

Stefanie Donner

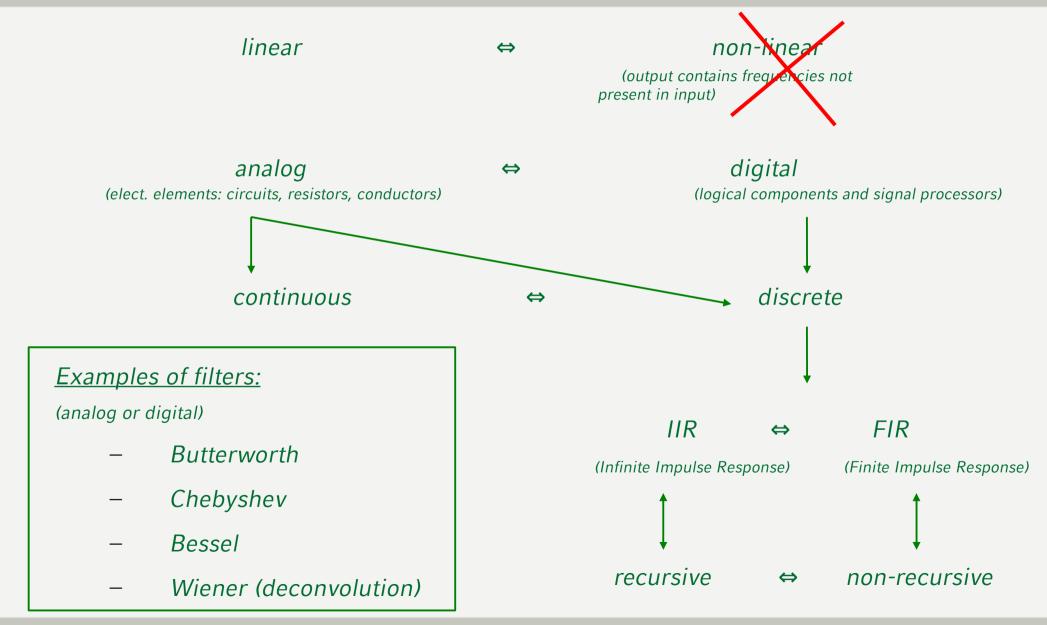
Geophysical Data Analysis

L08 – Filtering II



Classification

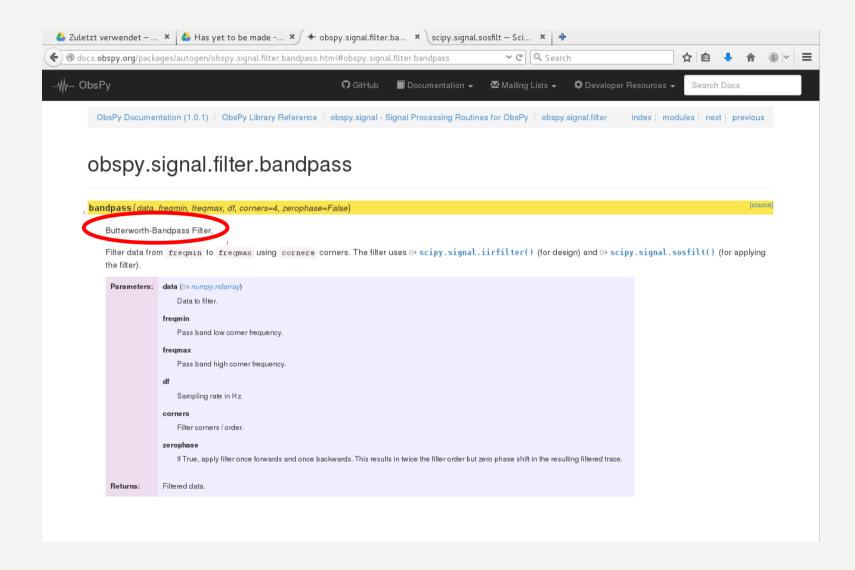






The Butterworth filter







The Butterworth filter



... designed to have as flat a frequency response as possible within the passband.

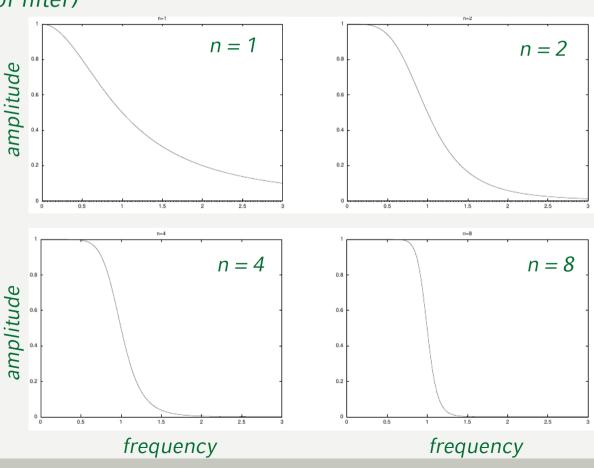
e.g. gain of a **low- pass filter** with a cut-off frequency at 1 Hz: with n the number of poles (i.e. order of filter)

$$G(\omega) = |T(j\omega)| = \sqrt{\frac{1}{1+\omega^{2n}}}$$

with angular frequency $\omega=1~{\rm Hz}$

$$G(\omega) = 1/\sqrt{2} = 0.707$$

- standard FFT filter
- very smooth response
- no ripples in pass-band

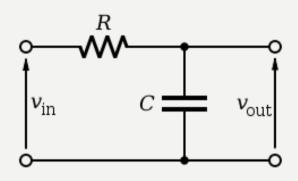




The Butterworth filter



Remeber the RC filter?



$$RC\dot{y}(t) + y(t) - x(t) = 0$$

$$\frac{A_0}{A_i} = \frac{1}{RCj\omega + 1} = T(j\omega)$$



Analog Butterworth filter of order n = 1!



The Butterworth filter



Other than low-pass filters can be constructed from this one:

Lowpass:
$$G(\omega)=|T(j\omega)|=\sqrt{\tfrac{1}{1+\omega^{2n}}}$$

$$G^2(\omega)=|T(j\omega)|^2=T(j\omega)T^*(j\omega)=\tfrac{1}{1+\omega^{2n}}=\tfrac{1}{1+(\tfrac{\omega}{\omega_c})^{2n}}$$

Highpass:
$$T_h(j\omega) = 1 - T_l(j\omega) \qquad \qquad T(j\omega) = \frac{RCj\omega}{\sqrt{1 + (RCj\omega)^2}}$$
 (for RC filter, n=1)

Bandpass: shifting transfer function along frequency axis to centre it around ω_b

$$|T_b(j\omega)|^2 = \frac{1}{1 + [(\omega - \omega_b)/\omega_c]^{2n}}$$



Poles & zeros (very roughly)



Laplace and z-transform are two mathematical tools to break the impulse response into sinusoids and decaying amplitude

$$L\left[f(t)\right] = \int_{-\infty}^{\infty} f(t)e^{-st}dt = F(s)$$

$$s = \sigma + j\omega$$

$$Z\{x[n]\} = \sum_{n=-\infty}^{\infty} x[n]z^{-n} = X(z)$$

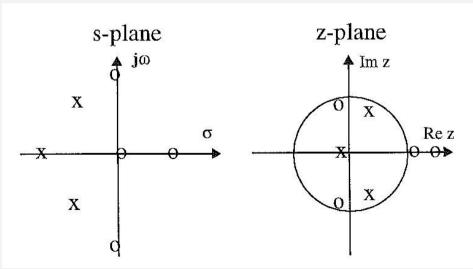
z = continuous complex variable

i.e. expressing the system's characteristics as one complex polynomial divided by another complex polynomial

$$T(j\omega) = \frac{a_0 + a_1(j\omega) + a_2(j\omega)^2 + \dots}{b_0 + b_1(j\omega) + b_2(j\omega)^2 + \dots}$$

Zeros: roots of numerator

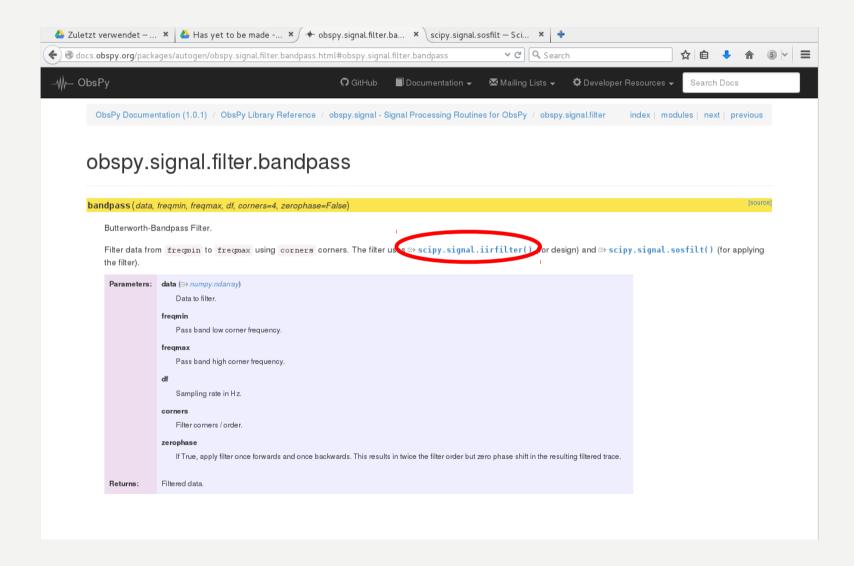
Poles: roots of denumerator





The Butterworth filter







Recursive filters



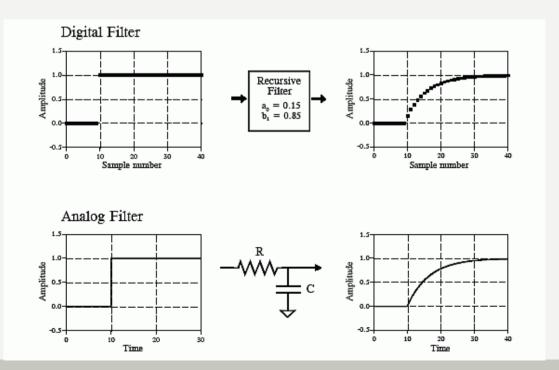
... filter, which re-uses one or more of its outputs as input (feedback system)

usually results in an unending impulse response (but not always!!!)

Recursive filters convolve the input signal with a very long fitler kernel. They *bypass* a longer convolution.

$$y[n] = a_0x[n] + a_1x[n-1] + a_2x[n-2] + a_3x[n-3] + \cdots + b_1y[n-1] + b_2y[n-2] + b_3y[n-3] + \cdots$$

... they can mimik analog filters ... (1st order lowpass filter)





IIR – Infinite Impulse Response

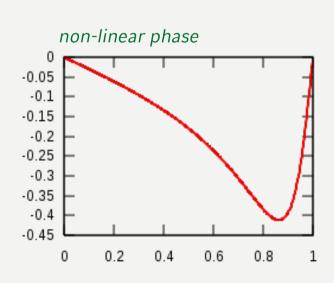


With recursive filters we can create filters with infinitely long impulse responses. Almost all analog electronic filters are IIR filters.

difference equation (for derivation of transfer function):

$$y[n] = \frac{1}{a_0} \left(\sum_{i=0}^{P} b_i x[n-i] - \sum_{j=1}^{Q} a_j y[n-j] \right)$$

- difficult to implement but easy construction
- require less computing effort than FIR filters (because it needs lower orders)
- problems with instability at higher orders (due to recursive character - "feedback")
- non-linear phase
- time-invariant and causal





IIR filter - phase



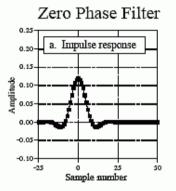
What happens to the signal, when the filter has a non-linear phase?

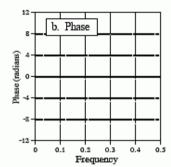
Pulse response =

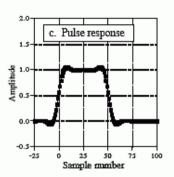
pos. step response + neg. step response

visualises what happens to rising
and falling edge in signal

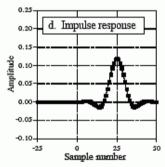
How to solve?

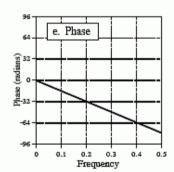


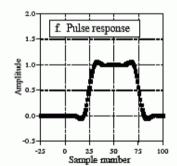




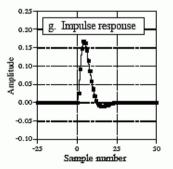
Linear Phase Filter

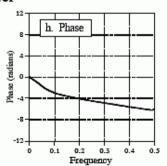


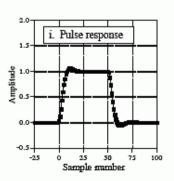




Nonlinear Phase Filter









FIR – Finite Impulse Response



FIR filters are non-recursive filters, i.e. the output only depends on the most recent input values

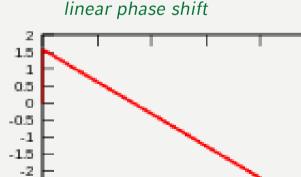
difference equation (for derivation of transfer function):

$$y[n] = b_0 x[n] + b_1 x[n-1] + \dots + b_N x[n-N] = \sum_{i=0}^{N} b_i x[n-i]$$

- easy to implement
- always stable
- easily designed to be linear- or zero-phase
- causal or acausal
- many coefficients needed for steep filter



not appropriate for FFT filtering, too slow & memory intensive, no real-time processing possible



0.4

0.6

-2.5

-3 -3.5

0

0.2

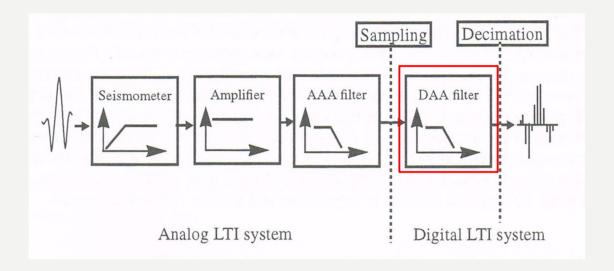
0.8



FIR – Finite Impulse Response



Application: as digital anti-alias filter in modern seismic acquisition systems



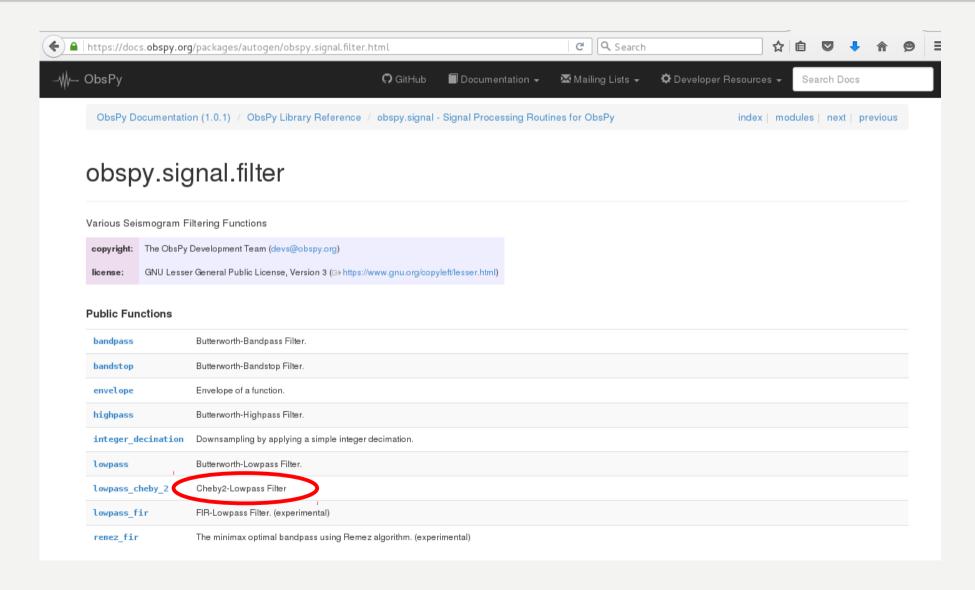
Because:

easy to match given design specifications with great accuracy very steep and stable filters possible linear-phase property can be implemented exactly



Chebyshev filter







Chebyshev filter



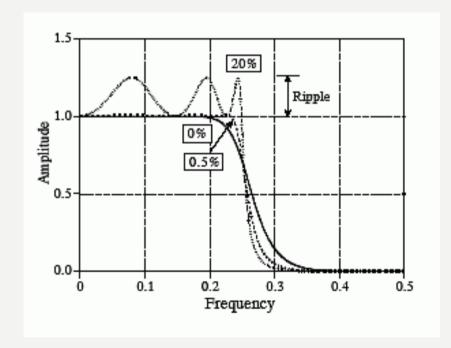
... steeper roll-off and more ripples than Butterworth

- Very fast (recursion rather than convolution)
- Mathematical characteristic derived from Chebyshev polynomials
- Ripples either in pass- (Chebyshev I) or stop-band (Chebyshev II)

$$G_n(\omega) = |T_n(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2 \cdot P_n^2(\frac{\omega}{\omega_0})}}$$

with ϵ as the ripple factor (good choice: 0.5%)

Used where the frequency content of the signal is more important than having a constant amplitude.



more ripples (bad)

→ steeper roll-off (good)



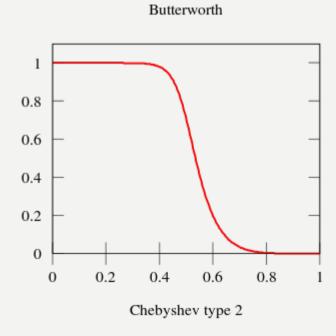
Comparison

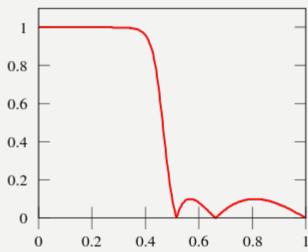


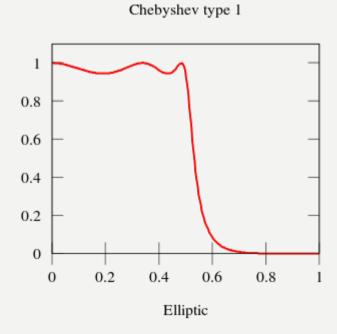
- Amplitude response functions
- All fifth-order filters

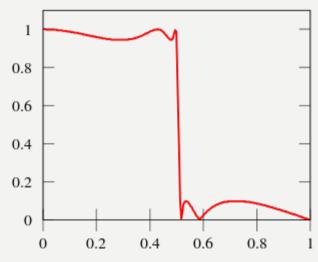
Butterworth: poles on a "circle"

Chebyshev: poles on an "ellipse"





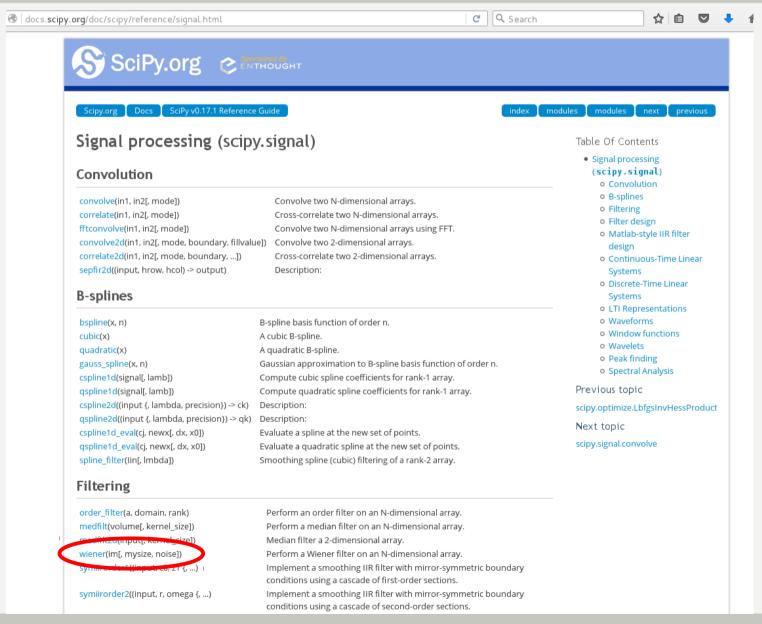






scypi signal processing

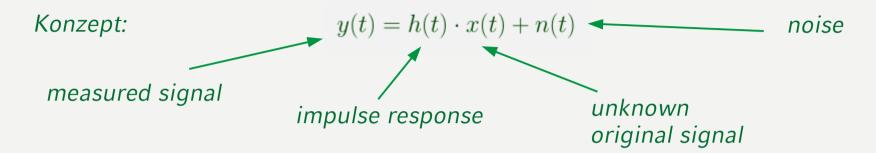






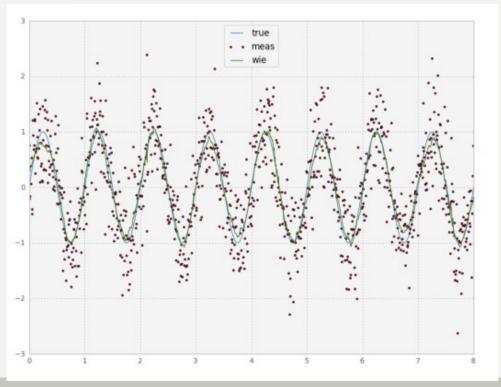
Wiener filter





Look for g(t), such that:
$$x(t) \approx \hat{x}(t) = g(t) \cdot y(t)$$

$$G(\omega) = \frac{H^*(\omega)X(\omega)}{|H(\omega)|^2 X(\omega) + N(\omega)}$$





Wiener filter

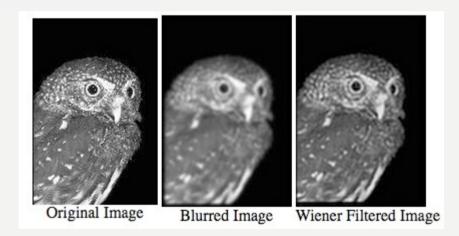


... used for **deconvolution** ...

Rewriting the equation:

$$G(\omega) = \frac{1}{H(\omega)} \left[\frac{|H(\omega)|^2}{|H(\omega)|^2 + \frac{N(\omega)}{X(\omega)}} \right]$$

- [] = 1 for noise-free data
 - → simple inverse filter
- If SNR decreases → [] decreases
 → frequencies are damped with dependance on SNR



However, we need to know the SNR (or at least have a good estimate).





So far, questions to



or ...





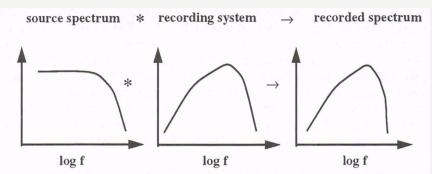


Inverse filters



Recording systems act as a filter on the data

$$X(\omega)\cdot T(j\omega) = Y(\omega)$$



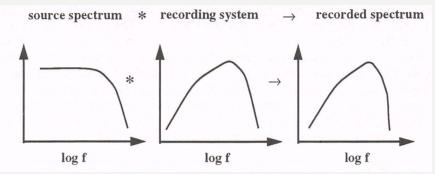


Inverse filters



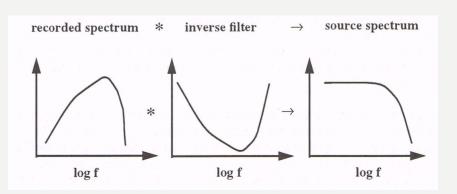
Recording systems act as a filter on the data

$$X(\omega) \cdot T(j\omega) = Y(\omega)$$



- Before analysis this filter needs to be reversed
 - restitution
 - deconvolution
 - removing the instrument response or instrument characteristic

$$Y(\omega) \cdot \frac{1}{T(j\omega)} = X(\omega)$$

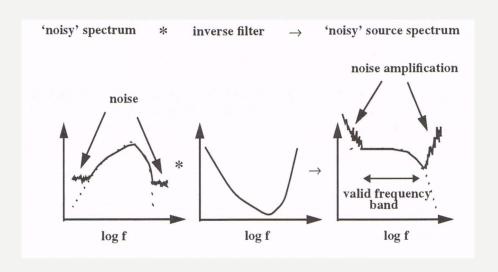




Inverse filter problems

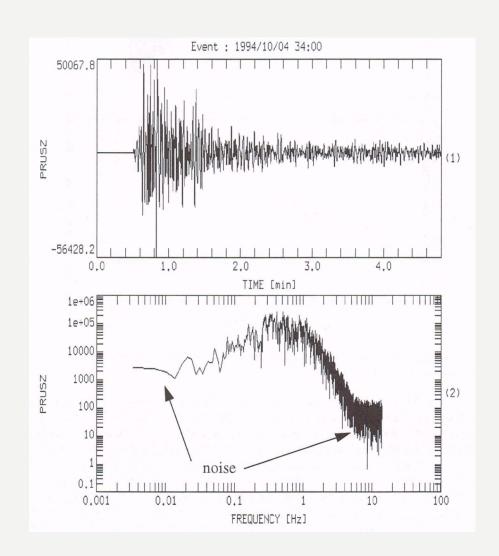


Noise in the data can get strongly amplified during the restitution.



Solution:

- → water-level method
- → apply bandpass afterwards





Simulation filter



- Simulation filters are used to modify a signal as if recorded under certain conditions
 - Seismogram recorded with a special instrument
 - A song played in a special surrounding (e.g. concert hall with special echoing)
 - Simulate site effects on the signal, e.g. influence of wind, overlapping second source, ...
- Simulation filters can be ANY filter (depending on what effect is wanted)

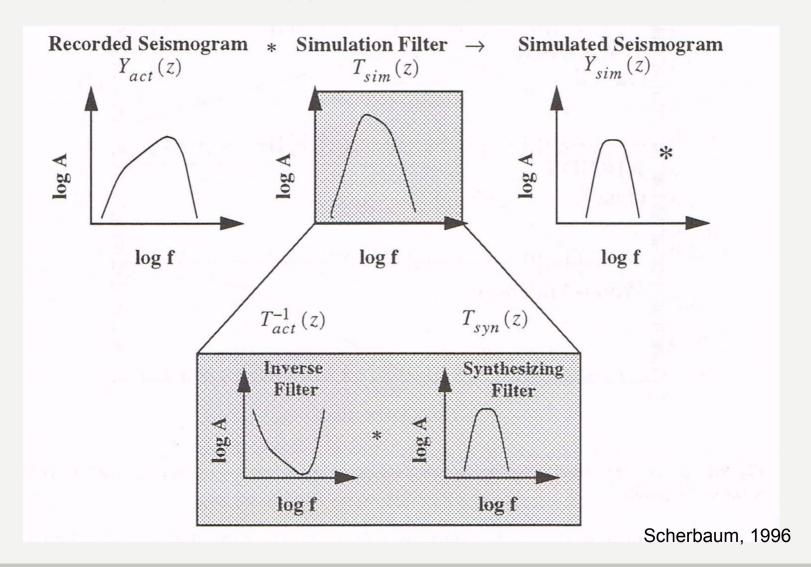
No single solution for set-up



Definition



Simulation is always a two step process, closely connected to inverse filters





Definition



Simulation is always a two step process, closely connected to inverse filters

$$Y_{sim}(z) = \frac{T_{syn}(z)}{T_{act}(z)} \cdot Y_{act}(z)$$

$$=T_{sim}(z)\cdot Y_{act}(z)$$

- Tact, Tsyn transfer function of actual and synthesized recording system, respectively
- Yact, Ysim z-transforms of recorded and simulated seismogram, respectively

Scherbaum, 1996



Necessities



To be able to obtain a high accuracy and stable simulation, the actual instrument used for the recording need to fulfil the following necessities:

Large bandwidth

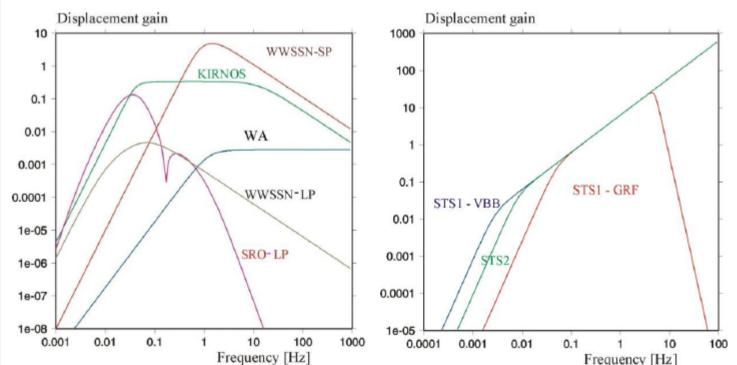
- Low instrumental self-noise
- Large dynamic range
- Low noise induced by variations of air pressure+ temperature

High resolution

Analytically exactly known transfer function



modern digital BB instruments



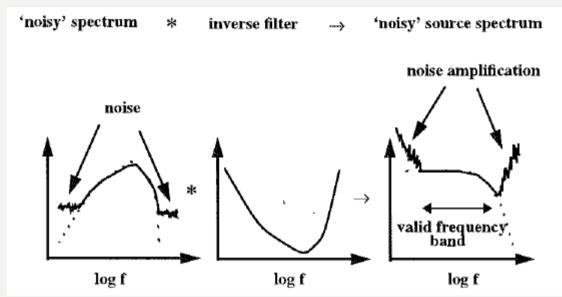
NMSOP 2013, chap. 11



Stability: 1st problem

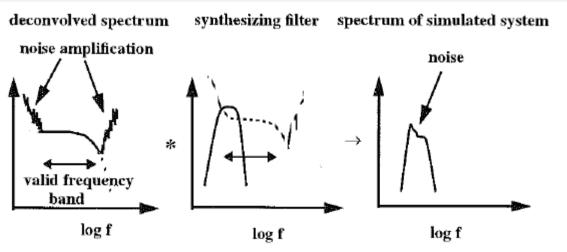


Noise



Possible solutions:

- bandpass filter final trace
- water-level during deconvolution



Scherbaum, 1996



Stability: 2nd problem



• Mathematical singularities in the transfer function at s = 0

$$T^{-1}(s) = \frac{s^2 + 2h\omega_0 s + w_0^2}{s^3}$$

Possible solution: regularization by subsequent highpass filtering

$$T^{-1}(s) \cdot T_{HP}(s) = \frac{s^2 + 2h\omega_0 s + w_0^2}{s^3} \cdot \frac{s^3}{(s+\epsilon)^3} = \frac{s^2 + 2h\omega_0 s + w_0^2}{(s+\epsilon)^3}$$

(Remember properties of linear systems ...)

Scherbaum, 1996

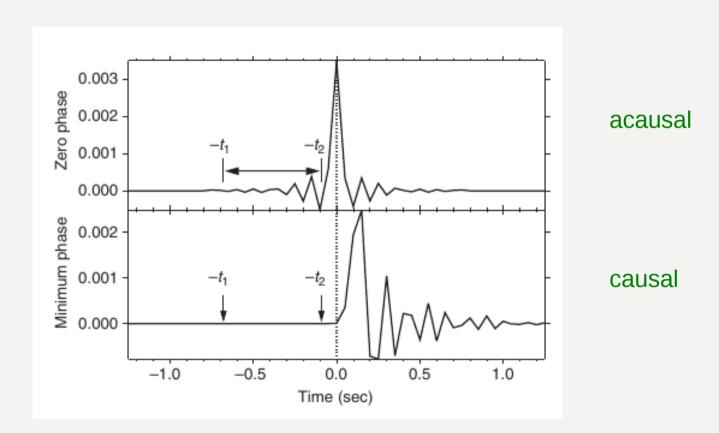


Stability: 3rd problem



Causality

(It basically has something to do with the relationship between the pole and zero position of the transfer function; see Scherbaum, 1996)

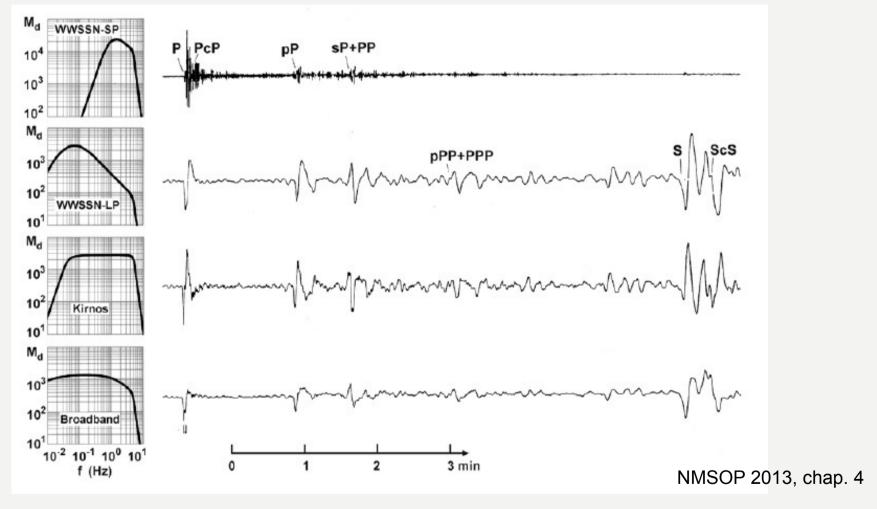


International Handbook of Earthquake & Engineering Seismology, Part 1, 2002



Example 1





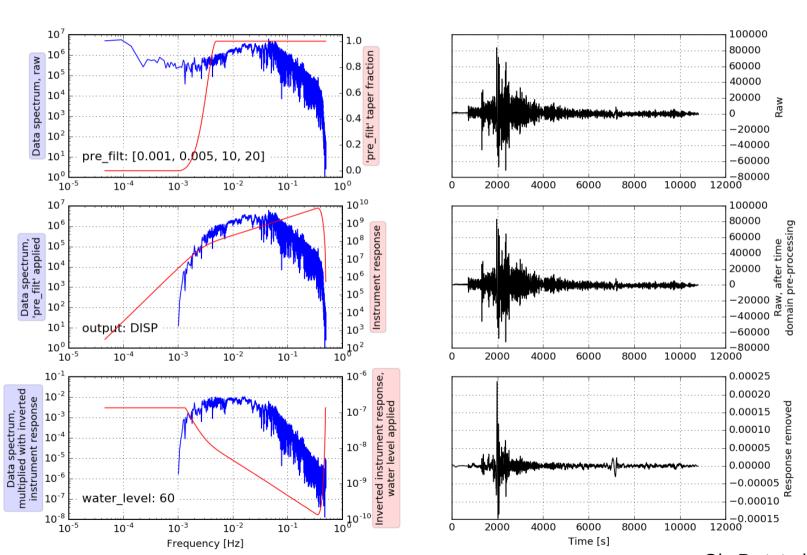
- Deep earthquake (h=570km; d=75°) at Gräfenberg Observatory
- Filtered according to response curves of some traditional standard characteristics
- Bottom trace: deconvolved seismogram (without instrument characteristic)



Example 2



IU.ULN.00.LH1 | 2015-07-18T02:27:33.069538Z - 2015-07-18T05:27:32.069538Z | 1.0 Hz, 10800 samples



ObsPy tutorial, no. 14