

Positive-definiteness of the Jacobian matrix of the Stokes system for homogeneous media

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The Stokes equation for incompressible fluid is stated as

$$\tau_{ij,j} - p_{,i} = f_i, \quad (1)$$

$$v_{i,i} = 0, \quad (2)$$

where τ_{ij} is the deviatoric stress tensor, p is pressure, v_i is velocity, and f_i stands for a body force. The weak form of the momentum conservative equation can be calculated by integrating the inner product of Eq. (1) and a virtual velocity δv_i across the computational domain Ω , which yields after integrating by part

$$\int_{\Omega} \delta \dot{\varepsilon}_{ij} \tau_{ij} d\Omega - \int_{\Omega} v_{i,i} d\Omega = \int_{\Omega} v_i f_i d\Omega, \quad (3)$$

where $\dot{\varepsilon}_{ij} \equiv (v_{i,j} + v_{j,i})/2$ denotes the strain rate tensor. Similarly, the weak form of mass conservative equation is obtained by multiplying Eq. (2) with a virtual pressure δp and integrating across Ω , which gives

$$\int_{\Omega} \delta p v_{i,i} d\Omega = 0. \quad (4)$$

With proper finite element approximation

$$v_i \approx \sum_I V^I \varphi_i^I, \quad p \approx \sum_I P^I \vartheta^I, \quad (5)$$

Eqs. (3) and (4) can be discretized into the algebraic form

$$\begin{bmatrix} \mathbf{A} & \mathbf{B}^T \\ \mathbf{B} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{V} \\ \mathbf{P} \end{bmatrix} = \begin{bmatrix} \mathbf{f} \\ \mathbf{0} \end{bmatrix}, \quad (6)$$

where the matrix and right-hand side blocks are defined by

$$A^{IJ} = \int_{\Omega} \varepsilon_{ij}^I \tau_{ij}^J d\Omega, \quad B^{IJ} = - \int_{\Omega} \varphi_{i,i}^I \vartheta^J d\Omega, \quad f^I = \int_{\Omega} \varphi_i^I f_i d\Omega.$$

In the above expressions, $\varphi_{ij}^I \equiv (\varphi_{i,j}^I + \varphi_{j,i}^I)/2$, and τ_{ij}^I is a function of φ_{kl}^I and ϑ^I satisfying $\sum_I \tau_{ij}^I V^I = \tau_{ij}$. For instance, if the fluid is Newtonian, then we have $\tau_{ij}^I = 2\eta \varphi_{ij}^I$, hence $\sum_I \tau_{ij}^I V^I = 2\eta \dot{\varepsilon}_{ij} = \tau_{ij}$. However, in geodynamic problems the relationship between τ_{ij} and $\dot{\varepsilon}_{kl}$ is generally nonlinear.

We employ the Newton-Raphson method to resolve the nonlinearity in Eq. (6). In each Newton iteration, we need to solve the linearized system

$$\begin{bmatrix} \mathbf{J}_{vv} & \mathbf{J}_{vp} \\ \mathbf{J}_{pv} & \mathbf{0} \end{bmatrix} \begin{bmatrix} d\mathbf{V} \\ d\mathbf{P} \end{bmatrix} = \begin{bmatrix} \mathbf{f} \\ \mathbf{0} \end{bmatrix} - \begin{bmatrix} \mathbf{A} & \mathbf{B}^T \\ \mathbf{B} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{V} \\ \mathbf{P} \end{bmatrix}. \quad (7)$$

The blocks of the Jacobian matrix have the following form:

$$J_{vv}^{IJ} = \int_{\Omega} \varphi_{ij}^I \frac{\partial \tau_{ij}}{\partial \dot{\epsilon}_{kl}} \varphi_{kl}^J d\Omega, \quad J_{vp}^{IJ} = \int_{\Omega} \varphi_{ij}^I \frac{\partial \tau}{\partial p} \vartheta^J d\Omega + B^{JI}, \quad J_{pv}^{IJ} = B^{IJ}.$$

More specifically, we assume that the material is *homogeneous*, i.e. τ_{ij} is parallel with $\dot{\epsilon}_{ij}$. In such cases, τ_{ij} can be expressed as

$$\tau_{ij} = 2\eta(\dot{\epsilon}, p)\dot{\epsilon}_{ij}, \quad (8)$$

where $\dot{\epsilon} \equiv \sqrt{\dot{\epsilon}_{ij}\dot{\epsilon}_{ij}}$ is the norm of $\dot{\epsilon}_{ij}$. Substitution of Eq. (8) in the expression of J_{vv}^{IJ} gives

$$J_{vv}^{IJ} = \int_{\Omega} 2\varphi_{ij}^I \left(\eta I_{ijkl}^s + \dot{\epsilon}_{ij} \frac{\partial \eta}{\partial \dot{\epsilon}_{kl}} \right) \varphi_{kl}^J d\Omega, \quad (9)$$

where $I_{ijkl}^s \equiv (\delta_{ik}\delta_{jl} + \delta_{il}\delta_{jk})/2$ is the symmetric projection tensor. Eq. (9) is equivalent to Eq. (14) in Fraters et al. [2019].

As illustrated by Fraters et al. [2019], to employ the Schur complement preconditioner to solve Eq. (7), we must guarantee that \mathbf{J}_{vv} is symmetric and positive-definite, otherwise the top-left block of the preconditioner cannot be implicitly inverted with the CG solver. To analyze the properties of \mathbf{J}_{vv} , we shall expand $\dot{\epsilon}_{ij} \frac{\partial \eta}{\partial \dot{\epsilon}_{kl}}$ straightforwardly:

$$\dot{\epsilon}_{ij} \frac{\partial \eta}{\partial \dot{\epsilon}_{kl}} = \epsilon_{ij} \frac{\partial \eta}{\partial \dot{\epsilon}} \frac{\partial \dot{\epsilon}}{\partial \dot{\epsilon}_{kl}} = \dot{\epsilon}_{ij} \frac{\partial \eta}{\partial \dot{\epsilon}} \frac{\dot{\epsilon}_{kl}}{\dot{\epsilon}} = \dot{\epsilon} \frac{\partial \eta}{\partial \dot{\epsilon}} \frac{\dot{\epsilon}_{ij}}{\dot{\epsilon}} \frac{\dot{\epsilon}_{kl}}{\dot{\epsilon}}. \quad (10)$$

Eq. (10) implies that J_{vv}^{IJ} is always symmetric. The positive-definiteness of J_{vv}^{IJ} , on the other hand, is not guaranteed since it depends on $\partial \eta / \partial \dot{\epsilon}$. For simplicity, we define

$$E \equiv \dot{\epsilon} \frac{\partial \eta}{\partial \dot{\epsilon}} \quad \text{and} \quad n_{ij} \equiv \frac{\dot{\epsilon}_{ij}}{\dot{\epsilon}}.$$

As seen, E is a scalar quantity in units of Pa·s, and n_{ij} is the unit tensor parallel to $\dot{\epsilon}_{ij}$. Then Eq. (10) can be rewritten as

$$\dot{\epsilon}_{ij} \frac{\partial \eta}{\partial \dot{\epsilon}_{kl}} = E n_{ij} n_{kl}. \quad (11)$$

It is easy to see from Eq. (11) that $\dot{\epsilon}_{ij} \frac{\partial \eta}{\partial \dot{\epsilon}_{kl}}$ has only one non-trivial eigenvalue E . In fact, we may consider n_{ij} as a 2-D unit vector on the π -plane of the principal strain rate space (the 3-D space with principal strain rate $\dot{\epsilon}_1$, $\dot{\epsilon}_2$ and $\dot{\epsilon}_3$ as coordinate axes), which is equivalent to applying a rotational transformation to n_{ij} . Denote the unit vector by $\mathbf{n} \equiv [\cos \phi \ \sin \phi]^T$, then Eq. (11) can be explicitly expressed as

$$E \mathbf{n} \mathbf{n}^T = E \begin{bmatrix} \cos^2 \phi & \cos \phi \sin \phi \\ \cos \phi \sin \phi & \sin^2 \phi \end{bmatrix}. \quad (12)$$

It is clear that the eigenvalues of $E \mathbf{n} \mathbf{n}^T$ are 0 and E . Consequently, the Jacobian matrix \mathbf{J}_{vv} is positive-definite as long as $E > -\eta$.

1 Power-law creep

The power-law creep is generally stated as

$$\eta = \eta_0 \dot{\epsilon}^{\frac{1}{n}-1}, \quad (13)$$

where η_0 is the prefactor, and n is a dimensionless parameter satisfying $n \geq 1$. Straightforward derivation gives

$$E = \eta_0 \left(\frac{1}{n} - 1 \right) \dot{\epsilon}^{\frac{1}{n}-1} = \left(\frac{1}{n} - 1 \right) \eta. \quad (14)$$

Since $n \geq 1$, we always have $E > -\eta$, which implies that \mathbf{J}_{vv} for the power-law rheology is always positive-definite.

2 The Drucker-Prager model

The yield function of the Drucker-Prager model is defined as

$$F = \frac{\tau}{\sqrt{2}} - \xi p - \zeta, \quad (15)$$

where $\tau \equiv \sqrt{\tau_{ij}\tau_{ij}}$, ξ and ζ are material parameters determined by the friction angle and the cohesion. When plastic yielding occurs, we have $F = 0$, which indicates that

$$\frac{\tau}{\sqrt{2}} = \xi p + \zeta. \quad (16)$$

Thus, we have

$$\eta = \frac{\tau}{2\dot{\epsilon}} = \frac{\xi p + \zeta}{\sqrt{2}\dot{\epsilon}}, \quad (17)$$

and

$$E = -\frac{\xi p + \zeta}{\sqrt{2}\dot{\epsilon}} = -\eta. \quad (18)$$

The equation above implies that \mathbf{J}_{vv} for the Drucker-Prager model is non-negative-definite (as plastic yielding does not occur everywhere). To restore the positive-definiteness of the top-left block, we should scale the Newton step with a factor $\alpha \in (0, 1)$.

3 Maxwell viscoplastic model

Simulations of lithosphere dynamics often employ a Maxwell-type viscoplastic model with an additive decomposition

$$\dot{\epsilon} = \dot{\epsilon}_v + \dot{\epsilon}_p, \quad (19)$$

where the subscripts v and p stand for viscous and plastic contributions, respectively. Thus, the comprehensive viscosity can be expressed as

$$\eta = \left(\frac{1}{\eta_v} + \frac{1}{\eta_p} \right)^{-1}, \quad (20)$$

where η_v and η_p are defined by Eq. (13) and Eq. (17), respectively. Then we have

$$E = -\dot{\epsilon}\eta^2 \left(-\frac{1}{\eta_v^2} \frac{\partial \eta_v}{\partial \dot{\epsilon}} - \frac{1}{\eta_p^2} \frac{\partial \eta_p}{\partial \dot{\epsilon}} \right) = \eta^2 \left(\frac{E_v}{\eta_v^2} + \frac{E_p}{\eta_p^2} \right) = \eta^2 \left(\frac{\frac{1}{n} - 1}{\eta_v} - \frac{1}{\eta_p} \right) = \left(\frac{\eta}{n\eta_v} - 1 \right) \eta. \quad (21)$$

As seen, \mathbf{J}_{vv} for Maxwell viscoplastic model is also positive-definite. In practice, however, we often run into situations with $\eta_p \ll \eta_v$, which makes $\frac{\eta}{n\eta_v}$ close to 0. Therefore, to guarantee the convergence of the CG solver, we had better scale the Newton step for Maxwell viscoplastic models as well.

References

M R T Fraters, W Bangerth, C Thieulot, A C Glerum, and W Spakman. Efficient and practical Newton solvers for non-linear Stokes systems in geodynamic problems. *Geophysical Journal International*, 218(2):873–894, August 2019. ISSN 0956-540X. doi: 10.1093/gji/ggz183.