

# Dynamic System Modeling & PID Controller Design for a Molten Salt Microreactor

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**University**ofIdaho

Department of Nuclear Engineering  
and Industrial Management

## Experience

B.S Chemical Engineering (2015-2019) - Michigan Technological University  
M.S. Nuclear Engineering (2021-2023) - University of Idaho - NRC Fellow  
Modeling and Simulation Intern at Idaho National Lab

## Select Publications

Root, S. J., et al., 2023. Thermodynamic analysis on xenon stripping to shorten restart time in molten salt microreactors.  
Nuclear Engineering and Design 414, 112606

Root, S. J., et al., 2023. Cyber hardening of nuclear power plants with real-time nuclear reactor operation, 1. preliminary operational testing.  
Progress in Nuclear Energy 162, 104742

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1 The Molten Salt Nuclear Battery

2 Process Control Engineering

3 Reactor Characterization

4 Results and Analysis

5 Conclusions

## 1 The Molten Salt Nuclear Battery

## 2 Process Control Engineering

## 3 Reactor Characterization

## 4 Results and Analysis

## 5 Conclusions

## Gen-IV

- Complete re-designs
- Smaller footprint
- Deployability
- Versatility

## Molten Salt Reactors

## Microreactors

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## Gen-IV

### Molten Salt Reactors

- High temperature
- Low pressure
- High specific heat

### Microreactors

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## Gen-IV

## Molten Salt Reactors

## Microreactors

- Less than 50 MW
- Assembly line manufacturing
- Deliver/installation vs. construction

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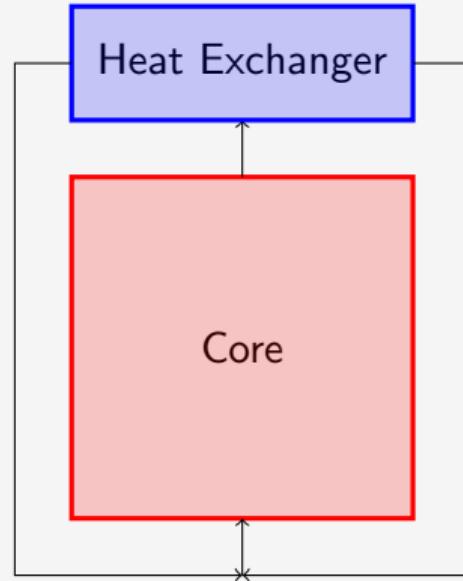
Conclusions

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## Fuel/Primary Coolant

- Self-Contained liquid fueled molten salt micro-reactor
- 10 year design
- 10 MWth using HALEU  $UF_4$  dissolved in  $FLiNaK$
- Natural circulation driven

## Control Drums



Simplified schematic drawing of an MSNB

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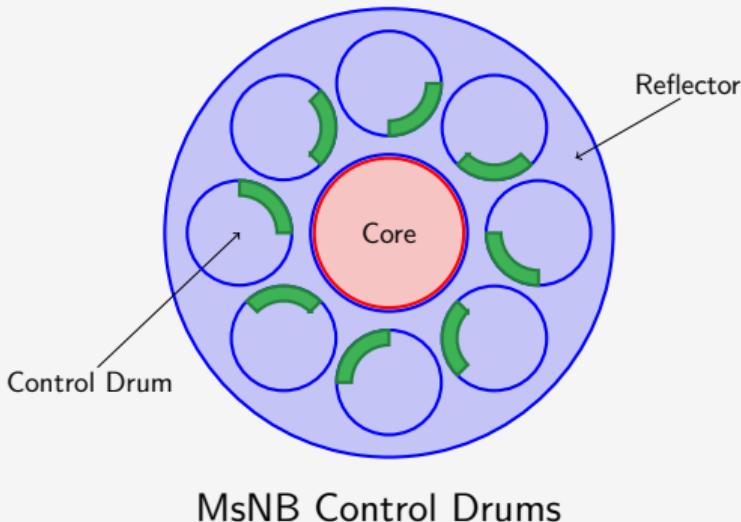
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## Fuel/Primary Coolant

## Control Drums

- Criticality is manipulated using axial control drums
- Neutron absorber plate covering cylinders of neutron reflector
- Drums are rotated to point more absorber towards the core to insert negative control reactivity



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## Neutronics [3]

- Control drums give a uniform axial and radial flux profile for all reactivity insertions
- Control drum vs. reactivity curve is sinusoidal

## Thermal Hydraulics [4]

## Process Control

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[3] Peterson, J., 8 2019. An analysis of the nuclear characteristics of a molten salt microreactor.  
Master's thesis, University of Idaho

[4] Carter, J. P., 2022. Multi-physics investigation of a natural circulation molten salt micro-reactor that utilizes an experimental in-pile device to improve core physics and system thermal-hydraulic performance.  
Ph.D. thesis, University of Idaho

## Neutronics [3]

## Thermal Hydraulics [4]

- Transient simulations can be reduced to 1D and still correspond to STAR-CCM+
- Stable autonomous load following for relatively small ramp function power demand transients

## Process Control

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## Neutronics [3]

## Thermal Hydraulics [4]

## Process Control

- Design controller *compliment* the autonomous capabilities provided by the passive feedback mechanisms
- Allow larger faster, more aggressive power changes
- Return MSNB to steady-state operation faster

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[3] Peterson, J., 8 2019. An analysis of the nuclear characteristics of a molten salt microreactor. Master's thesis, University of Idaho

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# Control Theory

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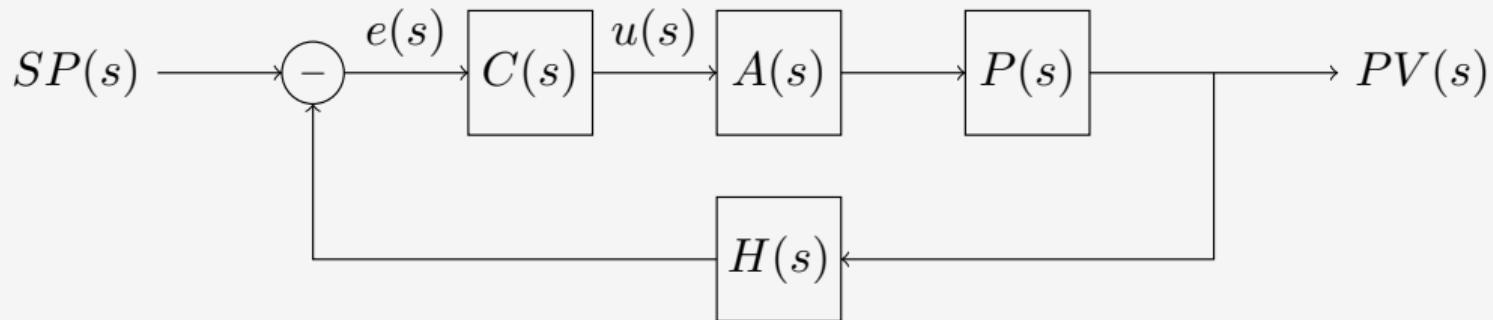
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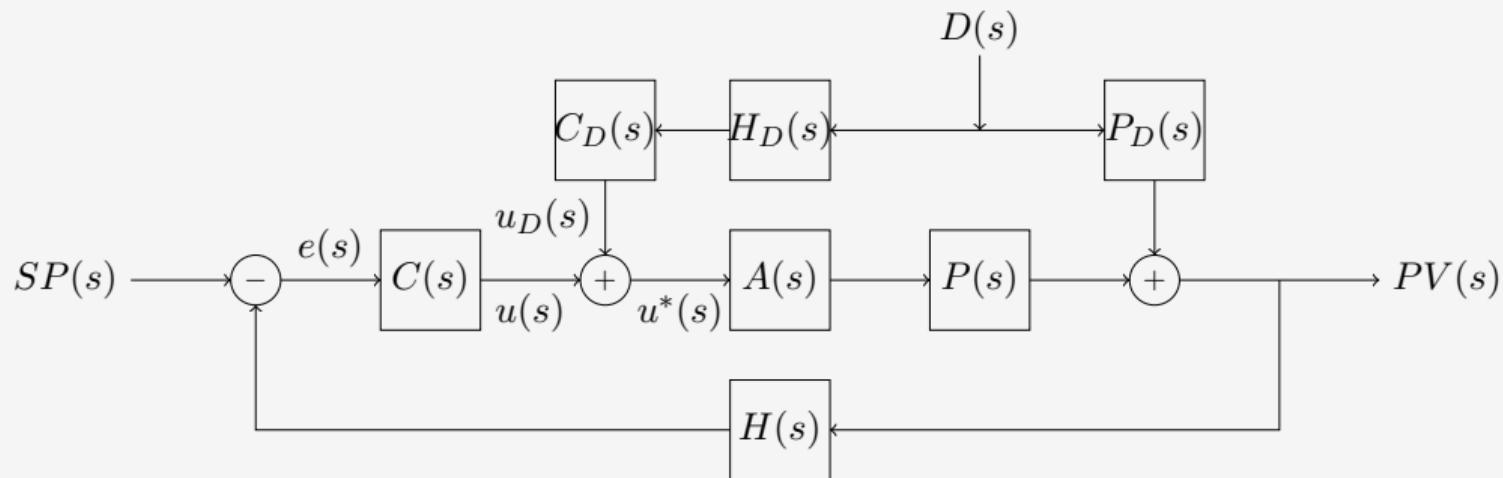
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$$u(t) = \underbrace{K_P e(t)}_{\text{Proportional}} + \underbrace{K_I \int_0^t e(t) dt}_{\text{Integral}} + \underbrace{K_D \frac{de(t)}{dt}}_{\text{Derivative}}$$

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## Proportional

- Control output is manipulated in proportion to the error defined by the proportional gain constant
- High gain yields an aggressive controller that is prone to overshooting the set-point
- Low gain may result in steady-state offset

## Integral

## Derivative

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## Proportional

## Integral

- Considers cumulative error to help eliminate steady-state offset
- As the process variable settles around the set-point, the cumulative error approaches a constant value and the effect of the integral controller diminishes.

## Derivative

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Proportional

Integral

Derivative

- Estimates the time rate of change of the error to dampen overshoot
- Backs-off the proportional response when the process variable rapidly approaches the set-point
- Can be difficult to tune

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# Transport Delay Problem

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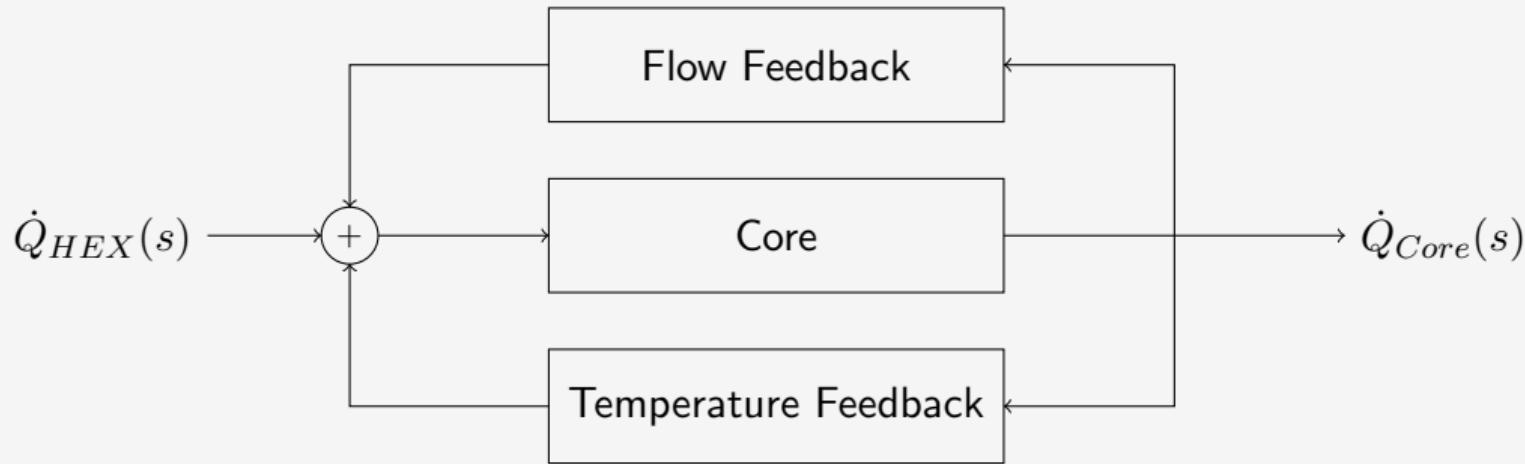
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Simplified block diagram of two primary passive feedback mechanisms in an MSNB

### Doppler broadening

- Resonance peaks lower and broaden with increased temperature
- High kinetic energy of target nucleus introduces more relative uncertainty of the center-of-mass energy [5, Ch. 7]
- More epithermal neutrons absorbed by  $^{238}U$  etc. [6, Ch. 6]

### Thermal Expansion

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[5] Kerlin, T. W. et al., 2019. Dynamics and Control of Nuclear Reactors.  
Knoxville, Tennessee: Elsevier Inc

[6] Duderstadt, J. J. et al., 1976. Nuclear Reactor Analysis.  
New York, NY: Wiley & Sons, first edition

### Doppler broadening

### Thermal Expansion

- Increased temperature leads to lower heavy metal density and smaller macroscopic fission cross-section at high temperature [3]
- Similar to moderator thinning in LWRs

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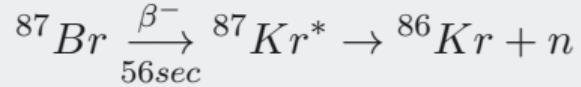
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### Delayed Neutron Precursors

- Most fission events release daughter neutrons *promptly*
- Sometimes, unstable nuclides which decay by neutron emission are produced instead
- $t_{1/2}$  from less than a second to over a minute [7, Ch. 6]



### Flowing Fuel

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### Delayed Neutron Precursors

### Flowing Fuel

- Precursors produced near the core exit and long lived precursors may emit their neutrons outside of the core
- These neutrons are effectively lost from the fission chain reaction [5, Ch. 3]
- Larger power transport requires a higher flow rate
- Greater delayed neutron losses
- Negative feedback

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## Dynamics associated with anticipated transients

- Natural circulation flow mode
- Passive feedback mechanisms
- Transport delays separating heat exchanger and core

## Thought Experiment

- Step increase in power demand to a steady-state critical MSNB
- Set-point is instantaneously equal to heat exchanger power consumption
- Ideal controller which produces rapid load following with minimal overshoot

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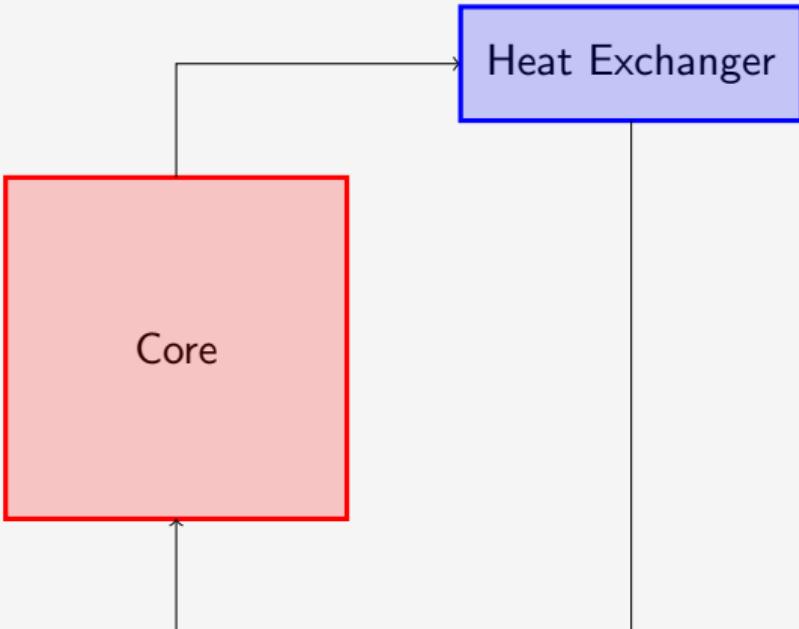
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# Main Operational Control Problem - Transport Delay



Simplified schematic drawing of a natural circulation MSNB

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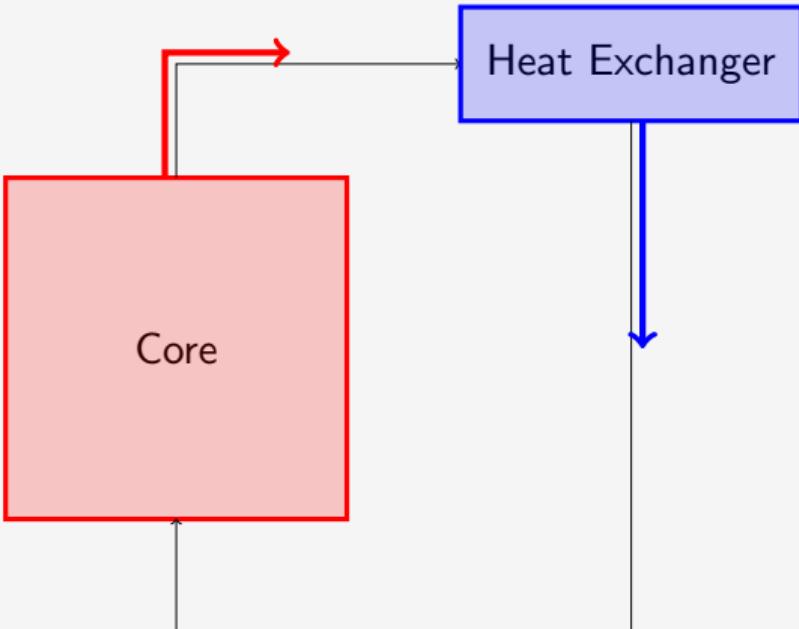
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# Main Operational Control Problem - Transport Delay

Immediate Response



Simplified schematic drawing of a natural circulation MSNB

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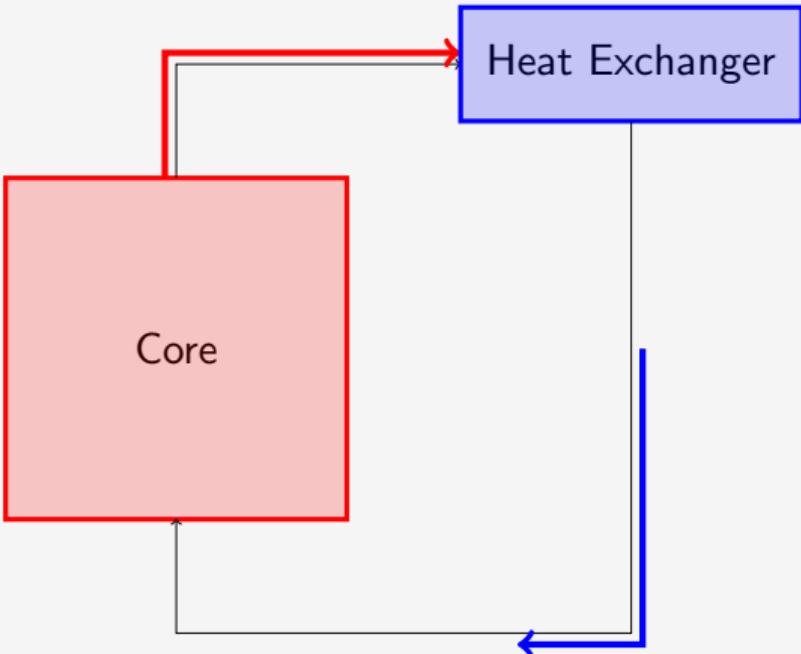
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# Main Operational Control Problem - Transport Delay

## Heat Exchanger Perturbation



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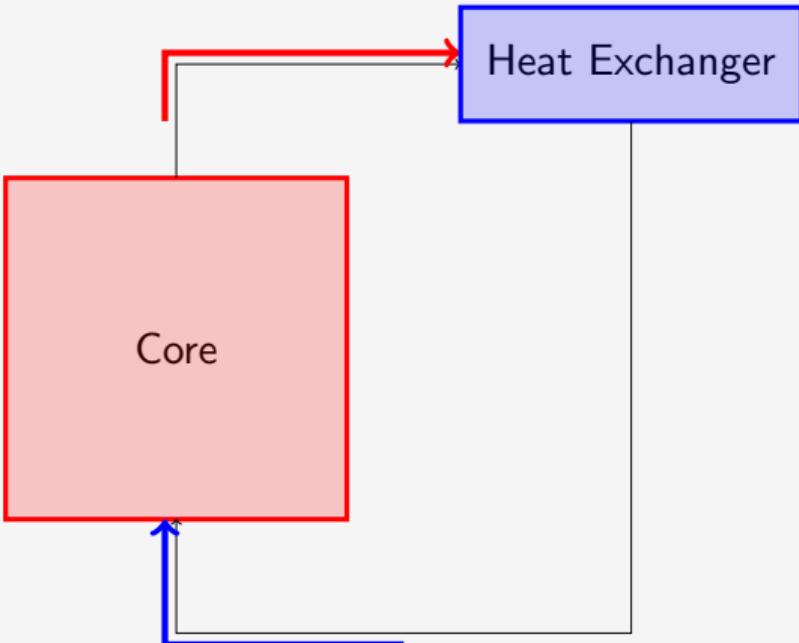
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Core Perturbation



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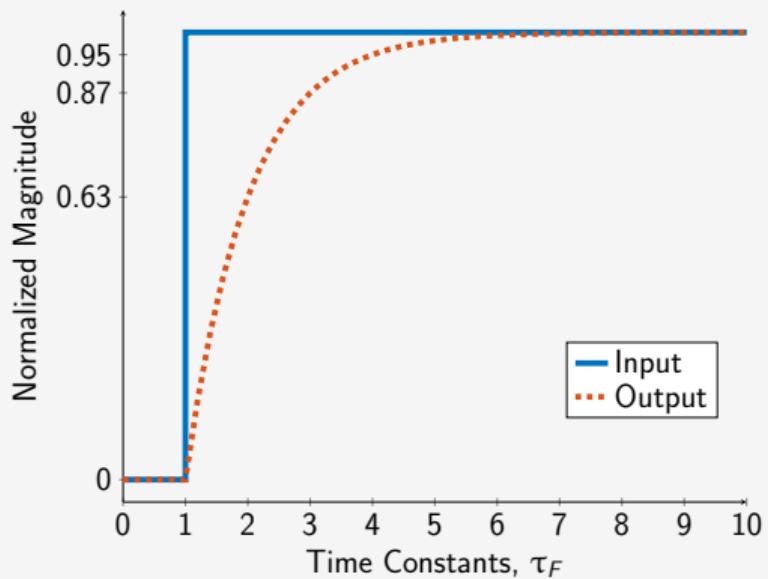
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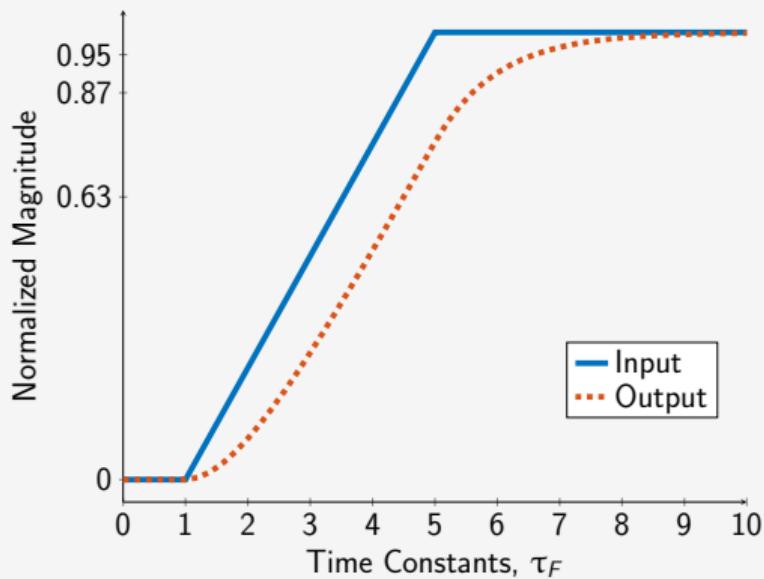
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Pre-Filter on a step-function



Pre-Filter on a ramp-function

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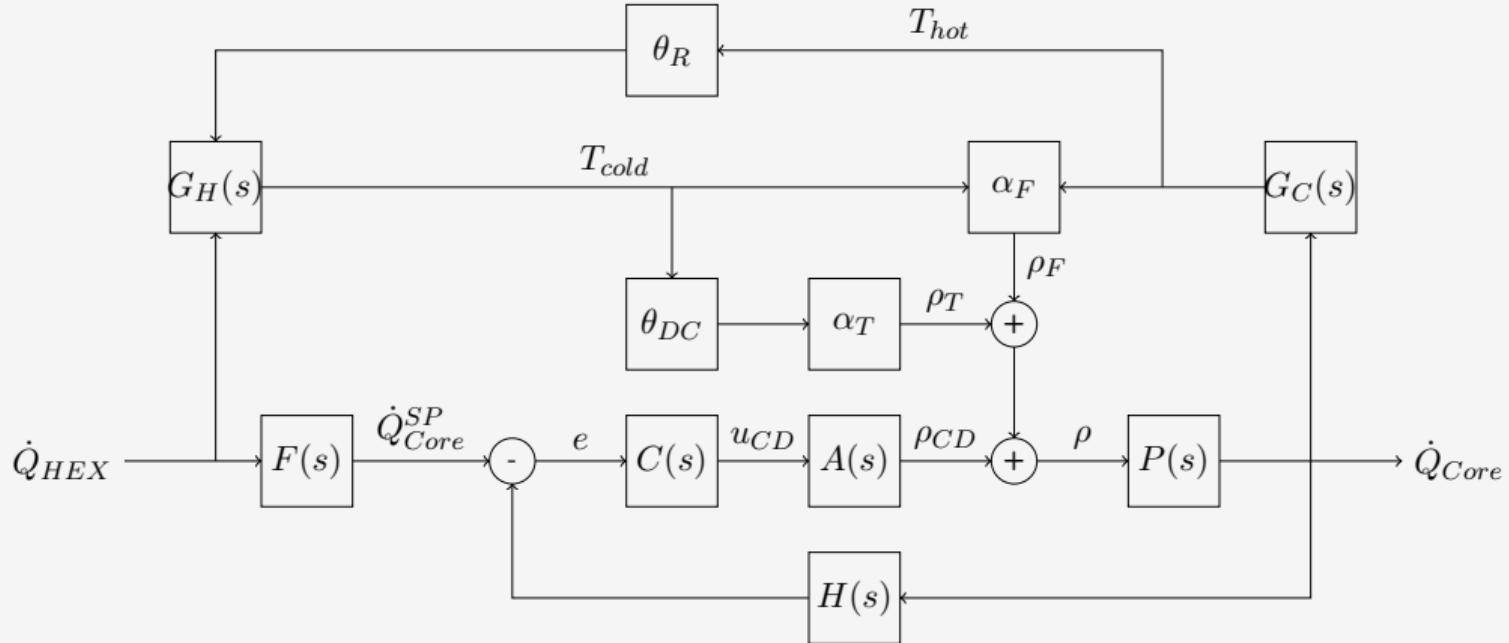
2 Process Control Engineering

3 Reactor Characterization

- Neutronics Modeling
- Process Simulation

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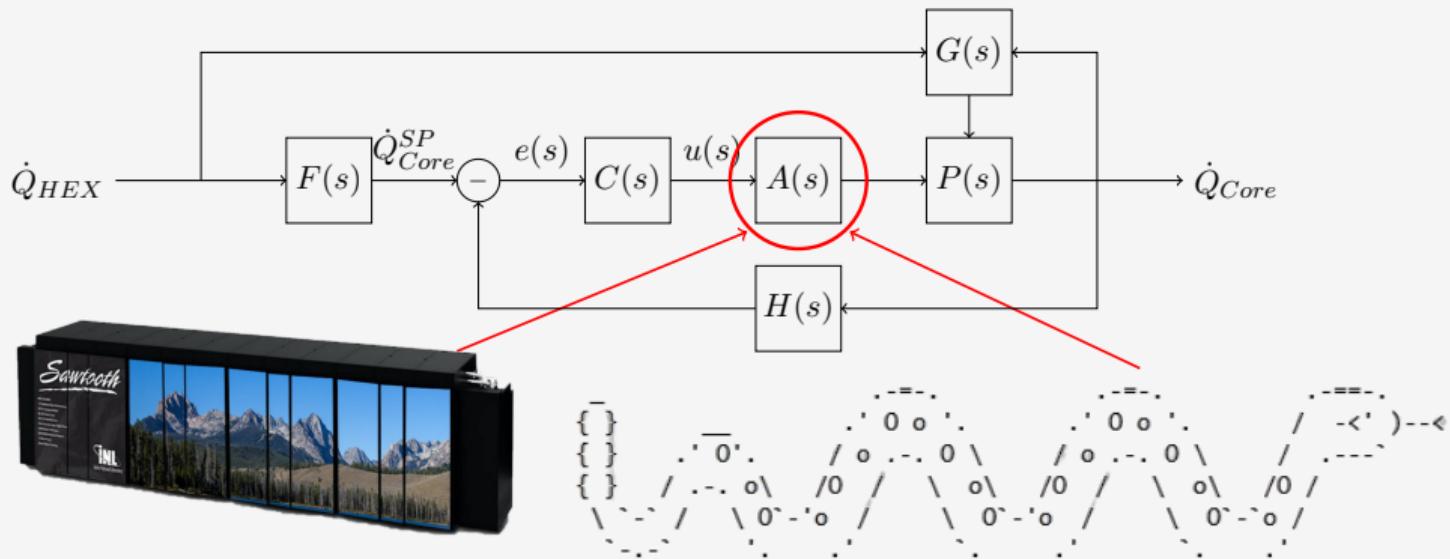
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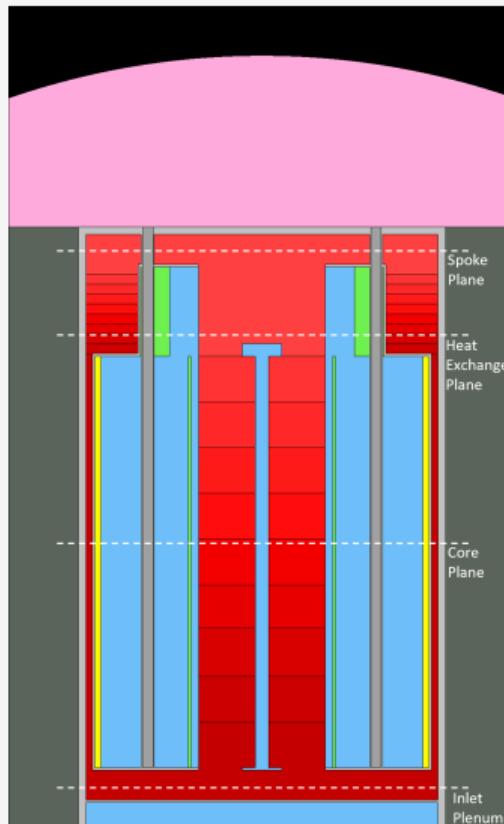
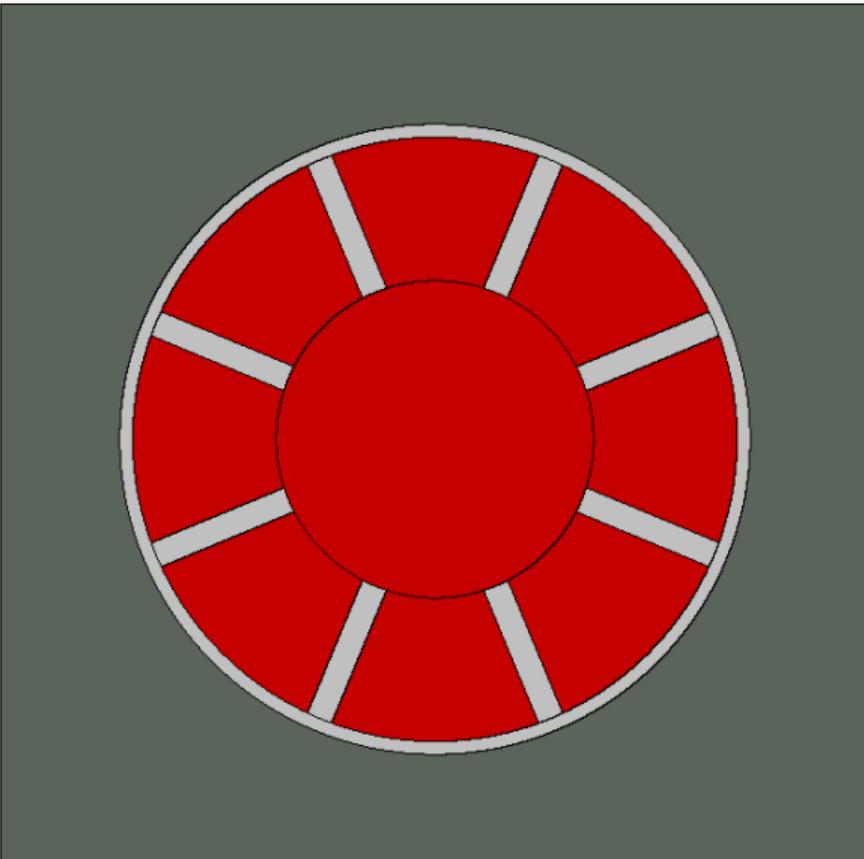
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# Geometry Specification



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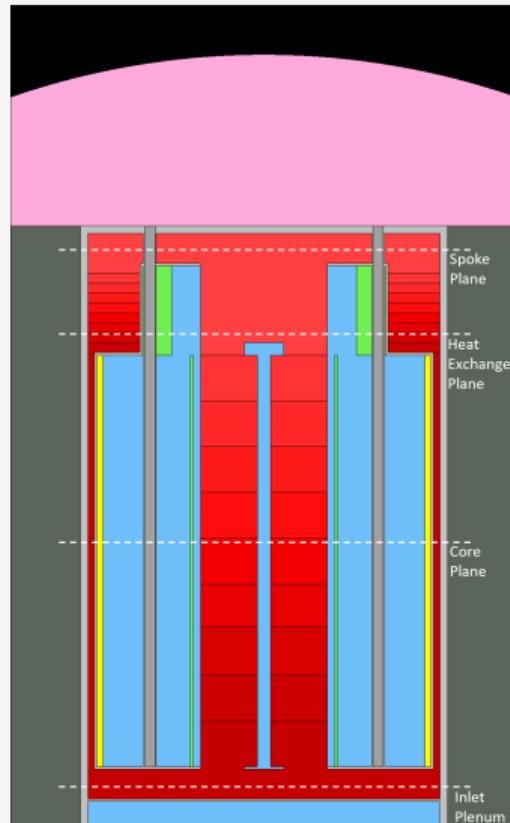
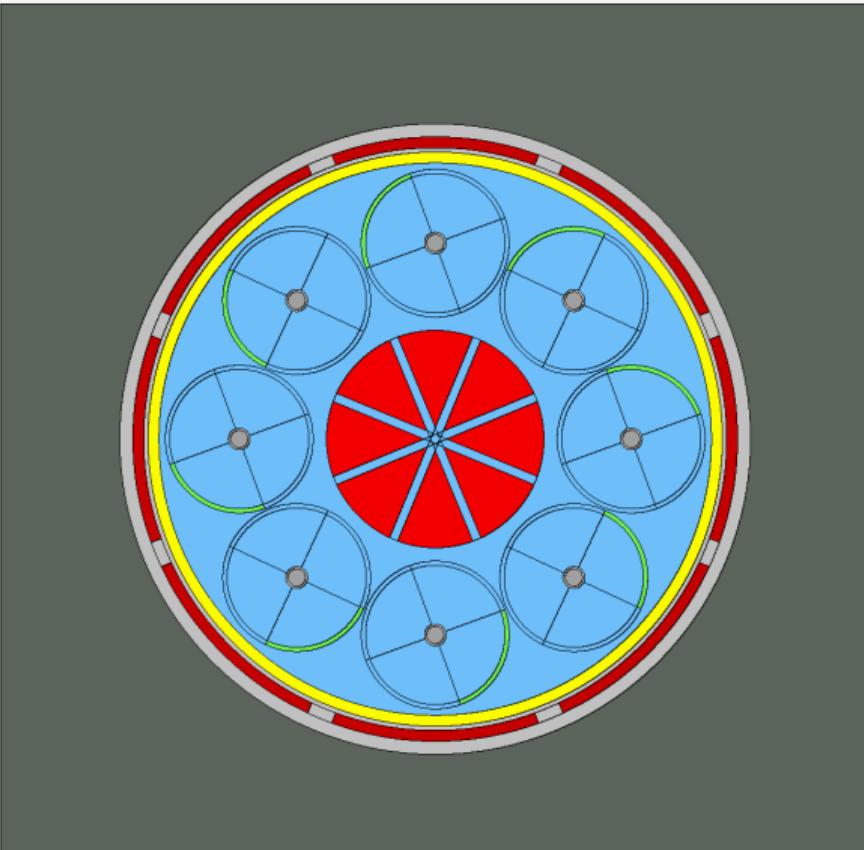
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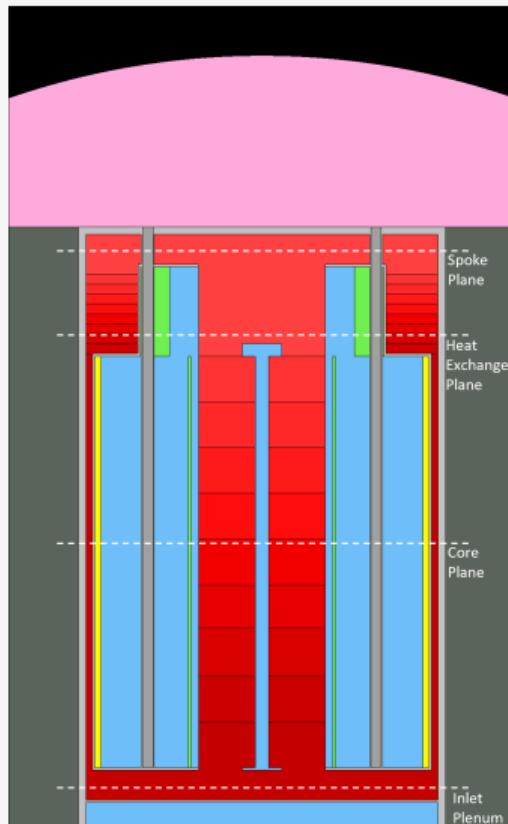
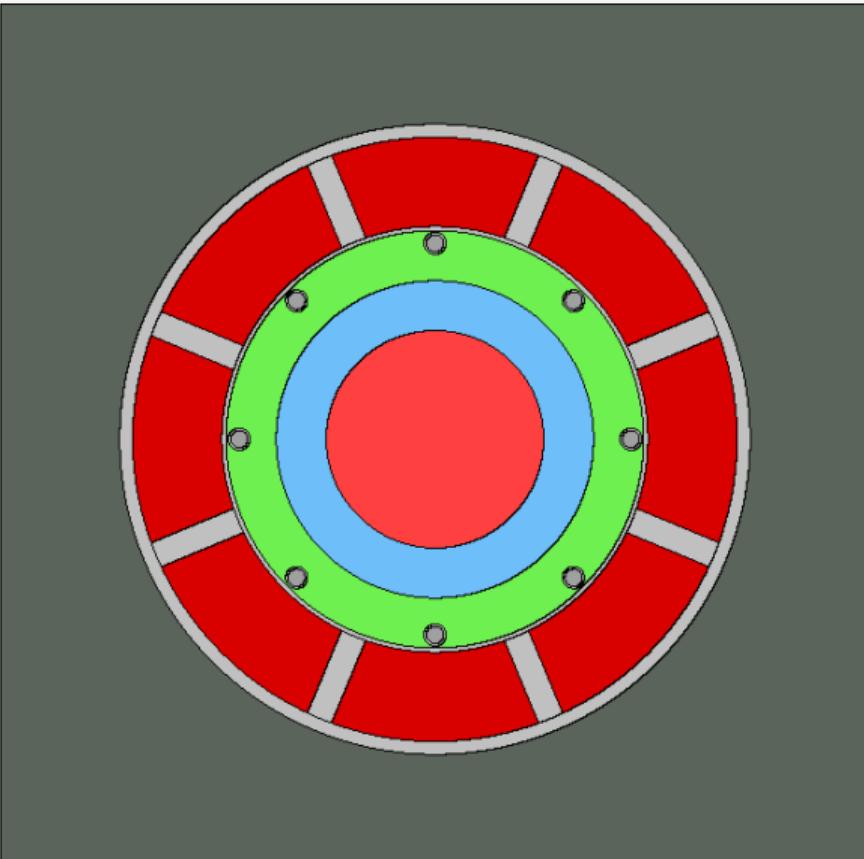
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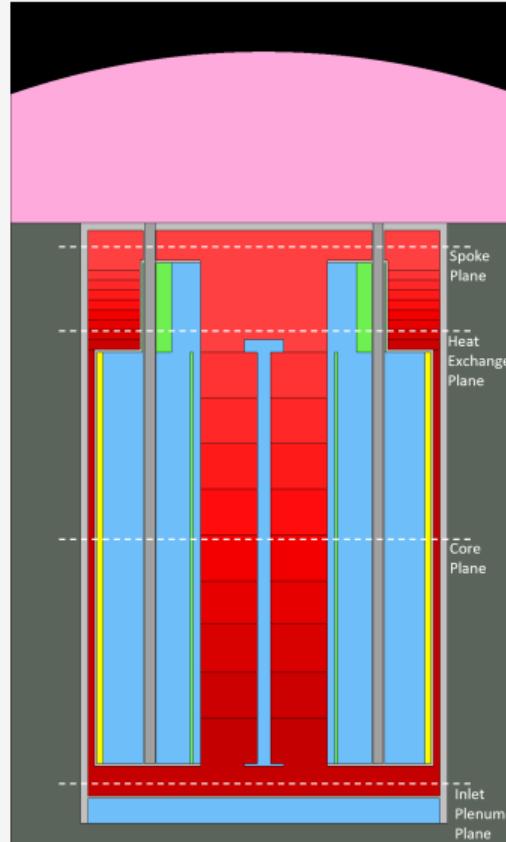
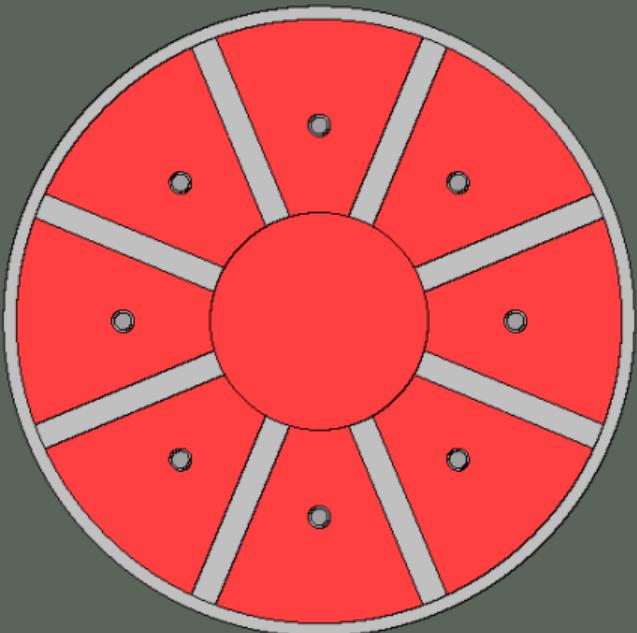
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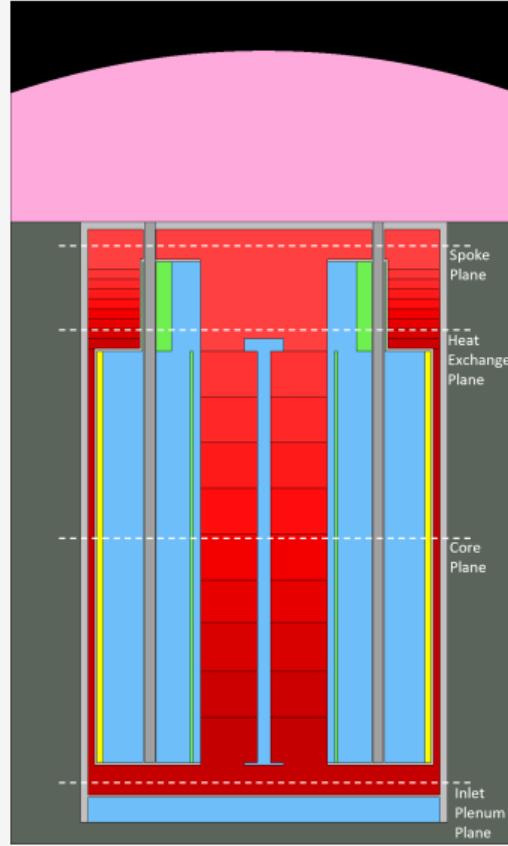
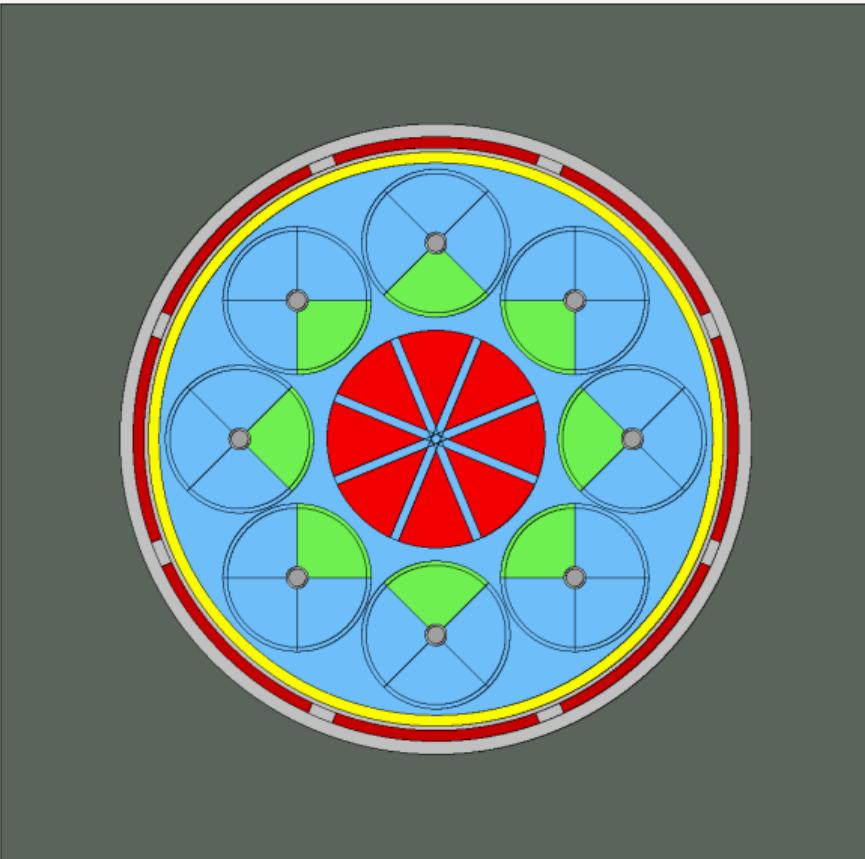
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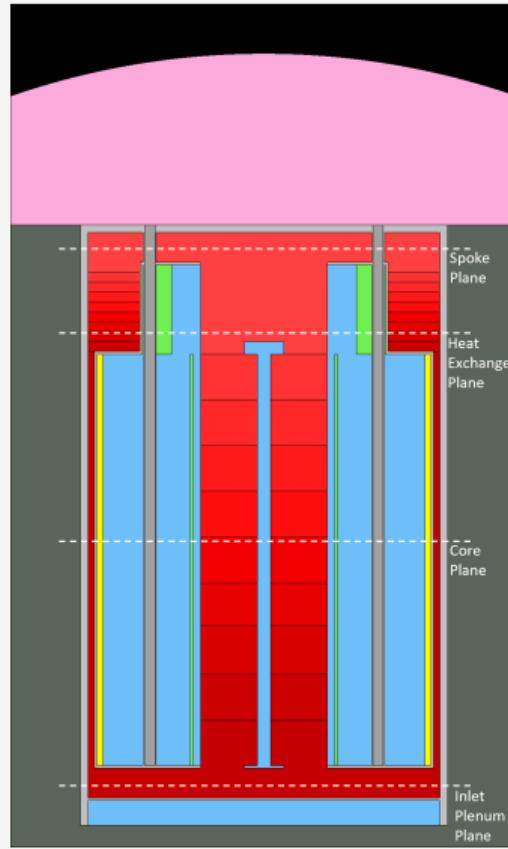
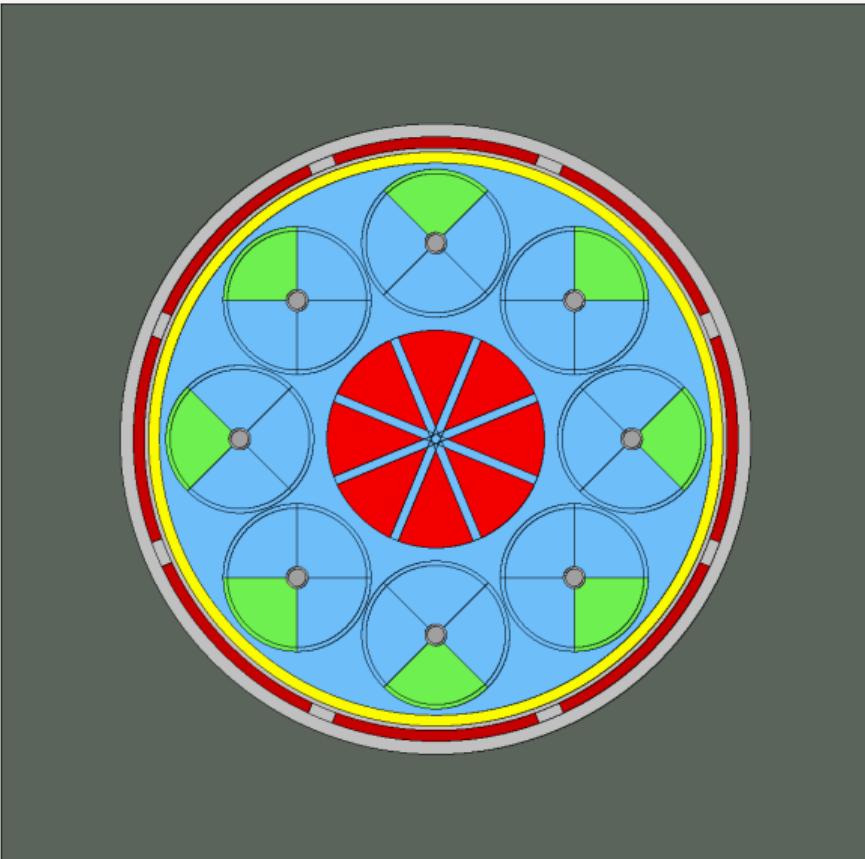
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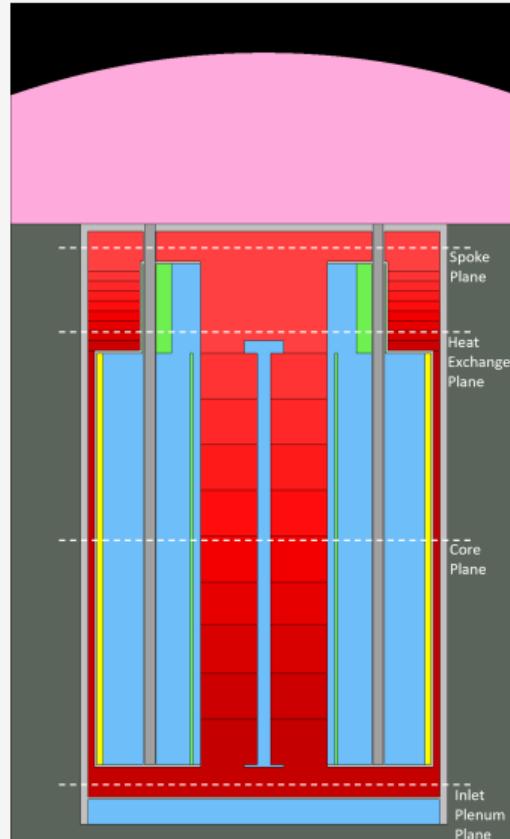
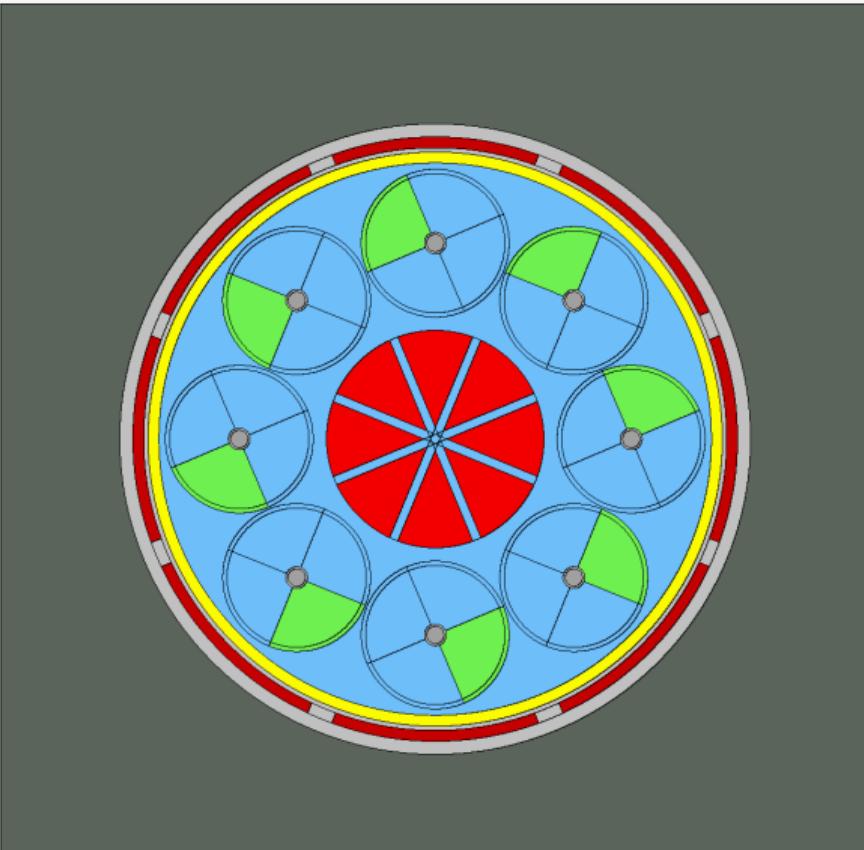
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## Criticality

- Set Pop 1,000,000 500 100 1
- Set Power 1e7 %10MWth

## Burn-Up

- Set mcvol 10,000,000
- Set nbuf
- Set printm 1 1e-10
- Set inventory "all"

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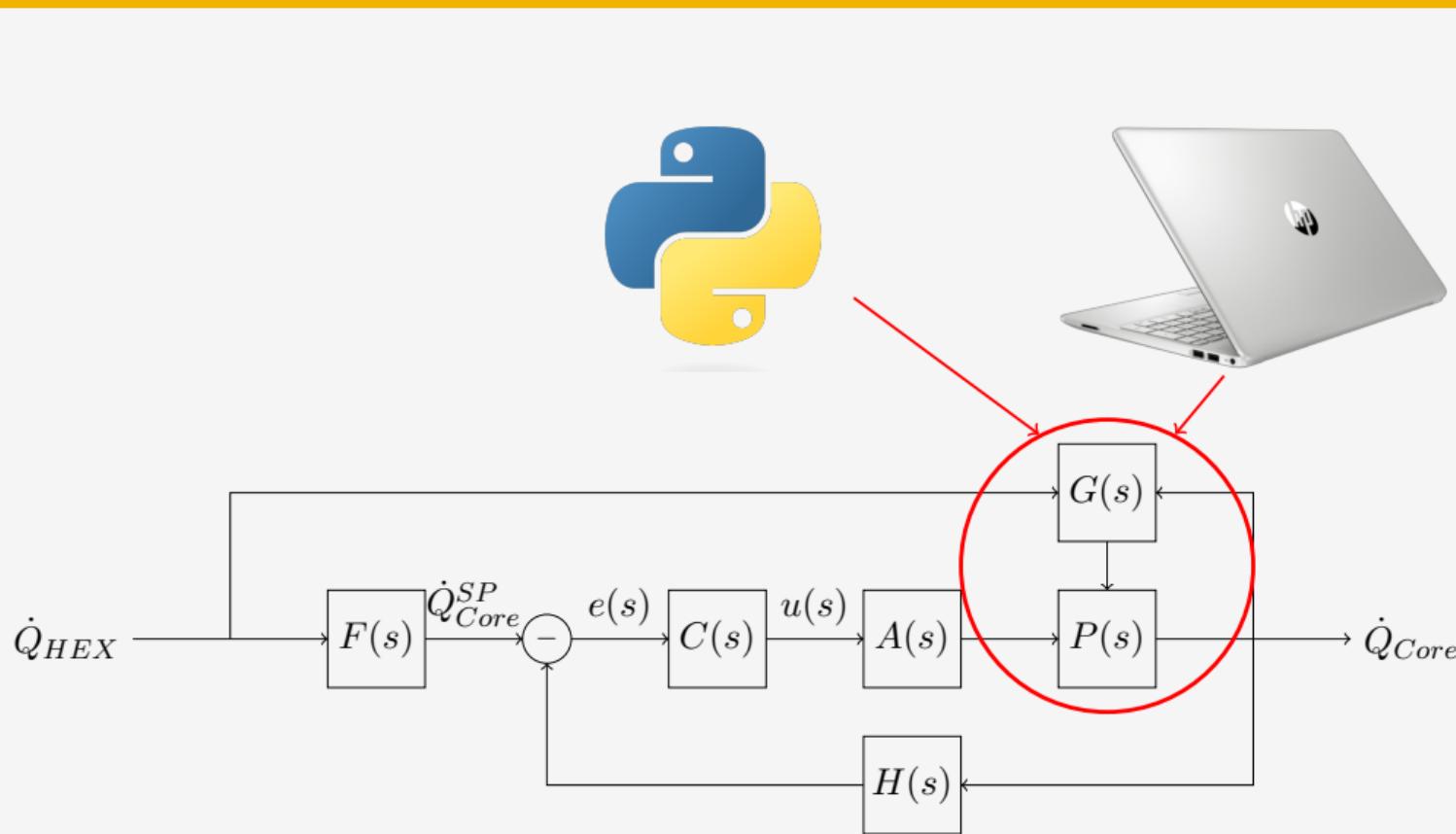
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## Natural Circulation (NC)

Updates flow rate by equating buoyant and frictional forces

$$v = \sqrt{2gh(\rho_{cold} - \rho_{hot})/\xi\rho}$$

## Reactor Point Kinetics (RPK)

## Uniform-State Uniform-Flow (USUF)

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## Natural Circulation (NC)

## Reactor Point Kinetics (RPK)

Updates core power by summing passive reactivity feedback

$$\rho_f = -\frac{L}{L+H} \beta_{eff} (1 - e^{-v\alpha_f})$$

$$\Delta\rho_T = \alpha_T \Delta T$$

$$\tau = \frac{l^*}{\rho} + \frac{\beta_{eff} - \rho}{\lambda\rho + \dot{\rho}}$$

$$Q_{core}[t + \delta t] = Q_{core}[t] e^{\delta t/\tau}$$

## Uniform-State Uniform-Flow (USUF)

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## Natural Circulation (NC)

## Reactor Point Kinetics (RPK)

## Uniform-State Uniform-Flow (USUF)

Updates temperature profile based on flow rate and core/heat-exchanger powers

$$\delta x A_x \frac{d\varrho}{dt} = v A_x (\varrho_{in} - \varrho_{out})$$

$$mu_x = \varrho(T_x) \delta x A_x c_p (T_x + T_r/2) (T_x - T_r)$$

$$\frac{d(mu)}{dt} = mu_{enter} - mu_{exit} + Q_{c.v.}$$

$$mu[t + \delta t] = mu[t] + \delta t \frac{d(mu)}{dt}[t]$$

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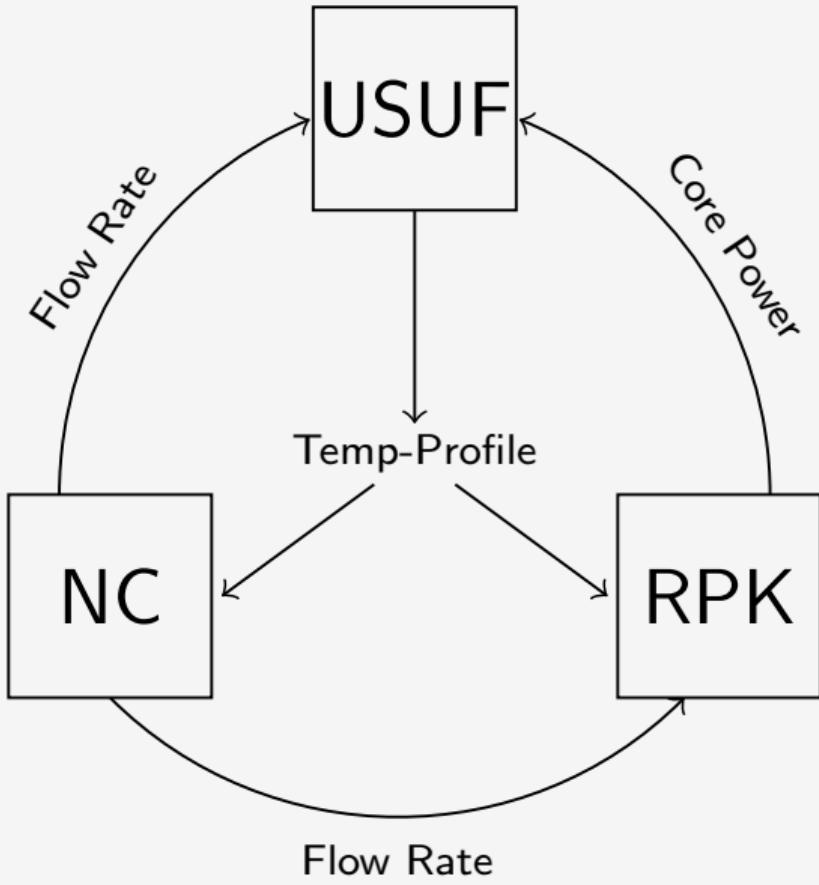
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# Control-Reactivity Curve

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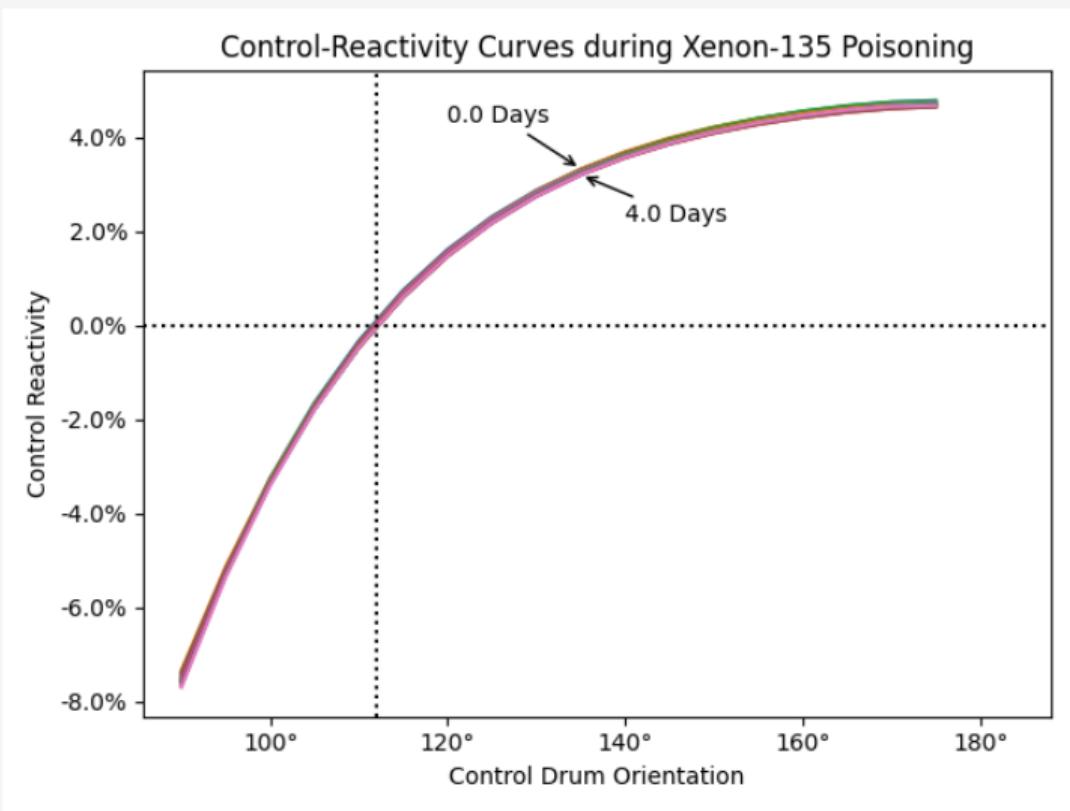
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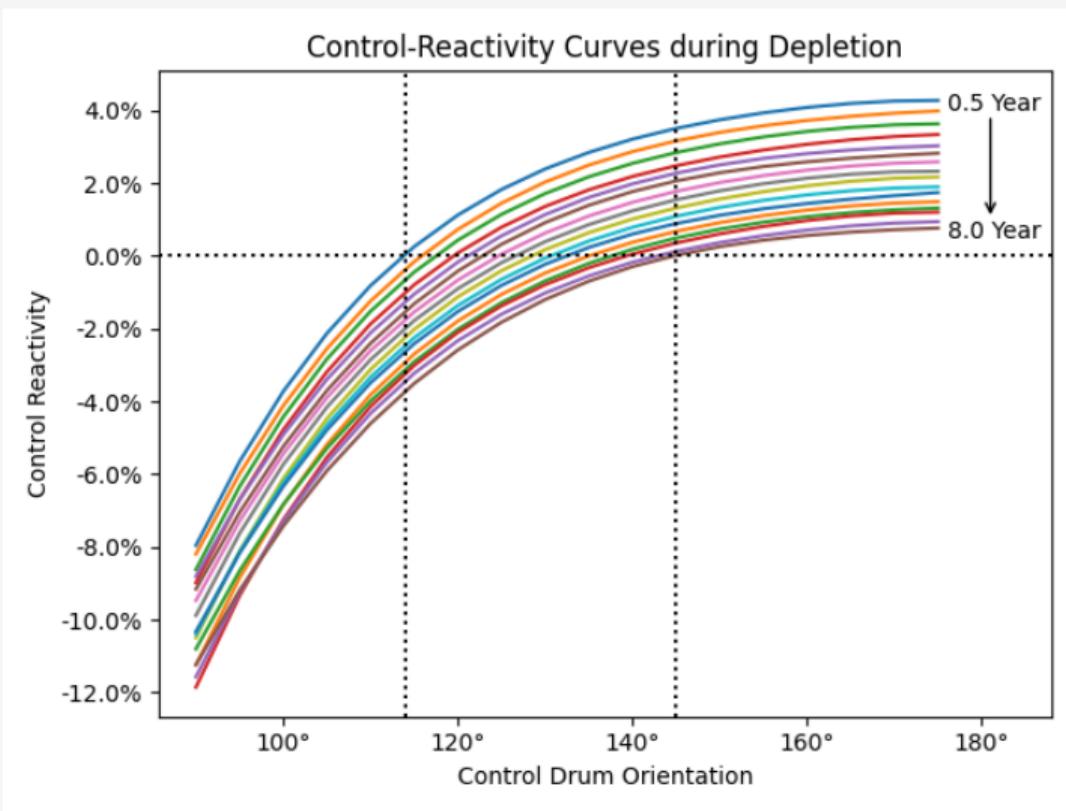
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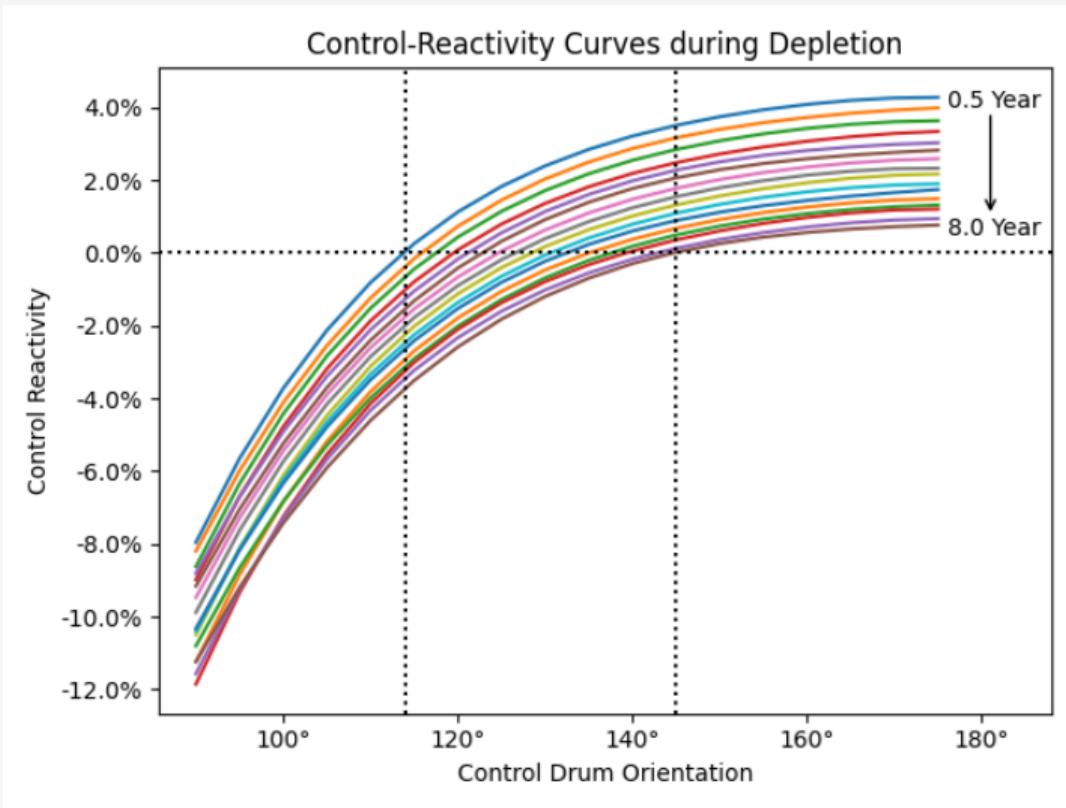
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# Control-Reactivity Curve



$$\rho = c_0 + c_1\theta + c_2\theta^2 + c_3\theta^3 + c_4\theta^4$$

# Curve Fits

Years	$c_4 \times 10^9$	$c_3 \times 10^6$	$c_2 \times 10^4$	$c_1 \times 10^2$	$c_0$	root (°)	slope (pcm/°)
0.0	-2.797	1.789	-4.361	4.829	-2.009	111.41	224.24
0.5	-2.755	1.755	-4.272	4.732	-1.976	113.69	203.69
1.0	-1.838	1.253	-3.253	3.826	-1.682	115.79	189.71
1.5	-2.533	1.632	-3.253	4.507	-1.909	117.38	175.96
2.0	-2.418	1.578	-3.930	4.440	-1.895	119.45	161.06
2.5	-1.461	1.026	-2.750	3.337	-1.515	121.06	152.71
3.0	-1.137	0.856	-2.425	3.070	-1.440	122.67	146.08
3.5	-2.054	1.357	-3.433	3.953	-1.727	124.58	130.85
4.0	-2.527	1.617	-3.967	4.438	-1.892	126.46	120.67
4.5	-2.869	1.831	-4.460	4.935	-2.081	128.35	111.30
5.0	-2.338	1.520	-3.785	4.291	-1.855	130.55	102.04
5.5	-1.471	1.054	-2.852	3.467	-1.585	132.29	93.34
6.0	-2.626	1.702	-4.211	4.729	-2.027	134.96	83.90
6.5	-1.672	1.141	-2.985	3.550	-1.607	137.45	77.56
7.0	-3.321	2.095	-5.036	5.492	-2.292	139.19	69.73
7.5	-2.419	1.579	-3.936	4.459	-1.932	142.69	59.45
8.0	-7.991	0.648	-1.960	2.623	-1.305	144.62	55.65

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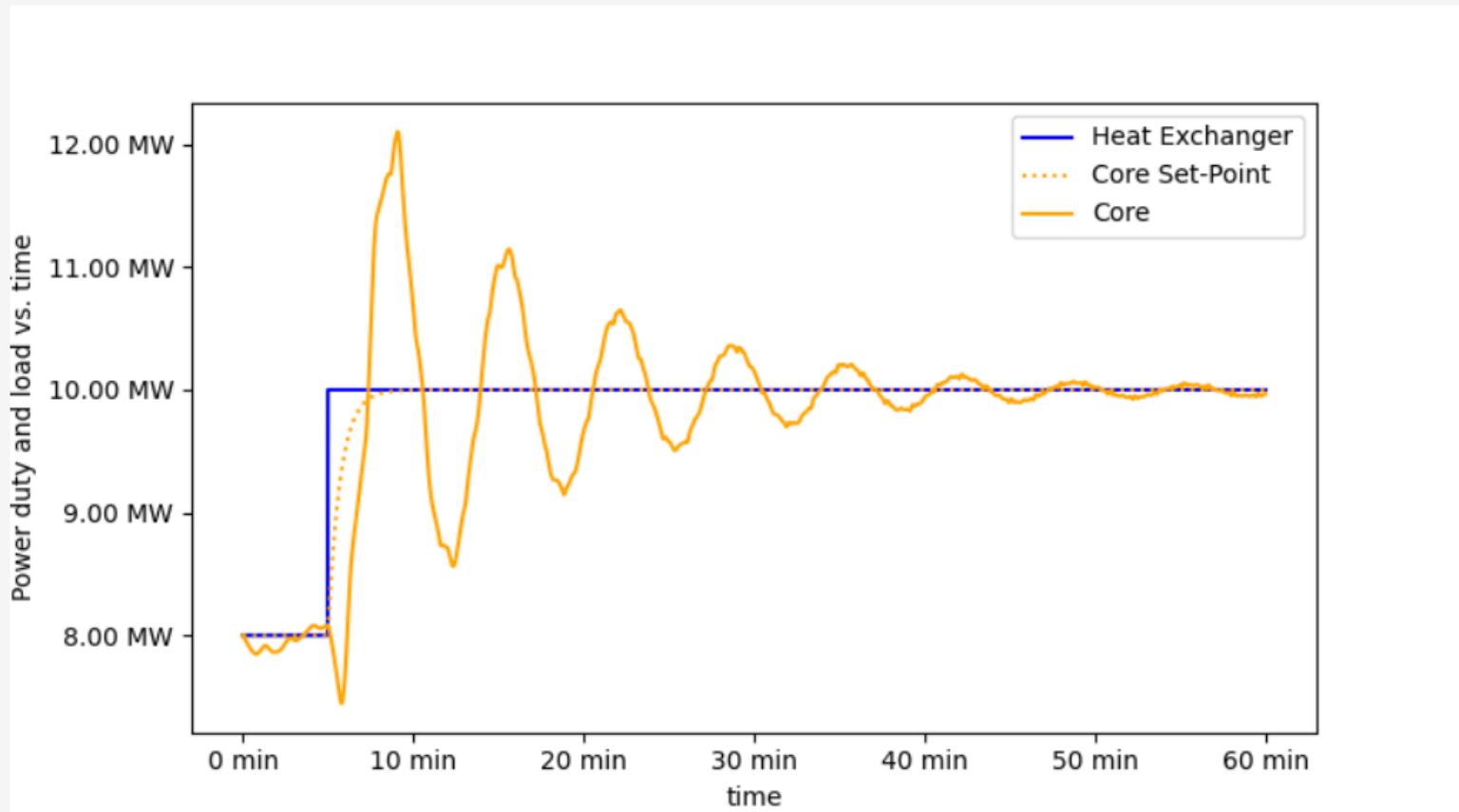
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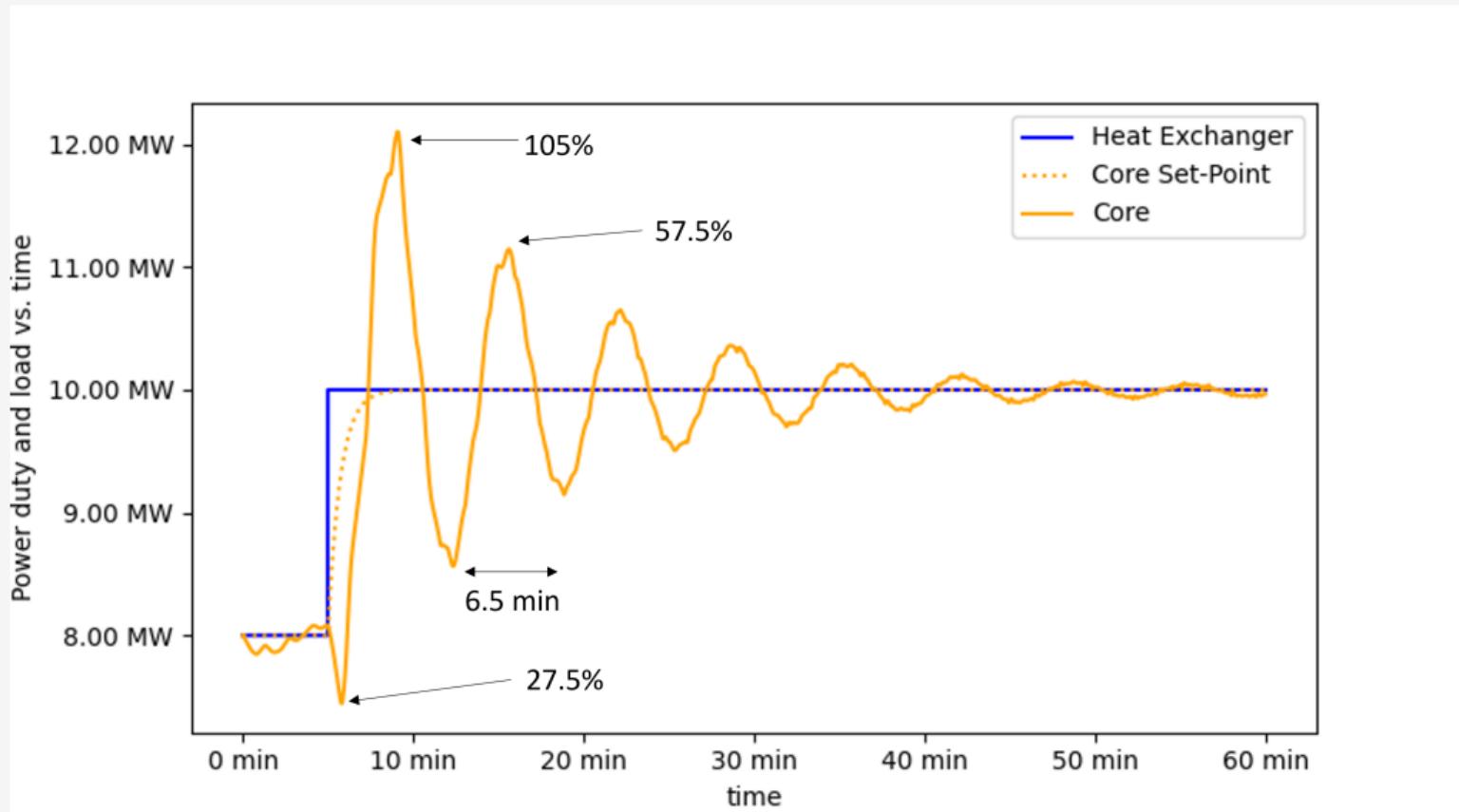
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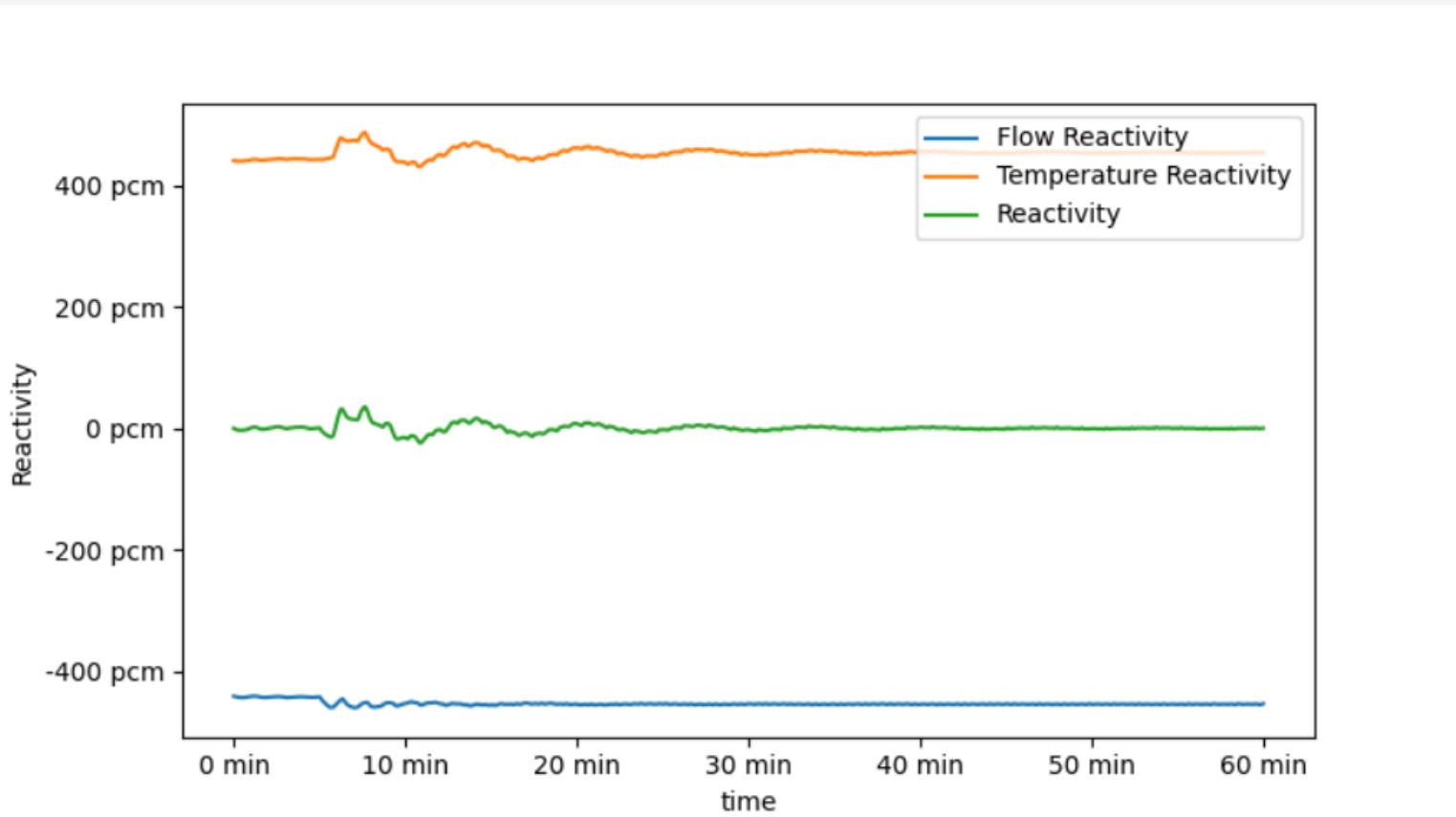
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## Ziegler Nichols Tuning Methodology

- P-Only Control
- Increase gain until sustained oscillations

## Controller Parameters

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## Ziegler Nichols Tuning Methodology

- P-Only Control
- Increase gain until sustained oscillations
- Ultimate gain -  $3 \times 10^{-4}$  degree/kW
- Ultimate period - 45 seconds

## Controller Parameters

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## Ziegler Nichols Tuning Methodology

### Controller Parameters

- Controller gain -  $1.35 \times 10^{-4}$  degree/kW at 0 years
- Controller-Actuator gain - 30.3 pcm/MW
- Integral time-constant - 37.5 seconds
- Derivative time-constant - 0 sec
- Controller bias -  $111.41^\circ$  at zero years,  $144.62^\circ$  at eight years

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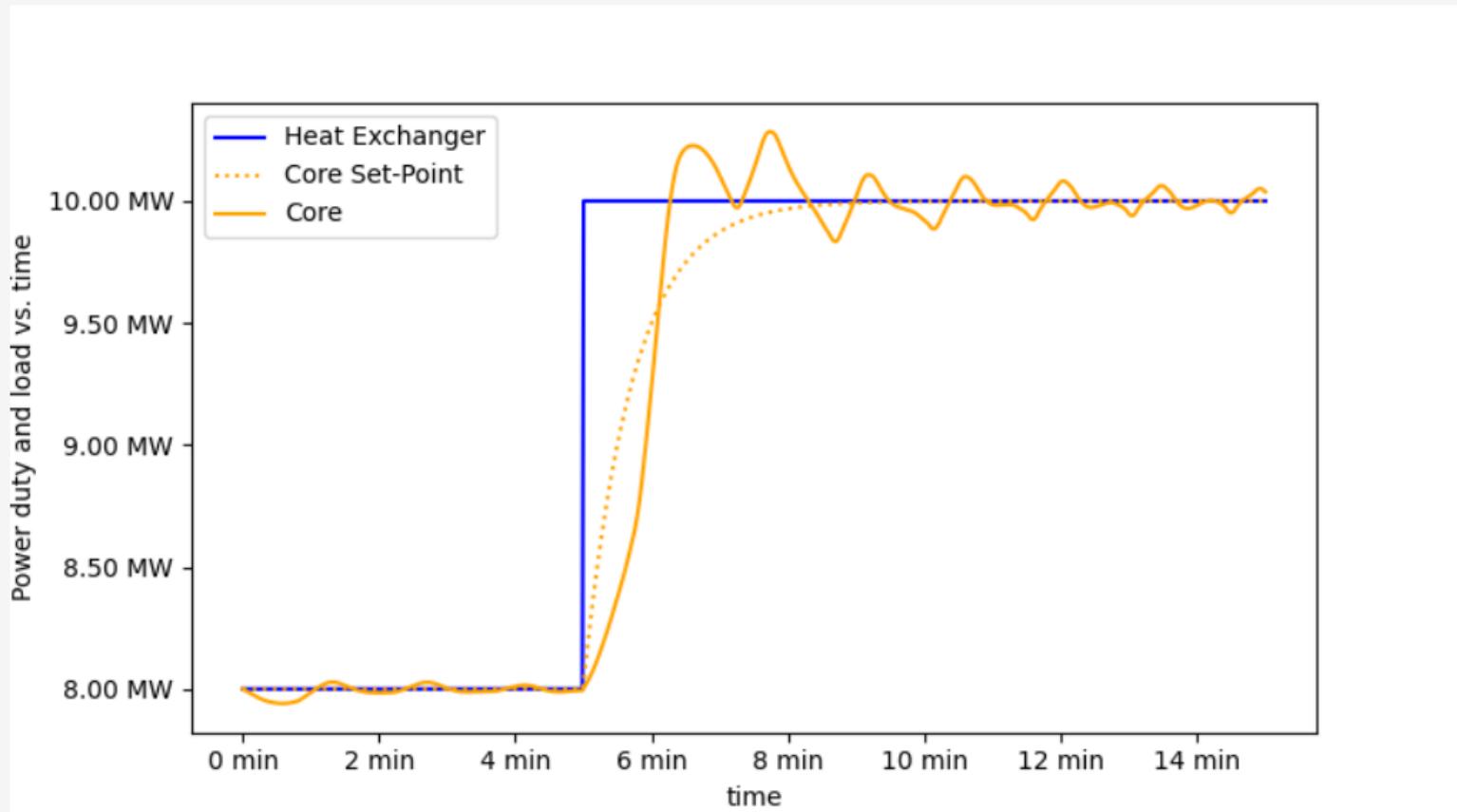
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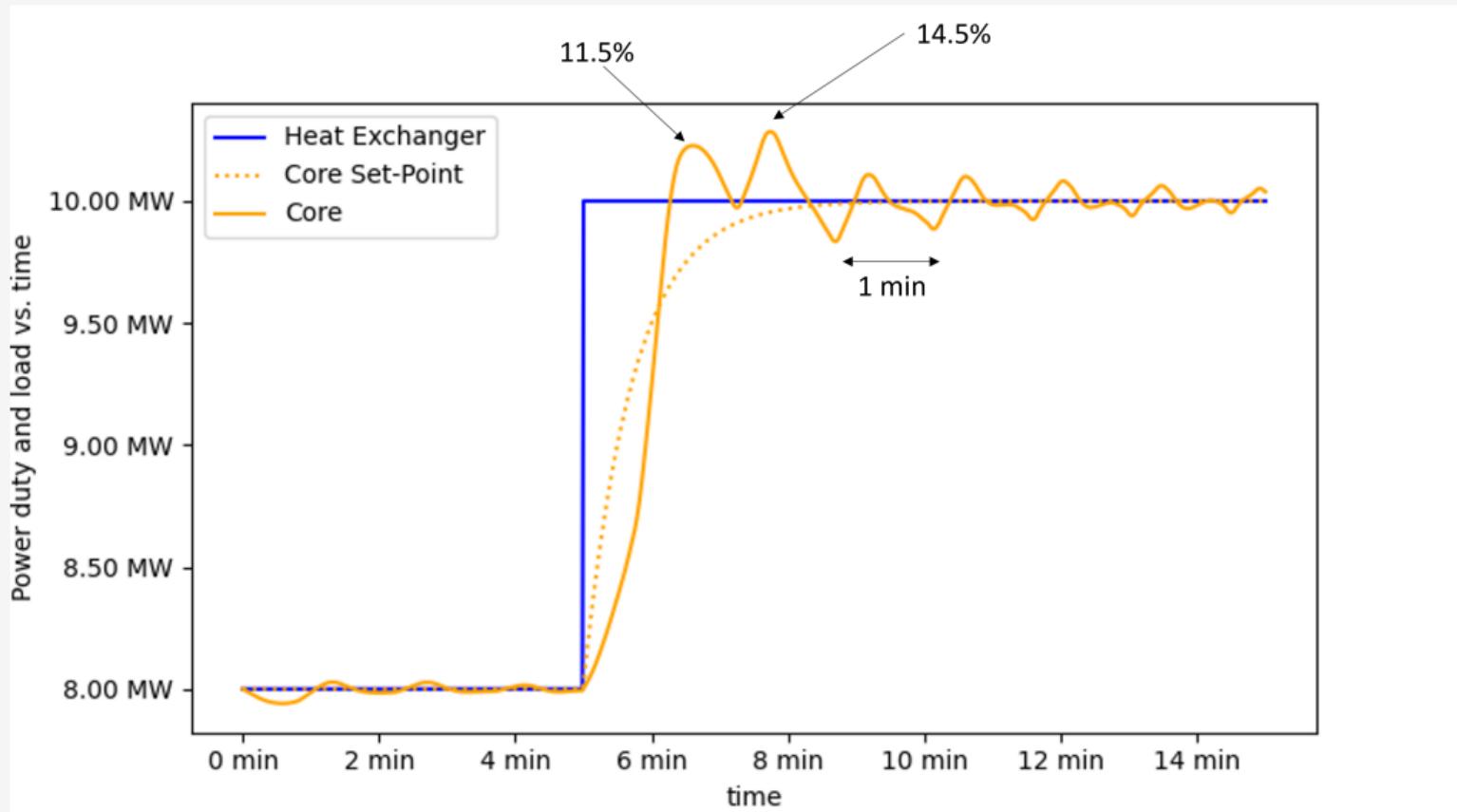
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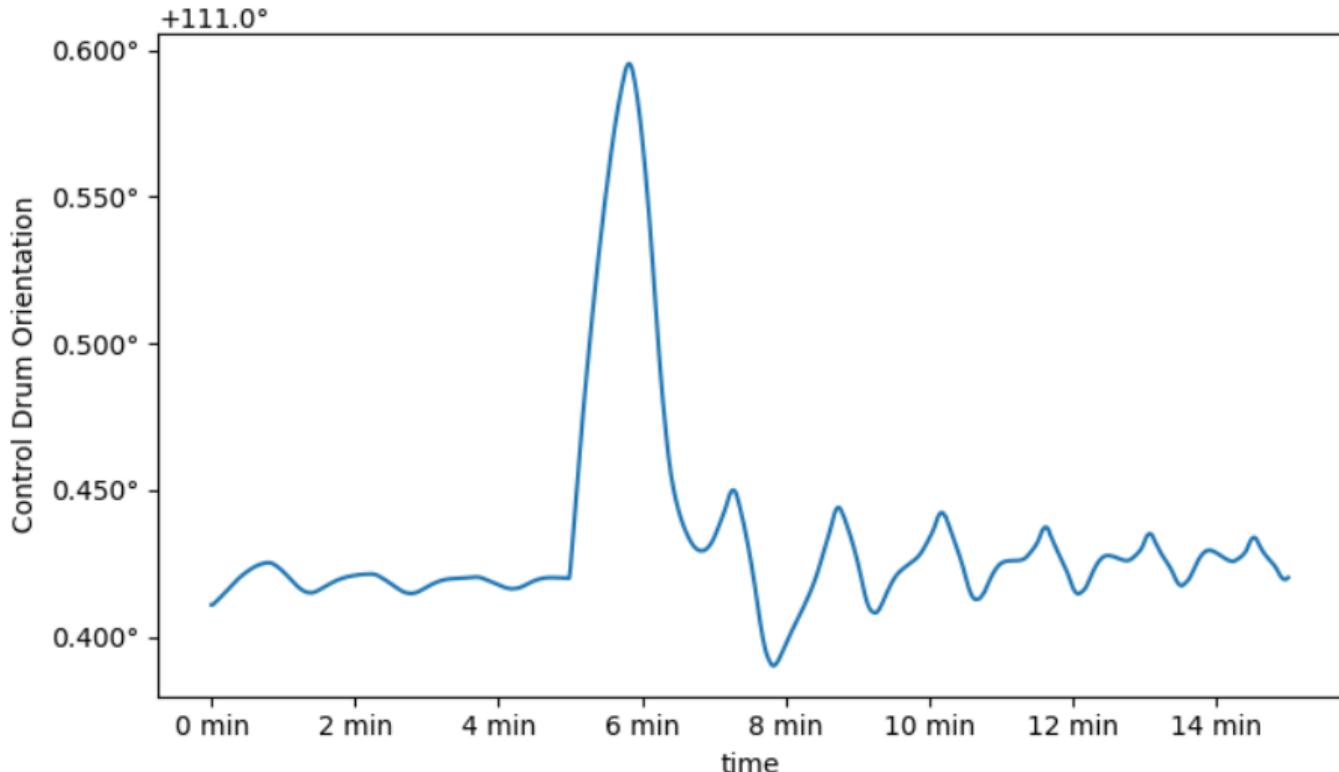
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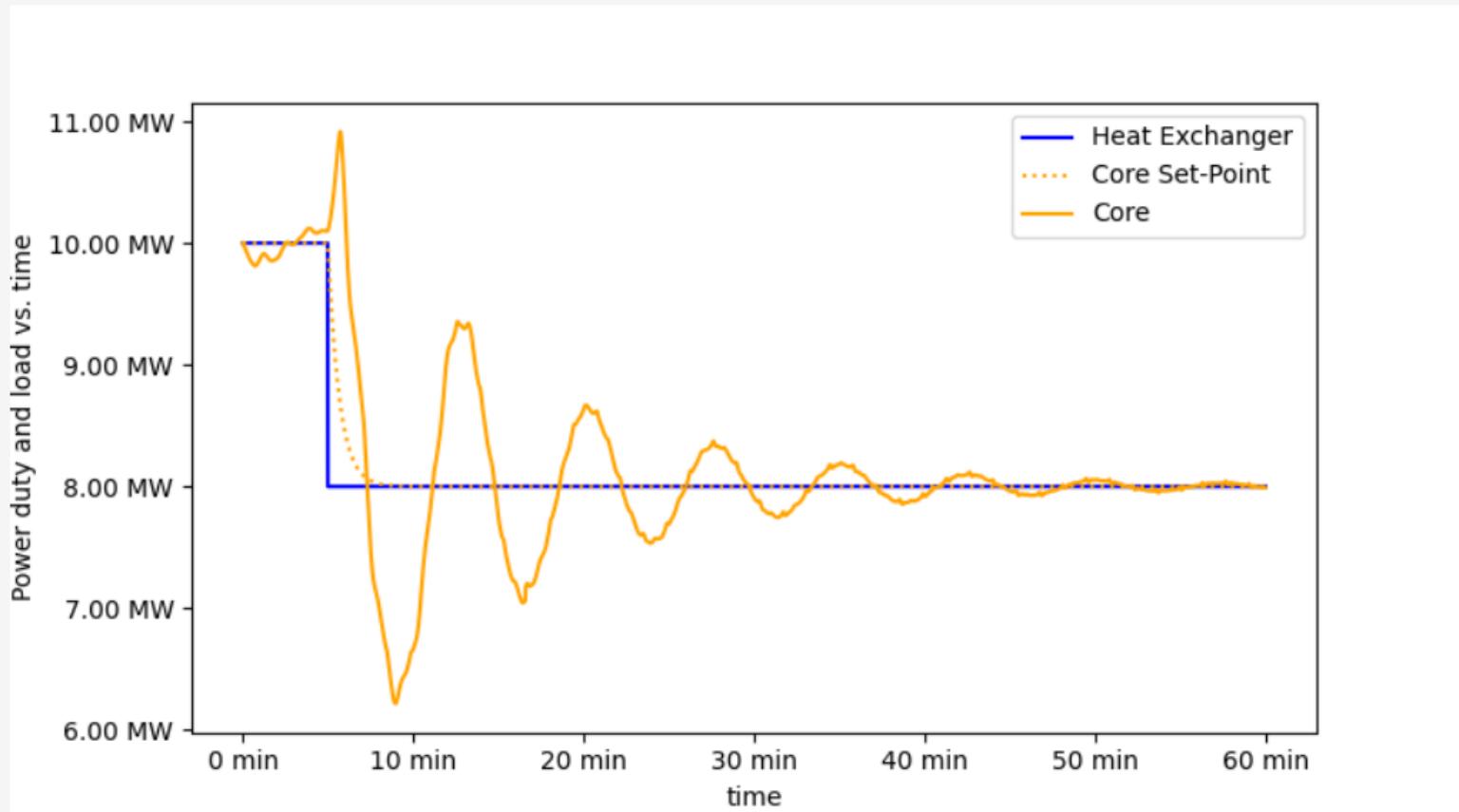
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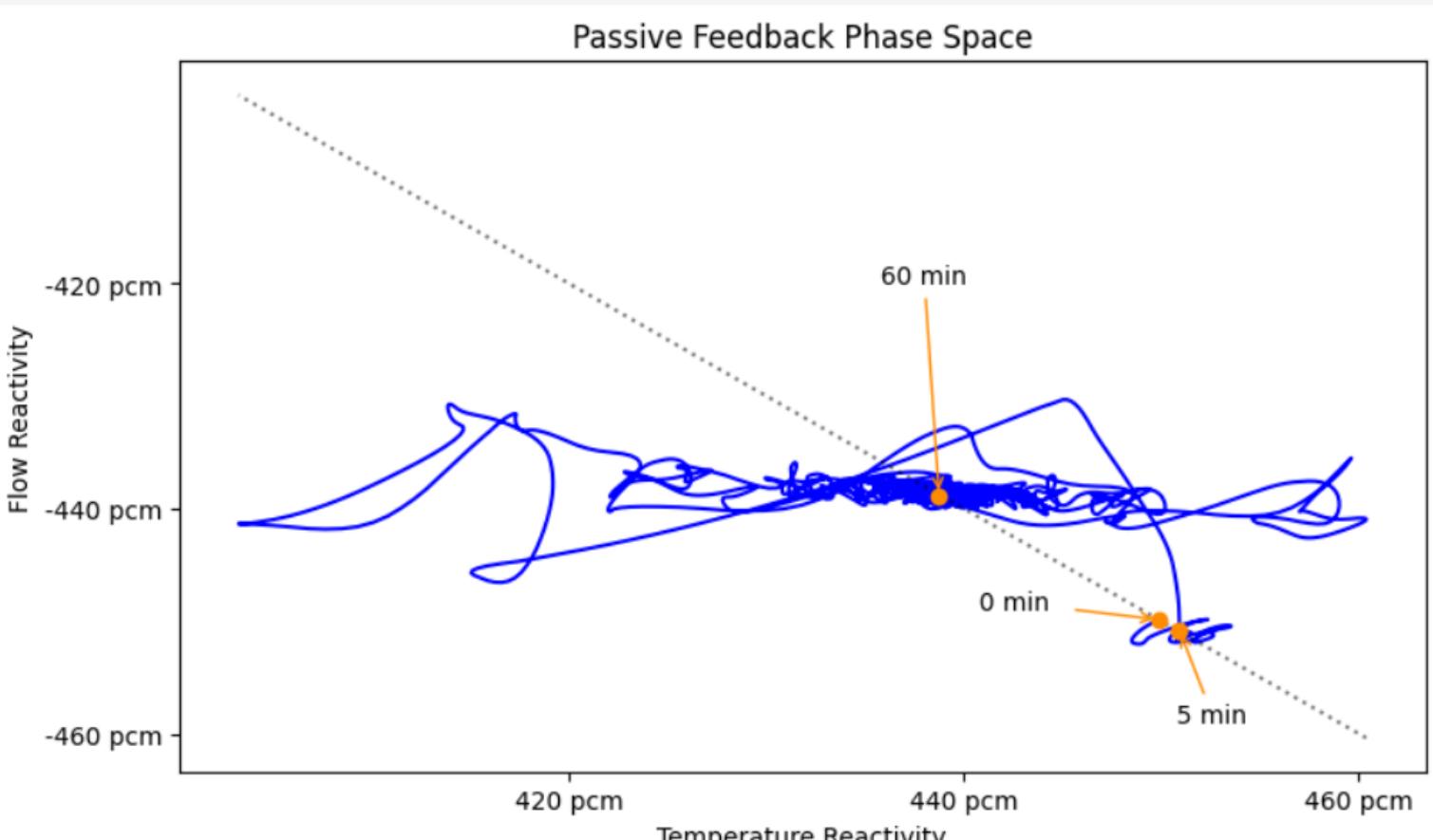
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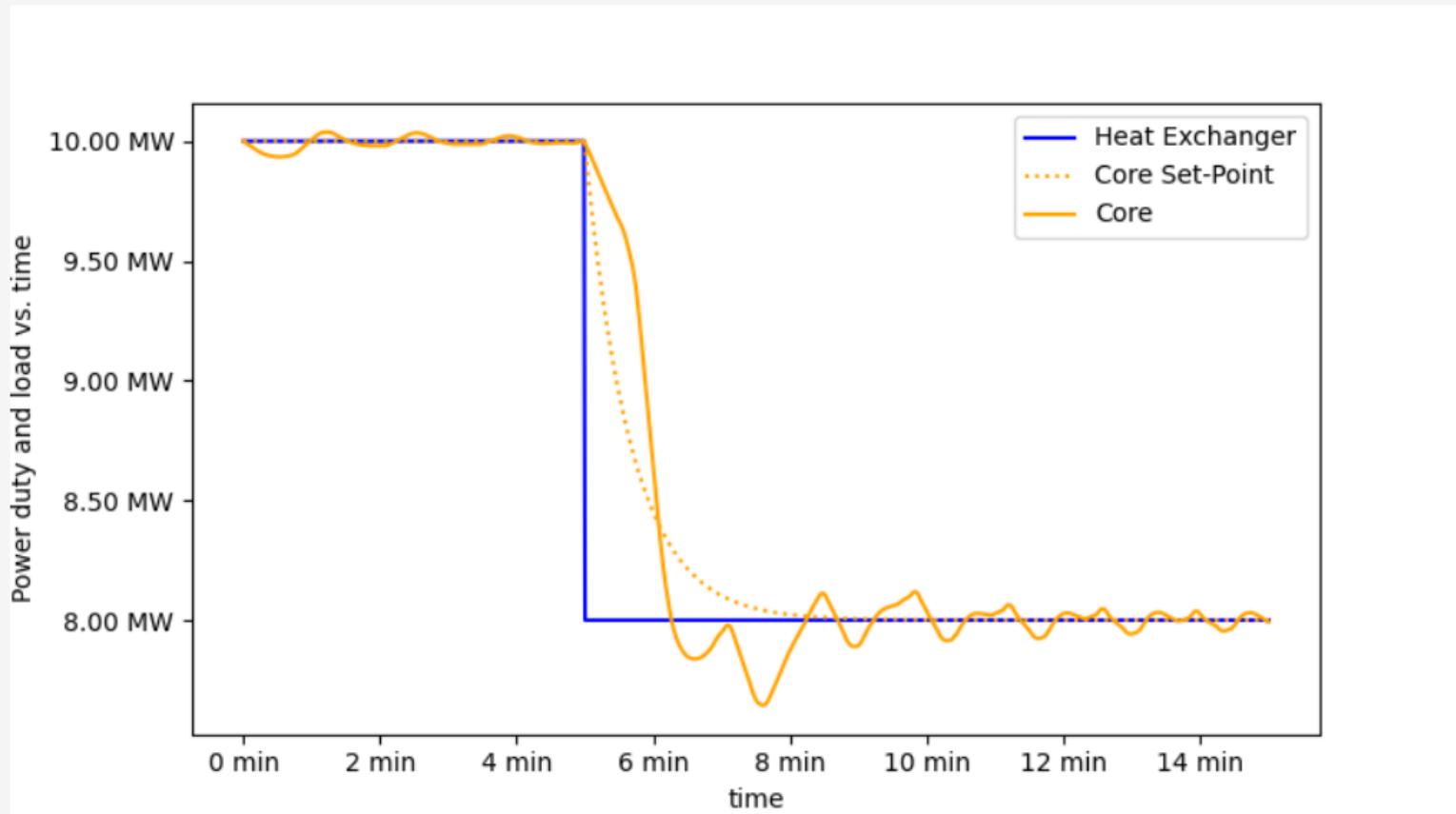
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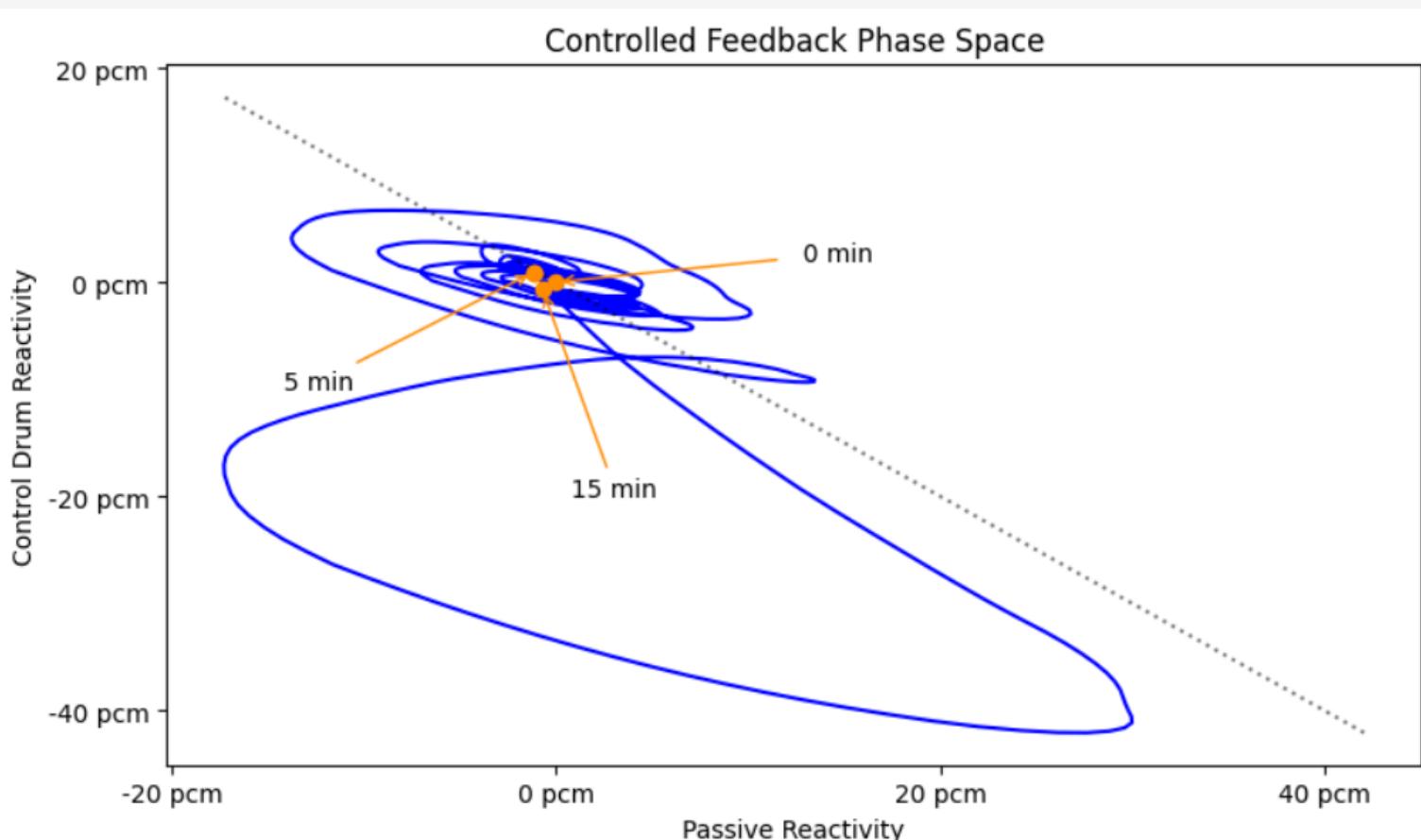
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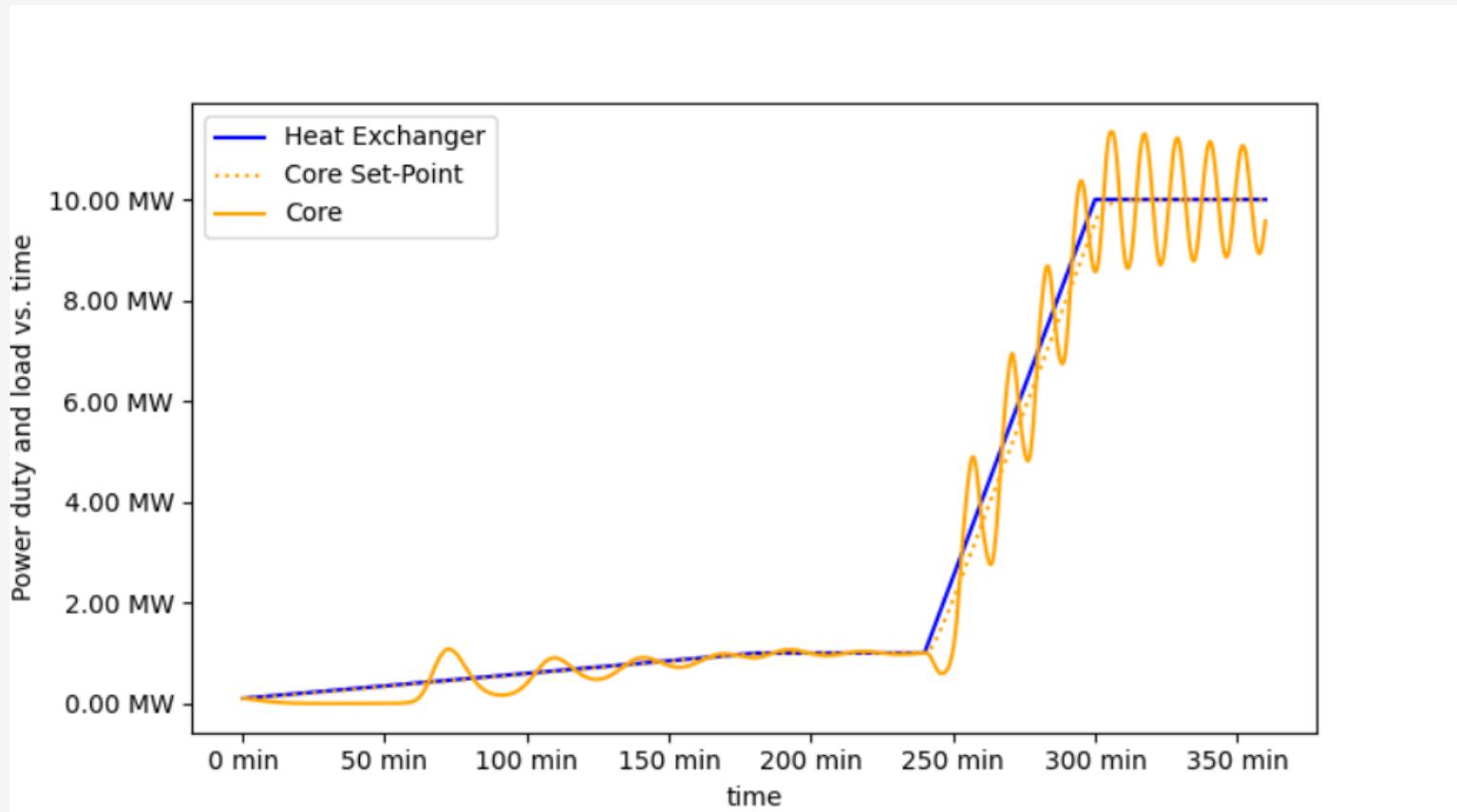
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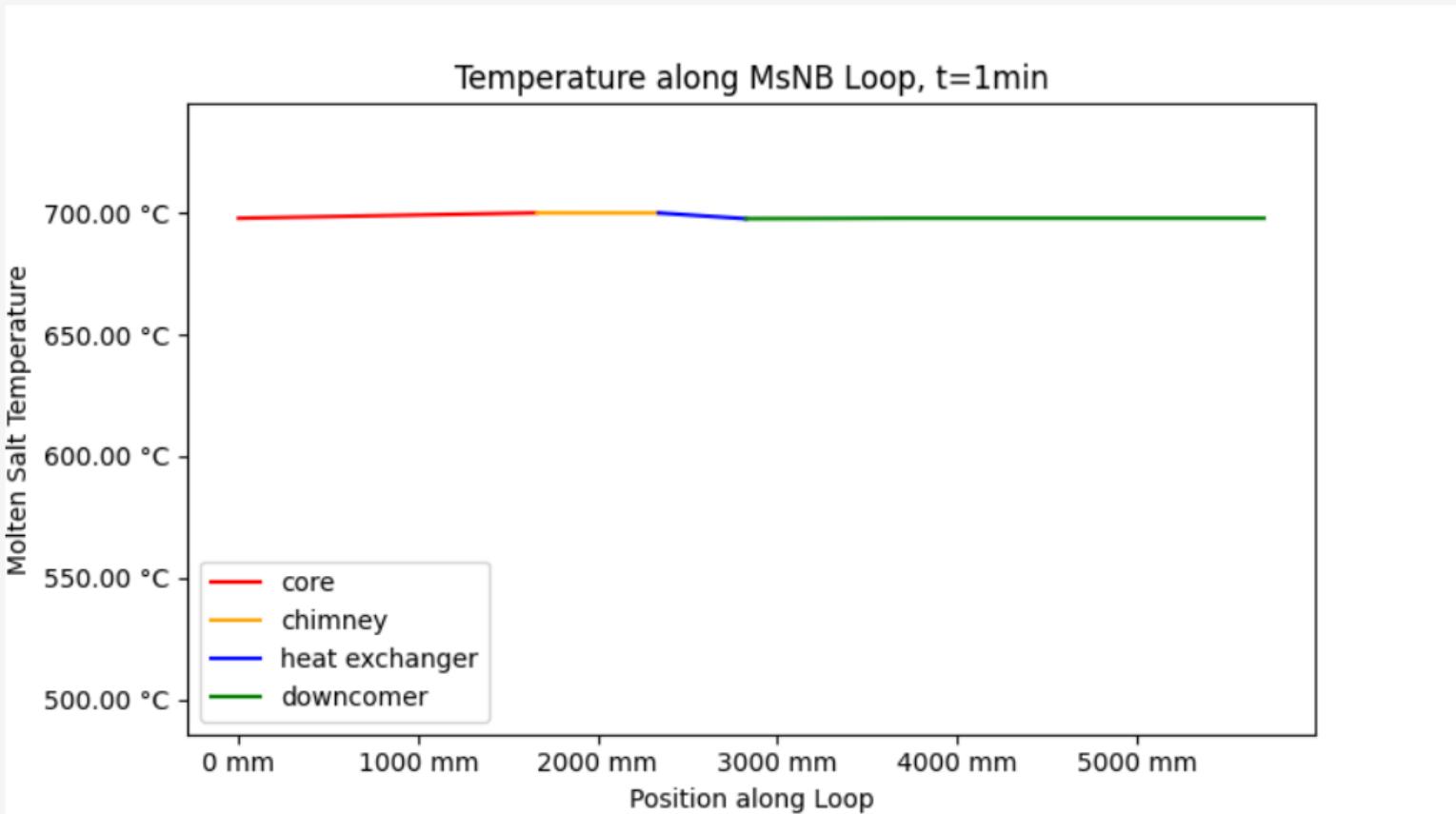
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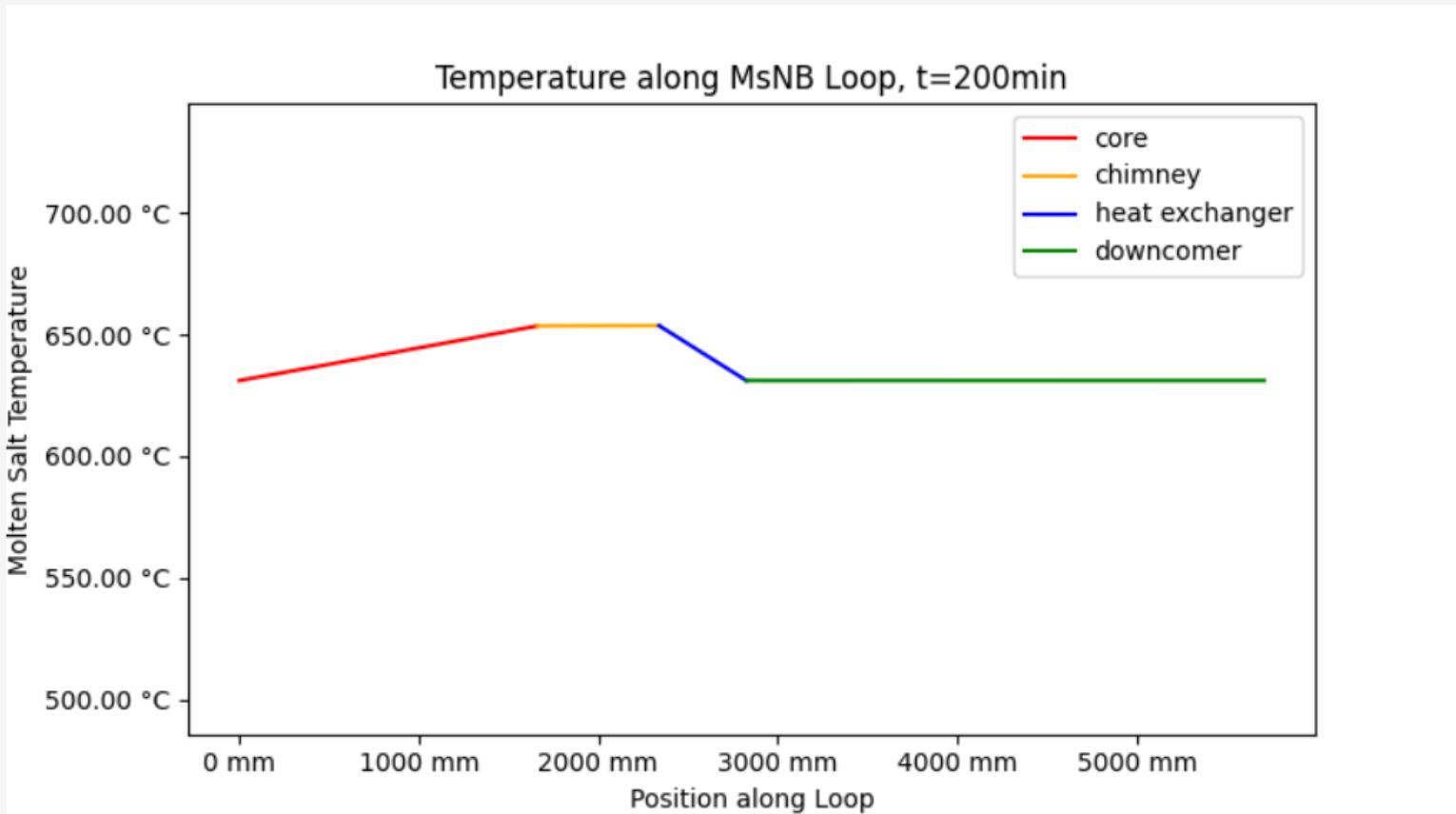
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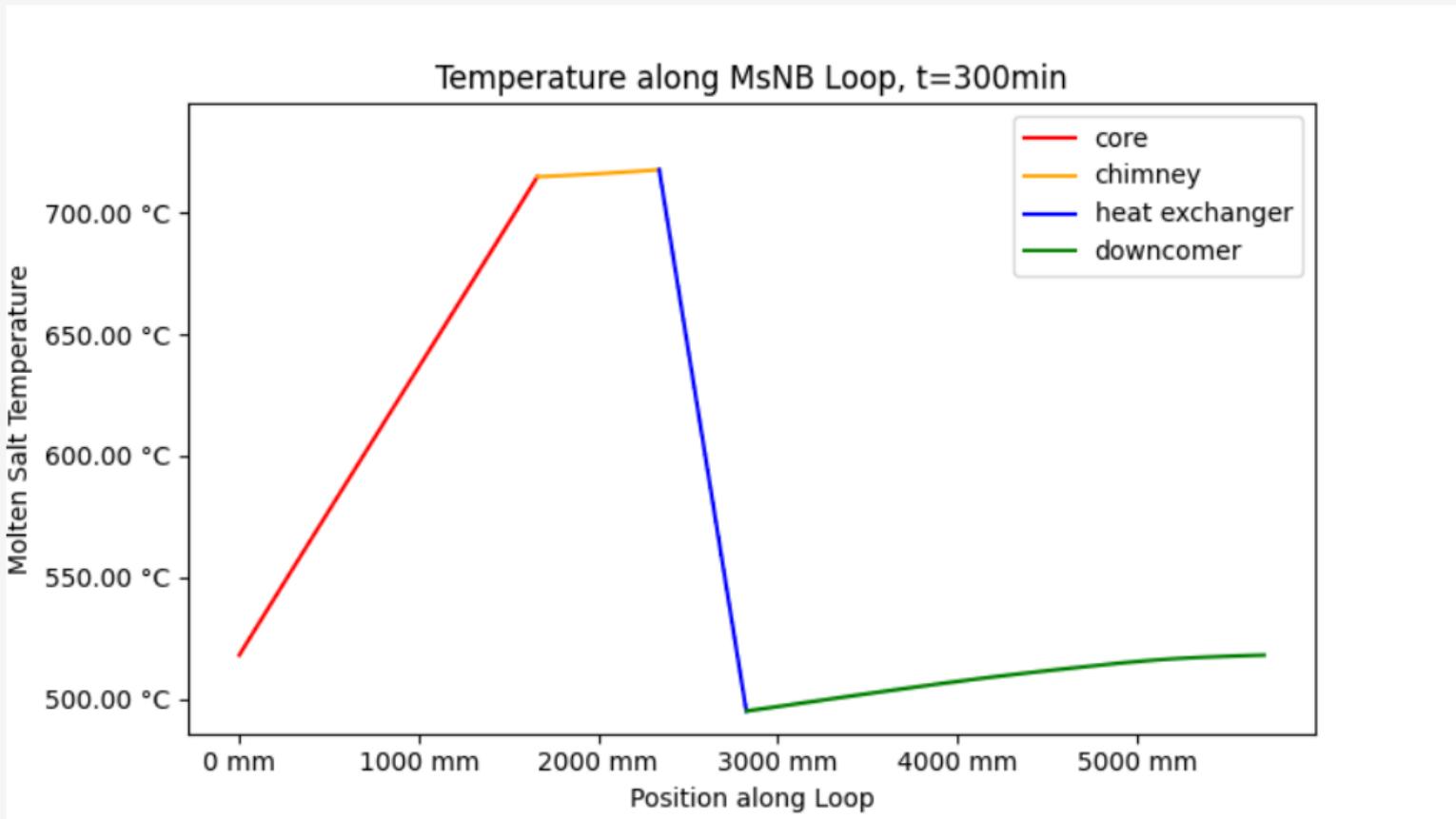
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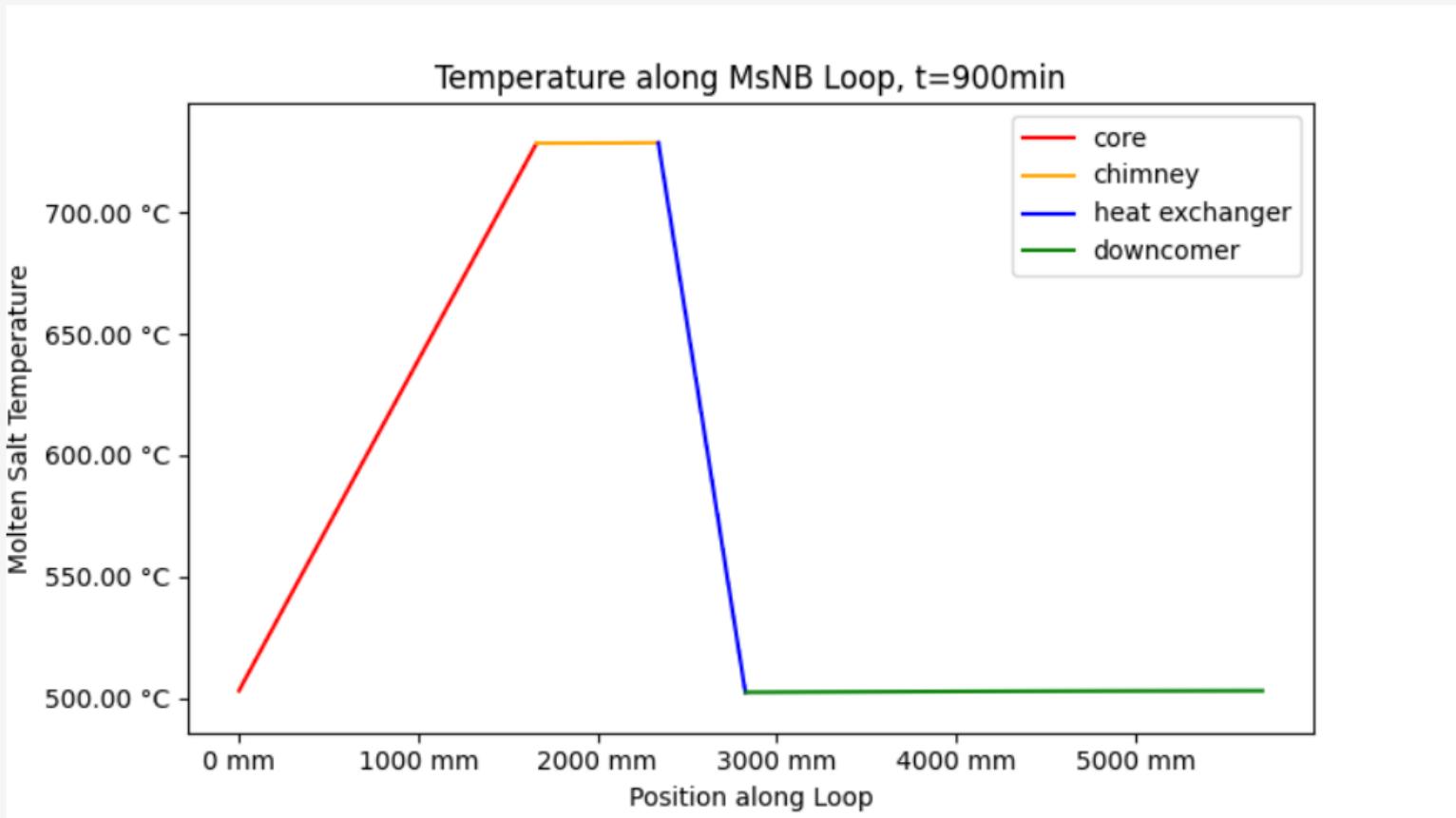
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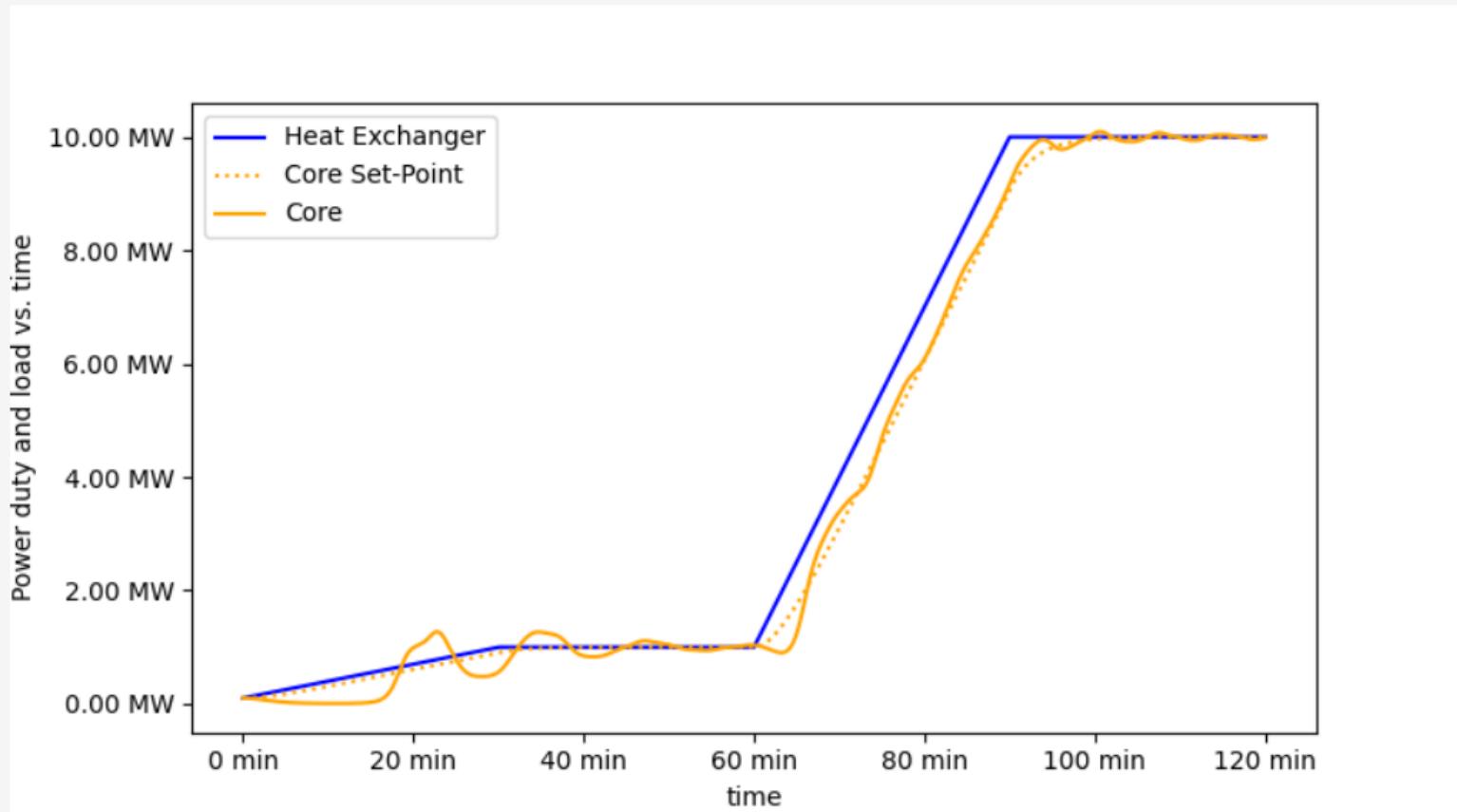
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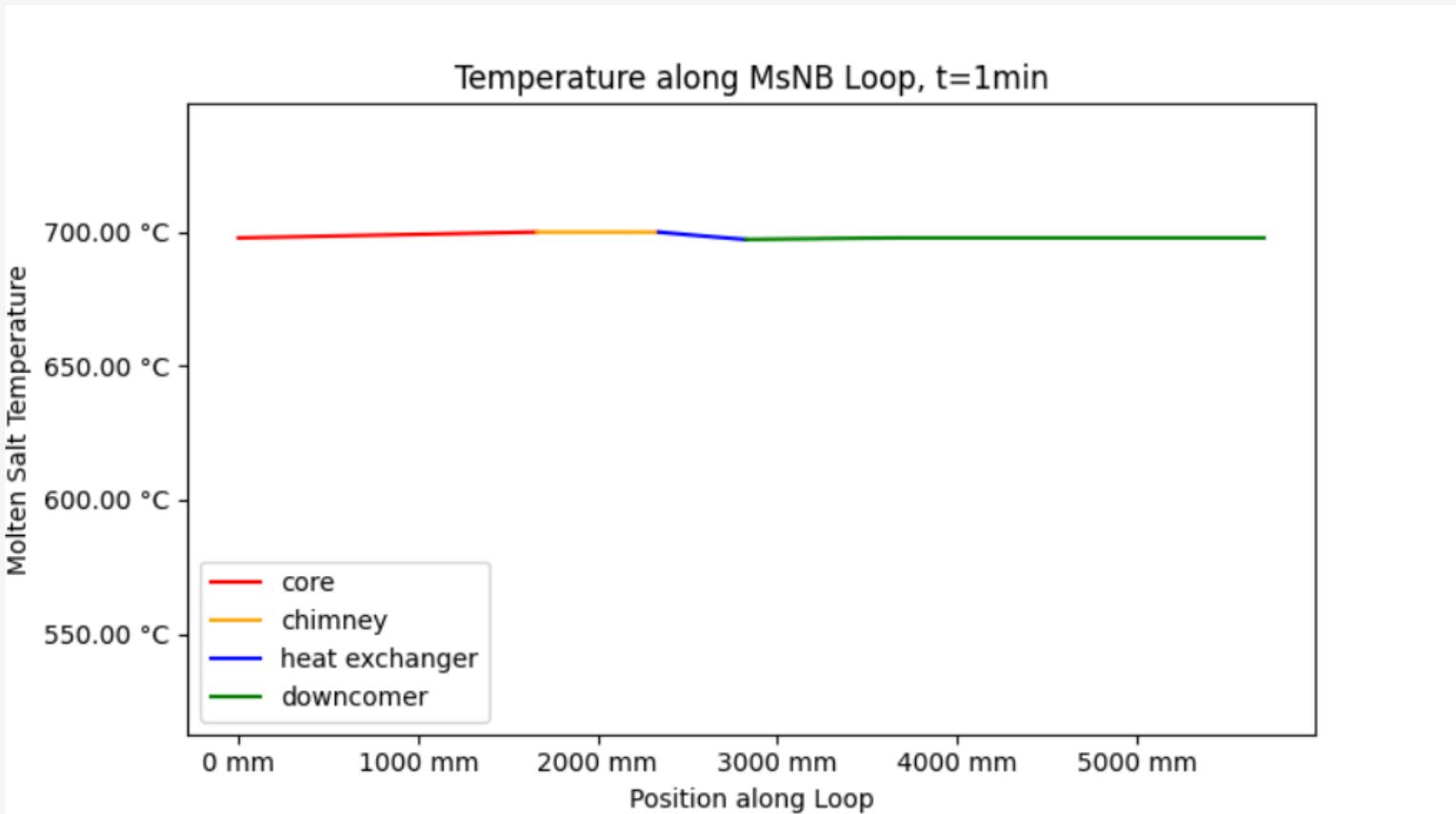
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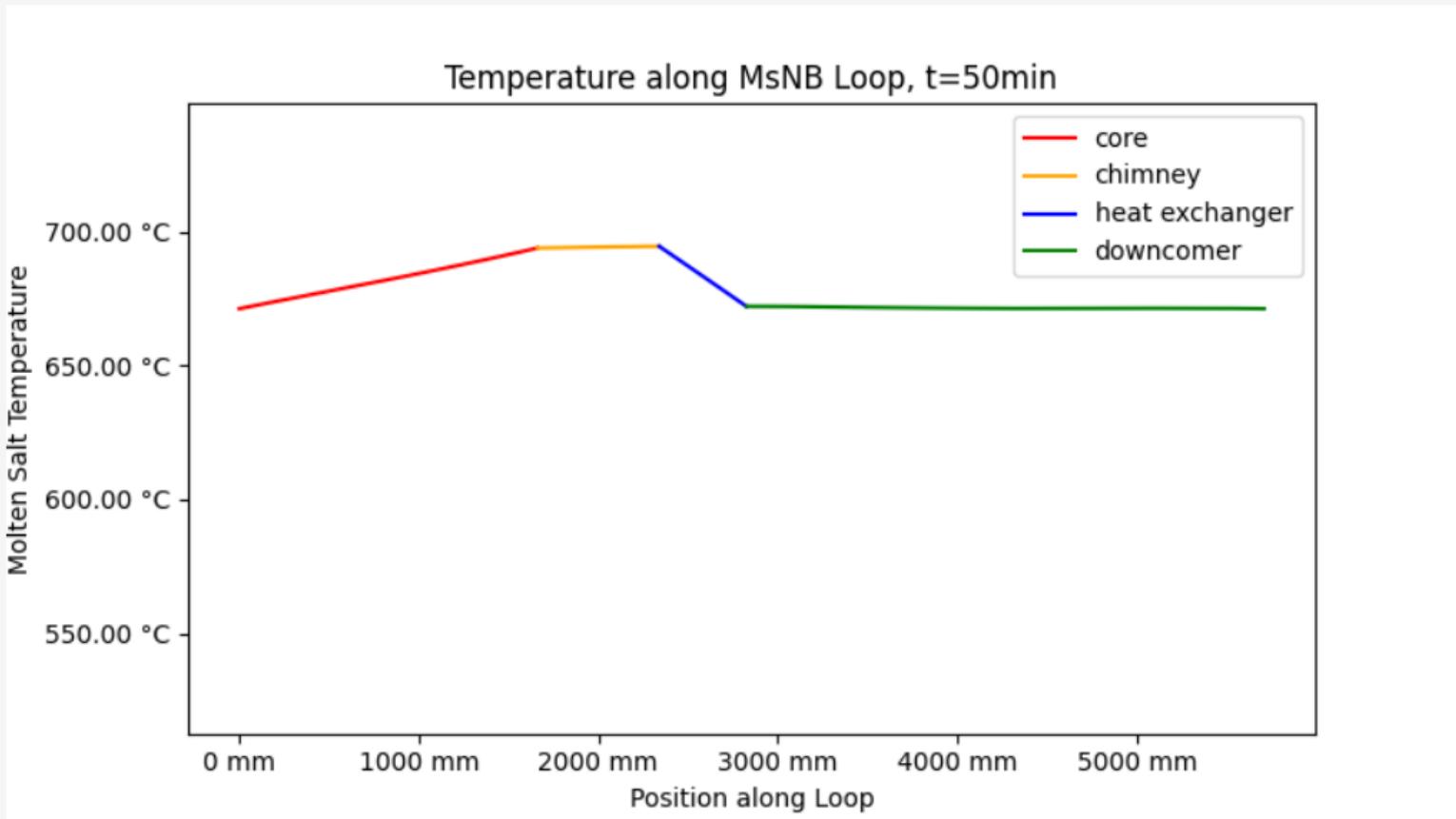
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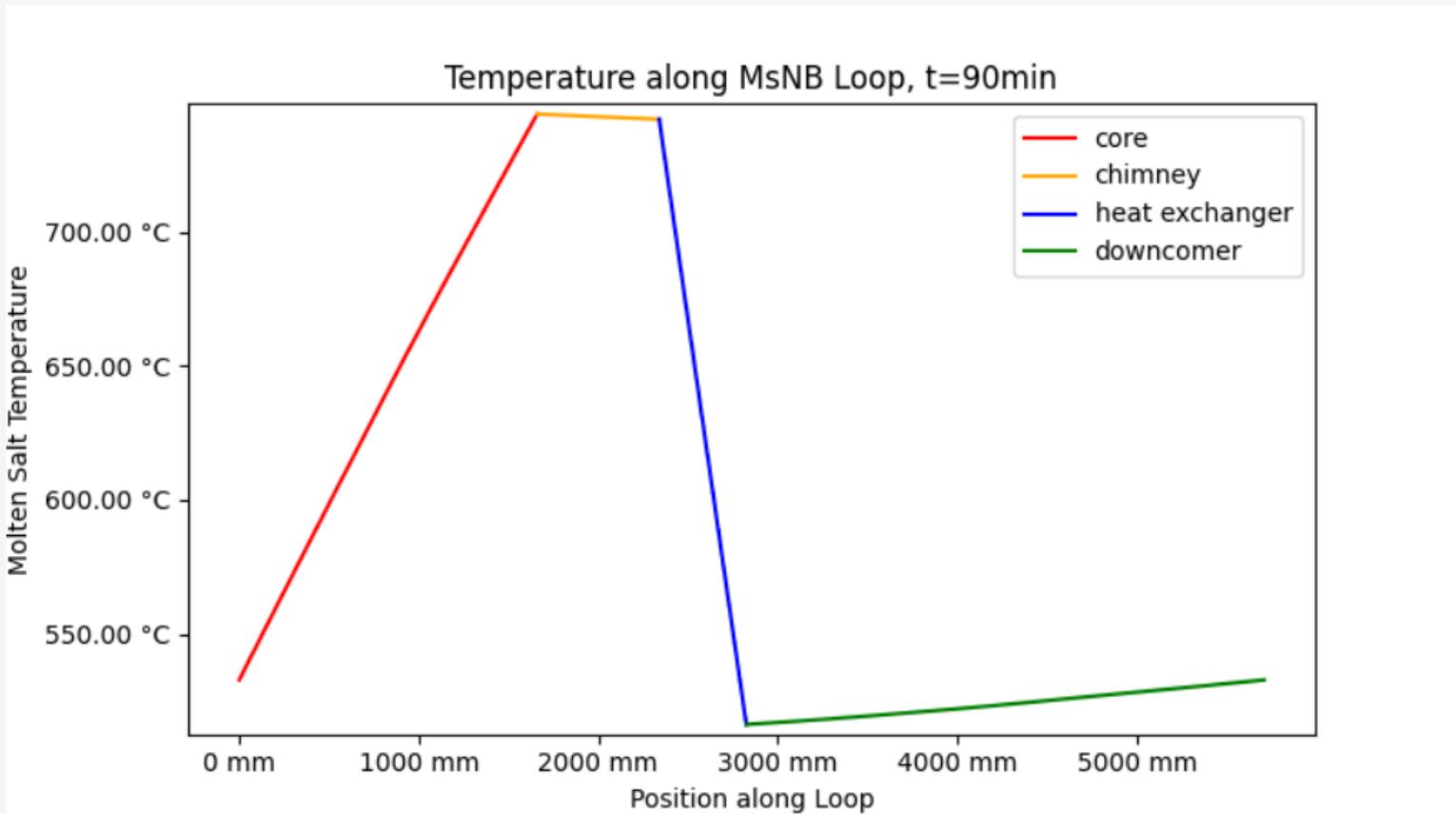
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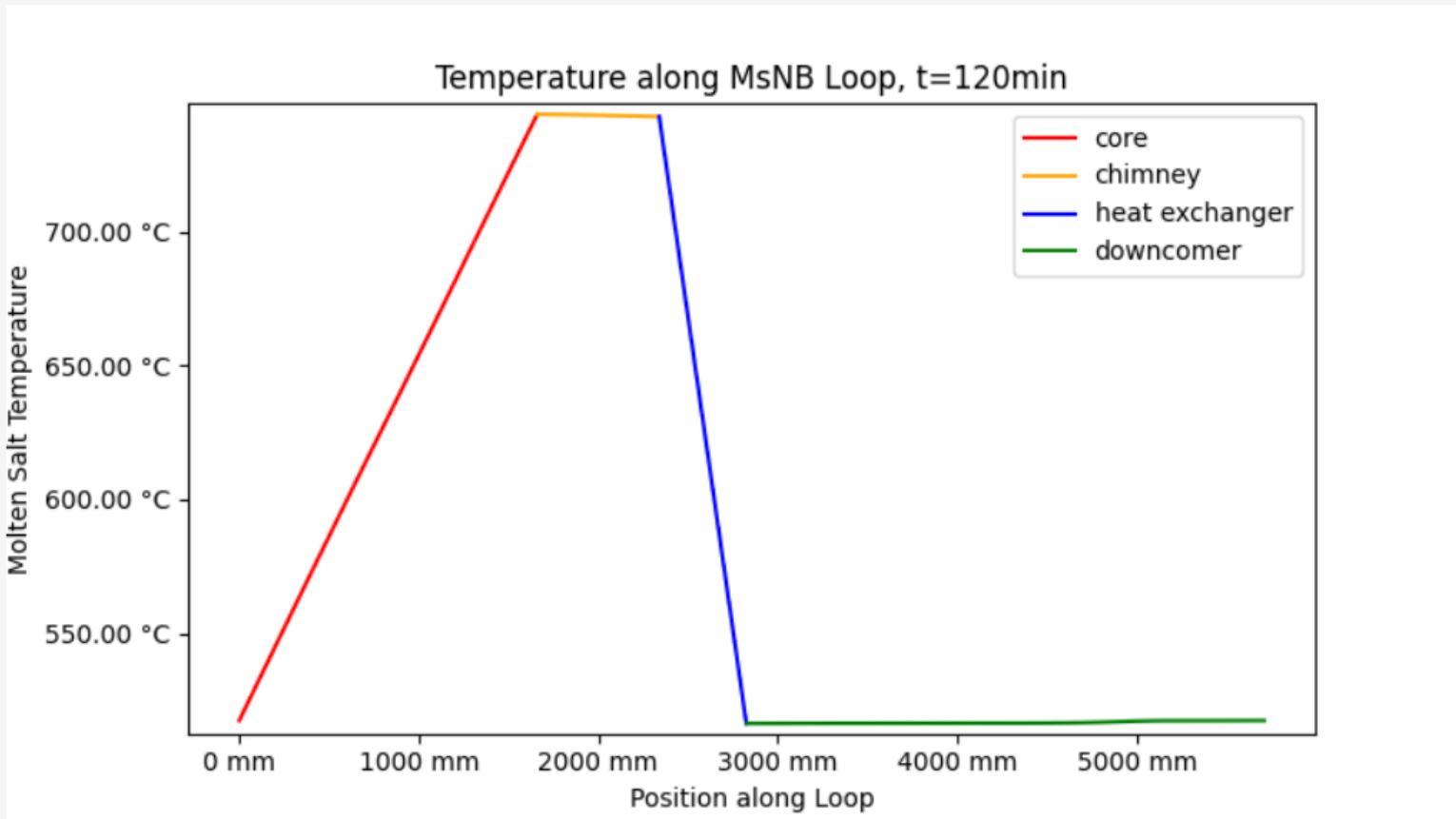
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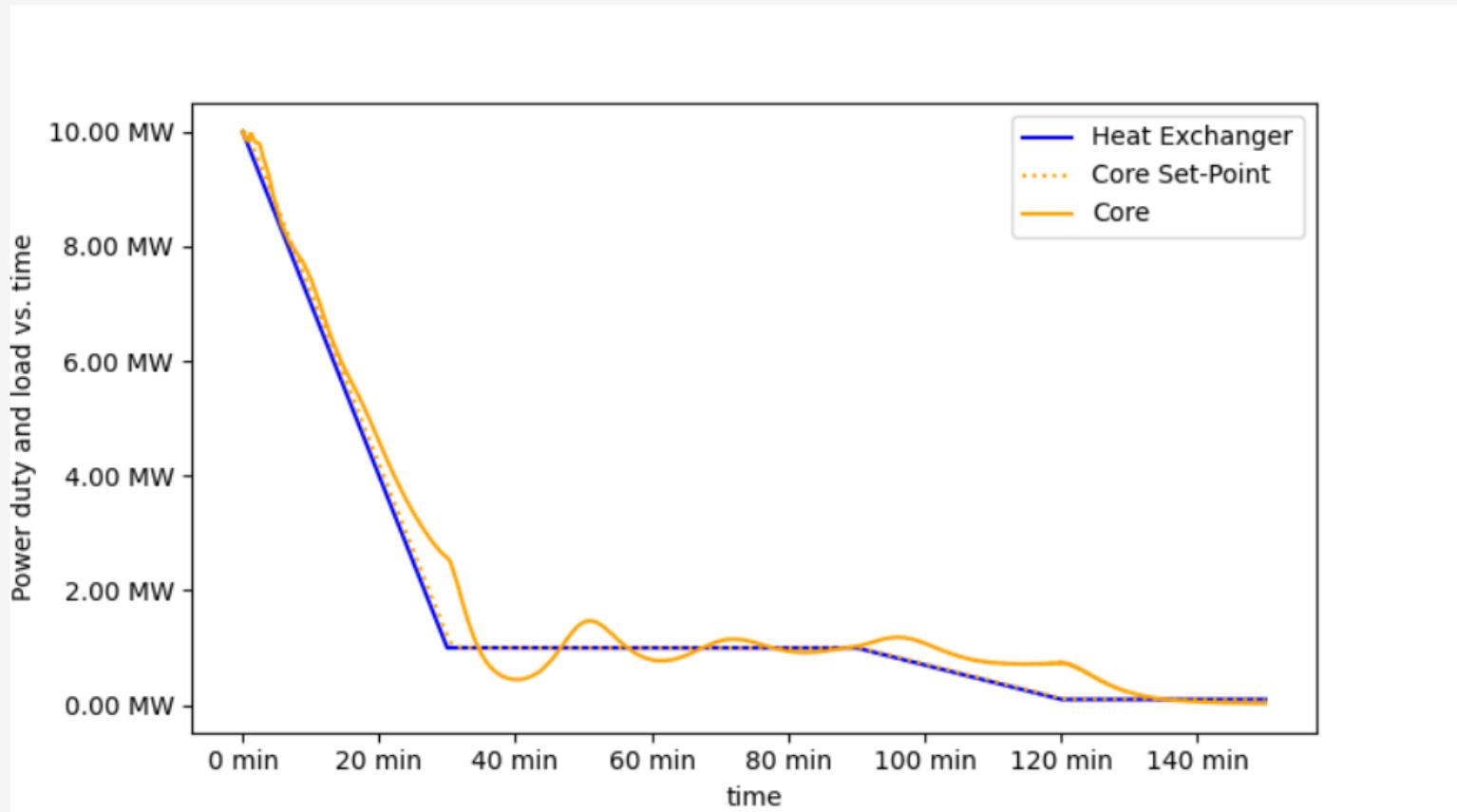
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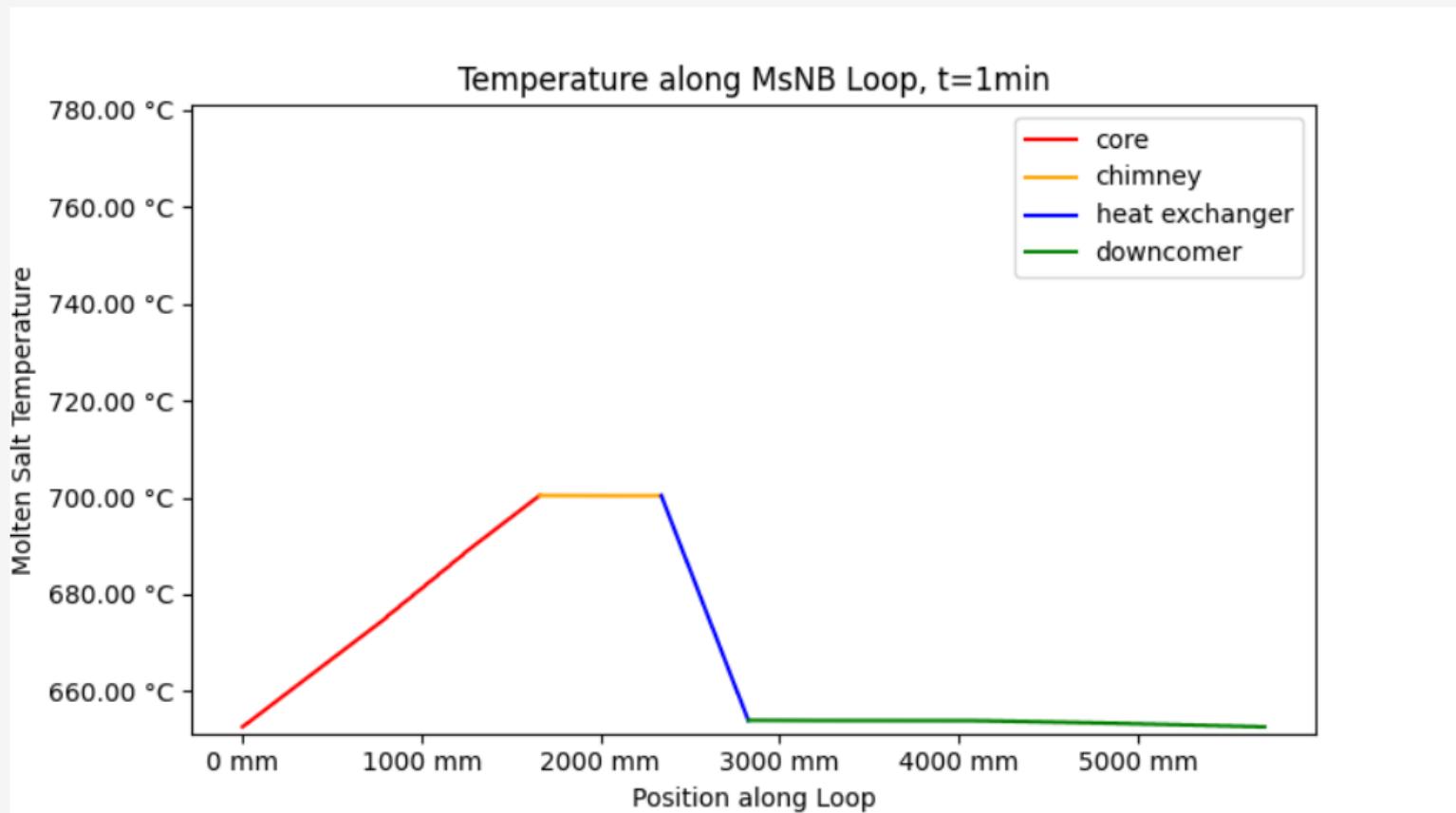
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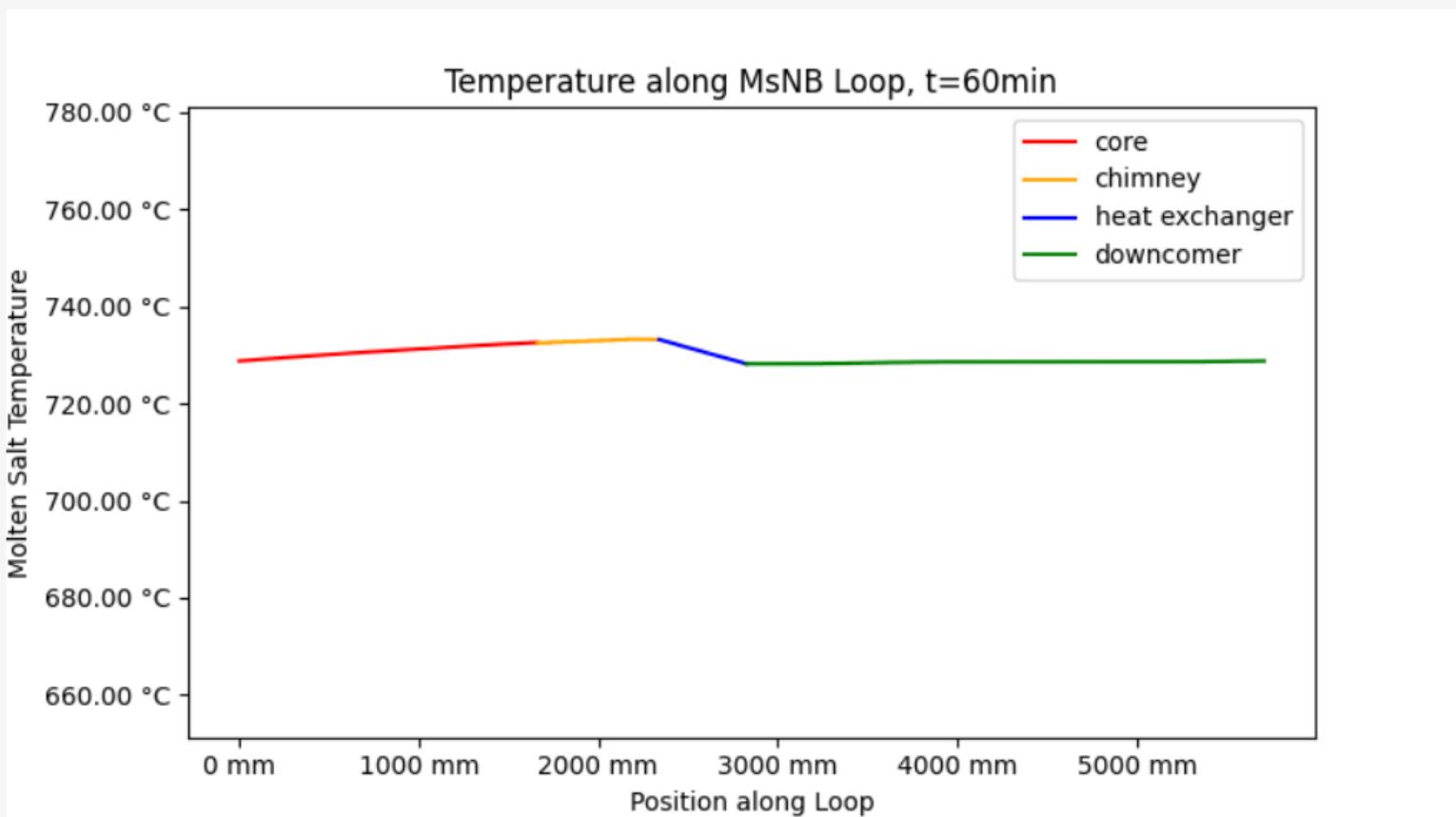
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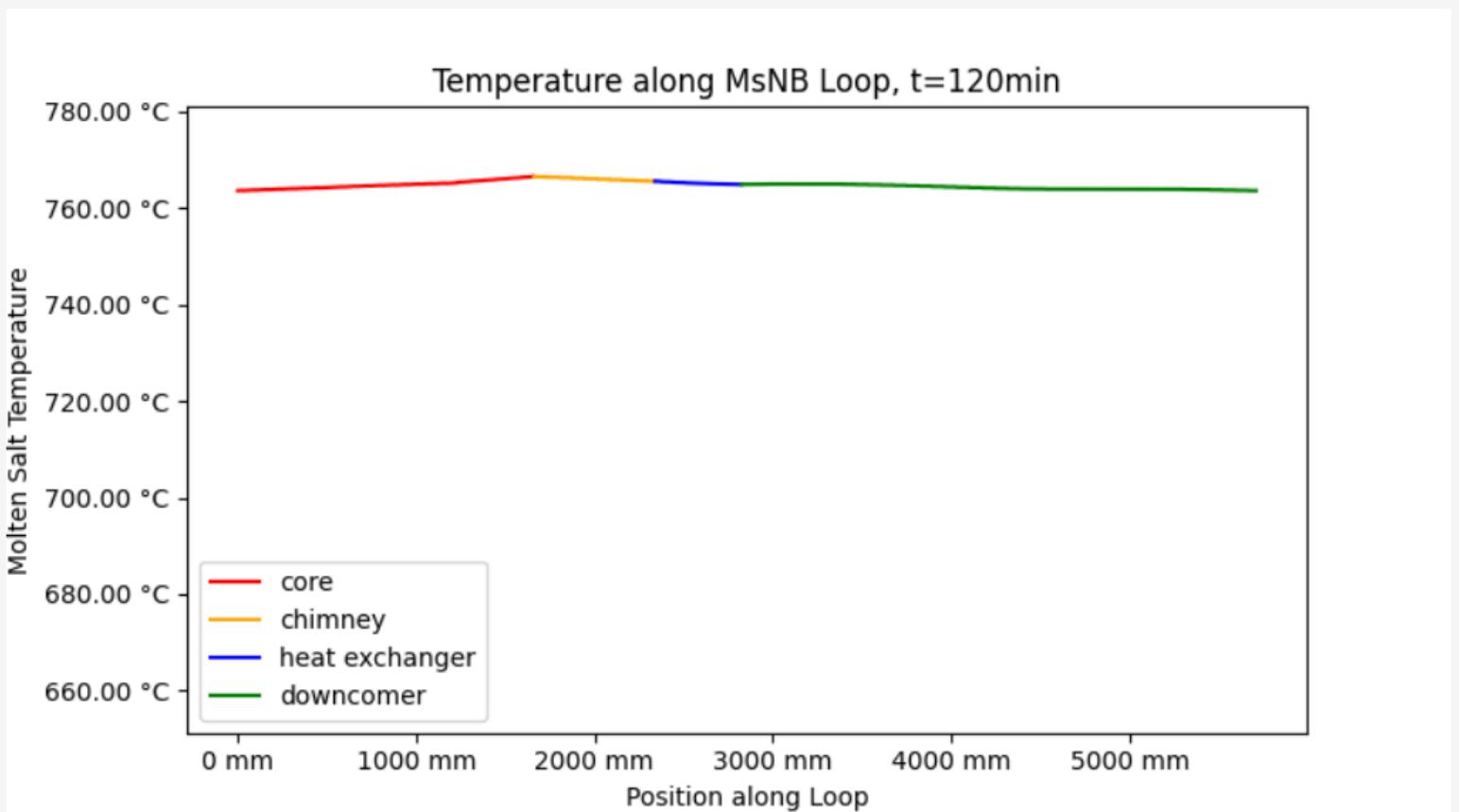
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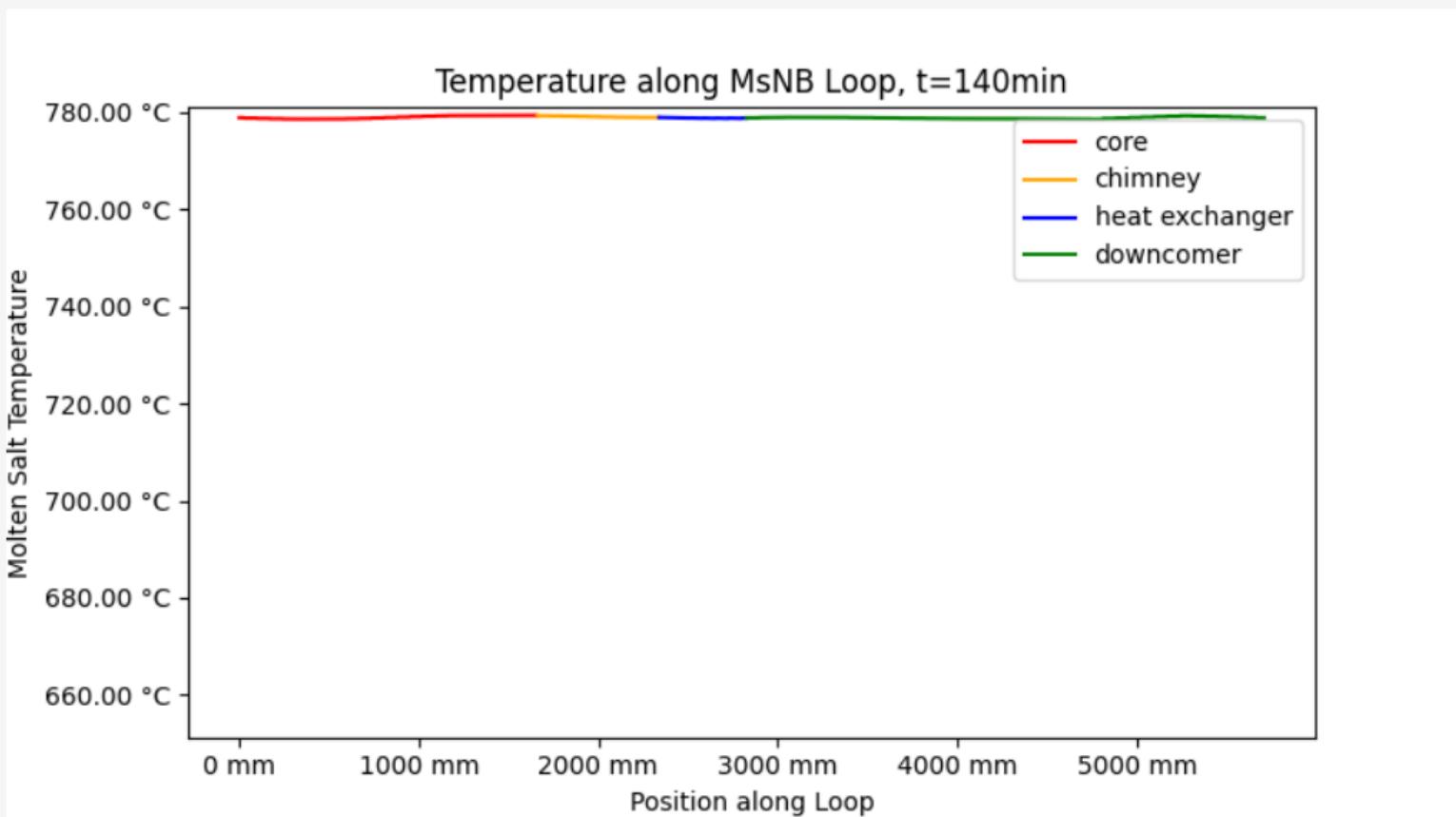
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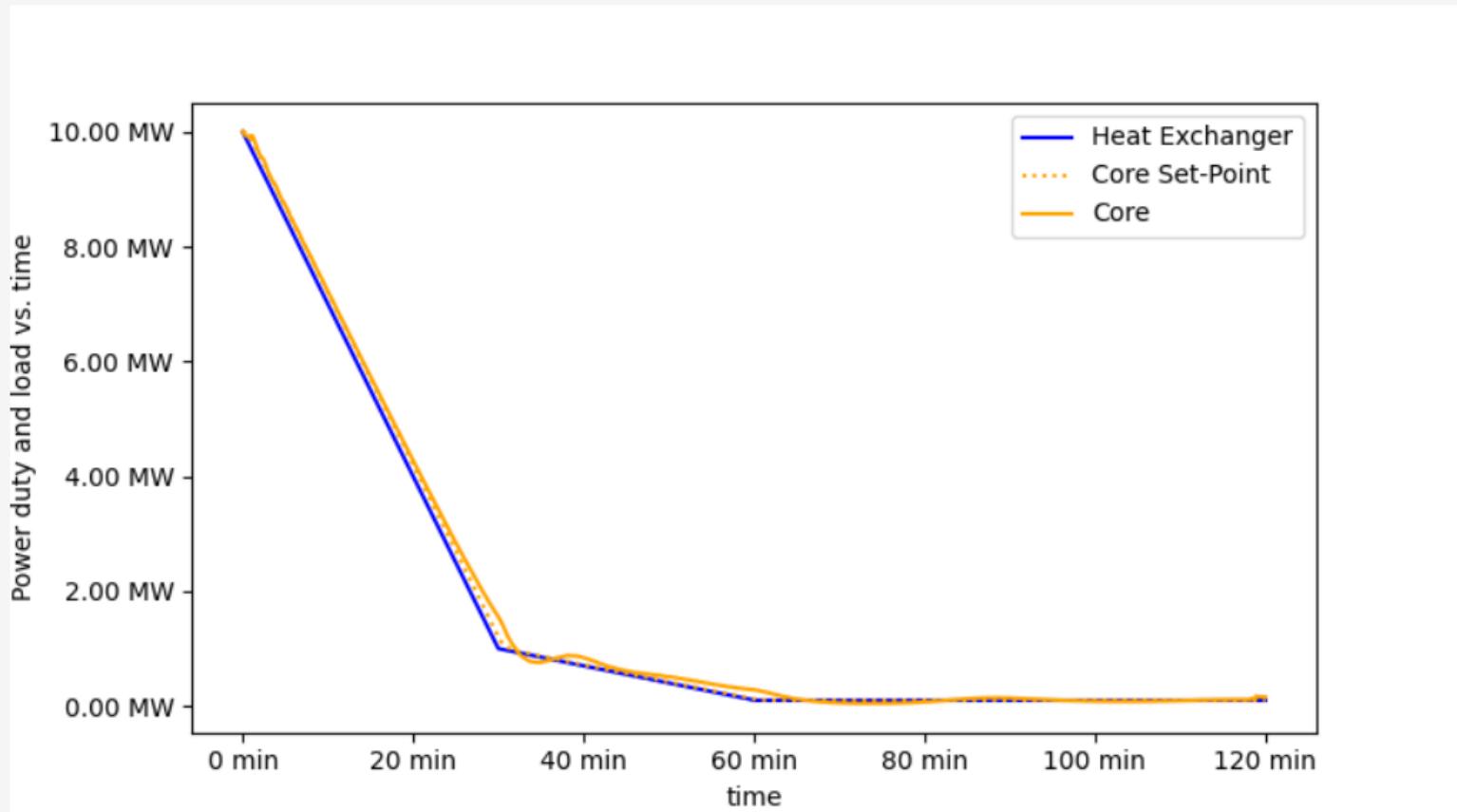
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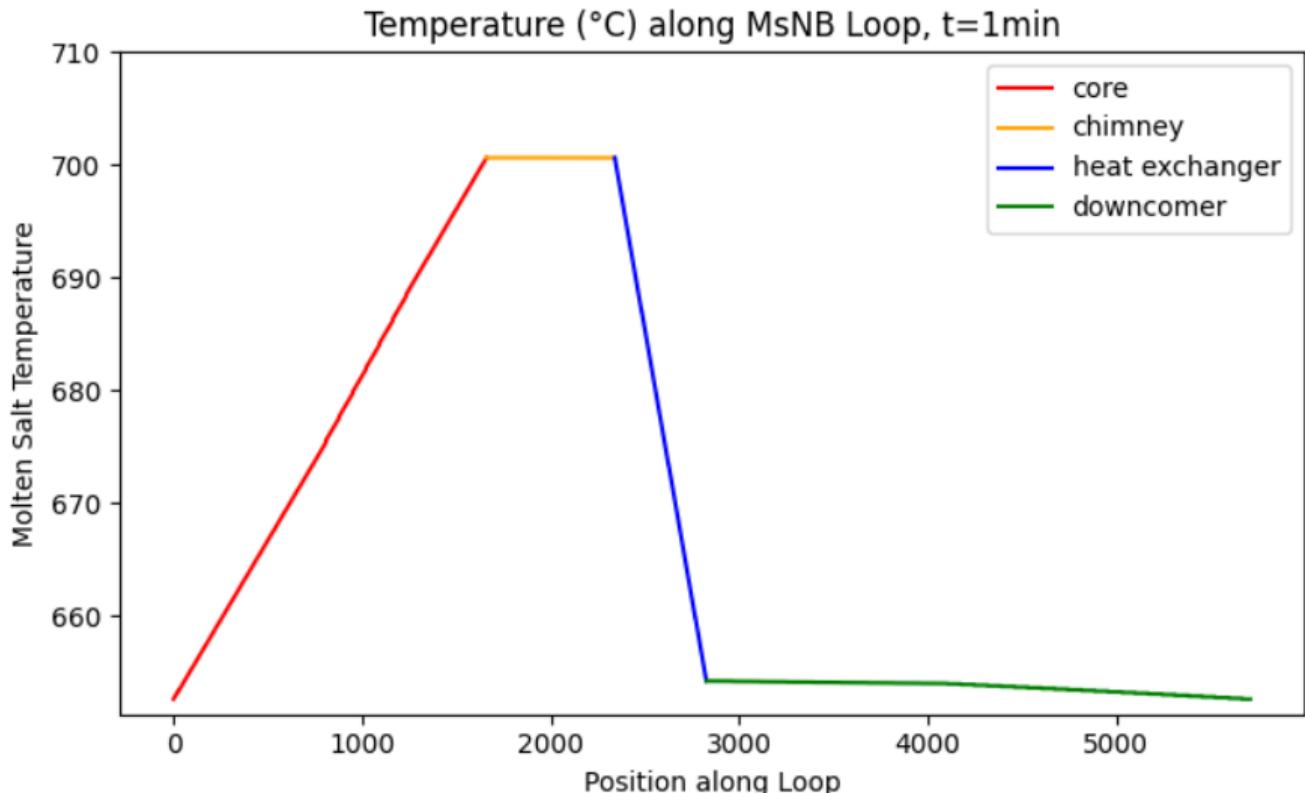
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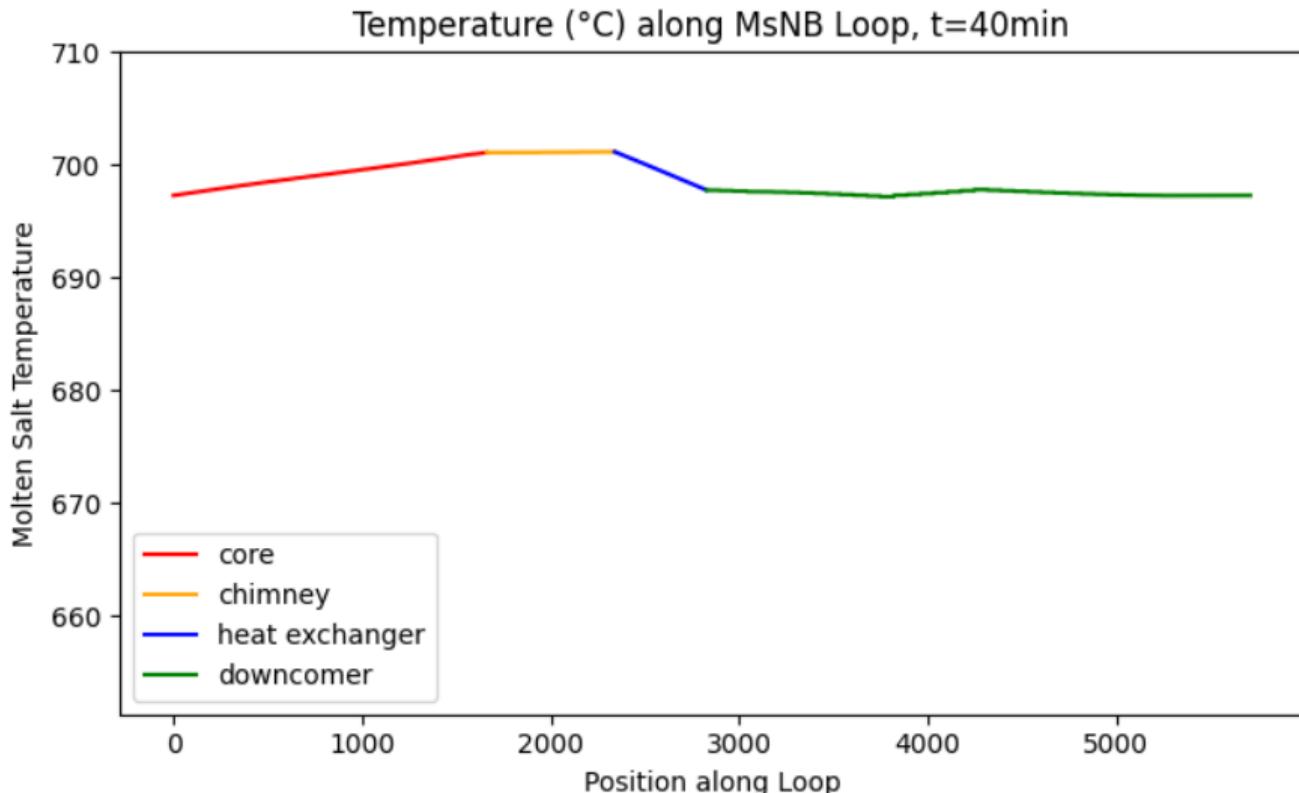
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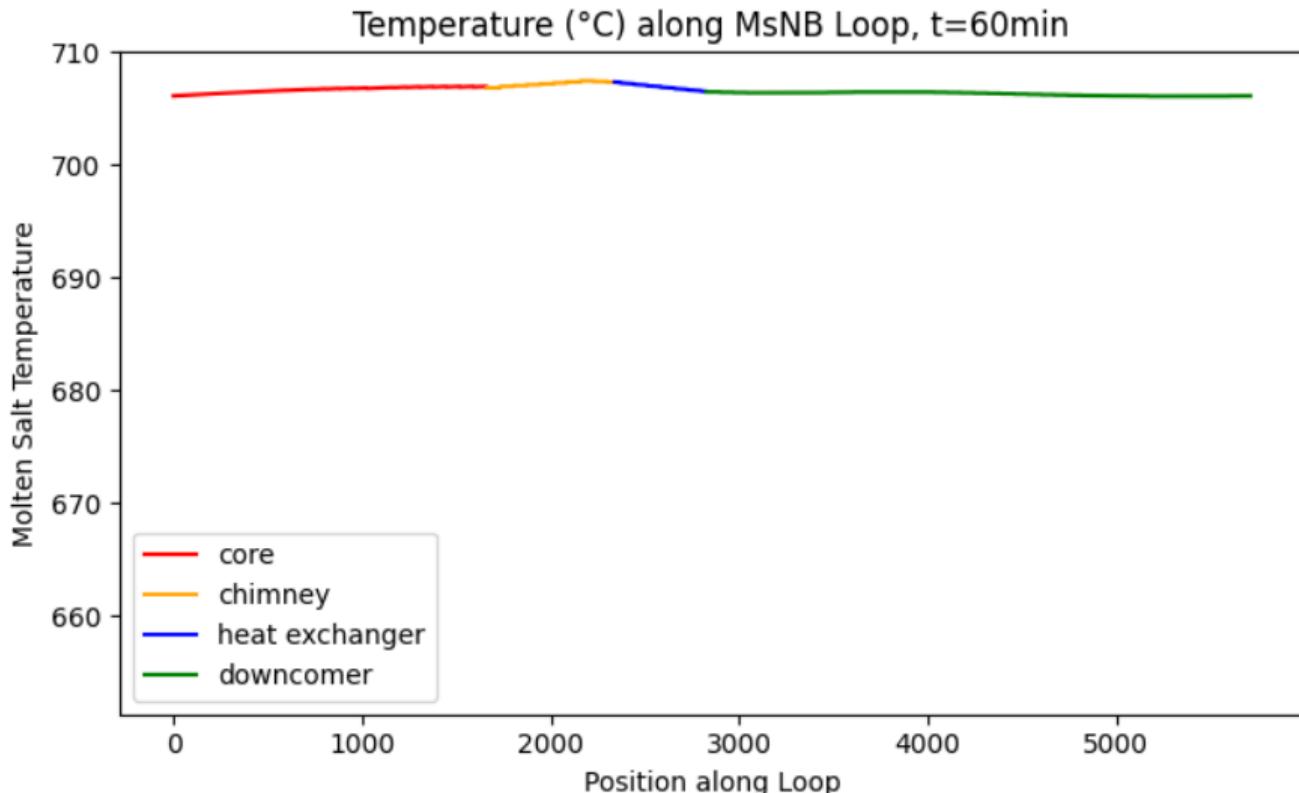
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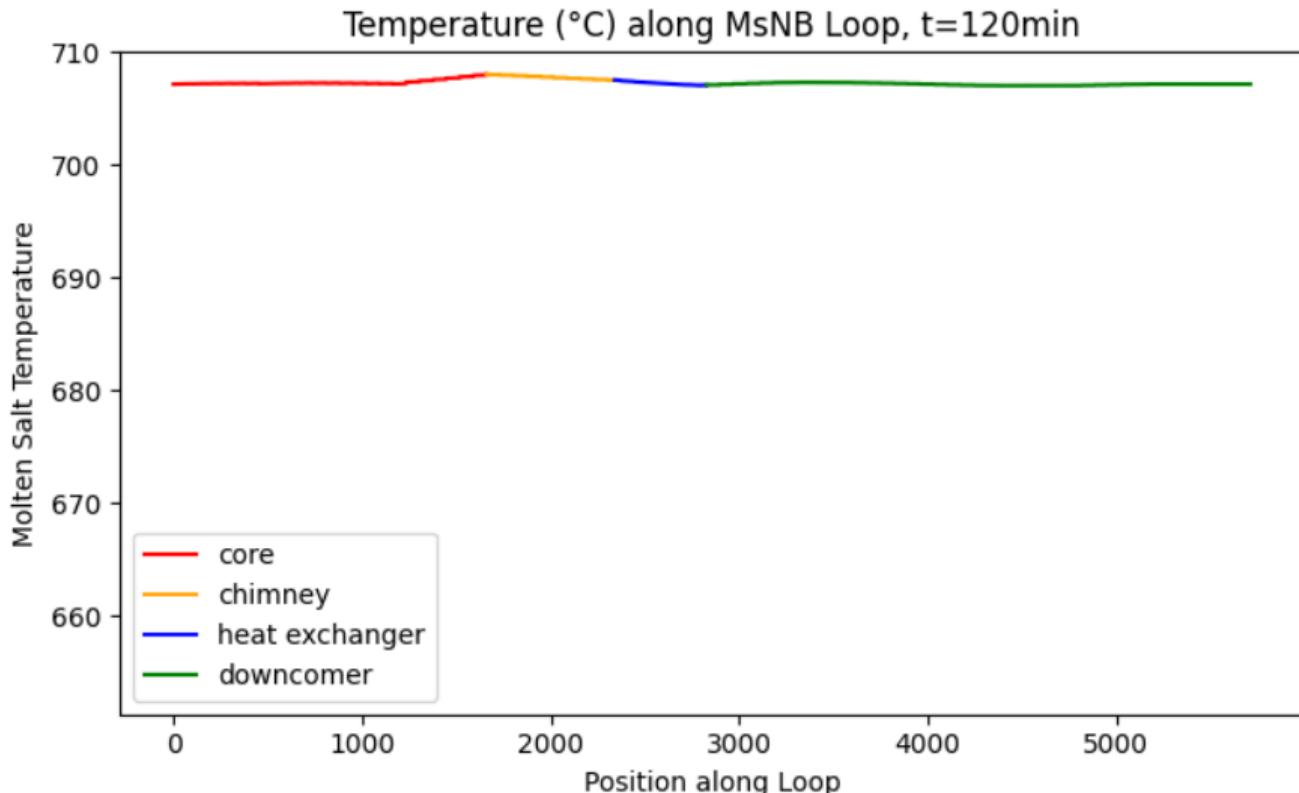
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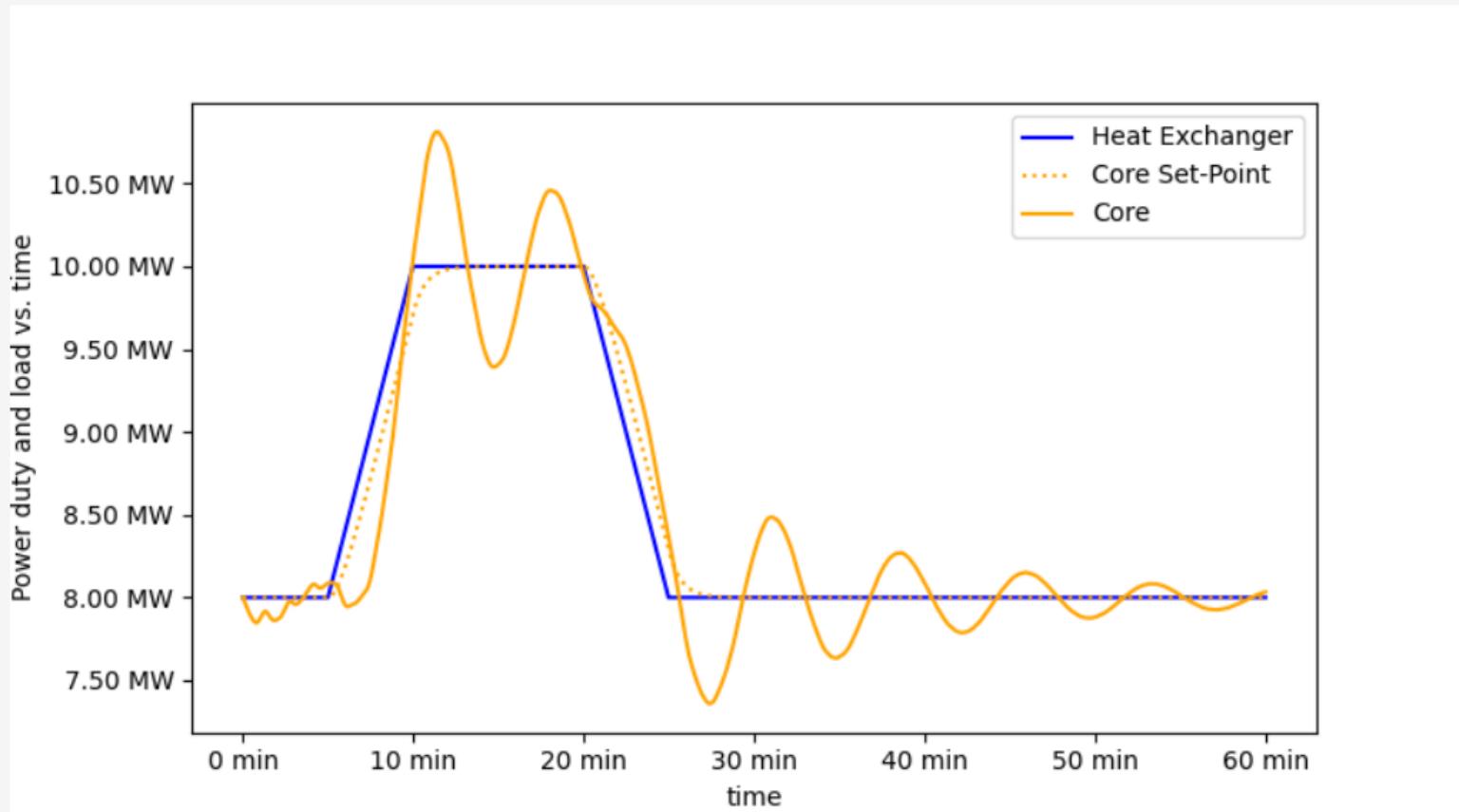
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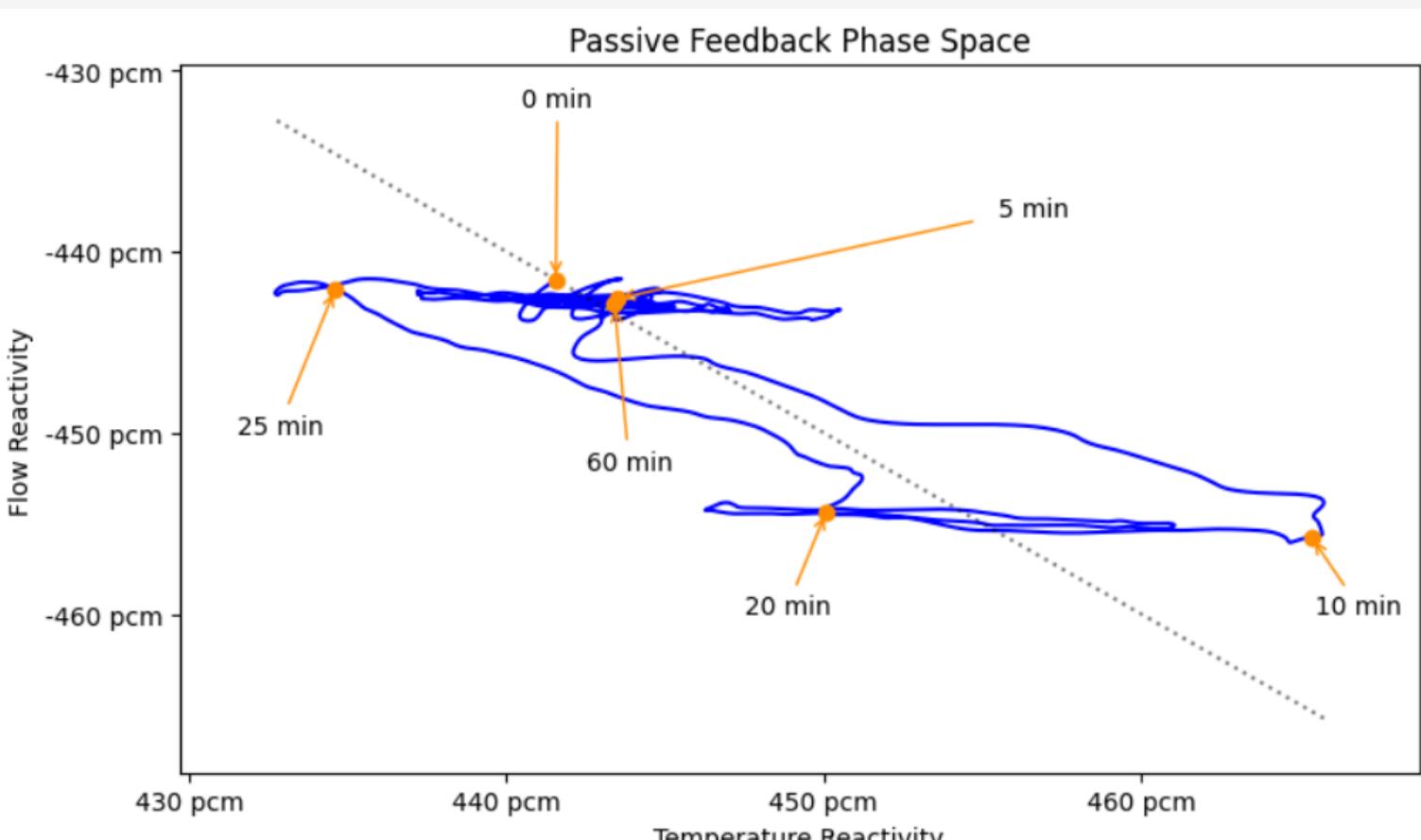
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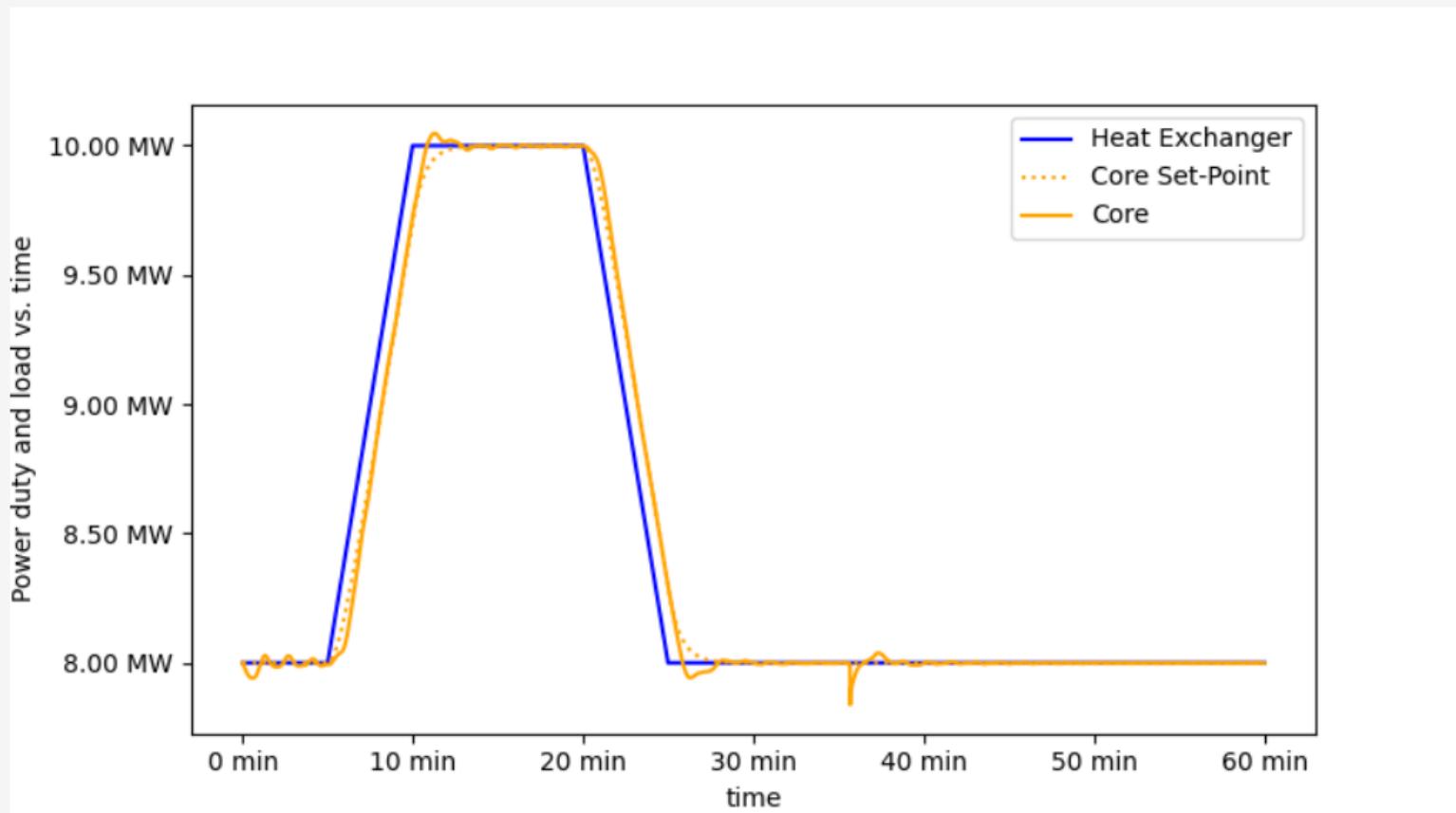
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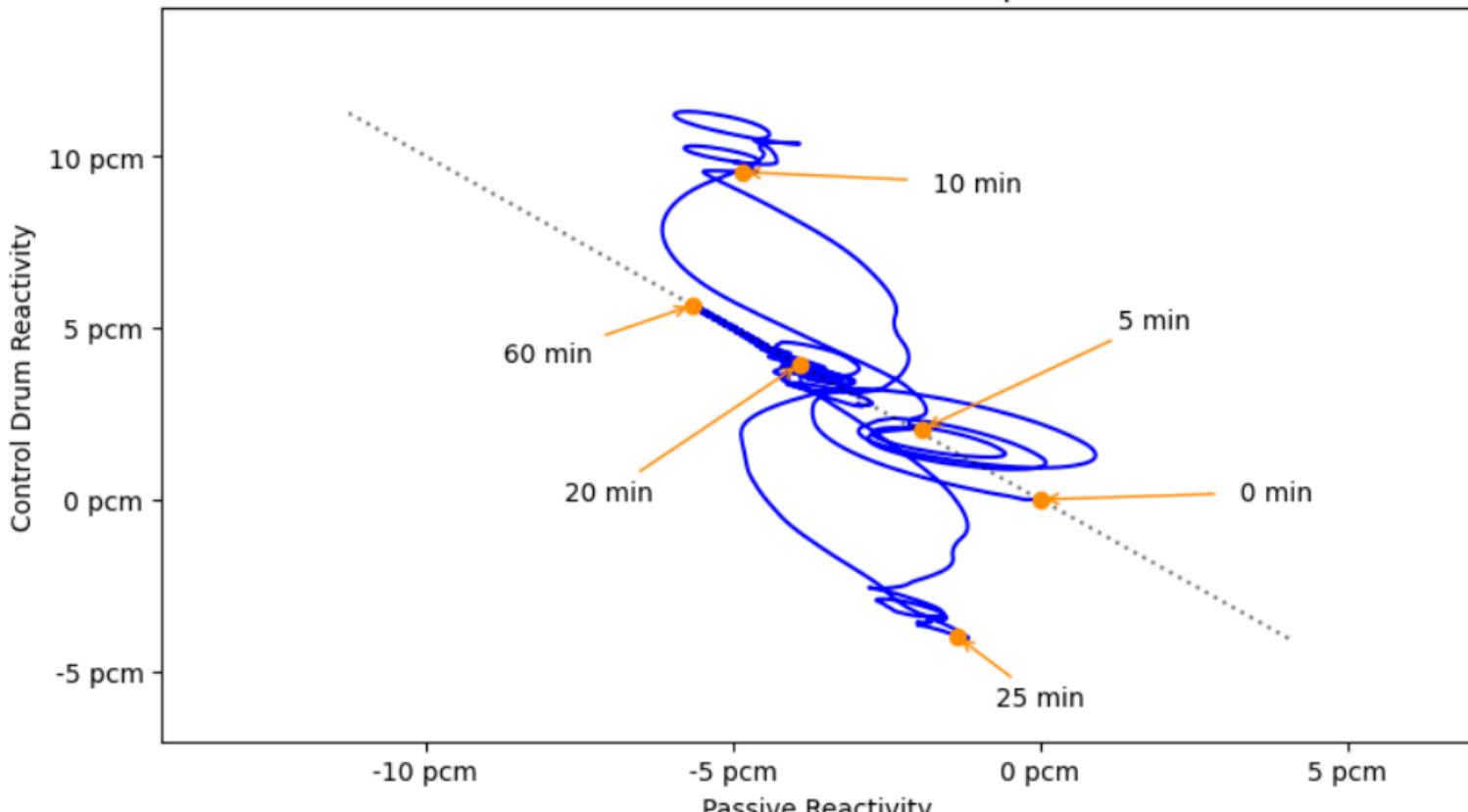
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## Controlled Feedback Phase Space



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## Summary of Models Completed

- Alternating criticality and burn-up models were developed in Serpent 2 to study the evolution of the control-reactivity curve over the life of the MSNB
- Mass and energy conservation were coupled to reactor point kinetics in a Python 3.10 code to predict the flow rate and power of the MSNB
- Time and spatial advancement routine simulates heat and mass advection according to uniform-state uniform-flow
- A pre-filter reshapes the heat exchanger demand
- A PI controller complements the passive feedback mechanisms inherent to the MSNB

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## Summary of Models Completed

## Results In-Brief

- The MSNB design studied in this work has an excess reactivity of 4.834% at hot-standby
- After 8 full-power years, the MSNB fuel is depleted enough to no longer provide enough excess reactivity for effective operation
- The autonomous response is stable, but significantly under-damped for 20% step functions and ramp functions of up to 400 kW/min
- The PI controller with improves the settling time by an order of magnitude for step functions, and essentially eliminates overshoot for ramp functions
- With a robust controller, the MSNB is suitable for load-following

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