

Project Necromancer

DESIGN DOCUMENT

Sponsored By: The Rainforest Connection (RFCx)

Submitted By: Joe Gibson gibsjose@mail.gvsu.edu
David Adlof adlofd@mail.gvsu.edu
Kalee Stutzman stutzmak@mail.gvsu.edu
Jesse Millwood millwooj@mail.gvsu.edu

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Executive Summary

Software, electrical, and hardware enhancements to Rainforest Connection's currently used device are proposed in this paper. The electrical enhancements include the addition of a new PCB that contains power regulation and battery charging circuitry, along with current, voltage, temperature, and humidity sensors. The software enhancements include sending sensor measurements to an Android cellphone. Sending measurements from the PCB to the phone will allow for diagnostic feedback that can be used for laboratory testing and verification as well as field statistics. The point of this project is not to entirely redesign the existing device but rather to provide modular enhancements and improvements to specific components.

Power consumption is a major concern and a key area for improvement on the existing device. We will use *Max Point Power Tracking*(MPPT) ICs in the design of the power regulation and solar panel interface to ensure maximum efficiency from the solar panels. In addition we will use Lithium-Ion battery management ICs to ensure that the batteries are properly charge, properly discharge, and to prevent overheating. A switching power regulator will boost the voltage from either the batteries or the solar panel to charge the phone and a linear dropout regulator will provide 3.3V to the regulation and diagnostic circuitry on the PCB.

Temperature is another major concern. To mitigate the heat produced by the phone, the power circuitry, and the environment, a heatsink will be attached to the PCB with direct thermal contact with the phone. The heatsink will extend outside of the enclosure, transferring heat outside of the device enclosure.

Sending diagnostics will be achieved using an 8-bit Atmel ATmega328P microcontroller. Power, temperature, and humidity data will be sent from the microcontroller to the cell phone via USB, where it will be received and displayed by an Android application.

Keywords

Rain forest, Recycling, RFCx, Rainforest Connection, cellphone, Android, logging

Grand Valley State University



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1 RFCx Background

Rainforest Connection (RFCx) is a non-profit organization that is dedicated to stopping illegal logging and deforestation in rainforests throughout the world. The destruction of tropical rainforests is a leading cause of carbon dioxide emission, and much of it is caused by illegal activities. RFCx combats illegal logging with devices using re-purposed cell-phones strategically placed in trees in remote areas. A picture of the entire device is shown below in Figure 1.1.



Figure 1.1: RFCx President Topher White installing an existing device in the rainforests of Borneo

These devices listen and record audio streams at all times, using their data connection to periodically send audio data to the RFCx server. On the server, digital signal processing algorithms are used to detect the sound of chainsaws and engines at a distance of up to $\frac{2}{3}$ of a mile. If a chainsaw is detected, a real-time alert is sent to pre-existing ground patrols, who can react to the situation and combat the threat. In addition to man-made sounds, the RFCx platform is also used to record the sounds of animals in the forest. These sounds can be used to gain information about certain species of animals and are open to anyone to use and analyze. Because of the sheer size of the area covered by a single human, it is impractical, if not impossible, to properly monitor the forests for illegal activities without the aid of technology. The flow of data, from audio collection to human intervention, is shown below in Figure 1.2.

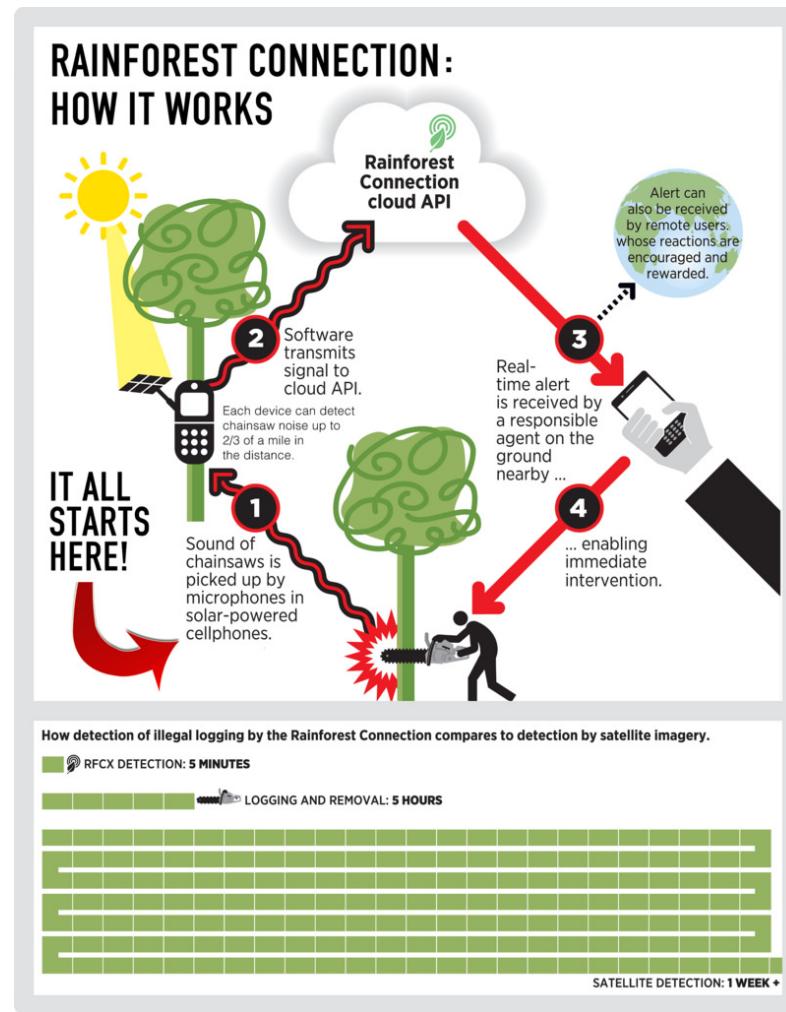


Figure 1.2: Infographic from RFCx website (www.rfcx.org) showing the flow of data

2 Project Introduction

RFCx Project Necromancer is primarily comprised of enhancements to the existing system in the areas of power consumption, power efficiency, temperature concerns, and overall modularity of components. The devices currently consist of an Android phone, Radioshack enclosure, off-the-shelf external microphone and antenna, RFCx solar petals, two dual-cell Lithium-Ion batteries, and various off-the-shelf PCBs and individual electrical components comprising the power regulation and solar and battery management control. The external microphone, antenna, solar petals, batteries (Appendix E.6), and Android phone will remain the same. A view inside of the device is shown in Figure 2.1.

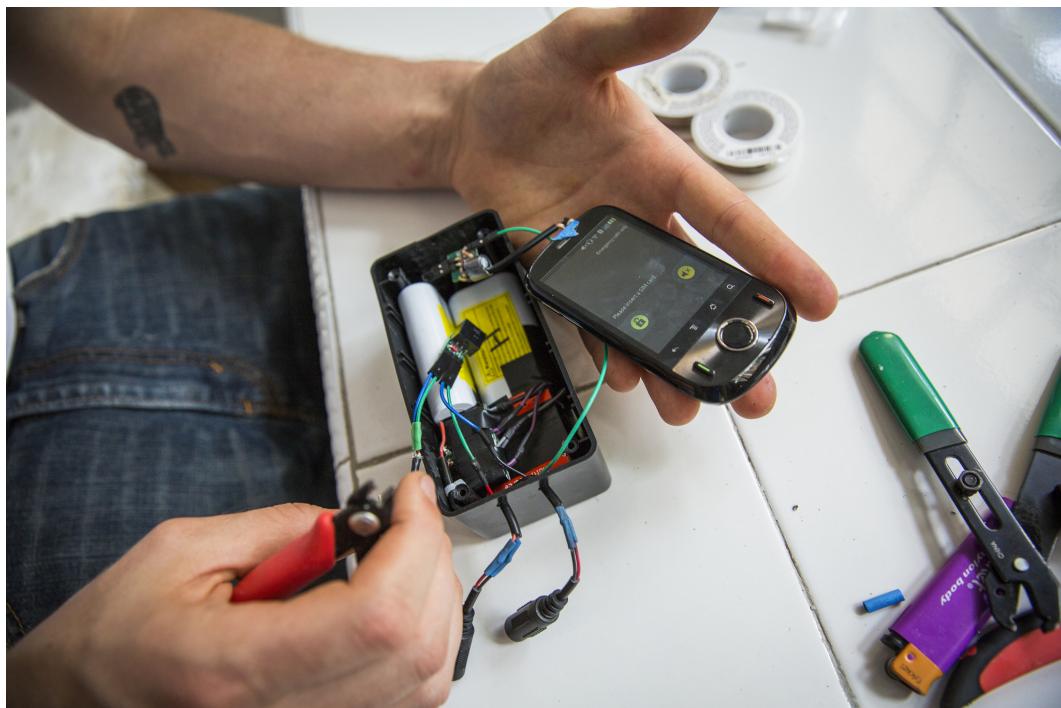


Figure 2.1: Inside of a device: Android phone, batteries, and various electrical components. Some solar charge controller PCBs can be seen in red at the bottom of the enclosure

The solar panel array consists of four petals, each of which has two solar panels on it. The panels are designed and patented by RFCx to work well under low light conditions such as those under the tree canopy. A single petal produces 1.5W of power under laboratory conditions. An individual petal can be seen in Figure 2.2



Figure 2.2: A single solar petal consisting of two panels. Each panel is made from three strips of panel scraps left over from manufacturing at major solar panel companies, connected in series to produce a 1.5V output on each panel

In regards to device enhancements, the principal objective of Project Necromancer is to merge all of the external electronics into a custom printed circuit board. This involves integrating the regulation circuitry and photovoltaic battery charge controller into a single board, and also introducing sensors for temperature, humidity, and power, a microcontroller, and other supporting electronics. The power, temperature, and humidity diagnostics will be sent from the microcontroller to the Android phone via a USB connection. Relaying the collected diagnostic data to the server is possible with the existing framework but is outside of the scope of this project. Instead, the collected data will be displayed for testing and verification purposes. A block diagram of the designed system is shown below in Figure 2.3.

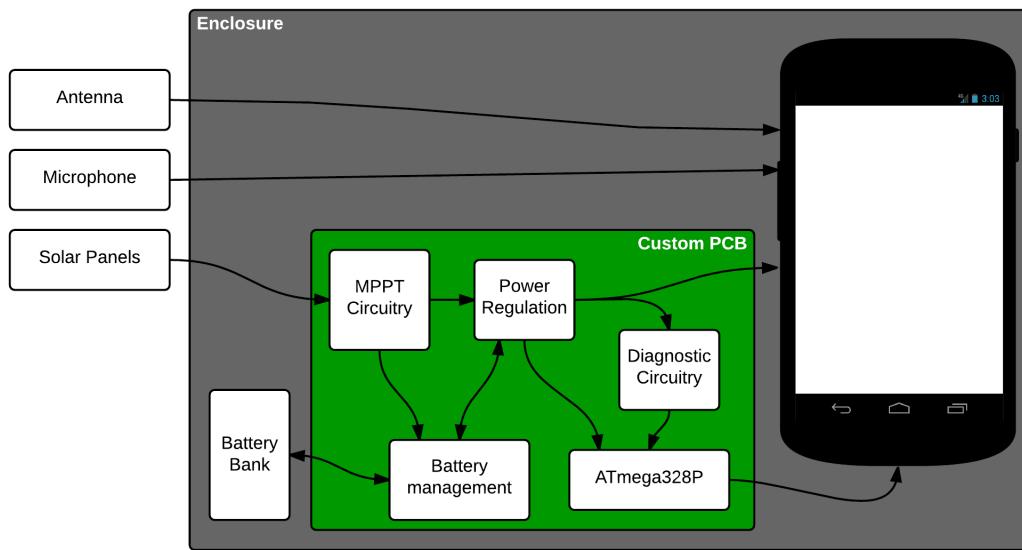


Figure 2.3: High Level Functional Diagram of the Major Components

On the phone, an app called RFCx Sentinel monitors the incoming diagnostics, displaying them to a screen, logging them to a file, and perhaps in the future transmitting them along with the audio data to the server. The RFCx Sentinel Application was developed by our team for the purpose of this project. An actual screenshot of the Sentinel application receiving data from a microcontroller is shown below in Figure 2.4. In addition, although outside of the scope of this project, different audio compression schemes may be investigated if time allows.

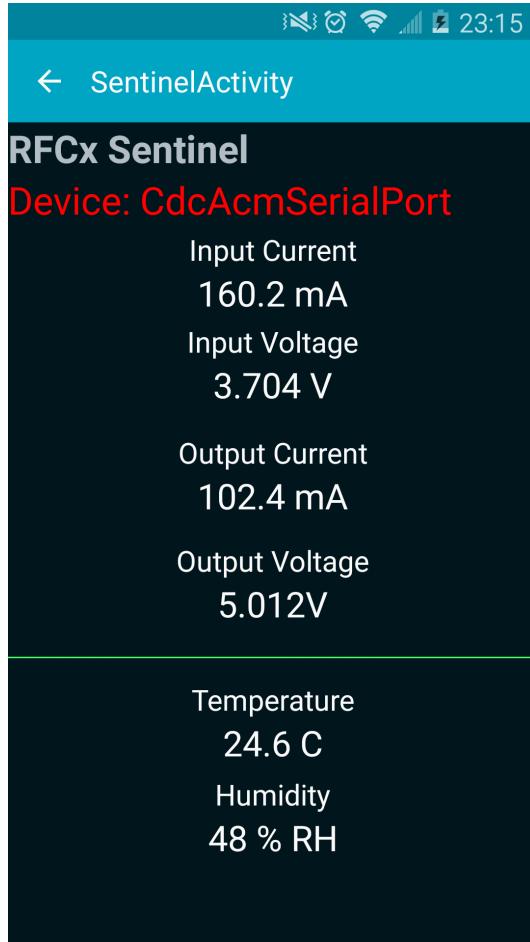


Figure 2.4: Actual RFCx Sentinel App Screenshot

3 Requirements and Functional Specifications

This section is organized by external and internal interfaces, with subsections in each for both hardware and software requirements.

3.1 External Interfaces Requirements

This section addresses the requirements of the enhanced device pertaining to its external interfaces. External interfaces are defined as components of the device interacting with something outside of the device enclosure, including the antenna, microphone, solar panels, and GSM data communication. The possibility of compression is included under external interfaces because it directly relates to the sending of data outside of the device to the server.

3.1.1 Hardware

Requirement 3.1.1.1. The device shall not exceed the existing power consumption and should reduce power consumption by at least 10%.

Requirement 3.1.1.2. The interface with the phone shall consist of a USB connection for power and data, a 3.5mm microphone connection via the standard audio jack, and a connection to the external antenna via the existing antenna cable.

Requirement 3.1.1.3. The device shall use the existing external microphone and antennae

Requirement 3.1.1.4. Shielding techniques should be investigated to reduce the GSM audio interference noted by Topher White in the audio recordings.

Requirement 3.1.1.5. Camouflage color scheme may be used to conceal the device from loggers. Additional camouflage features may be added so long as those features do not cover the solar panels.

Requirement 3.1.1.6. A simple assembly process shall be well documented with illustrations.

To verify **Requirement 3.1.1.6.**, a sample group of people with varying skill levels will be asked to provide feedback on the assembly process and will be timed. The assembly times will be compared with current assembly times.

Requirement 3.1.1.7. The assembly and installation documentation may be translated into Spanish, French, and/or Portuguese.

3.1.2 Software

Requirement 3.1.2.1. The algorithm used to compress the audio signal may be compared to other existing algorithms and may be changed as such depending on the outcomes of comparative testing.

To verify **Requirement 3.1.2.1.**, audio will be recorded and compressed using multiple algorithms including the current algorithm. An infographic hosted on RFCx's website, shown in Figure 2 illustrates the flow of data that is collected from the phone and analyzed on the server.

3.2 Internal Device Requirements

This section addresses the requirements of the enhanced device pertaining to its internal interfaces and software. Internal here is defined as anything inside of the device enclosure, including but not limited to the Android phone, batteries, custom PCB, and supporting electronics.

3.2.1 Hardware

Requirement 3.2.1.1. The PCB shall consist of battery management circuitry, the power regulation circuitry, power interface to the phone, power monitoring circuitry, as well as the microphone interface.

To verify **Requirement 3.2.1.1.**, SPICE will be used to simulate the power charging circuitry to obtain power consumption and efficiency calculations. The manufactured and assembled board will then be subjected to a load test in a lab setting.

Requirement 3.2.1.2. There should be a low power microcontroller included on the PCB that communicates with the Android phone, sending it diagnostic information about components on the PCB. This will be used to monitor power consumption and provide external control of peripherals through the Android Debug Bridge protocol over USB. Extra general purpose pins of the microcontroller should be easily accessible for interfacing with future hardware.

To verify **Requirement 3.2.1.2.**, simple packets will be sent from the microcontroller to the phone. These packets can be verified with debug tools or simple programs on the microcontroller and the phone. A debug serial port may be included as a peripheral to the microcontroller to aid in debugging. Any analog values read by the microcontroller will be verified with shop equipment.

Requirement 3.2.1.3. The monetary cost of the device, not including the solar panels, shall not exceed 25% more than the current device cost, also not including the solar panels. The current cost of the solar panels has been quoted at \$200 and the rest of the device has been quoted at \$200. Increases in monetary cost above the current cost and below 125% of the current cost are for enhancements in functionality (i.e. the PCB, etc.) and reductions in assembly time.

3.2.2 Software

Requirement 3.2.2.1. The microcontroller software should be capable of bi-directional communication between itself and the Android phone.

Requirement 3.2.2.2. The microcontroller software should be capable of communicating power usage diagnostics to the phone over the ADB protocol.

Requirement 3.2.2.3. An Android companion application may be capable of reporting power diagnostics from the microcontroller for testing and debugging.

Requirement 3.2.2.4. There shall be a header on the PCB to program to reprogram the microcontroller.

4 Component Justification

This section describes each component of the PCB in detail and gives justifications for their selection and a discussion of alternative choices that were considered. Two main concerns for every component is packaging and power consumption. There should be no component that the end user can not fix to the PCB without common soldering equipment. Power consumption is a major concern as the device is meant to be located in a remote area and powered by batteries and solar power.

The following is a list of the main ICs that comprise the PCB and are outlined in this section:

- **Atmel ATMega328P** : 8-bit AVR microcontroller (Appendix E.2)
- **SPV1040 Max Point Power Tracker** : Solar power controller and lithium-ion battery charger (Appendix E.12)
- **ADS1015** : External 4-input 12-bit Analog-to-Digital Converter, I2C communication (Appendix E.1)

- **LM75BD** : Ultra Low Power Temperature Sensor, $\pm 2^\circ C$, I2C communication (Appendix E.7)
- **(Optional) HIH6130** : 14-bit resolution Humidity and Temperature Sensor with accuracy of $\pm 4\%$ Relative Humidity and $\pm 1^\circ C$, I2C communication (Appendix E.5)
- **FT230X** : FTDI USB-UART interface for USB serial communication (Appendix E.13)
- **BQ2057CTS** : Linear Battery Charge Management IC (Appendix E.3)
- **LM61428** : Simple Switcher Boost Controller IC (Appendix E.8)
- **SM72238** : Micropower Fixed 3.3V LDO (Appendix E.11)
- **LTC6800** : Rail-To-Rail Input and Output Instrumentation Amplifier (Appendix E.10)
- **LTC4412** : Low loss powerpath controller (Appendix E.9)

4.1 Microcontroller

The ATmega328P microcontroller (Appendix E.2) was chosen as the microcontroller for the PCB. Many aspects were considered when choosing a microcontroller, including power consumption, available interfaces, availability of code samples, community support, ease of programming, and package size.

To this end, the ATmega328P is a logical choice; it is the microcontroller used by the popular Arduino platform, which means there are a multitude of code samples to reference for most any project. In addition, the 328P has a pico-power deep sleep mode, which consumes under $0.1\mu A$ of current. Unlike many options, the 328P has an easy to solder TQFP package. It is also easily programmed by the use of an ICSP interface and does not require expensive hardware programmers or debuggers.

USB communication was another concern when choosing a microcontroller. Similar MCUs that included on-board USB interfaces were also considered, but none could be found that offered the simple package, deep sleep mode, and I2C communication. I2C communication is needed to communicate with the analog-to-digital converter and temperature/humidity sensors.

4.2 MPPT

The SPV1040 Max Point Power Tracker (MPPT) (Appendix E.12) was chosen to perform the solar charge management. A driving factor in choosing the SPV1040 was that RFCx had already established a supplier and had many on-hand to ship us for prototyping. In addition, it has the advantage of being simpler to use than similar chips, like the Solar Magic SM72442, in that no I2C communication is necessary to set and configure registers to perform the same function. Finally, the currently used MCP73871 chip (currently on an off-the-shelf Adafruit board) fails in both the physical package being difficult to assemble by hand (QFN package) when used alone, and being meant for only single-cell Lithium-Ion batteries. In addition, the MCP73871 does not use a true MPPT algorithm, but rather an approximation.

4.3 MPPT Configuration

The MPPT configuration makes a large difference in many aspects of the selection of other components. First, each MPPT can only handle 1.8A of current. Also, the input voltage of each MPPT must be much less than the desired output voltage for them to function properly. Depending on the configuration, the number of MPPT ICs can vary from 1 to 8, increasing cost, and the voltage and current characteristics vary depending on whether they are connected in series or in parallel.

The following figure (Figure 4.1) describes the chosen MPPT configuration. In this configuration, each petal, which consists of two 1.5V panels, has its panels connected in series, giving an output of 3.0V, at 1.5W. This results in a current of 500mA for each MPPT, which is well below the maximum. Each petal (four total) is then connected to its own MPPT, which is set to boost to 5.2V. The MPPTs are then connected in parallel.

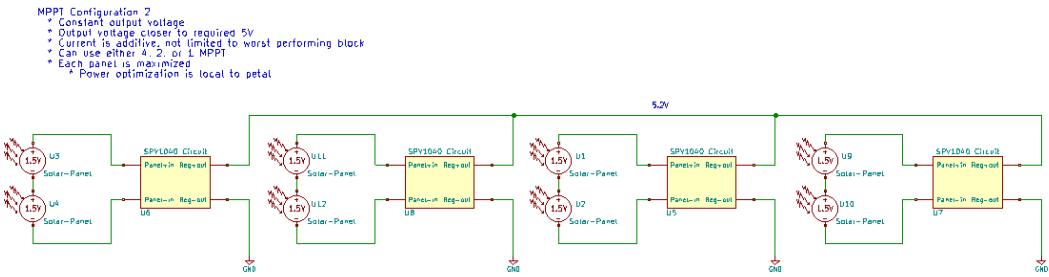


Figure 4.1: Four MPPTs are connected in parallel with the input being the series connection of each panel within a single petal

This configuration offers many benefits. First, the panels on a single petal can be either connected in series or in parallel. Since the SPV1040 can handle up to 1.8A, even when connected in parallel the petal will only produce a maximum of 1A. The input voltage to the MPPT can be either 1.5V (panels in parallel) or 3.0V (series), and the MPPT's internal boost regulator will still produce 5.2V. This allows for testing configurations where all petals have their panels connected in parallel, all in series, or a combination of both under different lighting conditions to see which performs the best without modifying the PCB in any way.

In addition, this configuration localizes the power tracking to an individual petal. Rather than maximizing the entire array, localizing to each petal allows for some petals to be in direct sunlight while others are in shade and each MPPT will react accordingly.

Furthermore, this configuration could be easily adapted to using less MPPTs if needed (to reduce cost, for example). To use two MPPTs, for example, instead of four, two of the ICs would simply not be populated and pairs of petals would be connected in parallel externally and connected to the two populated MPPTs. This is shown in Figure ??.

Finally, as required by the SPV1040, the input voltage will always be much less than the output in this configuration. The input voltage will be either 1.5V (parallel panels) or 3.0V (series), well below the 5.2V output.

Two other configurations that were considered are shown below. In the first alterate configuration, in Figure 4.2, two pairs of MPPTs connected in series are then connected in parallel. This has many drawbacks, including requiring a higher output voltage when it is not needed, and requiring the use of diodes to prevent current from backfeeding into the other MPPTs.

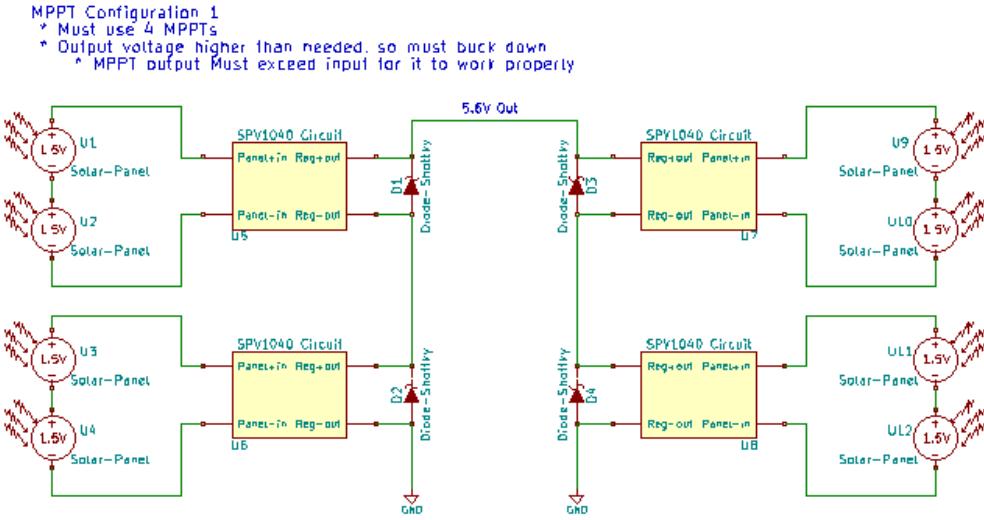


Figure 4.2: Two pairs of MPPTs are first connected in series, then in parallel, requiring the use of feedback diode protection and resulting in a higher than needed output voltage which must then be bucked down

The second alternate configuration, in Figure 4.3, is really the same as the chosen one, but using two MPPTs instead of four as described above.

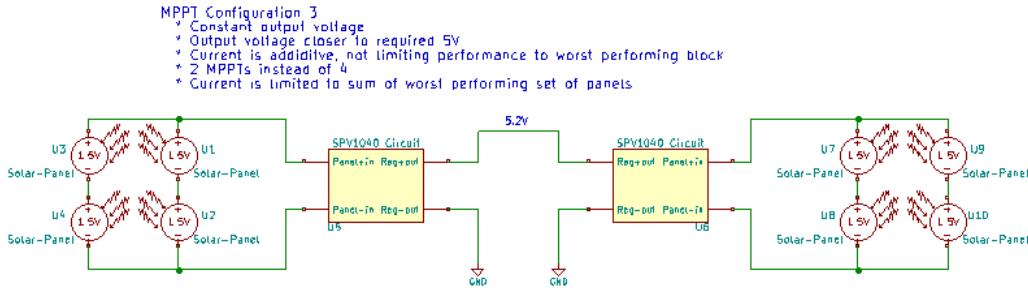


Figure 4.3: Chosen configuration but with two MPPTs instead of four. Results in less control but saves the cost of two ICs and the supporting circuitry of each

4.4 ADC

The ADS1015 external ADC (Appendix E.1) was chosen to perform analog-to-digital conversions for the power sensing. The ATmega328P does not have a strong internal ADC, being only 10-bit resolution, and the ADS1015 is easy to communicate with via I2C. In addition, I2C supports multiple devices in parallel, so only two of the ATmega328P's six analog pins are used. This frees the other four for future use. The ADS1015 consumes less than 150 μ A, has 12-bit resolution, and supports four single-ended analog inputs, which will be used to monitor input current, input voltage, output current, and output voltage on the PCB.

4.5 Temperature and Humidity Sensor

The LM75BD (Appendix E.7) was chosen as the temperature sensor. The LM75 is a super low power temperature sensor with an accuracy of $\pm 2^\circ\text{C}$. It uses less than 300 μ A during peak transmission, and costs under \$1.

An alternative sensor providing both temperature and humidity measurements, the HIH6130 (Appendix E.5), was

also considered. Also using I2C and also being low-power, the only real drawback is the price, at nearly \$14. For this reason the LM75BD was chosen, but the footprint for the HIH6130 will be included but unpopulated on the board as an option to the end user.

Other lower-cost humidity and temperature sensors were investigated, such as the DHT11 and DHT22. The DHT11 is affordable, at around \$5, but has a limited range of 0-50°C. The DHT22 has the range required and is accurate, but costs almost as much as the HIH6130 at around \$9. Both the DHT11 and DHT22 are not I2C, but rather use the one-wire-interface which requires elaborate timing to get the correct data, and take up another pin on the microcontroller. In addition, Adafruit and Amazon were the only places that stock the DHT22, neither of which offer the reliability or quantity of sources like Digikey or Mouser.

4.6 FTDI

The FT230X FTDI chip (Appendix E.13) was chosen for the UART to USB interface between the microcontroller and the Android phone. FTDI is widely used and supported, and, unlike similar devices like the Arduino's CDCACM, does not require another microcontroller to be added, configured, and flashed with software. In addition, the RFCx Sentinel application, which uses the open source usb-serial-for-android library, readily supports FTDI. Serial USB communication has already been achieved using an ATmega328P MCU, a similar FTDI chip, and the Sentinel app.

4.7 Battery Management

Battery management is important for the ability to reclaim and potentially fix a damaged battery, and also to prevent potential fire hazards. Being in a hot climate and surrounded by ample fuel for a large-scale forest fire, battery management was chosen to be included in the design. The BQ2057CTS battery charge management IC was thus chosen to control the charging of the Lithium-Ion batteries. It is designed for both single and dual-cell battery packs, and combines current and voltage regulation, charge status indication, and charge rate auto compensation.

4.8 Power Path Management

To manage the power selection between the solar panels and the batteries, a power path management solution was required. This was required because while the batteries are being charged the rest of the circuit should not draw from them. If the rest of the circuit draws from them while they are being charged, the battery charge management IC could get confused and damage the batteries by over charging or under charging. A diode-ORed configuration, in which power sources are ORed together via a near ideal diode($0.02V_f$), selects the source with the higher voltage. The LTC4412 (Appendix E.9) was chosen to perform this power path management. The ideal diodes are implemented externally with a FZT788B P-Channel MOSFET (Appendix E.4). This IC also has a very low quiescent current, below $1.15\mu A$.

4.9 Power Regulation

The LMR61428(Appendix E.8) Step-Up Voltage regulator was chosen because of its price, package, and performance. It is important for all of the ICs on this board to be in a package that the end user can assemble with without the aid of more advanced PCB assembly equipment such as solder paste/stencils and ovens. This means that they can not be in packages where there are pins underneath or too small to place with tweezers. The operation requirements for the LMR61428 were within the worst case behavior for the feeding circuitry. Some of the other buck/boost controllers required a much higher input voltage when the load current was around 500mA. The LMR61428 requires less than 2V, which is possible even when drawing from the batteries. Since this is a design for a remote device powered from batteries and solar power, quiecent current is a concern as well. The LM61428 only draws 80mA when in the operating mode.

4.10 Current Sensing

The LTC6800 precision instrumentation amplifier (Appendix E.10) was chosen to perform current sensing. This instrumentation amplifier operates rail-to-rail on the input and output, which provides a larger window to sense the voltage across the sense resistor. A sense resistor value of 0.010Ω was chosen to provide minimal power dissipation.

Although very small, since the leakage current into the opamp is also extremely small (on the order of 1nA), the trace resistance, which is approximately 0.035Ω , is not a concern. The LTC6800 also draws very little current. Under no load the LTC6800 draws a maximum of 1.3mA.

5 System Design

5.1 Hardware Design

5.1.1 Power Sources

The system is powered from eight solar cells that have been manufactured by RFCx. These solar panels have been reported to have an open circuit voltage of 1.6V and produce an average of 0.75W each under laboratory conditions. The other power sources on board are two dual-cell 4400mA/Hr lithium-ion (Li-ion) battery packs. As discussed in the MPPT configuration justification, the solar panels will be configured in a way that a pair on an individual petal may be wired in either series or parallel. The pairs will be wired how the end user would like them and the remaining wires will be connected to a terminal block with screw/leaf spring wire termination on the PCB board, which will be powering the MPPT controllers. This is illustrated in the figure 5.1.

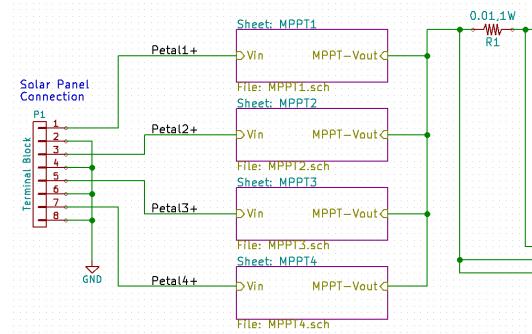


Figure 5.1: MPPT and Solar Panel Interface

With this configuration, a configurable output voltage of 5.2V, the maximum of the SPV1040, will be obtained at an average of about 1.15A, yeilding an input power of about 6W.

5.1.2 Solar Charging

A Max Point Power Tracker (MPPT) increases efficiency by adjusting the current and voltage of the output to achieve the maximum power. The SPV1040 will regulate the solar cell voltage up to 5.2V. From the MPPT the battery management circuitry, the 3.3V line, and the 5V line is powered.

5.1.3 Battery Management

The two dual-cell Lithium-Ion batteries are each managed by a bq2057CTS. Figure 5.2 shows the battery management circuitry for one of the 2-cell battery packs. This IC provides voltage and current regulation, battery conditioning, temperature monitoring, charge termination, charge status indication, as well as charge-rate compensation. The charging is started in the constant voltage phase and stops when the current falls bellow the current termination threshold. The bq2057 inhibits charging until the battery temperature is in the user defined range. This range is defined in this circuit with resistor $R24$. Only the lower temperature bound is set here because the device is not intended for cold environments. The charge rate compensation is set by resistors $R10$ and $R22$. The automatic charge compensation helps to charge the batteries faster and compensate for the battery pack's internal impedance.

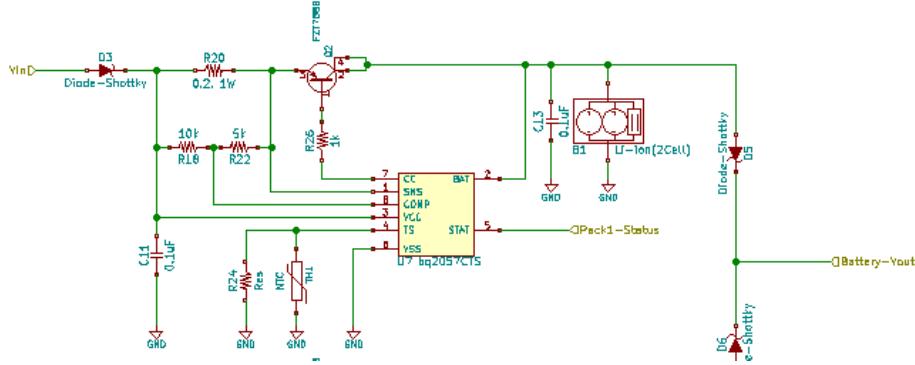


Figure 5.2: Battery Management Circuitry

The calculations for the component selection for the battery management circuitry is included in Appendix D.1.

5.1.4 Voltage Regulation

A diode-ORed power path management circuit was used to switch the power source that feeds the 3.3V and 5V regulation circuitry. This circuit is shown below in Figure 5.3.

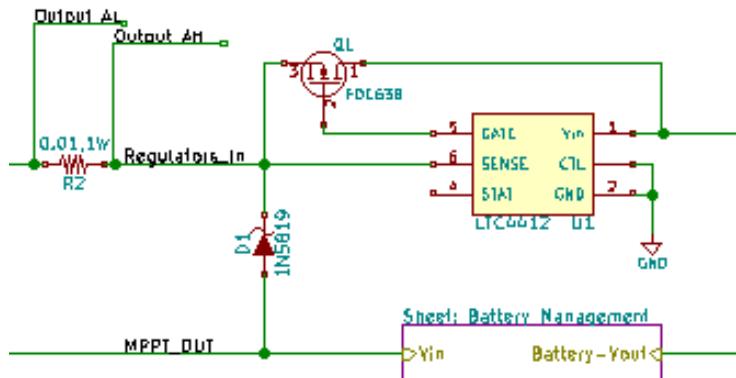


Figure 5.3: Diode Ored Circuit

This circuit provides power path switching in under $100\ \mu s$, and there is virtually no dip in the output voltage during the switch. A dip of approximately 500mV was observed when using a transistor alone to simply switch between the two sources, as shown in the simulation figure in Appendix 5.5. With the diode-ORed topology, the switch is clean, as seen in the simulation figure in Appendix 5.6.

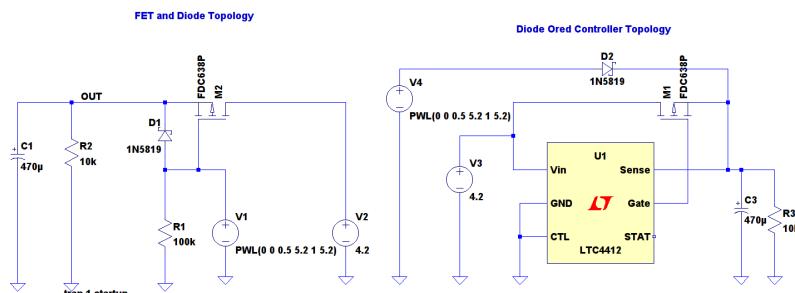


Figure 5.4: Simulation of Diode Ored Circuit

The two circuits were simulated with LTSpice. The same diode and transistor were used in each simulation. A load of 550mA was used because this is more than the calculated worst case current draw from the circuit.

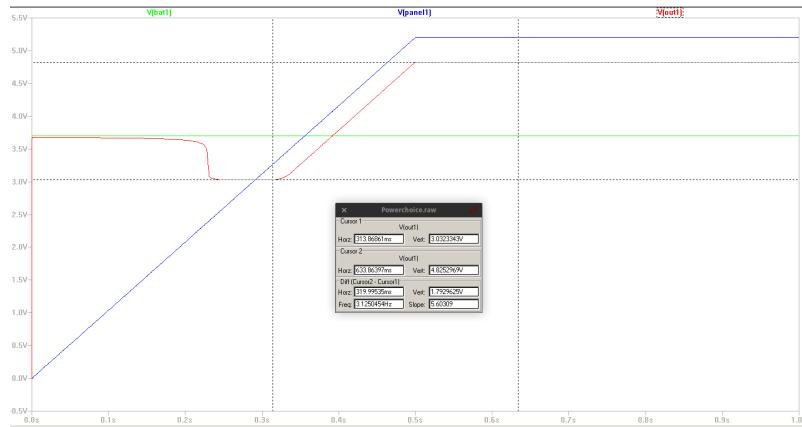


Figure 5.5: Simulation Result of Old Diode Ored Circuit

It can be seen that as the panel voltage is rising, there is a considerable dip to around 3.0V. If this occurred, the 3.3V linear drop out regulator would not be able to regulate properly and the 3.3V line would be deactivated. The diode-ored controller topology simulation result can be seen in the following figure.

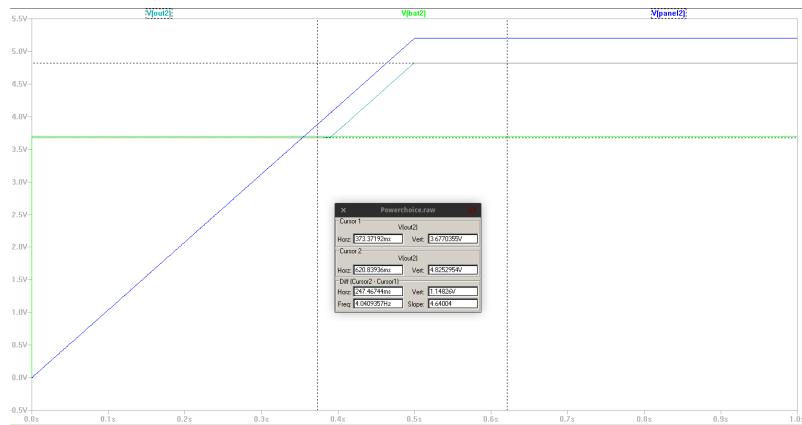


Figure 5.6: Simulation Result of Current Diode Ored Circuit

Here it can be seen that there is a very small drop in voltage when powered only from battery and a reasonable drop when powered from the solar panel. This is the desired behavior.

The LM61428 is a step-up voltage regulator that is configured to boost the input voltage to 5V at an output current of up to 1A. The output voltage of 5V is used to power the Android phone.

The calculations for the surrounding components can be seen in Appendix ???. The layout of the 5V boost regulator can be seen in the following figure.

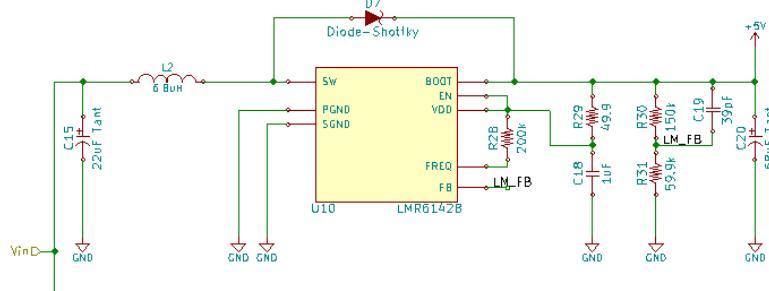


Figure 5.7: 5V Voltage Regulation

A Texas Instruments SM72238 Micropower fixed 3.3V LDO is used to regulate the 3.3V line. This was chosen over a switching regulator because the minimum voltage of 3.7 and the output voltage of 3.3V were too close together, causing the duty cycle calculations to come out to negative or not meet certain regulator's requirements. The SM72238 has very low dropout, which is in range for the need of this application. The only external components required by the LDO are two low ESR 1uF capacitors on the input and output.

5.1.5 Input and Output Current and Voltage Sensing

The ADS1015 is a 12-bit ADC that can communicate over I2C with the microcontroller.

The LTC6800 instrumentation amplifier is used to sense the voltage across a known sense resistor. The input current sense circuit is configured to have a gain of around 80.5. The sense resistor has been selected to be 0.01Ω . With this configuration the ADC will be able to sense the current with a resolution of $1\text{mA}/\text{bit}$. The calculations for this section can be seen in Appendix ???. The configuration of the current sense amplifier can be seen in Figure 5.8 below. The input and output voltage are sensed with simple resistor dividers that are fed to the ADC.

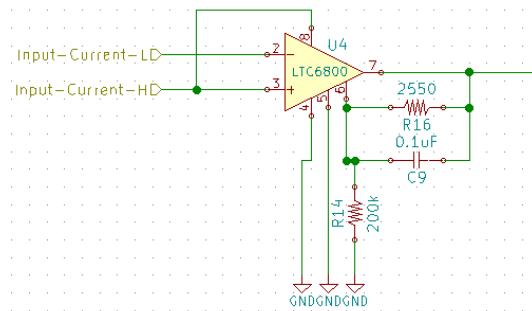


Figure 5.8: Current Sense Amplifier

5.1.6 Microcontroller

Three other microcontrollers were considered. Two ARM M0+ low power micro controllers were considered. The Atmel ATSAM ARM M0+ was not chosen because it drew more current than the 328P and was decided to be over kill for this application. Some nice features were that it had a built in USB module and required no external tools to program it. The Freescale KL25Z was also decided to be overkill for this application and was not chosen because the programming interface of the end user would have been difficult as it required a JTAG programmer. The other microcontroller was a Texas Instruments 16-bit RISC MSP430. This microcontroller was the most expensive, drew the highest current in active and sleep modes, and requires an external tool to program. The ATmega328P does require an external tool to program but it does have low power sleep modes, it is cheap, its is simple, and it is well documented not only by Atmel but by a very large community. It is felt that this would benefit the end user the most in the future.

5.1.7 Temperature and Humidity

A temperature sensor (LM75BD) and a humidity/temperature sensor(HIH6130) will be included on the board. The schematic connections of the two ICs is shown below in Figure 5.9.

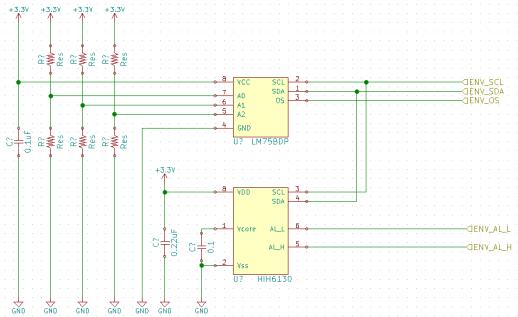


Figure 5.9: Temperature and Humidity Sensors

5.1.8 Connectors

The USB connection consists of a standard USB Micro A connector, soldered directly onto the board and is secured to the board as a strain-relief mechanism. A standard 3.5mm audio cable is used to connect the microphone. The existing standard GSM antenna adapter is used to interface with the phone's onboard GSM module.

5.1.9 GSM Interference

The use of X2Y TDMA filtering capacitors will be tested to reduce the noise produced by the stopping and starting of GSM packets, which is in the audible range at 217Hz. A pass-through 3.5mm microphone interface will be included to test the X2Y capacitors. In addition, a large heatsink will be attached to a large ground plane on one side of the board, and the phone will be attached to the same ground plane, which should help with some shielding.

5.1.10 PCB Size

Two size options were proposed for the PCB, including having only enough space for the components and having a long open space on the PCB for attaching the phone. Having a long PBC with space for the phone was chosen to simplify the assembly process for the device. The length of the open space is long enough to accommodate large phones, and variable length mounting holes in the PCB allow for any size phone to be securely mounted to the PCB using snap-fit mounting screws. A micro-USB cable is used to interface the phone to the rest of the board. Using a cable instead of a connector allows the use of any size phone in the device. Having the PCB only large enough to fit the electrical components on it requires a separate mounting mechanism for the phone, which complicates the assembly of the device.

5.1.11 Heat Dissipation

Multiple alternatives were explored for dissipating heat built up in the enclosure, including drilling holes into the enclosure, putting fans in the enclosure to control airflow in and out of the enclosure, and using a heat sink. Using a heat sink was chosen as the best design alternative for heat dissipation. Drilling holes in the enclosure can allow water, insects and dust to enter the enclosure. A wire mesh over the holes could be used to keep insects out of the enclosure, but water and dust could still get into the enclosure and damage the electronics. Running fans in the device creates a sound in a similar frequency range to the chainsaw noise the device is trying to detect. This can cause false detection of a chainsaw by the RFCx server. A heat sink also requires a hole to be drilled into the enclosure for the heat sink to reach outside of the enclosure. This opening is sealed with caulk or by other methods to prevent water, insects and dust from entering the enclosure. The battery cover on the phone is removed and thermal paste is used between the phone battery and the PBC, and between the PCB and the heat sink. This allows heat to dissipate out of the enclosure and help keep the phone attached to the PCB and the PCB attached

to the heat sink. Vias in the PCB help to transfer more readily through the board instead of trying to transfer the heat through the fiberglass the board is made of.

5.2 Hardware Implementation

5.2.1 Heat Sink

A heat sink, as described in Section 5.1 is shown in Figure 1.4. The current design calls for a rectangular opening to be cut into the front face of the enclosure so that the heat sink may pass through. The shape of the heat sink will be optimized for reduced interior air temperature through heat transfer calculations.

5.3 Software Design

The software used in the design will consist of C and C++ code running on the ATMega328P microcontroller, as well as a companion app (RFCx Sentinel) written in Java, running on the Android phone.

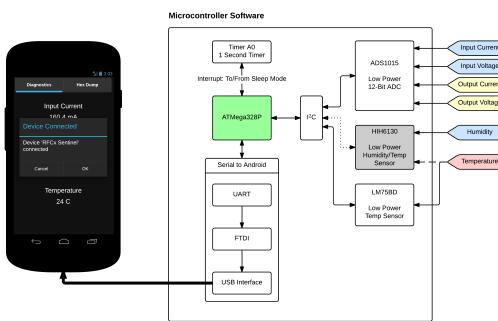


Figure 5.10: Software UML Diagram

The microcontroller software gathers data from a humidity/temperature sensor, and input/output current and voltage. This data is sent via the ATMega328P serial port to the Android phone via the FTDI chip on the PCB and the usb-serial-for-android libraries on the phone. Listing 1 describes the basic functionality of the microcontroller software.

Listing 1: MCU Flow Code Snippet

```
void wakeFromSleep() {
    //Get sensor measurements
    GetDiagnostics(&Diagnostics);
    //Send sensor measurements to phone
    SendDiagnostics(Diagnostics);
    //Go to sleep
    enterSleep();
}
```

5

5.4 Software Implementation

An ATMega328P microcontroller is used to take measurements from the sensors. The temperature (and possibly humidity) measurements are sent digitally via I2C to the microcontroller. On the same I2C bus is the ADS1015, which has four single-ended analog inputs for reading the input current, input voltage, output current, and output voltage. This data is sent to the phone using the standard AVR UART serial library.

The data, once sent to the phone, is monitored by the RFCx Sentinel app. This app is written in Java in Android Studio, and uses the open-source usb-serial-for-android library. The app opens a connection upon discovering a compatible device (FTDI is compatible), and allows the user to view a streamlined interface with relevant data, as

well as a tab for the raw hex dump of incoming serial data. The data may or may not be transmitted along with audio data to the RFCx server for real-time monitoring.

6 Verification

6.1 Hardware Verification

To verify the power consumption of the devices in **Requirement 3.1.1.1..** the voltage applied and current drawn by the both the enhanced device and the current device will be measured over the course of 1 hour during a realistic usage scenario. The average power will be verified to not exceed 90% of the existing device's usage.

To verify **Requirement 3.1.1.5..** a visual inspection by volunteers will qualify camouflage schemes. A successful inspection will be one in which more than 80% of the volunteers are unable to find the device within a 2 minute inspection window.

To verify **Requirement 3.1.1.6..** a sample group of people with varying skill levels will be asked to provide feedback the on assembly process.

6.2 Software Verification

To verify **Requirement 3.1.2.1..**, audio will be recorded and compressed using multiple algorithms including the current algorithm. An infographic hosted on RFCx's website, shown in Figure 2 illustrates the flow of data that is collected from the phone and analyzed on the server.

To verify **Requirement 3.2.1.2..**, simple packets will be sent from the microcontroller to the phone. These packets can be verified with debug tools or simple programs on the microcontroller and the phone. A debug serial port may be included as a peripheral to the microcontroller to aid in debugging. Any analog values read by the microcontroller will be verified with shop equipment.

7 Validation

??, **Requirement 3.1.1.2..**, and **Requirement 3.1.1.4.** can be validated by inspecting the components on the PCB to ensure all required components are present on the board. Requirements **Requirement 3.1.1.6.** and **Requirement 3.1.1.7.** can be validated by handing the assembly instructions out to a sample group of people with varying skill levels and receiving feedback on the set of instructions from them. People with the ability to read other languages can be used if the documents have been translated from English into other languages.

Requirement 3.2.1.3. can be validated by inspecting the total cost printed on the BOM for the enhanced device. **Requirement 3.2.1.1..**, **Requirement 3.1.1.1..**, and **Requirement 3.2.1.2.** can be validated by current and voltage measurements taken in the lab using a DMM. The power calculations made based on those measurements can be compared to similar calculations based on measurements taken from the current device. SPICE simulation data and values displayed on the RFCx Sentinel app will be compared to the actual power consumption of the new device.

Requirement 3.2.2.1.., **Requirement 3.2.2.2..**, **Requirement 3.2.2.3..**, and **Requirement 3.2.1.2.** can be validated by comparing the values reported in the RFCx Sentinel app to the calculated power consumption of the enhanced device.

Requirement 3.1.1.3. can be validated by changing the scale factor in the microcontroller program, reprogramming the microcontroller from the PCB header and comparing the values displayed on the RFCx Sentinel app to the previous displayed values. The new values displayed on the RFCx Sentinel app should reflect the change to the scale factor in the microcontroller program.

Requirement 3.1.1.3.., **Requirement 3.2.2.3..**, and **Requirement 3.1.2.1.** can be validated during a field test. The enhance device can be mounted at eye level in a tree and turned on to allow the device to start sending audio data to the RFCx server. Requirement **Requirement 3.1.1.5.** can be validated by having a volunteer outside of the project search for the device in a wooded area without knowing what it looks like to see if it sticks out. A chainsaw can be turned on 0.25 miles from the device to trigger an alert and validate that the enhanced device can communicate with the RFCx server. The size of the audio recording sent to the RFCx server after employing the audio compression algorithm can be compared to the size of audio data sent to the RFCx server by the current

device to determine the audio compression ratio of this algorithm. Both audio recordings can be played back to determine the level of audio interference created by GSM transmission.

8 Project Budget and Schedule

8.1 Budget

This project will require minor funding for manufacturing and populating the PCB, and the materials to construct a new enclosure, as well as general testing and component costs. As RFCx is a non-profit organization working solely on grant money, this budget is not expected to be covered by them.

- \$400 = 4 x \$100 for PCB manufacturing
- \$320 = 4 x \$80 for PCB components
- \$200 = 1 x \$200 for general needs
- Estimated Total: \$920

9 Schedule

The schedule in Figure 9.1 is the proposed schedule for all phases of the project. This will be used as a general timeline for guidance throughout the project.

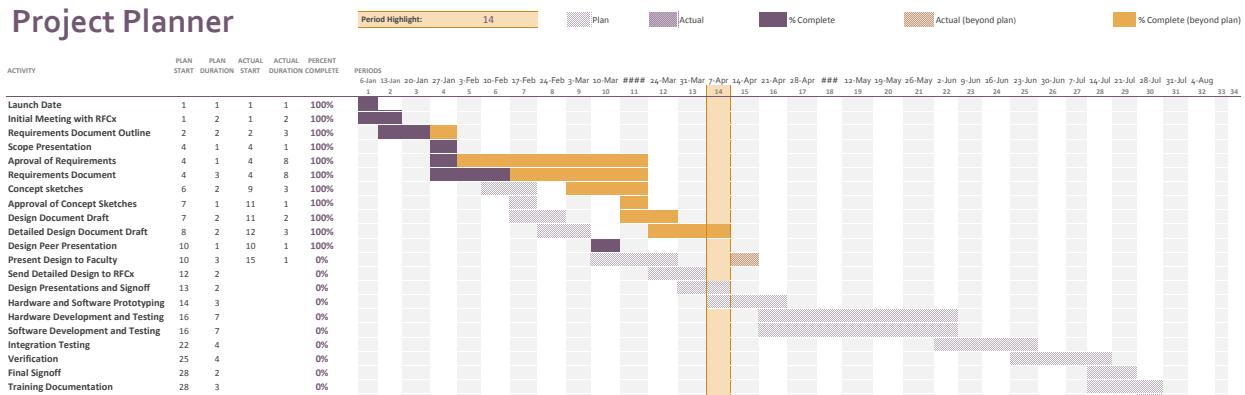


Figure 9.1: Gantt Chart for Schedule

Appendices

Appendix A Electrical Schematics

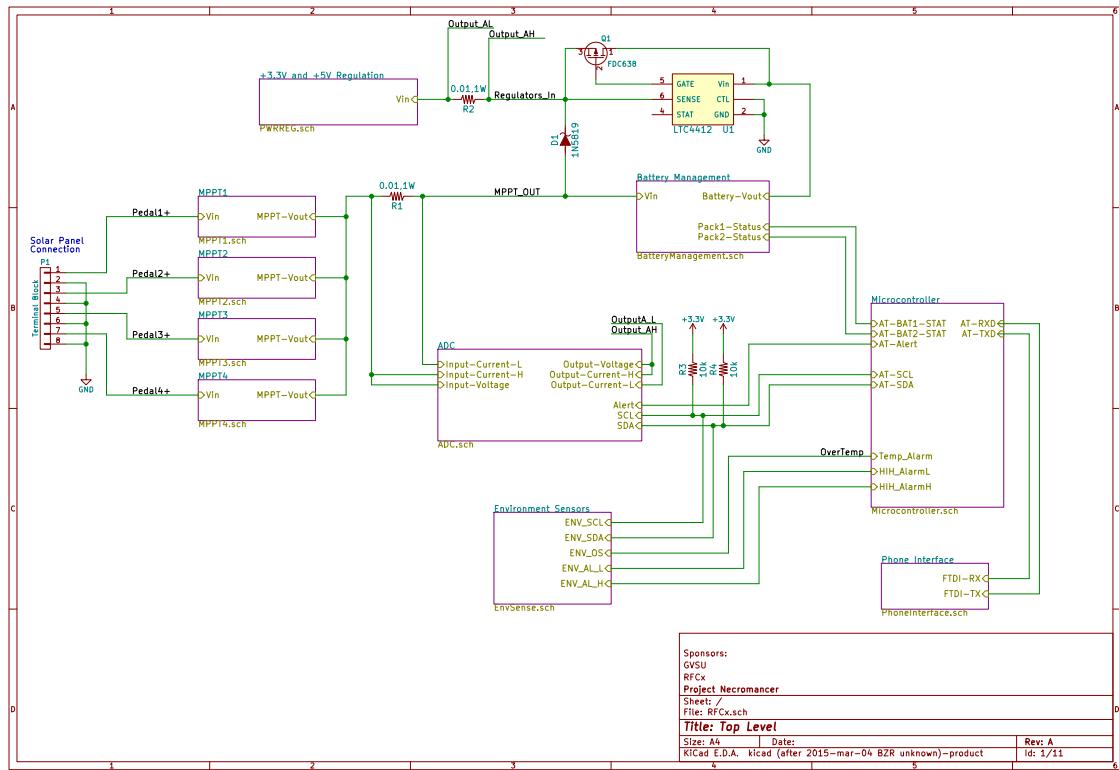


Figure A.1

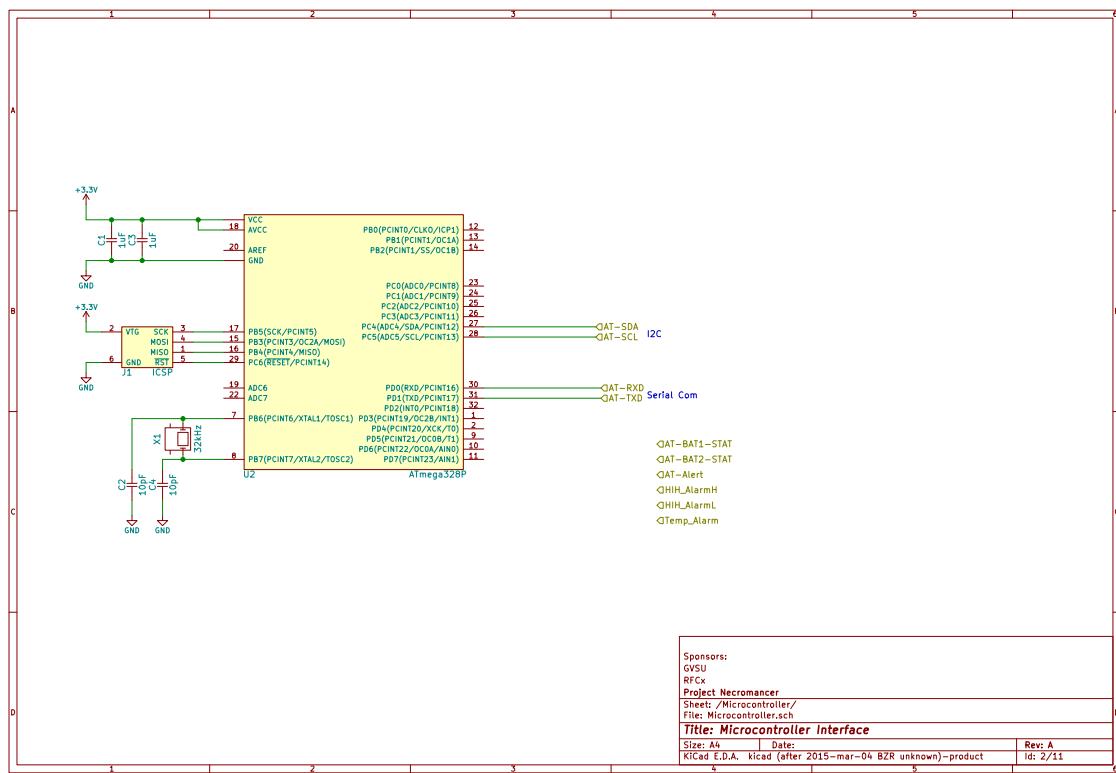


Figure A.2

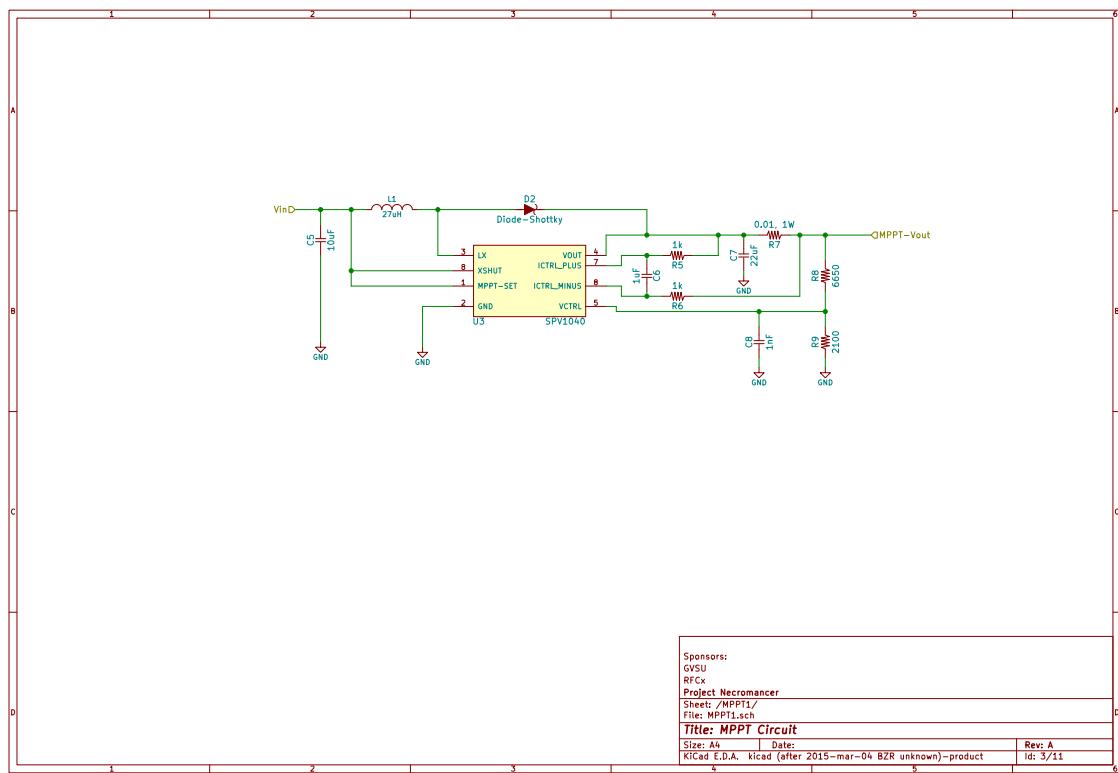


Figure A.3

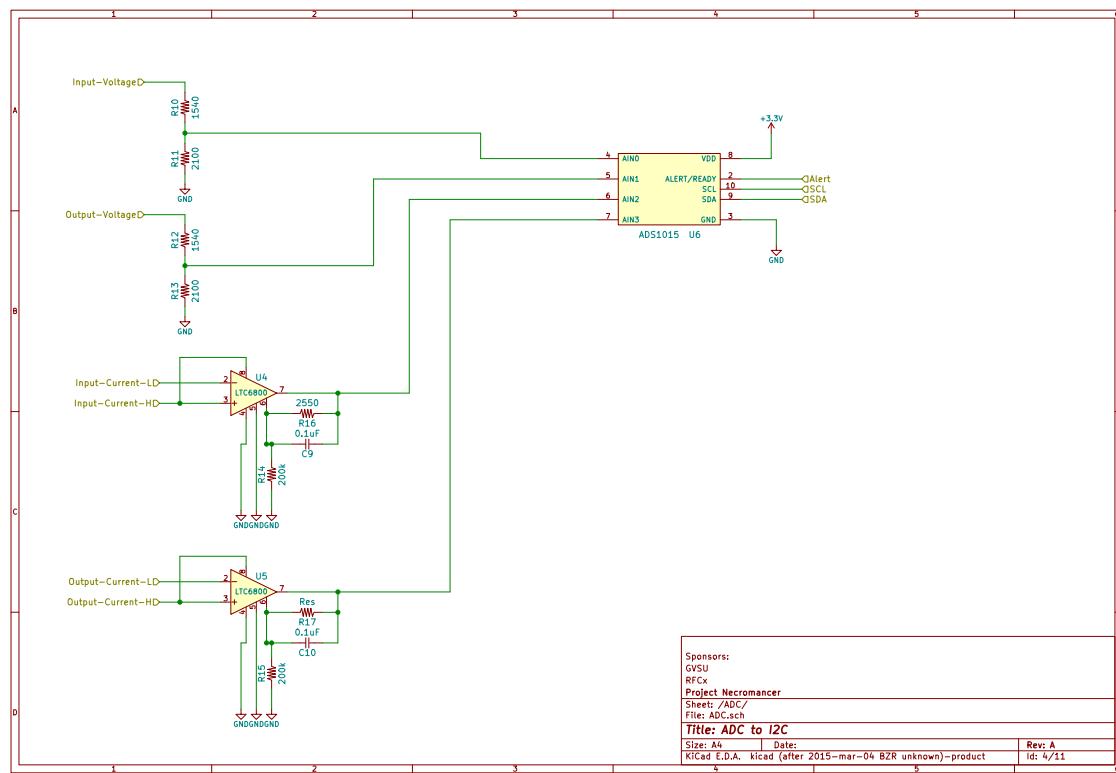


Figure A.4

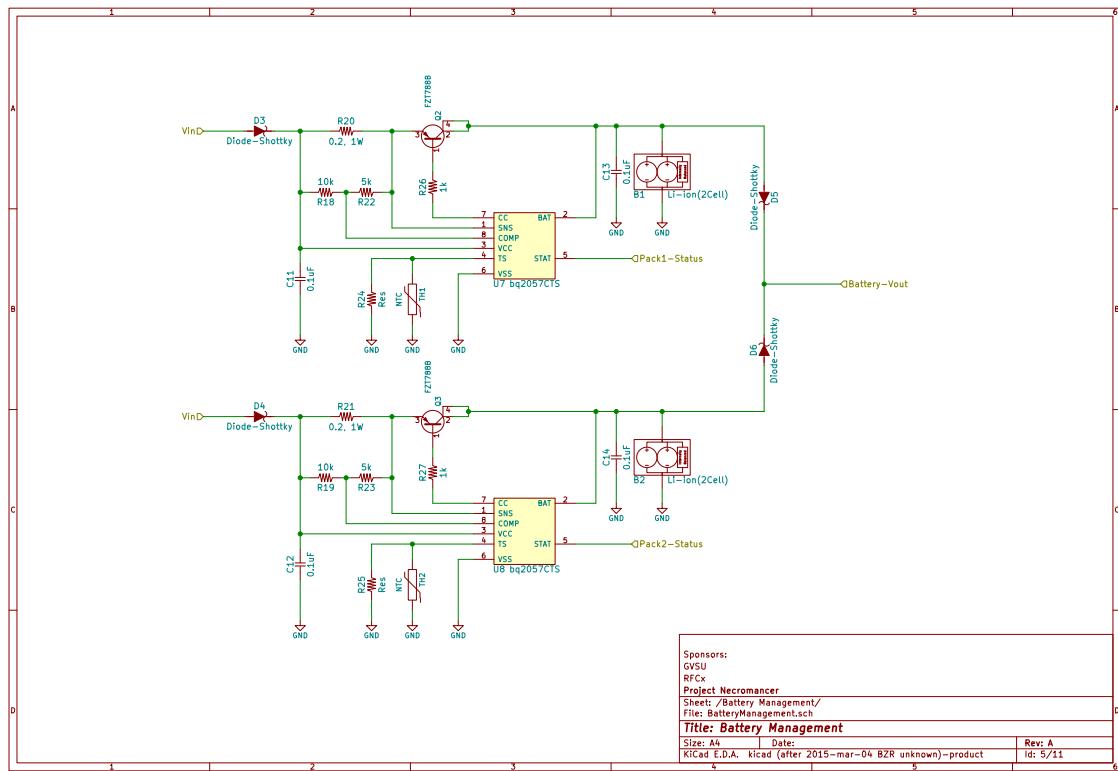


Figure A.5

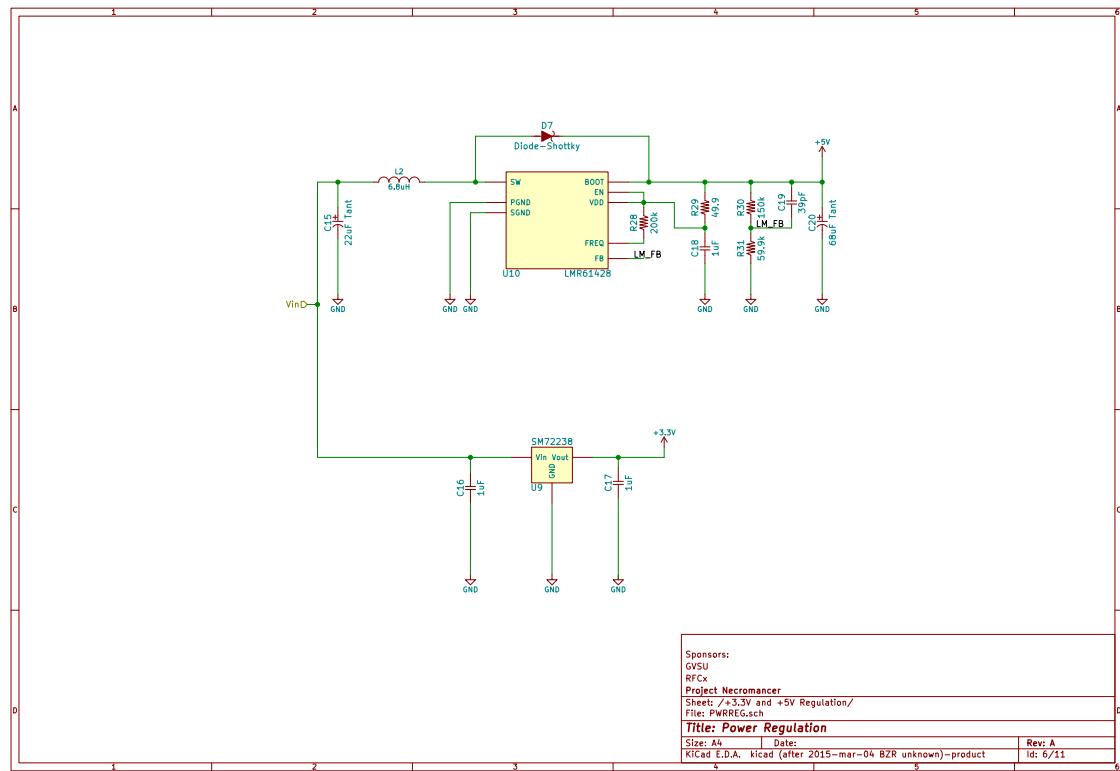


Figure A.6

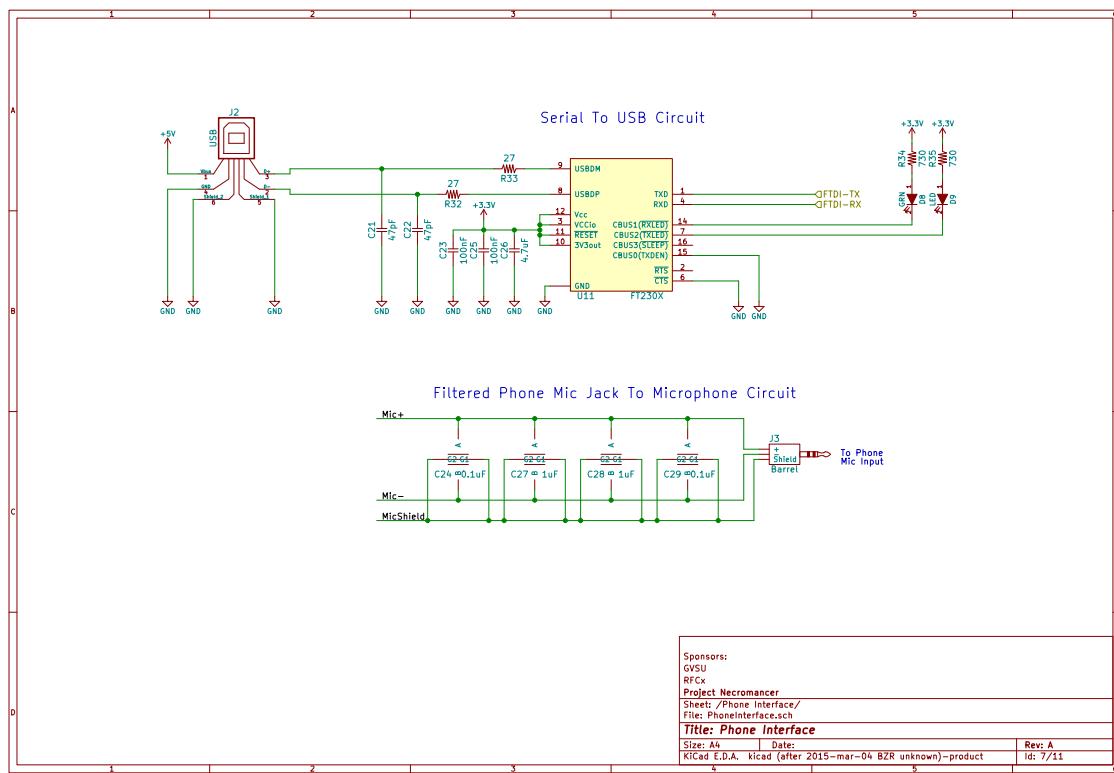


Figure A.7

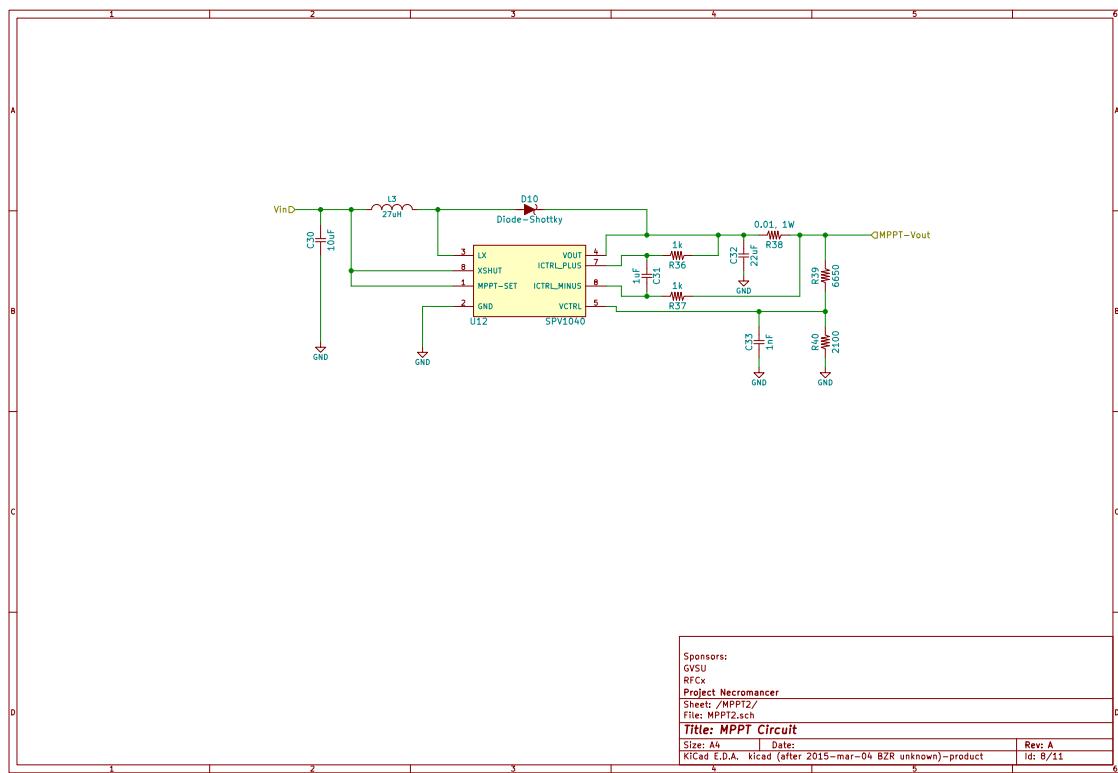


Figure A.8

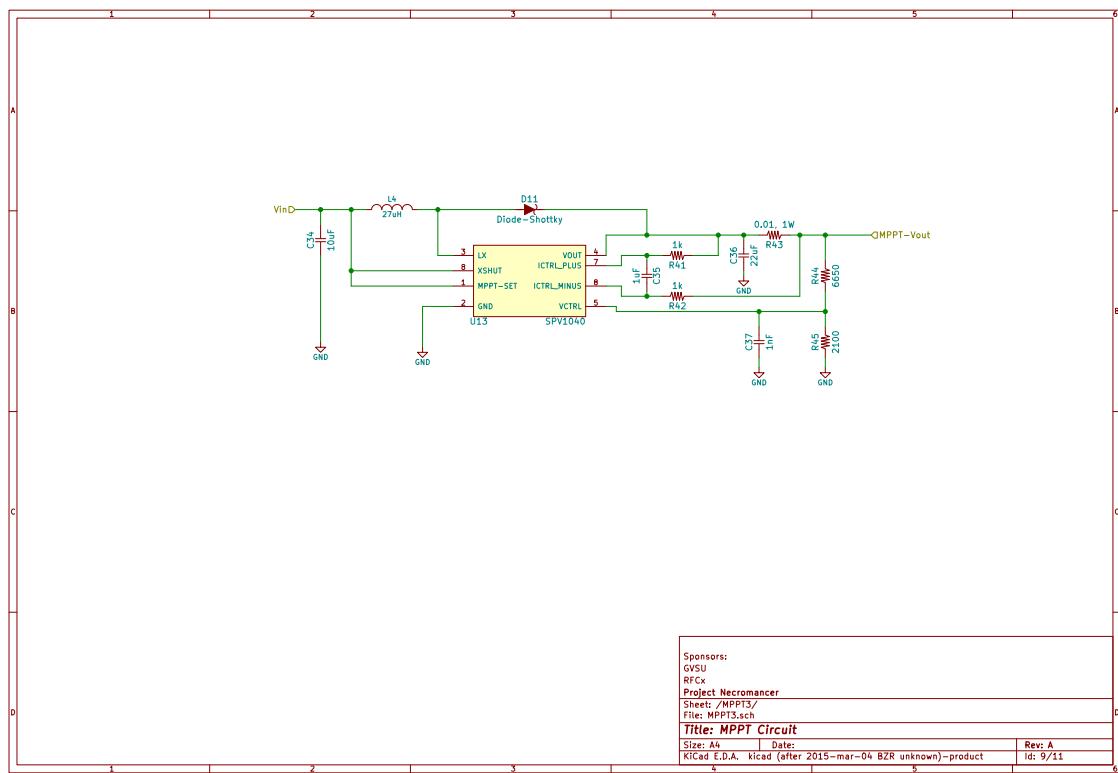


Figure A.9

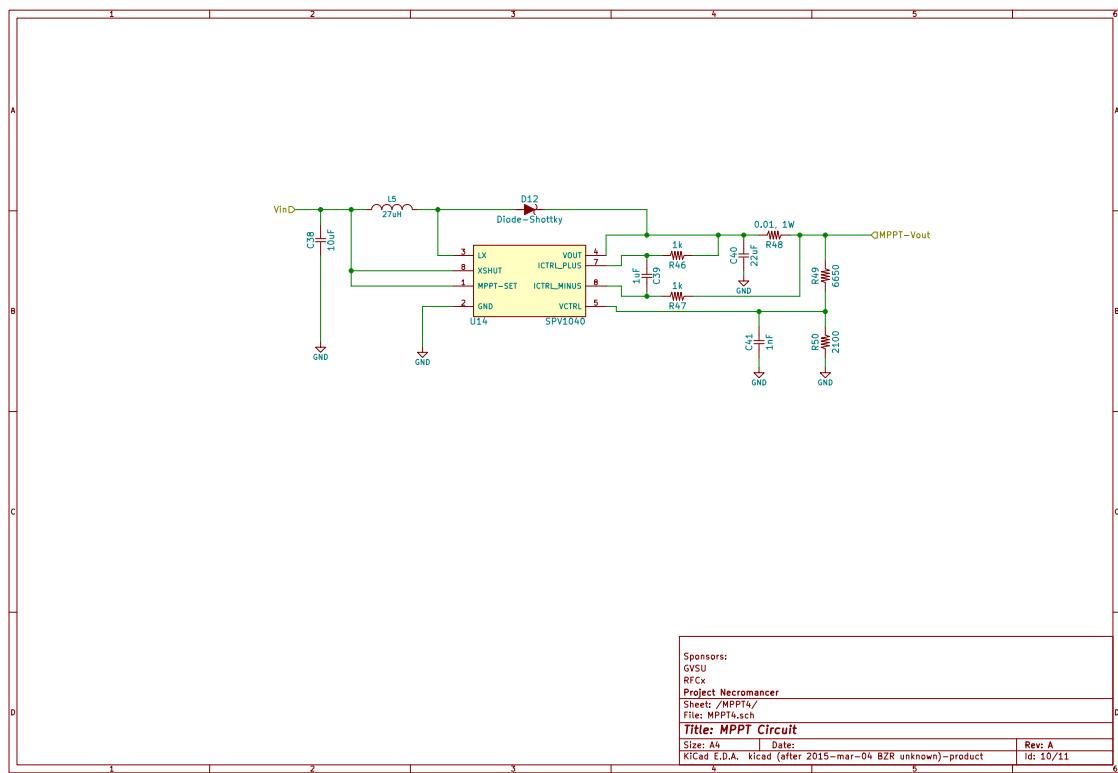


Figure A.10

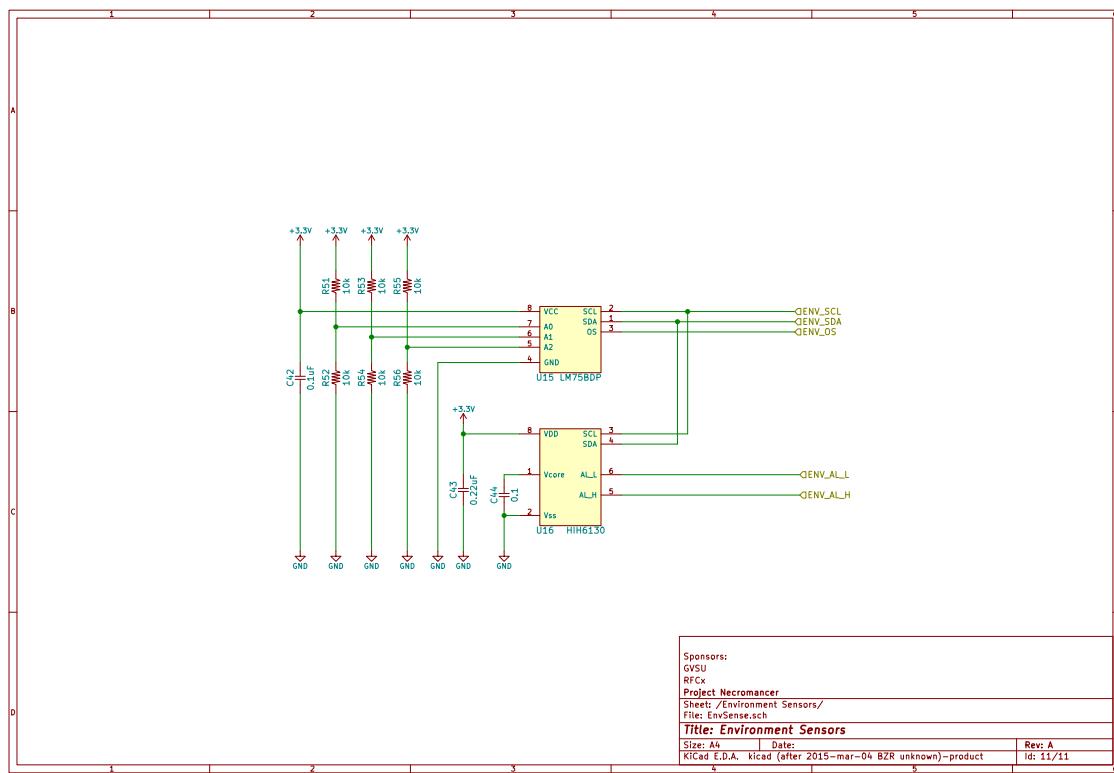


Figure A.11

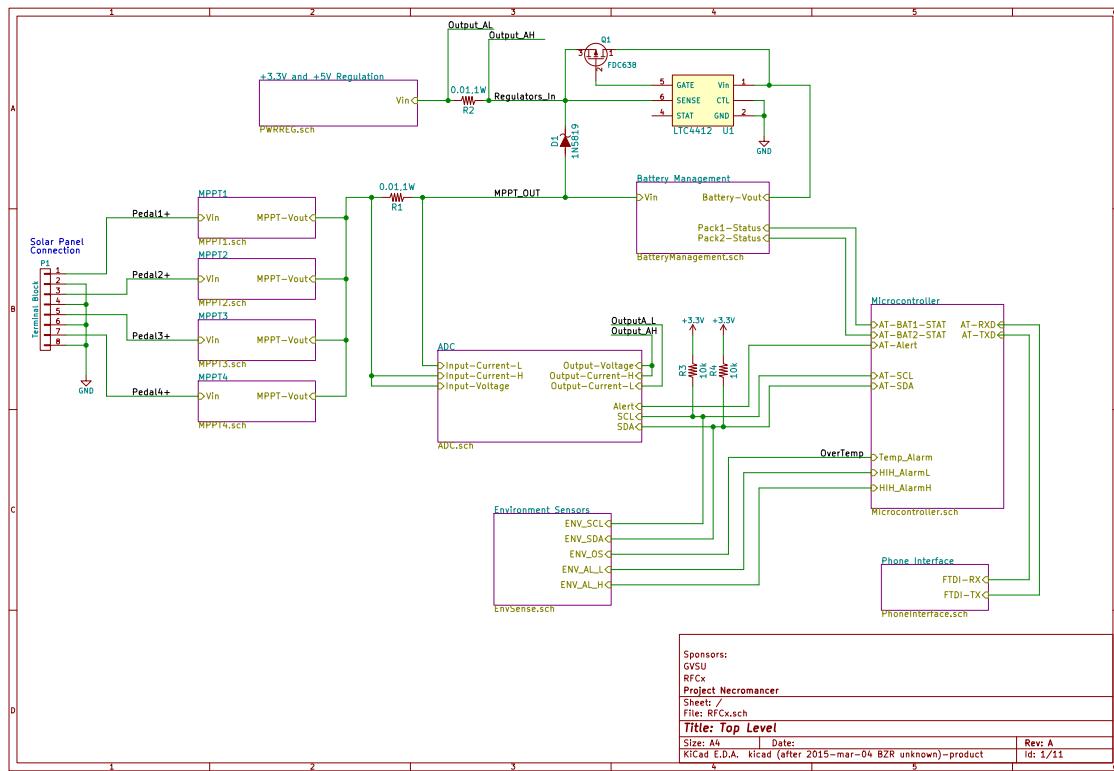


Figure A.12

Appendix B Bill Of Materials

RFCx_BOM

Project: RFCx
 Tool: kicad
 Number of Parts 145

| Reference | Quantity | Value | Distributor | Distributor # | Single Quantity Price | Extended Price |
|--|----------|-----------|-------------|------------------|-----------------------|----------------|
| Q1 | 1 | FDC638 | DigiKey | FDC638PCT-ND | \$0.55 | \$0.55 |
| C2,C4 | 2 | 10pF | DigiKey | 709-1168-1-ND | \$0.10 | \$0.20 |
| C3,C1,C6,C18,C17 ,C16,C31,C35,C39 | 9 | 1uF | DigiKey | 1276-1275-1-ND | \$0.10 | \$0.90 |
| C5,C30,C34,C38 | 4 | 10uF | DigiKey | 587-1312-1-ND | \$0.17 | \$0.68 |
| C7,C32,C36,C40 | 4 | 22uF | DigiKey | 1276-1822-1-ND | \$0.53 | \$2.12 |
| C8,C33,C37,C41 | 4 | 1nF | DigiKey | 399-1147-1-ND | \$0.10 | \$0.40 |
| C9,C10,C11,C13,C 12,C14,C29,C24,C 42,C25,C23,C44 | 12 | 0.1uF | DigiKey | 311-1245-1-ND | \$0.57 | \$6.84 |
| R20,R21 | 2 | 0.2, 1W | DigiKey | 989-1049-1-ND | \$0.61 | \$1.22 |
| Q2,Q3 | 2 | FZT788B | DigiKey | FZT788BCT-ND | \$1.01 | \$2.02 |
| C15 | 1 | 22uF Tant | DigiKey | 511-1506-1-ND | \$1.03 | \$1.03 |
| C19 | 1 | 39pF | DigiKey | 1276-1769-1-ND | \$0.10 | \$0.10 |
| C20 | 1 | 68uF Tant | DigiKey | 478-8414-1-ND | \$1.08 | \$1.08 |
| C26 | 1 | 4.7uF | DigiKey | 1276-1065-1-ND | \$0.21 | \$0.21 |
| C22,C21 | 2 | 47pF | DigiKey | 1276-1832-1-ND | \$0.10 | \$0.20 |
| C28,C27 | 2 | 1uF | DigiKey | 709-1108-1-ND | \$0.74 | \$1.48 |
| C43 | 1 | 0.22uF | DigiKey | 587-1287-1-ND | \$0.12 | \$0.12 |
| R1,R2,R7,R38,R43 ,R48 | 6 | 0.01,1W | DigiKey | RHM.010ASCT-ND | \$0.69 | \$4.14 |
| R3,R4,R18,R19,R5 2,R54,R56,R55,R5 3,R51 | 10 | 10k | DigiKey | P10KACT-ND | \$0.10 | \$1.00 |
| R5,R6,R26,R27,R3 6,R37,R41,R42,R4 6,R47 | 10 | 1k | DigiKey | P1.0KACT-ND | \$0.10 | \$1.00 |
| R8,R39,R44,R49 | 4 | 6650 | DigiKey | P6.65KCCT-ND | \$0.10 | \$0.40 |
| R9,R40,R45,R50,R 11,R13 | 6 | 2100 | DigiKey | P2.10KCCT-ND | \$0.10 | \$0.60 |
| R10,R12 | 2 | 1540 | DigiKey | P1.54KCCT-ND | \$0.10 | \$0.20 |
| R16,R17 | 2 | 2550 | DigiKey | 311-2.55KCRCT-ND | \$0.10 | \$0.20 |
| R14,R15,R28 | 3 | 200k | DigiKey | P200KACT-ND | \$0.10 | \$0.30 |
| R24,R25 | 2 | Res | NA | NA | \$0.00 | \$0.00 |
| R22,R23 | 2 | 5k | DigiKey | P4.99KCCT-ND | \$0.10 | \$0.20 |
| R29 | 1 | 49.9 | DigiKey | P49.9CCT-ND | \$0.10 | \$0.10 |
| R30 | 1 | 150k | DigiKey | P150KCCT-ND | \$0.10 | \$0.10 |
| R31 | 1 | 49.9k | DigiKey | P49.9KCCT-ND | \$0.10 | \$0.10 |
| D8 | 1 | GRN | DigiKey | 754-1939-1-ND | \$0.58 | \$0.58 |
| D9 | 1 | LED | DigiKey | 511-1293-1-ND | \$0.46 | \$0.46 |
| R34,R35 | 2 | 730 | DigiKey | P732CCT-ND | \$0.10 | \$0.20 |
| R33,R32 | 2 | 27 | DigiKey | P27ACT-ND | \$0.10 | \$0.20 |
| X1 | 1 | 32kHz | DigiKey | 300-8744-1-ND | \$1.18 | \$1.18 |

Page 1

Figure B.1

RFCx_BOM

| | | | | | |
|--------------------------------------|------------------|---------|-------------------|---------|---------|
| D2,D3,D4,D5,D6,D 7,D10,D11,D12,D1 | 10 1N5819 | DigiKey | 1N5819HW-FDICT-ND | \$0.52 | \$5.20 |
| L1,L3,L4,L5 | 4 27uH | DigiKey | SRR1260-270MCT-ND | \$0.99 | \$3.96 |
| L2 | 1 6.8uH | DigiKey | SRN6045-6R8YCT-ND | \$0.43 | \$0.43 |
| P1 | 1 Terminal Block | DigiKey | ED2615-ND | \$1.31 | \$1.31 |
| U1 | 1 LTC4412 | DigiKey | LTC4412ES6#TRPBFC | \$3.07 | \$3.07 |
| U2 | 1 ATmega328P | DigiKey | ATMEGA328P-AU-ND | \$3.58 | \$3.58 |
| J1 | 1 ICSP | DigiKey | S2011EC-03-ND | \$0.36 | \$0.36 |
| U3,U12,U13,U14 | 4 SPV1040 | DigiKey | NA | | \$0.00 |
| U4,U5 | 2 LTC6800 | DigiKey | LTC6800HMS8#PBF-N | \$3.12 | \$6.24 |
| U6 | 1 ADS1015 | DigiKey | 296-25227-1-ND | \$3.42 | \$3.42 |
| U7,U8 | 2 bq2057CTS | DigiKey | 296-25916-1-ND | \$1.91 | \$3.82 |
| B1,B2 | 2 Li-ion(2Cell) | NA | NA | | \$0.00 |
| TH1,TH2 | 2 NTC | DigiKey | BC2384-ND | \$1.54 | \$3.08 |
| U10 | 1 LMR61428 | DigiKey | LMR61428XMM/NOPB | \$1.87 | \$1.87 |
| U9 | 1 SM72238 | DigiKey | 296-39811-5-ND | \$1.67 | \$1.67 |
| U11 | 1 FT230X | DigiKey | 768-1135-1-ND | \$2.04 | \$2.04 |
| J2 | 1 USB | NA | NA | | \$0.00 |
| J3 | 1 Barrel | NA | NA | | \$0.00 |
| U15 | 1 LM75BDP | DigiKey | 568-4768-1-ND | \$0.62 | \$0.62 |
| U16 | 1 HIH6130 | DigiKey | 480-3651-1-ND | \$13.75 | \$13.75 |
| | | | TOTAL | | \$84.53 |

Appendix C Mechanical Drawings

Appendix D Calculations

D.1 bq2057CTS Battery Management Calculations

Current Regulation

$$R_{SNS} = \frac{V_{SNS}}{IO_{REG}} \quad (D.1)$$

$$= \frac{105mV}{0.2 \cdot 4400mAhr} \quad (D.2)$$

$$= 119m\Omega \quad (D.3)$$

Voltage Regulation

$$\frac{R_{B1}}{R_{B2}} = \left(N \cdot \frac{V_{CELL}}{V_{OREG}} \right) - 1 \quad (D.4)$$

Temperature Monitoring

Using PTC thermistor

External PNP Transistor

Max Power dissipation when battery is lowest (3V)

$$V_{in} = 5.2$$

$$I_{REG} = 880mA$$

$$V_{CS} = 0.176$$

$$V_D = 0.3$$

$$P_D = ((V_{in} - V_D - V_{CS}) - V_{BAT}) * I_{REG} \quad (D.5)$$

$$= (5.2 - 0.3 - 0.176 - 3) \cdot 0.88 \quad (D.6)$$

$$= 1.517W \quad (D.7)$$

Calculate β_{min}

$$\beta_{min} = \frac{I_{Cmax}}{I_B} \quad (D.8)$$

$$= \frac{0.88}{0.035} \quad (D.9)$$

$$= 25.14 \quad (D.10)$$

Input Capacitor

0.1 μ F Ceramic recommended on Vcc and Vss pins

Automatic Charge Rate Compensation

$$V(z) = 0.154 \quad (D.11)$$

$$V(comp) = \frac{0.154}{2.2} \quad (D.12)$$

$$= 0.07 \quad (D.13)$$

$$V(pack) = 4.2 + (2.2 \cdot 0.07) \quad (D.14)$$

$$= 4.354 \quad (D.15)$$

$$\frac{V_{comp}}{V_{sns}} = \frac{R_{comp2}}{R_{comp1} + R_{comp2}} \quad (D.16)$$

The data sheet recommended that R_{comp2} be $10k\Omega$ and that V_{sns} be $105mV$

$$R_{comp1} = \frac{R_{comp2} \cdot (V_{sns} - V_{comp})}{V_{comp}} \quad (\text{D.17})$$

$$R_{comp1} = \frac{10k \cdot (0.105 - 0.07)}{0.07} \quad (\text{D.18})$$

$$R_{comp1} = 5k\Omega \quad (\text{D.19})$$

D.2 Current and Voltage Sensing

Using the LTC6800 Output Voltage

$$V_{out} = \left(1 + \frac{R_2}{R_1}\right) \cdot V_{in} \quad (\text{D.20})$$

ADC Resolution 12-bit

$$\frac{3.3V}{2^{12}} = 805\mu V \quad (\text{D.21})$$

If 1A is drawn under worst case scenario and a sense resistor of $10m\Omega$ is chosen and the intended resolution is 1mA/bit:

$$R_{sense} = 0.01\Omega \quad (\text{D.22})$$

$$V_{sense} = 0.01V \quad (\text{D.23})$$

$$V_{ADC supply} = 3.3V \quad (\text{D.24})$$

$$Gain = \frac{V_{ADC supply}}{V_{sense}} \quad (\text{D.25})$$

$$= \frac{3.3}{0.01} \quad (\text{D.26})$$

$$= 330 \quad (\text{D.27})$$

$$3.3V/A \quad (\text{D.28})$$

$$\frac{805\mu V/Bit}{3.3} = \quad (\text{D.29})$$

$$= \quad (\text{D.30})$$

Appendix E Data Sheet Snippets

This appendix contains the 1st sheet of the data sheets for the parts used in this project.

TEXAS INSTRUMENTS

**ADS1013
ADS1014
ADS1015**

www.ti.com

SBAS473C – MAY 2009 – REVISED OCTOBER 2009

Ultra-Small, Low-Power, 12-Bit Analog-to-Digital Converter with Internal Reference

Check for Samples: **ADS1013 ADS1014 ADS1015**

| FEATURES | DESCRIPTION |
|--|--|
| <ul style="list-style-type: none"> • ULTRA-SMALL QFN PACKAGE: 2mm × 1.5mm × 0.4mm • WIDE SUPPLY RANGE: 2.0V to 5.5V • LOW CURRENT CONSUMPTION: Continuous Mode: Only 150µA Single-Shot Mode: Auto Shut-Down • PROGRAMMABLE DATA RATE: 128SPS to 3.3kSPS • INTERNAL LOW-DRIFT VOLTAGE REFERENCE • INTERNAL OSCILLATOR • INTERNAL PGA • I²CTM INTERFACE: Pin-Selectable Addresses • FOUR SINGLE-ENDED OR TWO DIFFERENTIAL INPUTS (ADS1015) • PROGRAMMABLE COMPARATOR (ADS1014 and ADS1015) | <p>The ADS1013, ADS1014, and ADS1015 are precision analog-to-digital converters (ADCs) with 12 bits of resolution offered in an ultra-small, leadless QFN-10 package or an MSOP-10 package. The ADS1013/4/5 are designed with precision, power, and ease of implementation in mind. The ADS1013/4/5 feature an onboard reference and oscillator. Data are transferred via an I²C-compatible serial interface; four I²C slave addresses can be selected. The ADS1013/4/5 operate from a single power supply ranging from 2.0V to 5.5V.</p> <p>The ADS1013/4/5 can perform conversions at rates up to 3300 samples per second (SPS). An onboard PGA is available on the ADS1014 and ADS1015 that offers input ranges from the supply to as low as ±256mV, allowing both large and small signals to be measured with high resolution. The ADS1015 also features an input multiplexer (MUX) that provides two differential or four single-ended inputs.</p> <p>The ADS1013/4/5 operate either in continuous conversion mode or a single-shot mode that automatically powers down after a conversion and greatly reduces current consumption during idle periods. The ADS1013/4/5 are specified from -40°C to +125°C.</p> |
| APPLICATIONS | <ul style="list-style-type: none"> • PORTABLE INSTRUMENTATION • CONSUMER GOODS • BATTERY MONITORING • TEMPERATURE MEASUREMENT • FACTORY AUTOMATION AND PROCESS CONTROLS |



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Figure E.1: 1st Page of ADS1013 Datasheet

Features

- High Performance, Low Power AVR® 8-Bit Microcontroller
- Advanced RISC Architecture
 - 131 Powerful Instructions – Most Single Clock Cycle Execution
 - 32 x 8 General Purpose Working Registers
 - Fully Static Operation
 - Up to 20 MIPS Throughput at 20 MHz
 - On-chip 2-cycle Multiplier
- High Endurance Non-volatile Memory Segments
 - 4/8/16/32K Bytes of In-System Self-Programmable Flash program memory (ATmega48PA/88PA/168PA/328P)
 - 256/512/1K Bytes EEPROM (ATmega48PA/88PA/168PA/328P)
 - 512/1K/1K/2K Bytes Internal SRAM (ATmega48PA/88PA/168PA/328P)
 - Write/Erase Cycles: 10,000 Flash/100,000 EEPROM
 - Data retention: 20 years at 85°C/100 years at 25°C⁽¹⁾
 - Optional Boot Code Section with Independent Lock Bits
 - In-System Programming by On-chip Boot Program
 - True Read-While-Write Operation
 - Programming Lock for Software Security
- Peripheral Features
 - Two 8-bit Timer/Counters with Separate Prescaler and Compare Mode
 - One 16-bit Timer/Counter with Separate Prescaler, Compare Mode, and Capture Mode
 - Real Time Counter with Separate Oscillator
 - Six PWM Channels
 - 8-channel 10-bit ADC in TQFP and QFN/MLF package
 - Temperature Measurement
 - 6-channel 10-bit ADC in PDIP Package
 - Temperature Measurement
 - Programmable Serial USART
 - Master/Slave SPI Serial Interface
 - Byte-oriented 2-wire Serial Interface (Philips I²C compatible)
 - Programmable Watchdog Timer with Separate On-chip Oscillator
 - On-chip Analog Comparator
 - Interrupt and Wake-up on Pin Change
- Special Microcontroller Features
 - Power-on Reset and Programmable Brown-out Detection
 - Internal Calibrated Oscillator
 - External and Internal Interrupt Sources
 - Six Sleep Modes: Idle, ADC Noise Reduction, Power-save, Power-down, Standby, and Extended Standby
- I/O and Packages
 - 23 Programmable I/O Lines
 - 28-pin PDIP, 32-lead TQFP, 28-pad QFN/MLF and 32-pad QFN/MLF
- Operating Voltage:
 - 1.8 - 5.5V for ATmega48PA/88PA/168PA/328P
- Temperature Range:
 - -40°C to 85°C
- Speed Grade:
 - 0 - 20 MHz @ 1.8 - 5.5V
- Low Power Consumption at 1 MHz, 1.8V, 25°C for ATmega48PA/88PA/168PA/328P:
 - Active Mode: 0.2 mA
 - Power-down Mode: 0.1 A
 - Power-save Mode: 0.75 A (Including 32 kHz RTC)



**8-bit AVR®
Microcontroller
with 4/8/16/32K
Bytes In-System
Programmable
Flash**

**ATmega48PA
ATmega88PA
ATmega168PA
ATmega328P**

Rev. 8161D-AVR-10/09



Figure E.2: 1st Page of ATmega328P Datasheet



bq2057, bq2057C
bq2057T, bq2057W

SLUS025F – MAY 2001 – REVISED JULY 2002

ADVANCED LINEAR CHARGE MANAGEMENT IC FOR SINGLE- AND TWO-CELL LITHIUM-ION AND LITHIUM-POLYMER

FEATURES

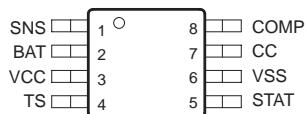
- Ideal for Single (4.1 V or 4.2 V) and Dual-Cell (8.2 V or 8.4 V) Li-Ion or Li-Pol Packs
- Requires Small Number of External Components
- 0.3 V Dropout Voltage for Minimizing Heat Dissipation
- Better Than $\pm 1\%$ Voltage Regulation Accuracy With Preset Voltages
- AutoComp™ Dynamic Compensation of Battery Pack's Internal Impedance to Reduce Charge Time
- Optional Cell-Temperature Monitoring Before and During Charge
- Integrated Voltage and Current Regulation With Programmable Charge-Current and High- or Low-Side Current Sensing
- Integrated Cell Conditioning for Reviving Deeply Discharged Cells and Minimizing Heat Dissipation During Initial Stage Of Charge
- Charge Status Output for Single or Dual Led or Host Processor Interface
- Automatic Battery-Recharge Feature
- Charge Termination by Minimum Current
- Automatic Low-Power Sleep Mode When V_{CC} Is Removed
- EVMs Available for Quick Evaluation
- Packaging: 8-Pin SOIC, 8-Pin TSSOP, 8-Pin MSOP

DESCRIPTION

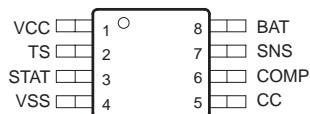
The BENCHMARQ bq2057 series advanced Lithium-Ion (Li-Ion) and Lithium-Polymer (Li-Pol) linear charge-management ICs are designed for cost-sensitive and compact portable electronics. They combine high-accuracy current and voltage regulation, battery conditioning, temperature monitoring, charge termination, charge-status indication, and AutoComp charge-rate compensation in a single 8-pin IC. MSOP, TSSOP, and SOIC package options are offered to fit a wide range of end applications.

The bq2057 continuously measures battery temperature using an external thermistor. For safety, the bq2057 inhibits charge until the battery temperature is within user-defined thresholds. The bq2057 then charges the battery in three phases: conditioning, constant current, and constant voltage. If the battery voltage is below the low-voltage threshold, V_(min), the bq2057 precharges using a low current to condition the battery. The conditioning charge rate is approximately 10% of the regulation current. The conditioning current also minimizes heat dissipation in the external pass-element during the initial stage of the charge. After conditioning, the bq2057 applies a constant current to the battery. An external sense-resistor sets the current. The sense-resistor can be on either the high or low side of the battery without additional components. The constant-current phase continues until the battery reaches the charge-regulation voltage.

bq2057xSN or bq2057xTS
SOIC (SN) or TSSOP (TS) PACKAGE
(TOP VIEW)



bq2057xDGK
MSOP (DGK) PACKAGE
(TOP VIEW)



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TEXAS INSTRUMENTS
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1

Figure E.3: 1st Page of bq2057 Datasheet

SOT223 PNP SILICON PLANAR MEDIUM POWER HIGH GAIN TRANSISTOR

ISSUE 3 - OCTOBER 1995

FZT788B

FEATURES

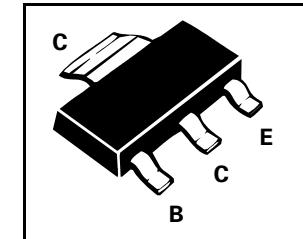
- * Low equivalent on-resistance; $R_{CE(sat)}$ 93m Ω at 3A
- * Gain of 300 at $I_C=2$ Amps and Very low saturation voltage

APPLICATIONS

- * Battery powered circuits

COMPLEMENTARY TYPE – FZT688B

PARTMARKING DETAIL – FZT788B



ABSOLUTE MAXIMUM RATINGS.

| PARAMETER | SYMBOL | VALUE | UNIT |
|---|----------------|-------------|------|
| Collector-Base Voltage | V_{CBO} | -15 | V |
| Collector-Emitter Voltage | V_{CEO} | -15 | V |
| Emitter-Base Voltage | V_{EBO} | -5 | V |
| Peak Pulse Current | I_{CM} | -8 | A |
| Continuous Collector Current | I_C | -3 | A |
| Power Dissipation at $T_{amb}=25^\circ\text{C}$ | P_{tot} | 2 | W |
| Operating and Storage Temperature Range | $T_j; T_{stg}$ | -55 to +150 | °C |

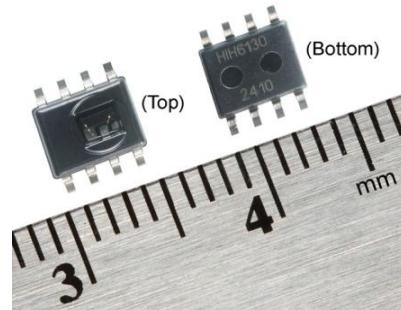
ELECTRICAL CHARACTERISTICS (at $T_{amb}=25^\circ\text{C}$)

| PARAMETER | SYMBOL | MIN. | TYP. | MAX. | UNIT | CONDITIONS. |
|---------------------------------------|-----------------------|--------------------------|-----------|---------------------------------|---------------|--|
| Collector-Base Breakdown Voltage | $V_{(BR)CBO}$ | -15 | | | V | $I_C=100\mu\text{A}$ |
| Collector-Emitter Breakdown Voltage | $V_{(BR)CEO}$ | -15 | | | V | $I_C=10\text{mA}^*$ |
| Emitter-Base Breakdown Voltage | $V_{(BR)EBO}$ | -5 | | | V | $I_E=100\mu\text{A}$ |
| Collector Cut-Off Current | I_{CBO} | | | -0.1 | μA | $V_{CB}=-10\text{V}$ |
| Emitter Cut-Off Current | I_{EBO} | | | -0.1 | μA | $V_{EB}=-4\text{V}$ |
| Collector-Emitter Saturation Voltage | $V_{CE(sat)}$ | | | -0.15 -0.25 -0.45 -0.5 | V | $I_C=0.5\text{A}, I_B=2.5\text{mA}^*$ $I_C=1\text{A}, I_B=5\text{mA}^*$ $I_C=2\text{A}, I_B=10\text{mA}^*$ $I_C=3\text{A}, I_B=50\text{mA}^*$ |
| Base-Emitter Saturation Voltage | $V_{BE(sat)}$ | | | -0.9 | V | $I_C=1\text{A}, I_B=5\text{mA}^*$ |
| Base-Emitter Turn-On Voltage | $V_{BE(on)}$ | | -0.75 | | V | $I_C=1\text{A}, V_{CE}=-2\text{V}^*$ |
| Static Forward Current Transfer Ratio | h_{FE} | 500 400 300 150 | | 1500 | | $I_C=10\text{mA}, V_{CE}=-2\text{V}^*$ $I_C=1\text{A}, V_{CE}=-2\text{V}^*$ $I_C=2\text{A}, V_{CE}=-2\text{V}^*$ $I_C=6\text{A}, V_{CE}=-2\text{V}^*$ |
| Transition Frequency | f_T | 100 | | | MHz | $I_C=50\text{mA}, V_{CE}=-5\text{V}$ $f=50\text{MHz}$ |
| Input Capacitance | C_{ibo} | | 225 | | pF | $V_{EB}=-0.5\text{V}, f=1\text{MHz}$ |
| Output Capacitance | C_{obo} | | 25 | | pF | $V_{CB}=-10\text{V}, f=1\text{MHz}$ |
| Switching Times | t_{on} t_{off} | | 35 400 | | ns | $I_C=500\text{mA}, I_{B1}=50\text{mA}$ $I_{B2}=-50\text{mA}, V_{CC}=-10\text{V}$ |

*Measured under pulsed conditions. Pulse width=300μs. Duty cycle ≤2%
Spice parameter data is available upon request for this device

Honeywell

Honeywell HumidIcon™ Digital Humidity/Temperature Sensors: HIH-6130/6131 Series



DESCRIPTION (★ = competitive differentiator)

Honeywell HumidIcon™ Digital Humidity/Temperature Sensors: HIH-6130/6131 Series, is a digital output-type relative humidity (RH) and temperature sensor combined in the same package. These devices offer several competitive advantages, including:

- Industry-leading Total Error Band
- Industry-leading stability
- Industry-leading reliability
- Lowest total cost solution
- True temperature-compensated digital I²C output
- Energy efficiency
- Ultra-small package

★ Industry-leading Total Error Band (TEB) (±5 %RH):

Honeywell specifies Total Error Band—the most comprehensive, clear, and meaningful measurement—that provides the sensor's true accuracy of ±5 %RH over a compensated range of 5 °C to 50 °C [41 °F to 122 °F] and 10 %RH to 90 %RH. TEB includes all errors due to:

- Humidity non-linearity
- Humidity hysteresis
- Humidity non-repeatability
- Thermal effect on zero
- Thermal effect on span
- Thermal hysteresis

Total Error Band should not be confused with "Accuracy", which is actually a component of Total Error Band. Many competitors simply specify the accuracy of their device; however, the specification may exclude hysteresis and temperature effects, and may be calculated over a very narrow range, at only one point in the range, or at their absolute best accuracy level. It is then up to the customer to calibrate the device to make sure it has the accuracy needed for the life of the application.

Honeywell's industry-leading Total Error Band provides the following benefits to the customer:

- Eliminates individually testing and calibrating every sensor, which can increase their manufacturing time and process
- Supports system accuracy and warranty requirements
- Helps to optimize system uptime
- Provides excellent sensor interchangeability—the customer can remove one sensor from the tape, remove the next sensor from the tape, and there is no part-to-part variation in accuracy

For more information about Total Error Band, please see the related Technical Note "Explanation of the Total Error Band Specification for Honeywell's Digital Humidity/Temperature Sensors."

★ Industry-leading long term stability (1.2 %RH over five years):

Competitive humidity sensors need to go through a 12 hour at 75 %RH rehydration process (which requires special equipment chambers) to correct reflow temperature offset. Honeywell's sensor also experiences an offset after reflow; however, it only requires a five hour rehydration under ambient conditions (>50 %RH). Honeywell's industry-leading long term stability provides the following benefits to the customer:

- Minimizes system performance issues
- Helps support system uptime by eliminating the need to service or replace the sensor during its application life
- Eliminates the need to regularly recalibrate the sensor in their application, which can be inconvenient and costly

★ Industry-leading reliability:

Honeywell's new HIH-6130/6131 Series sensors use a laser trimmed, thermoset polymer capacitive sensing element. The element's multilayer construction provides resistance to most application hazards such as condensation, dust, dirt, oils, and common environmental chemicals which help provide industry-leading stability and reliability.

Figure E.5: 1st Page of HIH6130 Datasheet



Specification No. APL-2013517

Edition No. 1.0

Cylindrical Li — ion Battery Pack

Product Specification

Model: 18650 3.7v 4400mAh

Hunan Sounddon New Energy Co., Ltd

Address:No.98, Fuzhou Road,Jinhua Demonstration Area,Xiangtan City,Hunan Province,China.

<http://www.soundnewenergy.com>

Tel: (86) 731 - 5856 7126

Fax: (86) 731 - 5823 6346

E-mail:linda.ding@soundnewenergy.com

Prepared by: Liu Li

Checked by: Zhu Qiang

Approve by: Xiao Linping

All 10 Sheets

Figure E.6: 1st Page of Li-Ion Battery Pack Datasheet



LM75B

Digital temperature sensor and thermal watchdog

Rev. 6.1 — 6 February 2015

Product data sheet

1. General description

The LM75B is a temperature-to-digital converter using an on-chip band gap temperature sensor and Sigma-Delta A-to-D conversion technique with an overtemperature detection output. The LM75B contains a number of data registers: Configuration register (Conf) to store the device settings such as device operation mode, OS operation mode, OS polarity and OS fault queue as described in [Section 7 "Functional description"](#); temperature register (Temp) to store the digital temp reading, and set-point registers (Tos and Thyst) to store programmable overtemperature shutdown and hysteresis limits, that can be communicated by a controller via the 2-wire serial I²C-bus interface. The device also includes an open-drain output (OS) which becomes active when the temperature exceeds the programmed limits. There are three selectable logic address pins so that eight devices can be connected on the same bus without address conflict.

The LM75B can be configured for different operation conditions. It can be set in normal mode to periodically monitor the ambient temperature, or in shutdown mode to minimize power consumption. The OS output operates in either of two selectable modes: OS comparator mode or OS interrupt mode. Its active state can be selected as either HIGH or LOW. The fault queue that defines the number of consecutive faults in order to activate the OS output is programmable as well as the set-point limits.

The temperature register always stores an 11-bit two's complement data giving a temperature resolution of 0.125 °C. This high temperature resolution is particularly useful in applications of measuring precisely the thermal drift or runaway. When the LM75B is accessed the conversion in process is not interrupted (that is, the I²C-bus section is totally independent of the Sigma-Delta converter section) and accessing the LM75B continuously without waiting at least one conversion time between communications will not prevent the device from updating the Temp register with a new conversion result. The new conversion result will be available immediately after the Temp register is updated.

The LM75B powers up in the normal operation mode with the OS in comparator mode, temperature threshold of 80 °C and hysteresis of 75 °C, so that it can be used as a stand-alone thermostat with those pre-defined temperature set points.

2. Features and benefits

- Pin-for-pin replacement for industry standard LM75 and LM75A and offers improved temperature resolution of 0.125 °C and specification of a single part over power supply range from 2.8 V to 5.5 V
- I²C-bus interface with up to 8 devices on the same bus
- Power supply range from 2.8 V to 5.5 V
- Temperatures range from -55 °C to +125 °C



Figure E.7: 1st Page of LM75B Datasheet



LMR61428

www.ti.com

SNVS815A – JUNE 2012 – REVISED APRIL 2013

LMR61428 SIMPLE SWITCHER® 14Vout, 2.85A Step-Up Voltage Regulator in VSSOP

Check for Samples: [LMR61428](#)

FEATURES

- 1.2V to 14V Input Voltage
- Adjustable Output Voltage up to 14V
- Switch Current up to 2.85A
- Up to 2 MHz Switching Frequency
- Low Shutdown I_Q , <1 μ A
- Cycle-by-Cycle Current Limiting
- VSSOP Packaging (3.0 x 5.0 x 1.09mm)
- WEBENCH® Enabled

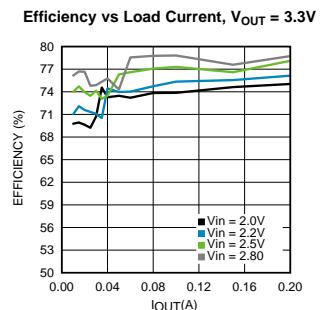
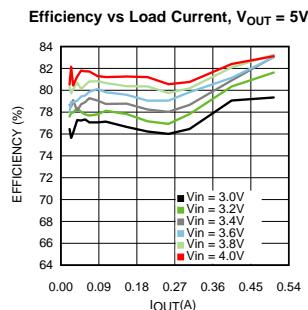
PERFORMANCE BENEFITS

- Extremely Easy to Use
- Tiny Overall Solution Reduces System Cost

APPLICATIONS

- Boost/SEPIC Conversions from 3.3V, 5V, and 12V
- Space Constrained Applications
- LCD Displays
- LED Applications

System Performance



DESCRIPTION

The LMR61428 is a step-up DC-DC switching regulator for battery-powered and low input voltage systems that can achieve efficiencies up to 90%. It has a wide input voltage range from 1.2V to 14V and a possible regulated output voltage range of 1.24V to 14V. It has an internal 0.17 Ω N-Channel MOSFET power switch.

The high switching frequency of up to 2MHz of the LMR61428 allows for tiny surface mount inductors and capacitors. Because of the unique constant-duty-cycle gated oscillator topology very high efficiencies are realized over a wide load range. The supply current is reduced to 80 μ A because of the BiCMOS process technology. In the shutdown mode, the supply current is less than 2.5 μ A. The LMR61428 is available in a VSSOP-8 package.

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Figure E.8: 1st Page of LMR61428 Datasheet



LTC4412

Low Loss PowerPath™
Controller in ThinSOT

FEATURES

- Very Low Loss Replacement for Power Supply OR'ing Diodes
- Minimal External Components
- Automatic Switching Between DC Sources
- Simplifies Load Sharing with Multiple Batteries
- Low Quiescent Current: 11µA
- 3V to 28V AC/DC Adapter Voltage Range
- 2.5V to 28V Battery Voltage Range
- Reverse Battery Protection
- Drives Almost Any Size MOSFET for Wide Range of Current Requirements
- MOSFET Gate Protection Clamp
- Manual Control Input
- Low Profile (1mm) ThinSOT™ Package

APPLICATIONS

- Cellular Phones
- Notebook and Handheld Computers
- Digital Cameras
- USB-Powered Peripherals
- Uninterruptible Power Supplies
- Logic Controlled Power Switch

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DESCRIPTION

The LTC®4412 controls an external P-channel MOSFET to create a near ideal diode function for power switchover or load sharing. This permits highly efficient OR'ing of multiple power sources for extended battery life and low self-heating. When conducting, the voltage drop across the MOSFET is typically 20mV. For applications with a wall adapter or other auxiliary power source, the load is automatically disconnected from the battery when the auxiliary source is connected. Two or more LTC4412s may be interconnected to allow load sharing between multiple batteries or charging of multiple batteries from a single charger.

The wide supply operating range supports operation from one to six Li-Ion cells in series. The low quiescent current (11µA typical) is independent of the load current. The gate driver includes an internal voltage clamp for MOSFET protection.

The STAT pin can be used to enable an auxiliary P-channel MOSFET power switch when an auxiliary supply is detected. This pin may also be used to indicate to a microcontroller that an auxiliary supply is connected. The control (CTL) input enables the user to force the primary MOSFET off and the STAT pin low.

The LTC4412 is available in a low profile (1mm) ThinSOT package.

TYPICAL APPLICATION

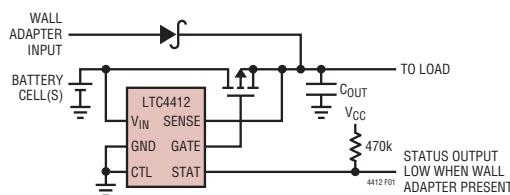
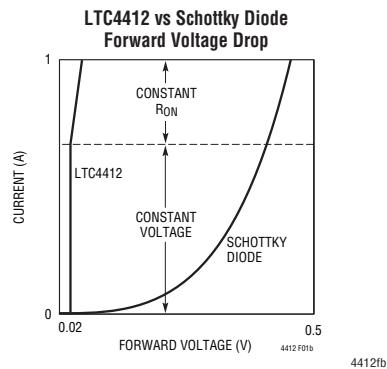


Figure 1. Automatic Switchover of Load Between a Battery and a Wall Adapter



For more information www.linear.com/LTC4412

1

Figure E.9: 1st Page of LTC4412 Datasheet



LTC6800

Rail-to-Rail,
Input and Output,
Instrumentation Amplifier

FEATURES

- 116dB CMRR Independent of Gain
- Maximum Offset Voltage: 100 μ V
- Maximum Offset Voltage Drift: 250nV/ $^{\circ}$ C
- -40 $^{\circ}$ C to 125 $^{\circ}$ C Operation
- Rail-to-Rail Input Range
- Rail-to-Rail Output Swing
- Supply Operation: 2.7V to 5.5V
- Available in MS8 and 3mm x 3mm x 0.8mm DFN Packages

APPLICATIONS

- Thermocouple Amplifiers
- Electronic Scales
- Medical Instrumentation
- Strain Gauge Amplifiers
- High Resolution Data Acquisition

DESCRIPTION

The LTC[®]6800 is a precision instrumentation amplifier. The CMRR is typically 116dB with a single 5V supply and is independent of gain. The input offset voltage is guaranteed below 100 μ V with a temperature drift of less than 250nV/ $^{\circ}$ C. The LTC6800 is easy to use; the gain is adjustable with two external resistors, like a traditional op amp.

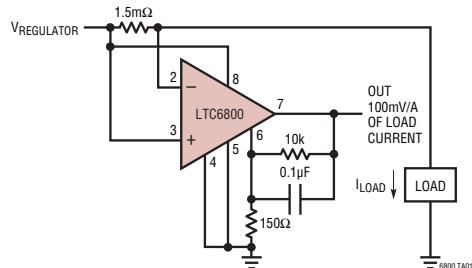
The LTC6800 uses charge balanced sampled data techniques to convert a differential input voltage into a single ended signal that is in turn amplified by a zero-drift operational amplifier.

The differential inputs operate from rail-to-rail and the single ended output swings from rail-to-rail. The LTC6800 is available in an MS8 surface mount package. For space limited applications, the LTC6800 is available in a 3mm x 3mm x 0.8mm dual fine pitch leadless package (DFN).

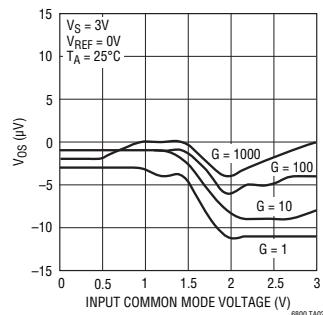
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TYPICAL APPLICATION

High Side Power Supply Current Sense



Typical Input Referred Offset vs Input Common Mode Voltage ($V_S = 3V$)



6800fb



1

Figure E.10: 1st Page of LTC6800 Datasheet



SM72238

www.ti.com

SNVS694C –JANUARY 2011–REVISED APRIL 2013

Micropower Voltage Regulator

Check for Samples: [SM72238](#)

FEATURES

- Renewable Energy Grade
- High-Accuracy Output Voltage
- Ensured 100mA Output Current
- Extremely Low Quiescent Current
- Low Dropout Voltage
- Extremely Tight Load and Line Regulation
- Very Low Temperature Coefficient
- Use as Regulator or Reference
- Needs Minimum Capacitance for Stability
- Current and Thermal Limiting
- Stable With Low-ESR Output Capacitors (10mΩ to 6Ω)

DESCRIPTION

The SM72238 is a micropower voltage regulator with very low quiescent current (75µA typ.) and very low dropout voltage (typ. 40mV at light loads and 380mV at 100mA). It is ideally suited for use in battery-powered systems. Furthermore, the quiescent current of the SM72238 increases only slightly in dropout, prolonging battery life.

The SM72238 is available in the surface-mount D-Pak package.

Careful design of the SM72238 has minimized all contributions to the error budget. This includes a tight initial tolerance (.5% typ.), extremely good load and line regulation (.05% typ.) and a very low output voltage temperature coefficient, making the part useful as a low-power voltage reference.

Block Diagram and Typical Applications

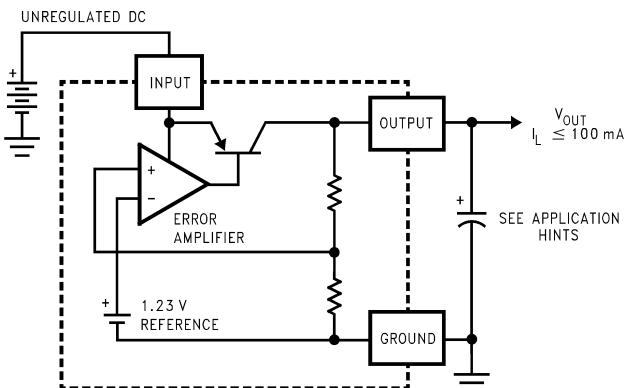


Figure 1. SM72238



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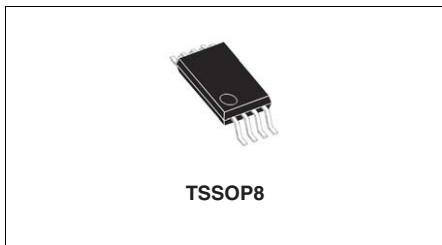
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Figure E.11: 1st Page of SM72238 Datasheet

**SPV1040**

High efficiency solar battery charger with embedded MPPT

Datasheet - production data



TSSOP8

Features

- 0.3 V to 5.5 V operating input voltage
- 140 mΩ internal synchronous rectifier
- 120 mΩ internal power active switch
- 100 kHz fixed PWM frequency
- Duty cycle controlled by MPPT algorithm
- Output voltage regulation, overcurrent and overtemperature protection
- Input source reverse polarity protection
- Built-in soft-start
- Up to 95% efficiency
- 3 mm x 4.4 mm TSSOP8 package

Applications

- Smart phones and GPS systems
- Wireless headsets
- Small appliances, sensors
- Portable media players
- Digital still cameras
- Toys and portable healthcare

Description

The SPV1040 device is a low power, low voltage, monolithic step-up converter with an input voltage range from 0.3 V to 5.5 V, and is capable of maximizing the energy generated by even a single solar cell (or fuel cell), where low input voltage handling capability is extremely important.

Thanks to the embedded MPPT algorithm, even under varying environmental conditions (such as irradiation, dirt, temperature) the SPV1040 offers maximum efficiency in terms of power harvested from the cells and transferred to the output.

The device employs an input voltage regulation loop, which fixes the charging battery voltage via a resistor divider. The maximum output current is set with a current sense resistor according to charging current requirements.

The SPV1040 protects itself and other application devices by stopping the PWM switching if either the maximum current threshold (up to 1.8 A) is reached or the maximum temperature limit (up to 155 °C) is exceeded.

An additional built-in feature of the SPV1040 is the input source reverse polarity protection, which prevents damage in case of reverse connection of the solar panel at the input.

Table 1. Device summary

| Order code | Package | Packaging |
|------------|---------|---------------|
| SPV1040T | TSSOP8 | Tube |
| SPV1040TTR | | Tape and reel |

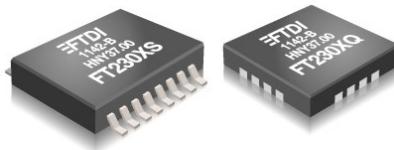


Future Technology Devices International Ltd.

FT230X (USB to BASIC UART IC)

The FT230X is a USB to serial UART interface with optimised pin count for smaller PCB designs and the following advanced features:

- Single chip USB to asynchronous serial data transfer interface.
- Entire USB protocol handled on the chip. No USB specific firmware programming required.
- Fully integrated 2048 byte multi-time-programmable (MTP) memory, storing device descriptors and CBUS I/O configuration.
- Fully integrated clock generation with no external crystal required plus optional clock output selection enabling a glue-less interface to external MCU or FPGA.
- Data transfer rates from 300 baud to 3 Mbaud (RS422, RS485, and RS232) at TTL levels.
- 512 byte receive buffer and 512 byte transmit buffer utilising buffer smoothing technology to allow for high data throughput.
- FTDI's royalty-free Virtual Com Port (VCP) and Direct (D2XX) drivers eliminate the requirement for USB driver development in most cases.
- Configurable CBUS I/O pins.
- Transmit and receive LED drive signals.
- UART interface support for 7 or 8 data bits, 1 or 2 stop bits and odd / even / mark / space / no parity
- Synchronous and asynchronous bit bang interface options with RD# and WR# strobes.
- USB Battery Charger Detection. Allows for USB peripheral devices to detect the presence of a higher power source to enable improved charging.
- Device supplied pre-programmed with unique USB serial number.
- USB Power Configurations; supports bus-powered, self-powered and bus-powered with power switching
- Integrated +3.3V level converter for USB I/O.
- True 3.3V CMOS drive output and TTL input; operates down to 1V8 with external pull ups. Tolerant of 5V input
- Configurable I/O pin output drive strength; 4 mA (min) and 16 mA (max).
- Integrated power-on-reset circuit.
- Fully integrated AVCC supply filtering - no external filtering required.
- UART signal inversion option.
- +5V Single Supply Operation.
- Internal 3V3/1V8 LDO regulators
- Low operating and USB suspend current; 8mA (active-typ) and 70uA (suspend-typ).
- UHCI/OHCI/EHCI host controller compatible.
- USB 2.0 Full Speed compatible.
- Extended operating temperature range; -40 to 85°C.
- Available in compact Pb-free 16 pin SSOP and 16 pin QFN packages (both RoHS compliant).



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Appendix F Source Code