

Dynamic System Modeling & PID Controller Design for a Molten Salt Microreactor

Sam J. Root

University of Idaho • Idaho Falls Center for Higher Education
Department of Nuclear Engineering and Industrial Management

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Department of Nuclear Engineering
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Experience

B.S Chemical Engineering (2015-2019) - Michigan Technological University
M.S. Nuclear Engineering (2021-2023) - University of Idaho - NRC Fellow
Modeling and Simulation Intern at Idaho National Lab

Select Publications

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Process
Control
Engineering

Reactor Char-
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Results and
Analysis

Conclusions

- 1 The Molten Salt Nuclear Battery
- 2 Process Control Engineering
- 3 Reactor Characterization
- 4 Results and Analysis
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1 The Molten Salt Nuclear Battery

- Introduction
- Xenon-135 Stripping In-Brief

2 Process Control Engineering

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Introduction

Gen-IV

blah

Molten Salt Reactors

Microreactors

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Xenon-135 Stripping In-Brief

$$\sigma_a^{135}\text{Xe} = 430\text{kb}$$

$$\sigma_a^{135}\text{I} = 260\text{mb}$$

$$\sigma_f^{235}\text{U} = 180\text{b}$$

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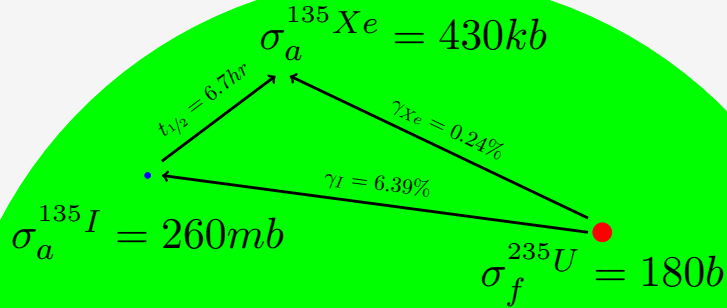
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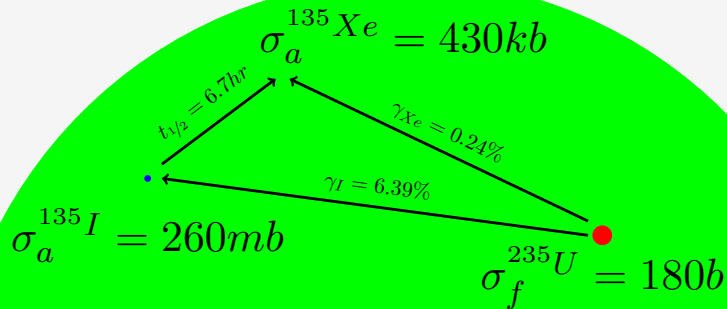
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$$\frac{dI}{dt} = \underbrace{\gamma_I \Sigma_f^F \phi(t)}_{\text{Fission Yield}} - \underbrace{\lambda_I I(t)}_{\text{Beta Decay}}$$

$$\frac{dXe}{dt} = \underbrace{\lambda_I I(t)}_{\text{Precursor Decay}} + \underbrace{\gamma_{Xe} \Sigma_f^F \phi(t)}_{\text{Fission Yield}} - \underbrace{\lambda_{Xe} Xe(t)}_{\text{Beta Decay}} - \underbrace{Xe(t) \sigma_a^{Xe} \phi(t)}_{\text{Radiative Capture}}$$

1 The Molten Salt Nuclear Battery

2 Process Control Engineering

- Control Theory
- Transport Delay Problem

3 Reactor Characterization

4 Results and Analysis

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Control Theory

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Transport Delay Problem

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- Neutronics Modeling
- Process Simulation

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Neutronics Modeling

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Process Simulation

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- Control-Reactivity Curve
- Controller Tuning
- Demand Response

5 Conclusions

Control-Reactivity Curve

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Controller Tuning

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Demand Response

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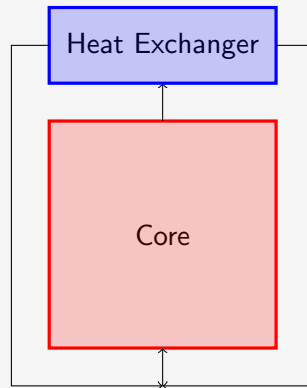
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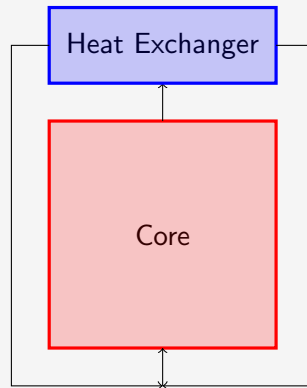
Conclusions

- Self-Contained liquid fueled molten salt micro-reactor - 10 year design
- 1 MW design using HALEU UF_4 dissolved in $FLiNaK$
- Criticality is manipulated using axial control drums
 - Neutron absorber plate covering cylinders of neutron reflector
 - Drums are rotated to point more absorber towards the core to insert negative control reactivity



Simplified schematic drawing of an MSNB

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Neutronics [?]

- Control drums give a uniform axial and radial flux profile for all reactivity insertions
- Fission product poisoning is the biggest challenge to reach the desired 10-year lifespan
- Control drum vs. reactivity curve is sinusoidal

Thermal Hydraulics [?]

Process Control

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Neutronics [?]

Thermal Hydraulics [?]

- The counteracting passive feedback effects of temperature reactivity and flow reactivity produce stable autonomous load following for relatively small ramp function power demand transients
- An in-core helix device can be used to manipulate temperature and power profiles in the core, as well as minimize advective loss of delayed-neutron precursors

Process Control

[?]

[?]

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Neutronics [?]

Thermal Hydraulics [?]

Process Control

- Design controller *compliment* the autonomous capabilities provided by the passive feedback mechanisms
- Allow larger faster, more aggressive power changes
- Additional focus on time periods with a high degree of time variance (start-up, shut-down, re-start)

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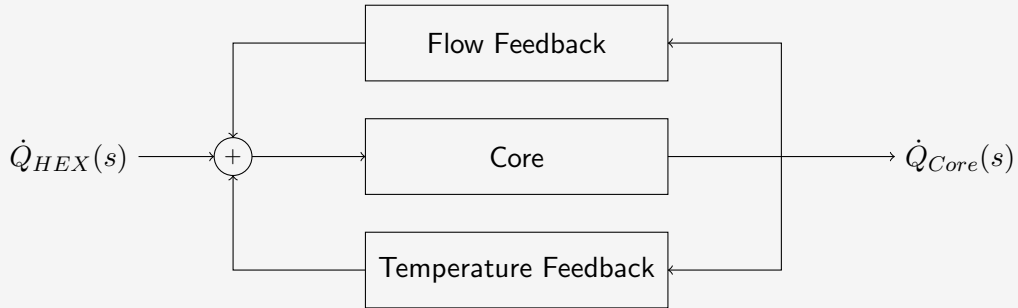
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Simplified block diagram of two primary passive feedback mechanisms in an MSNB

- Doppler broadening of resonance peaks results in more epithermal neutrons absorbed by ^{238}U etc. [1, Ch. 6]
- Molten salt fuels have high thermal expansion coefficient [1]
- Increased temperature leads to lower heavy metal density and smaller macroscopic fission cross-section at high temperature
- Similar to moderator thinning in LWRs
- These two effects combine to result in less power production at higher temperature

- Driven by advection of delayed neutron precursors [? , Ch. 3]
 - Most fission events release daughter neutrons *promptly*
 - Sometimes, unstable nuclides which decay by neutron emission are produced instead
 - $t_{1/2}$ from less than a second to over a minute [? , Ch. 6]
- Precursors produced near the core exit and long lived precursors may emit their neutrons outside of the core, so they are effectively *lost* from the fission chain reaction
- In natural circulation, larger power transport requires a higher flow rate, and greater delayed neutron losses

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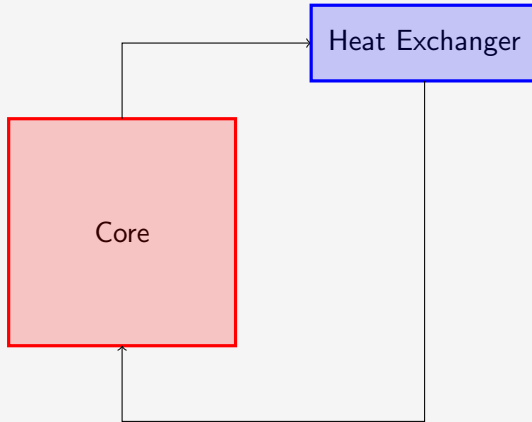
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- Start design process by discussing dynamics associated with anticipated transients
 - Natural circulation flow mode
 - Passive feedback mechanisms
 - Transport delays separating heat exchanger and core
- Thought Experiment
 - Step increase in power demand to a steady-state critical MSNB
 - Set-point is instantaneously equal to heat exchanger power consumption
 - Ideal controller which produces rapid load following with minimal overshoot



Simplified schematic drawing of a natural circulation MSNB

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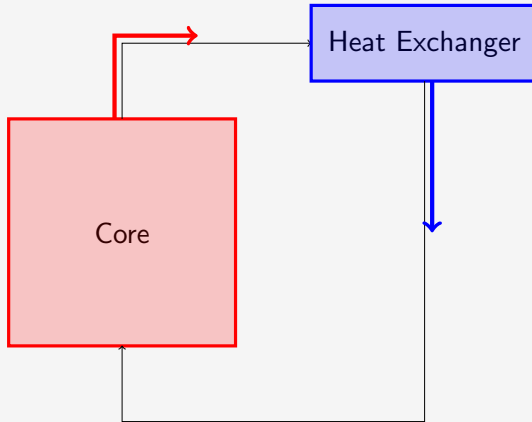
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Main Operational Control Problem - Transport Delay

Immediate Response



Simplified schematic drawing of a natural circulation MSNB

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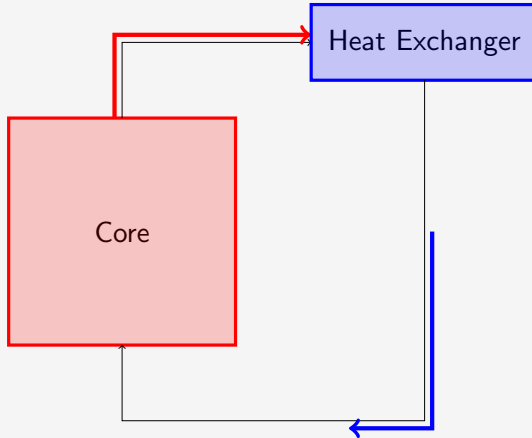
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Main Operational Control Problem - Transport Delay

Heat Exchanger Perturbation



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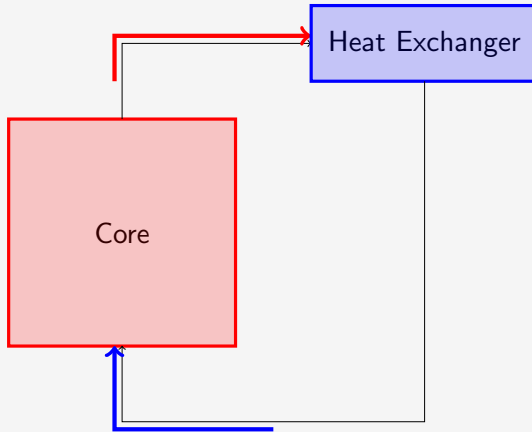
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Core Perturbation



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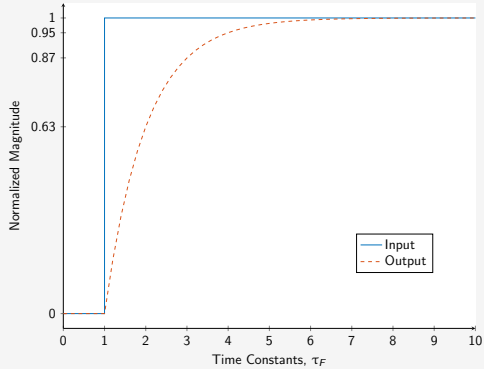
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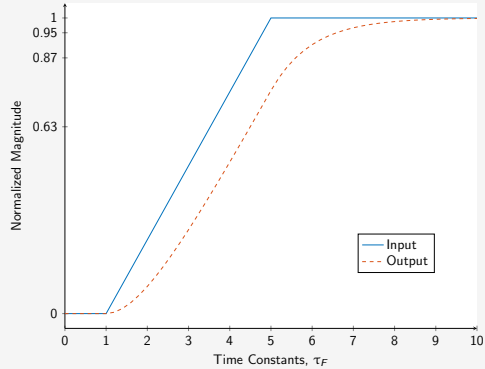
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Pre-Filter on a step-function



Pre-Filter on a ramp-function

- Minor perturbations will cause power fluctuations
- Fine grain and constant control actuation would burn out servos prematurely
- When the error is small, allow the passive feedback mechanisms to fine tune

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- Disturbances, particularly temperature reactivity, are extremely high frequency - On order of mean neutron lifetime [?, Ch. 7]
- Control actuation is similarly quick
- Time delays on the order of dozens of seconds to minutes
- Inserting control reactivity to counteract temperature reactivity at the exact right moment would be difficult or impossible, so it is unlikely that a disturbance feedforward controller could reject the disturbance before it causes error [?, Ch. 10]
- Disturbance rejection best left to feedback PID controller

- Sinusoidal control drum angle vs. reactivity curve - non-linear reactivity actuation - Taylor Series approximation to linearize around the operating point [? , Ch. 2]
- Fissile depletion changes the amount of control reactivity required to make the core critical - time-variant controller bias - Bias and gain schedule [?]
- Control drums manipulate *criticality*, not power directly - highly time-dependent control actuation

- Equilibrium Poisoning
 - Poisons like ^{135}Xe and ^{149}Sm build-up after the reactor starts - this causes a negative reactivity insertion
 - Reach equilibrium over the first ~ 100 hours
 - Gain/Bias schedule may be used
 - Alternatively, a burnable poison with appropriate *effective* half-life could be selected - ^{157}Gd shows promise to counteract ^{135}Xe build-up
- Restart Poisoning
 - ^{135}Xe levels increase following shut-down because its beta-precursor (^{135}I) decays faster
 - Requires a lot of excess control reactivity and very good control to counteract the positive reactivity insertion of poison burn-out after restart
 - Low-flux burn-out instead of full shut-down
 - Stripping ^{135}Xe and other fission gasses before re-start

- Use KCODE to develop control drum vs. reactivity curve at various points in the core lifespan
- Use Burn-up routine to study how the core criticality at different conditions effects the control drum vs. reactivity
 - Cold/clean start-up
 - Burnable poison start-up
 - Equilibrium poisoning
 - Long-term depletion of fissile isotopes
- Develop bias/unity point schedule
- Will to use HPC or Falcon

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- 1D+time finite element model that accounts for passive feedback mechanisms during unsteady state subcritical, critical, and supercritical modes to calculate the core power and flow loop temperature profile over time
- Simulate system response to:
 - Control actuation
 - Heat exchanger transients
- Empirical fitting of reactor transfer function
- Studies can be conducted locally or with cluster resources

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- Model control loop in Simulink
- Investigate system stability using frequency response tests
- Use built-in numerical methods to implement a PID controller tuning method
- Repeat for different core conditions to develop gain-schedule and/or look-up table for the controller parameters

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- Implement control drum reactivity, pre-filter, and PID controller into the process simulation
- Test autonomous response to heat exchanger power demand transients
- Repeat with controller active
- Quantitatively compare response using settling time, dampening ratio, peak overshoot ratio etc.

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Table: Timeframe for Execution of Project

Tasks	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	Apr.
Control Drums	X	X	X				
Process Simulation		X	X	X			
Controller Tuning				X	X		
Implementation					X	X	
Cross-Cutting						X	X
Defend							X

- Poison perturbations following power transients [?]
- Melting of *in-situ* frozen salt
- SCRAM system must be passive
- Decay heat system [?]
- Flow rate control

[?]

[?]

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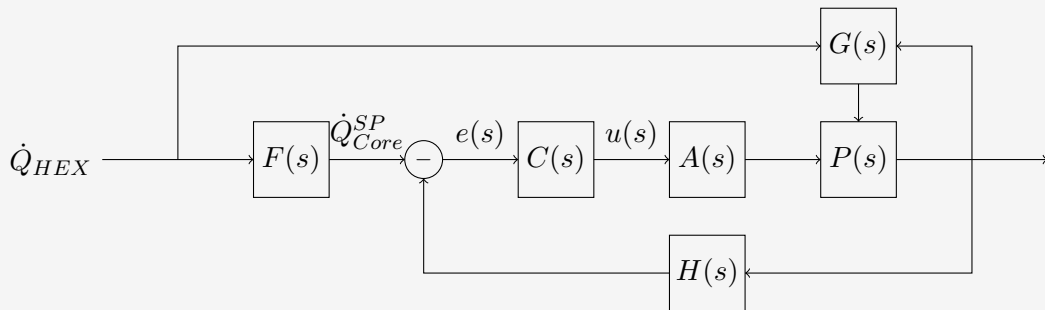
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Simplified control loop of a natural circulation MSNB

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