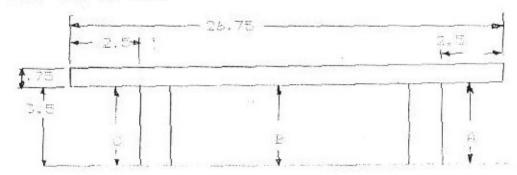
THERMAL/CREEP TEST

Performed: July 28 & 27, 1994 and August 1. 1994 Performed in Albuquerque, NM by C. Ford and G. Estepp Average local temperature during test equalled 97%F.

Test Setur Ti

Test object: .75 % 5.5 % Zs.75 piece of SBFRP produced plastic lumber. This test sample rad been produced from .25" grind post-consumer comingled material the last week of June '94.



Setur was placed on a flat section of driveway which was at all times in direct sunlight. Measurements were taken and recorded at one hour intervals beginning at 9:00 AM MT.

Raw Data	(inches) y		
	42	E	C
9:00 AM	5.37	3.65	3.31
10:00 AM	7.77	5.43	3,31
11:00 AM	5.57	3.63	3.31,
12:00 AM	표. 조건	5.63	3.31
1:00 FM	3.37	3.63	3,31
2:00 PM	3.37	3.43	3.31

Test repeated 7-29-94 from 9:00 AM to 12:00 AM with identical results.

Test Setup T2

Same as above but added a 5.0 pound stee) weight in the center. The dimensions of the steel weight are 1.0 \times 3.0 \times 6.0 inches. The same test object was used.

Raw Data (inches)

	A.	B	C
8:00 AM	3.37	0.56	3.37
9:00 AM	I. 17	T. 1 = 4:	3,37
10:00 AK	3.67	I.54	3.37 3.37
11:00 AM	3.37 3.37	3.5A 1.54	4. 44.

000319

3,54

3.37

1:00 FM

It appears that this sample exhibited very stable characteristics due to the application of radiated heat, even under small load conditions. More testing is required but this should satisfy a first glance inquiry.

5.37

31 MAY 1994

OUTGASSING TESTS FOR THE SOLVENT BASED PLASTICS RECYCLING **PROCESS**

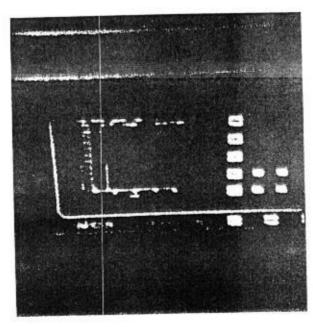
Performed by: John Cleveland, President Cleveland Enterprises, Inc. 4410 Hawkins NE, Suite C Albuquerque, NM 87109 (505) 345-7751

Testing performed for: Innovative Research Corporation PO Box 482 Peralta, NM 87042

Test Equipment: INFICON Quadex 200, quadrapole mass spectrometer and pumping system.

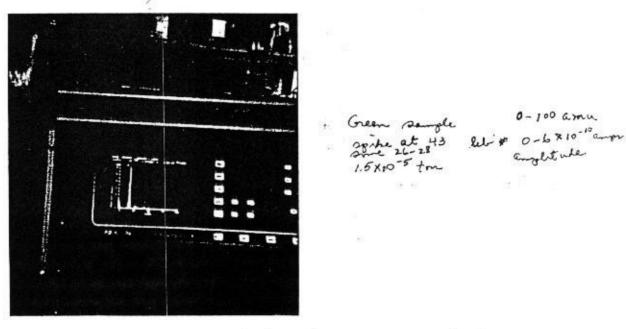
Testing Methods:

Test 1. Mass spectrometer was valved off and pumped down to 8.5 x 10E-9 torr. The system ran its self calibration and was detirmined to be working properly. The system was vented and a valved test fixture vacuum vessel was attached. The system was pumped down again, this time to 4.5 x 10E-7 torr, the valve was opened and a base line specrometer reading was obtained. The base line signal was photographed. The spectrometer was set to read from 0 to 100 atomic mass units (amu), element numbers, with a vertical scaling of 0 to 6 x 10E-10 amperes. The photo was fairly fuzzy but you will note that the 18 amu peak, water vapor is slightly saturated and off scale. The 17 amu peak is proportionally present. No other peaks are noticeable.



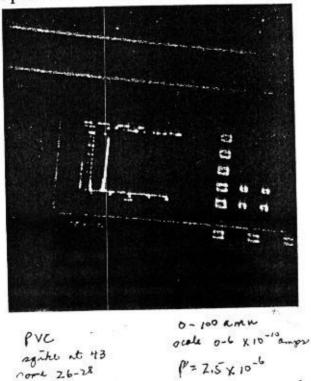
R. . l. . .

Test 2. The system was vented and the valved test fixture vacuum vessel was loaded with a .625 x 1.25 x 3.625 inch green colored sample from a 2 x 4 sample plastic lumber fabricated March 17th of this year. This sample contained an ABS-Polycarbonate blend, a blue polycarbonate, a red polycarbonate, an acetal, a styrene, a polyethylene, a glassfilled polycarbonate, an acrylic, an ABS, a PVC, a foamed polystyrene, 25% by volume of shredded paper and viewgraph film mix, two ounces of green coloring resin and solvent. This mixture was a total weight of 9 pounds with approximately equal amounts of each species by volume and a small amount of solvent. The system was pumped down again, this time to 1.5 x 10E-5 torr, the pressure was limited by the porosity of the material acting like a virtual leak. A spectrometer reading was obtained. The line signal was photographed. The spectrometer was set to read from 0 to 100 atomic mass units (amu), element numbers, with a vertical scaling of 0 to 6 x 10E-10 amperes. You will note that the 18 amu peak, water vapor is slightly saturated and off scale. The 17 amu peak is proportionally present. The 15, 28 and 43 peaks are noticeable. The 15 peak is slight but represents methane. The 28 peak is also slight and represents air (nitrogen). The 43 peak is the major peak related to the solvent used but at these levels are insignificant.



Test 3. The system was vented and the valved test fixture vacuum vessel was loaded with a .125 x .875 x 1.625 inch off white colored sample of PVC, typical of schedule 80 pipe. This sample was soaked in the desired solvent for five minutes prior to insertion. The system was pumped down again, this time to 2.5 x 10E-6 torr. A spectrometer reading

was obtained. The line signal was photographed. The spectrometer was set to read from 0 to 100 atomic mass units (amu), element numbers, with a vertical scaling of 0 to 6 x 10E-10 amperes. You will note that the 18 amu peak, water vapor is slightly saturated and off scale. The 17 amu peak is proportionally present. The 15, 26, 28 and 43 peaks are noticeable, the 15 peak is slight but still present and represents methane, possibly introduced unintentionally. The 26 peak is insignificant but noticeable and can be attributed to several elements such as complex hydrogen compounds or the accidental introduction of acetylene which is not really possible. The 28 peak is also slight and represents air (nitrogen). The 43 peak is the major peak related to the solvent used but at these levels are insignificant. No peaks representing hazardous compounds such as vinyl chloride which has a significant peak at 62 were noticed.



Test 4. Then a conglomerate of assorted post-consumer plastic waste soaked in solvent for approximately 20 minutes. This material was placed in the test chamber. The system was pumped down again, this time to 1.0 x 10E-4 torr, the pressure was high due to the high liquid content of the material introduced. A line spectrometer reading was obtained. The line signal was photographed. The spectrometer was set to read from 0 to 100 atomic mass units (amu), element numbers, with a vertical scaling of 0 to 6 x 10E-10 amperes. You will note that the 18 amu peak, water vapor is not saturated at this pressure level. The 17 amu peak is proportionally present. The 15, 26, 28 and 43 peaks are noticeable at higher levels due to the high concentration of solvent, air and water vapor present.



0-100 amu 0-6 ×10-10 onges agrille at 15,43 + 1420 20re 26-28 1×10-4 tm

CONCLUSIONS:

This testing proves without a doubt that no hazardous compounds are created by the reaction of the desired solvent and post-consumer plastic waste. There also appears to be no leaching of gases from fully cured products from this process.

ROCKY MOUNTAIN TESTING

ALBUQUERQUE NM 87107 6444 EDITH BLVD

TENSILE AND BENDING TESTS

PROJECT PALLET MATERIAL TESTS

TEST DATE 5/4/94

TESTED BY Len Leonard

LAB No 10748

TESTED IN ACCORDANCE WITHLUMBER TEST CUSTOMER INOVATIVE RESEARCH CORPORATION

TYPE OF SAMPLE

SAMPLE	WIDTH-IN	THICKIN	AREA	LOAD-LBS	STRENGTH-PSI	FAILURE	BENDING
WOOD	3½	3/4	N/A	2,704	N/A	BENDING	
LIGHT	3½	3/4	N/A	981	N/A	BENDING	
DARK	3½	3/4	N/A	186	N/A	BENDING	
					,		
WOOD	3½	13	N/A	12,000	N/A	COMPRESSION	
LIGHT	3½	13	N/A	32,000	N/A	COMPRESSION	
			ti				
WOOD	33	115	N/A	7,350	N/A	STRINGER	
LIGHT	3½	13	N/A	1,378	N/A	STRINGER	
Trepra							

PLASTIC HAD 4" GRAIN SIZE AND NO FIBER. COMMENTS:

000325



SINTECH A Division of MTS Systems Corporation

Fax #

July 8, 1993

70

From:

Subject:

Gary Estepp

Douglas Albert Brick Test Results

Dear Gary,

Sorry that it has taken me so long to get back to you with this data. I had the brick machine into eight pieces last week and had the testing completed

The following pages should include all of the information that you requested.

corrections, and flex tests. The yields were measured as "zero slope" yields Results are for compression tests, with and without machine compliance and not as offset yields. I was unsure of the procedure that you wanted to

Also, dimensions are noted on the reports. Yield was used in compression as there is not a distinctive point of failure.

other calculations that you may desire. I hope that these results are to your satisfaction. I have the results on disks and would be more than happy to include any

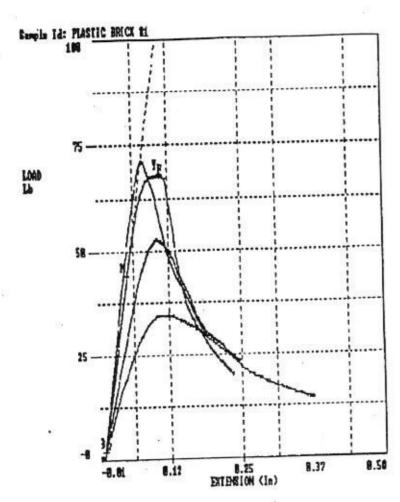
Best Regards

Douglas G. Albert

adlastallo

000326

Page 1 of 13



Detailed Report

Report Header goes here second line third line last line

ethod: 3 POINT FLEX ASTM D-790 BRICK

Sample ID> PLASTIC BRICK

Test Input(s):

Test Date: Jul 08, 1993 Operator ID: SINTECH

wi	dth (b) In	Depth (d)	Length (l)	Peak Load Lb	Peak Stress PSI	rield Load Lb	Yield Stress PSI	Elong @ Yield In	Xstrain a Yield	Modulus PSI
1 2 3 4	1.168 1.169 1.163 1.169	0.945 0.968 0.953 0.950	7.000 7.000 7.000 7.000	68.2 34.8 52.7 71.3	589 286 449 608	68.2 34.8 52.7 71.3	588.7 285.7 449.3 608.0	0.1065 0.1195 0.1010 0.0753	1.6773 1.9274 1.6048 1.1917	53188.86 24770.87 36657.74 60872.11
Heen Hin Hax StDV XCoV Hedn X Ref	1.167 1.163 1.169 0.003 0.246	0.945 0.968 0.010 1.038	7.000 7.000 0.000 0.000	56.8 34.8 71.3 16.8 29.5 60.5	483 286 608 149 31	34.8 71.3 16.8 29.5	149.3 30.9 519.0	0.1195 0.0186 18.4502 0.1038	1.9274 0.3055 19.0876 1.6410	43872.40 24770.87 60872.11 16255.32 37.05 44923.30
Cal	culat	ion Inp	!		orop op Elong		6.00 10 0.001 0.00	In % In Lb		

Min Slope Load

Max Slope Load

%Strain Point1

Initial Speed % Strain Limit

Load Limit HI

Brk Sensitivity

Ext Limit HI

2.00

0.0625

100.0

2000

20.0

75

10000.17

Lb

8

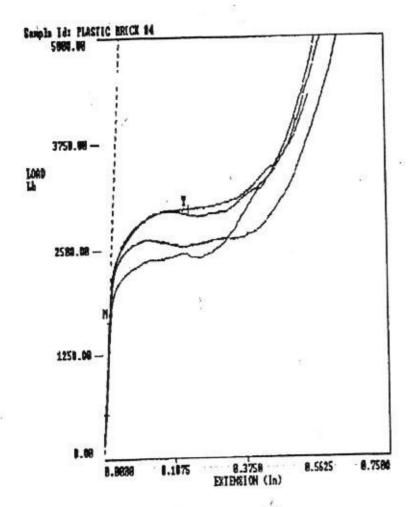
In/Min

Lb

In

\$

widt	h (b) In	Depth (d)		Peak Load Lb	Peak Stress PSI	Yield Load Lb	Yield Stress PSI	Elong 2 Yield In	XStrain a Yield X	Modulus PSI
			ample Mo						E	
otal	Num	ber of	Sample	3: 1						
	27 20020		7 000	56.8	483	56.8	482.9	0.1006	1.6003	43872.40
esn	1.167	0.95				56.8	482.9	0.1006	1.6003	43872.40
in	1.167					56.8	482.9	0.1006	1.6003	43872.40
ax	1.167				1 10 10 10 10 10 10 10 10 10 10 10 10 10	1000	2002	0.0000	0.0000	0.00
tDV	0,000			2	: W 195			0.0000	0.0000	0.00
Cov	0.000	0.00	0.000	0.0	Tronsparent Sil	******	*******	******	*****	*****
Ref										
			all spec							
otal	L Nu	mber o	f Specim	en: 4						
								0.1006	1,6003	
			, 700	n 56	R 483	56.8	482.5	0.1000		
	1.167				2.47				1.1917	24770.8
iin.	1.163	0.9	7.00	0 34.	8 / 286	34.8	285.	0.0753	1.1917 1.9274	24770.8 60872.1
rin .	1.163	0.9	7.00 58 7.00	0 34. 0 71.	8 286 3 608	34.8 3 71.3	285.7 5 608.1	0.0753	1.1917 1.9274 6 0.3055	24770.83 60872.13 16255.33
Mean Min Hax StDV	1.163	0.94 9 0.94 5 0.0	7.00 58 7.00 10 0.00	0 34. 0 71. 0 16.	8 286 3 608 8 145	34.8 3 71.3 9 16.8	285.3 608.1	7 0.0753 0 0.1199 3 0.0186	1.1917 1.9274 6 0.3055	43872.40 24770.87 60872.11 16255.36 37.00



Detailed Report

Report Header goes here second line third line last line

Method: BRICK TEST Sample ID> PLASTIC BRICK Test Date: Jul 07, 1993 Operator ID: SINTECH

Sample Information:

User In	out 1	User	Default	1
User In		User	Default	2
User In	put 3	User	Default	3
User In	put 4	User	Default	5
User In	nut 5	User	Default	6
User In	put 6		Default	
User In	put 7		Default	
User In	put R	User	Default	8
User In	put 0		Default	
User In	put 9	licer	Default	10
User In	put 10	USEL	DOLUME	-

	Width	Length	Height	Yield Load	Yield Stress	Elong & Yield	%Strain 8 Yield	Energy @ Yield	Modulus
	In	In	In	Lb	PSI	In	%	In-Lb	PS1
1 2 3 4	1.923	1.983	1.170	2955.8	775.1	0.1679	14.3483	409.3	22827.75
	1.970	1.965	1.184	2614.4	675.4	0.1316	11.1161	290.1	25405.55
	1.980	1.913	1.180	2439.8	644.1	0.2223	18.8414	480.5	25152.44
	1.989	1.910	1.180	2977.0	783.6	0.2321	19,6734	607.1	28229.15
Mean Min Max StDv XCov Medn X Ref	1.965 1.923 1.989 0.029 1.495 1.975	1.943 1.910 1.983 0.037 1.897 1.939	1.178 1.170 1.184 0.006 0.507 1.180	2746.8 2439.8 2977.0 263.6 9.6 2785.1	719.6 644.1 783.6 70.3 9.8 725.3	0.1885 0.1316 0.2321 0.0473 25.0916 0.1951		446.7 290.1 607.1 132.7 29.7 444.9	25403.72 22827.75 28229.15 2212.22 8.71 25279.00

Calculation Input(s):

Gage Length	1.18	In
Brk % Drop	10	*
Brk Drop Elong	0.001	In
Min Slope Load	0.00	Lb
Max Slope Load	10000.17	Lb
%Strain Point1	2.00	8

000331

Test Input(s):

rest Input(s):

Secondary Speed	0.05	In/Min
% Strain Limit	5.0	*
Deformation Lim	200.0	*
Load Limit HI	30001	Lb
Load Limit LO	-30001	Lb
Ext Limit HI	20.0	In
Ext Limit LO	-20.0	In
Brk Sensitivity	75	*

	Width	Length		Yield Load	Yield Stress PSI	Elong @ Yield In	Xstrain a Yield	Energy a Yield In-Lb	Modulus PSI
	tn .	In	In	Lb					
		of Sam						*	
an n x Dv ov Ref	1.965 1.965 1.965 0.000 0.000	1.943 1.943 1.943 0.000 0.000	1.178 1.178 1.178 0.000 0.000	2746.8 2746.8 2746.8 0.0 0.0	719.6 719.6 719.6 0.0 0.0	0.1885 0.1885 0.1885 0.0000 0.0000	15.9948 15.9948 15.9948 0.0000 0.0000	446.7 446.7 0.0 0.0	25403.72 25403.72 25403.72 0.00 0.00
tat		of all							
tat		of all			719.6	0.1885	15.9948	446.7	25403.77

Detailed Report

Report Header goes here second line third line last line

Method: BRICK TEST (no compliance) Sample ID> PLASTIC BRICK

Test Date: Jul 07, 1993 Operator ID: SINTECH

Sample Information:

	T	4	Heer	Default	1
User	Input	1	77442	Default	2
User	Input	2	User	Delauic	~
Heer	Input	3	User	Default	3
Heer	Input	. 4	User	Default	5
User	Input	5	User	Default	6
Heer	Input	6	User	Default	6
User	Imput	7		Default	
User	Input	6	liger	Default	8
User	Input	8	User	Default	9
User	Input	9	User	Deraule	10
User	Input	10	User	Default	10

		120							
	width	Length	Height	Yfeld Load	Yield Stress	Elong @ Yield	%Strain a Yield	Energy a Yield	Modulus
	In	In	In	Lb	PSI	In	%	In-Lb	PSI
1 2 3 4	1.923	1.983	1.17	2955.8	775.1	0.1712	14.6295	414.2	21092.62
	1.970	1.965	1.18	2614.4	675.4	0.1345	11.3629	293.9	23249.68
	1.980	1.913	1.18	2439.8	644.1	0.2251	19.0725	483.8	23071.90
	1.989	1.910	1.18	2977.0	783.6	0.2355	19.9554	612.1	25626.66
Mean Min Max StDv XCov Medn X Ref	1.965 1.923 1.989 0.029 1.495 1.975	1.943 1.910 1.983 0.037 1.897 1.939	1.18 1.17 1.18 0.01 0.51 1.18	2746.8 2439.8 2977.0 263.6 9.6 2785.1	719.6 644.1 783.6 70.3 9.8 725.3		24.6605 16.8510	451.0 293.9 612.1 133.0 29.5 449.0	23260.22 21092.62 25626.66 1855.99 7.98 23160.79

Calculation Input(s):

Gage Length	1.18	In
Brk % Drop Brk Drop Elong Min Slope Load Max Slope Load %Strain Point1	0.001 0.00 10000.17 2.00	In Lb Lb

Test Input(s):

0.05

est Input(s):

% Strain Limit	5.0	*	
Deformation Lim	200.0	*	
Load Limit HI	30001	Lb	
Load Limit LO	-30001	Lb	
Ext Limit HI	20.0	In	
Ext Limit LO	-20.0	In	
Brk Sensitivity	75	*	

	Width In	Length In	Height In	Yield Load Lb	Yield Stress PSI	Elong a Yield In	XStrain & Yield X	Energy a Yield In-Lb	Modulus PS1
	·		•••••		***************************************	••••••			
tat:	istics	of Samp	ole Mea	ns.				ě.	
ota	l Numbe	er of Sa	imples:	1					
		1.943	1.18	2746.8	719.6	0.1916	16,2551	451.0	23260.2
ean	1.965	1.943	1.18	2746.8	719.6	0.1916	16.2551	451.0	23260.2
in	1.965	1.943	1.18	2746.8	719.6	0.1916	16.2551	451.0	23260.2
ax	0.000	0.000	0.00	0.0	0.0	0.0000	0.0000	0.0	0.0
tDv	0,000	0.000	0.00	0.0	0.0	0.0000	0.0000	0.0	0.0
Cov Ref	0.000	0.000	0.00	*****	******	*******	***	******	*****
		of all		nen.	•••••		***************************************	•••••	
	10 W 40 PM			27/4 8	719.6	0.1916	16.2551	451.0	23260.2
lean	1.965	1.943	1.18	2746.8 2439.8	644.1	0.1345	11.3629	293.9	21092.6
lin	1.923	1.910	1.18	2977.0	783.6	0.2355	19.9554	612.1	25626.6
lax	1.989	1.983	0.01	263.6	70.3	0.0473	4.0086	133.0	1855.9
tDv	0.029	0.037	0.51	9.6	9.8	24.7036	24.6605	29.5	7.9
Cov Ref	1.495	1.897	0.51	*****	******	*****	*****	*****	*****