

PID Tuning Cheatsheet for a Servo with a Fast Current (Torque) Loop

Goal: Practical recipe to pick **PID** gains for a **single outer position loop** when the drive's **current loop is fast** (~20 kHz), so torque is proportional to current command.

1) Assumptions & Symbols

- Inner current loop tightly closed \rightarrow torque follows command:

$$\tau(t) \approx K_t i_q^*(t)$$

- Use an effective torque gain (K_t) (set ($K_t=K_t$) if your controller outputs current; otherwise fold it into PID gains).
- Mechanical plant about motor shaft (load reflected): inertia (J), viscous damping (b).
- Laplace variable (s), position ($\Theta(s)$), speed ($\Omega(s)$).
- Mechanical pole (no control):

$$\omega_m = \frac{b}{J} \quad [\text{rad/s}]$$

2) Plant and Loop Definitions

Torque \rightarrow motion:

$$G_{\omega\tau}(s) = \frac{\Omega(s)}{\tau(s)} = \frac{1}{Js + b}, \quad G_{\theta\tau}(s) = \frac{\Theta(s)}{\tau(s)} = \frac{1}{s(Js + b)}.$$

Controller (PID):

Ideal form

$$C_{\text{ideal}}(s) = K_p + \frac{K_i}{s} + K_d s = \frac{K_d s^2 + K_p s + K_i}{s}.$$

Practical derivative (noise-friendly)

$$C(s) = K_p + \frac{K_i}{s} + \frac{K_d s}{1 + \tau_d s}.$$

Open loop (unity position feedback):

$$L(s) = C(s) K_{\tau} G_{\theta_{\tau}}(s).$$

Closed-loop complementary sensitivity (command \rightarrow position):

$$T(s) = \frac{\Theta(s)}{R(s)} = \frac{L(s)}{1 + L(s)}.$$

Sensitivity (disturbance rejection; error to reference):

$$S(s) = \frac{1}{1 + L(s)}.$$

With ideal PID, these expand to

$$L_{\text{ideal}}(s) = \frac{K_{\tau}(K_d s^2 + K_p s + K_i)}{J s^3 + b s^2},$$

$$T_{\text{ideal}}(s) = \frac{K_{\tau}(K_d s^2 + K_p s + K_i)}{J s^3 + (b + K_{\tau} K_d) s^2 + (K_{\tau} K_p) s + (K_{\tau} K_i)}.$$

Stability margins (from Bode of $(L(j\omega))$):

$$\text{PM} = 180^\circ + \angle L(j\omega_{gc}), \quad \text{GM}_{\text{dB}} = -20 \log_{10} |L(j\omega_{pc})|.$$

Recommended: PM 45–60°, GM 6–10 dB.

3) One-Shot Tuning Recipe (Position Loop Only)

Shapes the loop to look like $(\sim K/s)$ at crossover (good damping).

A. “Velocity feedback”: place controller zero near the mechanical pole

$$T_d = \frac{J}{b}, \quad K_d = K_p T_d.$$

B. Pick target crossover (ω_c) . Start with $(\omega_c \in [0.5, 2] \omega_m)$.

C. Proportional gain (unity-gain at crossover)

$$\boxed{K_p = \frac{b \omega_c}{K_{\tau}}}.$$

D. Add slow integral (remove steady-state error)

$$T_i \in \left[\frac{8}{\omega_c}, \frac{16}{\omega_c} \right], \quad \boxed{K_i = \frac{K_p}{T_i}}.$$

E. Filter derivative

$$\tau_d \approx \frac{1}{10\omega_c}.$$

Summary (compute in this order):

1. ($T_d = J/b$)
2. choose (ω_c)
3. ($K_p = b \cdot \omega_c / K_\tau$)
4. ($K_d = K_p T_d$)
5. choose ($T_i \in [8, 16] / \omega_c$) and set ($K_i = K_p / T_i$)
6. ($\tau_d \approx 1 / (10 \omega_c)$)

4) How to Verify

- **Bode of (L)** → read PM/GM.
- **Step of (T)** → rise/overshoot/settling; integrator zero steady-state error.
- **Bode of (S)** → low-frequency ($|S|$) small is good.
- **Control effort** ($C/(1+L)$) → check torque limits; add anti-windup if needed.

5) Worked Example

Given ($J=0.01$) $\text{kg} \cdot \text{m}^2$, ($b=0.001$) $\text{N} \cdot \text{m} \cdot \text{s}/\text{rad}$, ($K_\tau = K_t = 0.10$) $\text{N} \cdot \text{m}/\text{A}$:

- ($\omega_m = b/J = 0.1$) rad/s
- choose ($\omega_c = 1.0$) rad/s
- ($T_d = J/b = 10$) s
- ($K_p = b \cdot \omega_c / K_\tau = 0.010$)
- ($K_d = K_p T_d = 0.10$)
- ($T_i = 8 / \omega_c = 8$) s ($K_i = 1.25 \times 10^{-3}$)
- ($\tau_d \approx 1 / (10 \omega_c) = 0.10$) s

6) Python Snippet (Step & Bode)

```
import control as ctl, matplotlib.pyplot as plt, math

# Example parameters
J, b, K_tau = 0.01, 0.001, 0.10
omega_c = 1.0
T_d = J/b
Kp = b*omega_c/K_tau
Kd = Kp*T_d
Ti = 8/omega_c
Ki = Kp/Ti
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tau_d = 1/(10*omega_c)

s = ctl.TransferFunction.s
G = 1/(s*(J*s+b))
C = Kp + Ki/s + (Kd*s)/(1+tau_d*s)

L = C*K_tau*G
T = ctl.feedback(L,1)
S = 1/(1+L)

gm, pm, wg, wp = ctl.margin(L)
print(f"GM={gm:.2g} ({20*math.log10(gm):.1f} dB) @ {wg:.3g} rad/s, PM={pm:.1f}° @ {wp:.3g} rad/s")

t, y = ctl.step_response(T)
plt.figure(); plt.plot(t,y); plt.grid(True); plt.title("Closed-loop Step"); plt.xlabel("Time")
plt.figure(); ctl.bode(L, dB=True); plt.suptitle("Open-loop Bode"); plt.show()

```

7) Practical Notes

- Too slow? Increase (ω_c) \rightarrow raise (K_p); keep ($T_d=J/b$), reduce (T_i); keep ($\tau_d \approx 1/(10\omega_c)$).
- Ringing / low PM? Lower (ω_c) or increase phase lead slightly (increase (T_d)); if integral is aggressive, increase (T_i).
- Noisy control? Increase (τ_d) or lower (ω_c).
- Friction (Coulomb/stiction): treat as disturbance; stronger integral helps but watch overshoot/windup.
- Gearing & load reflection: if gear ratio ($N=\omega_m/\omega_L$),

$$J = J_m + N^2 J_L, \quad b = b_m + N^2 b_L, \quad \theta_L = \theta_m / N.$$

- Resonances/compliance: consider notch filters or add an inner velocity loop.
- Anti-windup: clamp integrator or back-calculate when torque saturates.