# Sensors of temperature (contact)

AE3B38SME - Sensors and Measurement

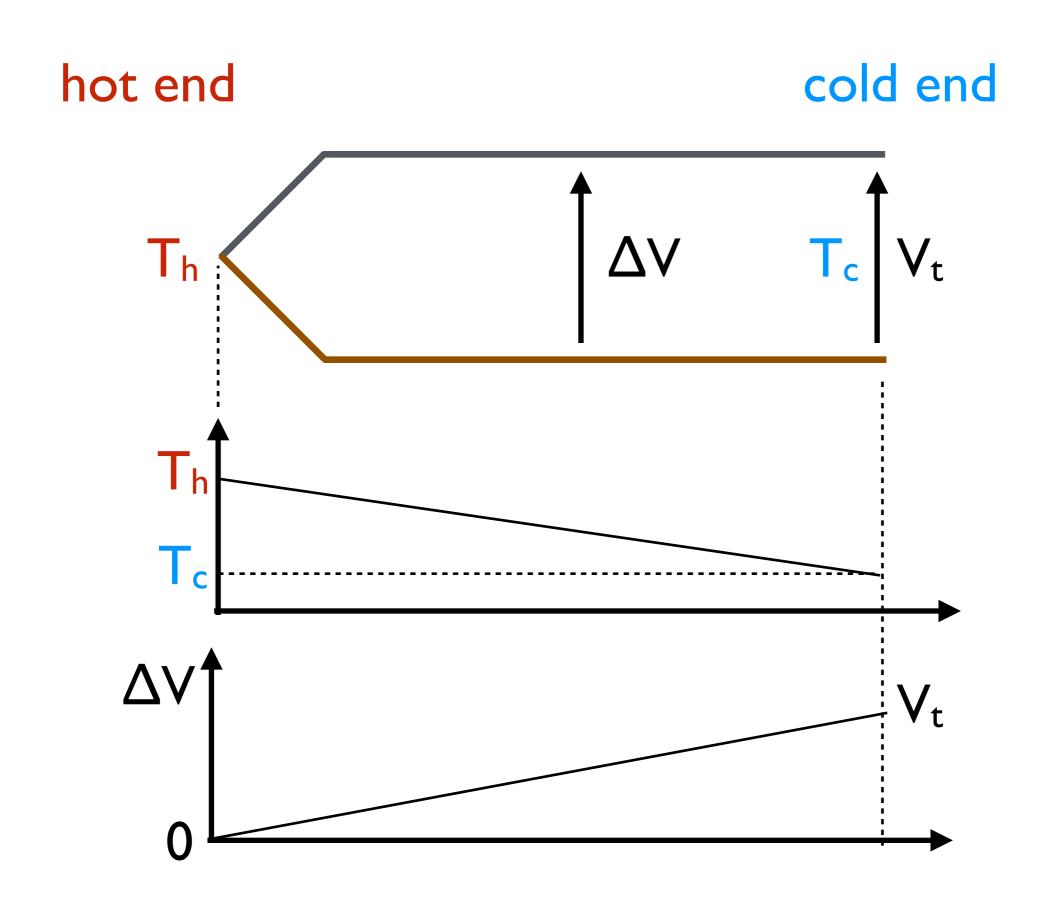
### Thermocouples



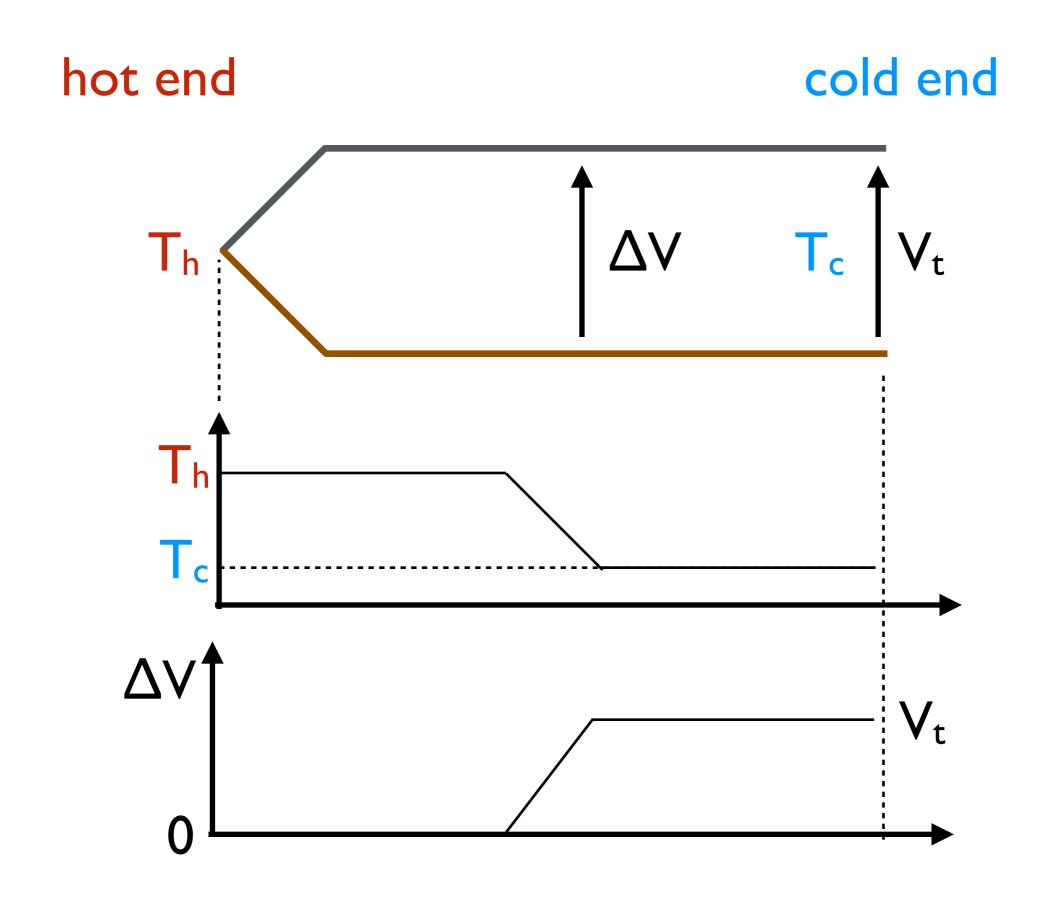
$$V_t = k \left( T_h - T_c \right)$$

- it is composed of different materials
- it measure the difference of temperature

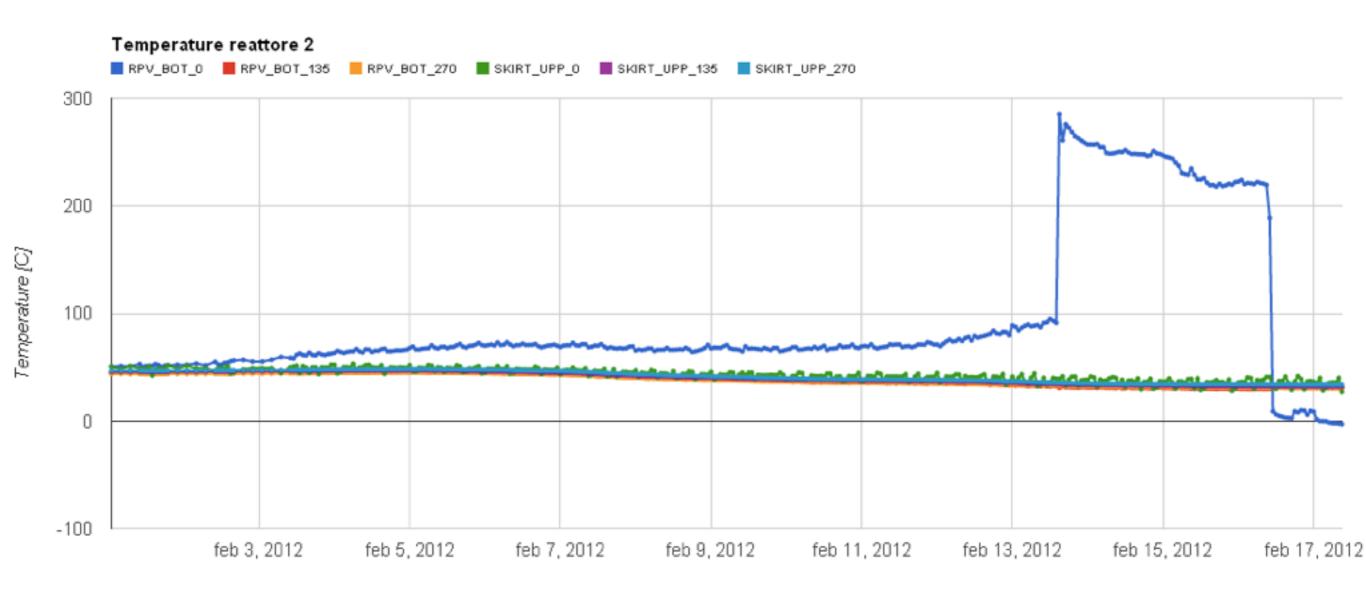
# The voltage is generated by gradient of temperature



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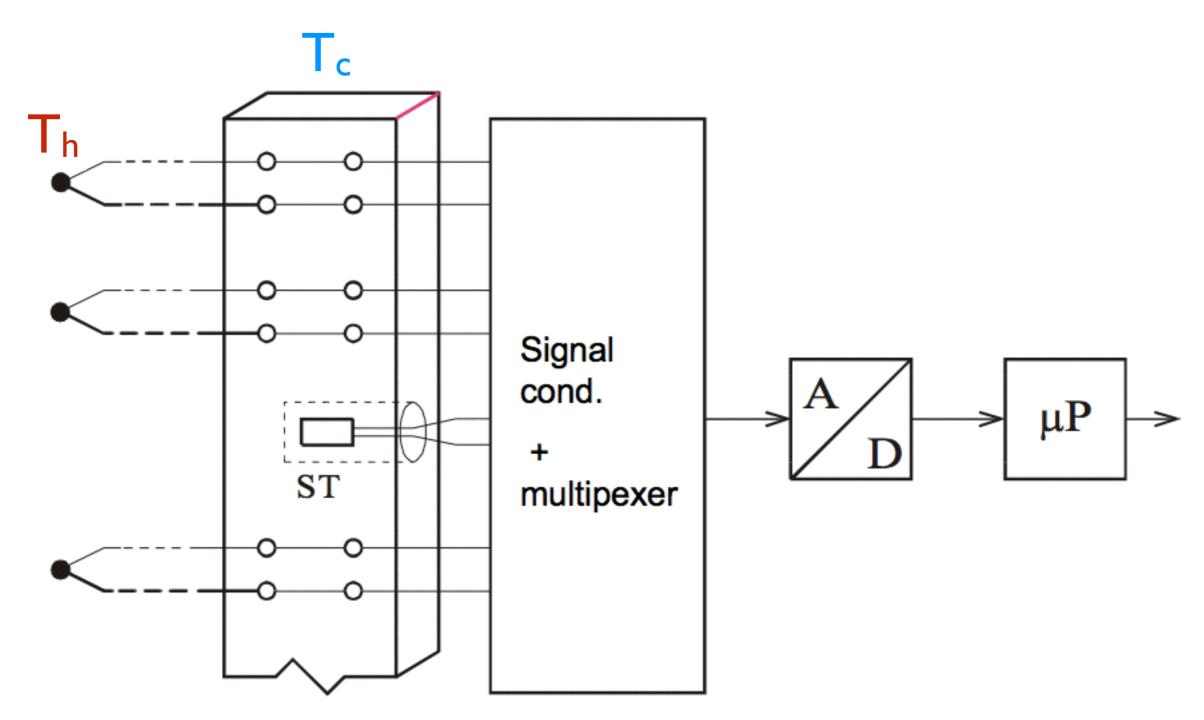


# Thermocouples are very robust, but they might fail too



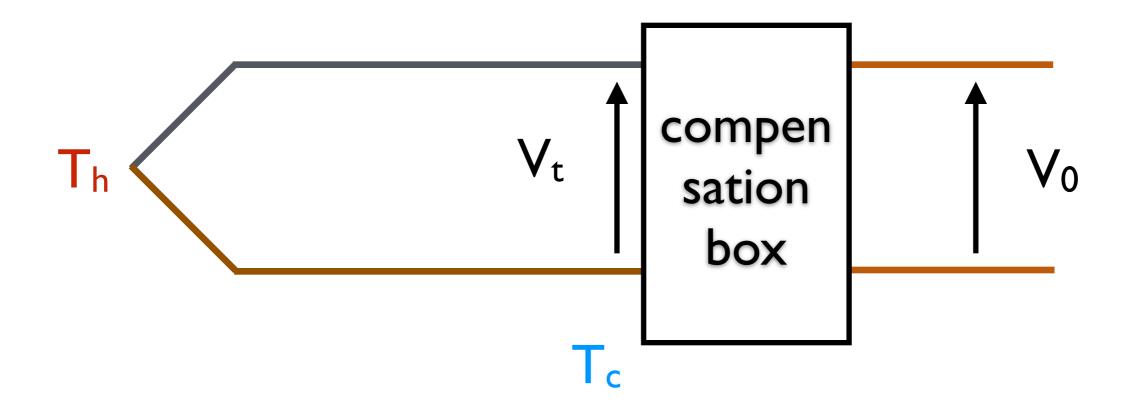
# Compensation of cold end temperature

- by measuring the temperature at cold end and numerically adjust the reading



# Compensation of cold end temperature

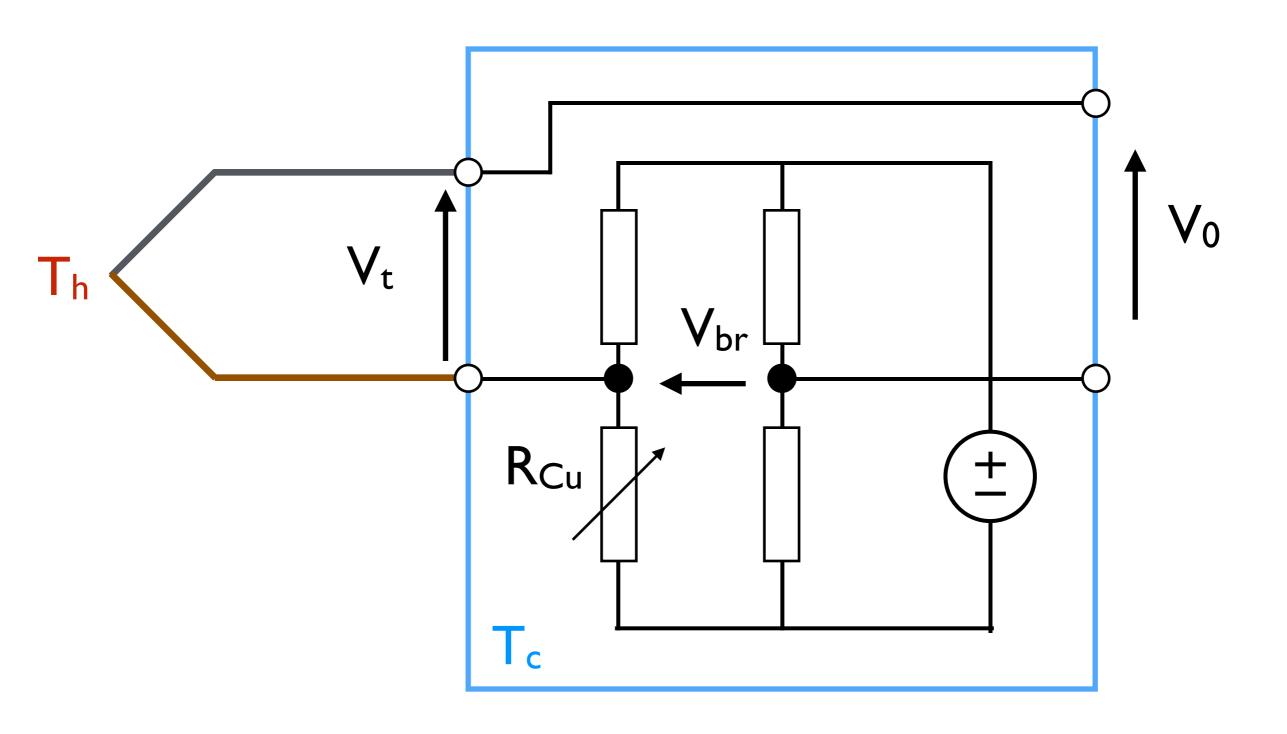
- using compensation box



$$V_t = k \left( T_h - T_c \right)$$

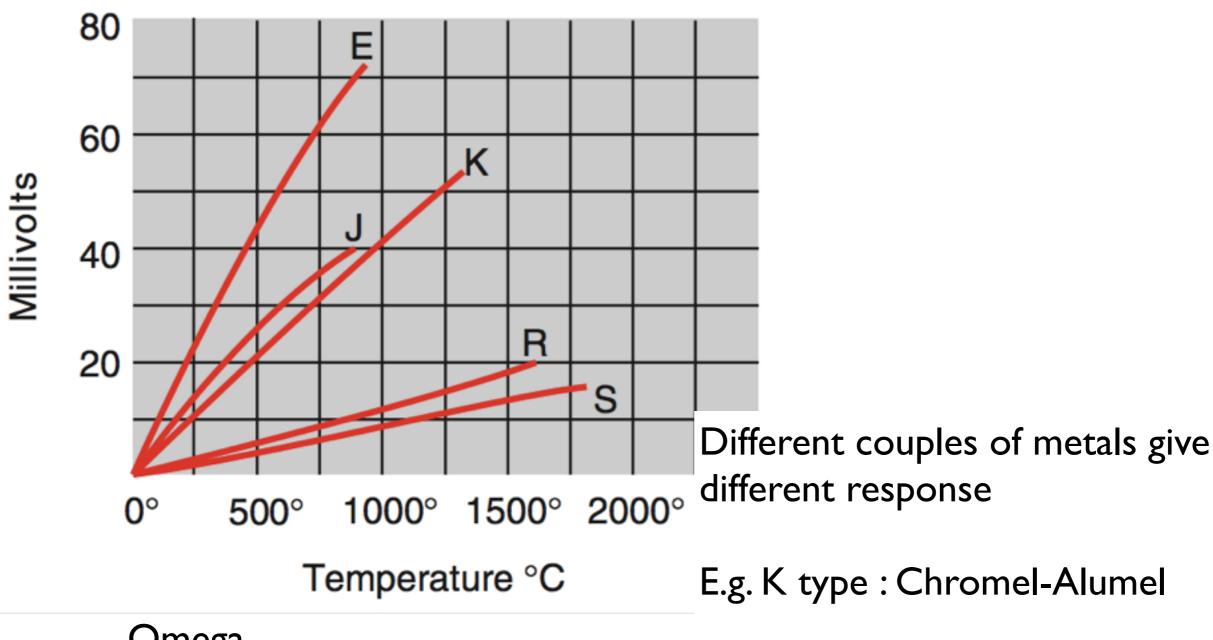
$$V_0 = k T_h$$

# Compensation box



$$V_0 = V_{t+} V_{br} = k \left( T_h - T_c \right) + k' T_c$$

# Types of thermocouples

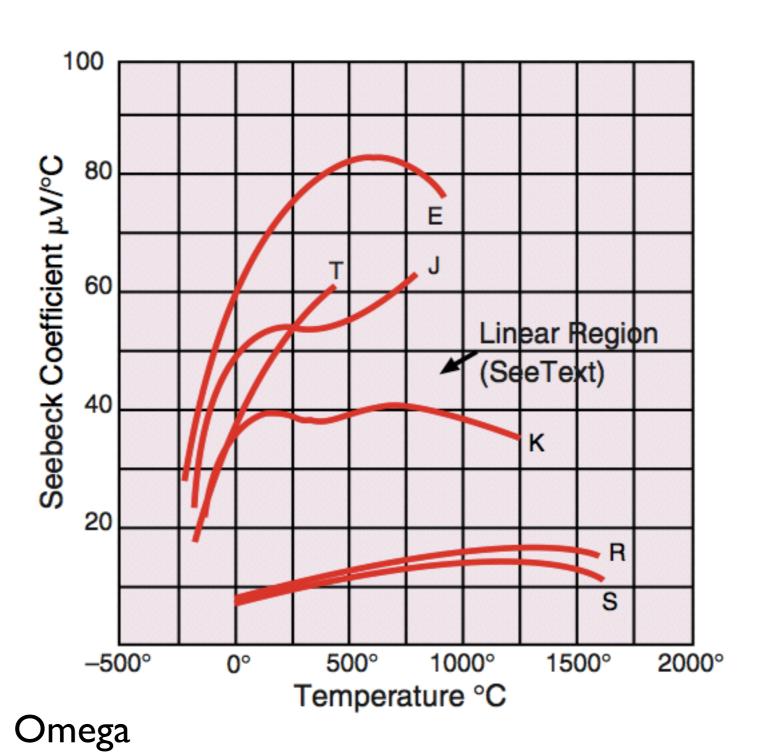


Omega

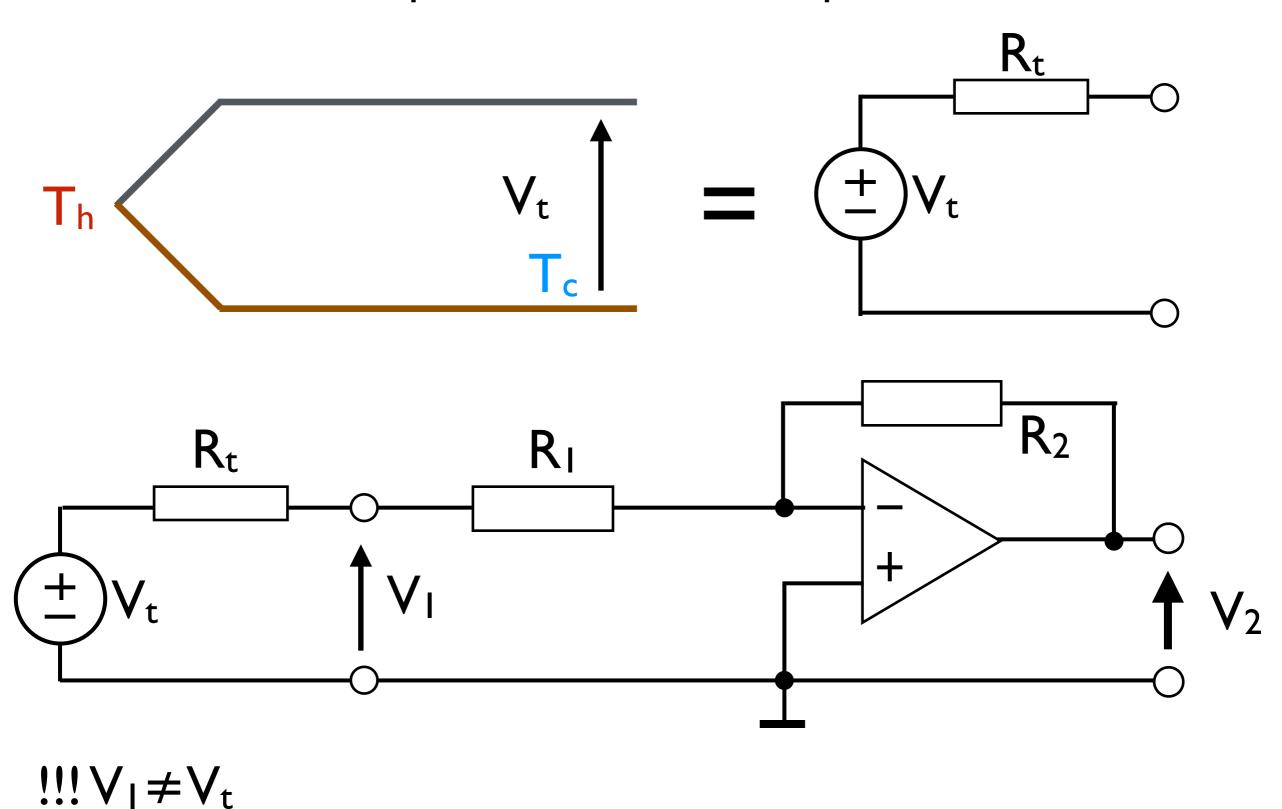
Chromel:90% nickel + 10% chromium

Alumel: 95% nickel, 2% manganese, 2% aluminium

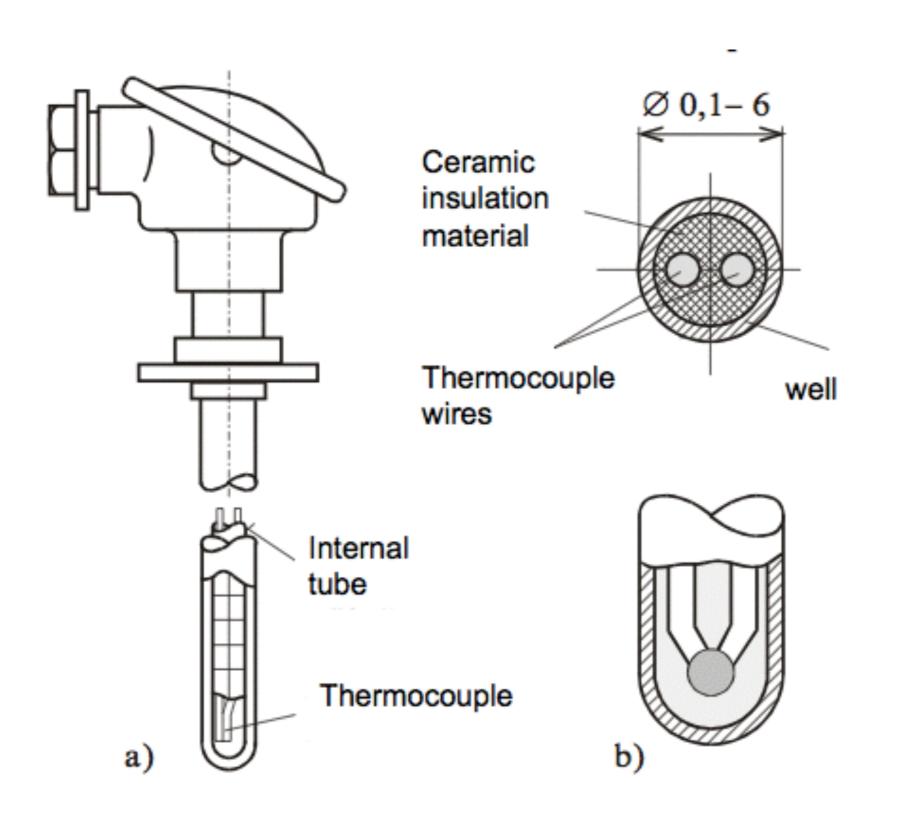
# Sensitivity is not always constant



The sensitivity is always about tens of  $\mu V/K$ . Amplification is often required.



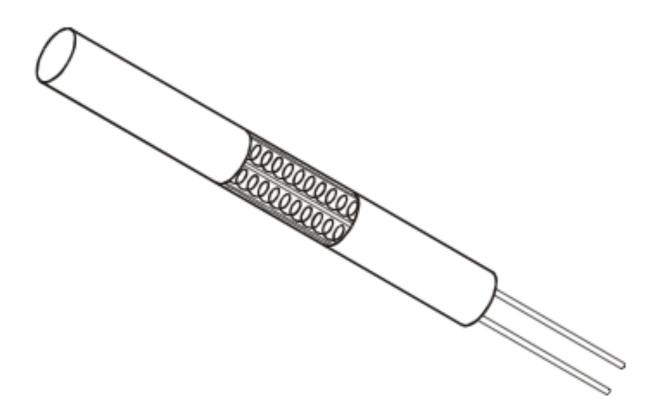
# Industrial thermocouple





#### Metal Resistive Thermometers

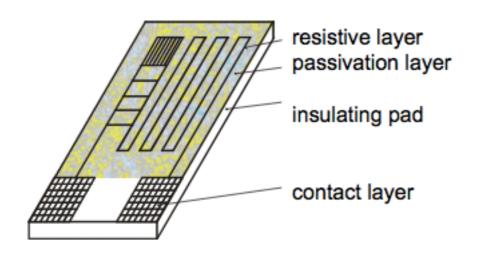
#### wire wound thermometer



# $R=R_0\cdot(I+\alpha\cdot\Delta T)$

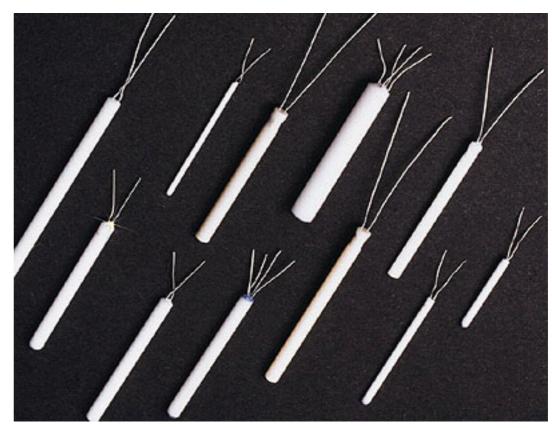
#### Common materials

#### thin layer resistive thermometer



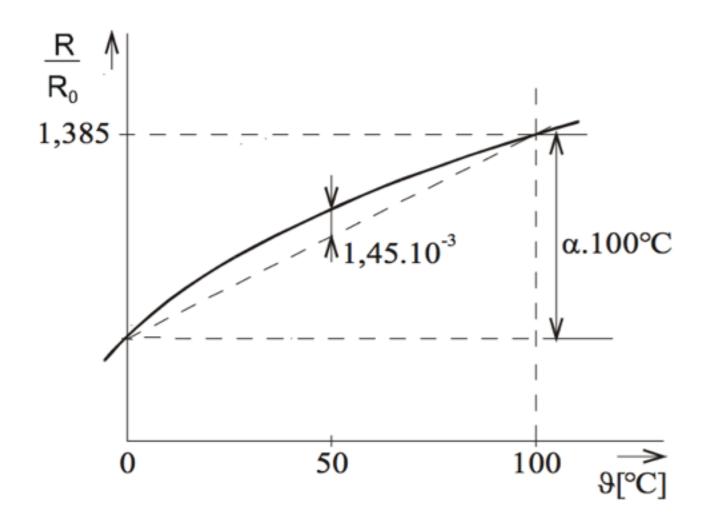
	α [%/K]	range [°C]
Platinum	0.39	- 200 / 850
Nickel	0.69	- 80 / 320
Copper	0.43	- 200 / 260





#### Platinum resistive thermometers

#### Normalized resistance



 $R_{100} / R_0 = 1.385$ 

Standards define the ratio between the resistance at 100 °C and the resistance at 0°C

(1.3910 in GB, USA, Japan, Russia)

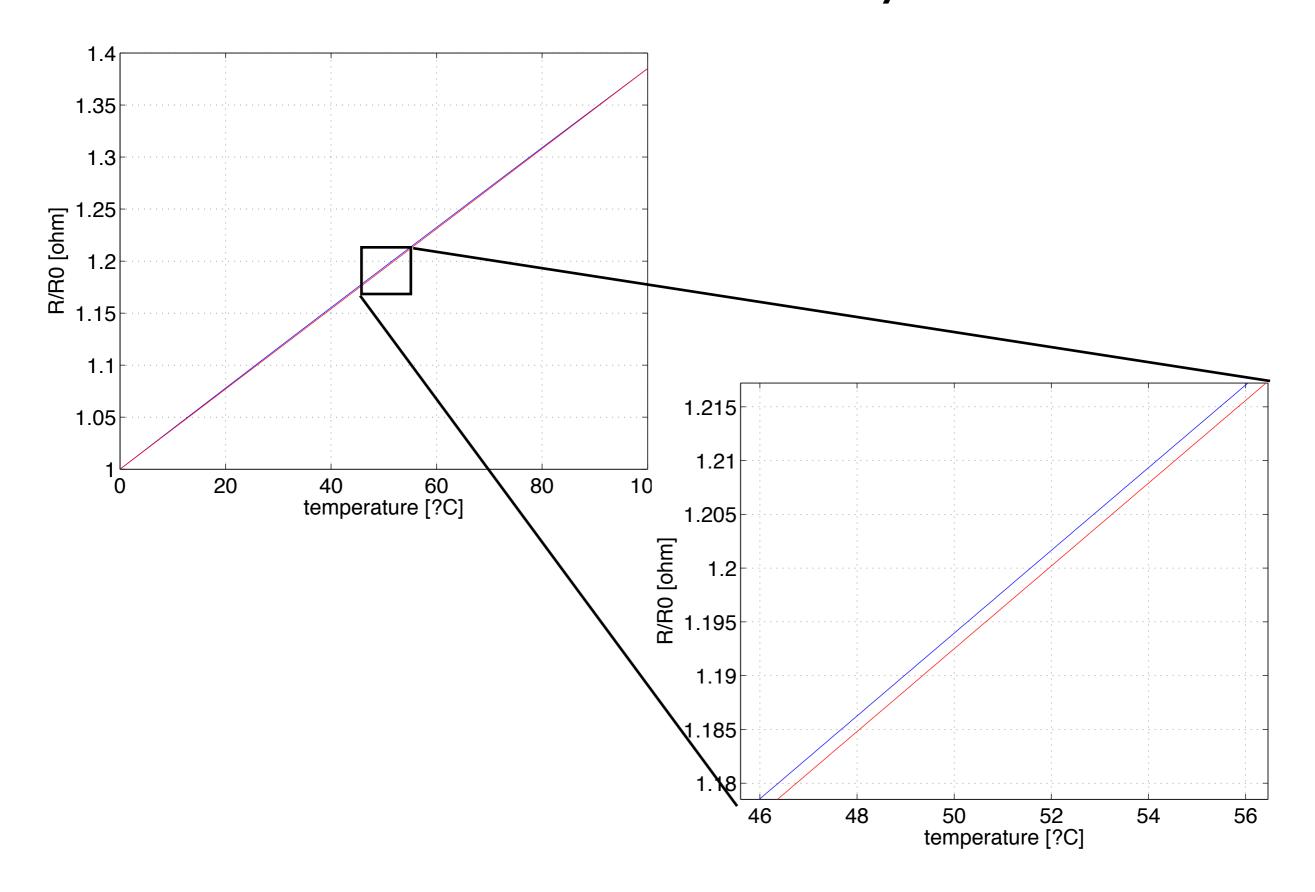
The resistance is not linear

$$R_t = R_0 [I + A \cdot t + B \cdot t^2 + C \cdot t^3 (t - 100)]$$

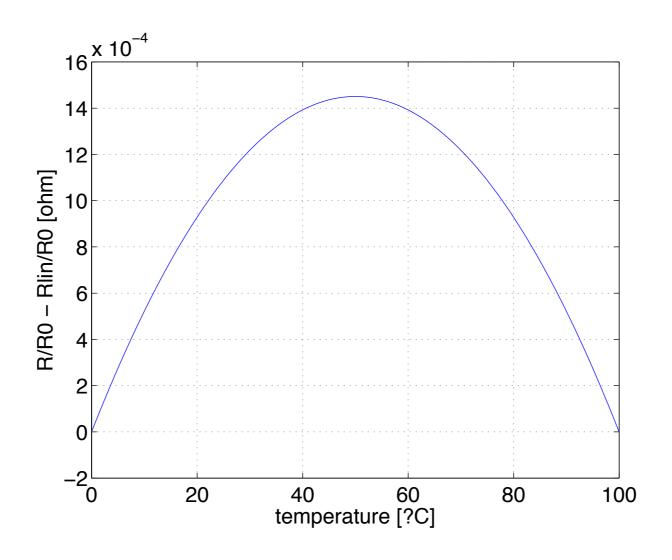
$$A = 3.90802.10-3 K^{-1}$$
  
 $B = -5,802.10-7 K^{-2}$ 

$$t < 0$$
°C C= -4,27350.10-12 K<sup>-4</sup>  
 $t > 0$ °C C=0

# Actual non-linearity



# Actual non-linearity

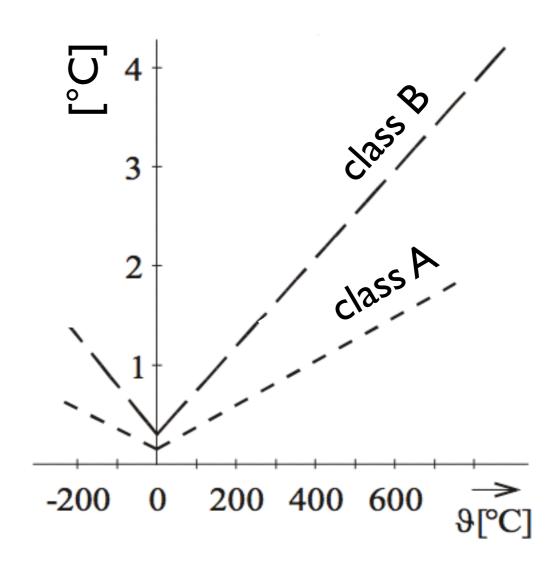


#### Standard value of Pt resistance:

PtI00  $\rightarrow$  0°C R= 100  $\Omega$ 

200, 500, 1000, 2000 Ω

tollerance



#### Nickel resistance thermometer:

- high sensitivity, quick response, small dimensions
- limited temperature range

$$R_t = R_0 [I + A \cdot t + B \cdot t^2 + C \cdot t^2 (t - 100)]$$

A= 
$$5.49 \ 10^{-3} \ K^{-1}$$
  
B=  $6.80 \ 10^{-6} \ K^{-2}$   
C=  $9.24 \ 10^{-9} \ K^{-3} \ for \ t>0 \ (else C=0)$ 

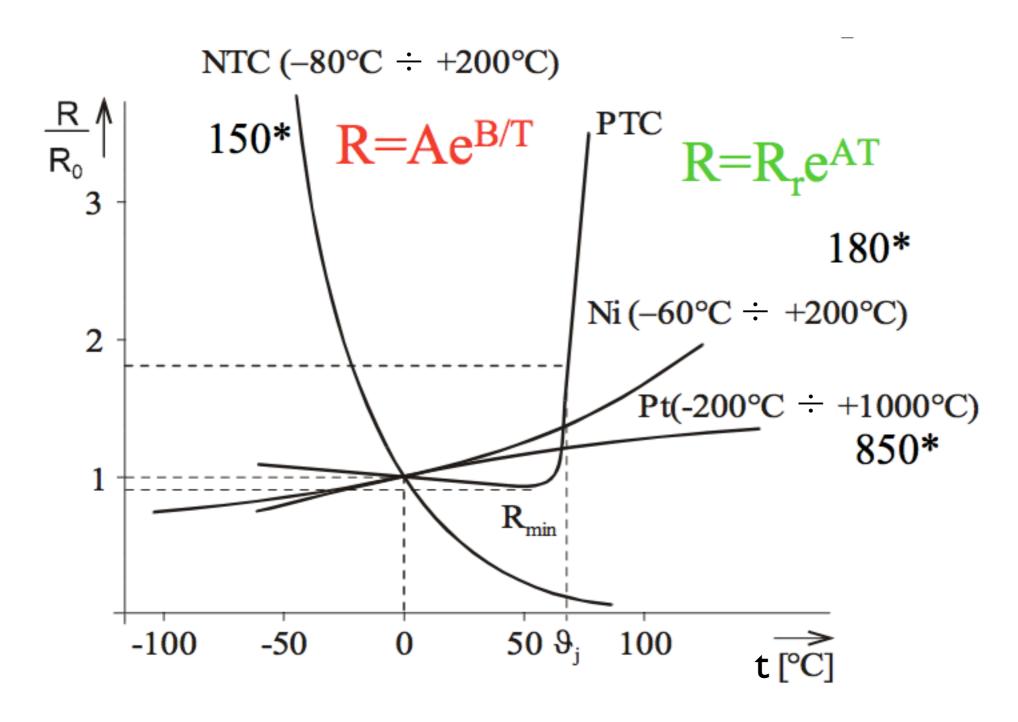
## Copper resistance thermometer:

- limited range (from -200°C to + 200°C)
- small resistance
- direct measurement of windings temperature

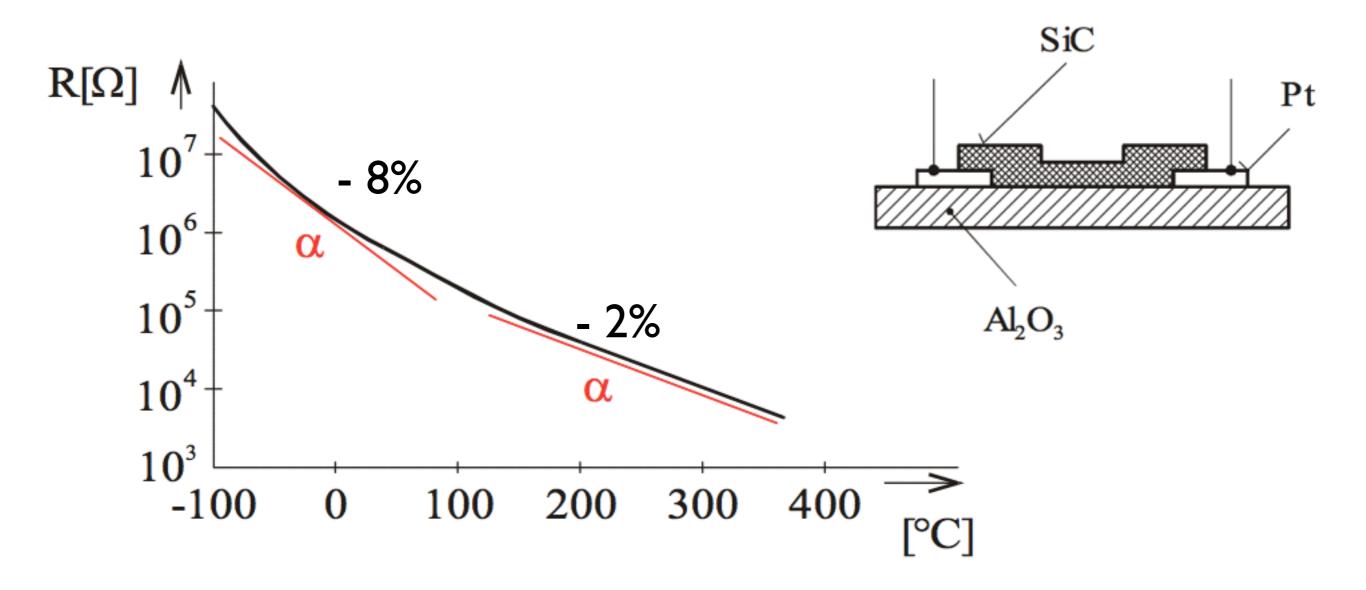
$$R_t = R_0 [I + \alpha \cdot t]$$
  $\alpha = 4.26 I0^{-3} K^{-1}$ 

# Semiconductor resistive sensors of temperature

Thermistor PTC - Positive Temperature Coefficient NTC - Negative Temperature Coefficient



# NTC - Negative Temperature Coefficient



-produced e.g. by sintering technology from the powder of metal oxides -usable range - from 4.2K to 1000 °C

$$R=A \cdot e^{\frac{B}{T}}$$

$$R_1 = A \cdot e^{\frac{B}{T_1}}$$

$$R_2 = A \cdot e^{\frac{B}{T_2}} \rightarrow R_2 = e^{\left(\frac{B}{T_1} - \frac{B}{T_2}\right)} \rightarrow B$$

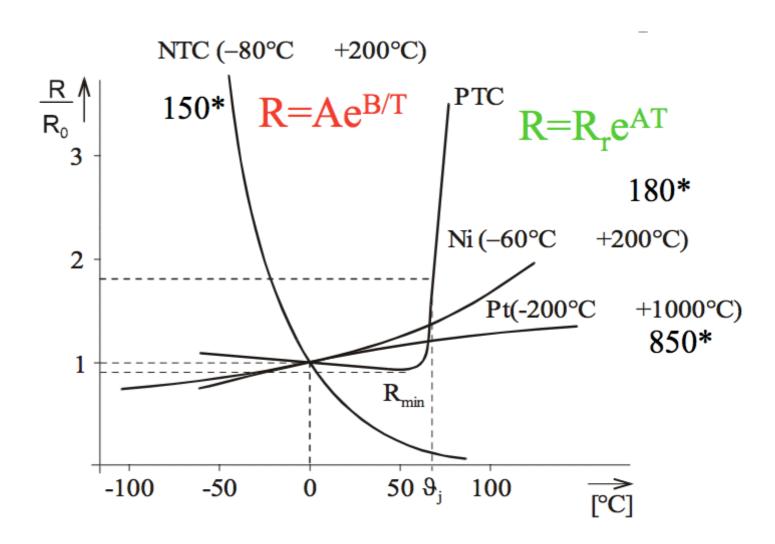
#### PTC, posistors

 $\alpha > 0$ 

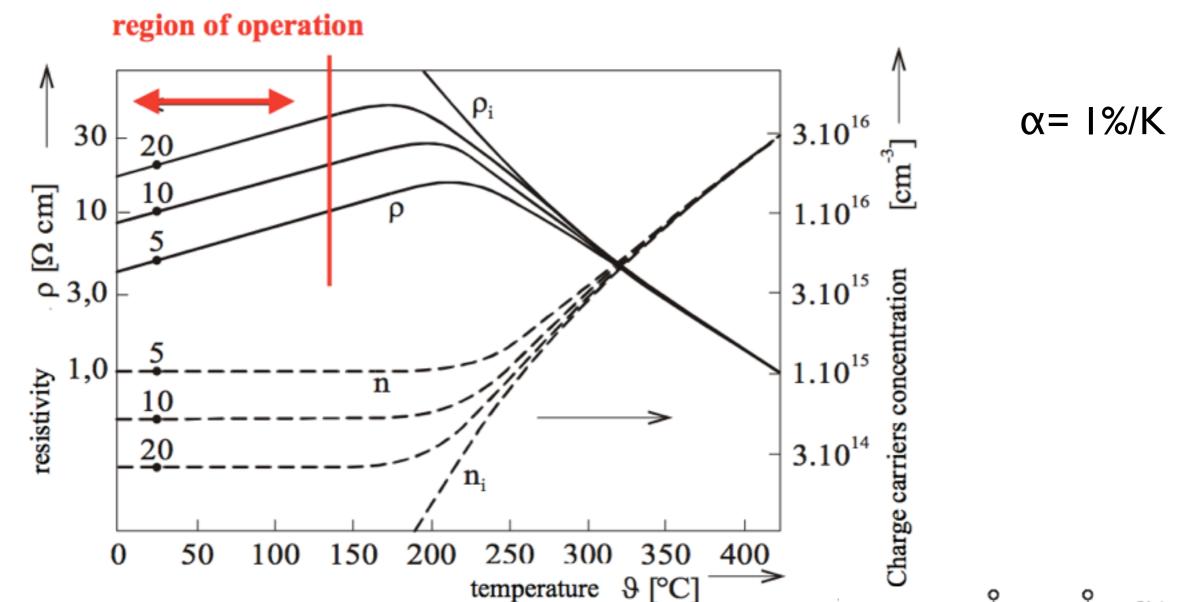
- made from polycrystalline ferroelectric ceramics e.g. (BaTiO3)
- application: two state sensors
   (thermal switches indication of excessing max. temp.)

resistance slowly decrease with increasing temperature

after Curie point rapid increase of resistance - relation for increase of resistance



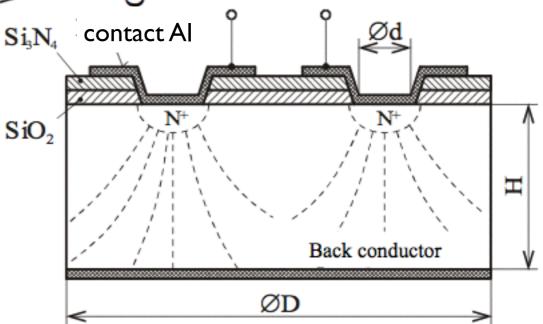
# Semiconductor monocrystalline sensors of temperature



Resistance of the sensor

 $\beta$ – geometrical factor d – diameter of contact  $\rho$  – resistivity

$$R = \frac{\rho}{\beta d}$$
 sio<sub>2</sub>



# Problem: in order to measure a resistance we need to inject a current which generates heat!

#### **SELF HEATING**

difference of temperature given by self heating:

$$\Delta T = \frac{RI^2}{D}$$
thermal resistance

Pt100 : max I mA to have max  $\Delta T=0.1^{\circ}C$ 

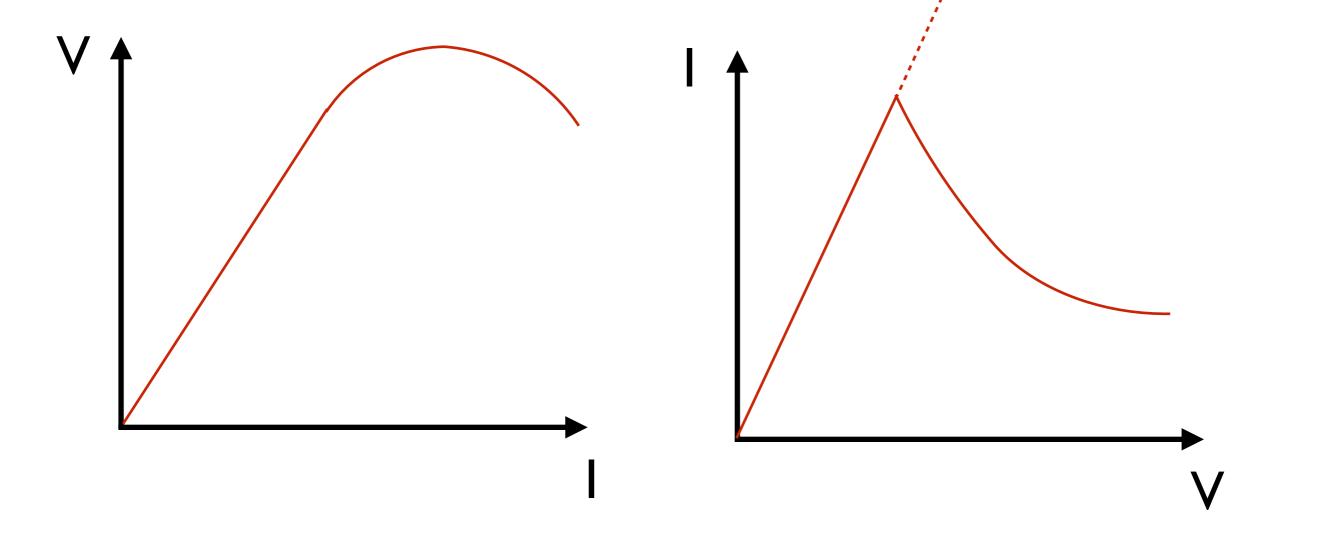
#### Effect of self heating on

negastor (NTC thermistor)

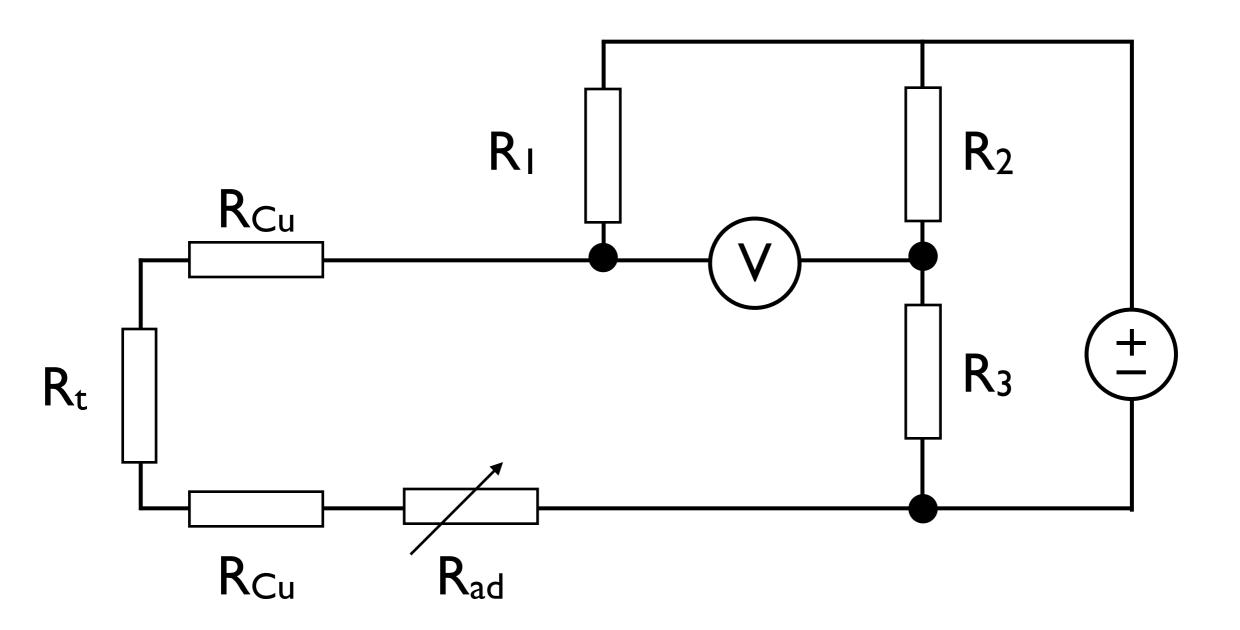
posistor (PTC thermistor)

at high I the temp increases so the R drops and therefore V=RI drops.

we can't increase I because increment of I would increase R and then decrease I back.

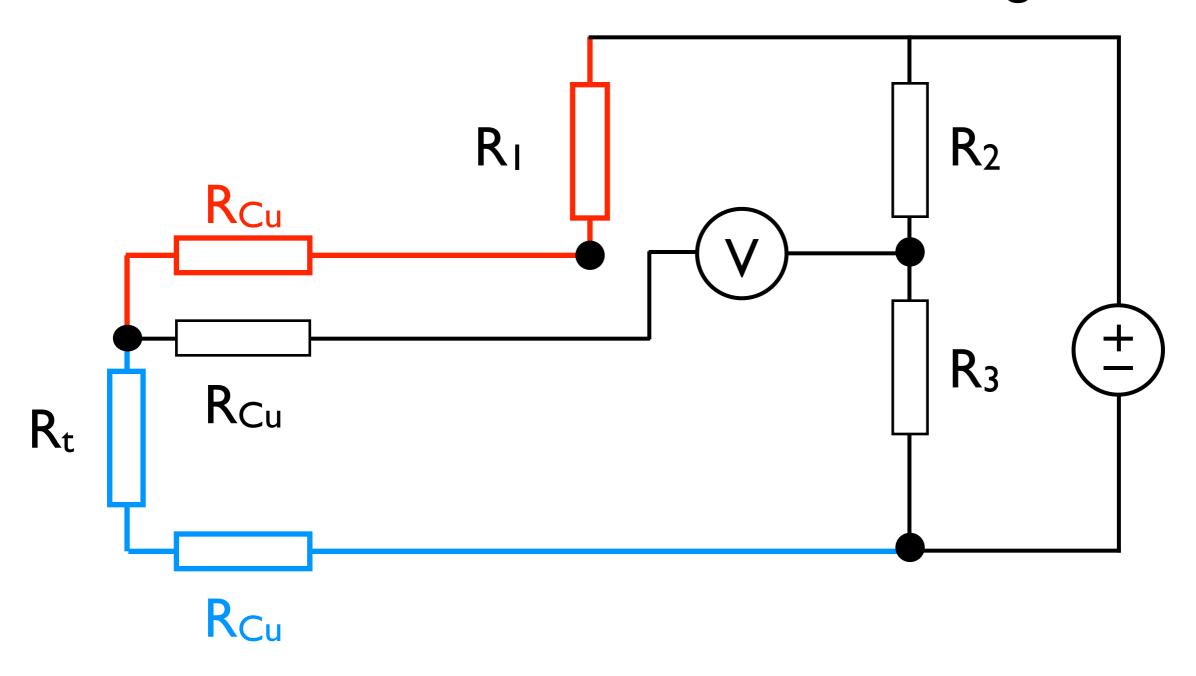


# Two wire connection in a bridge



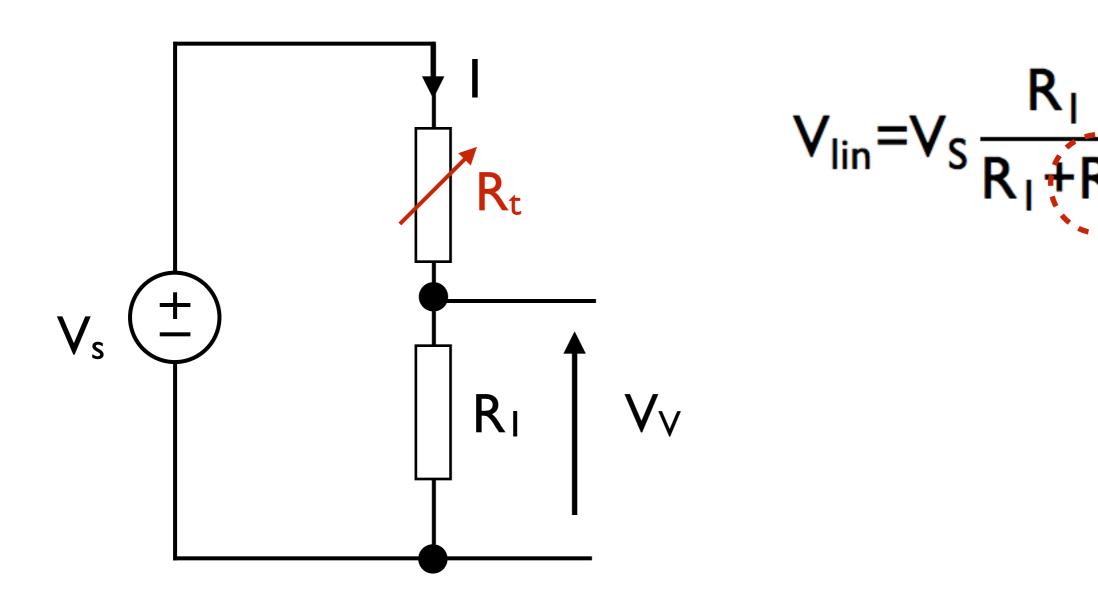
 $R_{ad}$  can be adjusted to balance the bridge and null the contribution of  $R_{cu}$ . Problem: the resistance of the cables might change too with temperature

# Three wire connection in a bridge

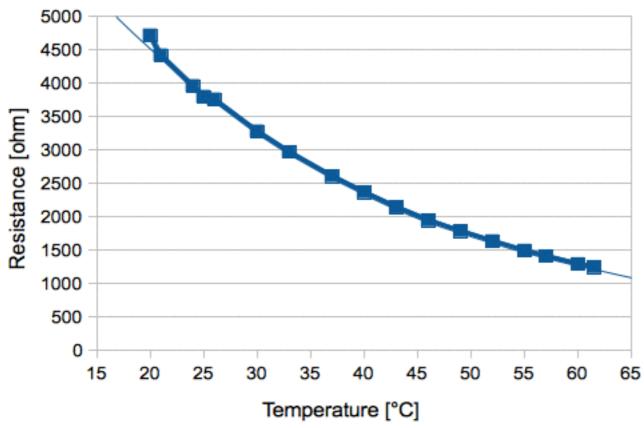


Two resistances of the cables fall in opposite sides of the bridge's leg, the compensate each other. The 3rd cable resistance has no effect (lv=0)

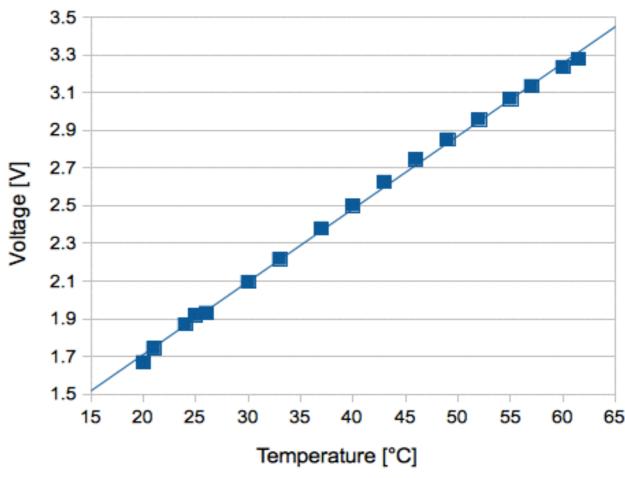
#### Linearization of thermistor with a series resistor



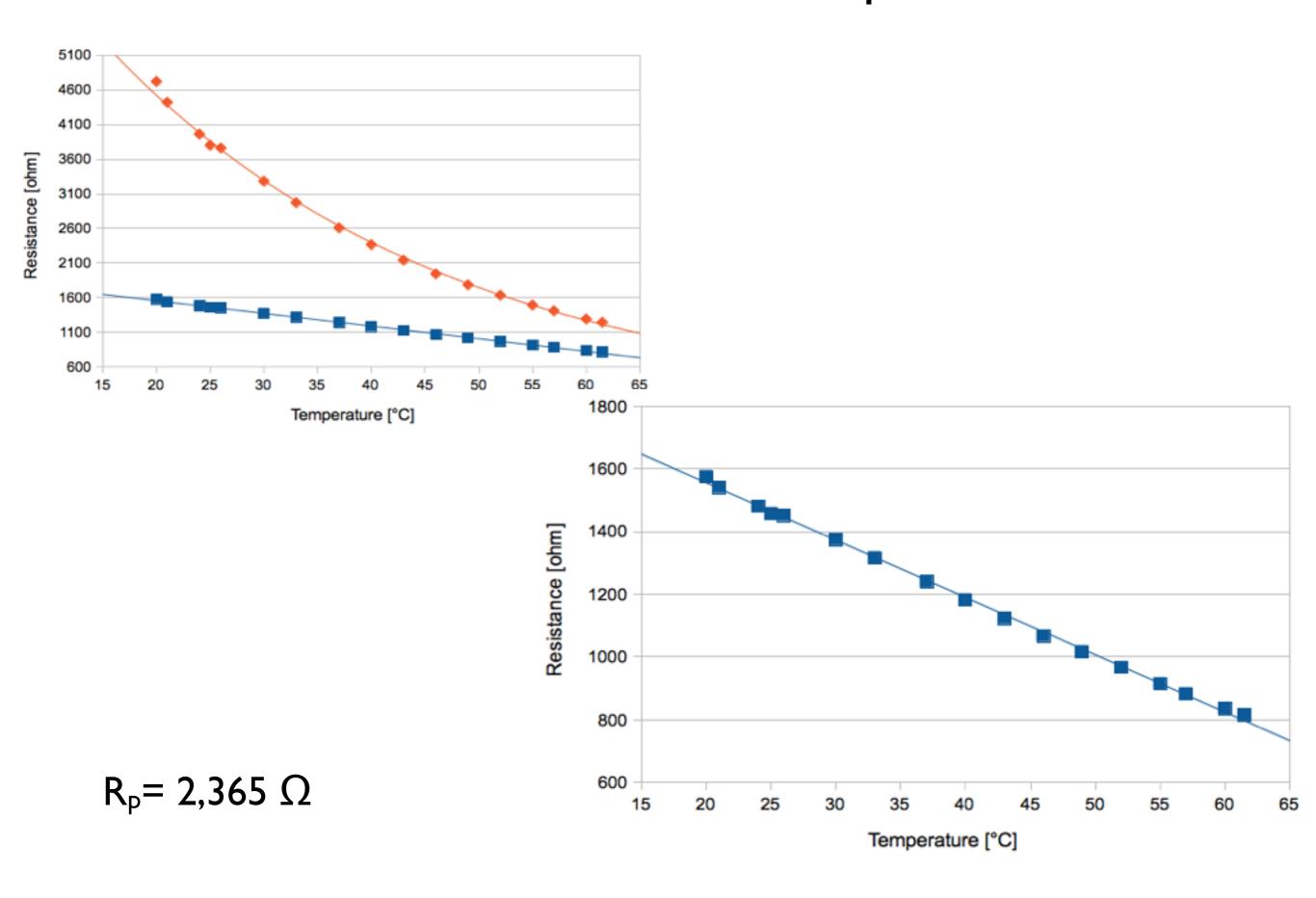
#### Linearization of thermistor with a series resistor



 $V_s = 5 V$  $R_1 = 2,365 \Omega$ 

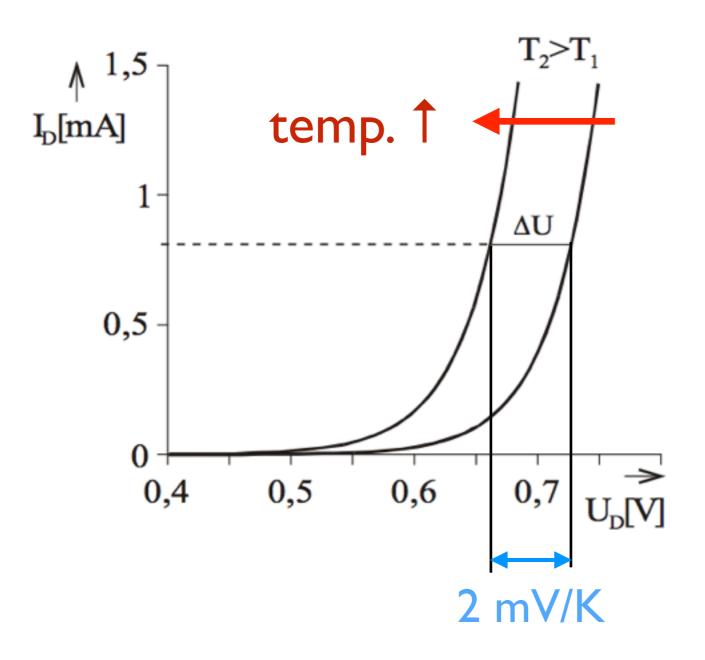


# Linearization of thermistor with parallel resistor



# PN junction based sensors of temperature

The V-I curve of PN junction depends on temperature



Shockley equation

$$I_D = I_S \left( e^{\frac{V_D}{mV_T}} - I \right)$$

$$V_D = m \cdot V_T \cdot \ln \left( \frac{I_D}{I_S} + I \right)$$

Is – reverse saturation current

ID - forward current in PN junction

m – coefficient of recombination

V<sub>D</sub> – forward voltage on PN junction

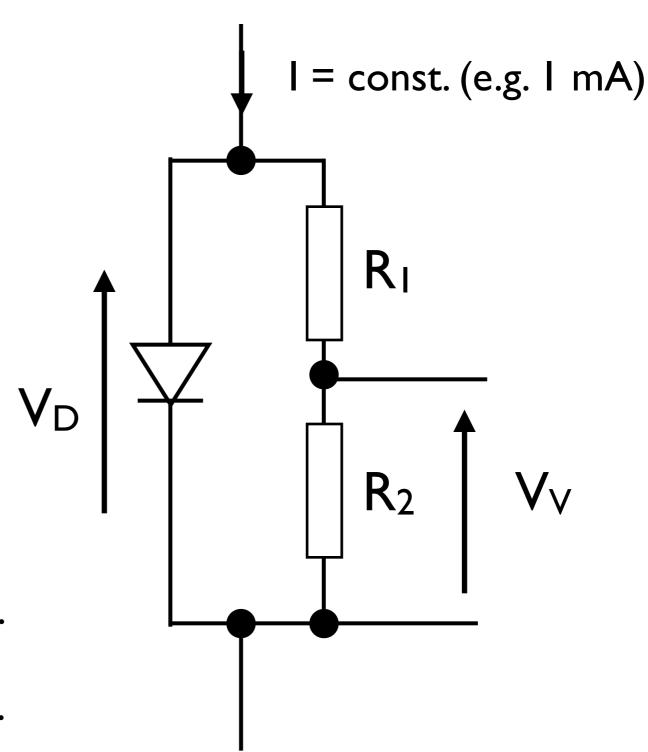
VT – thermal voltage

e – elementary charge

k – Boltzmann constant

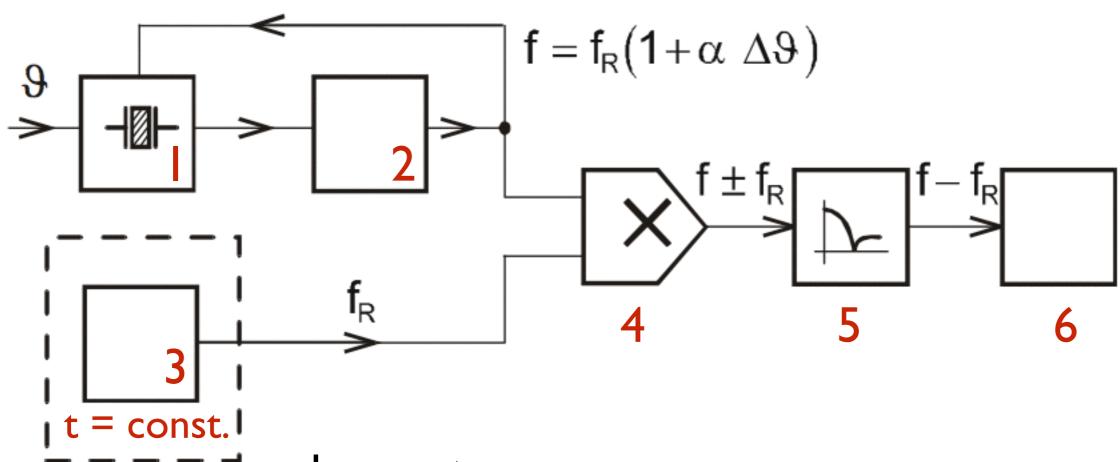
$$V_T = \frac{kT}{e}$$

# This principle can be used to create a compensation circuit for thermocouples cold end



V<sub>D</sub> changes with about 2 mV/K. A voltage divider is used to achieved the desired sensitivity.

#### Quartz thermometer



- I quartz
- 2 quartz controlled oscillator
- 3 ref. quartz controlled oscillator (thermostated)
- 4 mixer (analogue multiplier)
- 5 low frequency filter (4+5=synchronous detector)
- 6 counter with display

very precise!

# Reversible temperatur labels



# Non-reversible temperatur labels

