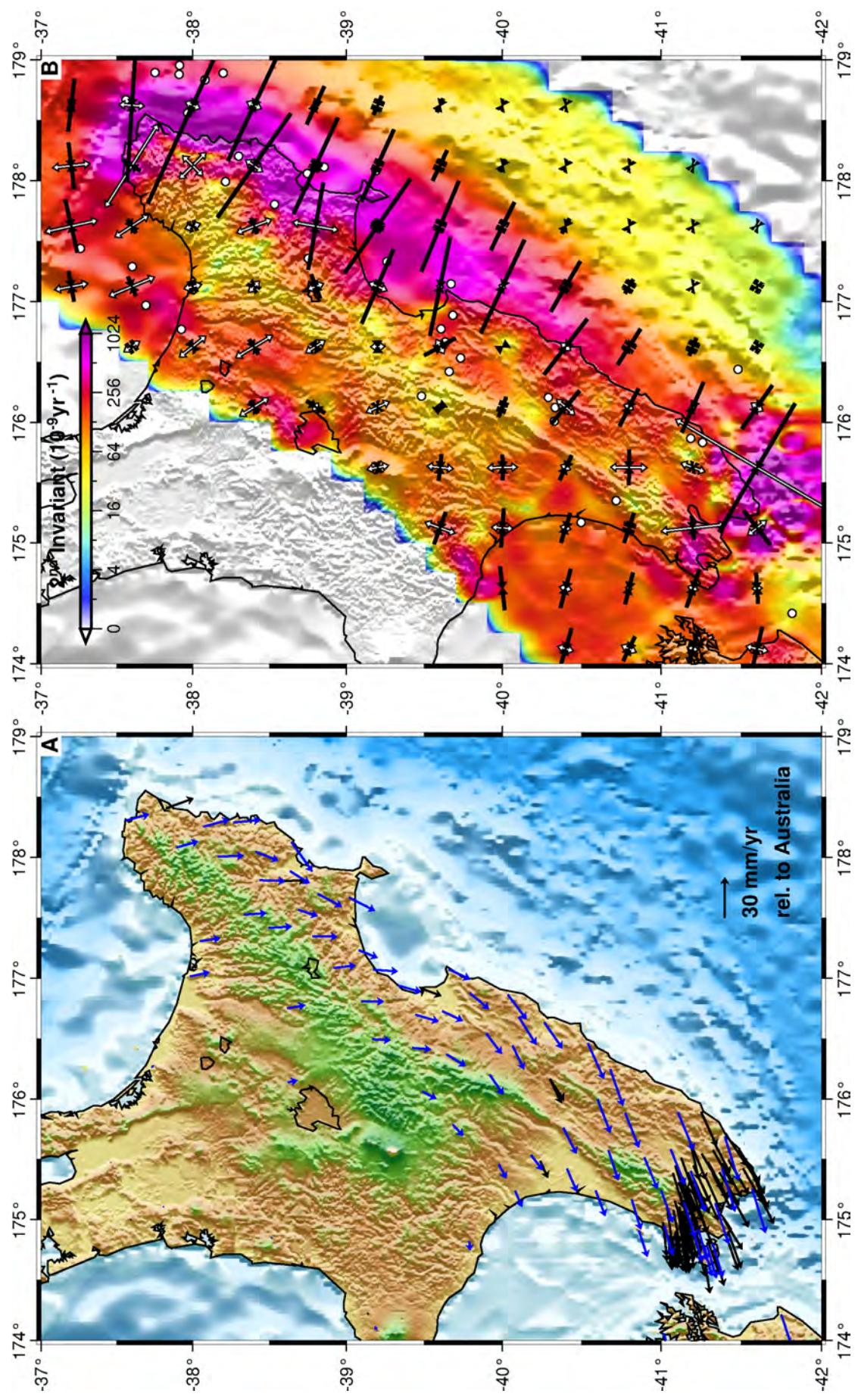


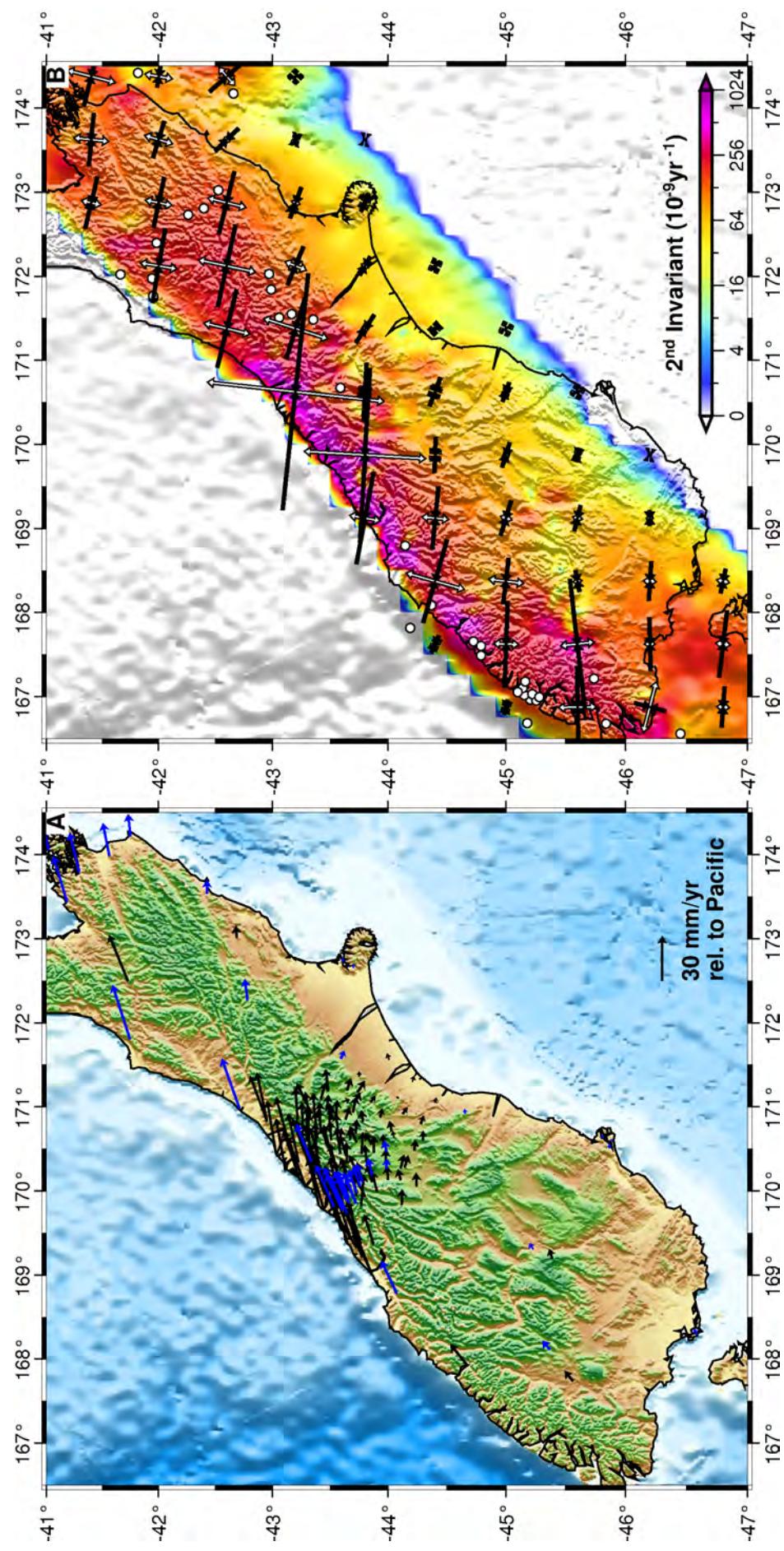












APPENDIX B Published Studies in GPS Compilation

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APPENDIX C Velocities used to Constrain Plate Motions

IGS08 velocities and residuals for sites used to constrain the rigid body plate rotations

station	Lon. (°E)	Lat. (°N)	Vel. E (mm/yr)	Vel. N (mm/yr)	SdVel E. (mm/yr)	SdVel N. (mm/yr)	Resid. E. (mm/yr)	Resid. N. (mm/yr)	Plate	Study
GMAS	344.366	27.765	16.67	17.62	0.36	0.29	0.31	0.34	AF	1
HARO ^a	27.707	-25.887	17.72	18.51	0.36	0.32	-0.13	0.40	AF	1
HRAO	27.687	-25.890	17.71	18.43	0.28	0.27	-0.14	0.32	AF	1
LPAL	342.106	28.764	16.03	16.55	0.34	0.38	0.30	-0.40	AF	1
MAS1	344.367	27.764	16.69	17.00	0.22	0.20	0.33	-0.28	AF	1
NKLG	9.672	0.354	22.28	18.91	0.26	0.22	-0.47	-0.16	AF	1
SUTH	20.810	-32.380	16.89	19.02	0.31	0.27	-0.30	0.32	AF	1
TGCV	337.017	16.755	19.05	15.86	0.26	0.21	0.22	-0.24	AF	1
WIND	17.089	-22.575	19.66	19.38	0.62	0.48	-0.37	0.47	AF	1
YKRO	354.760	6.871	21.85	18.59	0.37	0.36	-0.16	0.14	AF	1
E001	134.290	48.280	22.67	-12.24	0.80	0.80	-0.43	0.25	AM	1
E018	122.340	53.490	23.77	-10.49	0.70	0.70	0.16	0.21	AM	1
E056	116.780	48.660	25.87	-9.78	0.70	0.70	0.29	-0.07	AM	1
JB10	131.170	46.650	23.98	-12.00	0.80	0.80	-0.03	0.07	AM	1
CHA0 ^b	125.444	43.791	25.33	-11.58	0.95	0.76	-0.14	-0.37	AM	1
DAV1	77.973	-68.577	-2.62	-5.13	0.17	0.25	0.23	0.26	AN	1
DUM1	140.002	-66.665	7.96	-11.90	0.40	0.43	0.13	0.62	AN	1
KERG	70.256	-49.351	4.94	-3.27	0.28	0.35	0.29	0.55	AN	1
MAW1	62.871	-67.605	-3.77	-2.13	0.19	0.25	-0.39	0.13	AN	1
MCM4	166.669	-77.838	9.63	-11.67	0.25	0.29	0.18	-0.23	AN	1
SYOG	39.584	-69.007	-3.90	2.77	0.19	0.22	-0.03	-0.03	AN	1

VESL	357.158	-71.674	-0.38	10.25	0.20	0.23	-0.23	-0.06	AN	1
BAHR	50.608	26.209	30.87	30.04	0.26	0.27	-0.29	-0.12	AR	1
BHR1	50.608	26.209	31.40	29.98	0.24	0.27	0.24	-0.18	AR	1
KUWT	47.971	29.325	29.38	29.64	0.41	0.36	0.39	0.02	AR	1
SOLA	46.401	24.911	31.57	29.24	0.31	0.26	0.69	0.03	AR	1
YIBL	56.112	22.186	33.37	31.47	0.35	0.28	-0.83	0.31	AR	1
MYKN	25.333	37.487	6.78	-13.13	0.60	0.60	0.43	-0.82	AS	2
AKIT	23.296	35.873	7.03	-12.88	0.30	0.30	-0.22	-0.07	AS	3
MKN2	25.379	37.449	6.23	-12.40	0.20	0.20	-0.13	-0.10	AS	3
TUC2	24.071	35.533	7.79	-12.05	0.34	0.33	0.51	0.58	AS	1
ALIC	133.886	-23.670	32.34	59.07	0.16	0.14	0.38	0.15	AU	1
CEDU	133.810	-31.867	29.01	58.64	0.16	0.17	0.29	-0.28	AU	1
DARW	131.133	-12.844	35.80	59.21	0.32	0.33	-0.11	0.06	AU	1
HOB2	147.439	-42.805	14.12	55.96	0.27	0.38	-0.03	0.12	AU	1
KARR	117.097	-20.981	38.84	58.34	0.16	0.15	-0.25	0.16	AU	1
TIDB	148.980	-35.399	18.17	55.28	0.31	0.26	-0.15	-0.01	AU	1
TOW2	147.056	-19.269	28.94	55.89	0.23	0.23	-0.14	-0.08	AU	1
YAR2	115.347	-29.047	38.73	57.72	0.19	0.18	-0.40	-0.09	AU	1
AGUA	248.700	25.590	-47.18	20.74	0.30	0.60	-0.34	0.56	BC	4
CARD	249.220	24.150	-48.08	20.84	1.30	0.50	-0.03	0.89	BC	4
MELR	244.261	30.980	-41.80	21.28	0.44	0.43	0.78	-0.92	BC	5
AB04	189.433	63.657	-0.94	-23.48	0.76	1.05	0.00	0.21	BG	1
AC58	189.782	57.156	-4.15	-23.96	1.41	1.04	0.01	-0.20	BG	1
AVES	296.382	15.667	12.09	13.99	2.10	0.90	-0.19	-0.41	CA	1
GREO	298.360	12.222	13.66	15.19	0.52	0.48	-0.17	0.11	CA	1
SAN0	278.284	12.580	13.04	7.46	0.58	0.49	0.23	0.02	CA	1
EDI1	41.677	13.845	38.74	25.18	0.93	0.85	0.81	1.54	DA	6
EDTI	41.353	14.359	35.95	22.04	1.23	1.13	0.66	-0.06	DA	6

TIO1	40.961	14.615	34.12	20.57	0.63	0.60	0.17	0.35	DA	6
TIGE	40.477	14.891	31.43	17.57	1.37	1.23	-1.07	-0.34	DA	6
GELA	40.088	15.114	31.71	15.18	0.64	0.61	0.38	-0.88	DA	6
ASAB	42.654	13.063	40.78	28.09	0.76	0.68	-1.22	-0.22	DA	1
ARTU	58.560	56.430	25.16	6.17	0.23	0.22	-0.15	0.29	EU	1
GLSV	30.497	50.364	22.28	12.76	0.28	0.28	-0.58	0.55	EU	1
KOSG	5.810	52.178	18.09	15.97	0.24	0.23	0.38	0.54	EU	1
NRIL	88.360	69.362	22.13	-2.10	0.21	0.22	-0.93	0.20	EU	1
NVSK	83.235	54.841	26.90	-1.14	0.38	0.47	0.40	-0.26	EU	1
NYAL	11.865	78.930	10.44	14.12	0.17	0.17	0.12	-0.77	EU	1
VILL	356.048	40.444	18.87	16.28	0.22	0.21	0.06	0.34	EU	1
WTZR	12.879	49.144	20.32	15.47	0.21	0.20	0.38	0.69	EU	1
BOSC	283.030	18.400	3.91	7.30	0.40	0.40	-0.35	-0.18	GV	7
DISC	282.600	18.460	4.11	8.10	0.40	0.40	-0.08	0.97	GV	7
NGLF	281.680	18.280	4.71	6.30	0.30	0.30	0.40	-0.08	GV	7
NUTF	283.170	18.310	3.41	6.80	1.00	0.50	-0.93	-0.79	GV	7
PYRA	282.190	18.490	3.21	6.20	1.00	0.80	-0.93	-0.60	GV	7
JERE	285.828	18.663	4.59	10.44	2.52	2.19	0.43	0.71	GV	8
HYDE	78.551	17.417	41.11	34.33	0.34	0.33	0.21	-0.58	IN	1
IISC	77.570	13.021	41.07	35.77	0.50	0.36	-0.68	0.89	IN	1
MALD	73.526	4.189	43.88	33.92	1.06	0.73	1.00	-0.73	IN	1
PAGA	145.757	18.126	-30.05	9.91	3.17	3.07	0.81	-2.54	MA	9
GUGU	145.832	17.309	-29.10	9.79	2.62	2.57	-1.68	-2.97	MA	9
ANAT	145.633	16.364	-21.51	8.18	2.75	2.57	1.95	-3.75	MA	9
CNMO ^c	145.743	15.230	-18.70	12.74	0.66	0.52	-0.04	0.35	MA	1
ALGO	281.929	45.956	-16.39	2.50	0.29	0.28	0.39	-0.76	NA	1
FLIN	258.022	54.726	-17.67	-7.15	0.21	0.31	0.75	-0.90	NA	1
GODE	283.173	39.022	-14.64	4.14	0.13	0.13	0.10	0.38	NA	1

MSS0 ^d	270.386	30.375	-12.31	-0.34	0.38	0.20	-0.20	1.03	NA	1
NLIO ^e	268.425	41.772	-15.56	-1.20	0.18	0.18	0.14	0.95	NA	1
PLTC	255.274	40.182	-14.62	-5.95	0.19	0.19	-0.10	1.36	NA	1
RCMO ^f	279.616	25.614	-10.83	3.06	0.23	0.24	-0.42	0.72	NA	1
STJO	307.322	47.595	-14.75	12.80	0.21	0.22	-0.20	0.08	NA	1
THU2	291.175	76.537	-22.39	4.71	0.12	0.17	-0.89	-2.17	NA	1
YELL	245.519	62.481	-17.22	-11.32	0.28	0.28	1.03	-0.42	NA	1
KAVI	150.807	-2.582	-63.97	32.67	2.70	1.60	-0.77	1.23	NB	10
KAVI	150.807	-2.582	-64.71	30.98	1.70	1.10	-1.51	-0.46	NB	11
PNGM	147.366	-2.043	-64.08	24.85	0.42	0.36	0.11	-0.01	NB	1
FLIX	279.912	-26.297	62.68	17.57	1.00	1.00	0.24	-0.06	NZ	12
RBSN	281.163	-33.629	63.56	17.82	1.00	1.00	0.08	-0.68	NZ	12
GLP0 ^g	269.696	-0.743	50.37	10.28	0.21	0.24	-0.01	0.04	NZ	1
OKRG	143.804	50.292	15.25	-15.76	2.73	2.75	1.23	0.87	OK	13
PILG	143.646	50.049	14.26	-15.08	2.55	2.56	0.21	1.51	OK	13
TAL1	152.392	61.130	13.01	-20.43	2.30	2.23	1.09	-2.16	OK	13
MAGO	150.770	59.576	12.47	-20.14	0.73	1.00	0.07	-2.15	OK	1
MAGJ	150.810	59.578	12.22	-17.01	0.55	0.66	-0.17	0.99	OK	1
J734	128.894	27.817	31.19	-33.95	1.22	0.80	0.89	1.09	ON	1
J735	128.651	27.401	33.20	-34.75	0.82	0.94	1.90	0.71	ON	1
J736	127.945	26.944	32.86	-37.27	0.87	0.78	0.34	-0.58	ON	1
J739	127.232	26.583	32.80	-37.91	0.73	0.73	-0.73	-0.01	ON	1
J742	127.144	26.373	33.58	-37.98	0.80	0.67	-0.43	0.07	ON	1
J743	126.739	26.348	32.69	-40.44	0.91	0.98	-1.49	-1.70	ON	1
GAMB	225.035	-23.130	-67.51	31.96	0.37	0.28	-0.03	0.16	PA	1
ASPA	189.278	-14.326	-63.48	34.12	0.59	0.62	-0.06	-0.11	PA	1
THT0 ^h	210.394	-17.577	-65.81	34.40	0.36	0.28	0.06	-0.01	PA	1
KOKB	200.335	22.126	-62.15	34.67	0.37	0.28	0.19	-0.25	PA	1

KRTM	202.552	2.047	-67.16	34.77	0.27	0.21	-0.02	-0.13	PA	1
MCI0 ⁱ	153.979	24.290	-71.73	23.79	0.34	0.37	-0.01	-0.17	PA	1
MKEA	204.544	19.801	-62.45	34.94	0.23	0.19	-0.01	0.10	PA	1
KIRI	172.923	1.355	-67.75	31.28	0.45	0.34	-0.17	0.37	PA	1
ALBR	280.442	8.988	17.52	10.36	1.00	1.00	-1.80	-2.98	PM	14
CHEP	281.965	8.252	24.45	13.77	1.00	1.00	3.38	-2.94	PM	14
CHIT	279.594	7.989	25.83	11.64	1.00	1.00	4.24	0.18	PM	14
FLAM	280.480	8.910	19.63	11.86	1.00	1.00	0.13	-1.56	PM	14
CHEP	281.965	8.252	24.74	18.32	4.88	1.58	3.67	1.61	PM	15
CHIT	279.594	7.989	22.67	11.64	2.70	0.93	1.08	0.19	PM	15
ACP1	280.050	9.371	17.02	11.28	0.54	0.77	-1.41	-1.19	PM	1
ACP6	280.592	9.238	17.07	12.32	0.77	1.26	-1.68	-1.34	PM	1
AZUE	279.567	7.956	22.69	13.85	0.63	0.48	1.03	2.45	PM	1
PMPA	280.439	8.955	18.10	12.47	1.04	0.87	-1.29	-0.86	PM	1
BYSP	293.839	18.408	8.94	13.76	0.47	0.39	0.20	0.10	PR	1
CUPR	294.717	18.307	8.89	13.90	0.68	0.49	-0.02	-0.52	PR	1
MIPR	293.473	17.886	9.56	13.37	0.47	0.41	0.35	0.02	PR	1
MOPR	292.069	18.077	8.69	11.85	1.19	0.75	-0.25	-0.29	PR	1
P780	293.421	18.075	8.94	13.34	0.59	0.56	-0.09	0.04	PR	1
ZSU1	294.007	18.431	8.54	14.03	0.30	0.35	-0.19	0.22	PR	1
J746	131.291	25.954	-39.17	24.17	0.51	0.44	-0.10	0.47	PS	1
PALO ^j	134.450	7.328	-65.09	20.11	0.27	0.22	0.03	-0.12	PS	1
NMPL	39.258	-15.123	19.63	15.91	0.23	0.19	-0.01	-0.01	RO	16
PMBA	40.484	-12.964	20.31	15.91	1.41	0.72	0.30	0.14	RO	1
BELE	311.537	-1.409	-4.79	12.55	0.28	0.38	-0.03	0.10	SA	1
BRAZ	312.122	-15.947	-3.82	12.45	0.32	0.31	0.04	-0.03	SA	1
BRFO ^k	321.574	-3.877	-4.58	12.83	0.47	0.30	0.19	0.05	SA	1
CHPI	315.015	-22.687	-3.64	12.49	0.37	0.33	-0.04	-0.11	SA	1

KOUR	307.194	5.252	-5.33	12.87	0.38	0.35	-0.15	0.68	SA	1
LPGS	302.068	-34.907	-0.72	11.82	0.36	0.39	0.38	0.04	SA	1
MPL0 ^l	302.429	-38.006	-0.73	12.02	0.70	0.61	0.04	0.20	SA	1
RIOD	316.694	-22.818	-3.73	12.33	0.30	0.34	0.01	-0.34	SA	1
UFPO ^m	310.769	-25.448	-3.18	12.25	0.26	0.27	-0.17	-0.16	SA	1
VICO	317.130	-20.761	-3.86	12.43	0.36	0.43	0.04	-0.25	SA	1
JACQ	151.505	-5.645	15.54	-49.63	4.10	2.20	0.33	-0.04	SB	10
WITU	149.435	-4.688	26.14	-22.93	8.10	4.20	-1.28	0.16	SB	10
ABOZ	33.102	29.141	24.25	18.79	0.54	0.49	-0.04	-0.05	SI	6
ALON	34.607	31.708	22.46	19.20	0.39	0.34	-0.23	-0.26	SI	1
CSAR	34.890	32.488	22.12	19.57	0.29	0.22	-0.06	-0.01	SI	1
TELA	34.781	32.068	22.64	19.68	0.27	0.24	0.18	0.15	SI	1
J500	123.792	24.426	38.50	-61.22	1.22	1.92	-0.59	-0.93	SK	1
J748	124.692	24.642	35.51	-49.97	1.65	1.46	-0.31	-0.50	SK	1
J749	124.301	24.537	37.90	-53.92	1.00	0.72	0.52	0.25	SK	1
DAL1	301.322	-62.241	8.12	14.07	1.49	2.36	-4.00	-3.15	SL	17
PRA1	300.350	-62.478	7.12	15.20	1.87	3.16	-4.46	-3.36	SL	17
FERR	301.607	-62.086	14.54	17.50	0.26	0.24	1.97	0.67	SL	18
PRTT	300.334	-62.484	8.93	18.91	0.37	0.35	-2.64	0.33	SL	19
JUAN	299.604	-62.662	10.84	17.82	0.32	0.38	-0.35	-1.77	SL	19
FREI	301.019	-62.194	9.26	17.24	0.86	0.97	-3.10	-0.40	SL	1
MAL0 ⁿ	40.194	-2.996	17.60	10.84	0.54	0.48	0.31	-0.43	SO	1
REUN	55.572	-21.208	24.92	11.33	1.06	0.66	0.31	0.03	SO	1
SEY1	55.479	-4.674	16.98	11.02	0.68	0.48	-0.62	0.42	SO	1
VACS	57.497	-20.297	31.31	-23.68	1.06	0.79	0.46	-1.37	SO	1
J723	130.275	30.785	26.55	-21.39	1.45	0.84	-0.86	1.53	ST	1
J777	130.136	31.416	26.28	-9.47	3.90	1.80	-1.41	0.75	ST	1
PANG	111.670	-2.686	33.04	-8.89	1.17	0.79	-0.58	0.04	SU	20

NONN	108.263	16.004	34.06	-5.92	0.43	0.32	0.30	-0.21	SU	21
UTHA	100.013	15.384	33.23	-8.11	0.87	0.64	-0.34	-0.48	SU	21
UBRT	104.871	15.245	33.15	-7.82	0.45	0.32	-0.35	-0.37	SU	21
SRIS	104.416	14.901	32.64	-5.57	0.42	0.28	-0.50	0.56	SU	21
CHON	101.045	13.121	32.17	-6.26	4.56	2.96	-0.87	-0.14	SU	21
RYNG	101.033	12.764	32.43	-12.65	1.00	0.71	0.68	0.13	SU	21
PUER	118.851	10.086	30.17	-8.25	1.26	0.95	1.12	0.92	SU	21
TABA	108.891	0.863	29.07	-8.25	1.11	0.72	1.09	-0.12	SU	21
TANJ	106.176	-1.881	33.34	-13.63	1.00	0.70	1.60	-0.85	SU	21
PUER	118.851	10.086	89.61	-6.33	1.66	1.60	0.90	0.44	SU	22
TNGA	184.818	-21.149	89.25	-5.63	1.14	0.94	0.47	1.19	TO	1
TONG	184.821	-21.145	131.15	-26.00	0.73	0.70	-0.37	-0.75	TO	1
VAVS	186.017	-18.651	22.65	16.17	0.89	0.68	0.43	-0.14	TO	1
KIOM	33.912	-6.134	24.56	16.32	1.70	1.37	1.61	-0.24	VI	16
NZG2	33.183	-4.257	24.96	16.34	0.43	0.50	0.49	-0.47	VI	16
EBBE	32.445	0.038	23.74	17.55	0.35	0.23	-0.52	0.17	VI	1
MBAR	30.738	-0.601	24.14	17.09	0.82	0.76	0.33	-0.50	VI	1
NURK	30.090	-1.945	19.76	84.68	4.60	2.00	-5.16	1.43	VI	1
GUA1	152.943	-9.225	20.66	76.07	2.50	1.40	-2.22	-0.70	WL	10
LOUS	151.125	-8.535	25.66	63.97	2.90	1.80	5.02	-0.01	WL	10
MORO	147.590	-7.742	31.94	-11.70	0.80	0.80	-0.46	-0.21	WL	10
C053	113.860	34.030	32.63	-11.95	0.90	0.90	-1.00	-0.15	YA	1
F027	115.800	23.430	31.91	-12.51	0.33	0.30	-0.18	0.08	YA	1
SHAO	121.200	31.100	33.34	-11.61	0.33	0.37	0.41	-0.04	YA	1
WUHN	114.357	30.532	16.67	17.62	0.36	0.29	0.31	0.34	YA	1

Studies: 1) This Study, 2) [Floyd *et al.*, 2010], 3) [Müller *et al.*, 2013], 4) [Plattner *et al.*, 2007], 5) [Shen *et al.*, 2011], 6) [Reilinger and McClusky, 2011], 7) [Benford *et al.*, 2012], 8) [Manaker *et al.*, 2008], 9) [Kato *et al.*, 2003], 10) [Tregoning *et al.*, 1998], 11) [Tregoning, 2002], 12) [Wang *et al.*, 2007], 13) [Apel *et al.*, 2006], 14) [Drewes and Heidbach, 2012], 15) [Trenkamp *et al.*, 2002], 16) [Saria *et al.*, 2013], 17) [Dietrich *et al.*, 2004], 18) [Jiang *et al.*, 2009], 19) [Taylor *et al.*, 2008], 20) [Bock *et al.*, 2003], 21) [Simons *et al.*, 2007], 22) [Yu *et al.*,

2013]. Velocities were derived for concatenated time-series for: a) HART, HARK & HARB, b) CC06 & CHAN, c) CNMI & CNMR, d) NDBC & MSSC, e) NLIB & IACI, f) RCM5, RCM6 & RMND, g) GALA & GLPS, h) PAMA & THTI, i) MARC & MCIL, j) PAL1 & PALA, k) FORT & BRFT, l) MPLA & MPL2, m) PARA & UFPR, and n) MALI & MAL2

APPENDIX D GPS Data Analysis Details (IGS Format)

NGL/UNR GPS Data Analysis Strategy Summary

ANALYSIS CENTER	Nevada Geodetic Laboratory University of Nevada, Reno 1664. N. Virginia St. MS 178 Reno NV 89557 USA Data Archives: http://geodesy.unr.edu/
CONTACT PERSON	Dr. Geoffrey Blewitt E-mail: gblewitt (at) unr.edu
SOFTWARE USED	GIPSY/OASIS-II Version 6.1.1 developed at JPL
PRODUCTS USED	Final, non-fiducial daily products from JPL archive: ftp://sideshow.jpl.nasa.gov/pub/JPL_GPS_Products/Final Including: GPS satellite orbit estimates GPS satellite clock estimates WLPB estimates (widelane & phase biases) Name of TRF (terrestrial reference frame) Transformation parameter estimates to named TRF Time-pole parameter estimates GPS satellite eclipse times Name of IGS ANTEX antenna calibration file Auxiliary data updated periodically from JPL: IGS ANTEX antenna calibration file JPL planetary ephemeris CODE CA-P DCB (differential code biases)

	GPS receiver type codes GPS constellation configuration history IERS/BIH leap seconds history IERS earth orientation parameters Auxiliary data updated from IGS Central Bureau: http://igscb.jpl.nasa.gov/ IGS station receiver/antenna configuration history Auxiliary data from Chalmers University, Sweden: http://holt.oso.chalmers.se/loading/ Ocean tidal loading coefficients for all stations Custom daily data (from NGL/UNR) ftp://gneiss.nbmng.unr.edu/xfiles Transformation parameter estimates to frame NA12 Ref: http://dx.doi.org/10.1016/j.jog.2013.08.004
GPS DATA USED:	RINEX files from various archives, including: UNAVCO ftp://data-out.unavco.org CDDIS ftp://cddis.gsfc.nasa.gov CORS ftp://cors.ngs.noaa.gov/cors SIO ftp://garner.ucsd.edu EUREF ftp://igs.bkg.bund.de/EUREF GEONET ftp://ftp.geonet.org.nz GREF ftp://igs.bkg.bund.de/GREF IGN ftp://rgpdata.ign.fr AUSTRALIA ftp://ftp.ga.gov.au GSI ftp://terras.gsi.go.jp SONEL ftp://ftp.sonel.org
PREPARATION DATE	October 15, 2013
MODIFICATION DATES	October 15, 2013 Creation
EFFECTIVE DATE FOR DATA ANALYSIS	2011-12-17 onward using JPL version 2 reprocessing with IERS2010/IGS08 conventions

MEASUREMENT MODELS	
Preprocessing	RINEX header must be interpretable - approximate XYZ replaced with NGL database values - alias table replaces antenna type with IGS standard - fix obvious formatting errors - require antenna type has IGS ANTEX calibrations - non-calibrated radome set to "NONE" (IGS standard) Require minimum file size, typically ~18 hr/day Apply CA-P1 biases

	Fix non-compliant time-tags for older receiver types Remove non-GPS GNSS data (e.g., GLONASS) Remove L2C and C2 data Cycle slip detection Delete phase connected arcs < 20 minutes Carrier Phase: Decimated to 5 minutes Pseudorange: Carrier aided smoothing to 5 minutes
Basic Observable	Undifferenced ionosphere-free carrier phase, LC Undifferenced ionosphere-free pseudorange, PC
	Elevation angle cutoff: 7 degrees Sampling rate: 5 minutes Data weight, LC: 1 cm Data weight, PC: 1 m
Modeled observable	Undifferenced LC and PC combinations CA-P1 biases from CODE applied
RHC phase rotation corr.	Applied
Marker -> antenna	dN, dE, dU eccentricities from RINEX header applied
ARP eccentricity	to compute station marker coordinates
Ground antenna phase center cal.	PCV model from igs08_www.atx applied Receiver antenna and radome types from RINEX header
Troposphere	A priori model: Pressure from GPT model (Boehm et al, 2007) Hydrostatic delay from Davis (1985) Wet delay 10 cm Mapping Function: Global Mapping Function (GMF) Estimation: Zenith delay and horizontal gradients
Ionosphere	1st order effect: Removed by LC and PC combinations 2nd order effect: Not modeled
Plate motions	Not applied to apriori positions
Tidal	Solid earth tide: IERS 2010 Conventions
	Permanent tide: NOT removed from model, so NOT in estimated site coordinates
	Pole tide: IERS 2010 Conventions
	Ocean Tide Loading: Diurnal, Semidiurnal, MF, and MM Model: FES04

	Semiannual: Self-consistent equilibrium model hardisp.f from IERS2010
	Surface deformations computed with respect to instantaneous center of mass
	Ocean Pole Tide Loading: Not applied
Non-tidal loading	Atmospheric Pressure: Not applied
	Ocean Bottom Pressure: Not applied
	Surface Hydrology: Not applied
	Other Effects: None applied
Earth Orientation Parameter (EOP) Model	IERS 2010 Conventions for diurnal, semidiurnal, and long period tidal effects on polar motion and UT1
Satellite center of mass correction	Phase centers offsets from igs08_www.atx applied
Satellite antenna phase variations	PCV model w.r.t. phase center from igs08_www.atx applied
Relativistic corrections	Periodic Clock Corrections, (-2*R*V/c): Applied Gravitational Bending (Shapiro Delay): Applied
GPS Attitude model	GYM95 nominal yaw rate model from Bar-Sever (1996) and yaw rates estimated for Block II satellites

ORBIT MODELS (JPL ORBIT PRODUCTS)	
Geopotential	EGM2008 12x12 C20, C30, C40, C21, S21 from IERS2010 standards
	GM = 398600.4415 km**3/sec**2
	AE = 6378.1363 km
Third-body	Sun, Moon, and All Planets
	Ephemeris: JPL DE421

Solar radiation pressure	Block II/IIA/IIR: JPL empirical SRP model, GSMPM-10, Bar-Sever and Kuang, (2004) Sibthorpe et al, 2010

	Estimate GPS "Y-Bias" and solar radiation pressure(SRP) coefficient as constant with no a-priori constraint.
	Make small time-varying (stochastic) adjustments to SRP coefficients in spacecraft body-fixed X and Z directions (1% process noise sigma with 1 hr 11 sec updates and 4-hour correlation time.) Estimate tightly constrained time-varying empirical acceleration in spacecraft Y direction (0.01 nm/s^2 process noise sigma with 1 hr 11 sec updates and 4-hour correlation time.)

	Earth shadow model: conic model with oblate Earth, umbra and penumbra

	Earth albedo: applied

	Attitude Model: GYM95 yaw model from Bar-Sever (1996)
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Tidal forces	Solid earth tides: IERS 2010 Conventions

	Ocean tides: FES2004 to degree and order 30 with convolution formalism of Desai and and Yuan (2006)

	Solid Earth Pole tide: IERS 2010 conventions

	Ocean Pole tide: IERS 2010 conventions
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Relativity	Applied Acceleration due to point mass of Earth Acceleration due to geodesic precession Acceleration due to Lense-Thirring precession
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Numerical Integration	Variable high order Adams predictor-corrector with direct integration of second-order equations

	Integration step: variable

	Starter procedure: RKF

	Arc length: 30 hours centered at 12:00 of each day
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ESTIMATED PARAMETERS (APRIORI VALUES & SIGMAS)	
Adjustment	Stochastic Kalman filter/smooth implemented as square root information filter with smoother
Station coordinates	Daily PPP estimates for all sites Apply daily transformation into IGS08 and NA12
Satellite clock	Fixed to JPL clock products, which are given every 5 minutes relative to reference clock (e.g. USN3/AMC2)
Receiver clock	Estimate every 5 minutes relative to satellite clocks
Orbital	Fixed to JPL ECEF orbit products interpolated to 5 min
GPS Attitude	Fixed to JPL products: yaw rates when in eclipse
Troposphere	Zenith delay: random walk $5.0d-8$ km/sqrt(sec) Horizontal delay gradients: random walk $5.0e-9$ km/sqrt(sec)
	Mapping function: GMF
Ionosphere	1st order effects removed by LC and PC combinations and 2nd order effects not modeled
Ambiguity	Resolve ambiguities using WLPB products from JPL
Earth Orientation Parameters	Fix to JPL products: polar motion, polar motion rate, and LOD, where UT1 is integrated from estimated LOD

REFERENCE FRAMES	
Inertial	J2000 Geocentric
Terrestrial	Daily transformed coordinates into IGS08 and NA12
Interconnection	Precession: IAU 2006 Precession Theory
	Nutation: IAU 2006 Nutation Theory
	A priori EOPS: EOPC04 updated daily, with polar motion and length of day estimated daily

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THE GLOBAL EARTHQUAKE MODEL

The mission of the Global Earthquake Model (GEM) collaborative effort is to increase earthquake resilience worldwide.

To deliver on its mission and increase public understanding and awareness of seismic risk, the GEM Foundation, a non-profit public-private partnership, drives the GEM effort by involving and engaging with a very diverse community to:

- Share data, models, and knowledge through the OpenQuake platform
- Apply GEM tools and software to inform decision-making for risk mitigation and management
- Expand the science and understanding of earthquakes.

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 **GEM**
GLOBAL EARTHQUAKE MODEL
working together to assess risk