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# Electronics for Information Technology

(Điện tử cho Công nghệ Thông tin)

IT3420E

**Đỗ Công Thuần**

Department of Computer Engineering

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# General Information

- Course: **Electronics for Information Technology**
- ID Number: IT3420
- Credits: 2 (2-1-0-4)
- Lecture/Exercise: 32/16 hours (48 hours, 16 weeks)
- Evaluation:
  - Midterm examination and weekly assignment: **50%**
  - Final examination: **50%**
- Learning Materials:
  - Lecture slides
  - Textbooks
    - *Introductory Circuit Analysis* (2015), 10<sup>th</sup> – 13<sup>th</sup> ed., Robert L. Boylestad
    - *Electronic Device and Circuit Theory* (2013), 11<sup>th</sup> ed., Robert L. Boylestad, Louis Nashelsky
    - *Microelectronics Circuit Analysis and Design* (2006), 4<sup>th</sup> ed., Donald A. Neamen
    - *Digital Electronics: Principles, Devices and Applications* (2007), Anil K. Maini

# Contact Your Instructor

- You can reach me through office in **Room 802, B1 Building**, HUST.
  - You should make an appointment by email before coming.
  - If you have urgent things, just come and meet me!
- You can also reach me at the following **email** any time. This is the best way to reach me!
  - [thuandc@soict.hust.edu.vn](mailto:thuandc@soict.hust.edu.vn)

# Course Contents

- The Concepts of Electronics for IT
- **Chapter 1: Passive Electronic Components and Applications**
- **Chapter 2: Semiconductor Components and Applications**
- **Chapter 3: Operational Amplifiers**
- **Chapter 4: Fundamentals of Digital Circuits**
- **Chapter 5: Logic Gates**
- **Chapter 6: Combinational Logic**
- **Chapter 7: Sequential Logic**

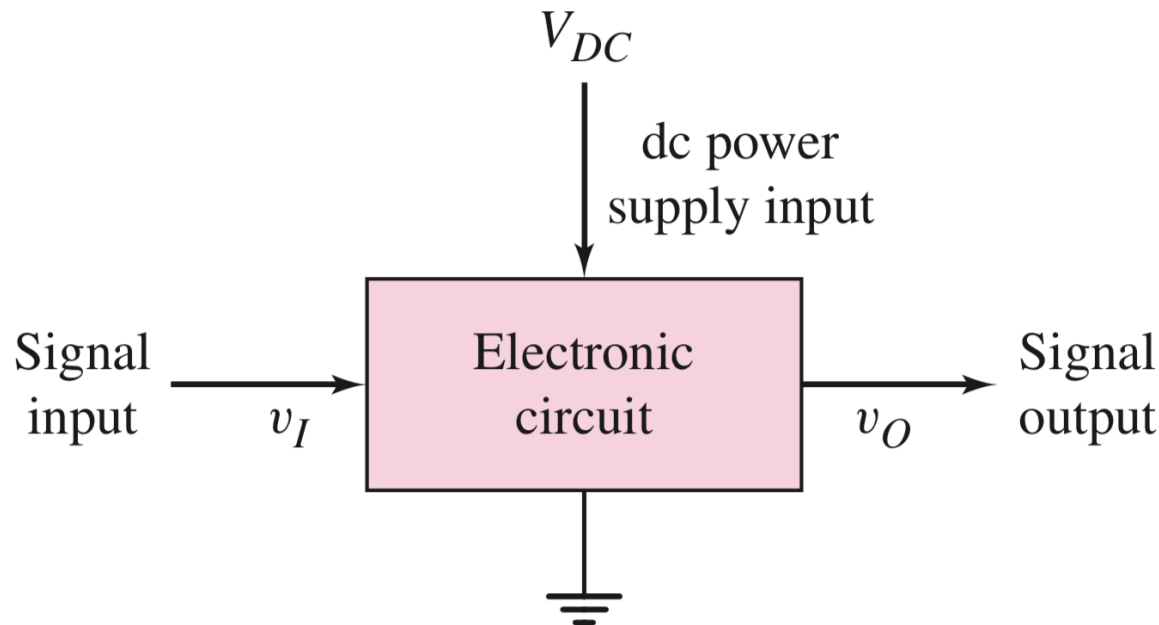
# Chapter 2:

# **Semiconductor Components and Applications**

- Semiconductor Materials
- Diodes and Applications
- Transistors and Applications

# Analog Circuits

- A signal contains some type of information.
  - Ex: a sound wave produced by a speaking human
- Electronic circuits that process analog signals are called **analog circuits**.
  - Ex: a linear amplifier



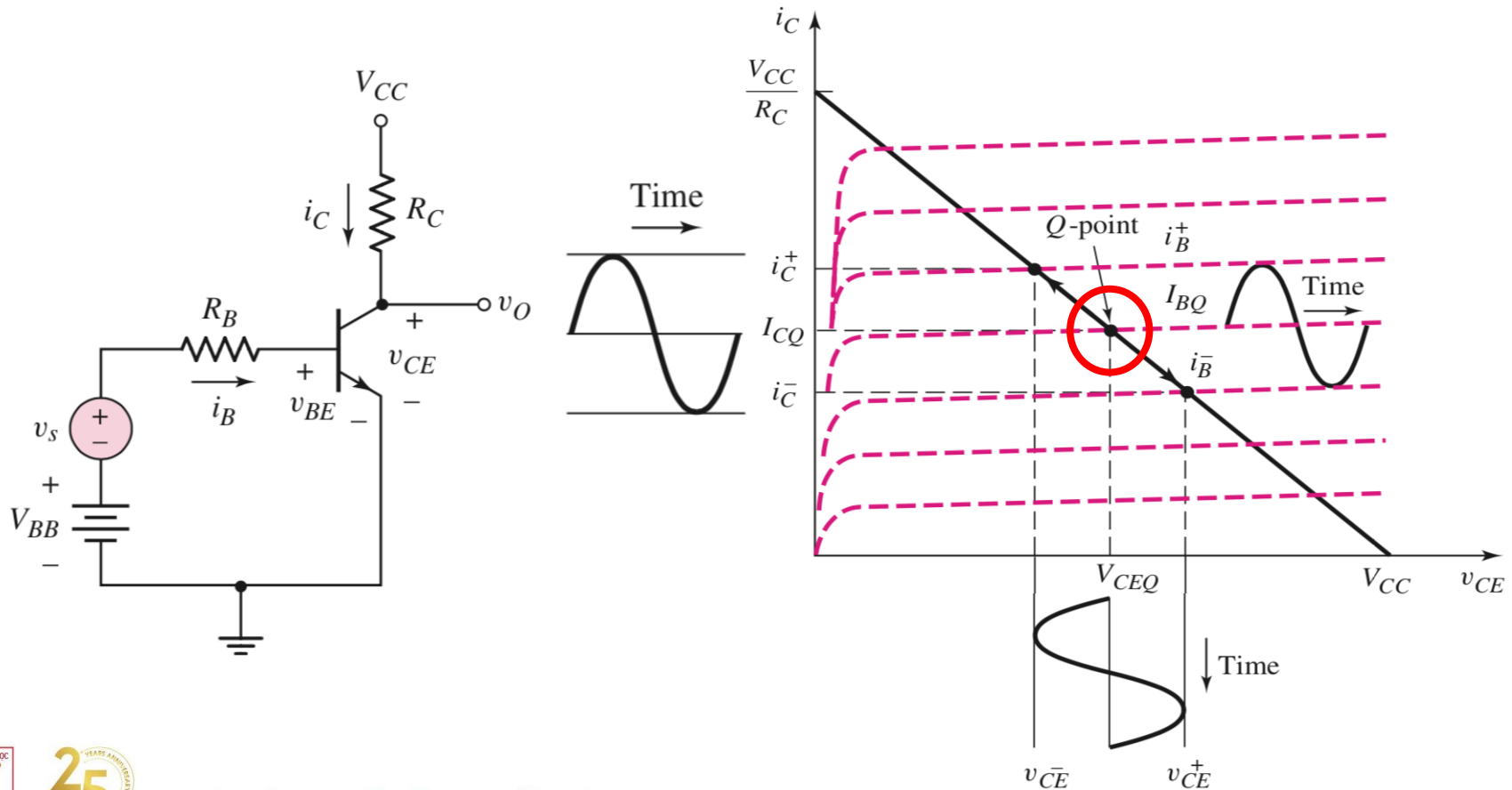
# Analysis Method

- **Using a small-signal analysis → a linear model**
  - Doing the **DC analysis** to establish the **Q-point** of the transistor in the linear amplifier
  - Doing the **AC analysis** to determine the **relationships** between the **time-varying output** and **input** signals
  - Applying the superposition principle (thanks to the linear model)
    - “*The response of a linear circuit excited by multiple independent input signals is the **sum of the responses** of the circuit to each of the input signals alone.*”

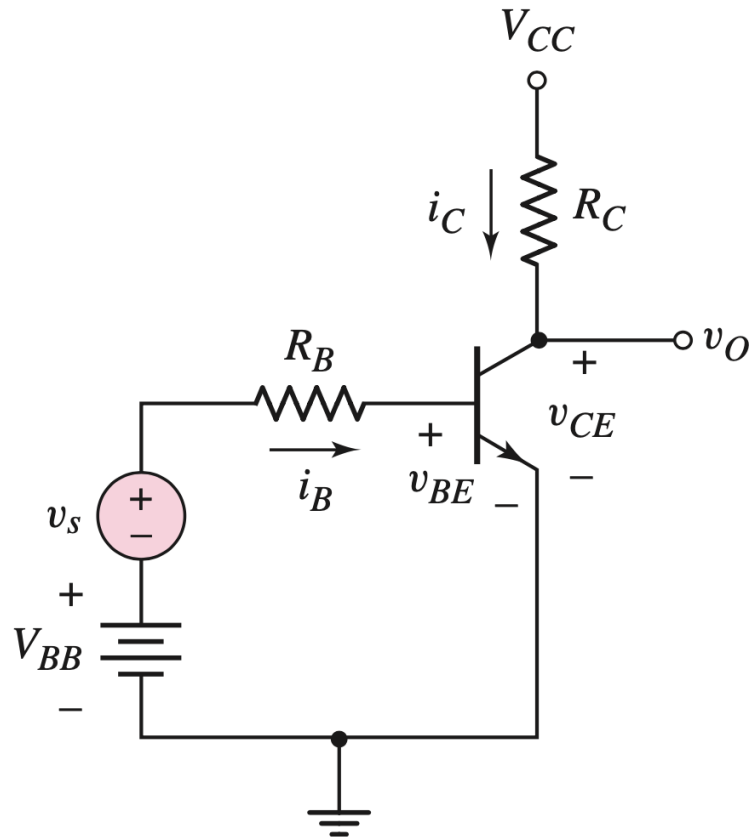


# Graphical Analysis

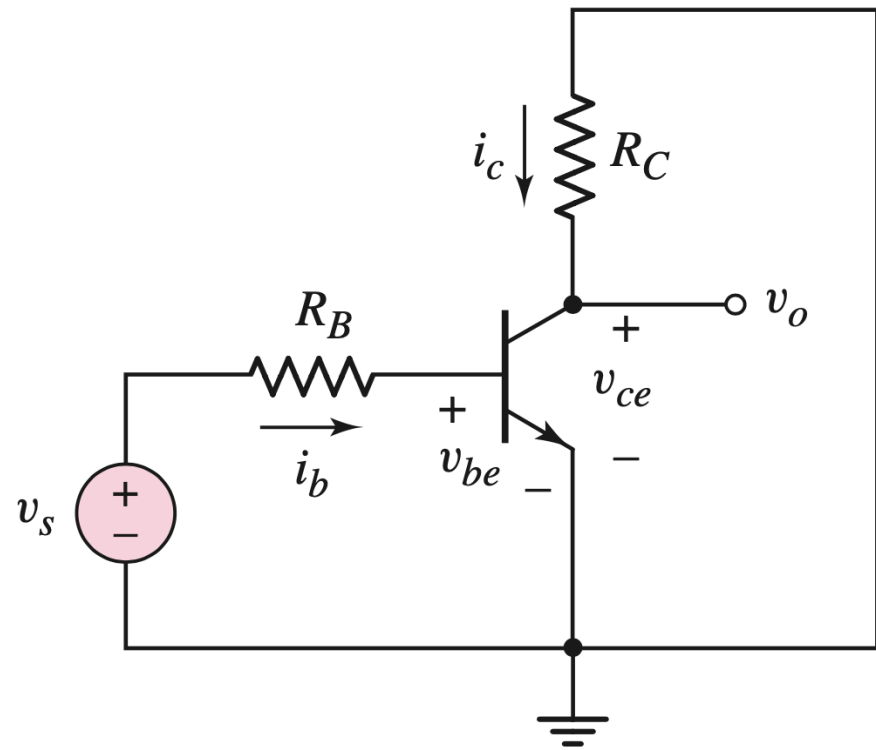
- **DC Analysis:** to find the desired Q-point
- **AC Analysis:** to determine the relationships between the time-varying output and input signals



# AC Equivalent Circuit

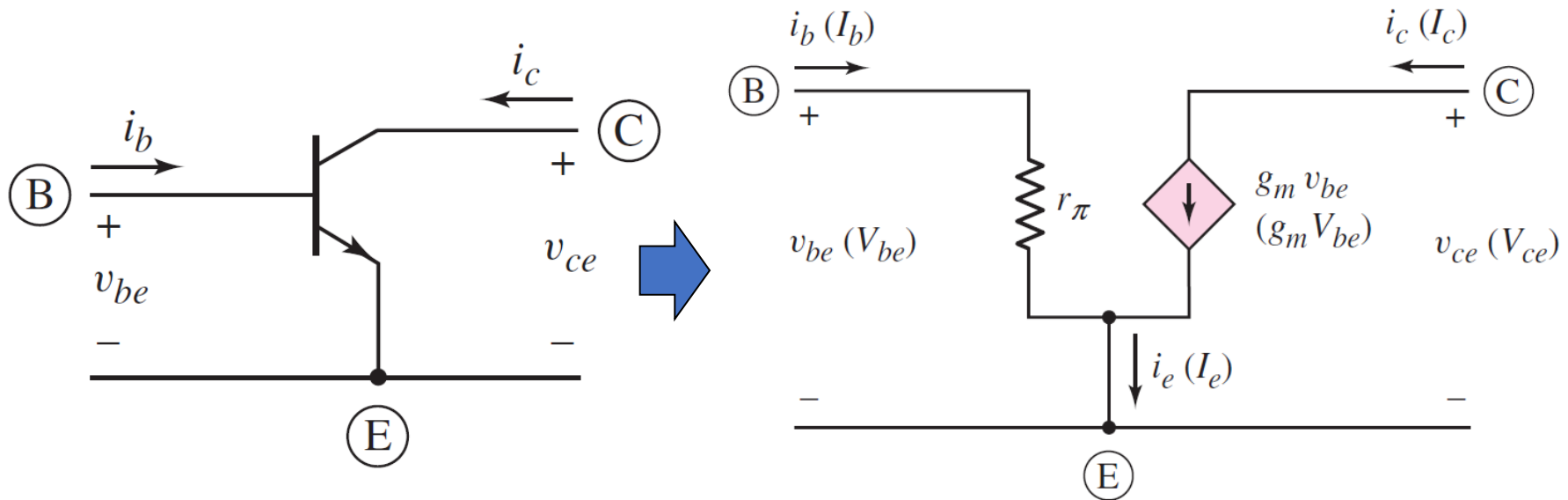


Common-Emitter Circuit



AC equivalent circuit

# Small-Signal Hybrid- $\pi$ Equivalent Circuit



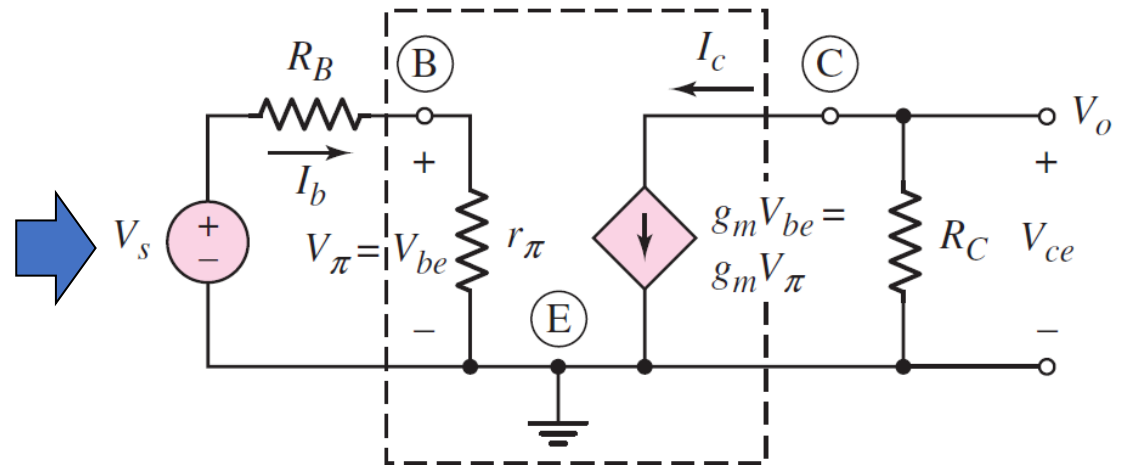
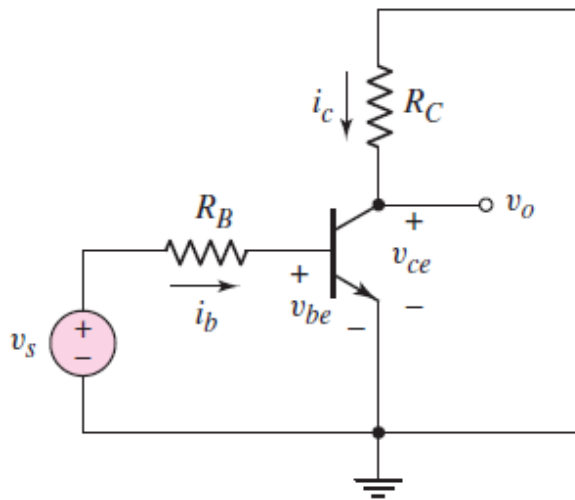
Can treat the bipolar transistor as a two-port network

Hybrid- $\pi$  equivalent circuit with small time-varying signals

$$r_{\pi} = \frac{V_T}{I_{BQ}} \quad \text{Diffusion resistance or B-E input resistance}$$

$$g_m = \frac{I_{CQ}}{V_T} \quad \text{Transconductance}$$

# Hybrid- $\pi$ Equivalent Circuit



**Output signal  
voltage**

$$V_o = V_{ce} = -(g_m V_{\pi}) R_C$$

**Small-signal  
B-E voltage**

$$V_{\pi} = \left( \frac{r_{\pi}}{r_{\pi} + R_B} \right) \cdot V_s$$

**Small-signal  
voltage gain**

$$A_v = \frac{V_o}{V_s} = -(g_m R_C) \cdot \left( \frac{r_{\pi}}{r_{\pi} + R_B} \right)$$

## Example 2.13

- Calculate the small-signal voltage gain.
- Assume:

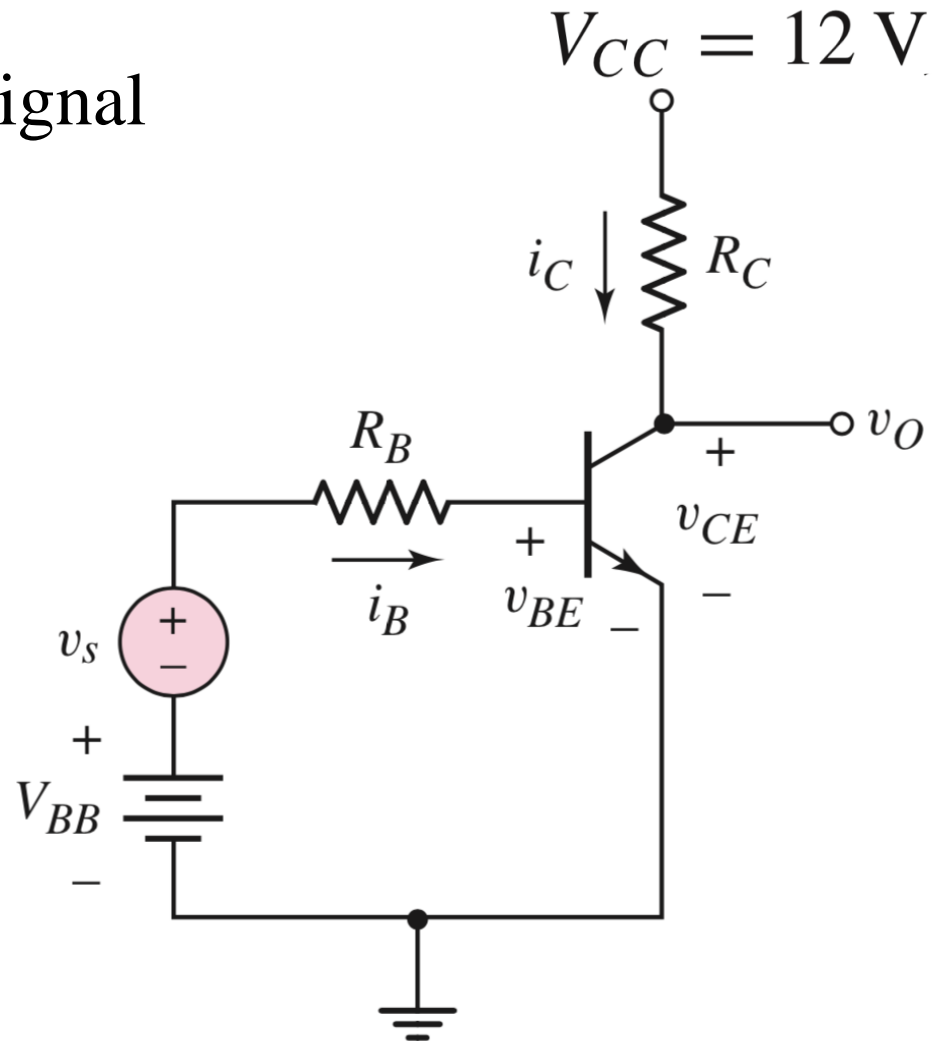
$$\beta = 100$$

$$V_{BE} = 0.7 \text{ V}$$

$$R_C = 6 \text{ k}\Omega$$

$$R_B = 50 \text{ k}\Omega$$

$$V_{BB} = 1.2 \text{ V}$$



# Example 2.13: DC Analysis

- DC equivalent circuit:

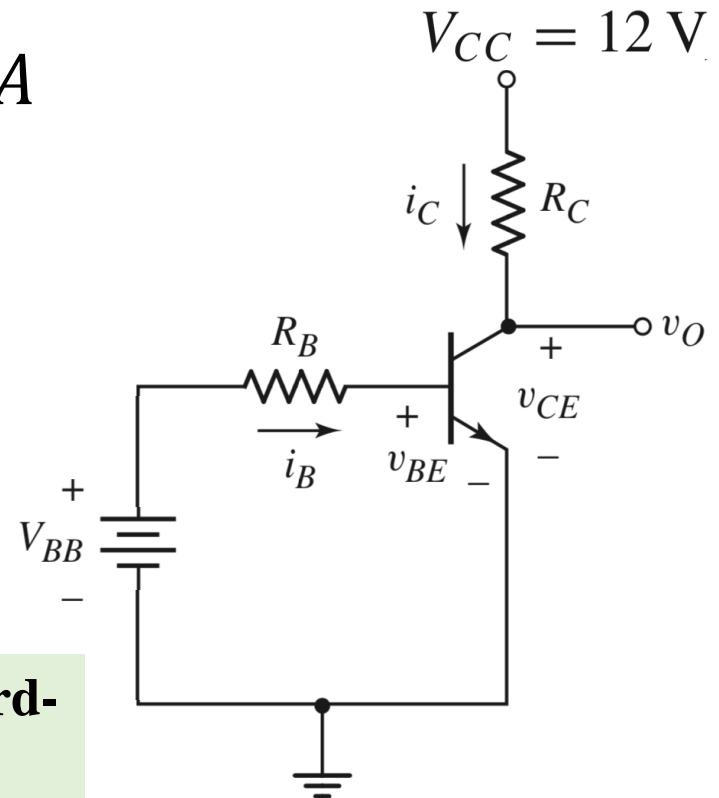
$$I_{BQ} = \frac{V_{BB} - V_{BE}(on)}{R_B} = \frac{1.2 - 0.7}{50} = 10 \mu A$$

$$I_{CQ} = \beta I_B = 100 * 0.01 = 1 mA$$

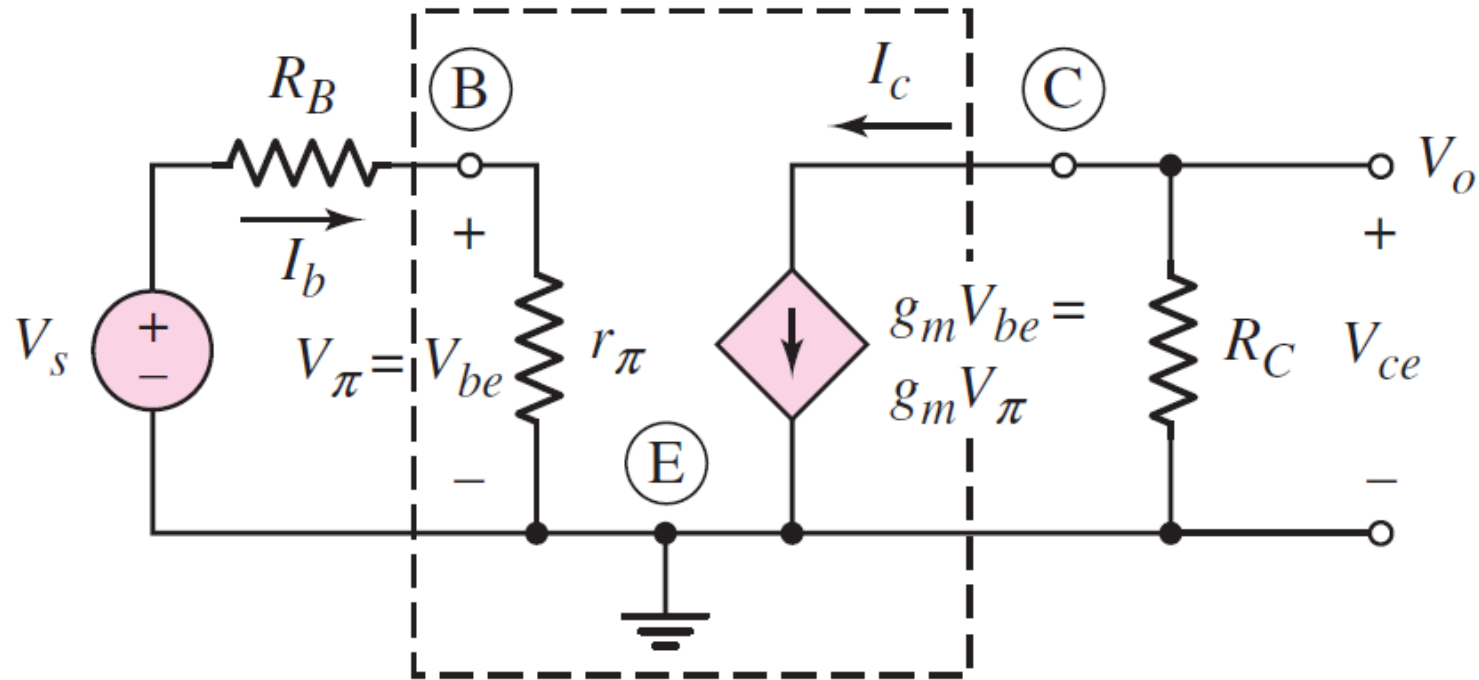
$$\begin{aligned} V_{CEQ} &= V_{CC} - I_C R_C \\ &= 12 - 1 * 6 = 6V \end{aligned}$$

➔ 
$$\begin{cases} I_{BQ} = 10 \mu A \\ I_{CQ} = 1 mA \\ V_{CEQ} = 6V \end{cases}$$

➔ The transistor is biased in the forward-active mode



## Example 2.13: Hybrid- $\pi$ Equivalent Circuit



**Small-signal  
voltage gain**

$$A_v = \frac{V_o}{V_s} = -(g_m R_C) \cdot \left( \frac{r_\pi}{r_\pi + R_B} \right)$$

# Example 2.13: AC Analysis

- The small-signal hybrid- $\pi$  parameters are:

$$r_{\pi} = \frac{\beta V_T}{I_{CQ}} = \frac{(100)(0.026)}{1} = 2.6 \text{ k}\Omega$$

$$g_m = \frac{I_{CQ}}{V_T} = \frac{1}{0.026} = 38.5 \text{ mA/V}$$

$$\begin{aligned} A_v = \frac{V_o}{V_s} &= -(g_m R_C) \cdot \left( \frac{r_{\pi}}{r_{\pi} + R_B} \right) \\ &= -(38.5)(6) \left( \frac{2.6}{2.6 + 50} \right) \\ &= -11.4 \end{aligned}$$



## Example 2.13: Sinusoidal Input Voltage

- Considering a specific sinusoidal input voltage:

$$v_s = 0.25 \sin \omega t \text{ V}$$

- The sinusoidal base current is given by:

$$i_b = \frac{v_s}{R_B + r_\pi} = \frac{0.25 \sin \omega t}{50 + 2.6} \rightarrow 4.75 \sin \omega t \text{ } \mu\text{A}$$

- The sinusoidal base current is given by:

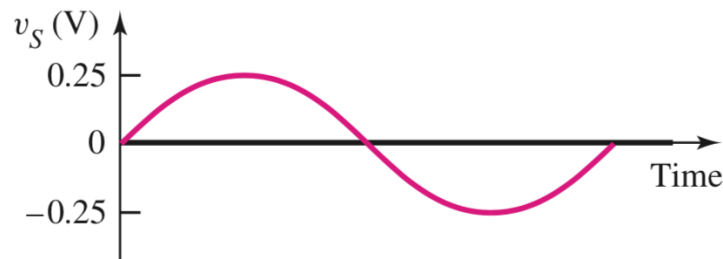
$$i_c = \beta i_b = (100)(4.75 \sin \omega t) \rightarrow 0.475 \sin \omega t \text{ mA}$$

- The sinusoidal C-E voltage is:

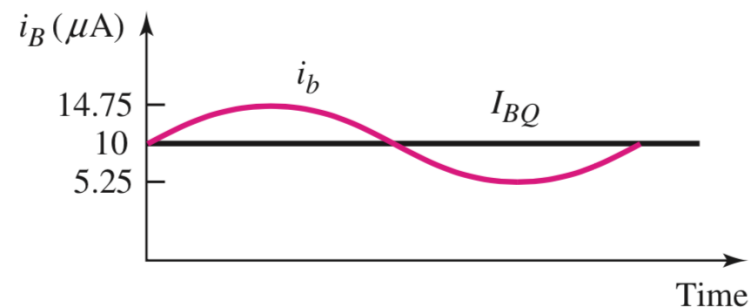
$$v_{ce} = -i_c R_C = -(0.475)(6) \sin \omega t = -2.85 \sin \omega t \text{ V}$$

# Example 2.13: Sinusoidal Input Voltage

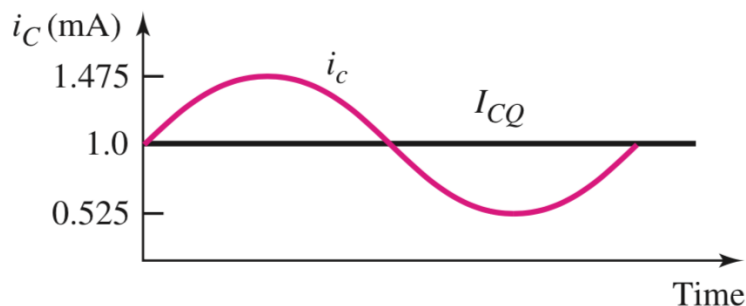
- The DC and AC signals in the common-emitter circuit:



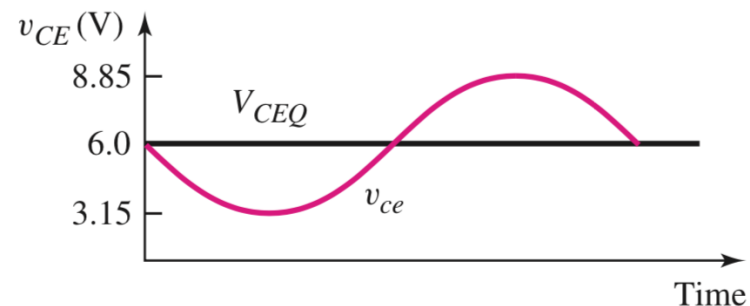
(a)



(b)



(c)






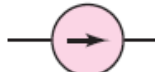



(d)

# Problem-Solving Technique: AC Analysis

- **Step 1:** Analyze the circuit with **only the dc sources** present → **Q-point**. The transistor must be biased in the **forward-active** region to produce a linear amplifier.
- **Step 2:** Replace each element in the circuit with its **small-signal** model. Apply the **small-signal hybrid- $\pi$**  model to the transistor.
- **Step 3:** Analyze the small-signal equivalent circuit, setting the **dc source components equal to zero**, to produce the response of the circuit to the time-varying input signals only.
- **Step 4:** Apply the **principle of superposition**.

# Transformation of Elements in DC and Small-Signal Analysis

| Element                    | $I$ - $V$ relationship       | DC model  | AC model   |
|----------------------------|------------------------------|---|--|
| Resistor                   | $I_R = \frac{V}{R}$          | $R$   | $R$  |
| Capacitor                  | $I_C = sCV$                  | Open<br>     | $C$  |
| Inductor                   | $I_L = \frac{V}{sL}$         | Short<br>    | $L$  |
| Diode                      | $I_D = I_S(e^{v_D/V_T} - 1)$ | $+V_\gamma - r_f$   | $r_d = V_T/I_D$<br> |
| Independent voltage source | $V_S = \text{constant}$      | $+V_S$<br> | Short<br>         |
| Independent current source | $I_S = \text{constant}$      | $I_S$<br>  | Open<br>          |

# Superposition Principle

- The time-varying signals are superimposed on dc values:

$$i_B = I_{BQ} + i_b$$

$$i_C = I_{CQ} + i_c$$

$$v_{CE} = V_{CEQ} + v_{ce}$$

$$v_{BE} = V_{BEQ} + v_{be}$$

| Variable      | Meaning                    |
|---------------|----------------------------|
| $i_B, v_{BE}$ | Total instantaneous values |
| $I_B, V_{BE}$ | DC values                  |
| $i_b, v_{be}$ | Instantaneous ac values    |
| $I_b, V_{be}$ | Phasor values              |

# Example 2.13: Superposition Principle

- The total instantaneous base current is given by:

$$\begin{aligned}i_B &= I_{BQ} + i_b \\&= 10 + 4.75\sin\omega t \mu A\end{aligned}$$

- The total instantaneous collector current is given by:

$$\begin{aligned}i_C &= I_{CQ} + i_c \\&= 1 + 0.475\sin\omega t mA\end{aligned}$$

- The total instantaneous C-E voltage is given by:

$$\begin{aligned}v_{CE} &= V_{CEQ} + v_{ce} \\&= 6 - 2.85\sin\omega t V\end{aligned}$$

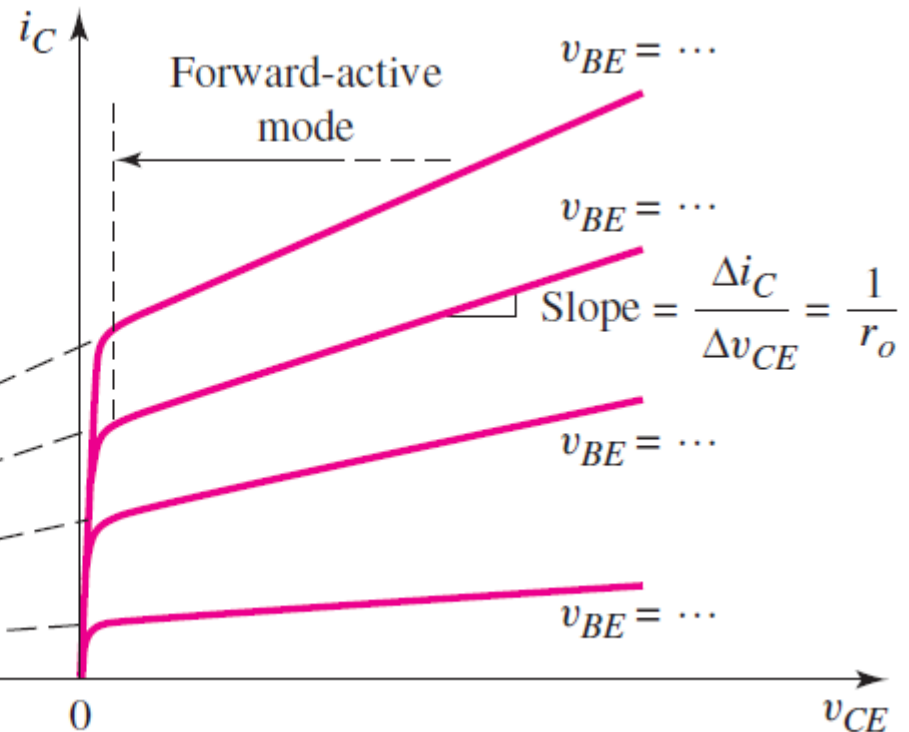
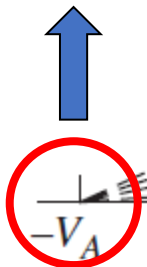
# Hybrid- $\pi$ Equivalent Circuit, Including the Early Effect

- When the curves are extrapolated to zero current, they meet at a point on the negative voltage axis, at  $v_{CE} = -V_A$ .

Output resistance

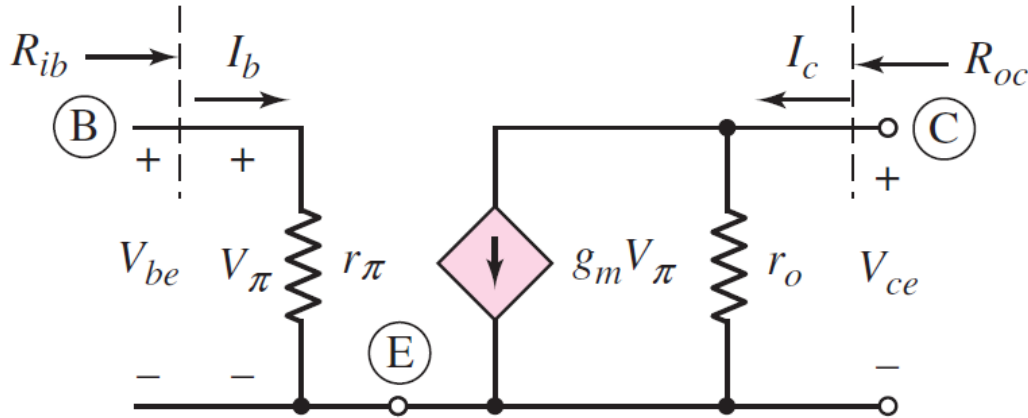
$$r_o \cong \frac{V_A}{I_C}$$

Early voltage



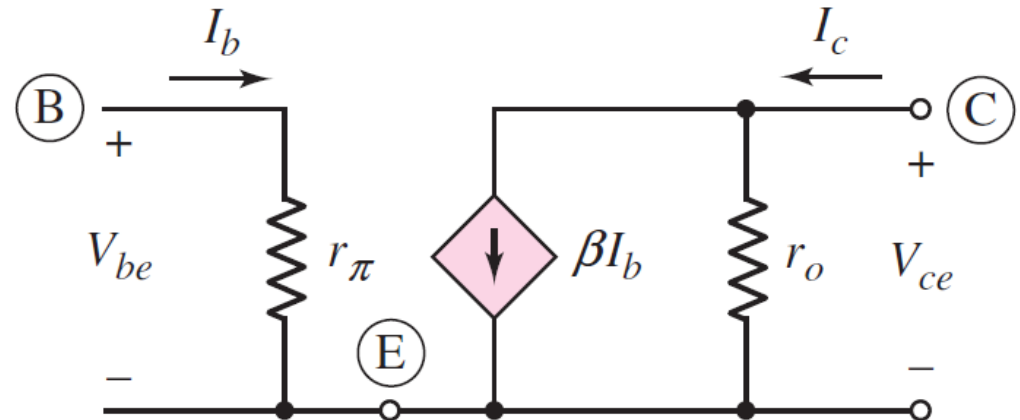
- Typical values of  $V_A$ :  $50 < V_A < 300 \text{ V}$

# Hybrid- $\pi$ Equivalent Circuit, Including the Early Effect



The small-signal equivalent circuit, including the **output resistance** when the circuit contains the **transconductance** parameter.

The small-signal equivalent circuit, including the **output resistance** when the circuit contains the **current gain** parameter.



$$r_o = \frac{V_A}{I_{CQ}}$$

**Small-signal transistor output resistance**



# Example 2.14

- Determine the small-signal voltage gain, including the effect of the transistor output resistance  $r_o$ , with the parameters:

$$\beta = 100$$

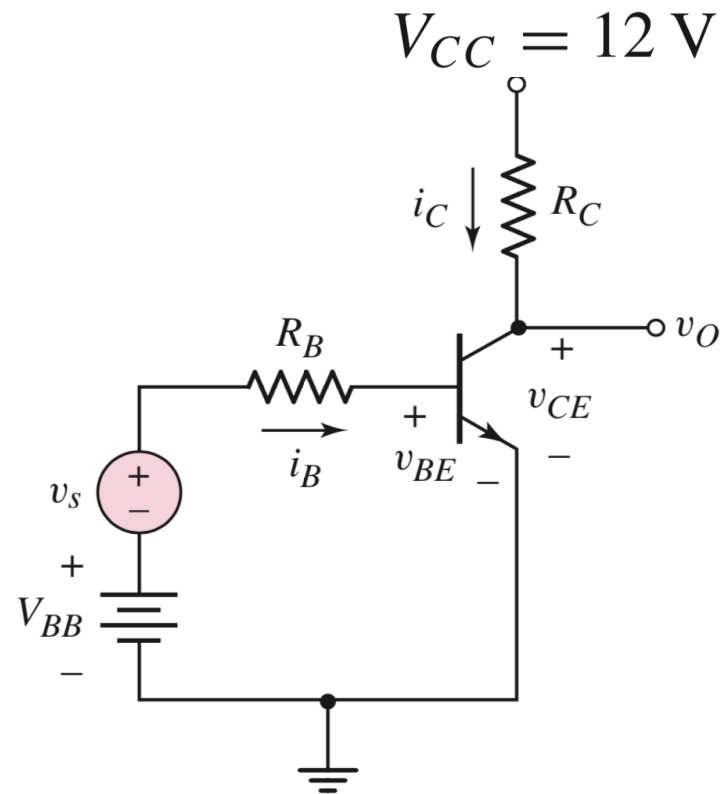
$$V_{BE} = 0.7 \text{ V}$$

$$R_C = 6 \text{ k}\Omega$$

$$R_B = 50 \text{ k}\Omega$$

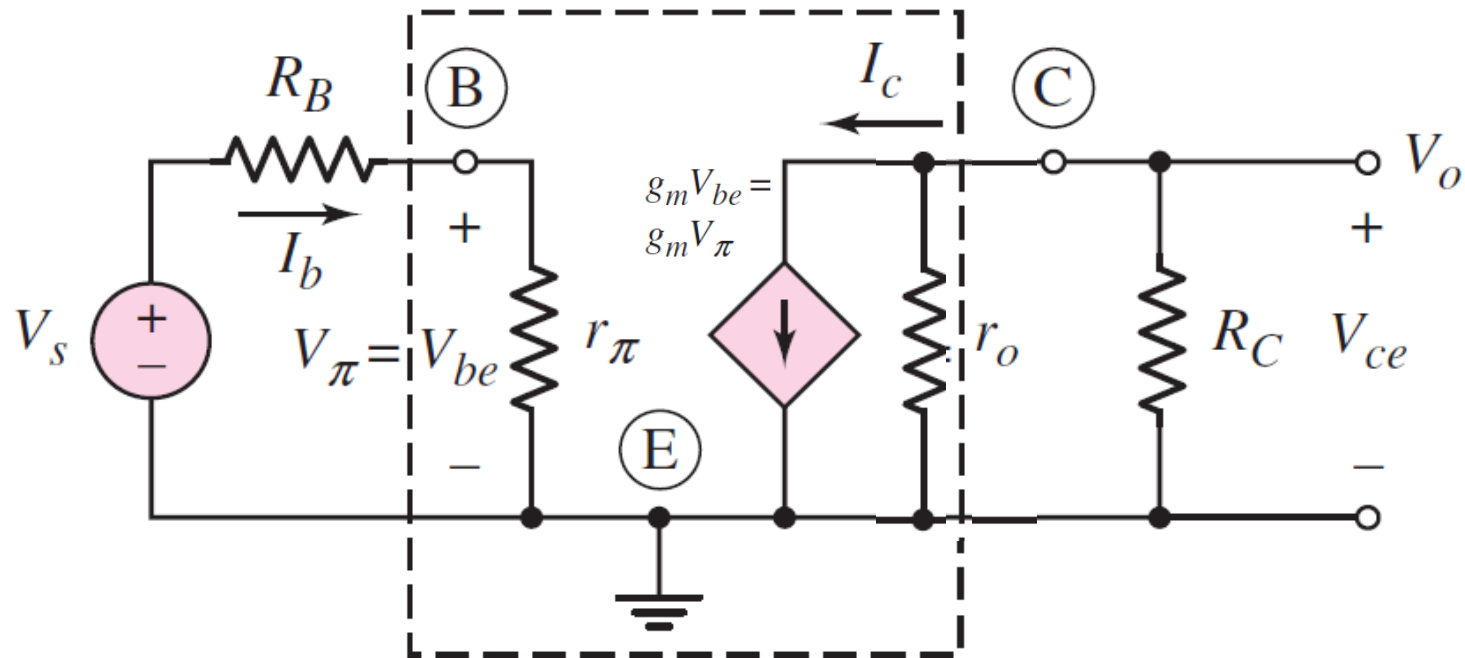
$$V_{BB} = 1.2 \text{ V}$$

$$V_A = 50 \text{ V}$$



# Example 2.14

- The small-signal equivalent circuit, including the output resistance  $r_o$ :



$$A_v = \frac{V_o}{V_s} = -g_m (R_C \parallel r_o) \left( \frac{r_{\pi}}{r_{\pi} + R_B} \right)$$

## Example 2.14

- The output resistance is given by:

$$r_o = \frac{V_A}{I_{CQ}} = \frac{50}{1 \text{ mA}} = 50 \text{ k}\Omega$$

- The small-signal voltage gain is therefore:

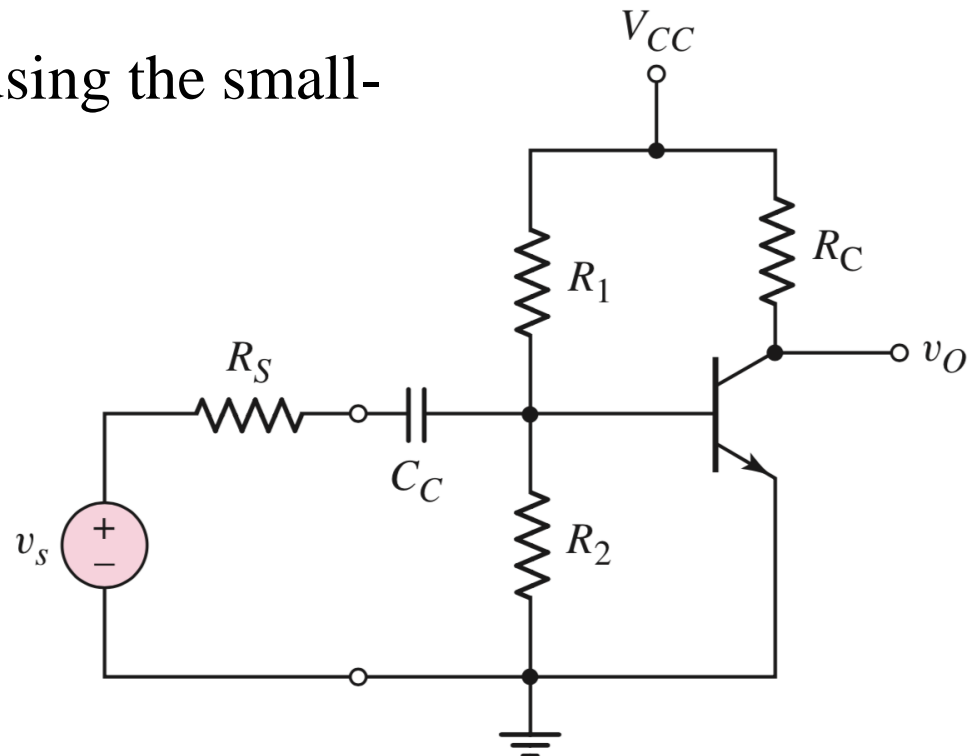
$$\begin{aligned} A_v = \frac{V_o}{V_s} &= -g_m(R_C \parallel r_o) \left( \frac{r_\pi}{r_\pi + R_B} \right) \\ &= -(38.5)(6 \parallel 50) \left( \frac{2.6}{2.6 + 50} \right) \\ &= -10.2 \end{aligned}$$



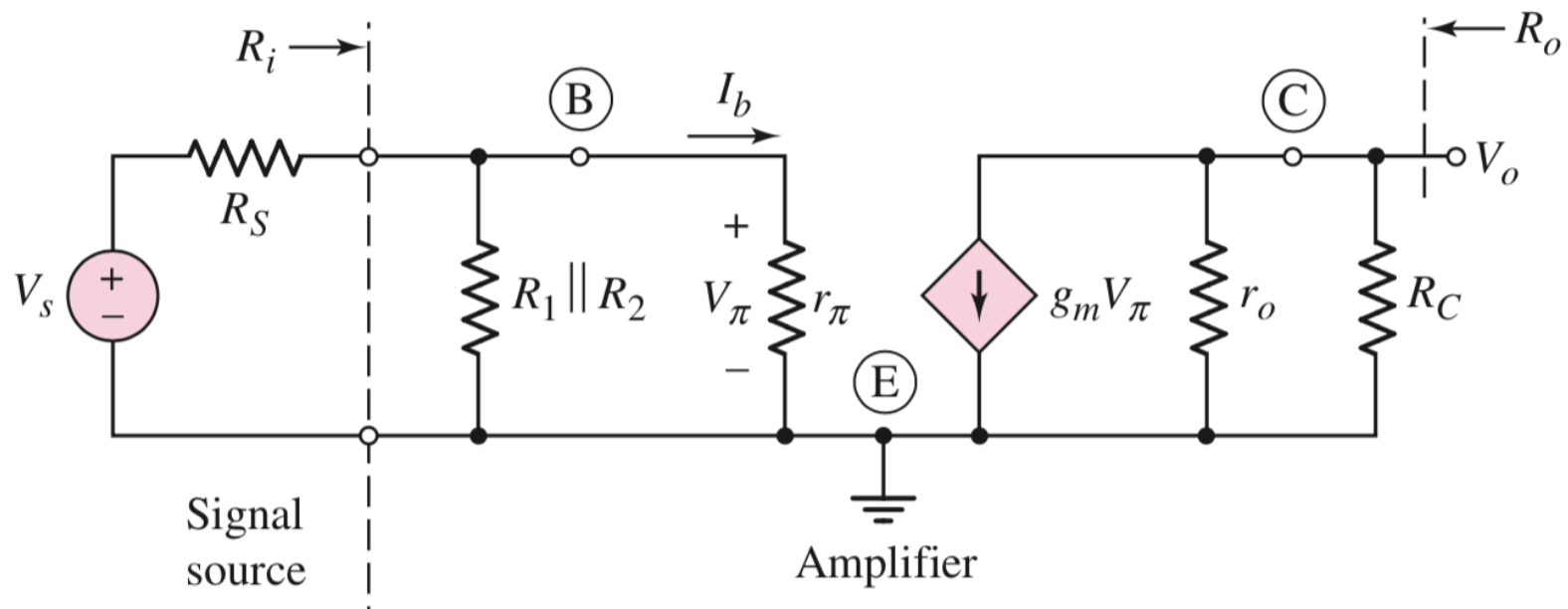
**$r_o$  reduces the magnitude of the small-signal voltage gain**

# Basic Common-Emitter Amplifier Circuit

- Basic common-emitter circuit with voltage-divider biasing:
  - Do the dc analysis (to find the Q-point).
  - Do the ac analysis using the small-signal model.



# Basic Common-Emitter Amplifier Circuit



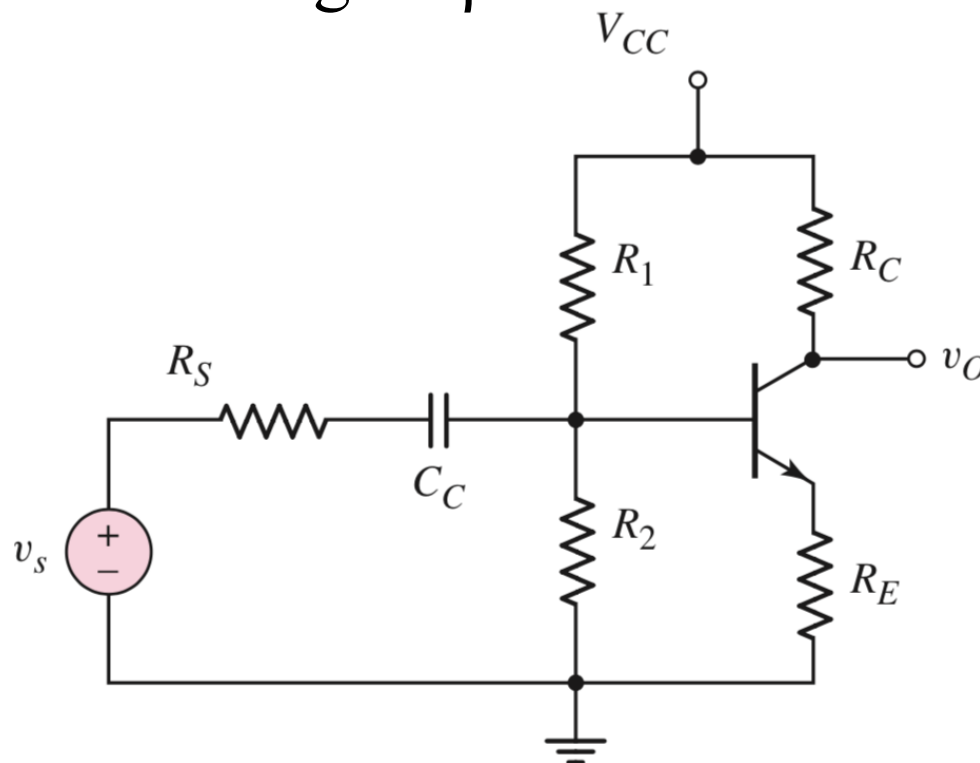
Output voltage:  $V_o = -g_m V_\pi (r_o \parallel R_C)$

Control voltage:  $V_\pi = \frac{R_1 \parallel R_2 \parallel r_\pi}{R_1 \parallel R_2 \parallel r_\pi + R_S} \cdot V_s$

Voltage gain:  $A_v = \frac{V_o}{V_s} = -g_m (r_o \parallel R_C) \left( \frac{R_1 \parallel R_2 \parallel r_\pi}{R_1 \parallel R_2 \parallel r_\pi + R_S} \right)$

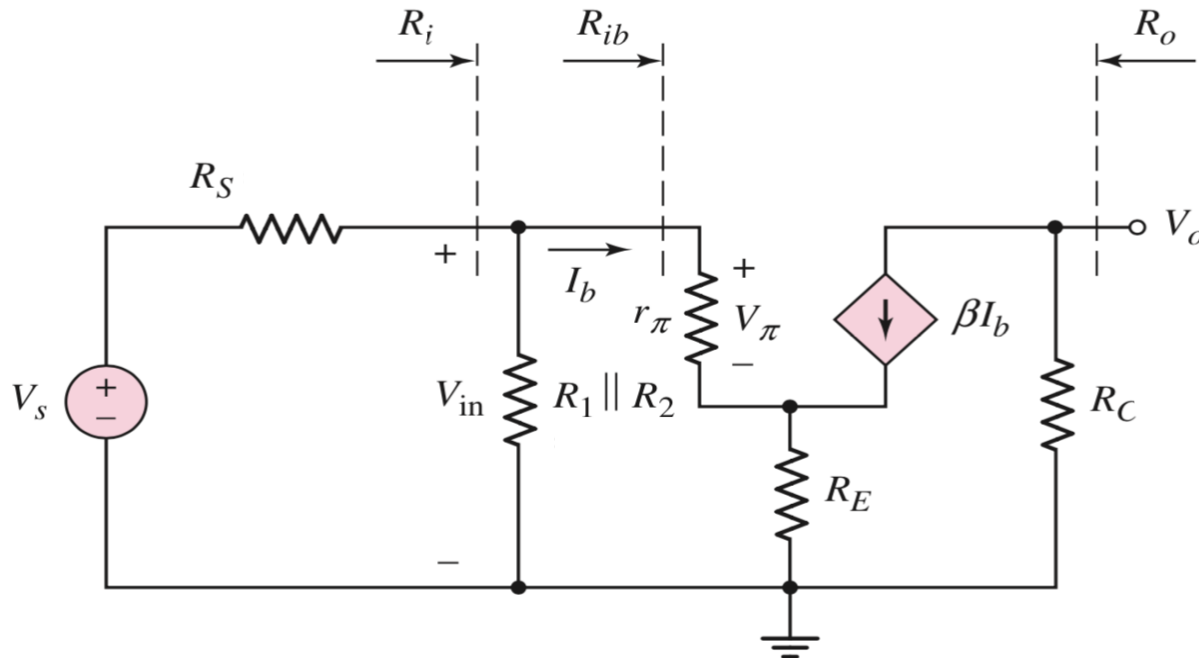
# Basic Common-Emitter Amplifier Circuit

- Using the Emitter resistor ( $R_E$ ) so that the voltage gain of the amplifier circuit will be less dependent on the transistor current gain  $\beta$ .



# Basic Common-Emitter Amplifier Circuit

- The small-signal equivalent circuit:



Output voltage:  $V_o = -(\beta I_b) R_C$

Input resistance:  $R_{ib} = \frac{V_{in}}{I_b} = r_\pi + (1 + \beta) R_E$

# Basic Common-Emitter Amplifier Circuit

- Input resistance to the amplifier:  $R_i = R_1 \parallel R_2 \parallel R_{ib}$

- Input voltage:  $V_{in} = \left( \frac{R_i}{R_i + R_S} \right) \cdot V_s$

- The small-signal voltage gain is:

$$A_v = \frac{V_o}{V_s} = \frac{-(\beta I_b) R_C}{V_s} = -\beta R_C \left( \frac{V_{in}}{R_{ib}} \right) \cdot \left( \frac{1}{V_s} \right)$$

or:

$$A_v = \frac{-\beta R_C}{r_\pi + (1 + \beta) R_E} \left( \frac{R_i}{R_i + R_S} \right)$$



# Basic Common-Emitter Amplifier Circuit

- Voltage gain is:

$$A_v = \frac{-\beta R_C}{r_\pi + (1 + \beta)R_E} \left( \frac{R_i}{R_i + R_S} \right)$$

- If:

$$\begin{cases} R_i \gg R_S \\ (1 + \beta)R_E \gg r_\pi \end{cases}$$

- Voltage gain is approximately:

$$A_v \cong \frac{-\beta R_C}{(1 + \beta)R_E} \cong \frac{-R_C}{R_E}$$

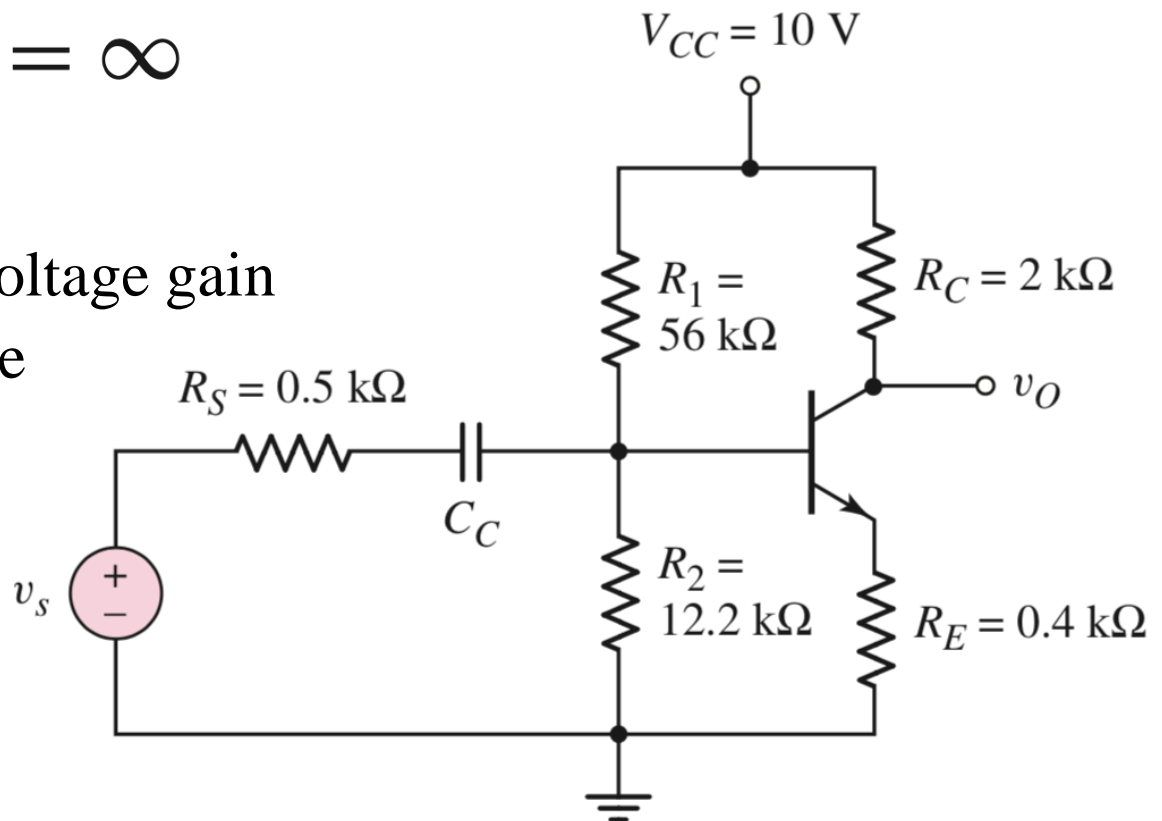
# Example 2.15

- For the circuit in the figure:

$$V_{BE(\text{on})} = 0.7 \text{ V}$$

$$\beta = 100 \quad V_A = \infty$$

- Determine:
  - Small-signal voltage gain
  - Input resistance

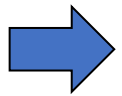


# Example 2.15: DC Analysis

- DC solution:

$$V_{CEQ} = 4.81 \text{ V}$$

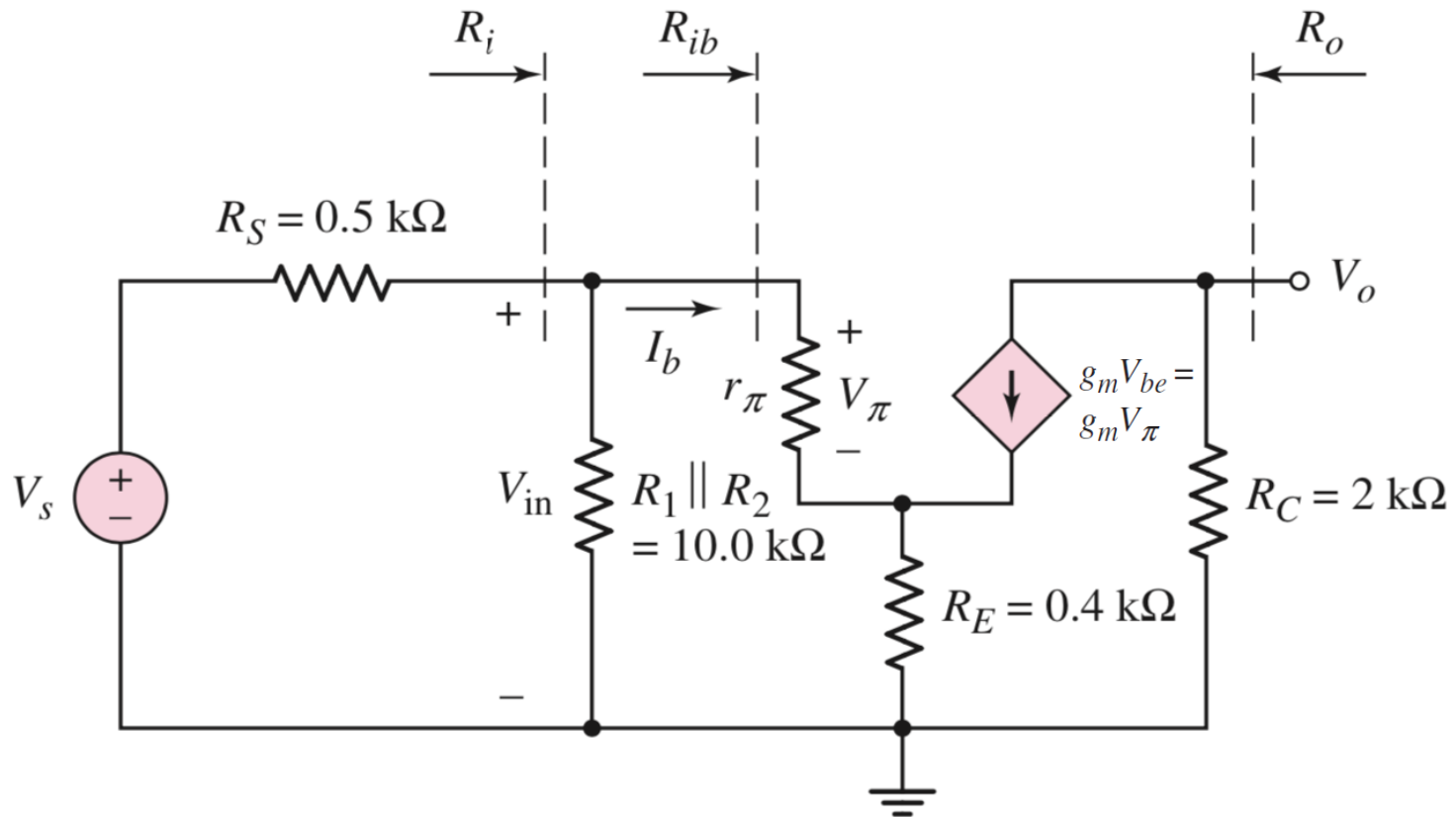
$$I_{CQ} = 2.16 \text{ mA}$$



The transistor is biased in the forward-active mode

# Example 2.15: AC Analysis

- The small-signal equivalent circuit:



## Example 2.15: AC Analysis

- The small-signal hybrid- $\pi$  parameters:

$$r_{\pi} = \frac{V_T \beta}{I_{CQ}} = \frac{(0.026)(100)}{(2.16)} = 1.20 \text{ k}\Omega$$

$$g_m = \frac{I_{CQ}}{V_T} = \frac{2.16}{0.026} = 83.1 \text{ mA/V}$$

- The input resistance to the base:

$$R_{ib} = r_{\pi} + (1 + \beta)R_E = 1.20 + (101)(0.4) = 41.6 \text{ k}\Omega$$

- The input resistance to the amplifier :

$$R_i = R_1 \parallel R_2 \parallel R_{ib} = 10 \parallel 41.6 = 8.06 \text{ k}\Omega$$

# Example 2.15: AC Analysis

- Voltage gain:

$$A_v = \frac{-(100)(2)}{1.20 + (101)(0.4)} \left( \frac{8.06}{8.06 + 0.5} \right) \\ = -4.53$$

- Approximate voltage gain:

$$A_v \cong \frac{-\beta R_C}{(1 + \beta)R_E} \cong \frac{-R_C}{R_E}$$

- Obtain:

$$A_v = \frac{-R_C}{R_E} = \frac{-2}{0.4} = -5.0$$

## Example 2.15: Comment

- The magnitude of the voltage gain is **substantially reduced** when an emitter resistor ( $R_E$ ) is included.
  - Because of the  $(1 + \beta)R_E$  term in the denominator
- $-R_C/R_E$  can be used in the **initial design** of a common-emitter circuit with an emitter resistor.
- The amplifier gain is **nearly independent** of changes in the current gain parameter  $\beta$ .

| $\beta$ | $A_v$ |
|---------|-------|
| 50      | -4.41 |
| 100     | -4.53 |
| 150     | -4.57 |