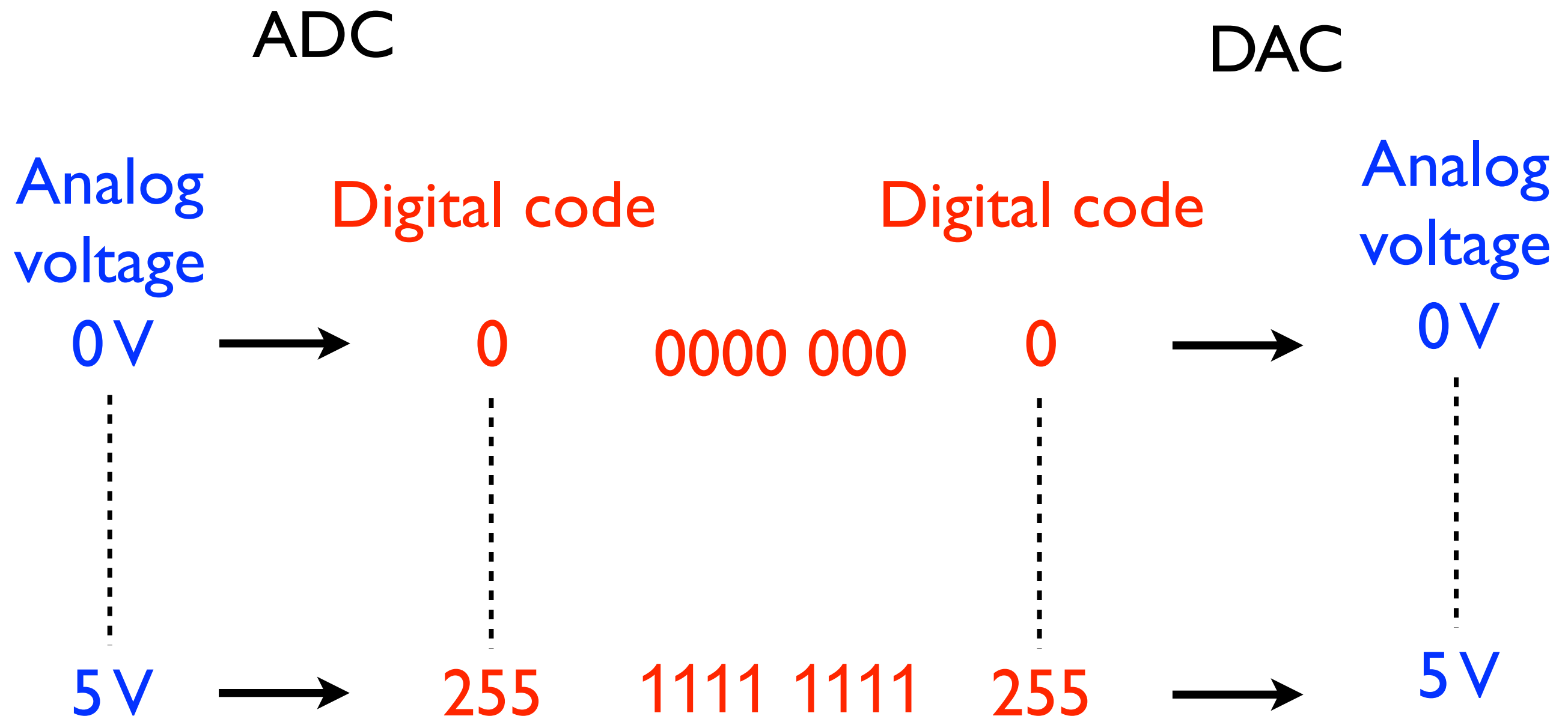


# Lecture 6

- reference sources
  - DA converters
- spectrum analyzers
- signal generators

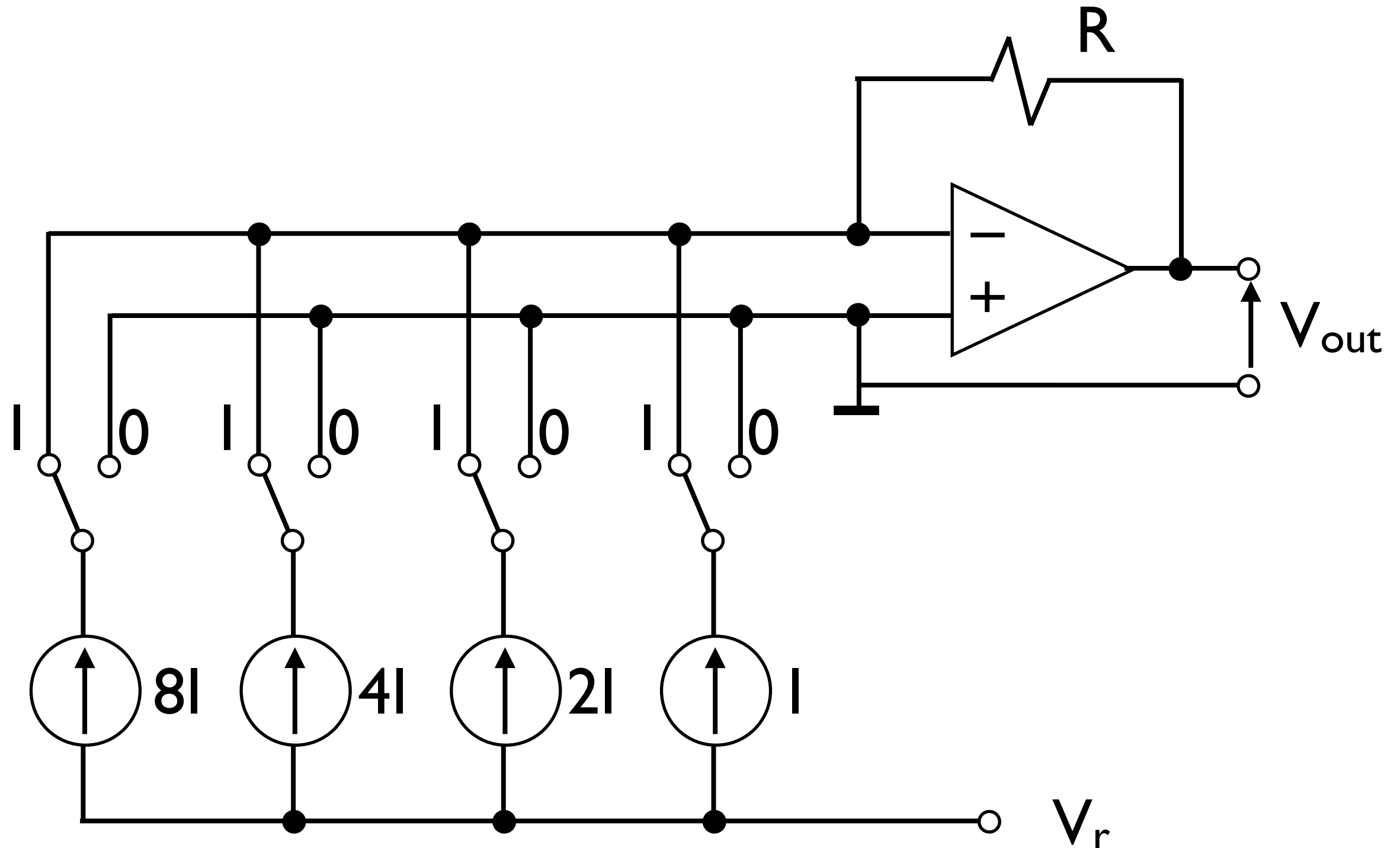
# DAC - digital to analog converter

It's the opposite of ADC

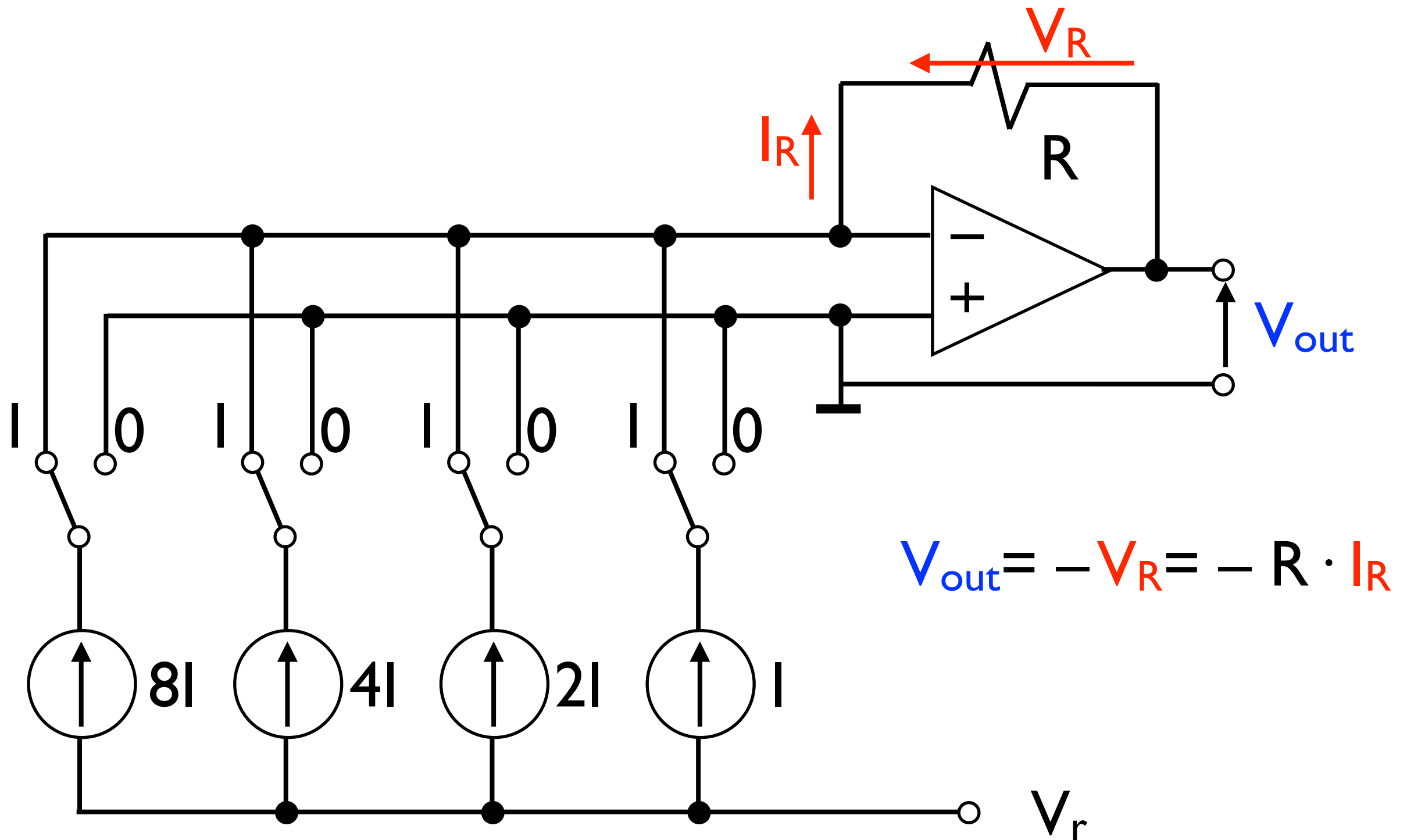


# I - DAC with switched over current sources

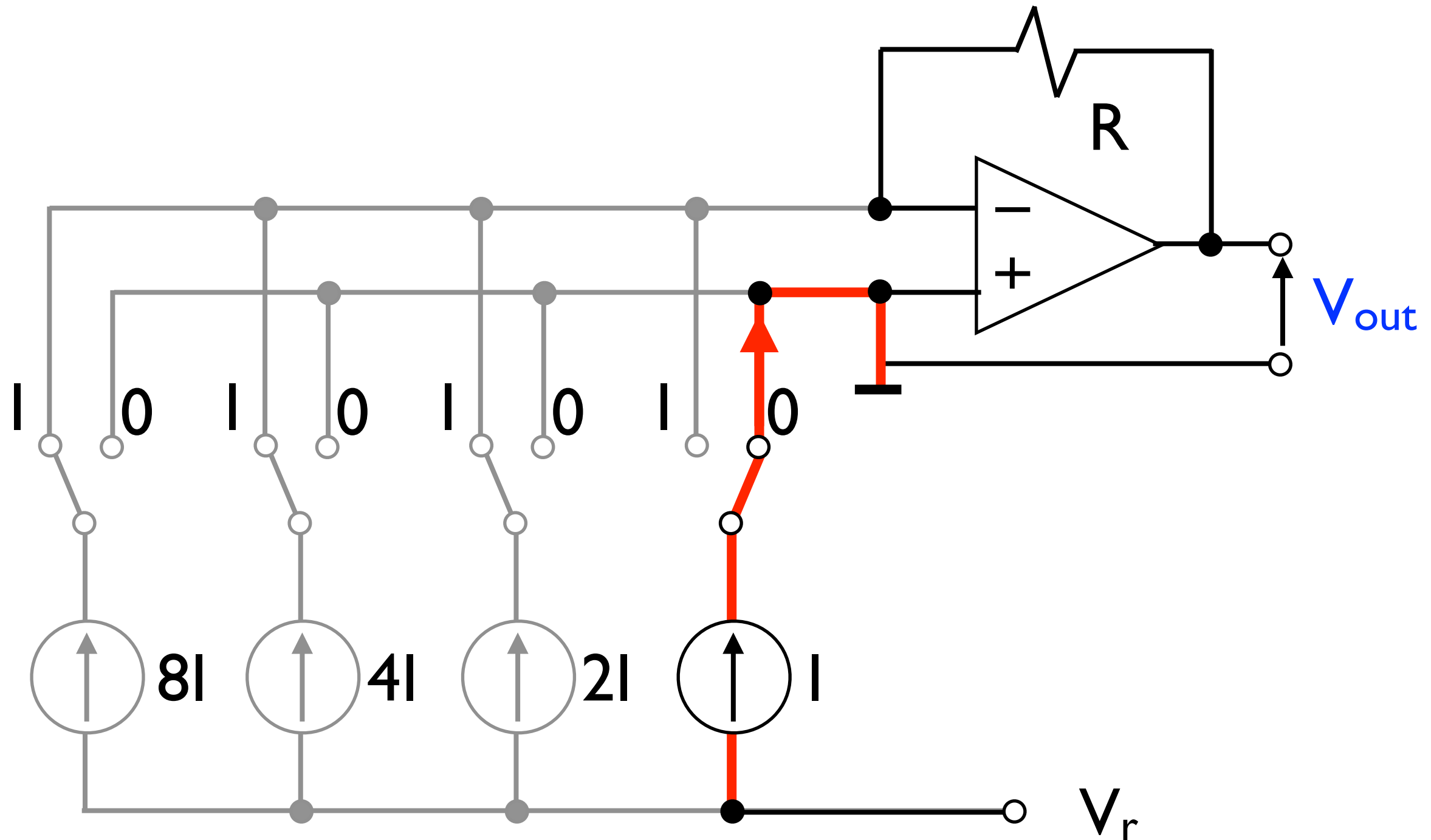
## Structure



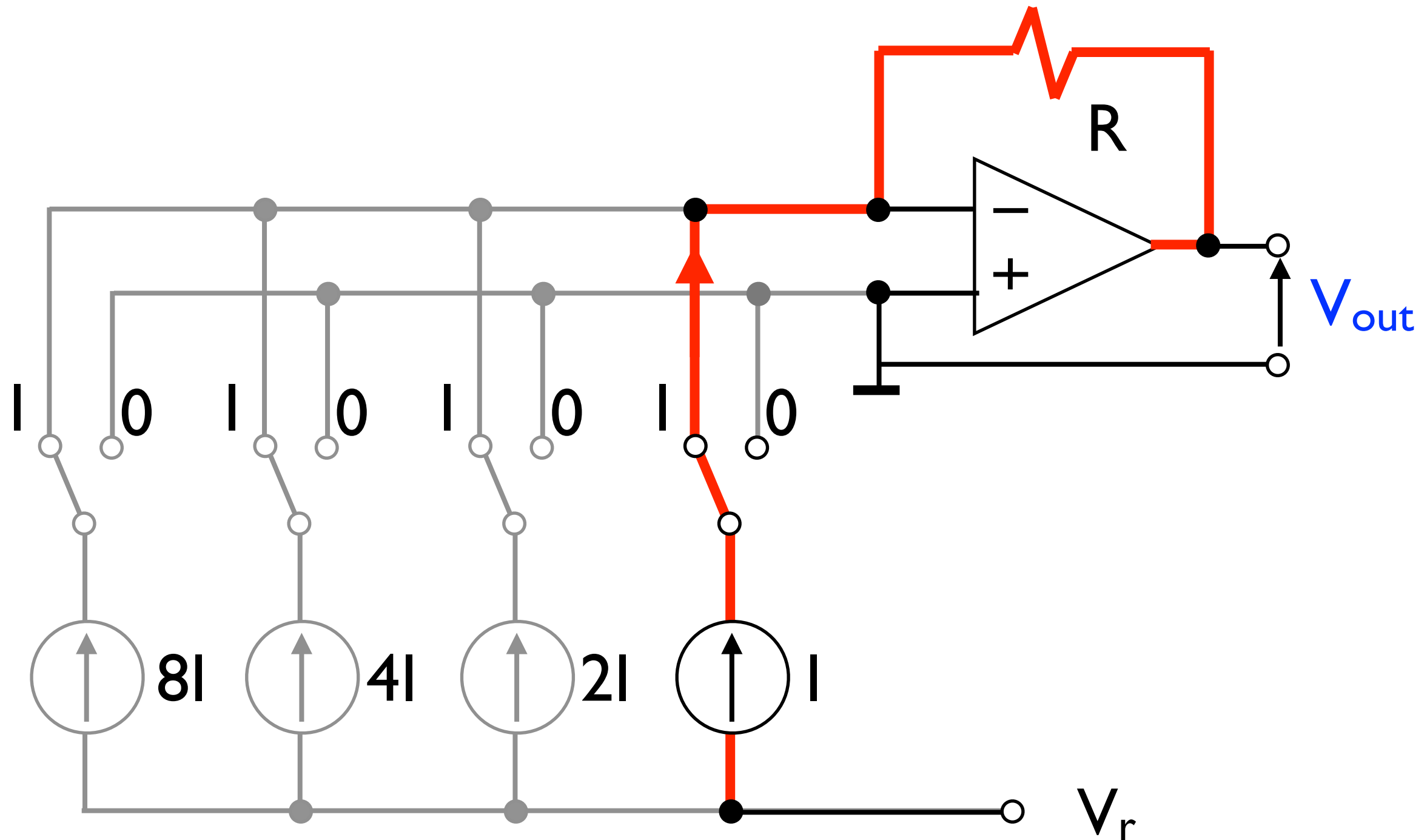
# I - DAC with switched over current sources



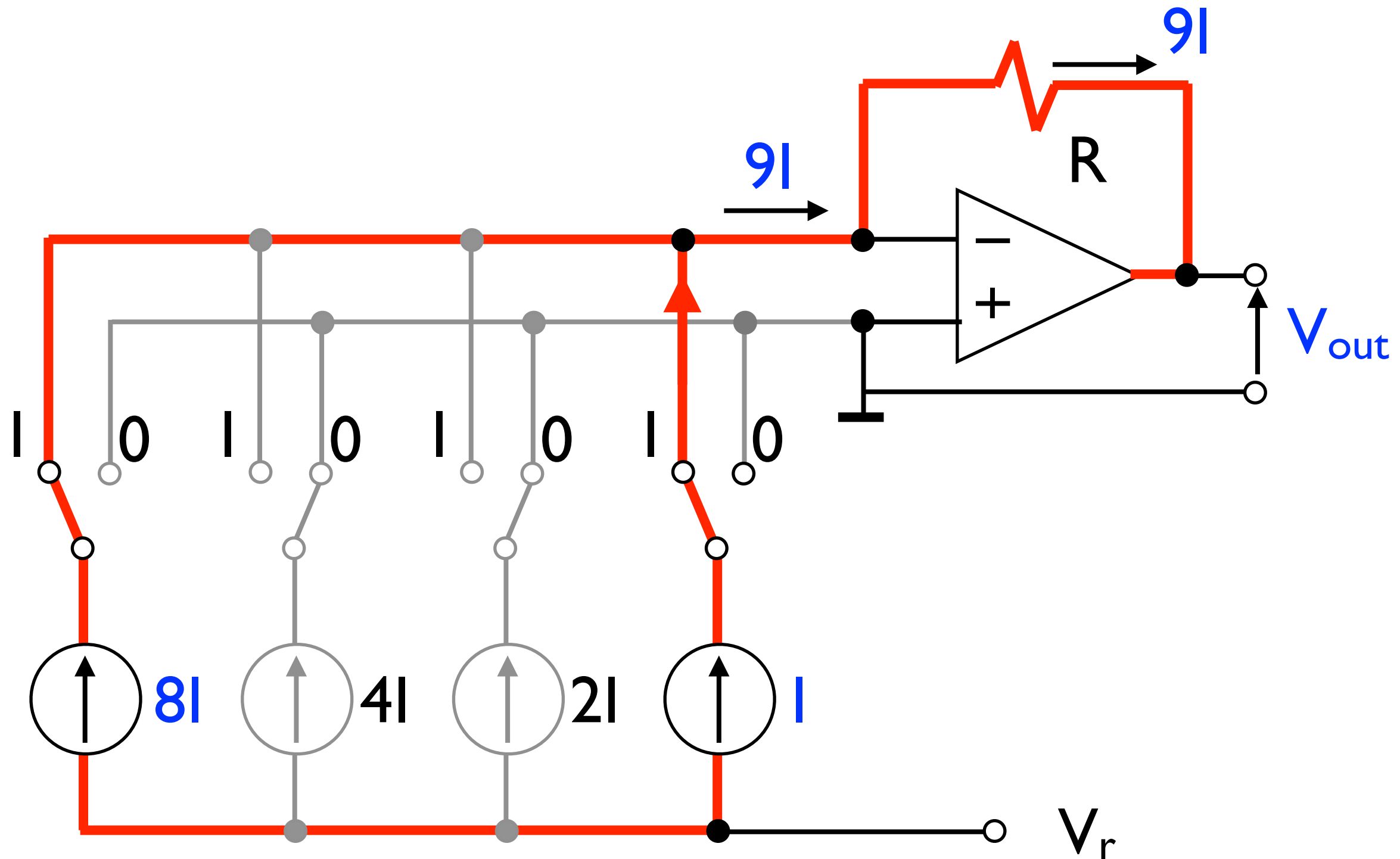
# I - DAC with switched over current sources



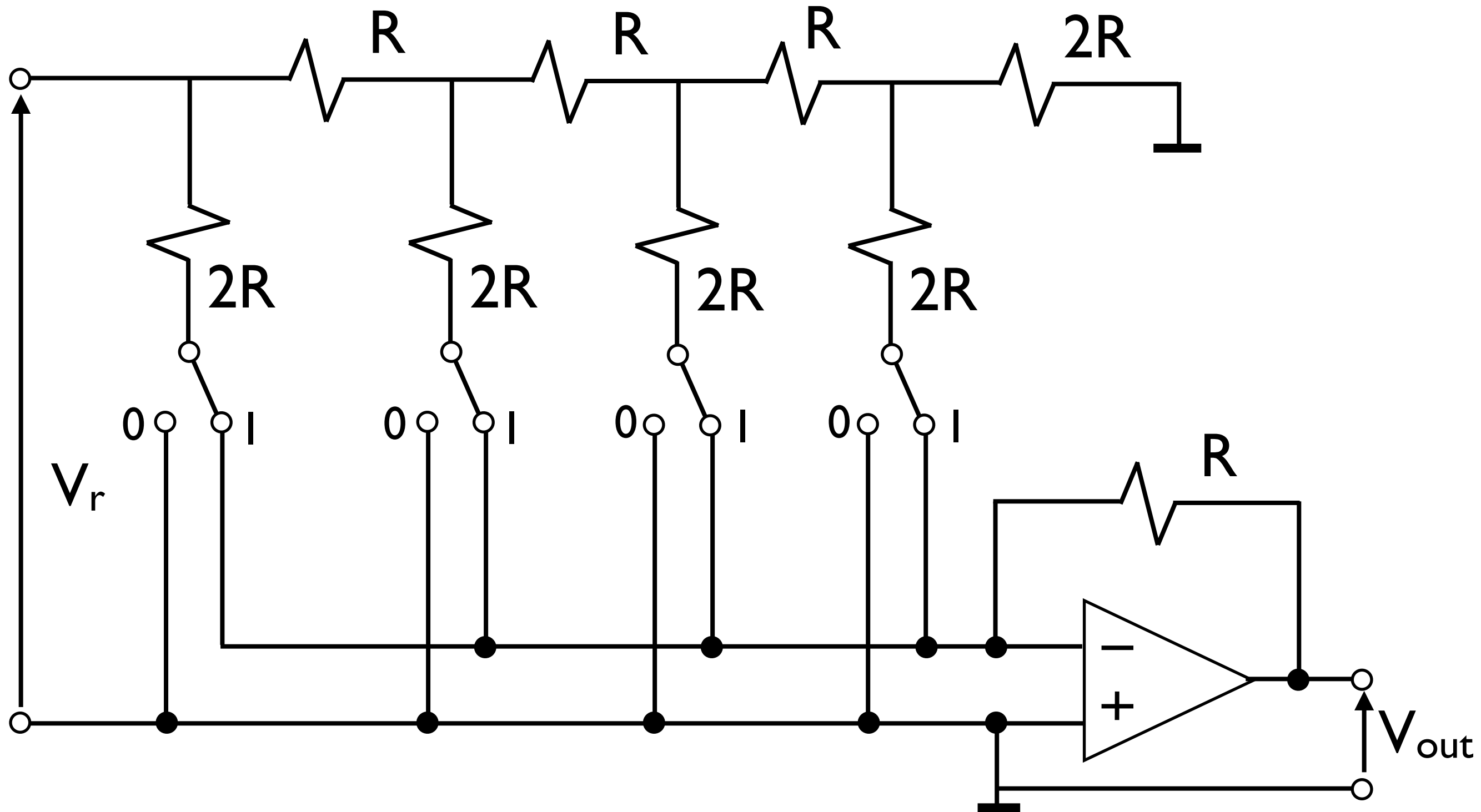
# I - DAC with switched over current sources



# I - DAC with switched over current sources

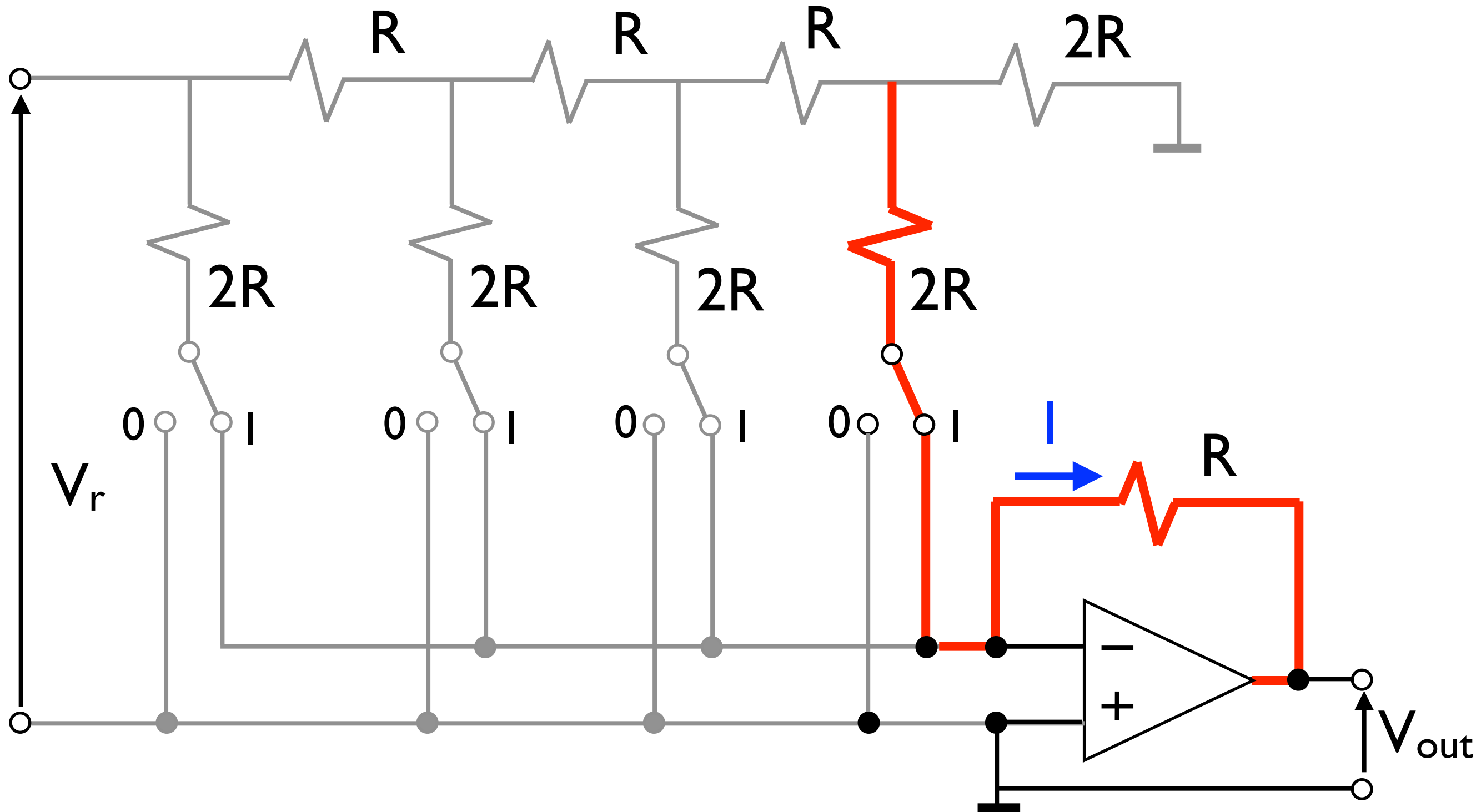


## 2 - DAC using R-2R Resistance ladder

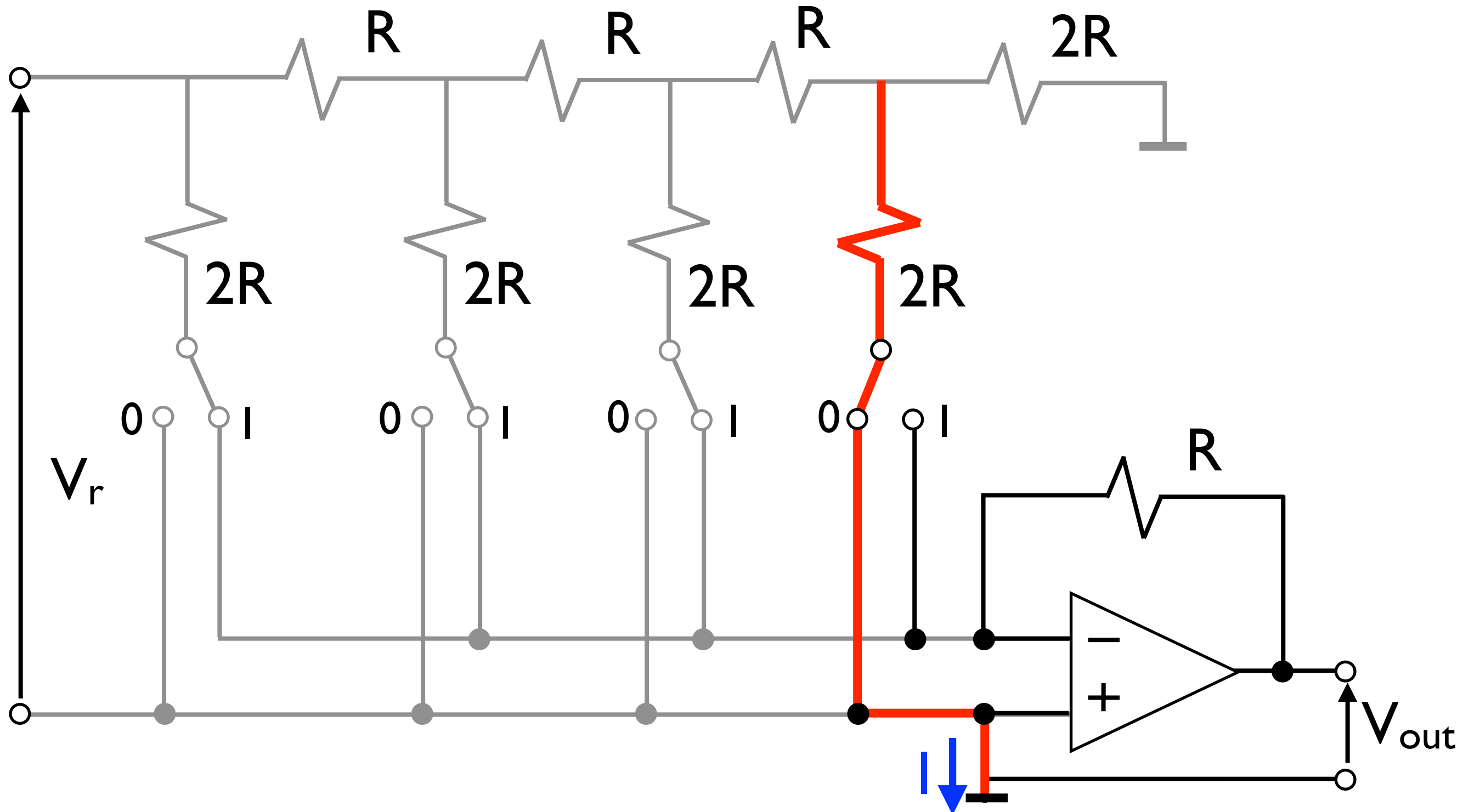




## 2 - DAC using R-2R Resistance ladder

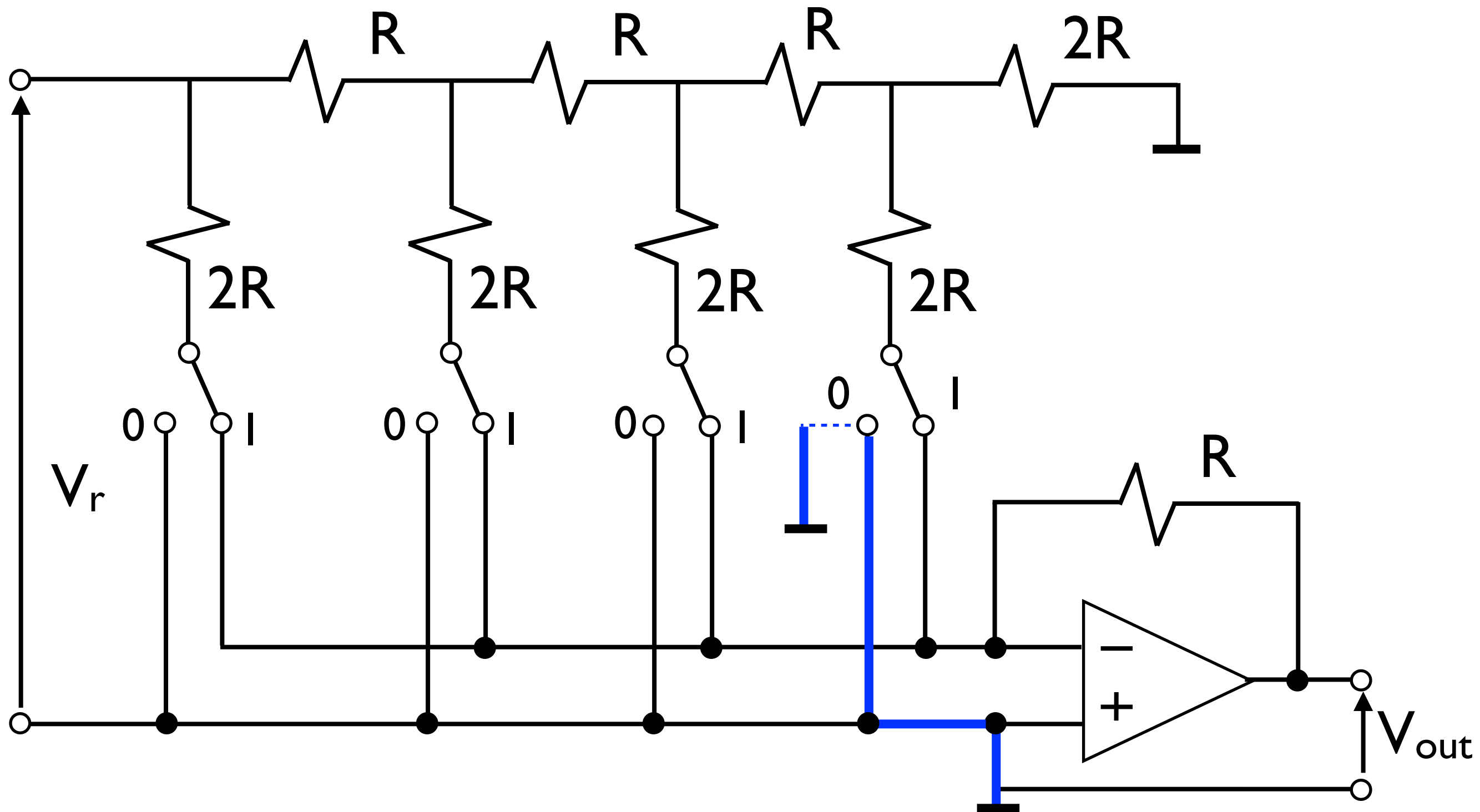


## 2 - DAC using R-2R Resistance ladder



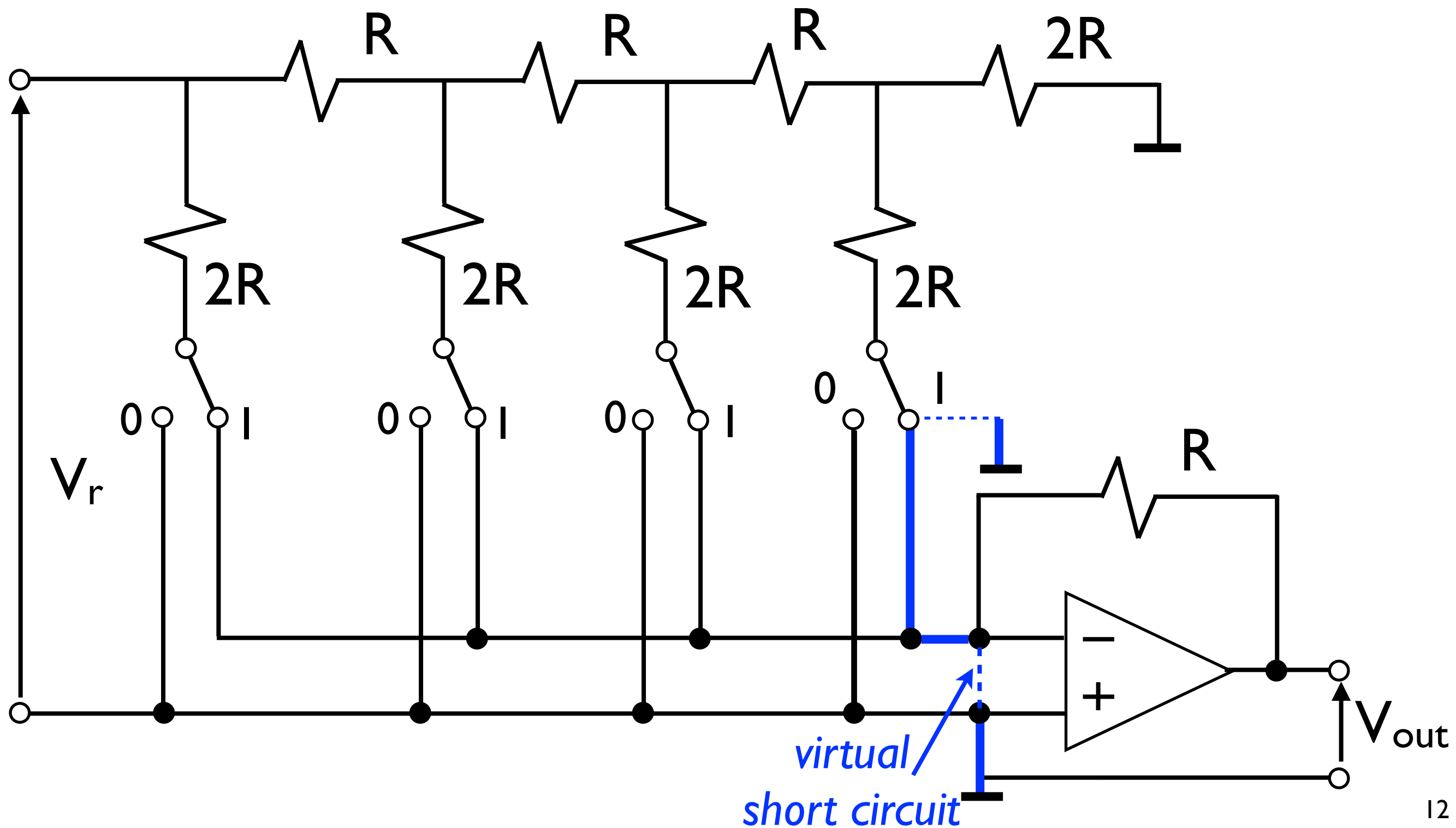
## 2 - DAC using R-2R Resistance ladder

*In both cases  $2R$  is connected to ground*



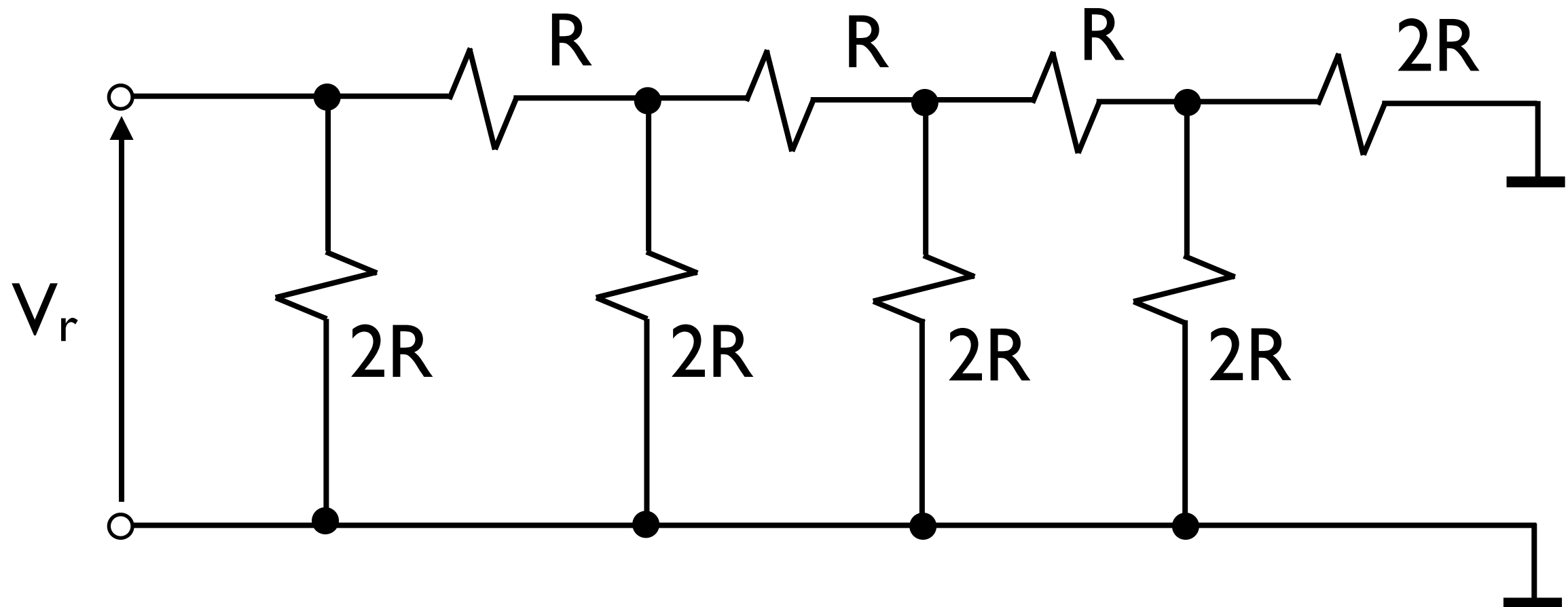
## 2 - DAC using R-2R Resistance ladder

*In both cases  $2R$  is connected to ground*

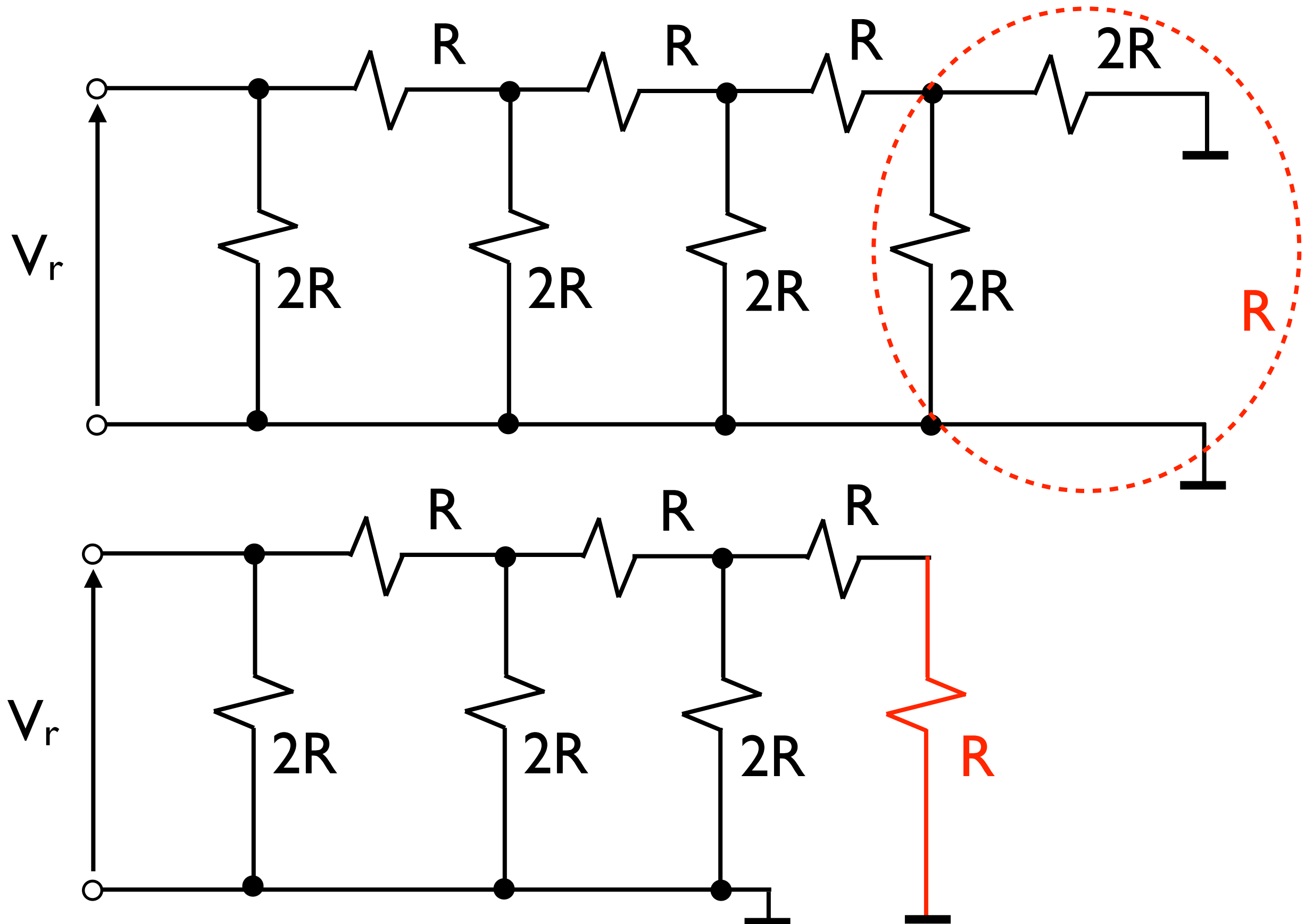


## 2 - DAC using R-2R Resistance ladder

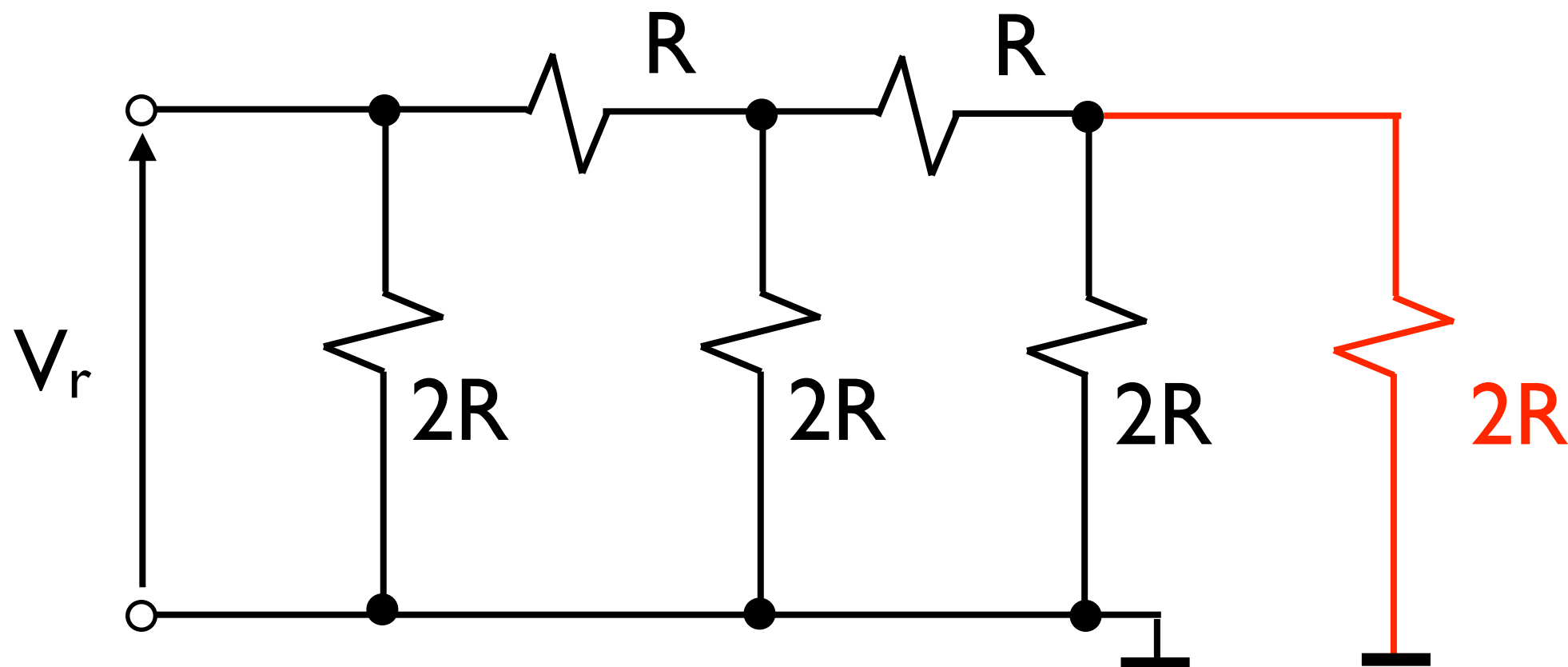
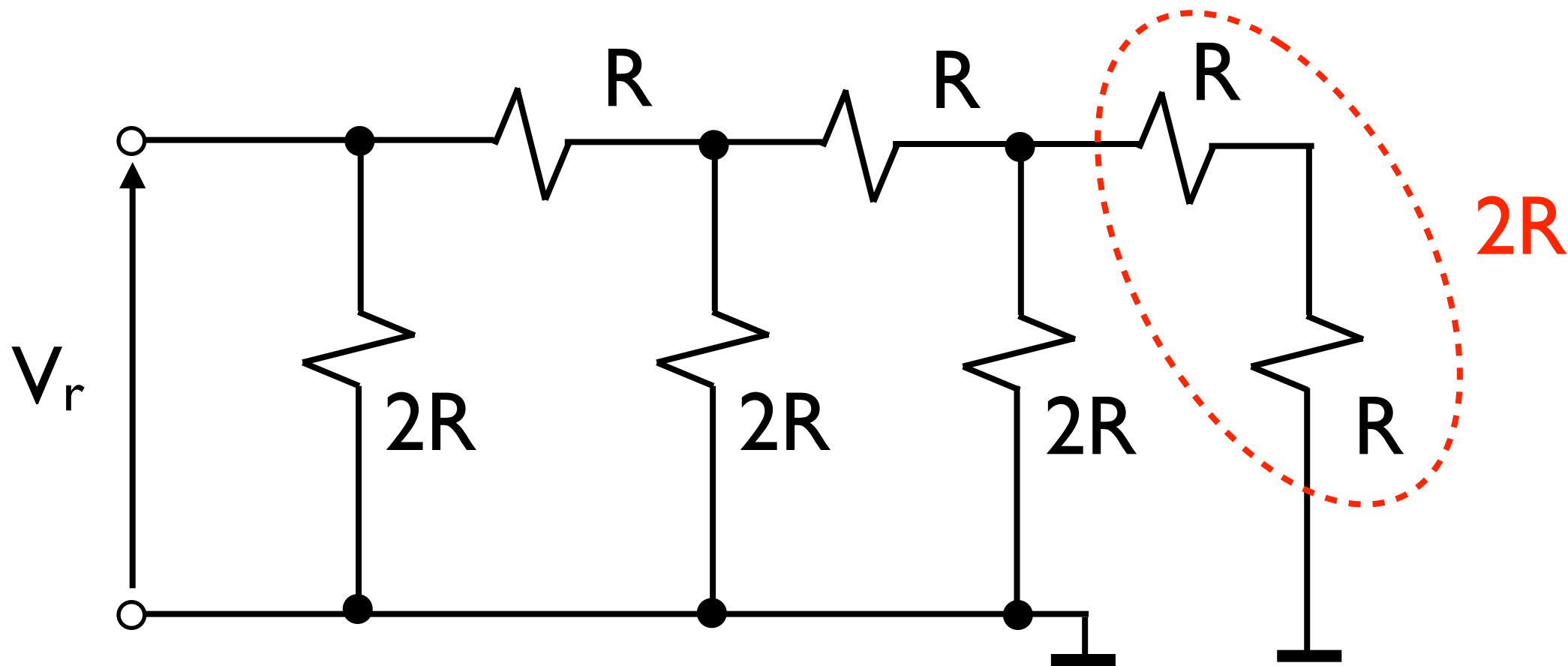
*Equivalent circuit resistive ladder*



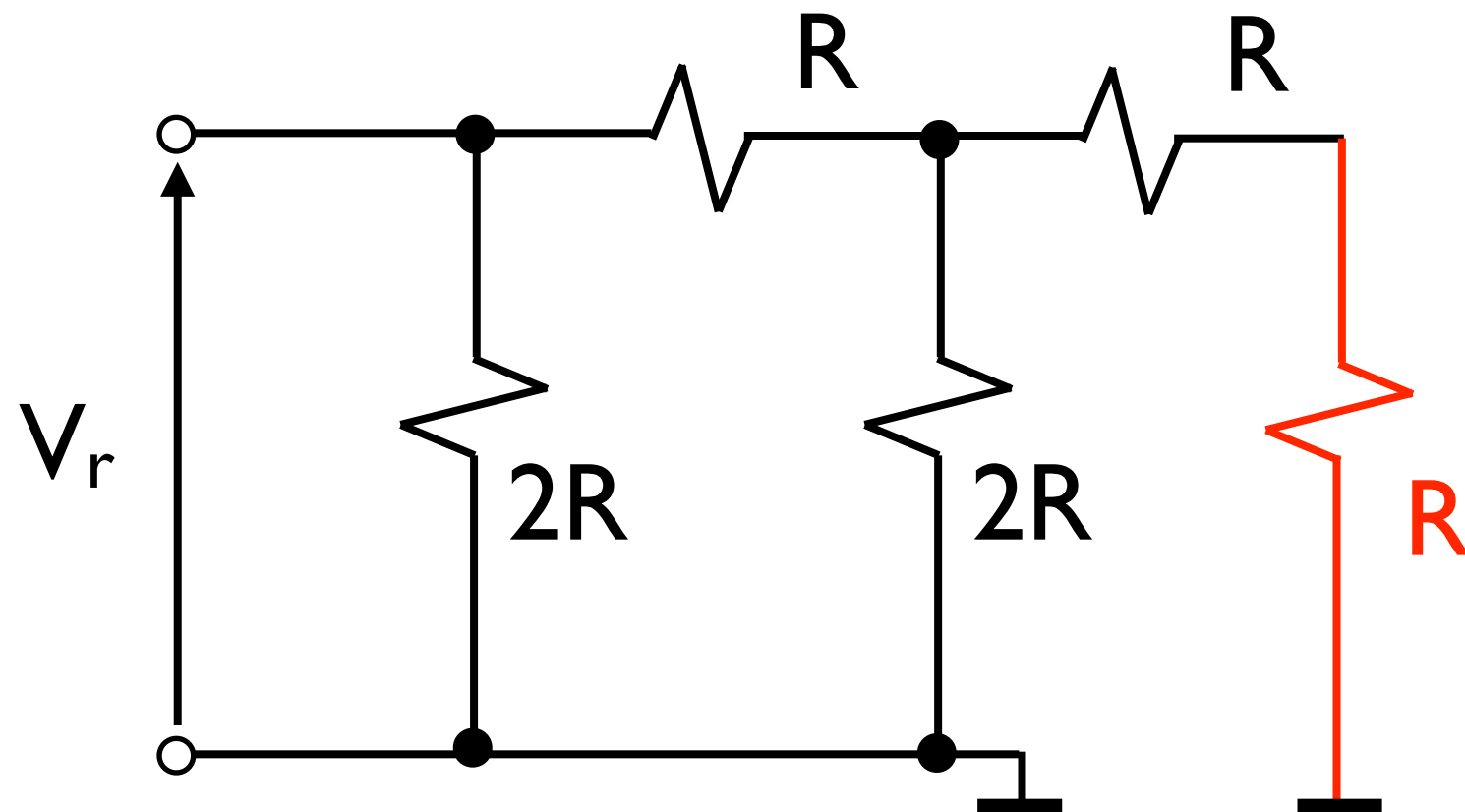
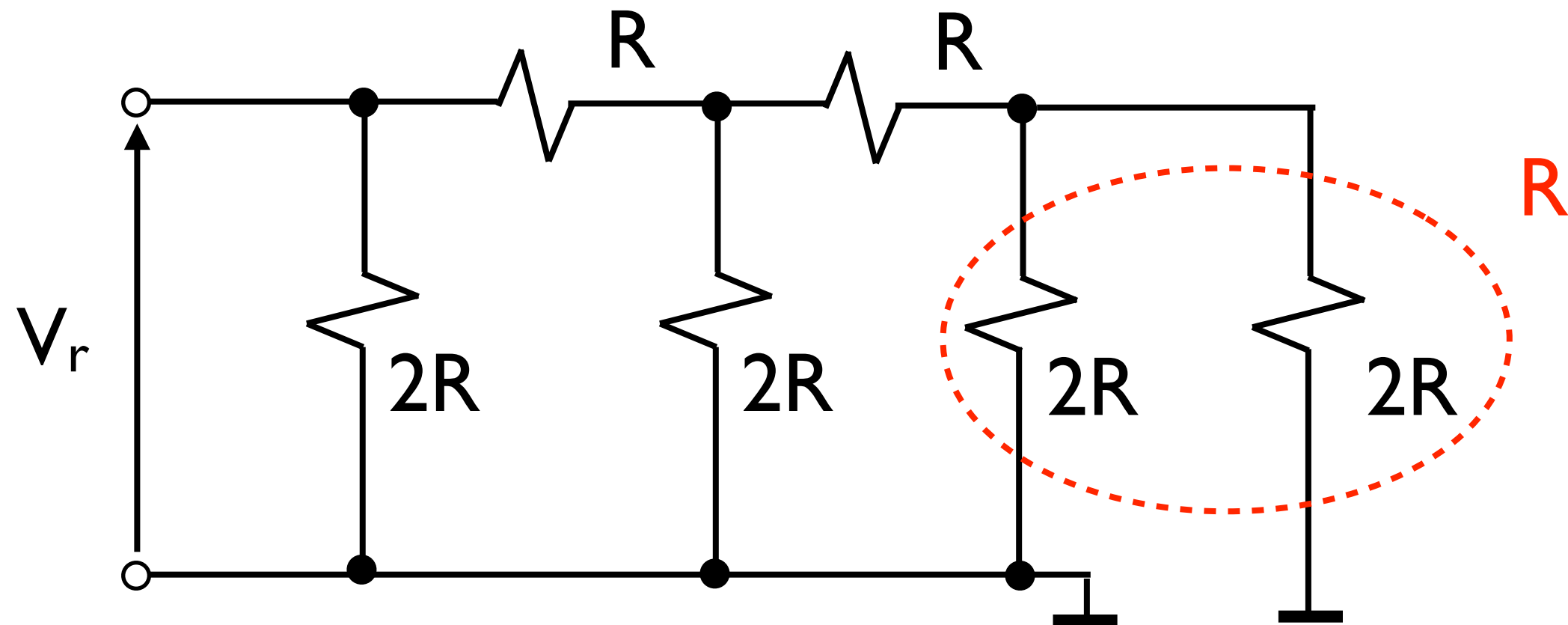
## 2 - DAC using R-2R Resistance ladder



## 2 - DAC using R-2R Resistance ladder

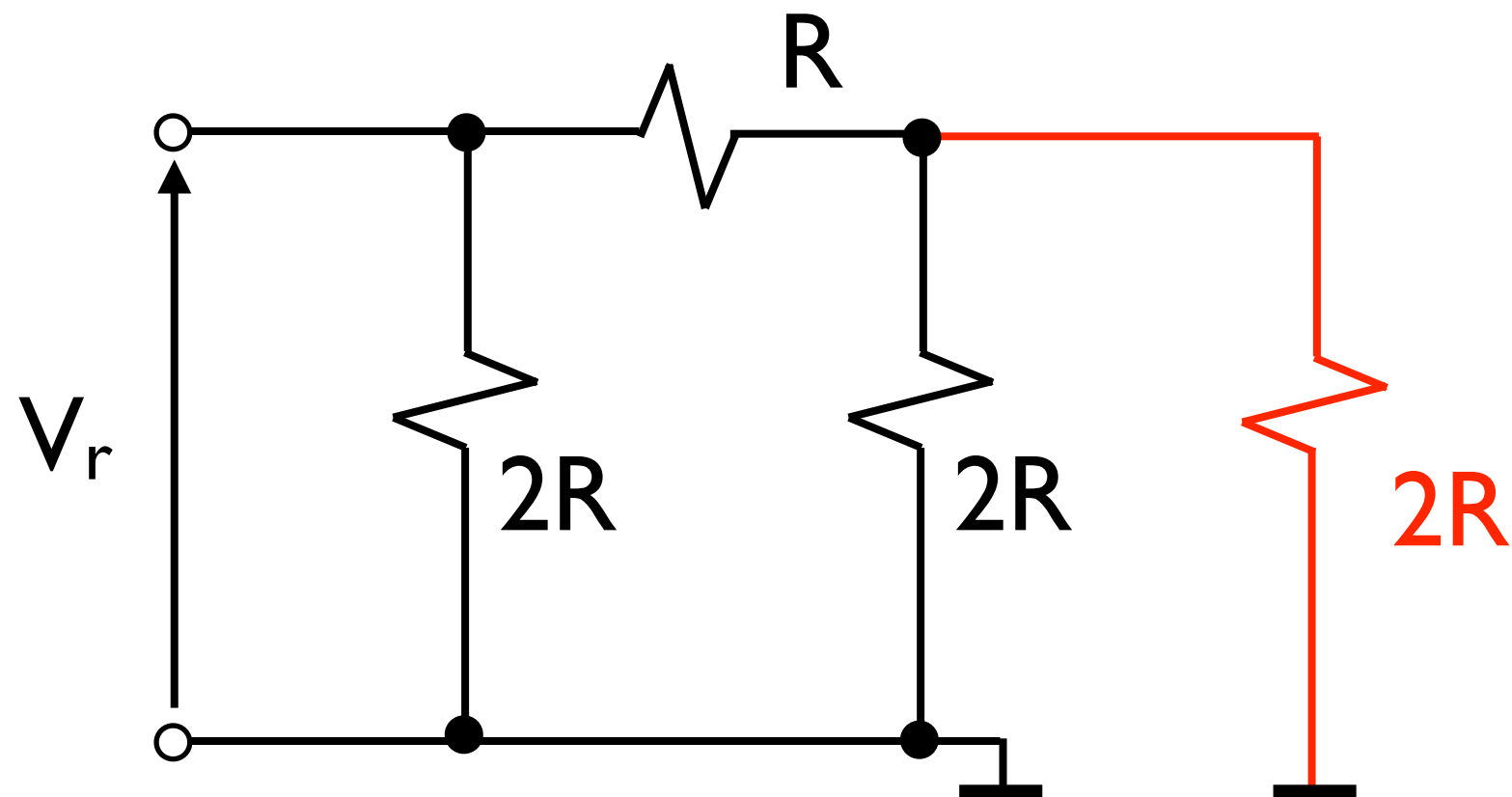
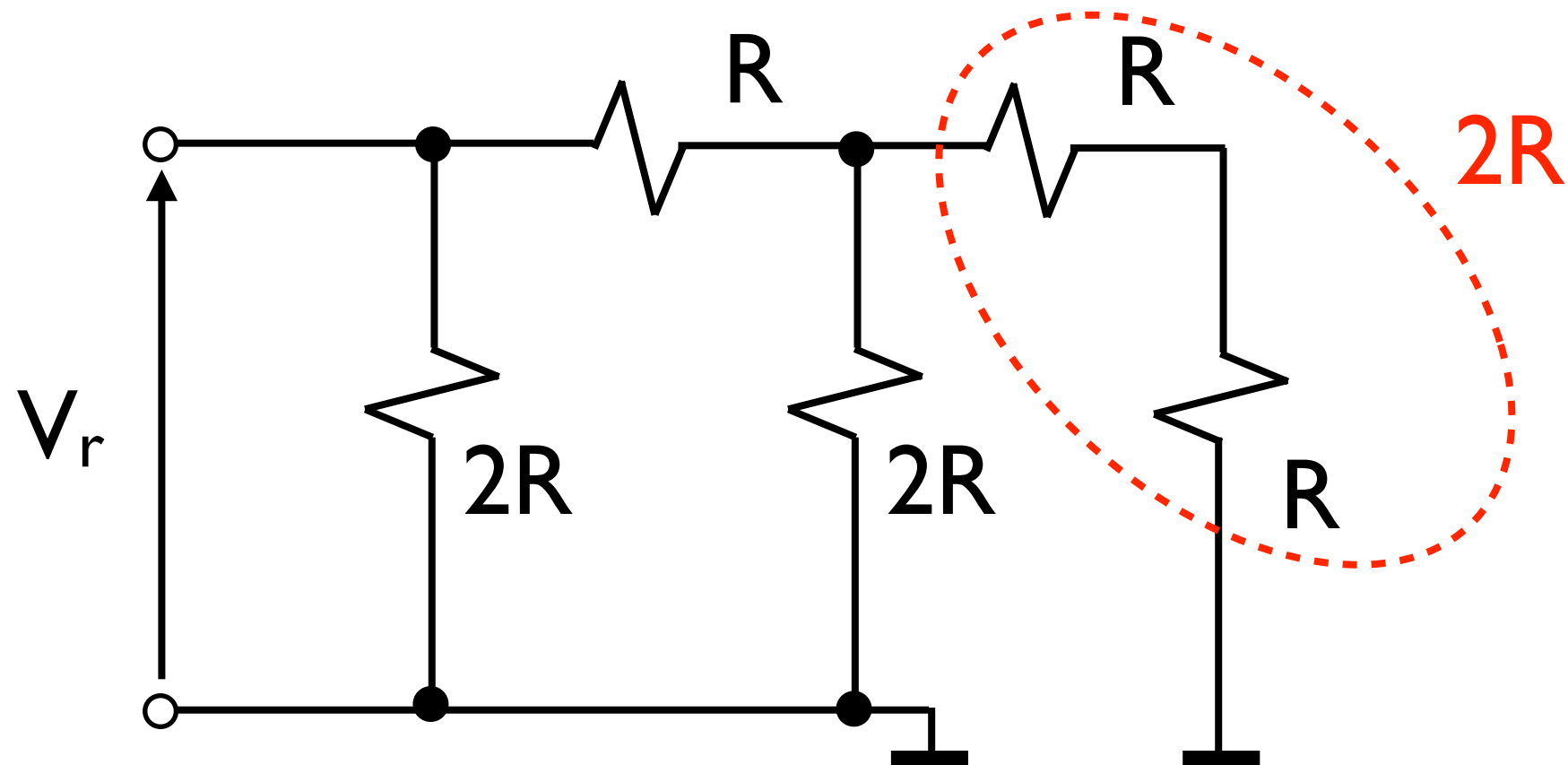


## 2 - DAC using R-2R Resistance ladder



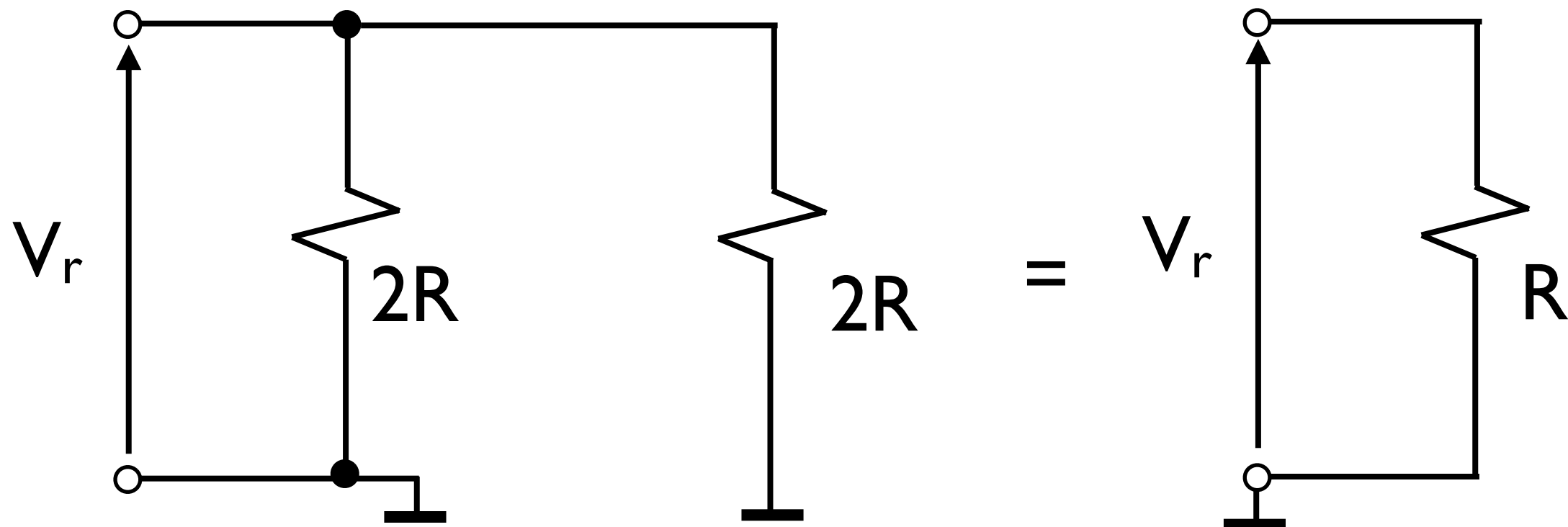


## 2 - DAC using R-2R Resistance ladder



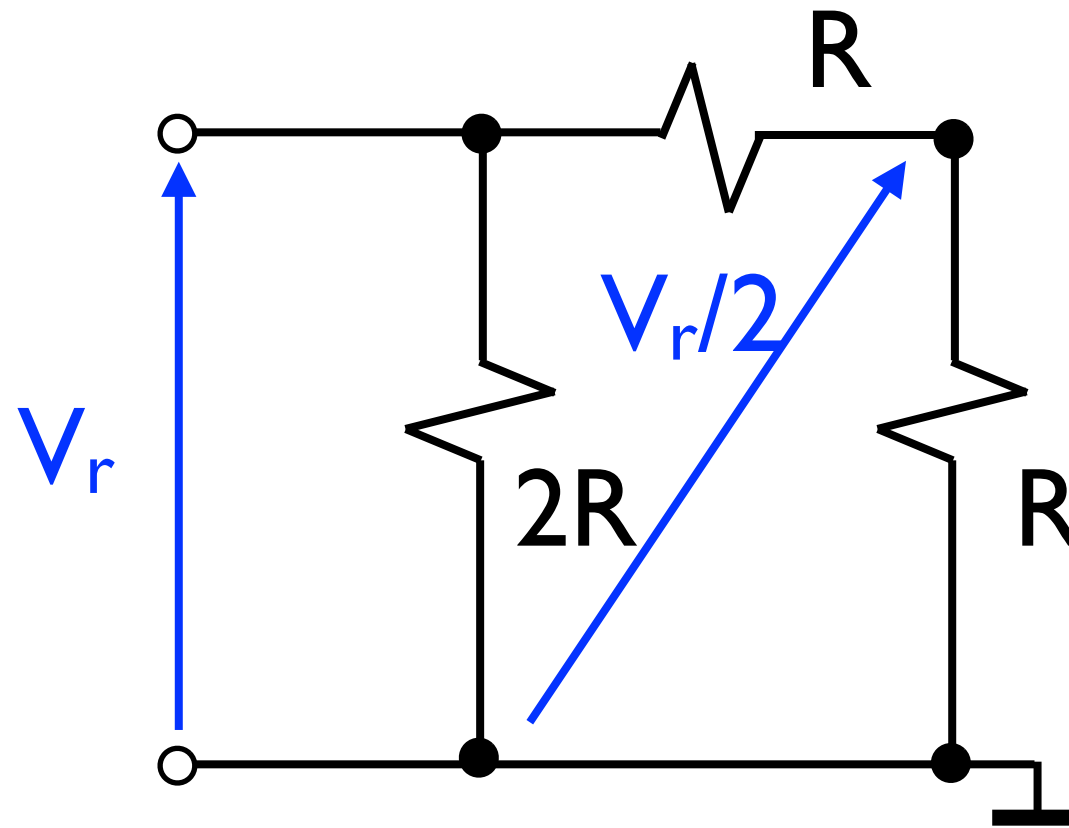
## 2 - DAC using R-2R Resistance ladder

*The reference voltage is applied to R*



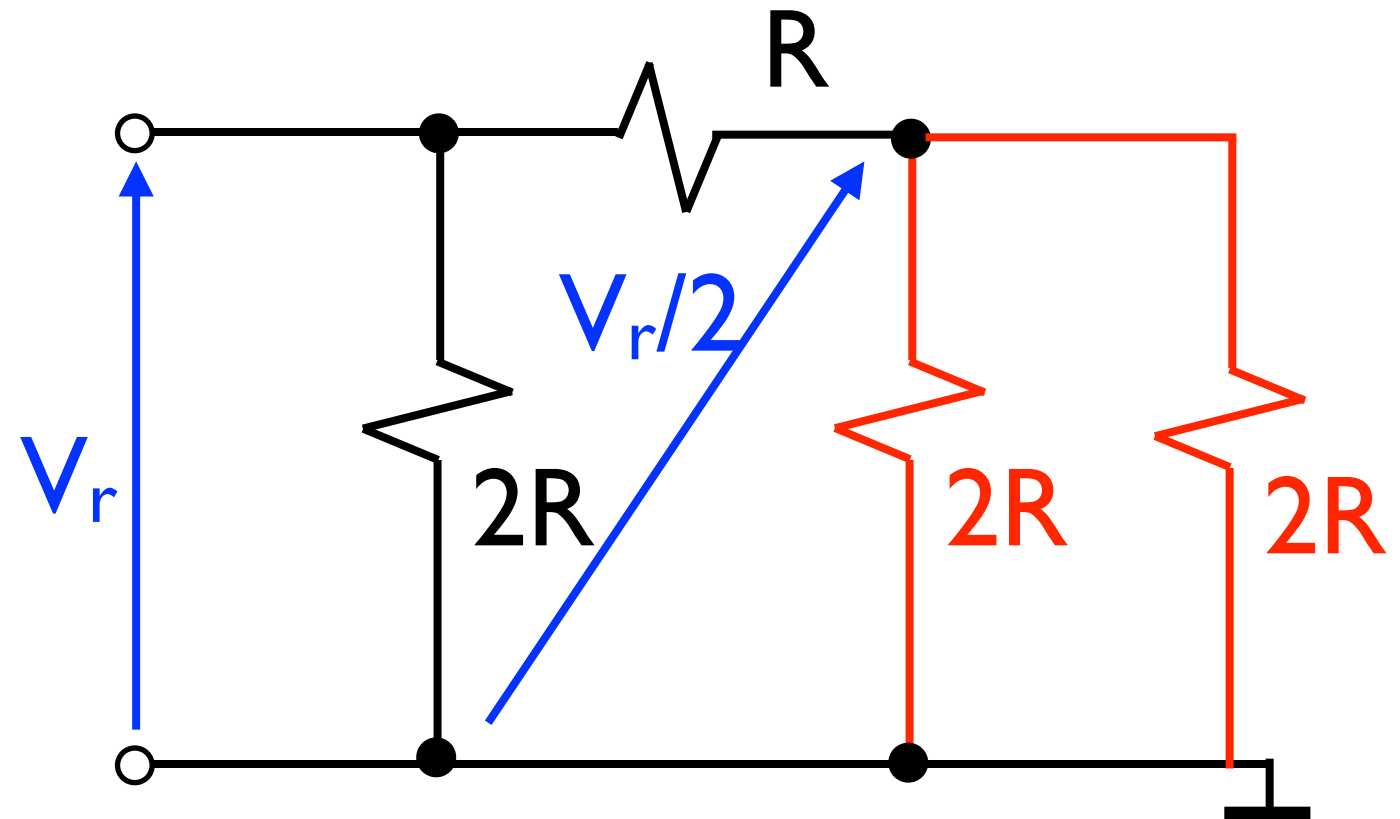
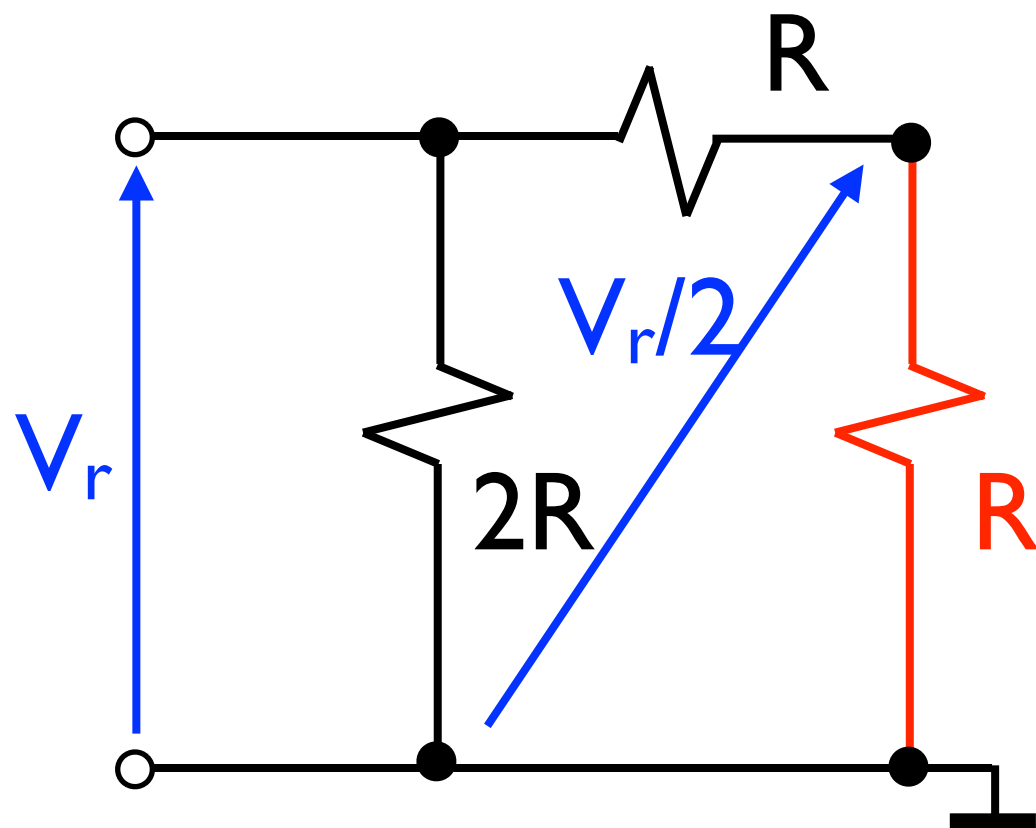
## 2 - DAC using R-2R Resistance ladder

*at each stage the voltage is divided by 2*



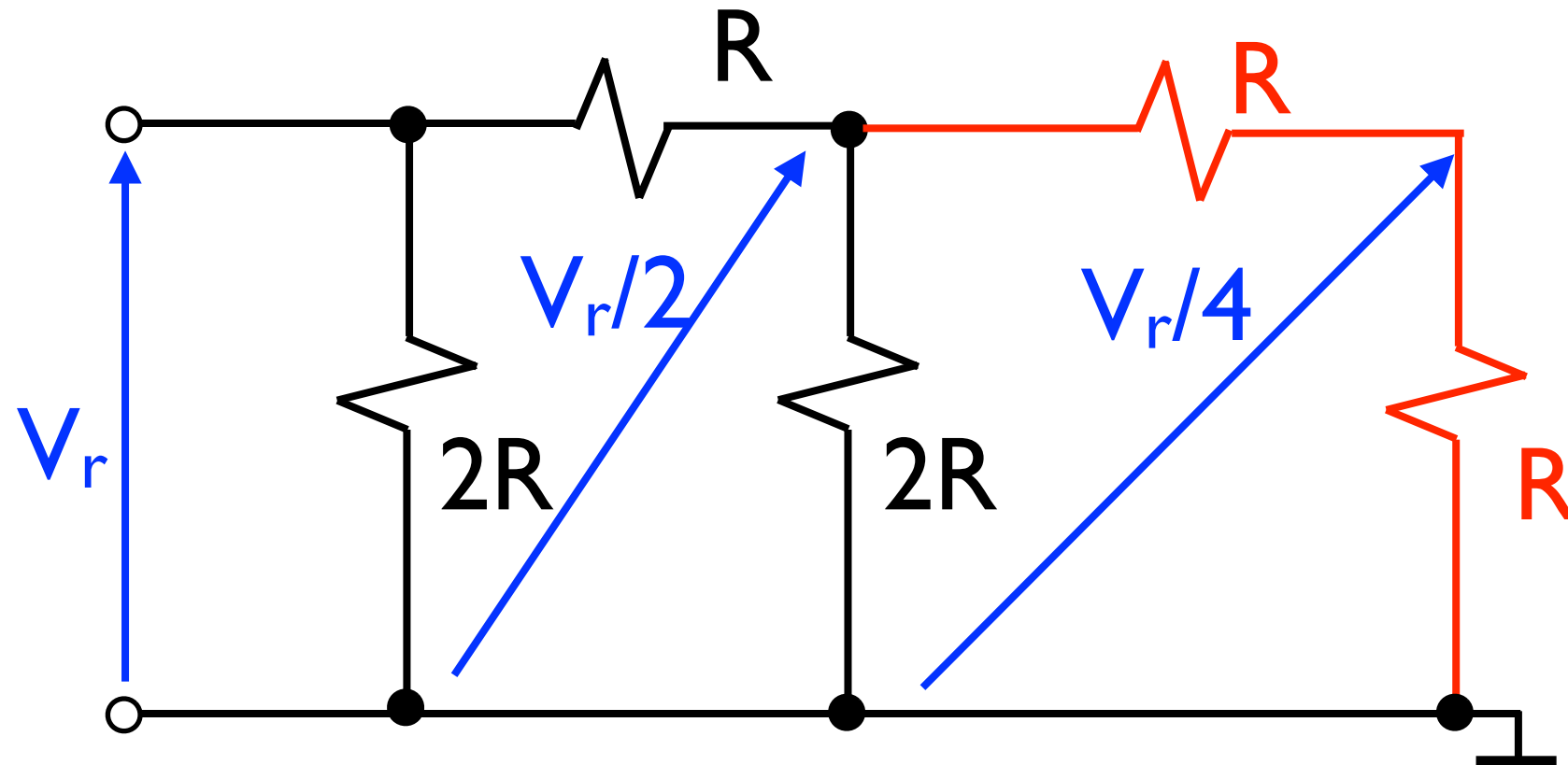
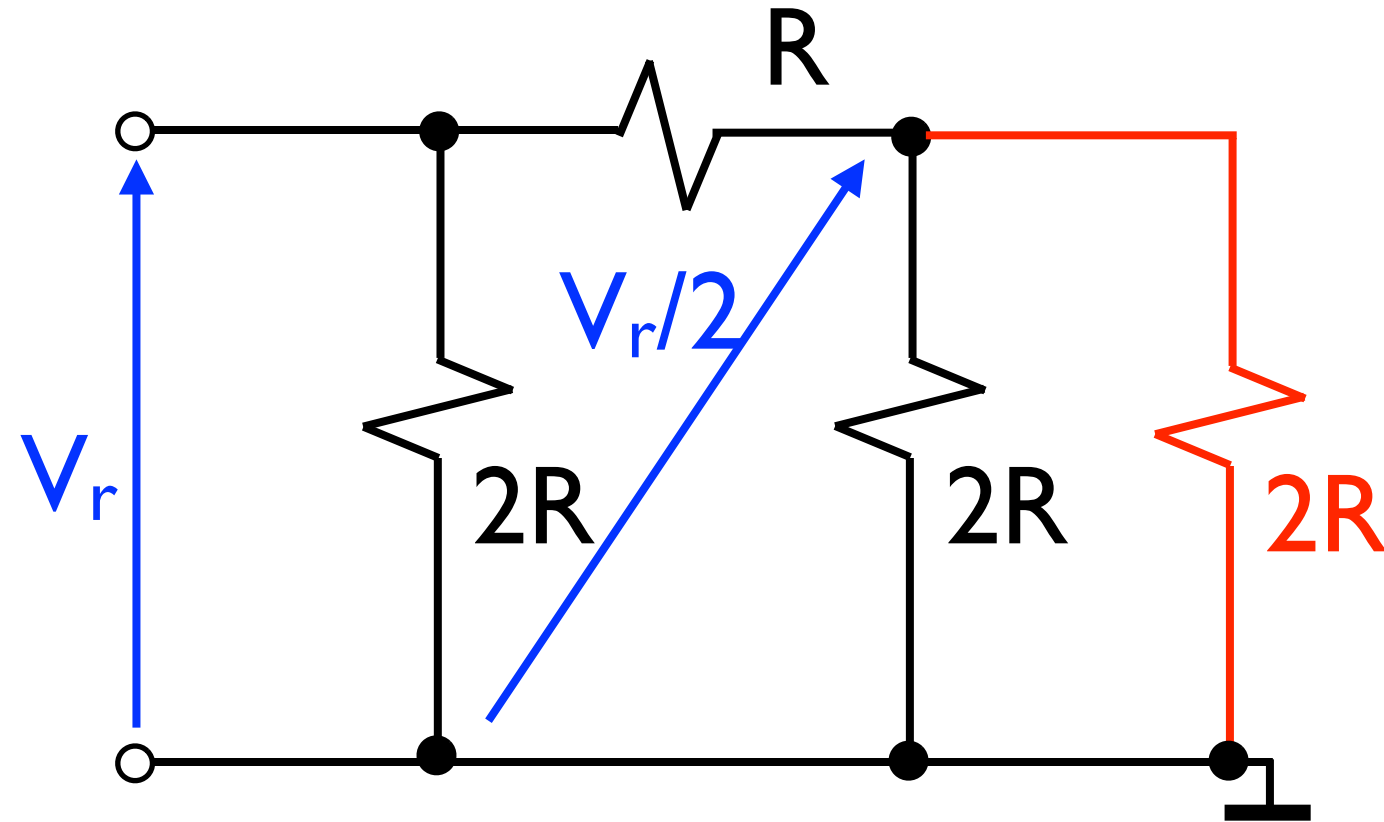
## 2 - DAC using R-2R Resistance ladder

*at each stage the voltage is divided by 2*



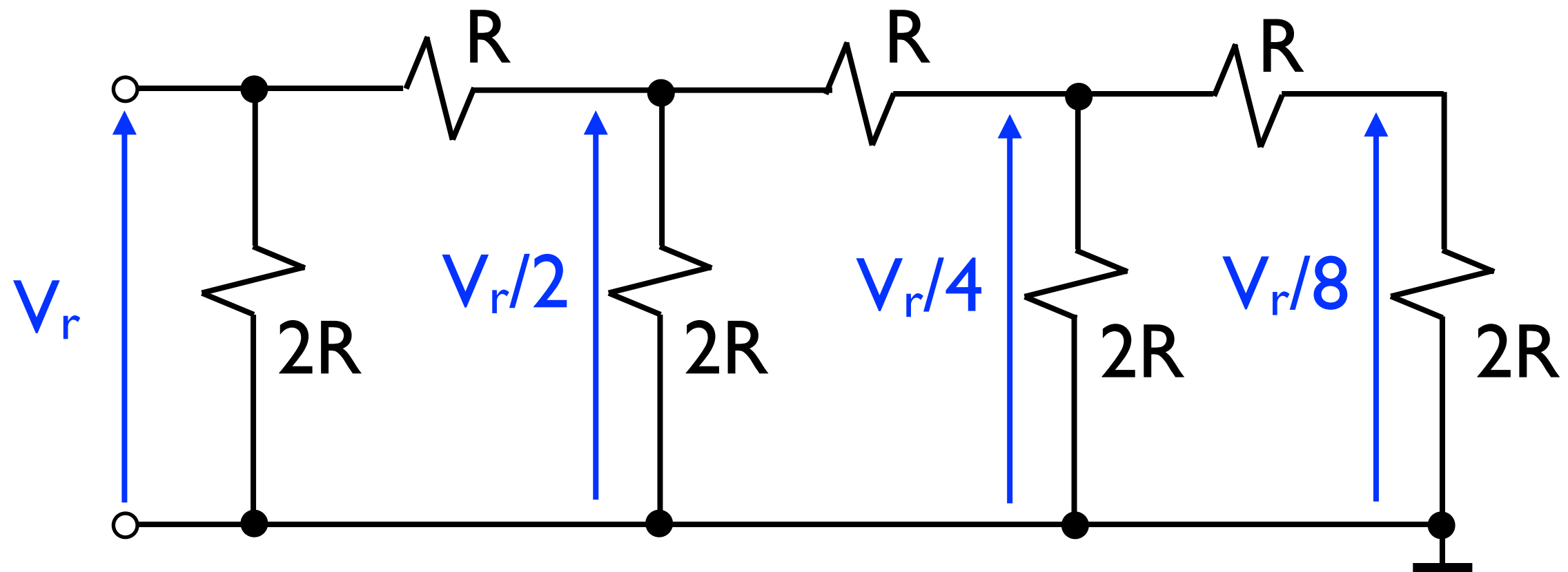
## 2 - DAC using R-2R Resistance ladder

*at each stage the voltage is divided by 2*



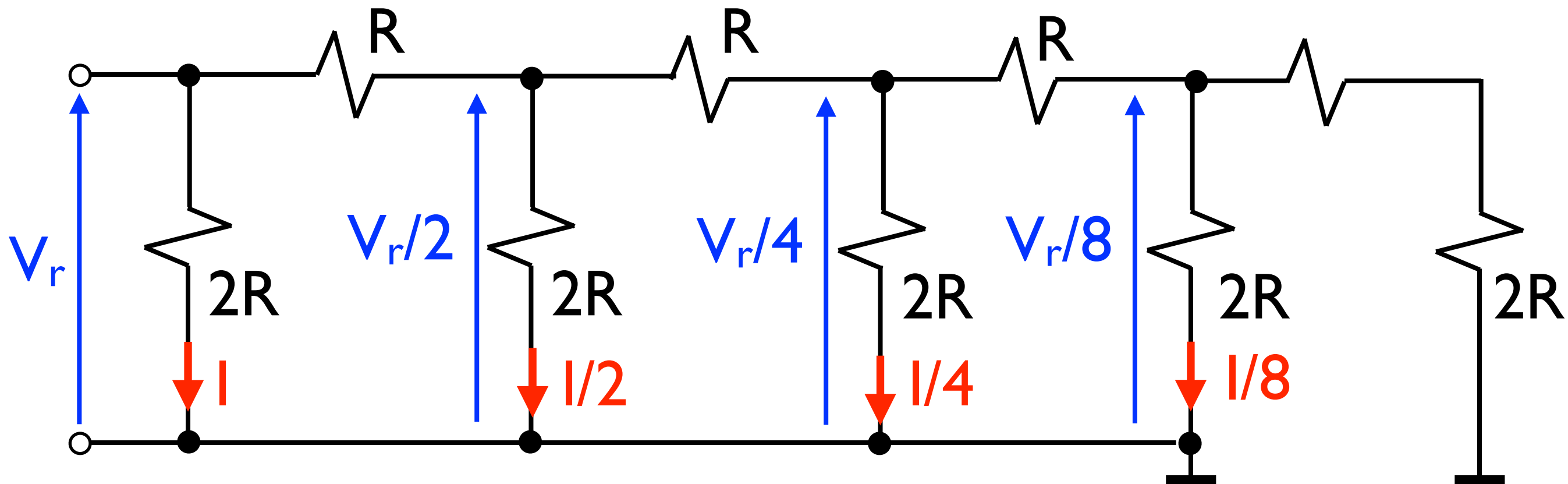
## 2 - DAC using R-2R Resistance ladder

*at each stage the voltage is divided by 2*

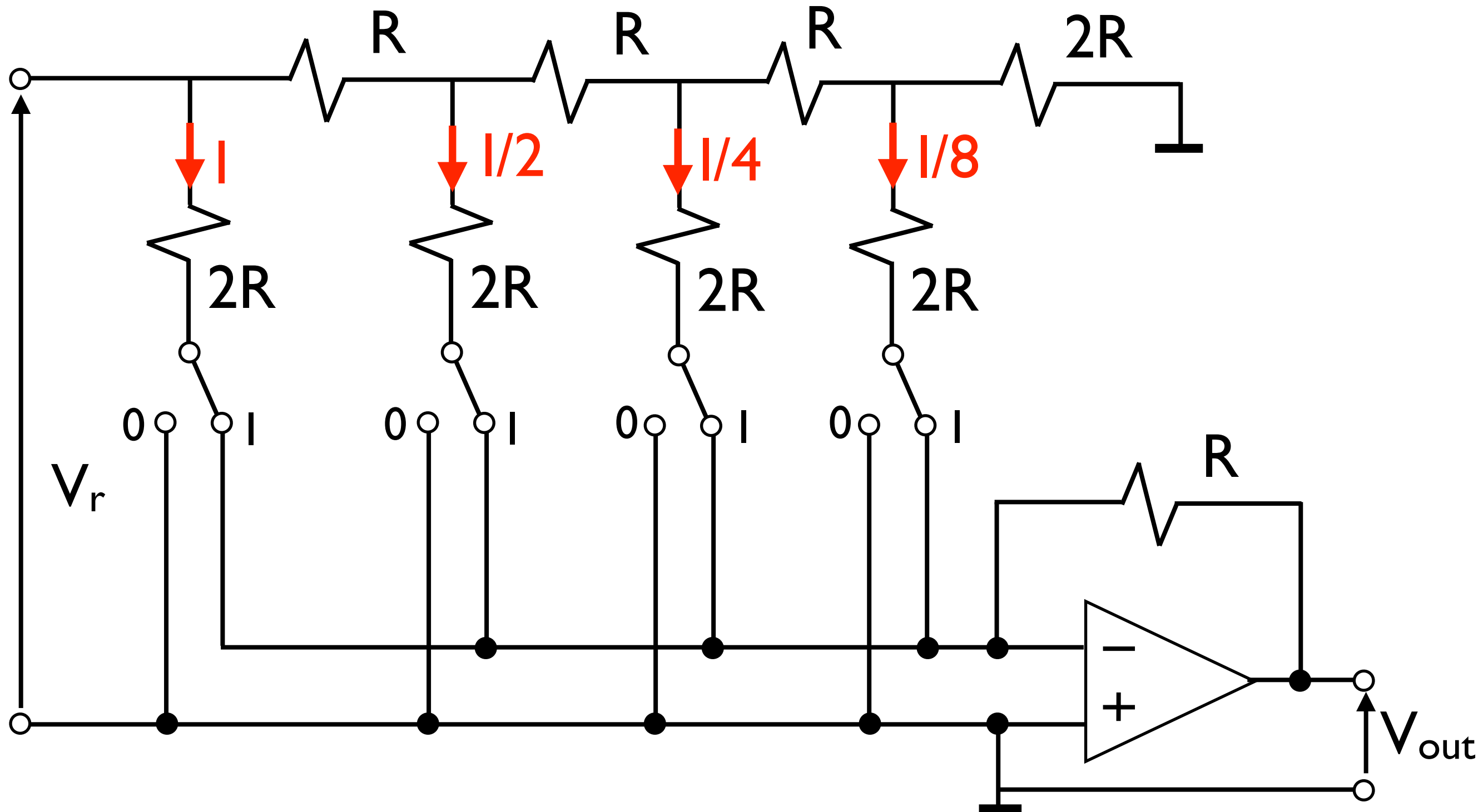


## 2 - DAC using R-2R Resistance ladder

*Each current flowing through each resistor is half of the previous current*

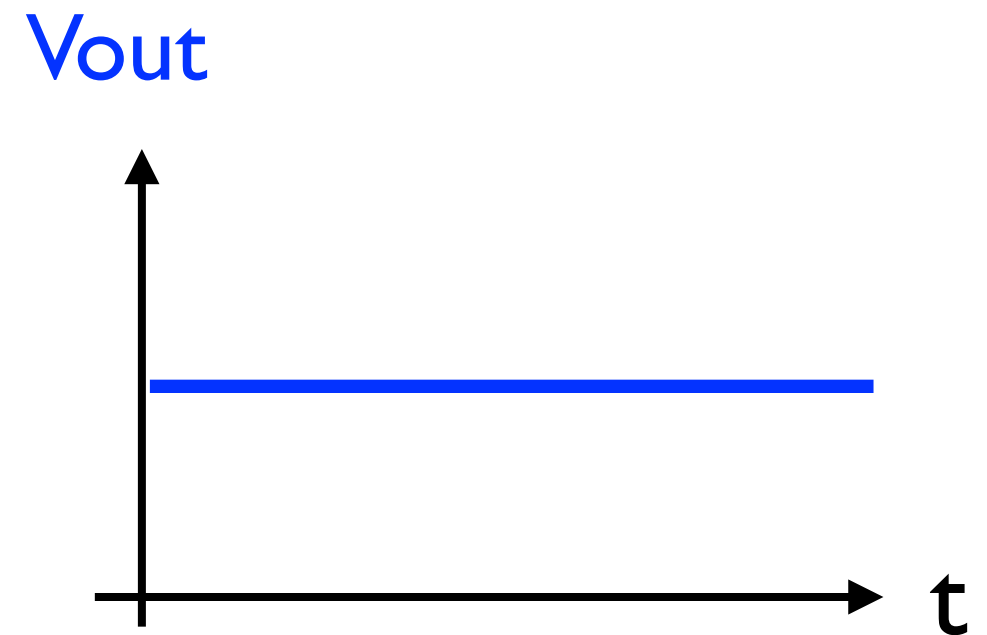
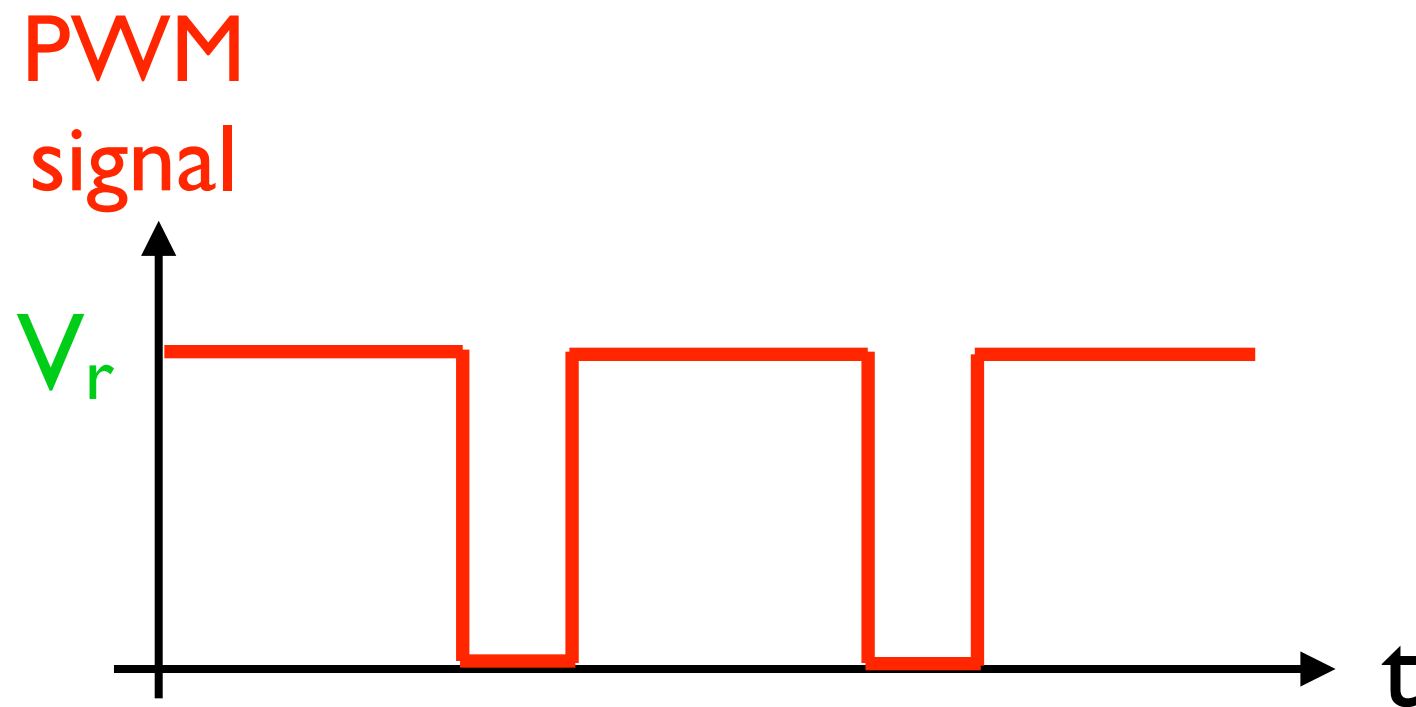
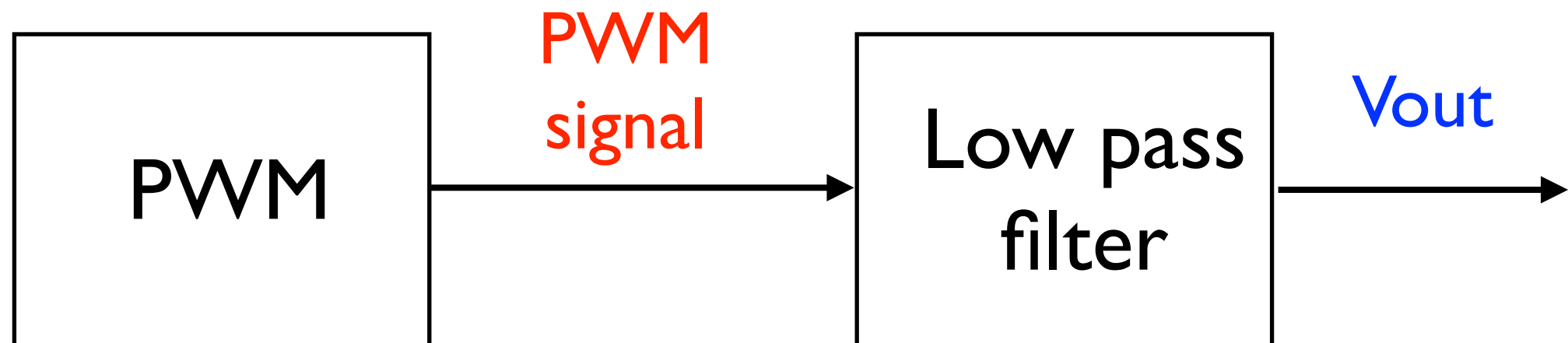


## 2 - DAC using R-2R Resistance ladder

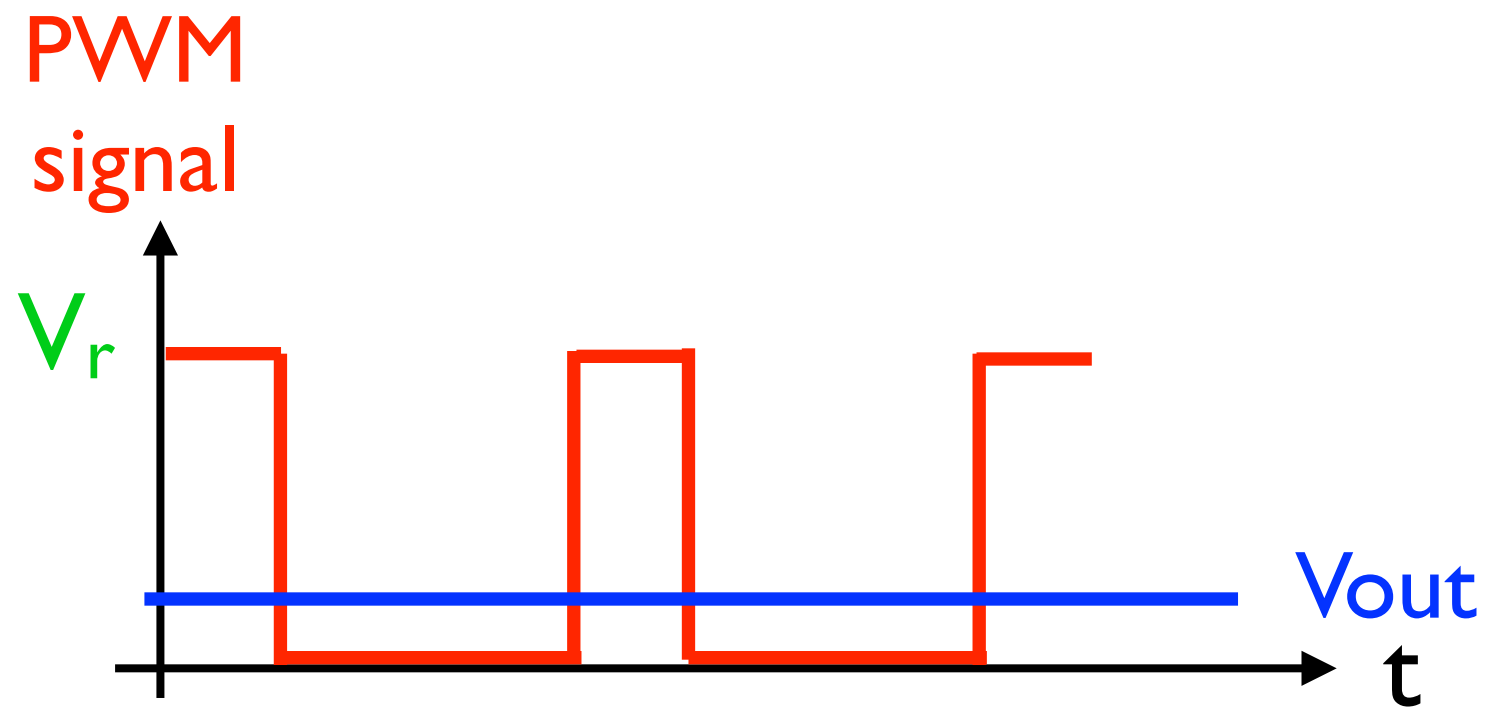
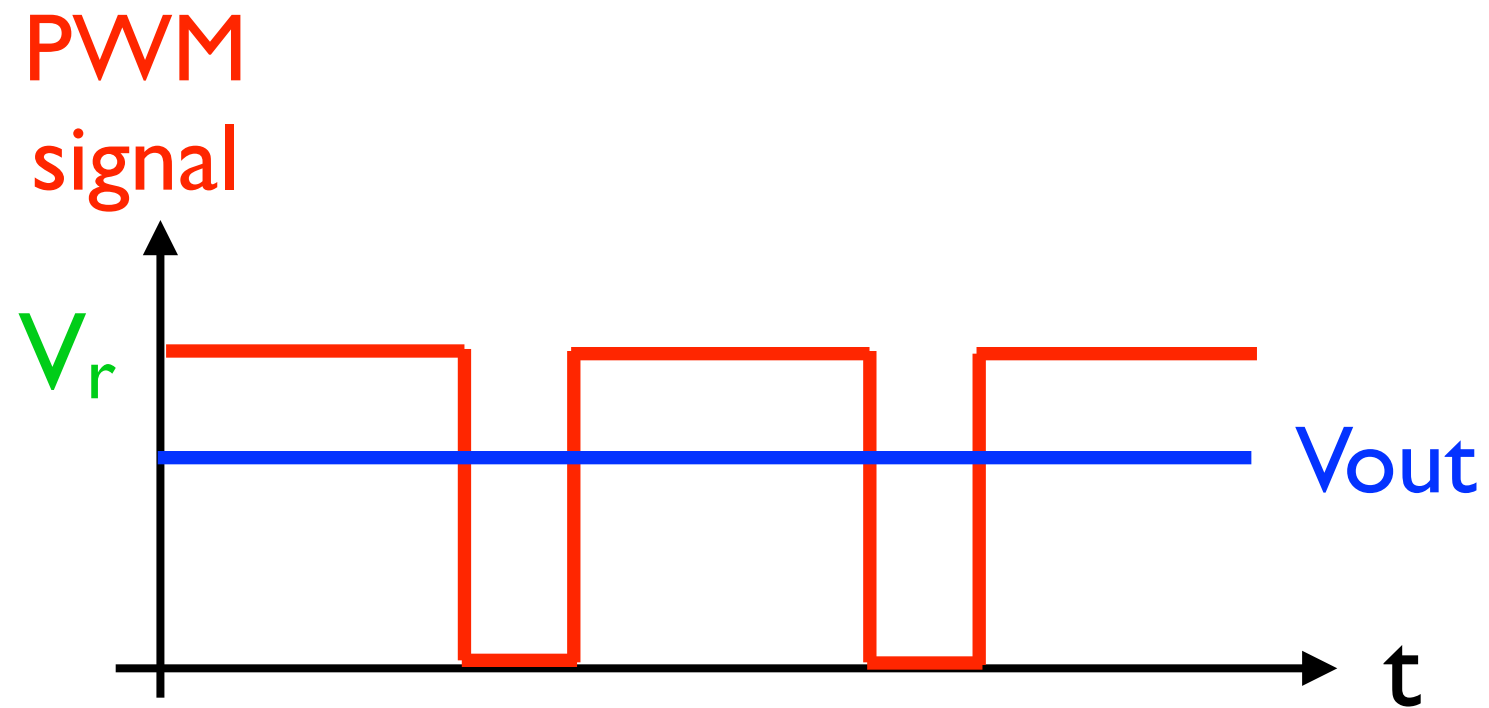




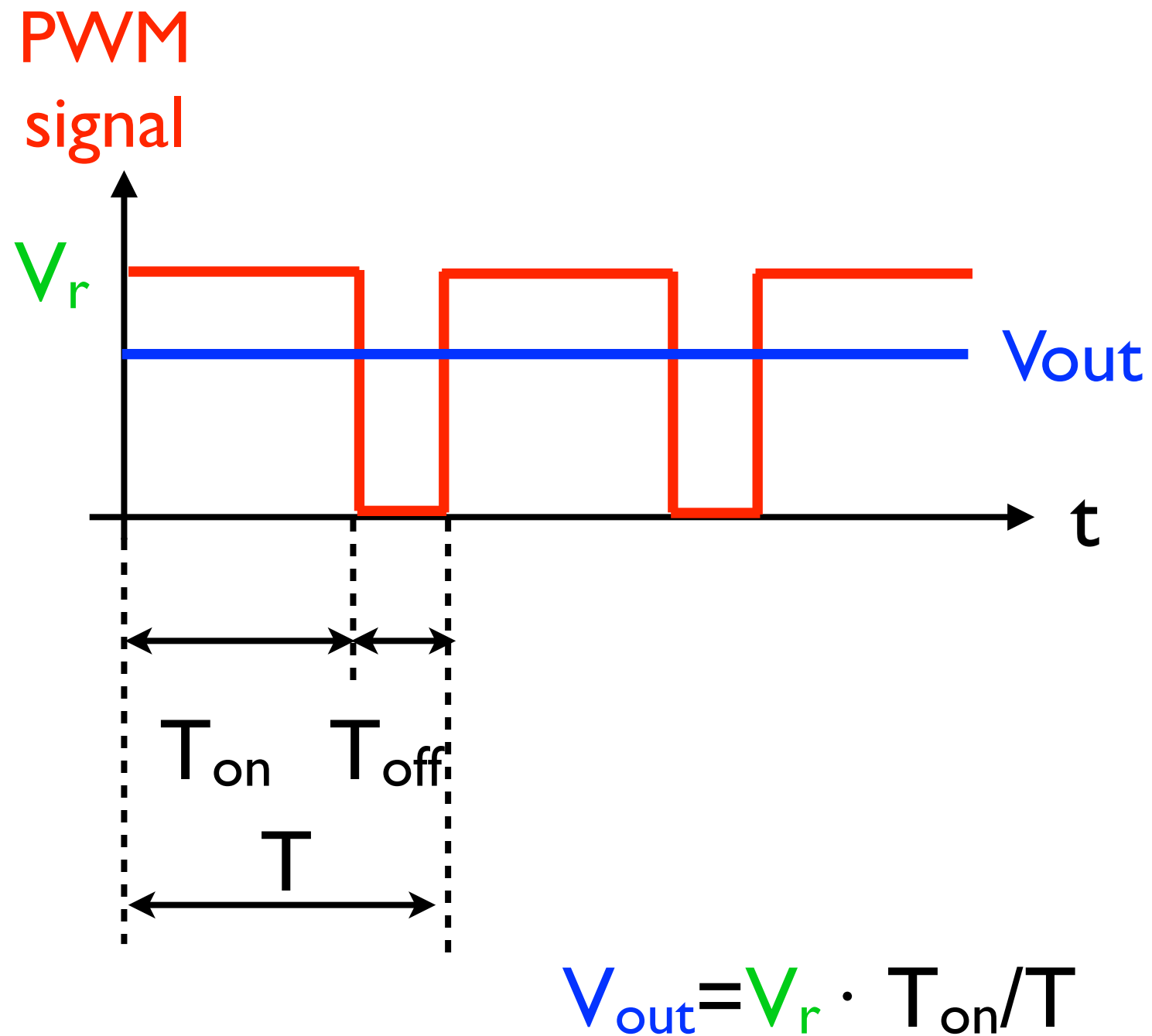
### 3 - DAC based on PWM



### 3 - DAC based on PWM



### 3 - DAC based on PWM

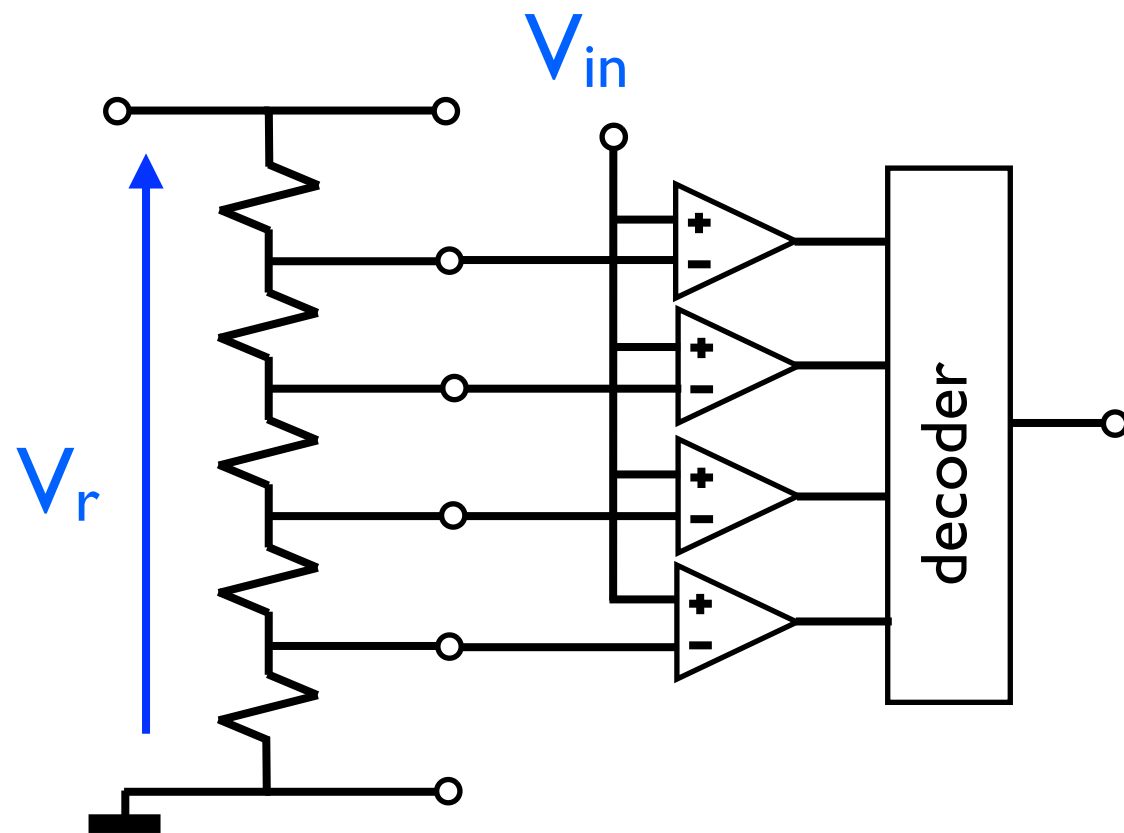


$$T = T_{on} + T_{off}$$

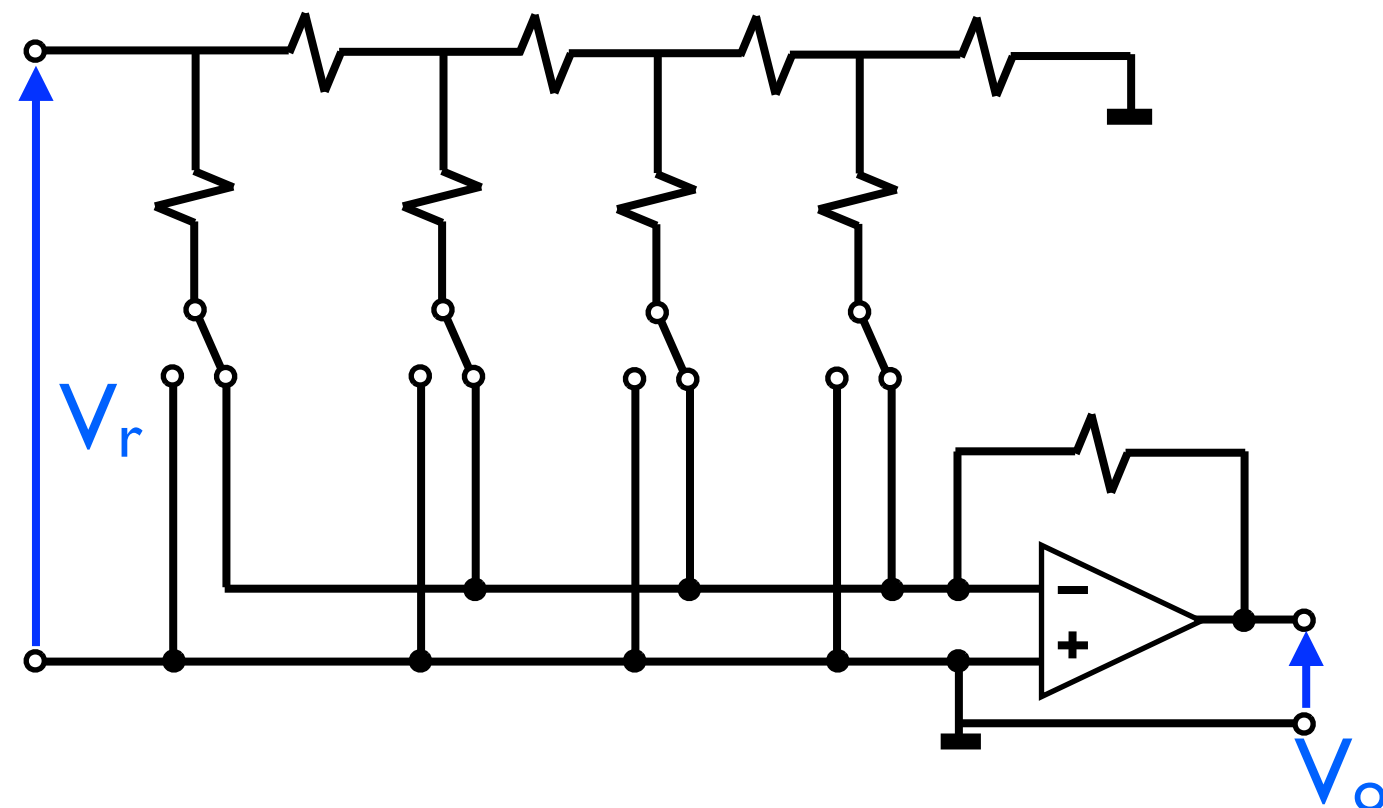
# VOLTAGE REFERENCES

- necessary for both ADCs and DACs
- they must provide constant voltage, independent on time and temperature

## ADC

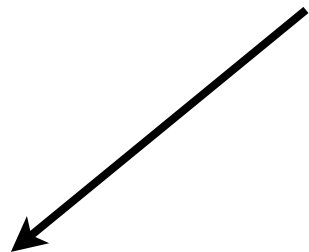


## DAC

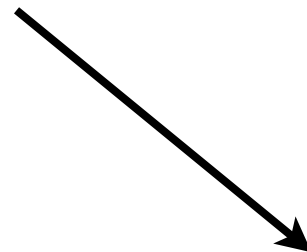


# VOLTAGE REFERENCES

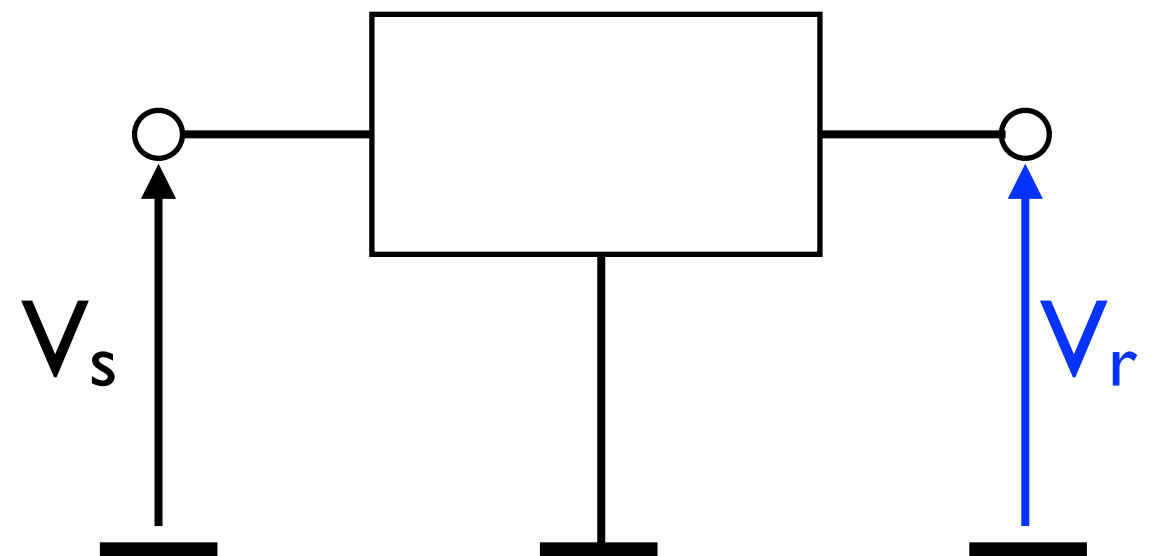
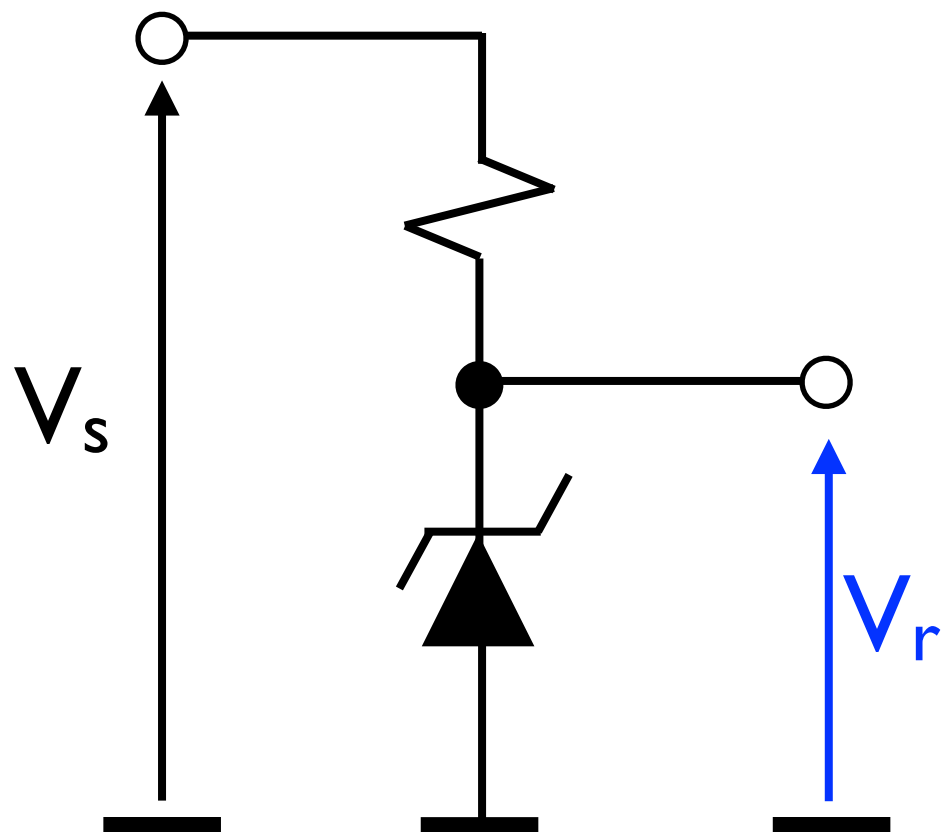
Two basic structures



SHUNT



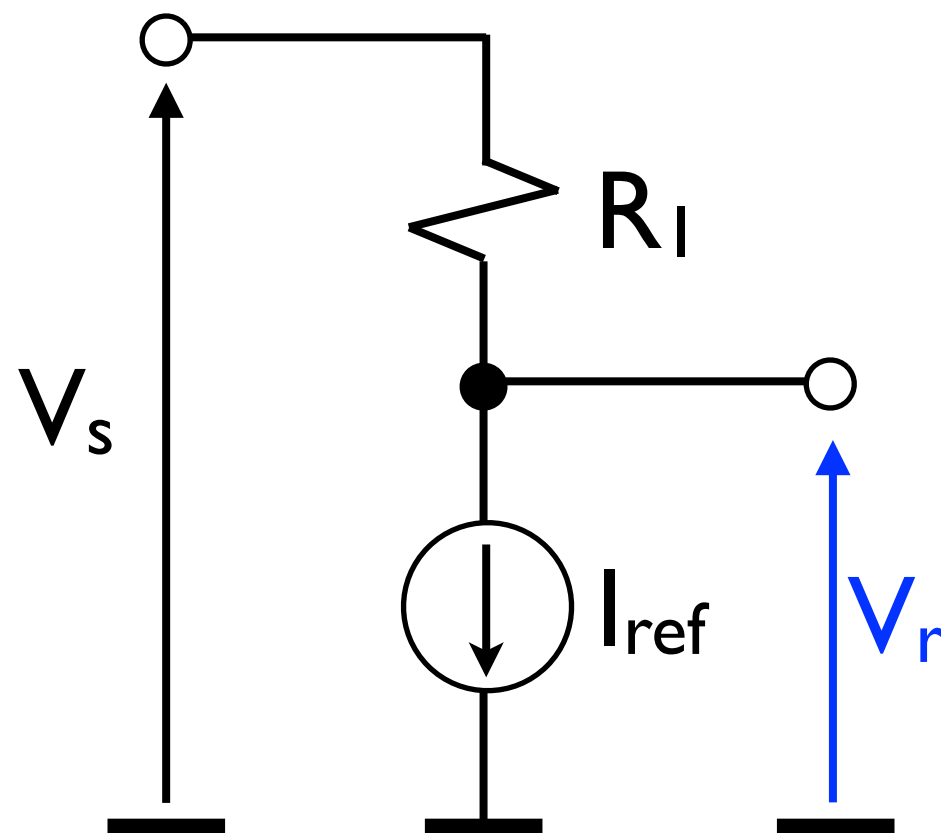
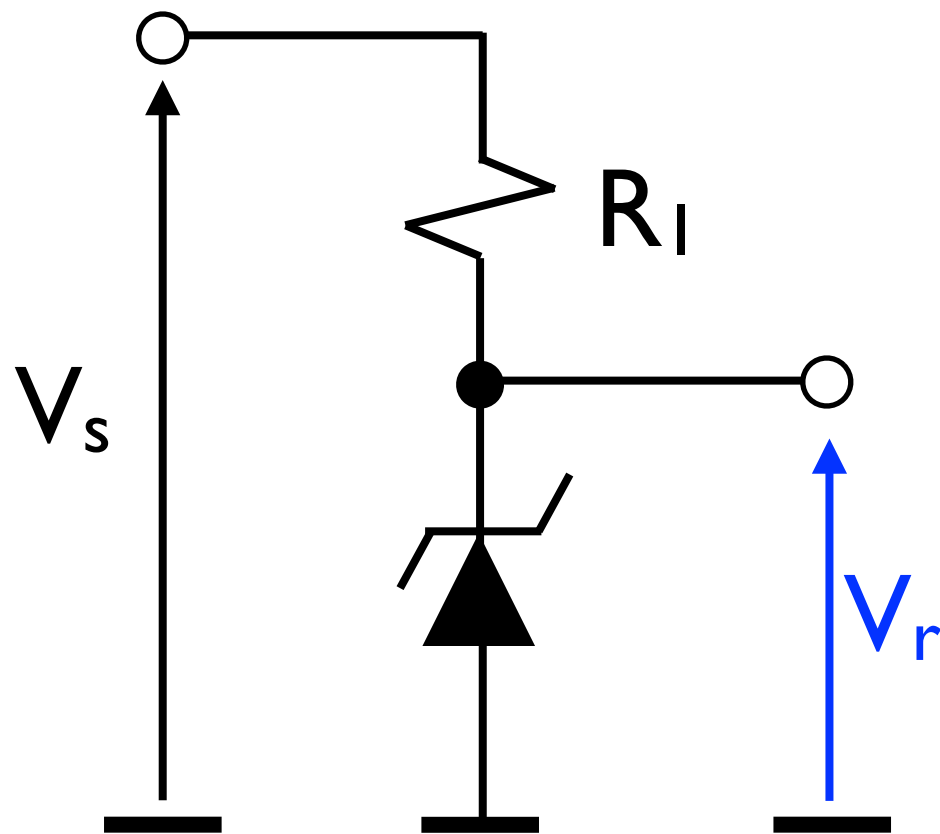
SERIES



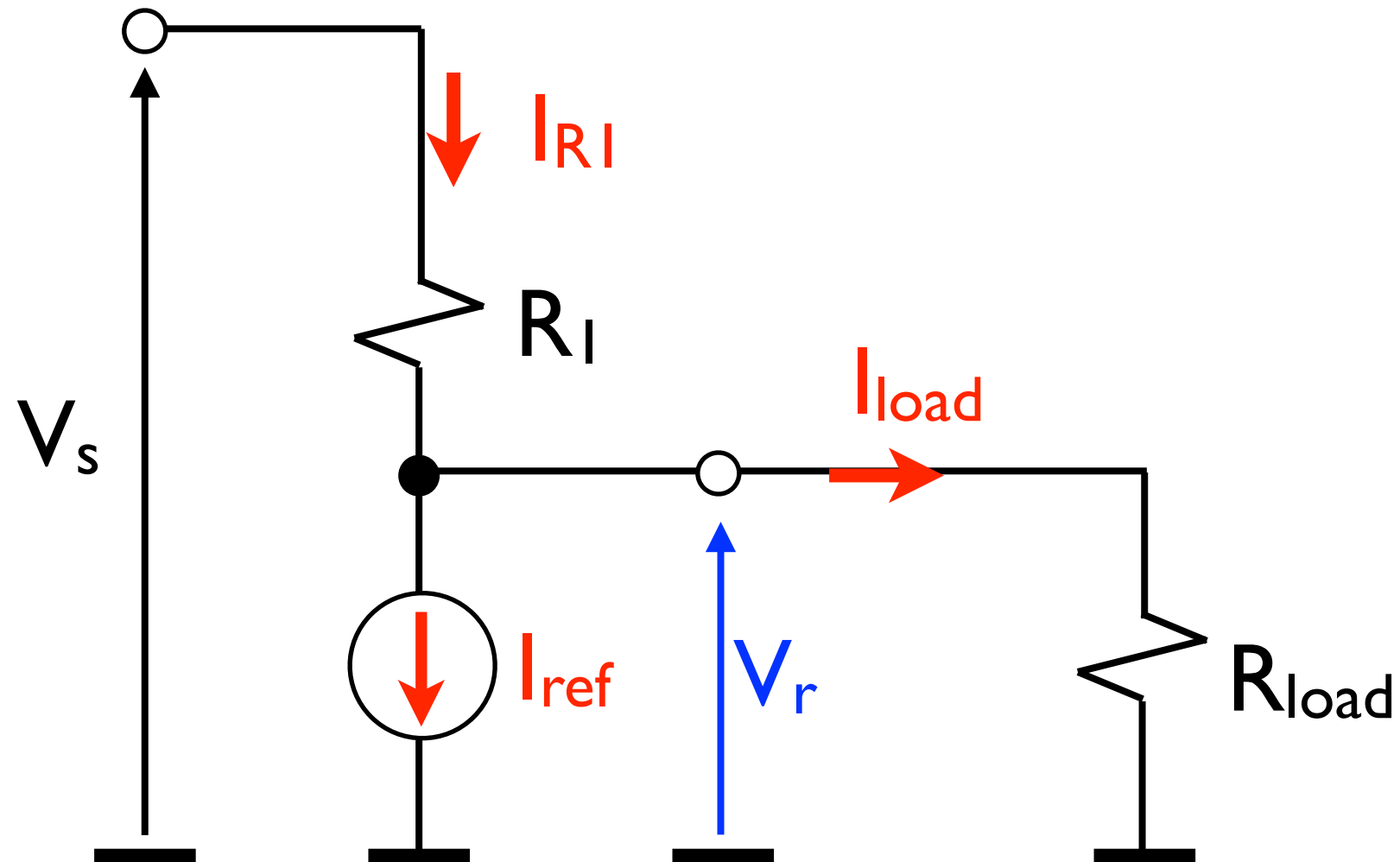
# SHUNT VOLTAGE REFERENCE

Working principle:

You can see it as a current source which adjust the current level in order to have constant  $V_r$



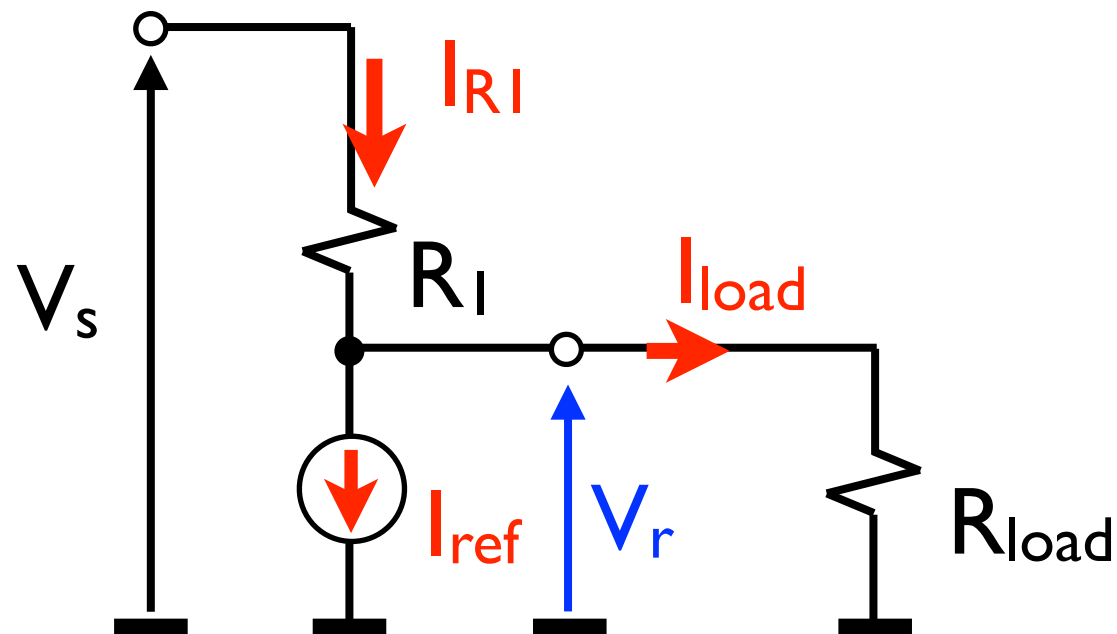
# SHUNT VOLTAGE REFERENCE



$$\begin{aligned} V_r &= V_s - R_I \cdot I_{RI} \\ &= V_s - R_I \cdot (I_{ref} + I_{load}) \end{aligned}$$

$I_{ref}$  is automatically adjusted so that  $I_{RI}$  is constant whatever is the load

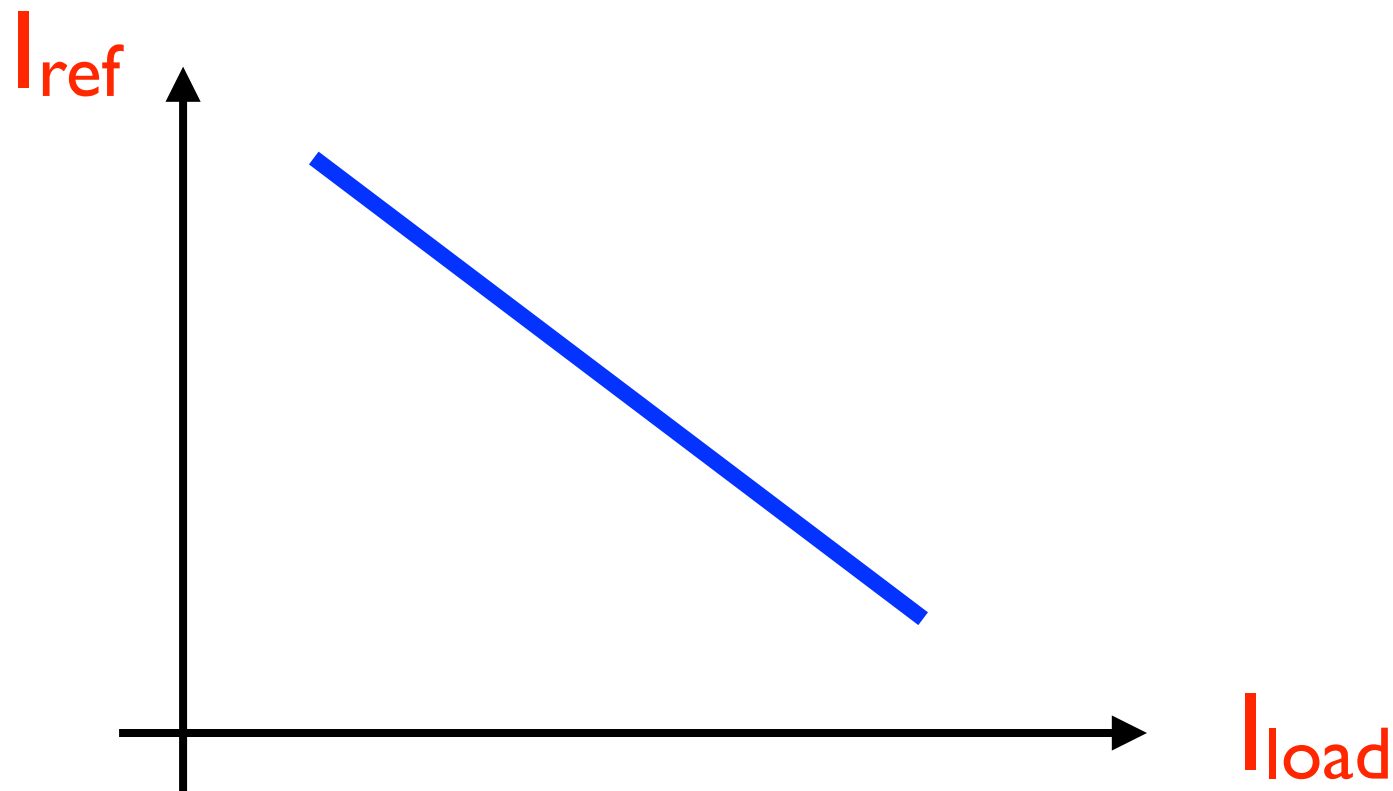
# SHUNT VOLTAGE REFERENCE



$$V_r = V_s - R_I \cdot (I_{ref} + I_{load})$$

$(I_{ref} + I_{load})$  must be constant

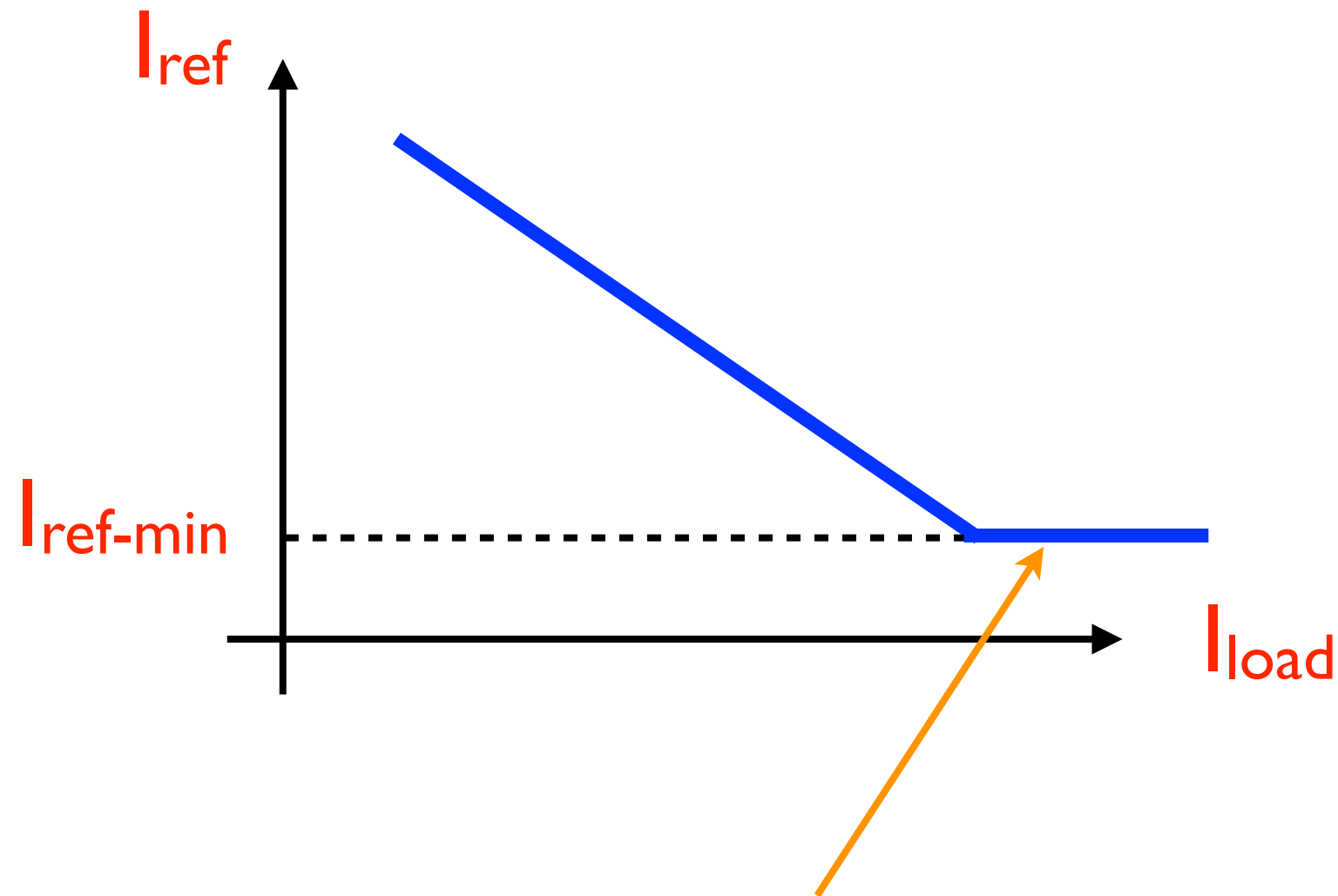
if  $I_{load}$  increases  $I_{ref}$  decreases





Problem 1:  $I$  cannot decrease indefinitely.

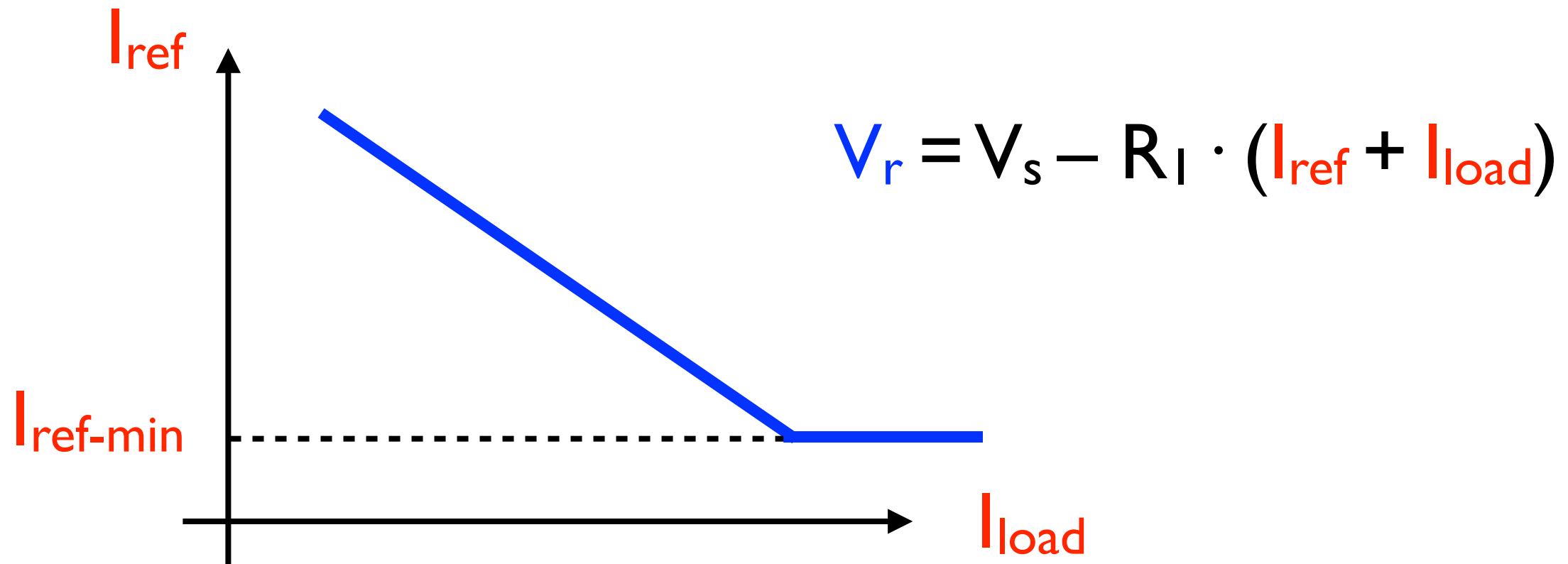
There is a minimum value  $I_{\text{ref-min}}$



here  $(I_{\text{ref}} + I_{\text{load}})$  will be larger than required,  
therefore the voltage drop on  $R_1$  will be  
higher and  $V_r$  will fall down

Problem 1:  $I$  cannot decrease indefinitely.

There is a minimum value  $I_{\text{ref-min}}$



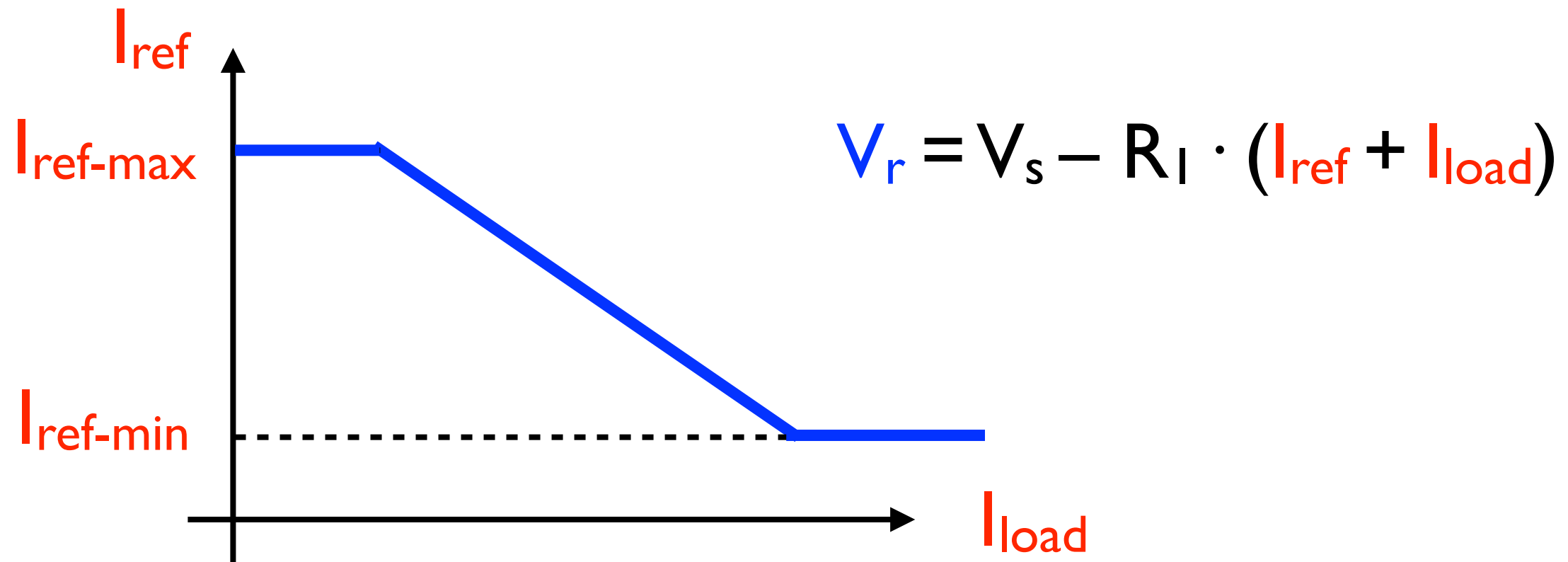
$$R_I = \frac{V_s - V_r}{I_{\text{ref-min}} + I_{\text{load-max}}} \quad \text{limit condition}$$

It's better a larger resistance so that  $I_{\text{ref}} > I_{\text{ref-min}}$

$$R_I > \frac{V_s - V_r}{I_{\text{ref-min}} + I_{\text{load-max}}}$$

Problem 2: cannot increase indefinitely.

There is a maximum value  $I_{\text{ref-max}}$



$$R_l = \frac{V_s - V_r}{I_{\text{ref-max}} + I_{\text{load-min}}}$$

limit condition

It's better a lower resistance so that  $I_{\text{ref}} < I_{\text{ref-max}}$

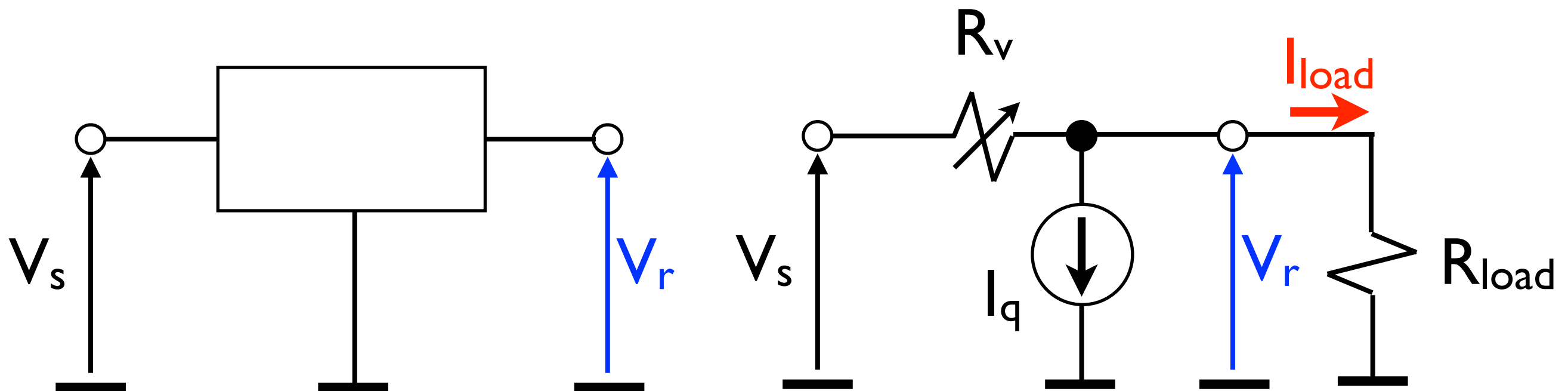
$$R_l < \frac{V_s - V_r}{I_{\text{ref-max}} + I_{\text{load-min}}}$$

Joining both conditions we can find  
the range of resistance

$$\frac{V_s - V_r}{I_{\text{ref-min}} + I_{\text{load-max}}} < R_l < \frac{V_s - V_r}{I_{\text{ref-max}} + I_{\text{load-min}}}$$

# SERIES VOLTAGE REFERENCE

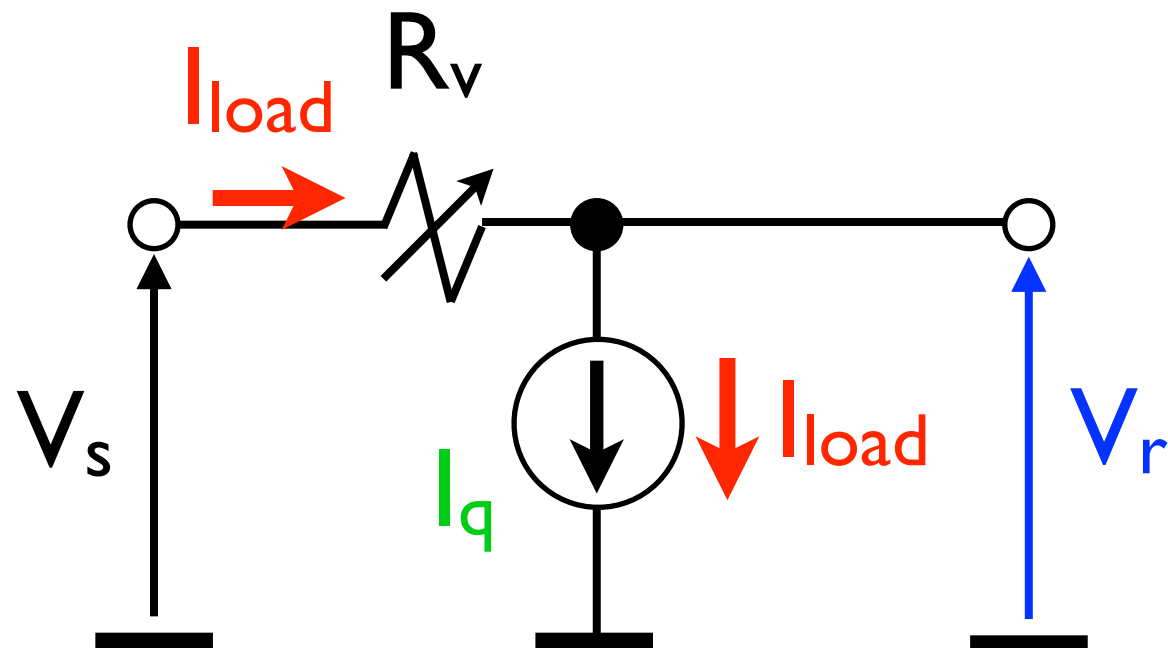
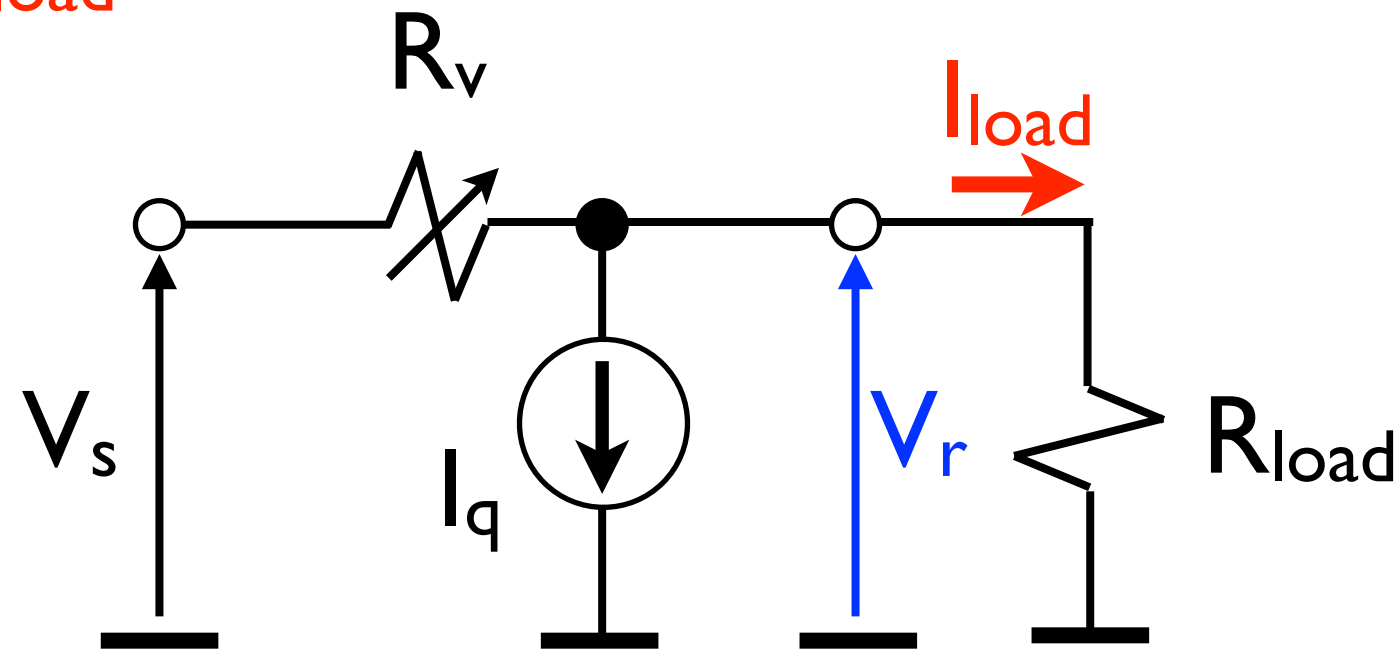
Working principle: it can be seen as a variable resistor in series to the load. The value of the resistor is regulated to have proper voltage drop according whatever is the load



$$V_r = V_s - R_v \cdot I_{load}$$

# SERIES VOLTAGE REFERENCE

$$V_r = V_s - R_v \cdot I_{load}$$



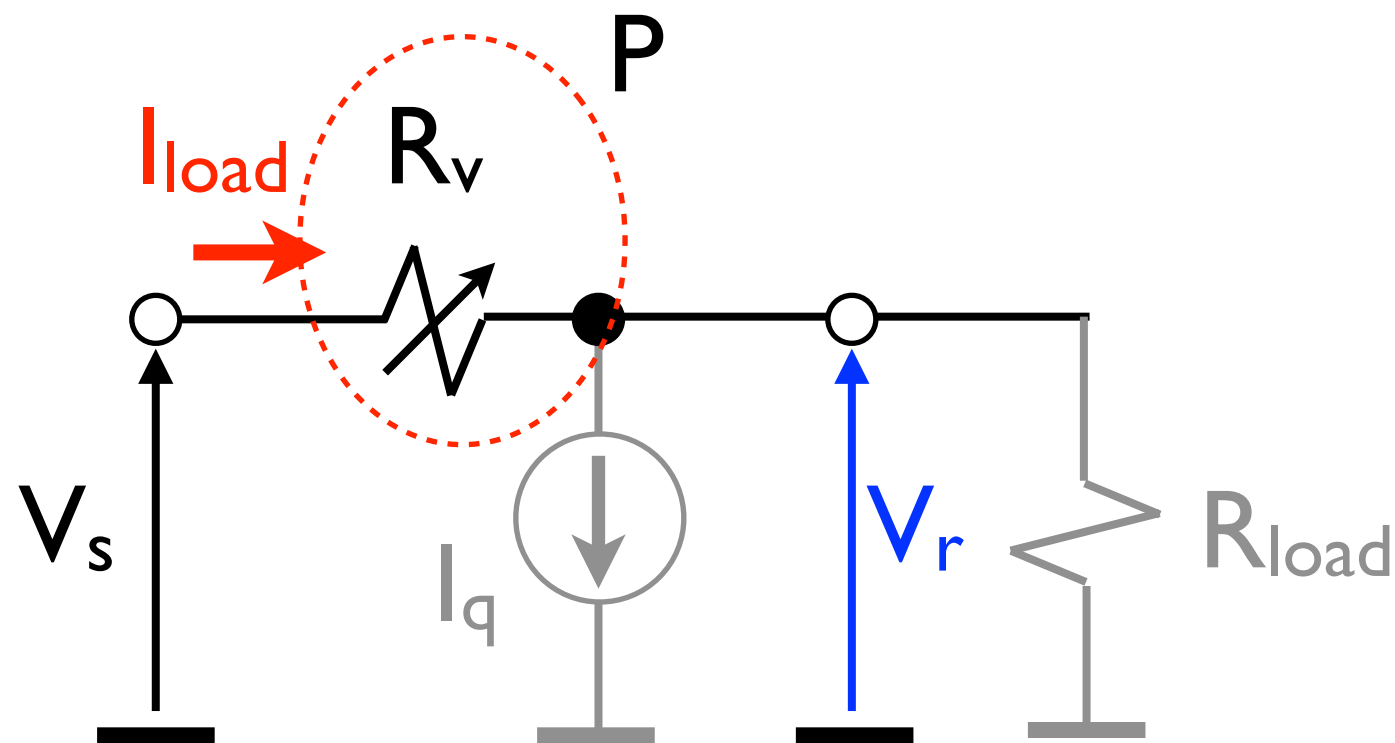
$I_q$  is a quiescent current, necessary to have a voltage drop on  $R_v$  even if no load is applied

# SERIES VOLTAGE REFERENCE

**IMPORTANT!**

A power is lost on the resistor  $R_v$ .

$$P = (V_r - V_s) \cdot I_{\text{load}}$$



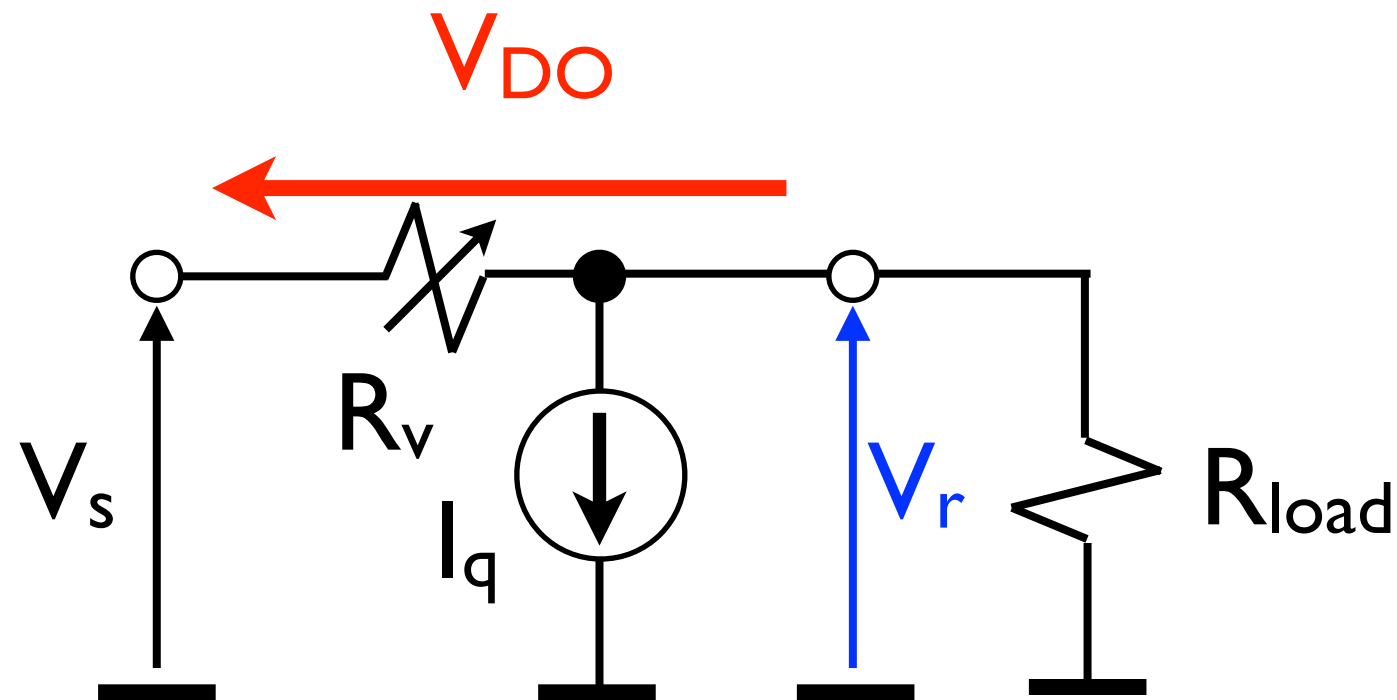
You must take into account the lost power  
to avoid overheating

# SERIES VOLTAGE REFERENCE

**ALSO VERY IMPORTANT!**

The difference between the supply voltage and the reference voltage must be higher than **dropout voltage**

$$(V_r - V_s) > V_{DO}$$





# IMPORTANT PARAMETERS

**Initial accuracy** from 1% to 0.02%

E.g.:

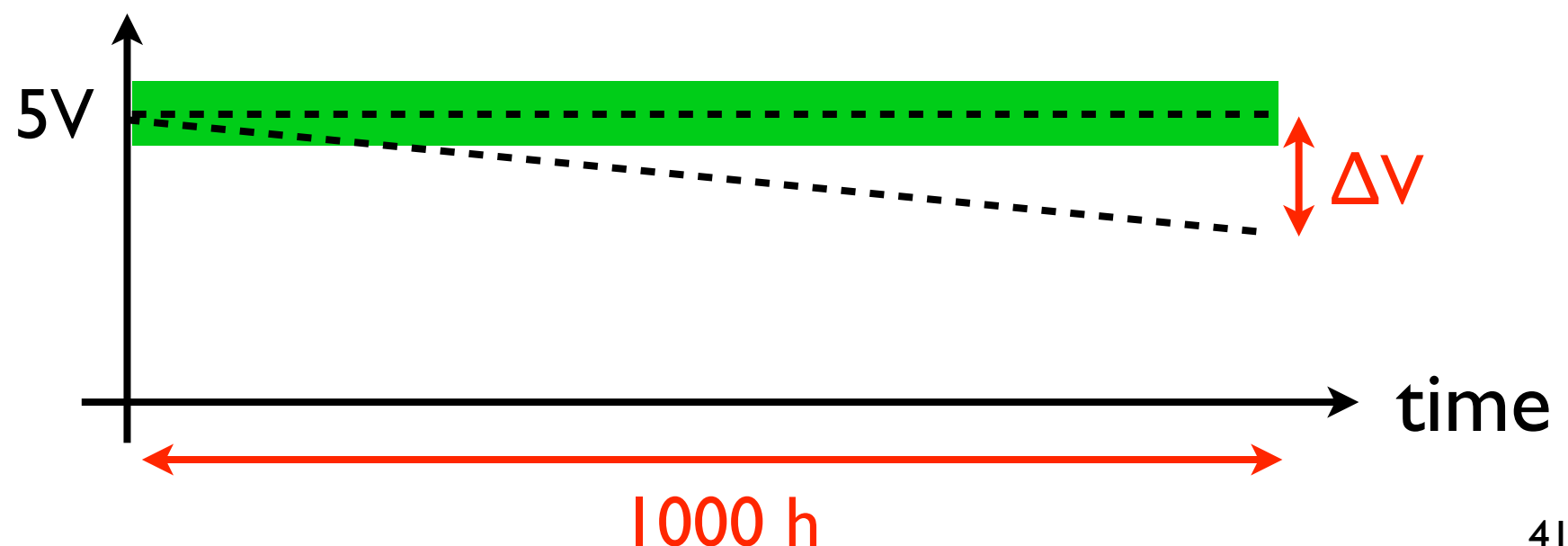
if  $V_r = 5\text{ V}$  and initial accuracy is 0.5%, the actual  $V_r$  is :

$$5 - 5 \cdot 0.005 < V_r < 5 + 5 \cdot 0.005 \quad [\text{V}]$$

$$5 - 0.025 < V_r < 5 + 0.025 \quad [\text{V}]$$

$$4.975 < V_r < 5.025 \quad [\text{V}]$$

**Long term stability**  
in ppm/1000 h

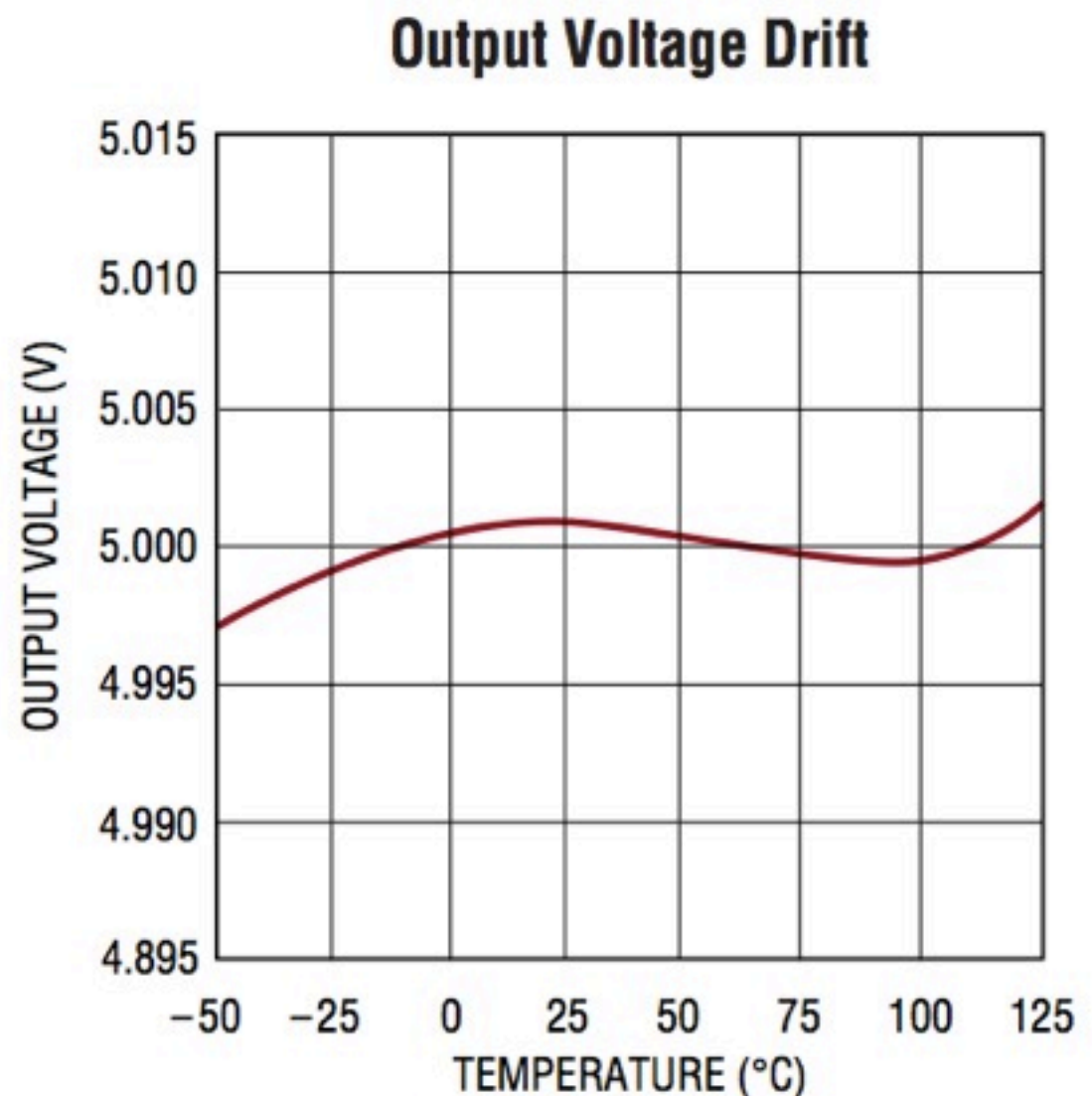


# IMPORTANT PARAMETERS

## Temperature coefficient (tempco)

Usually given in ppm/°C... but it is NOT linear!

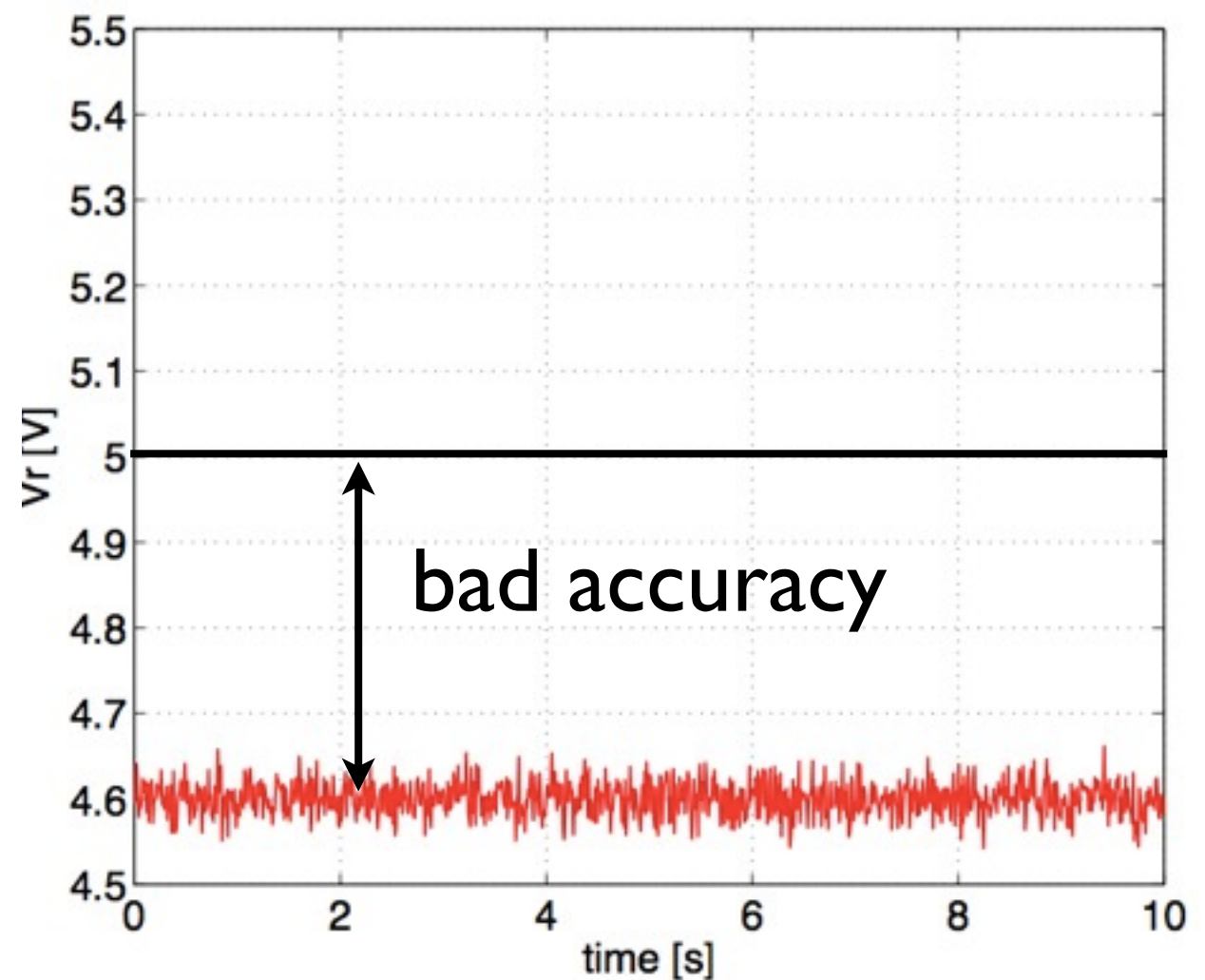
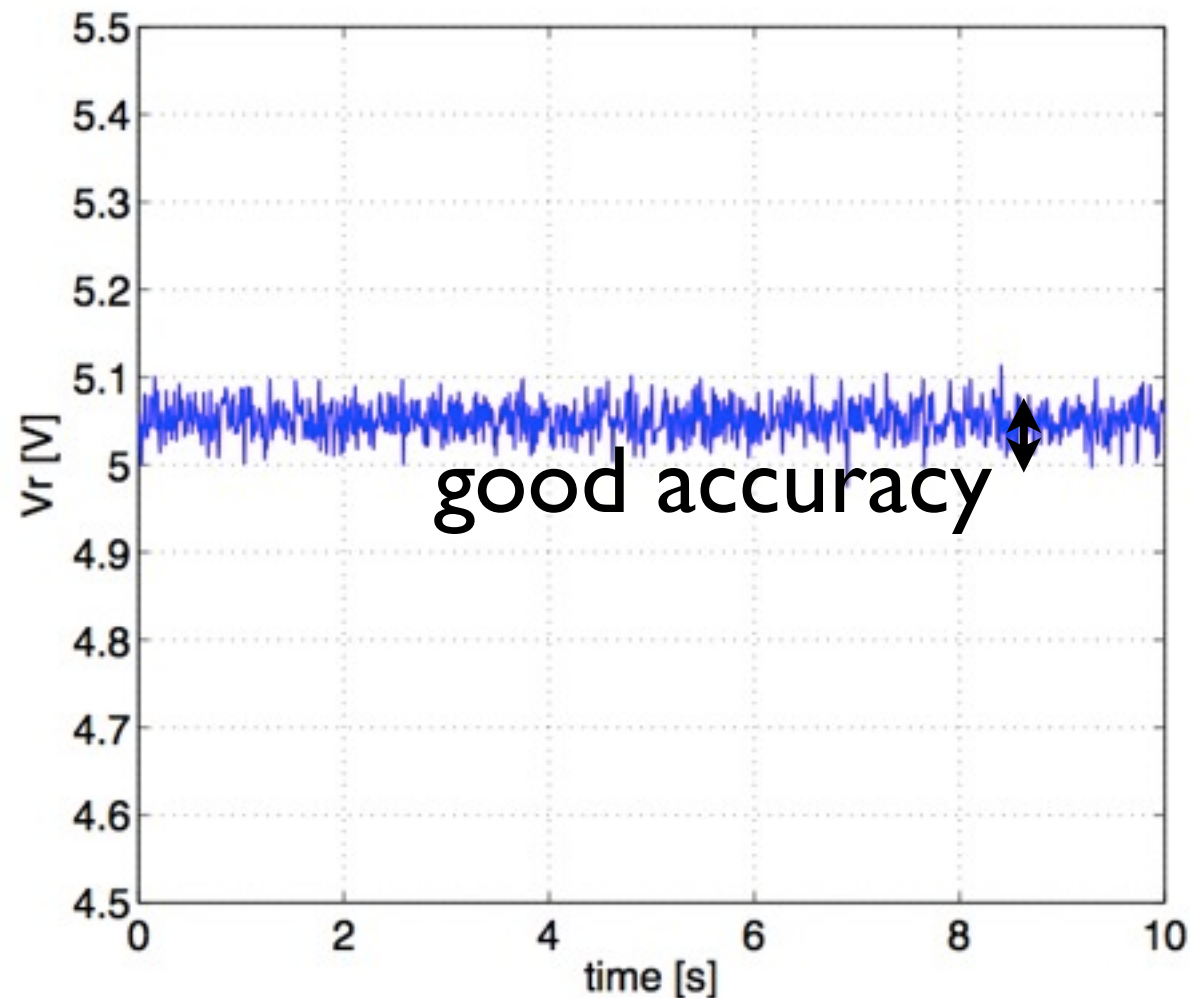
*E.g.: LT1029 - Linear Technologies*



# IMPORTANT PARAMETERS

## Noise

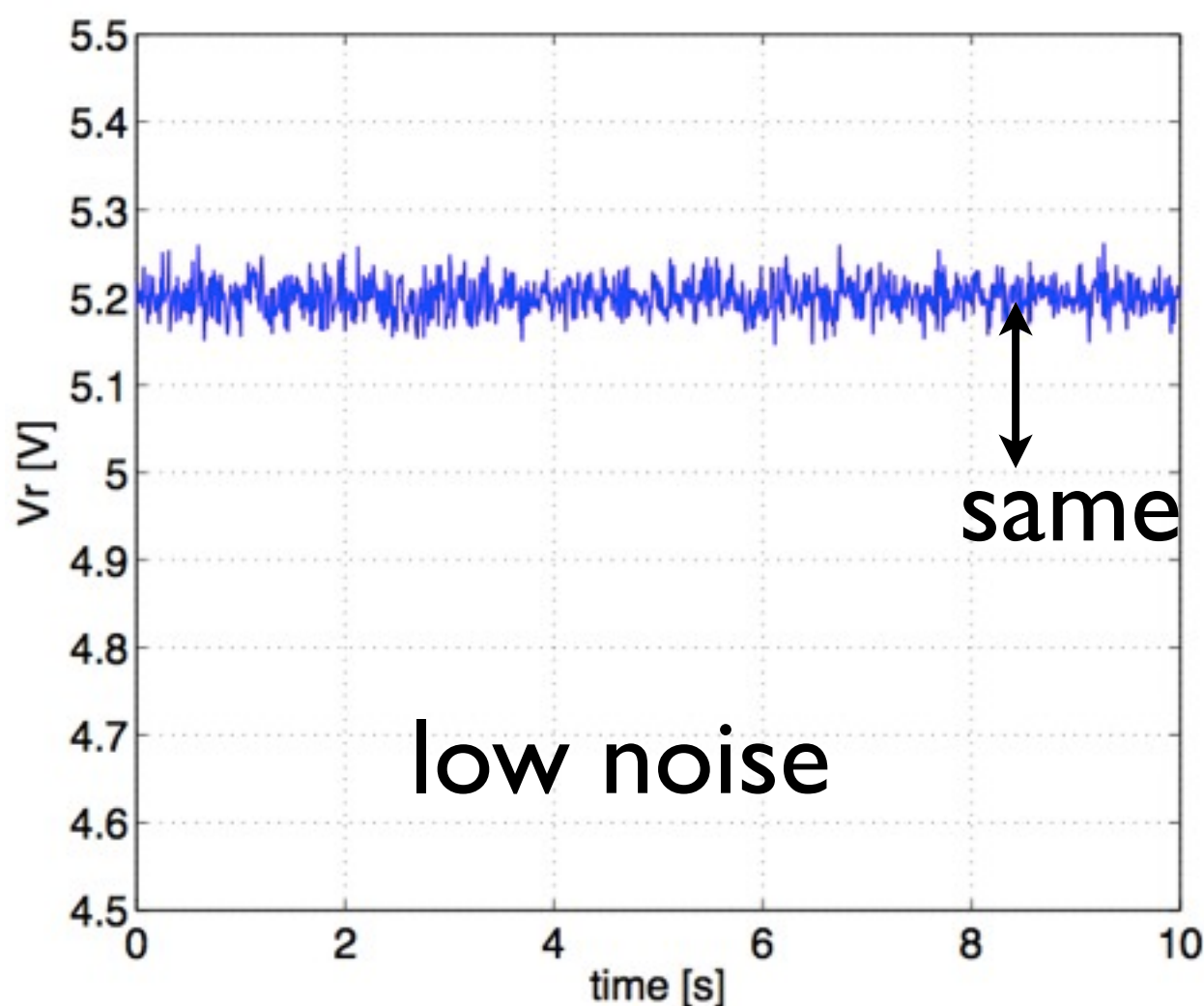
The accuracy only tells you how “precise” is the average value of  $V_r$ . It does not tell you how much “swings” around it



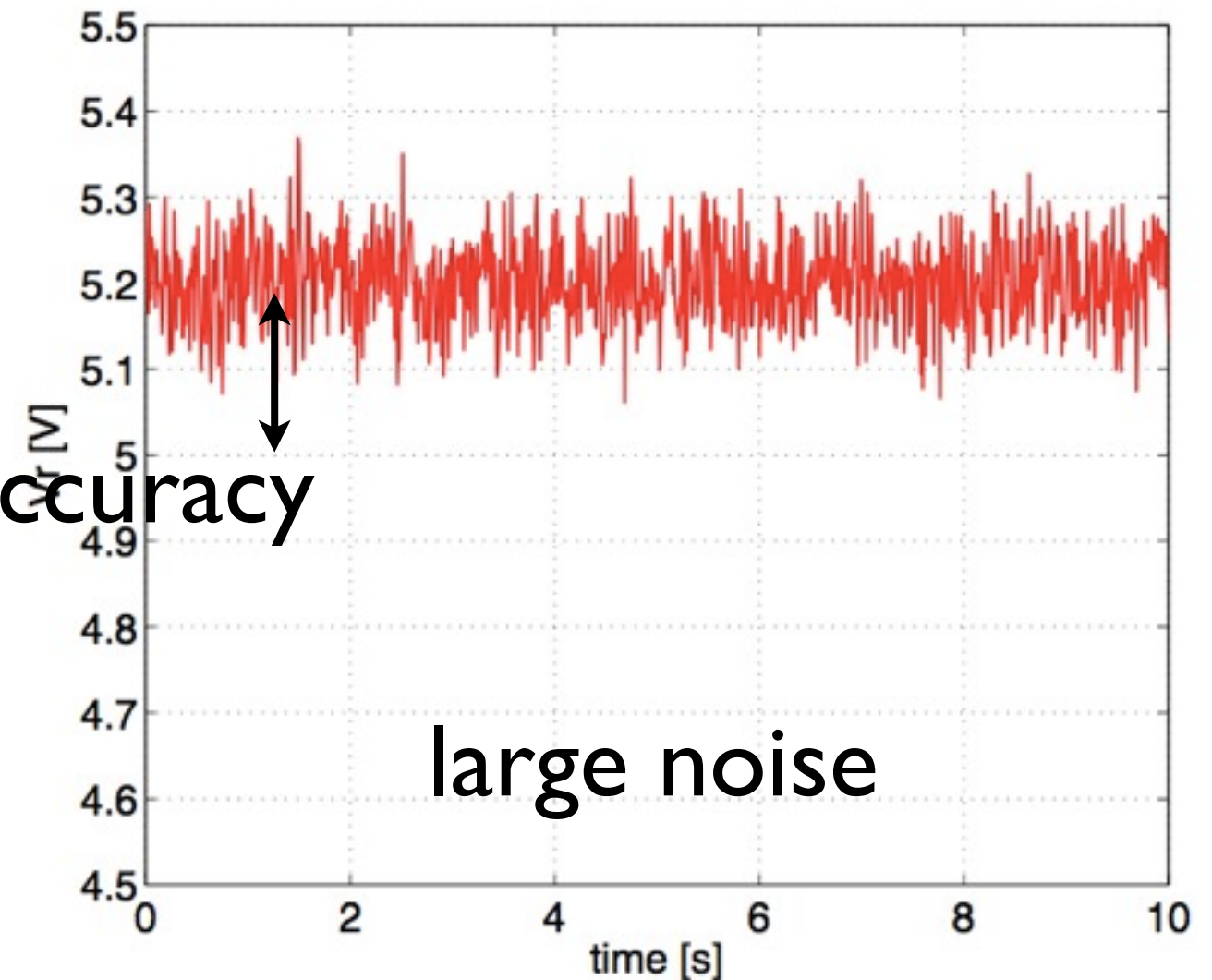
# IMPORTANT PARAMETERS

## Noise

The accuracy only tells you how “precise” is the average value of  $V_r$ . It does not tell you how much “swings” around it

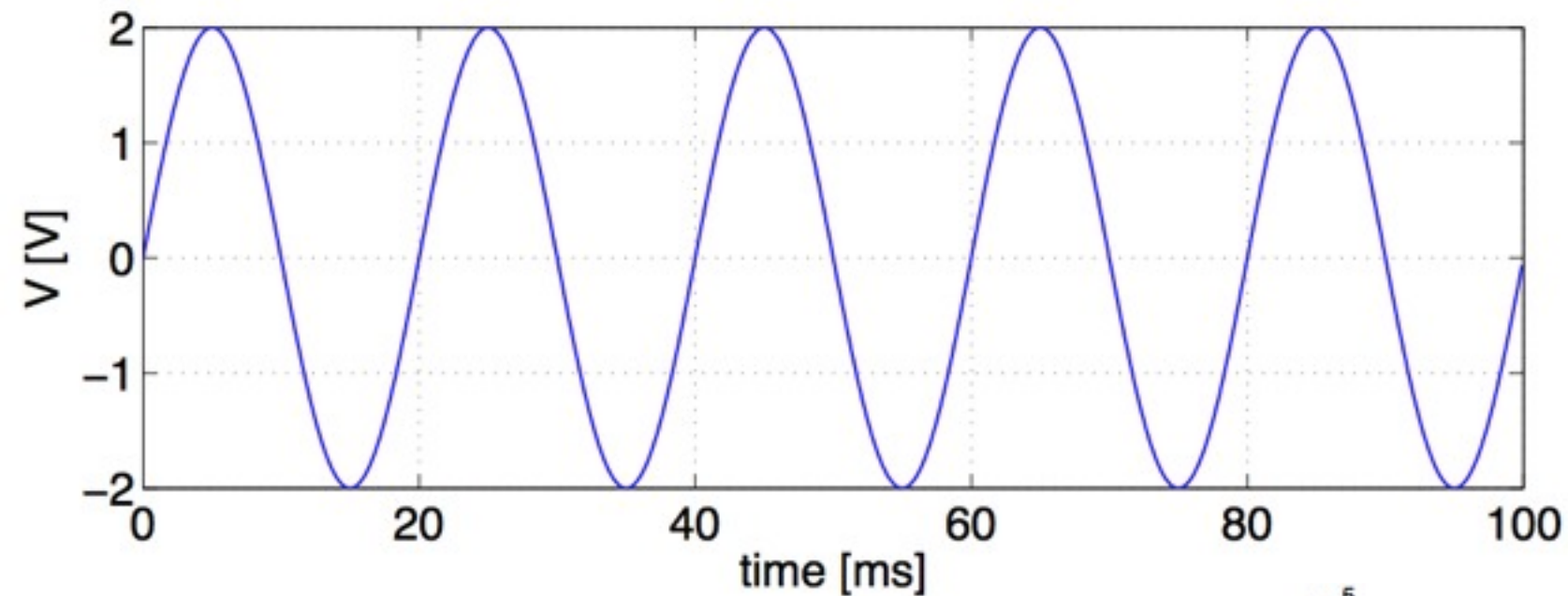


same accuracy



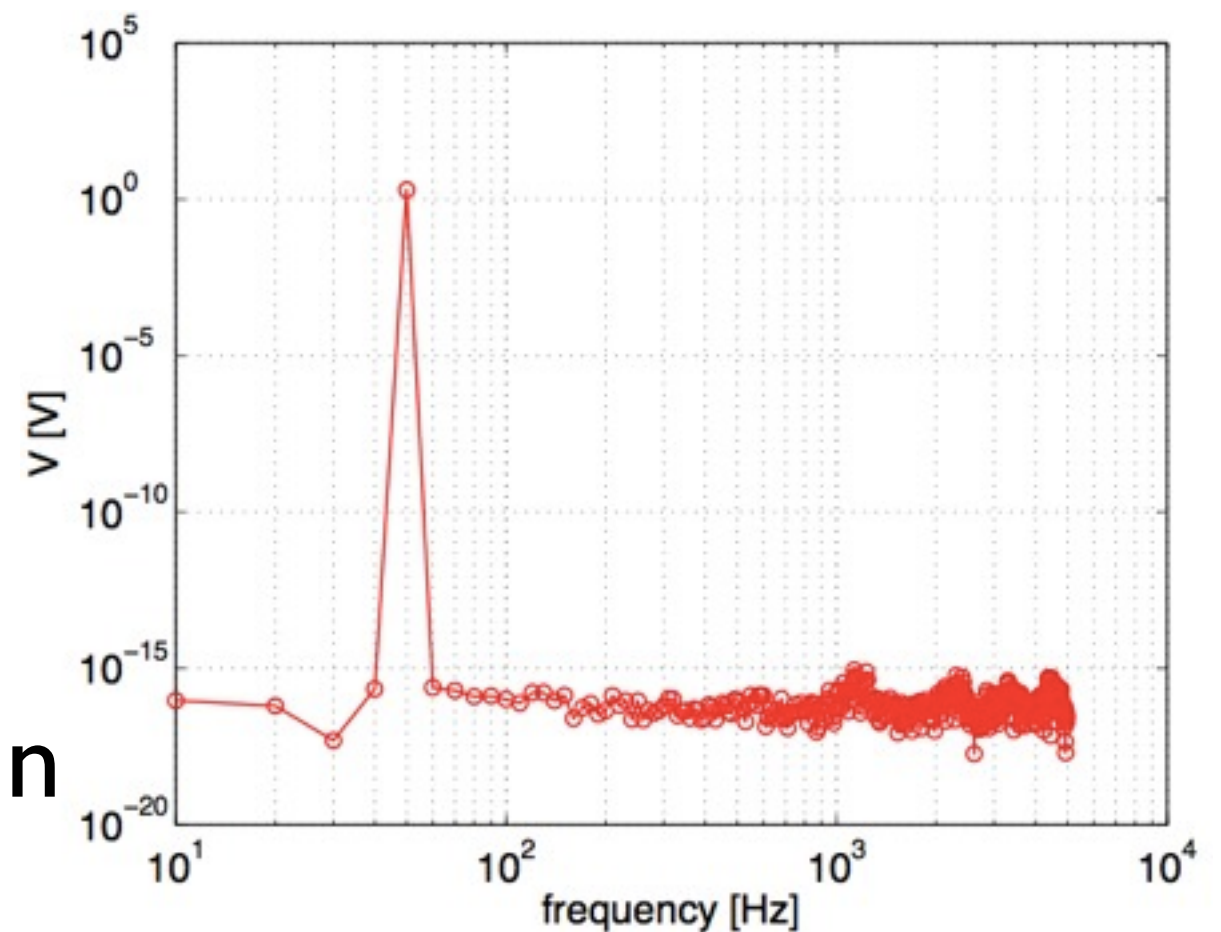
# SPECTRUM ANALYZER

The same signal can be viewed in



time domain

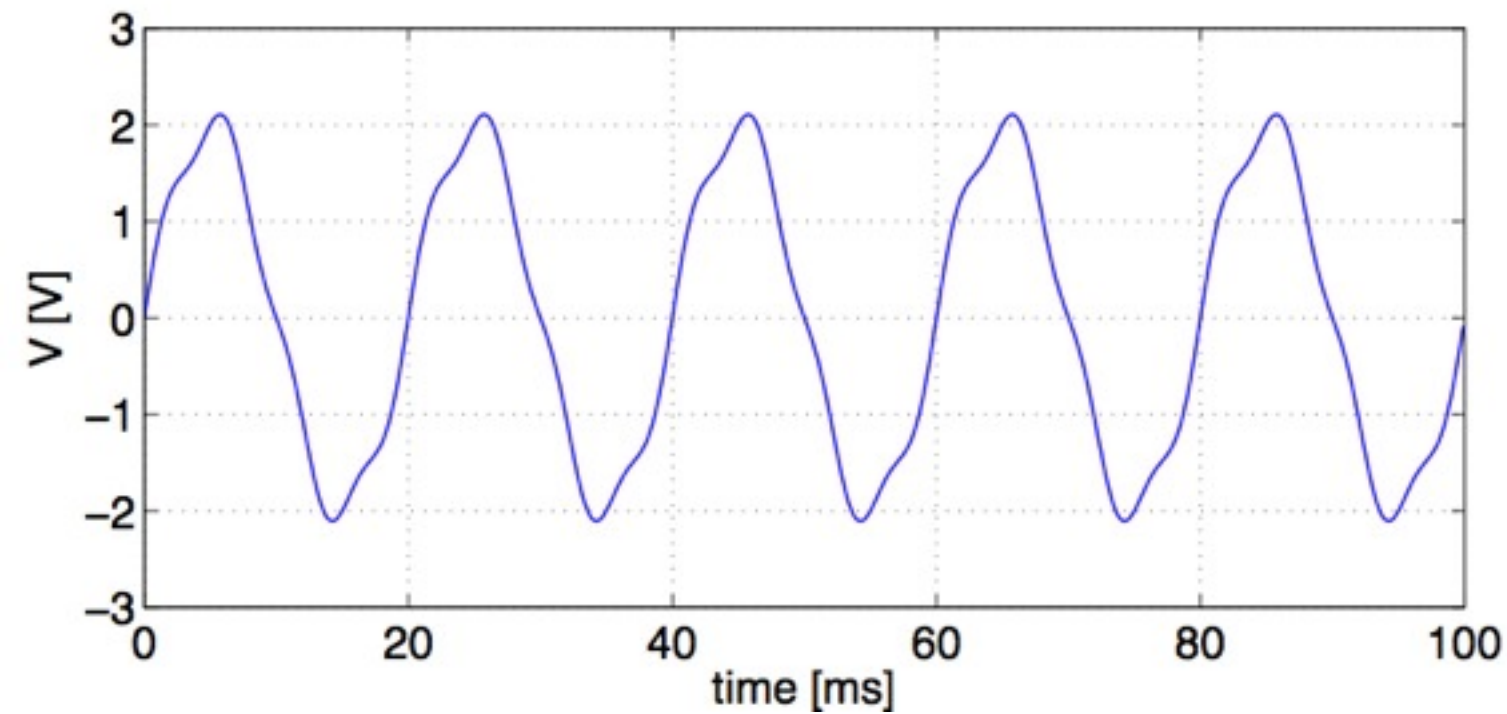
frequency domain





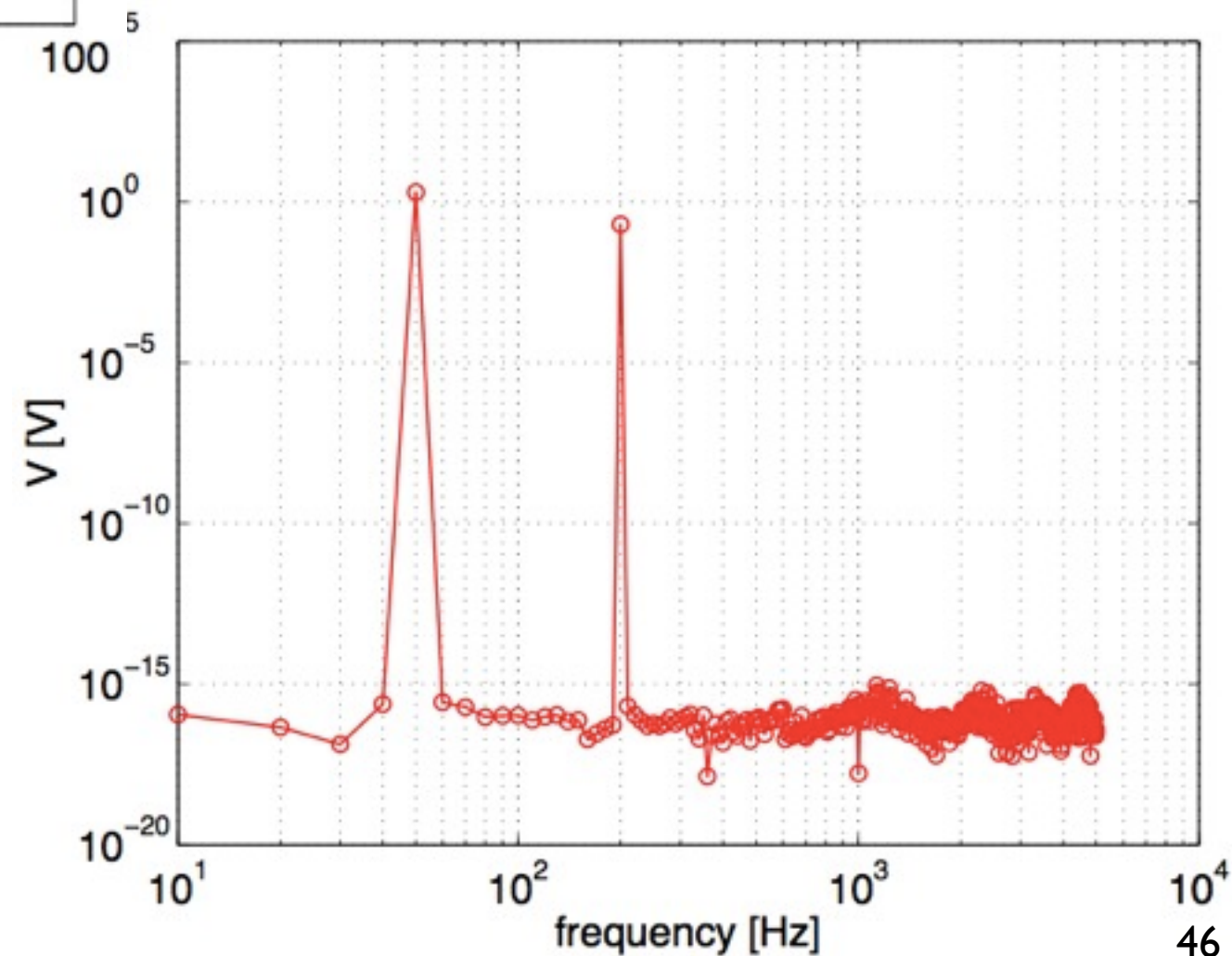
# SPECTRUM ANALYZER

The same signal can be viewed in



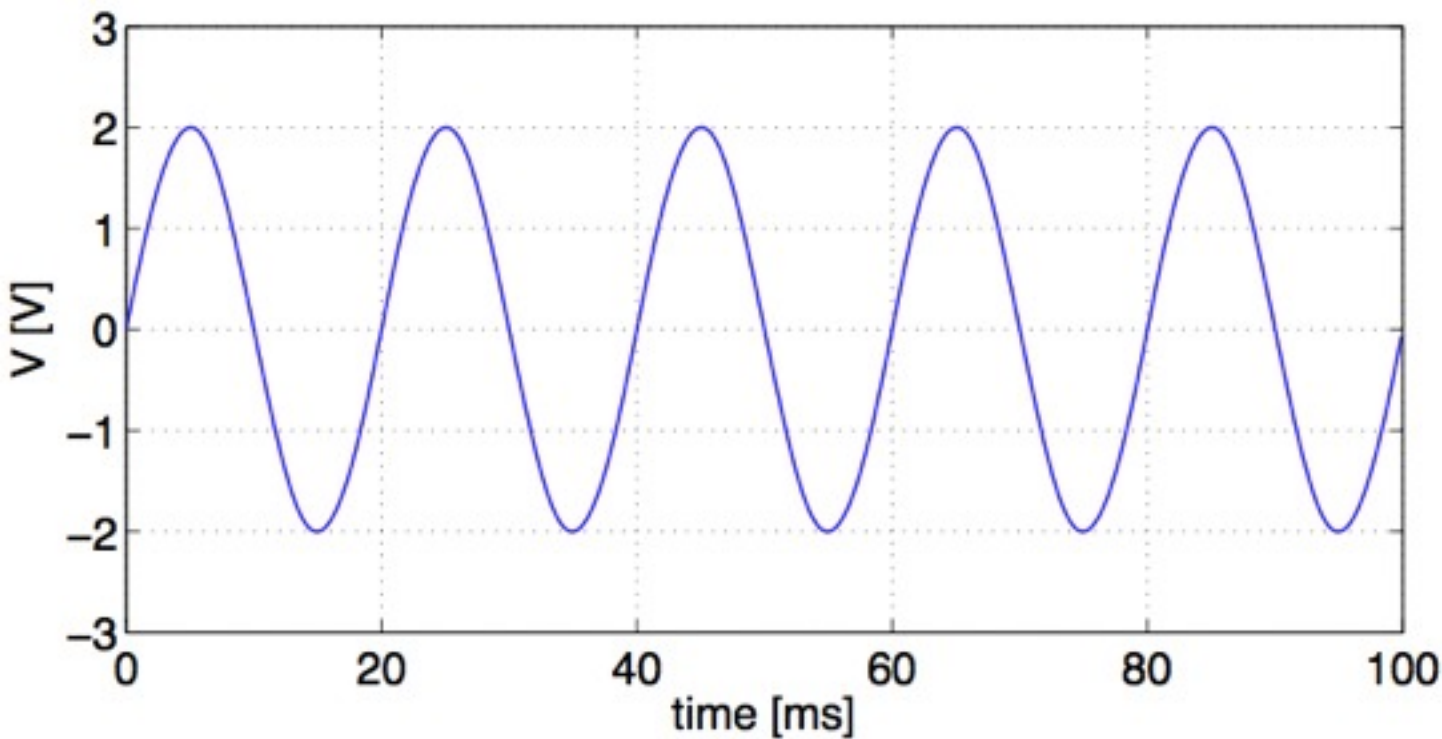
time domain

frequency domain



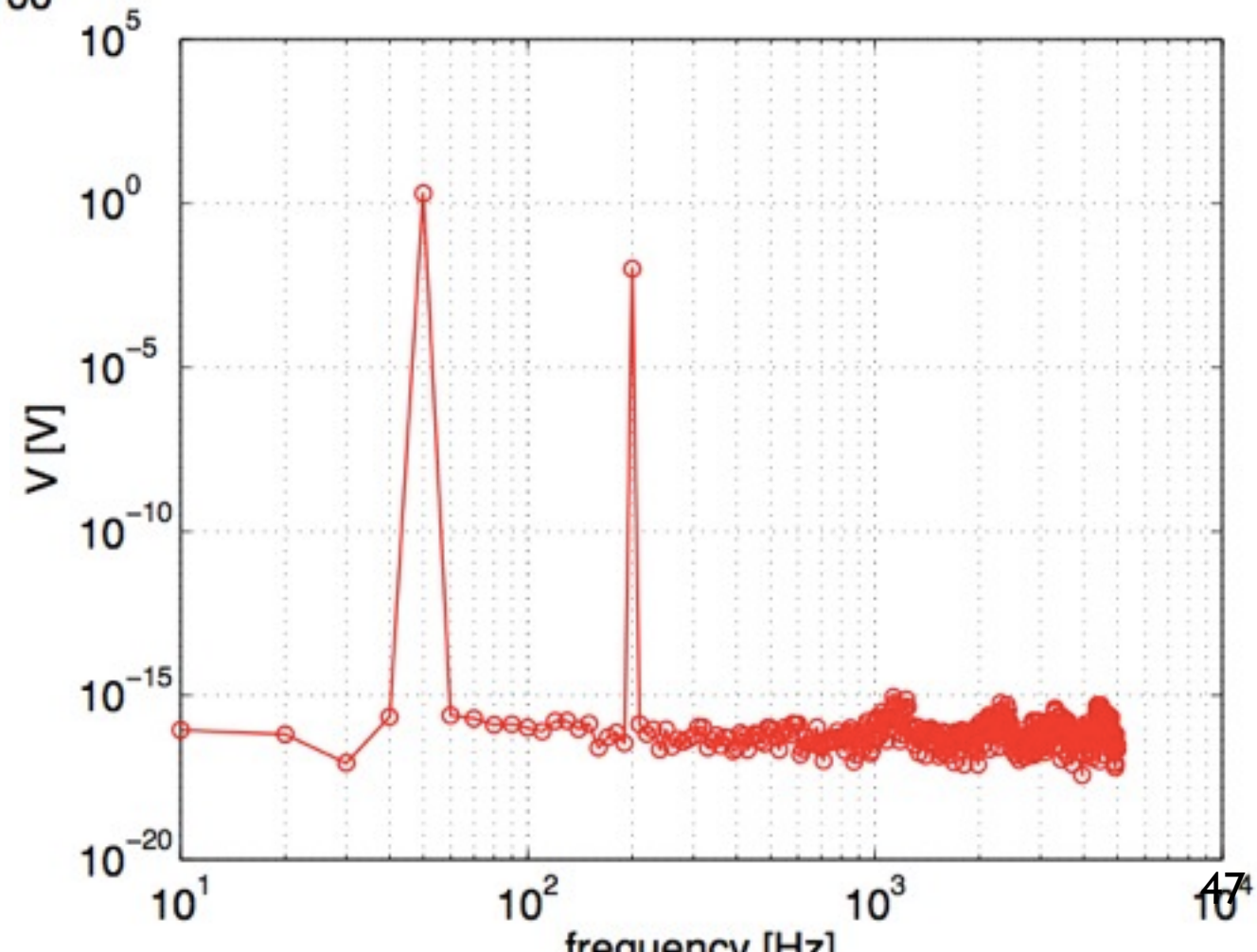
# SPECTRUM ANALYZER

It can be useful to observe harmonics we can't see in time domain

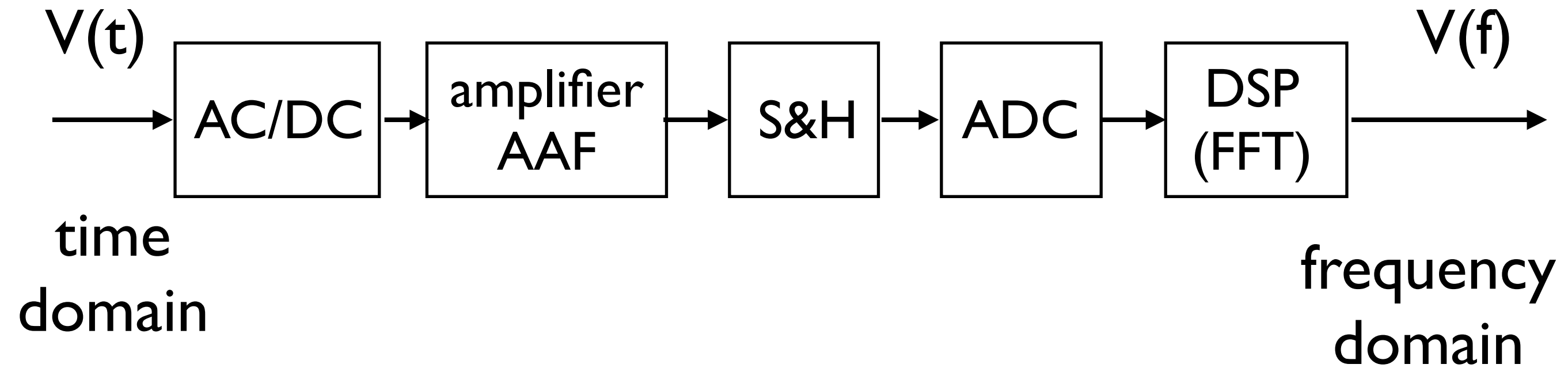


time domain

frequency domain



# FFT SPECTRUM ANALYZER

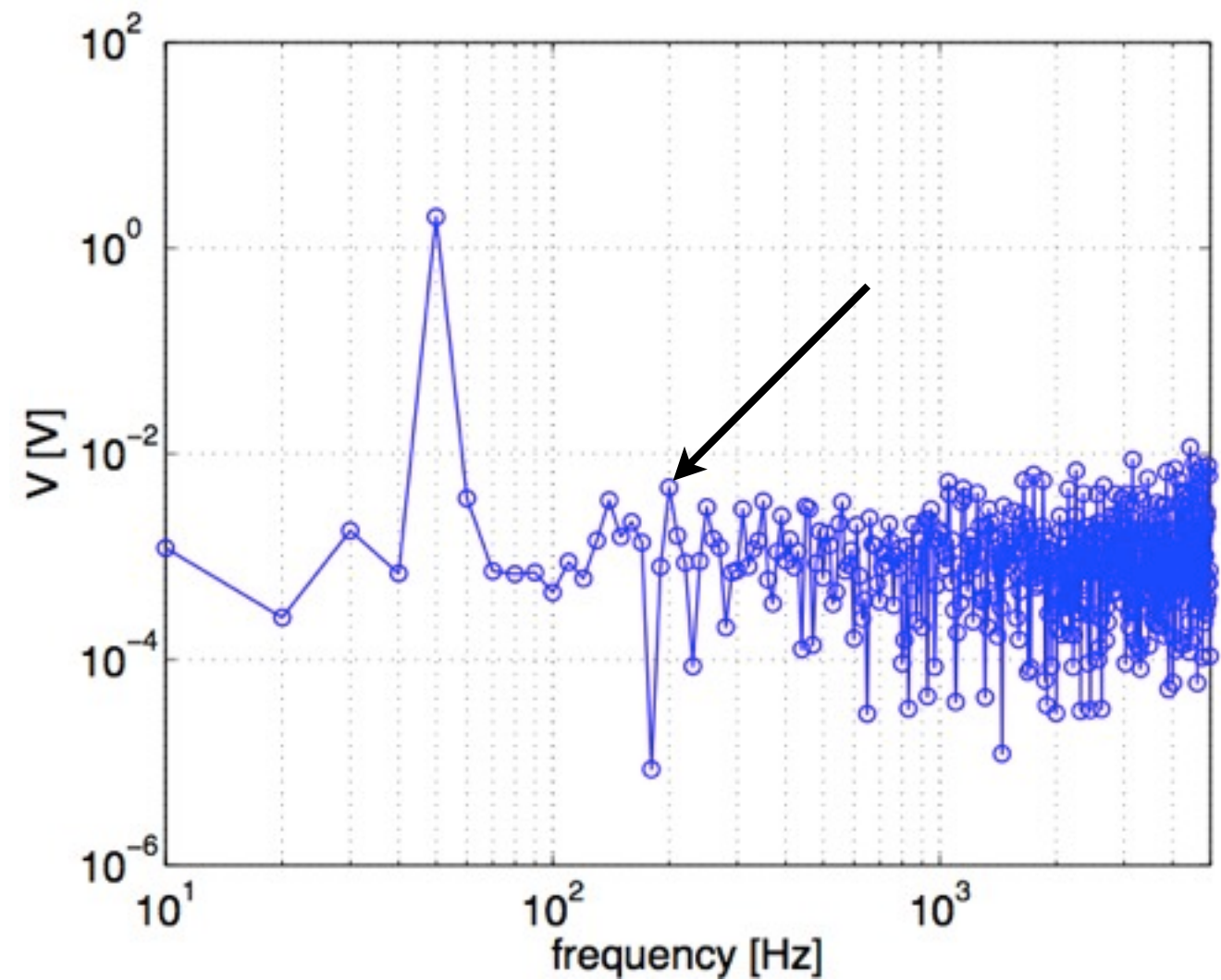
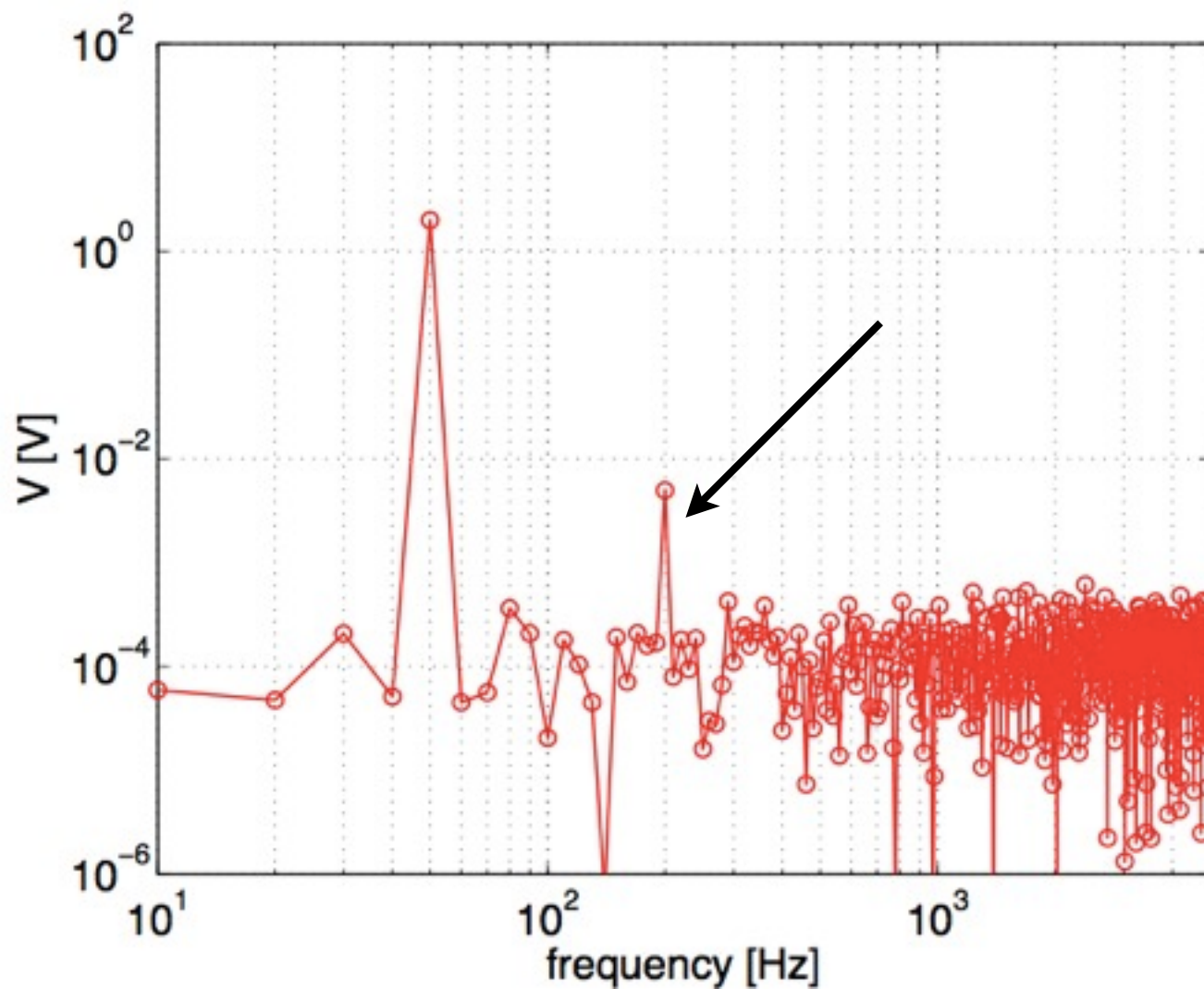


AAF=anti-aliasing filter



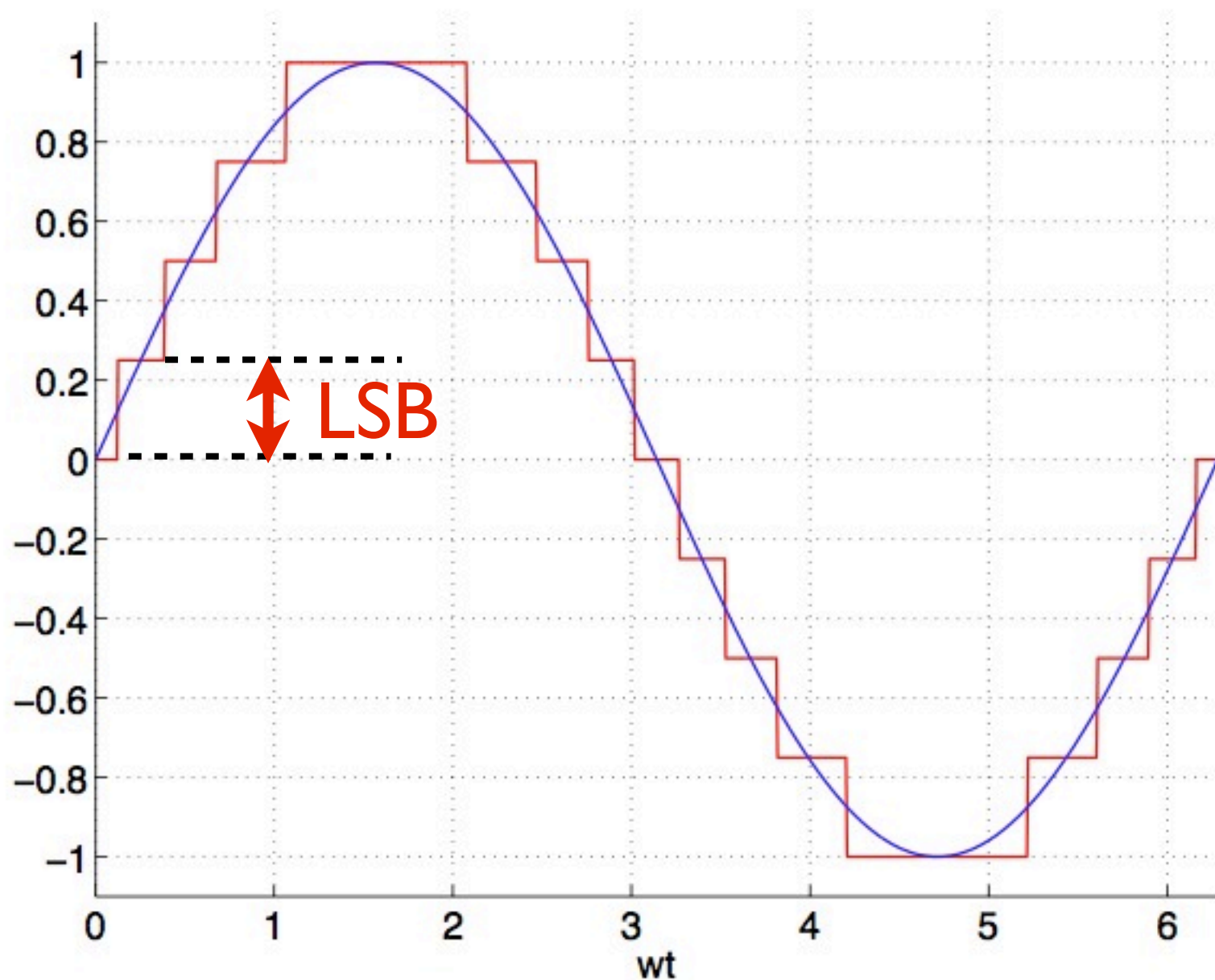
# The noise floor is important!

If the noise floor is too high we can't see tiny harmonics



# Back to lesson 1...

## How does LSB affect the digital signal?



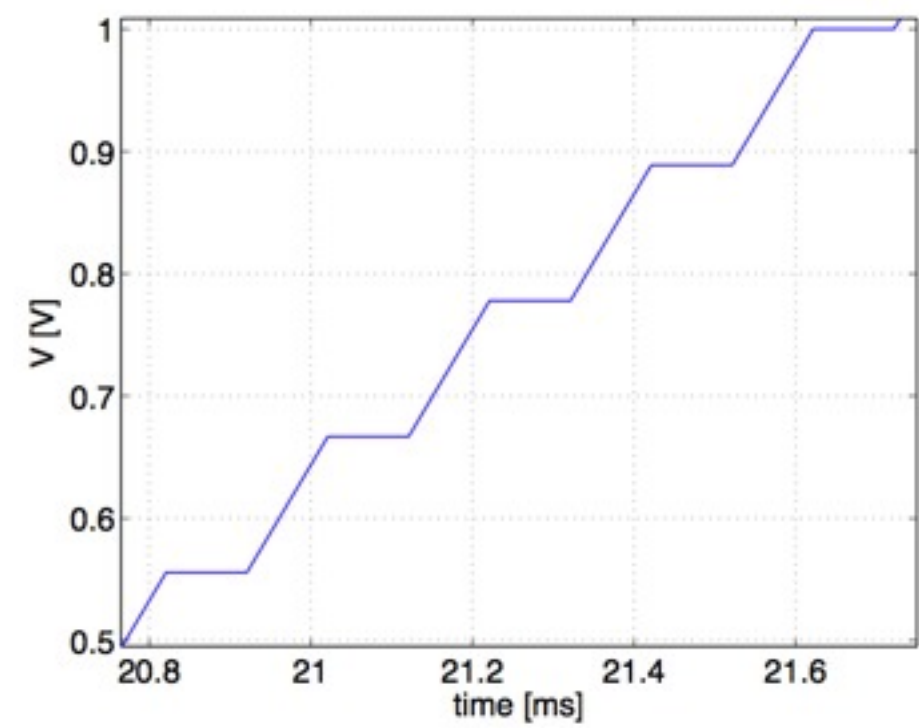
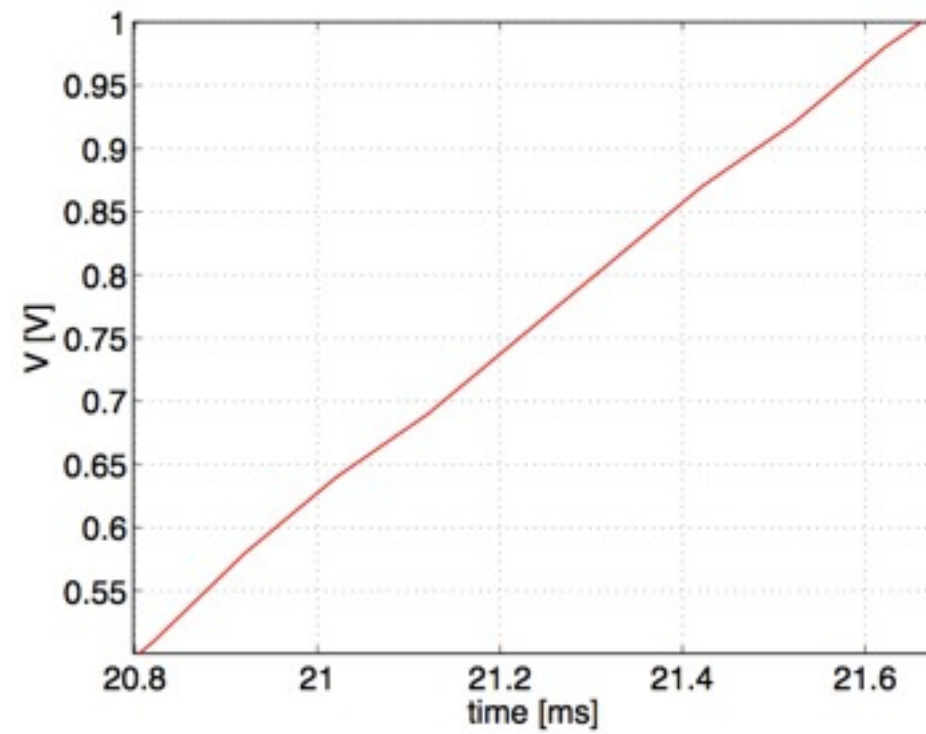
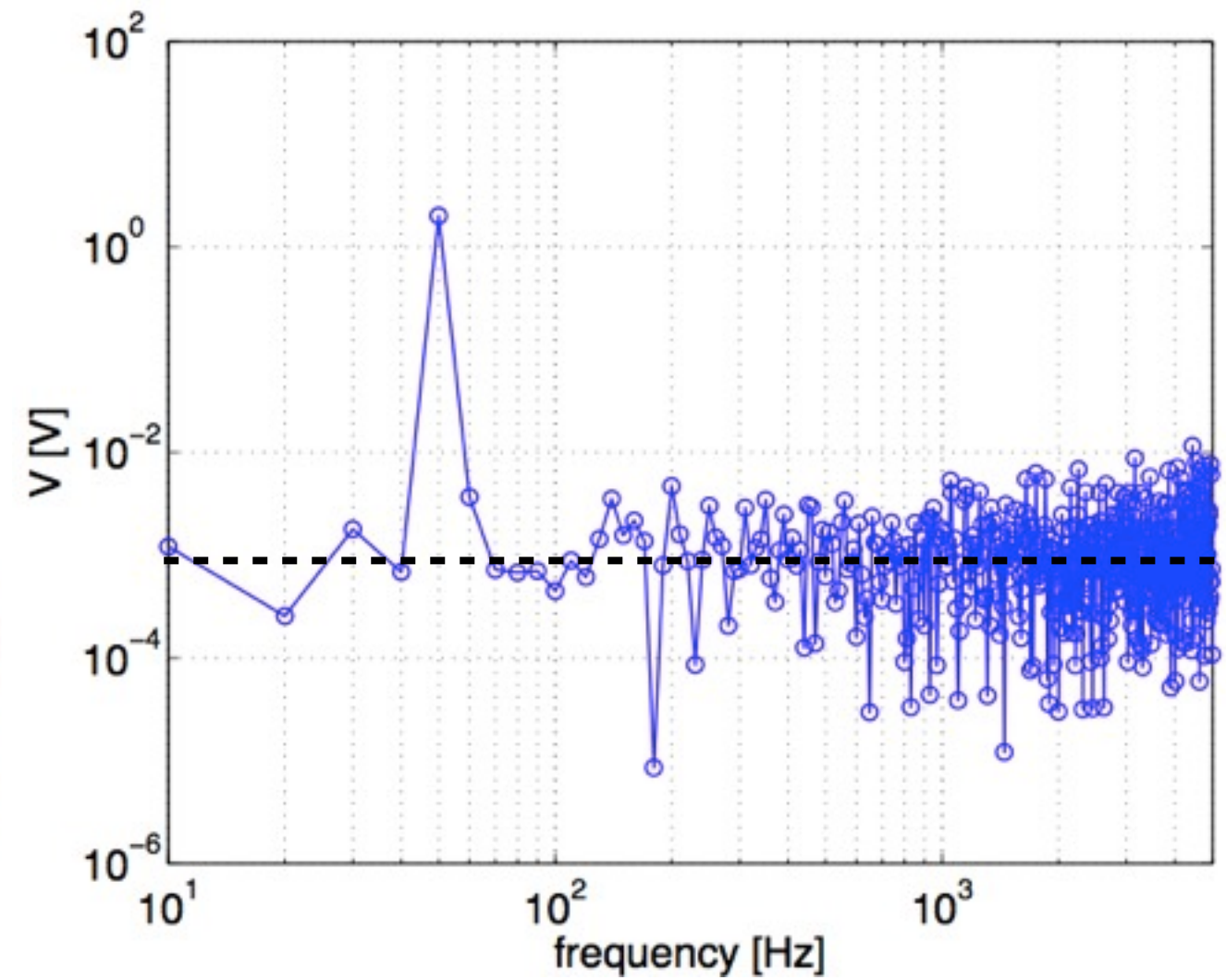
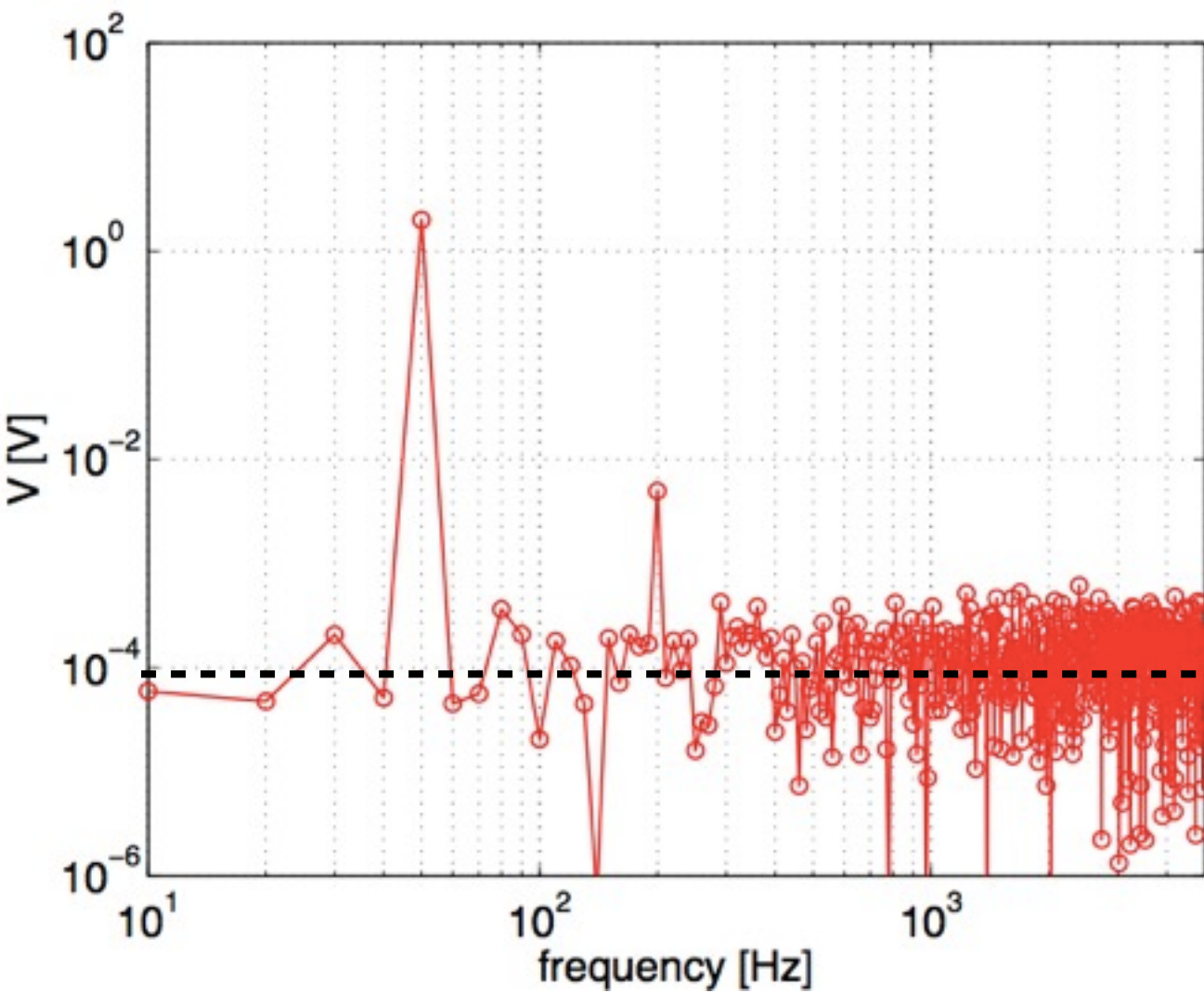
3 bits ADC

$$2^3 = 8$$

Maximum voltage range 2V

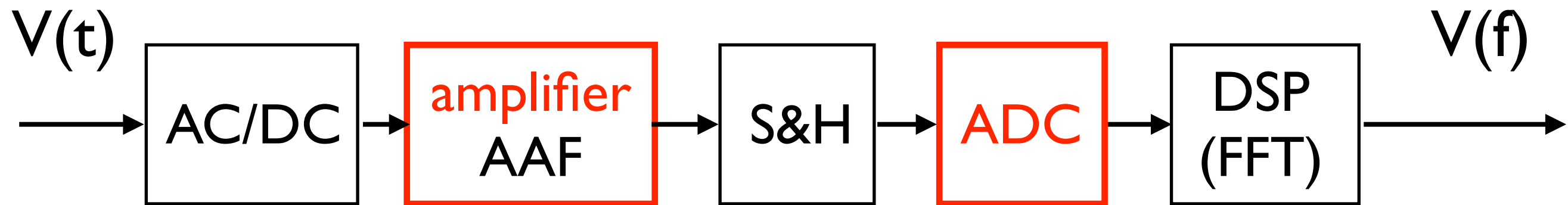
$$\text{LSB} = 2\text{V}/8 = 0.25\text{ V}$$

# Poor resolution (large LSB) makes the noise floor larger



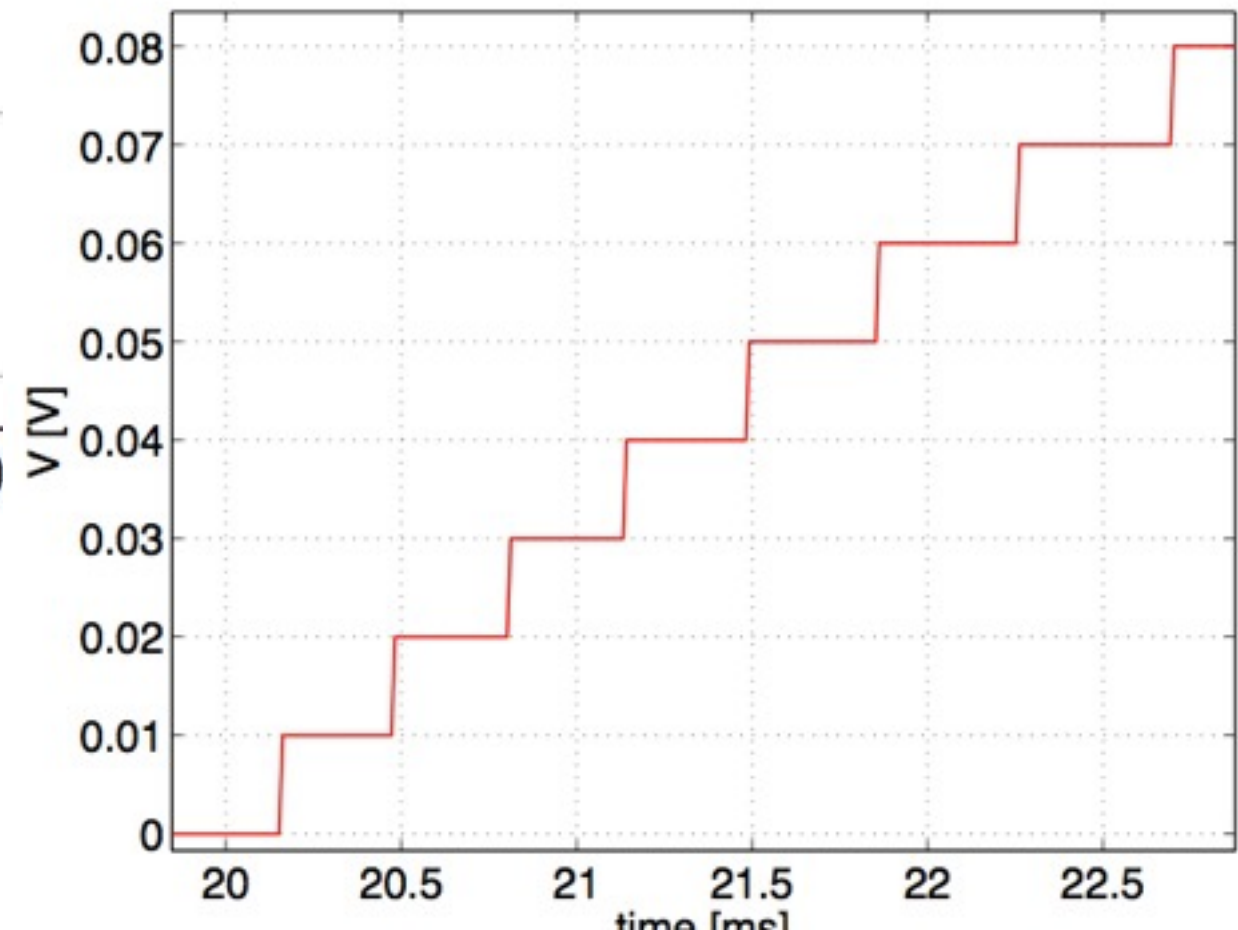
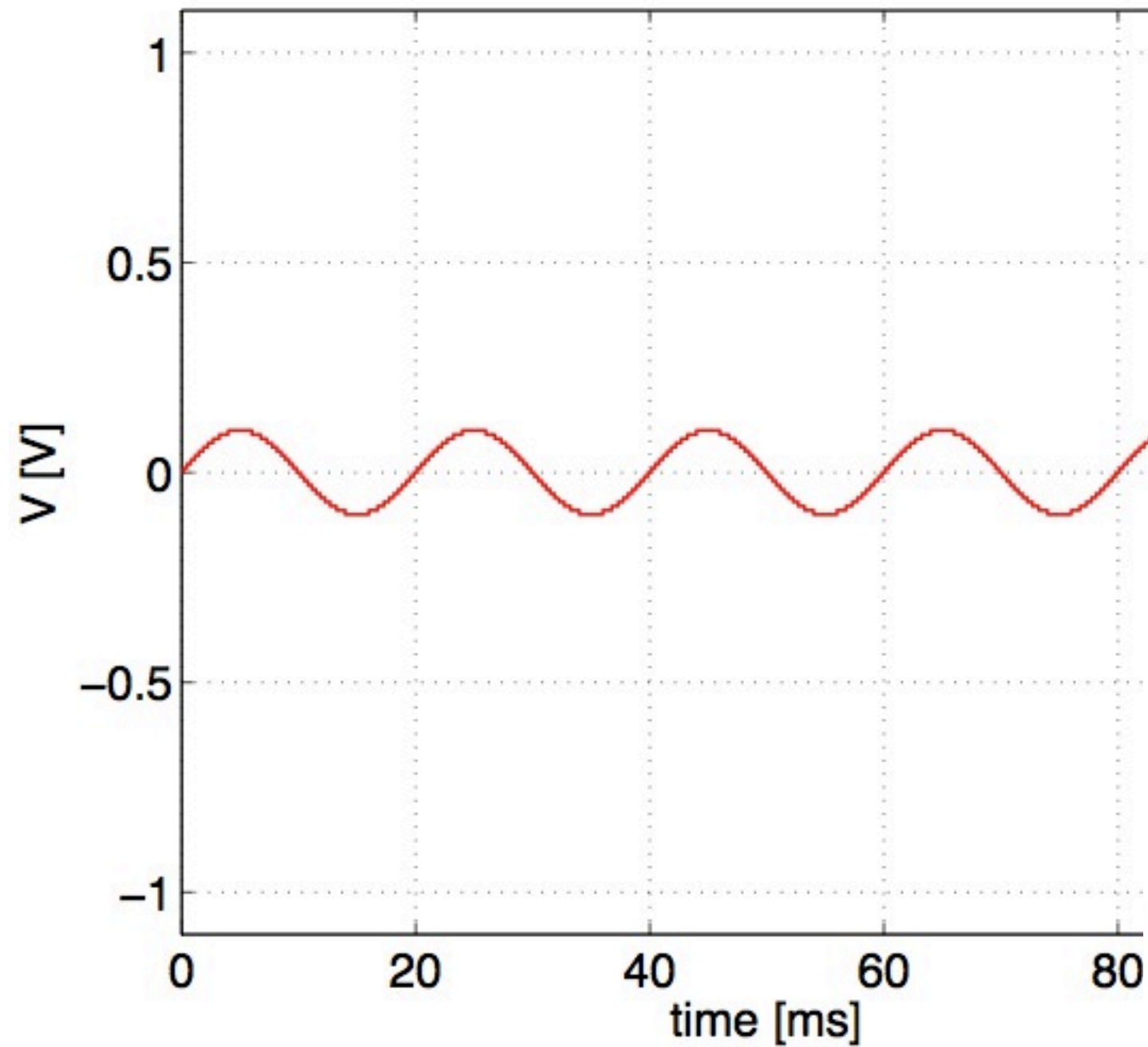


We need LSB as low as possible

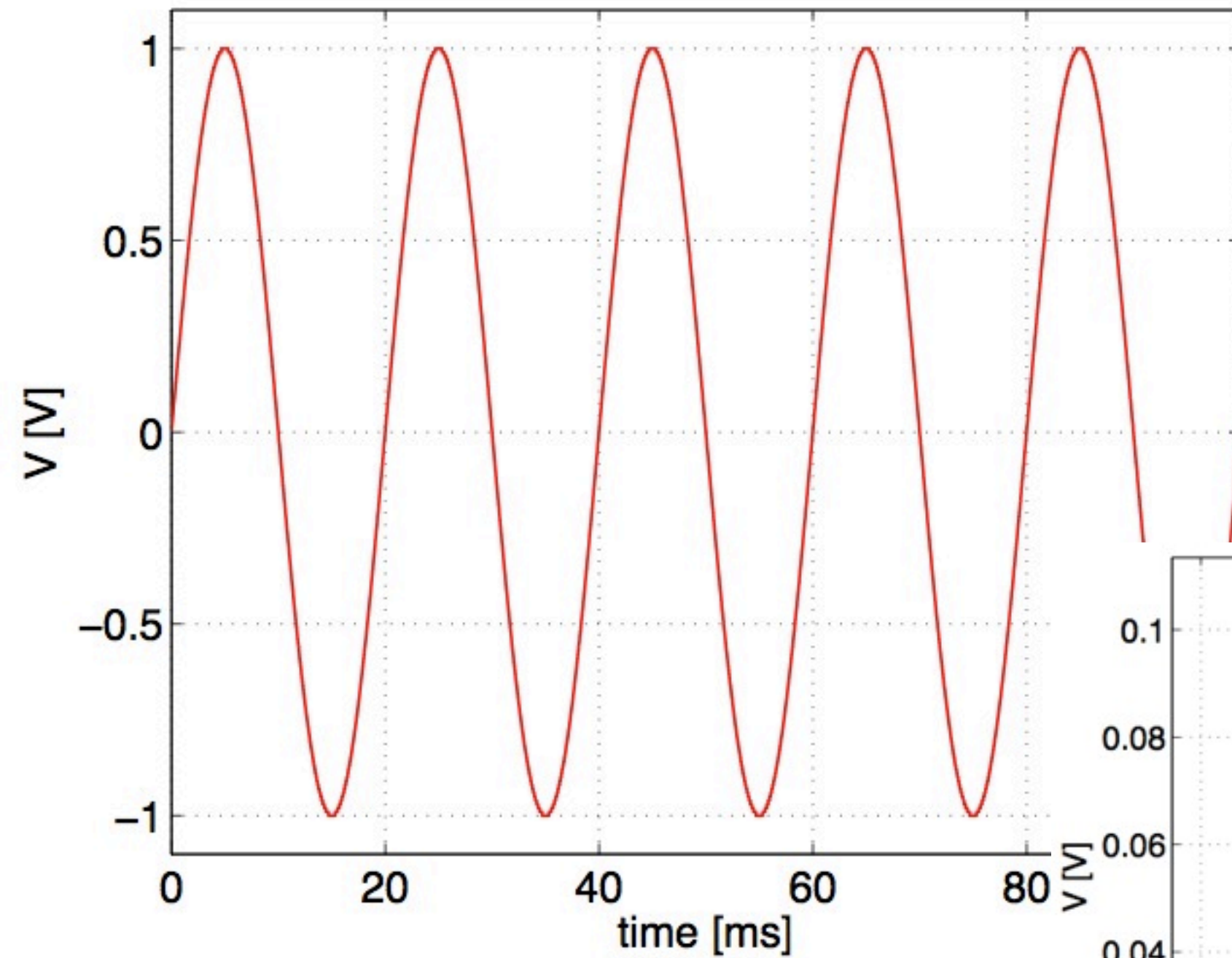


In fact the ADC does not change. We amplify the voltage before ADC so that the LSB will be *proportionally* lower

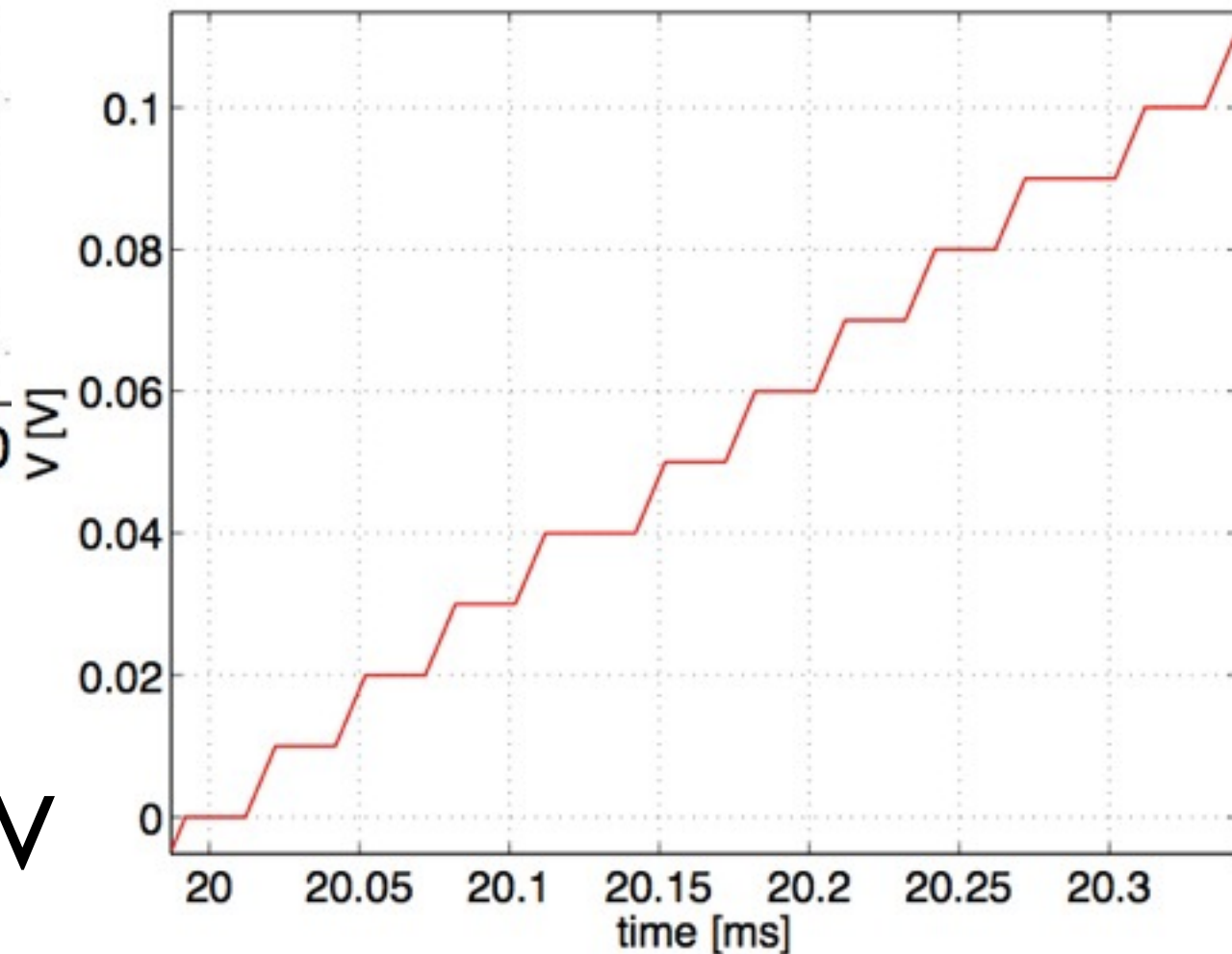
Example: the signal span is from  $-0.1\text{ V}$  to  $0.1\text{ V}$   
 $\text{LSB} = 0.01\text{ V}$



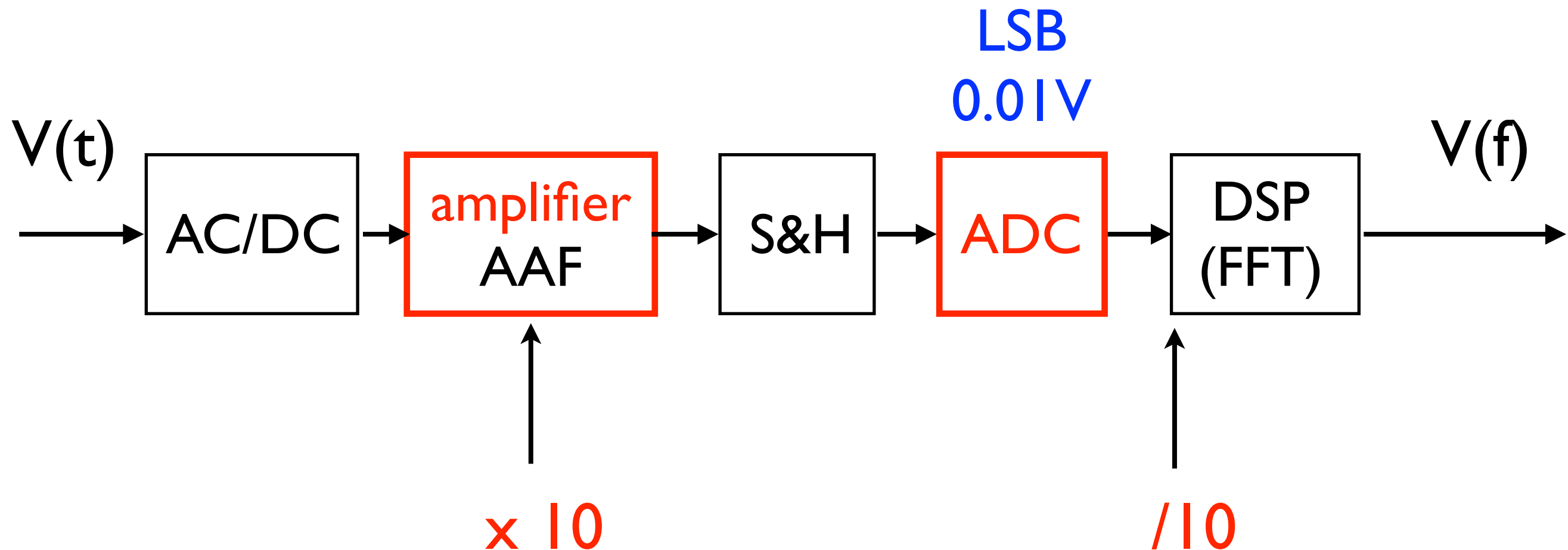
I amplify the signal 10 times before the quantization



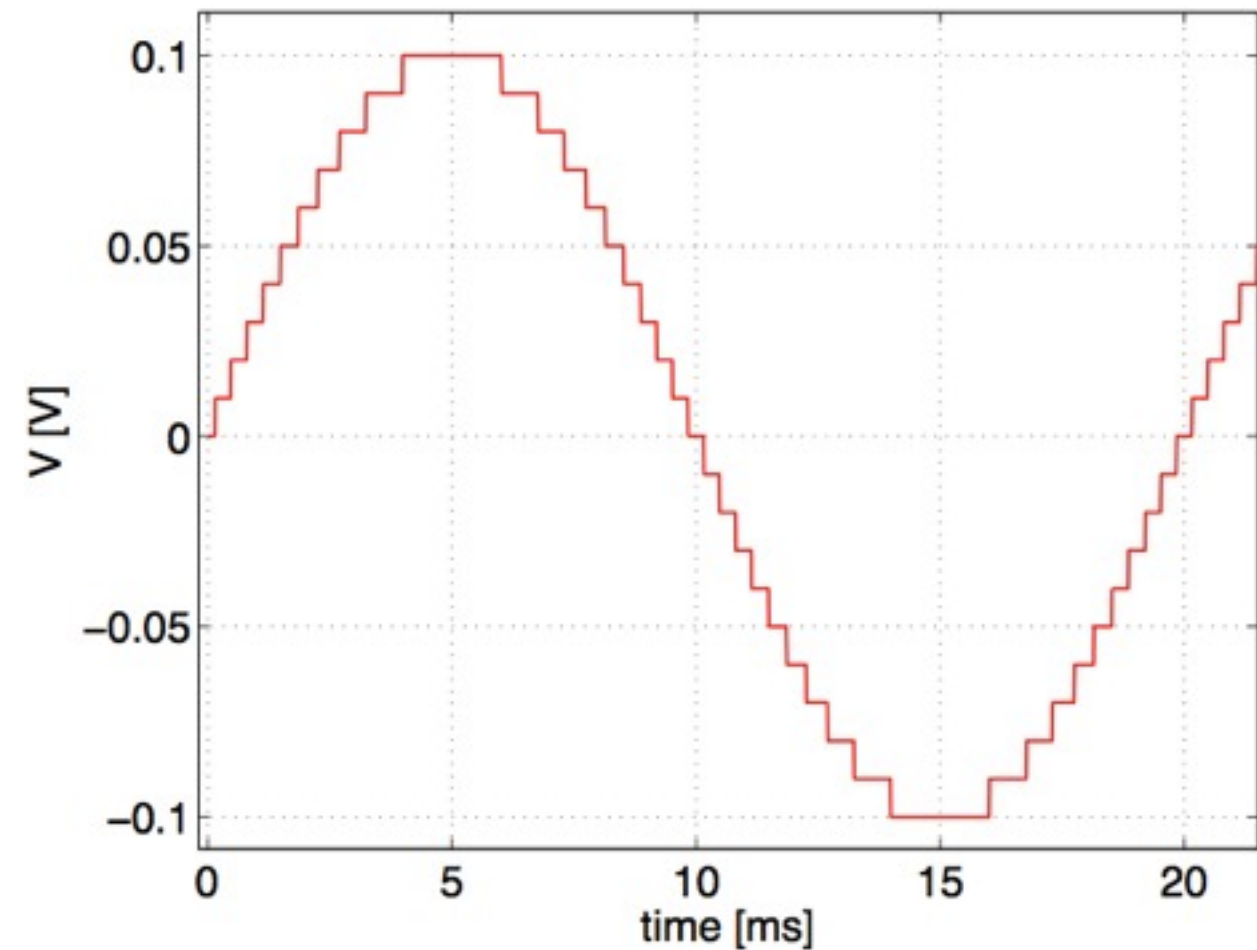
LSB is still 0.01 V



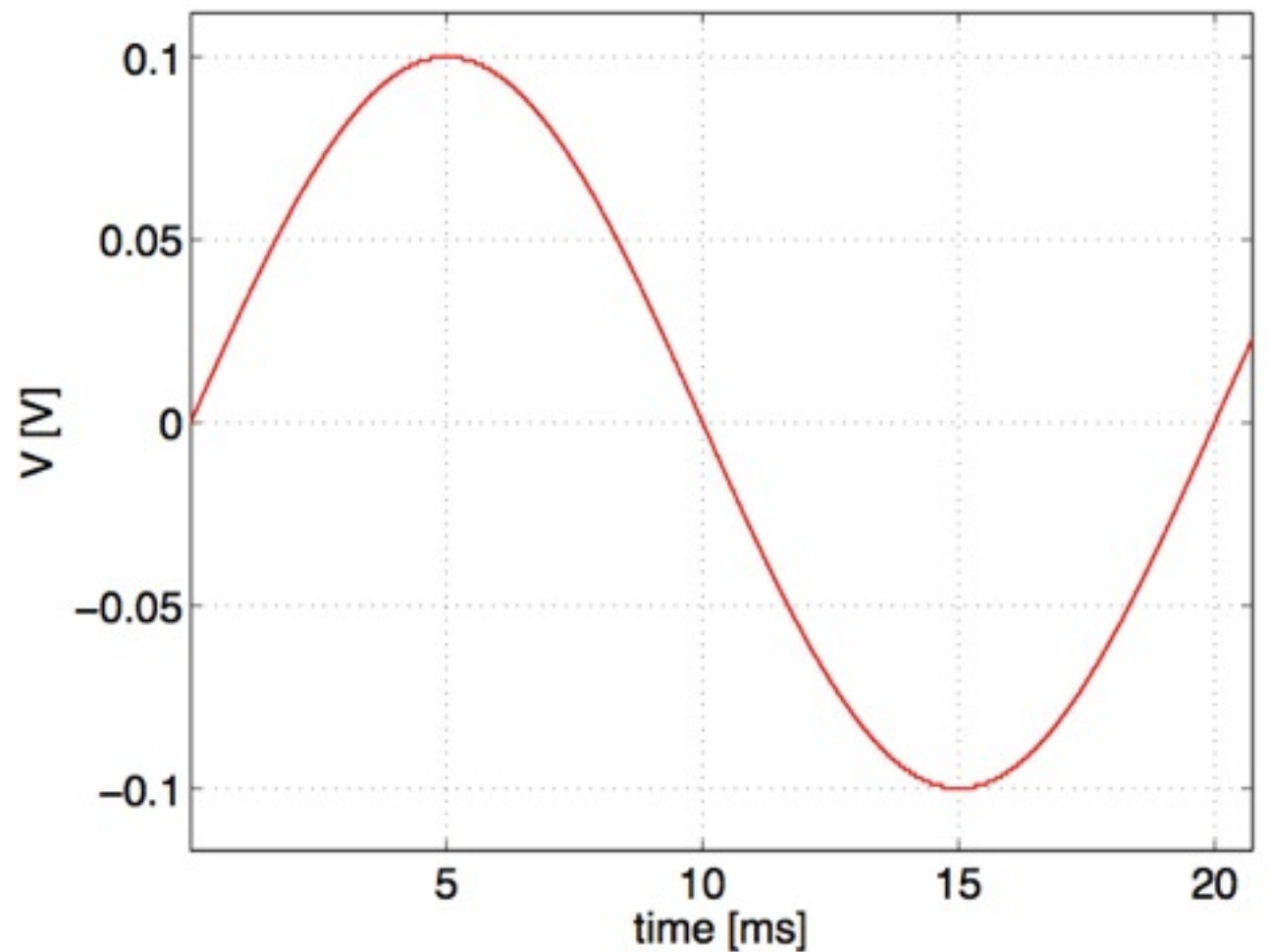
After Analog to digital conversion the signal is quantized.  
I have to *numerically* divide it by 10 to obtain the correct gain.  
Therefore also the LSB will be divided by 10



The quantized signal has lower quantization if we amplify it before ADC and then divide it numerically



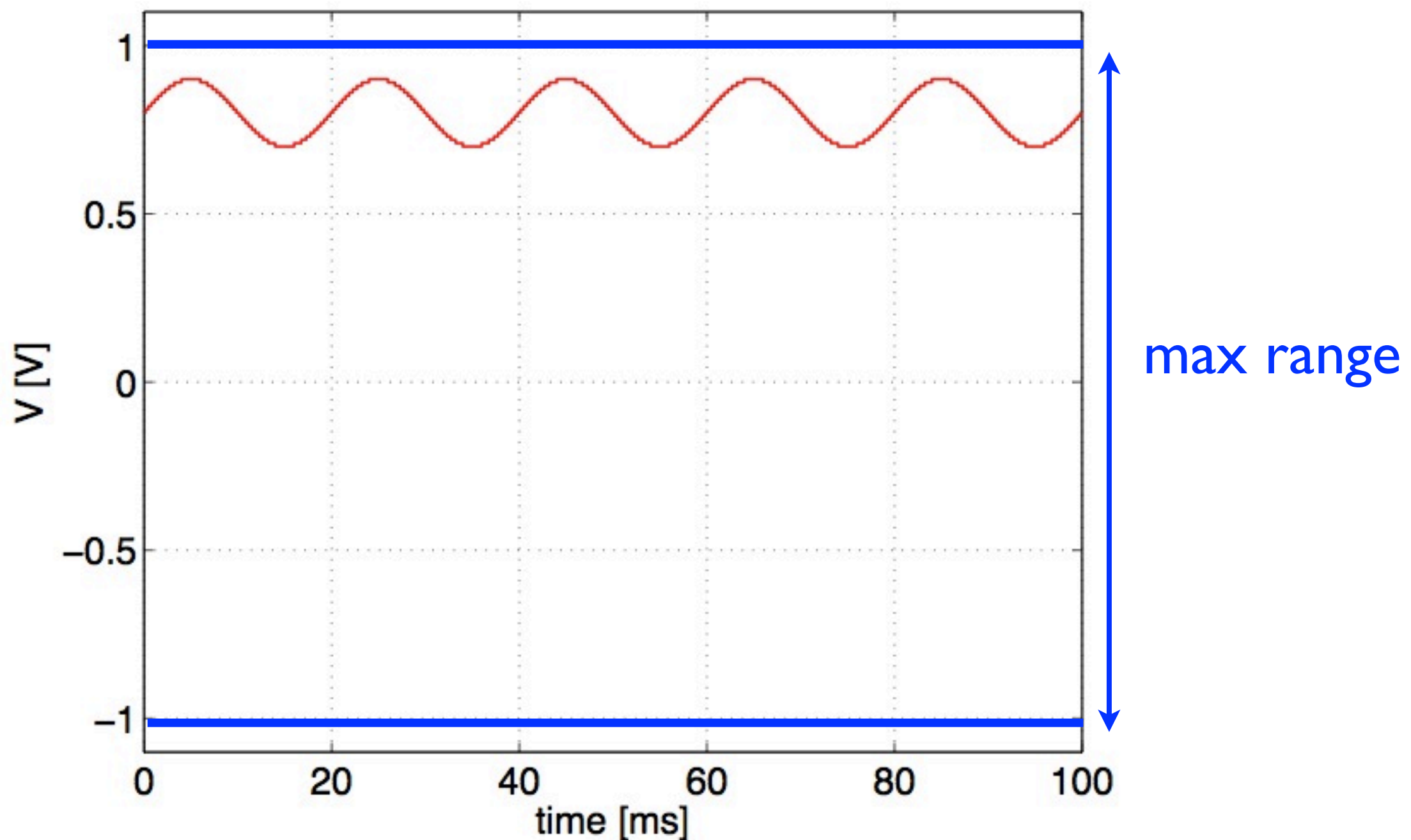
without  
amplification



with  
amplification

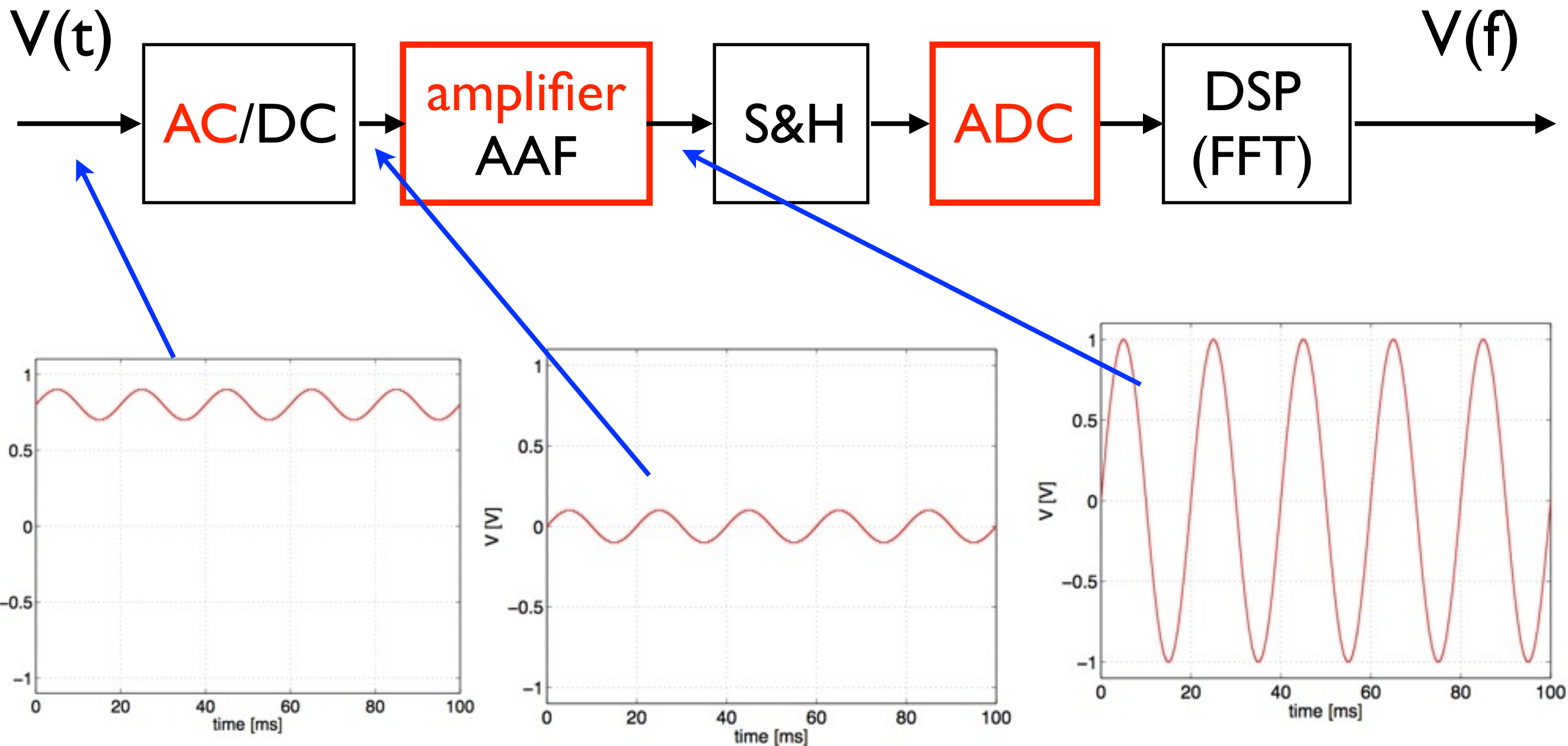


Unfortunately is not always possible to amplify.  
For instance is the average value is large.

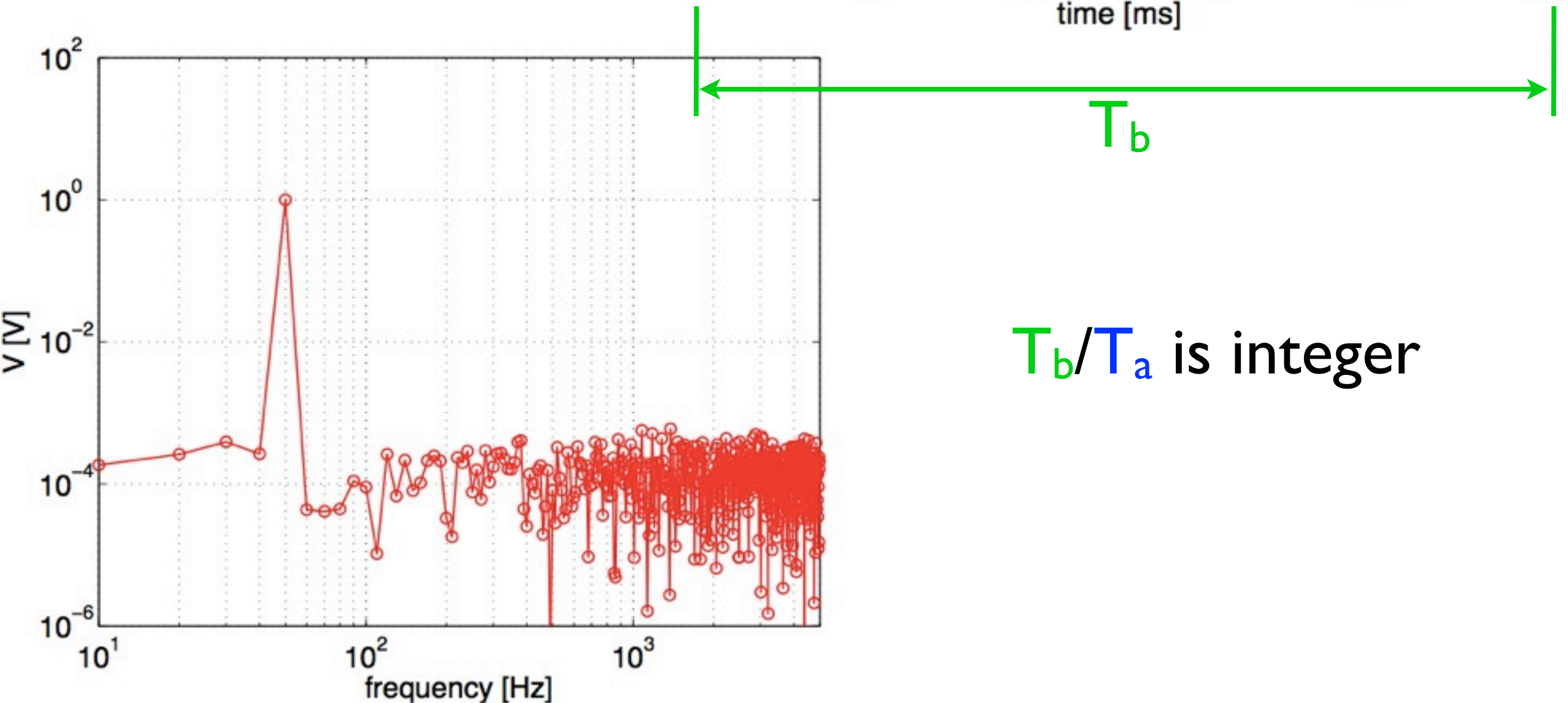
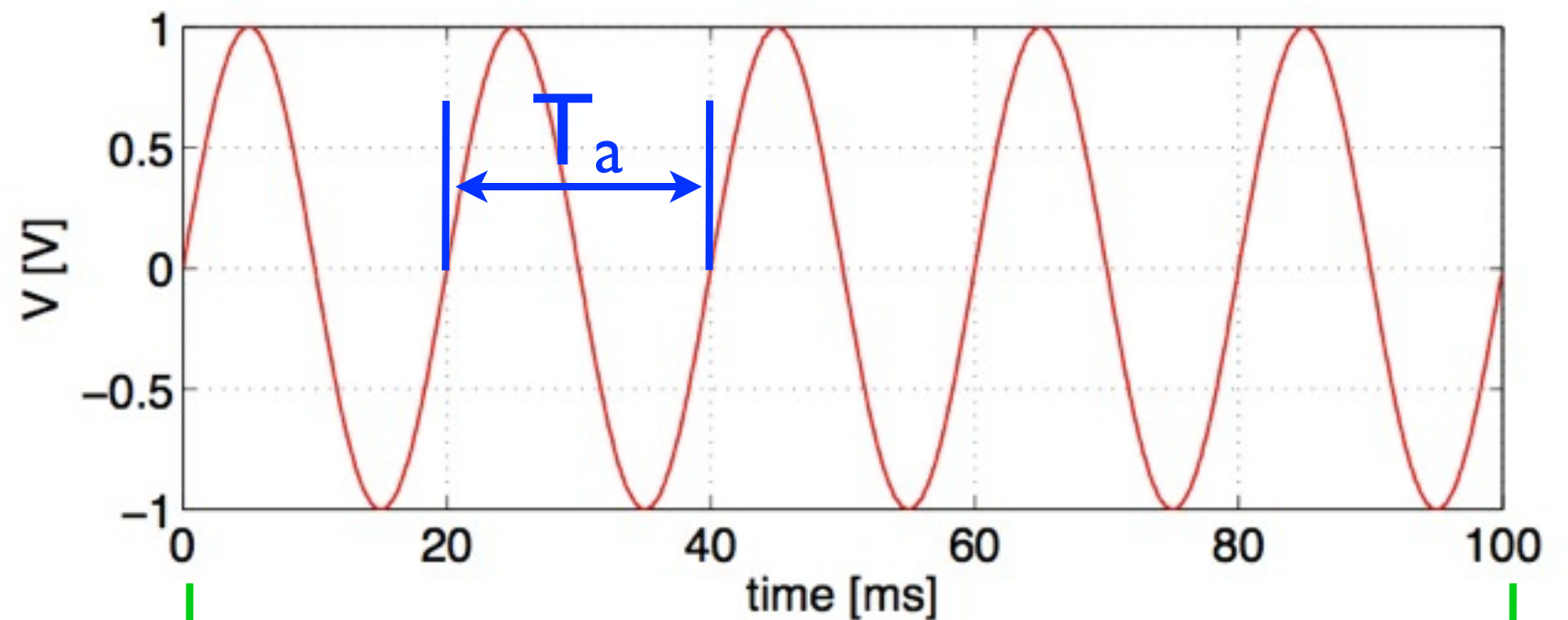


if I amplify I will get into saturation!

In this case, if you are not interested in the average value of the signal you can use AC input to cut it off



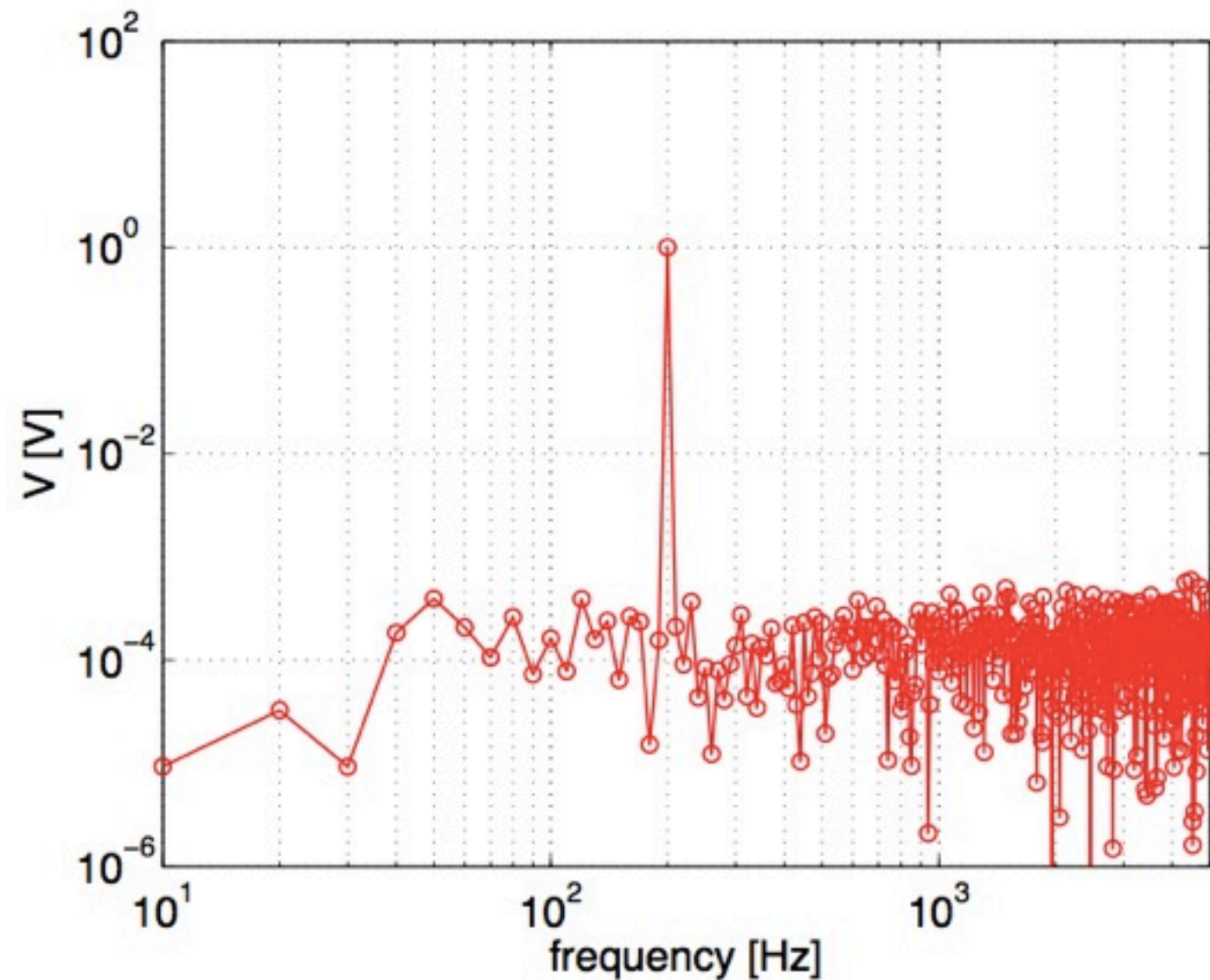
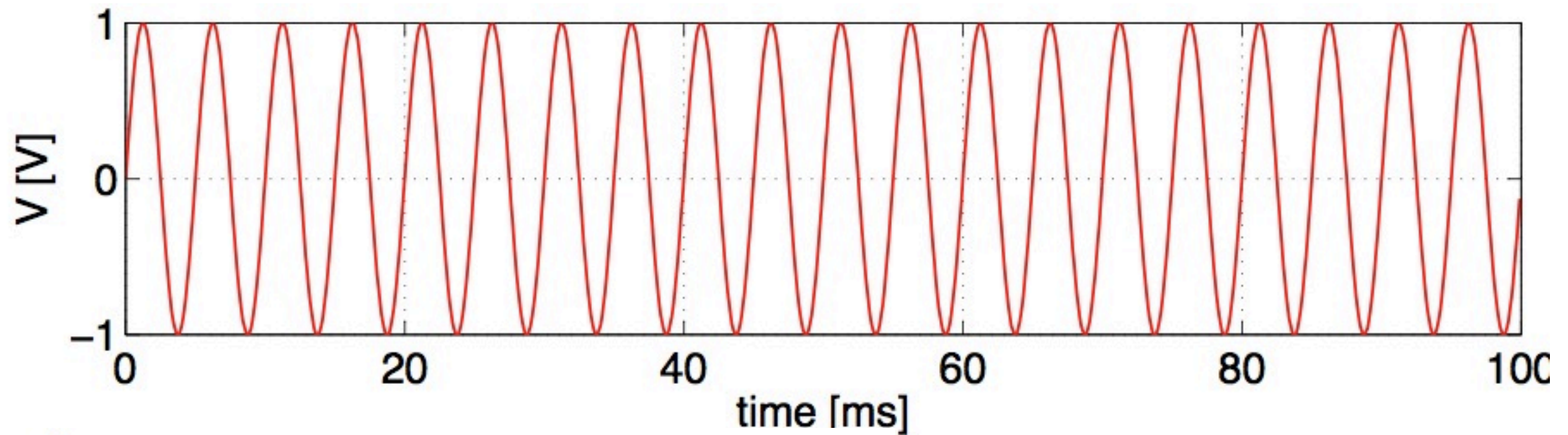
So far we considered only synchronous harmonics.



$T_b/T_a$  is integer

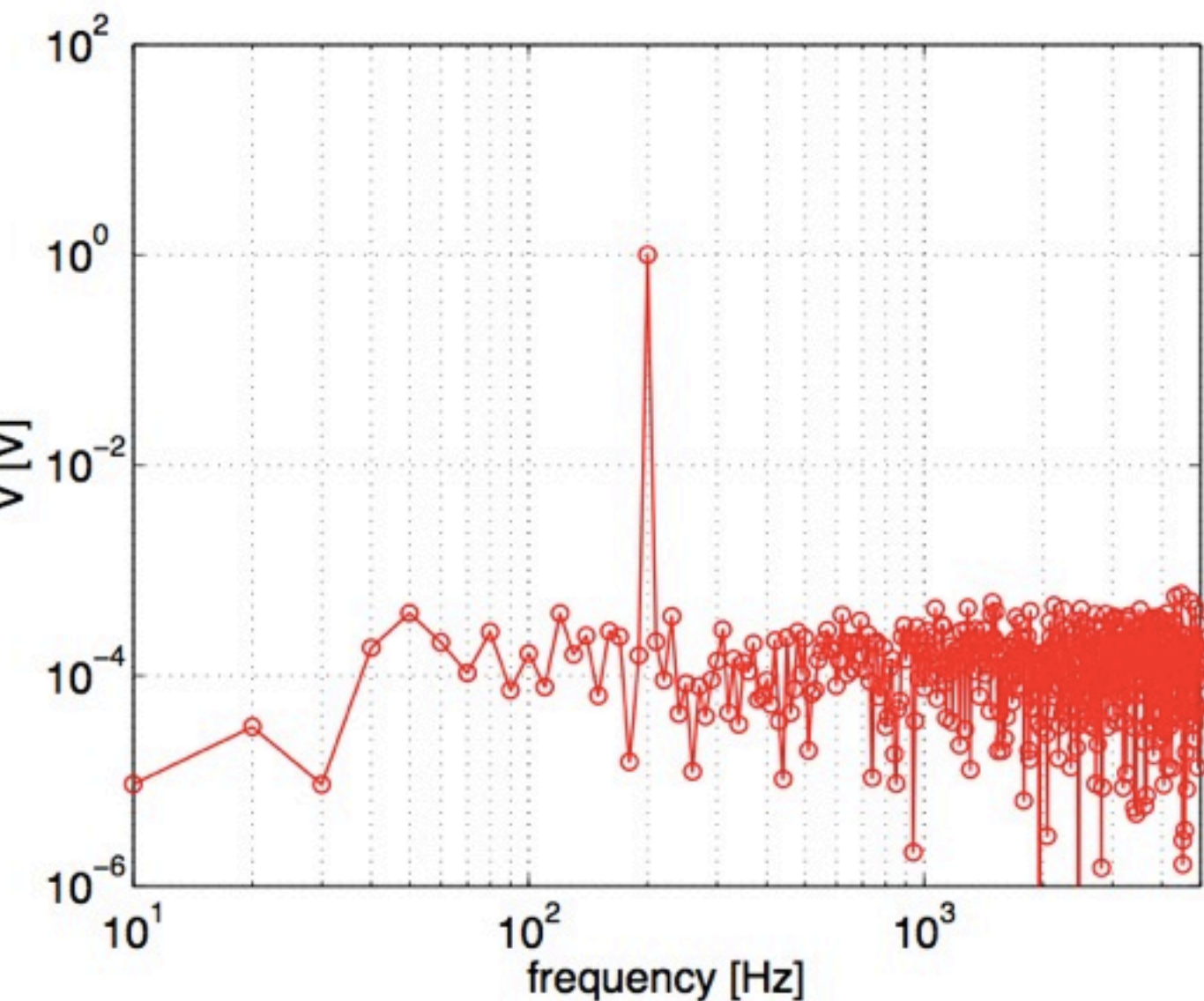


So far we considered only synchronous harmonics.



If the frequency is not synchronous it does not match any of the available frequencies in the spectrum

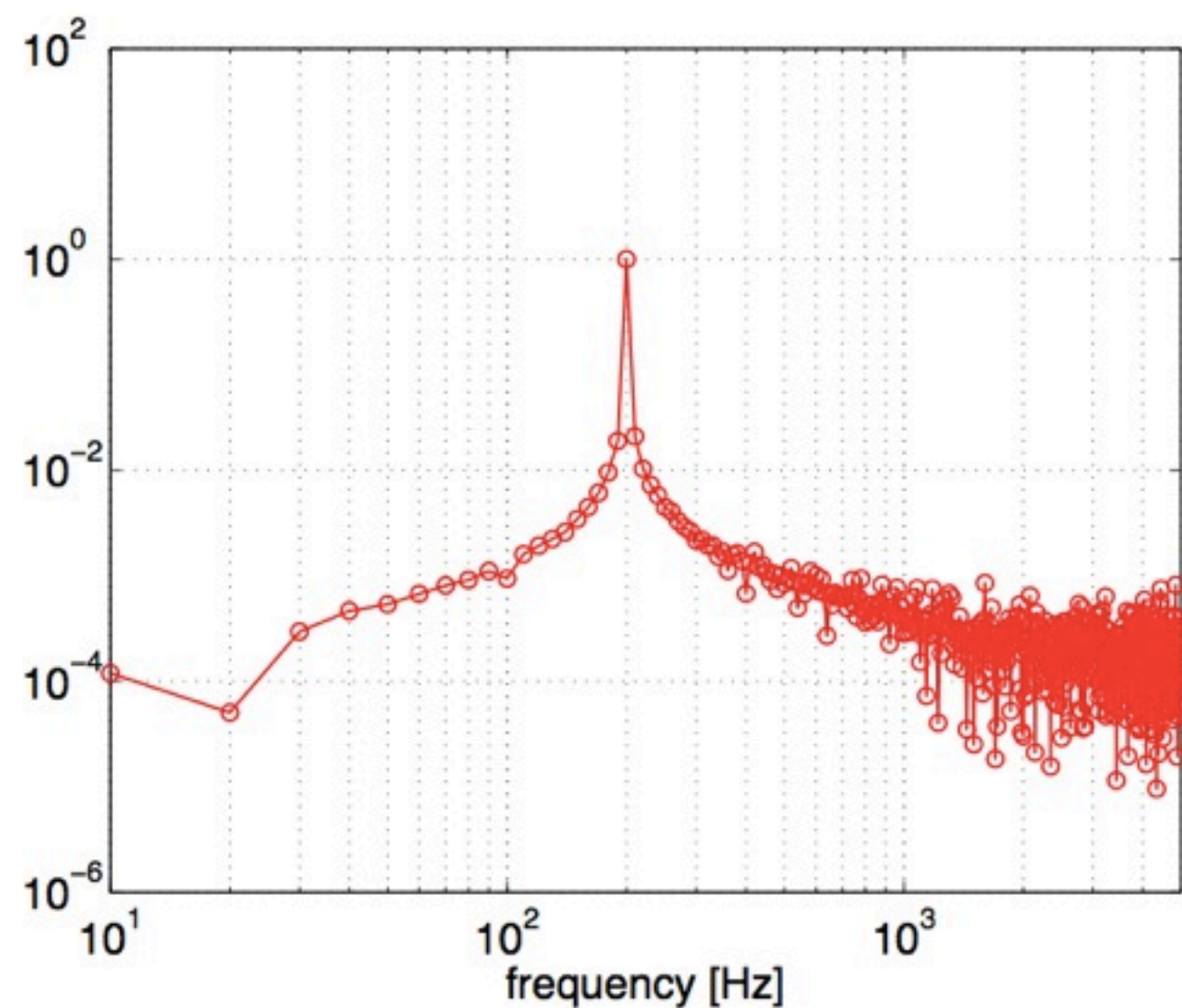
$f=200$  Hz



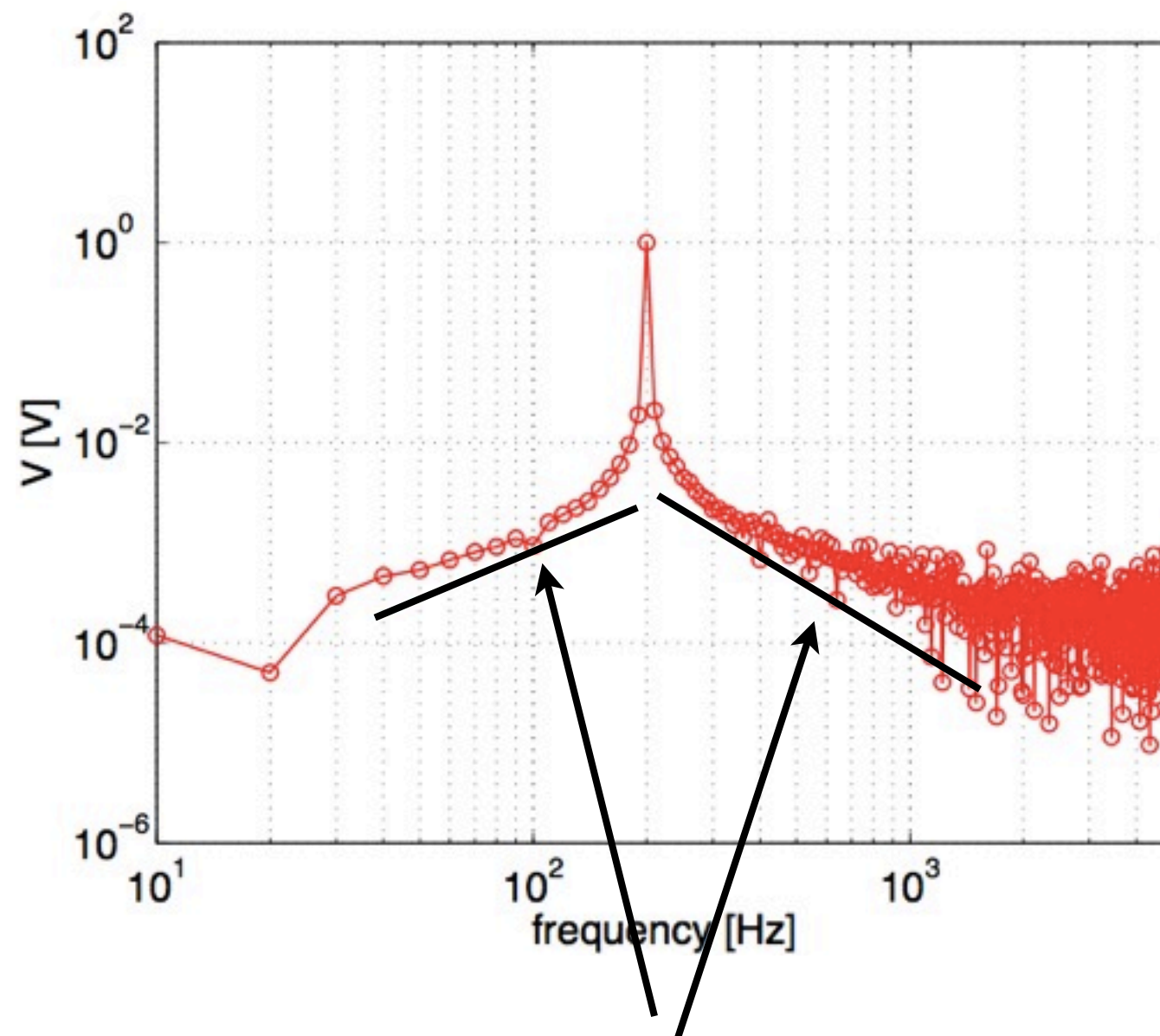
$f=200.2$  Hz

$200 <$

$< 210$



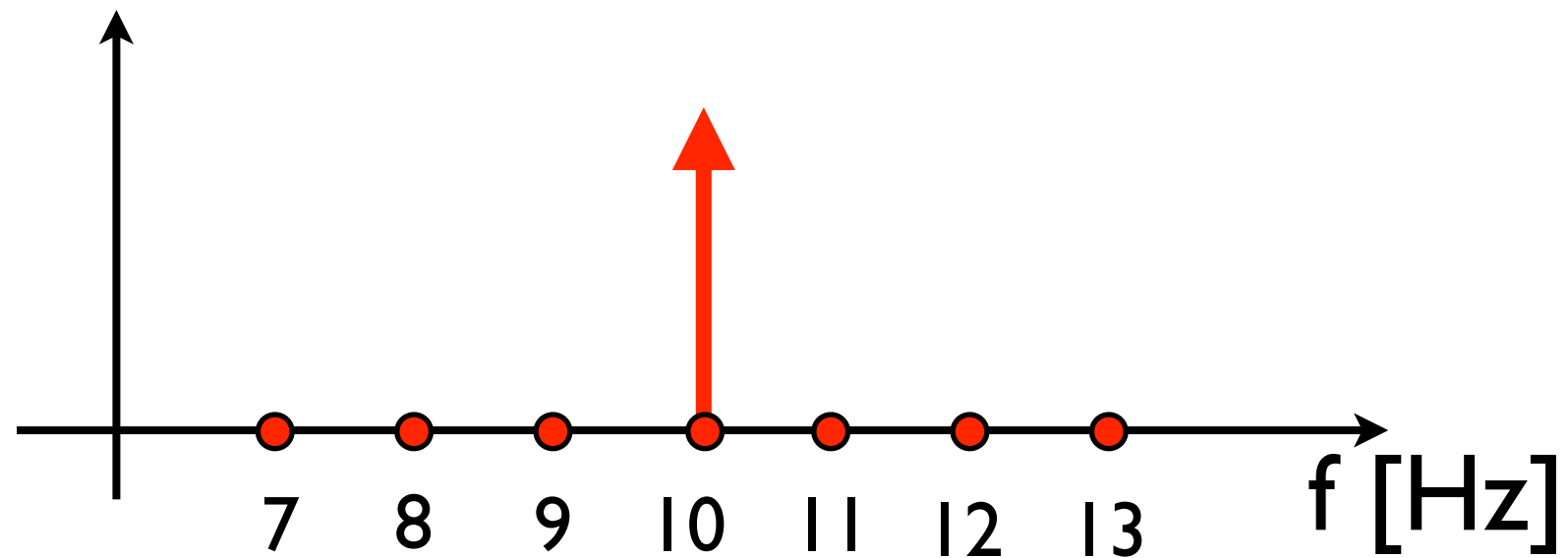




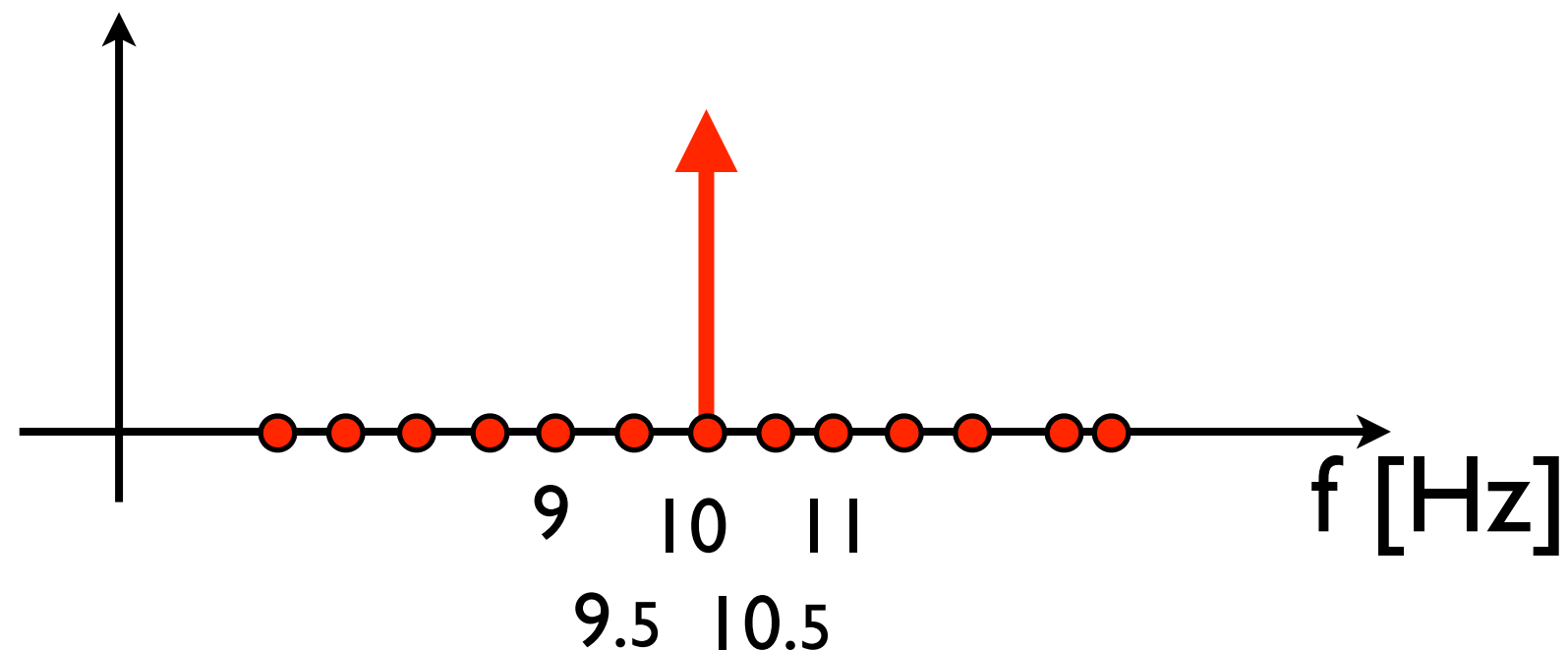
These components in the spectrum do NOT exist!  
They are just artifacts.

In order to avoid this problem on the spectrum analyzer  
you must use proper **WINDOW**

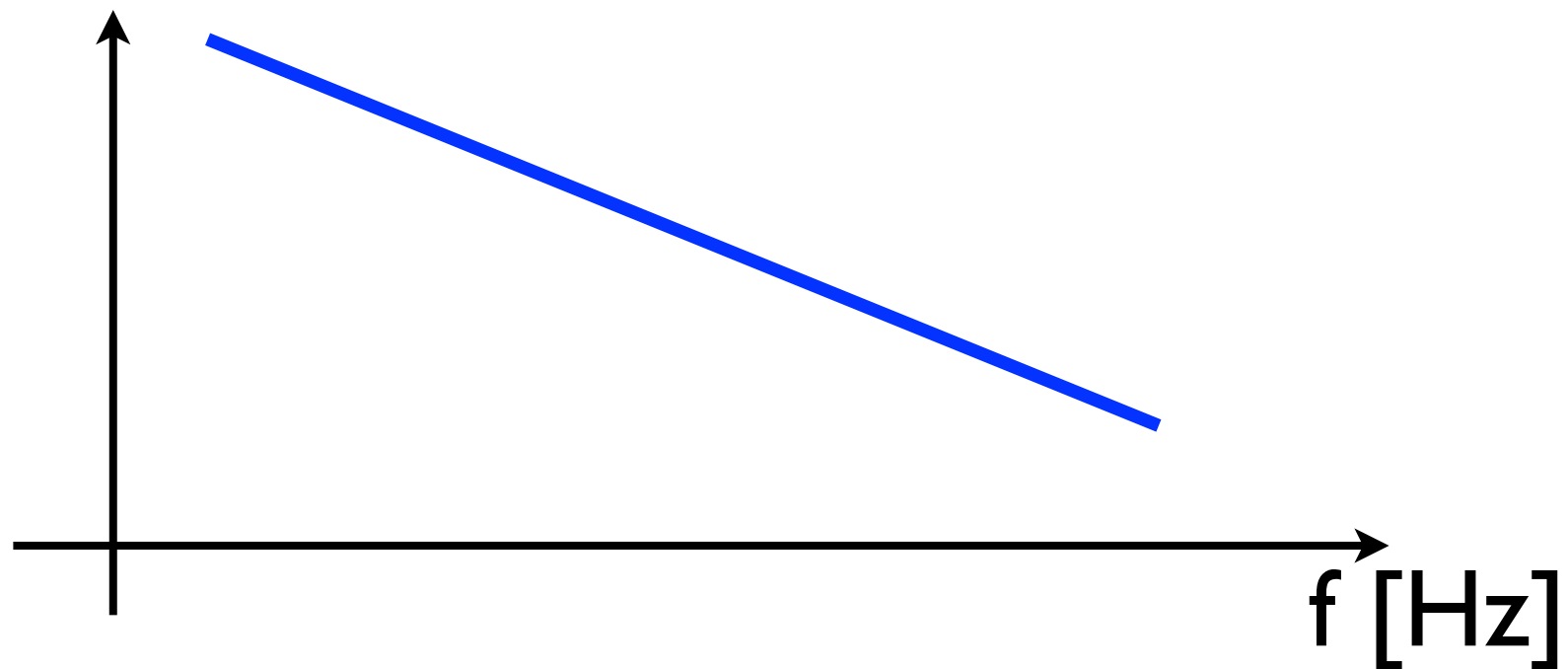
Some signal are “concentrated” in a single frequency



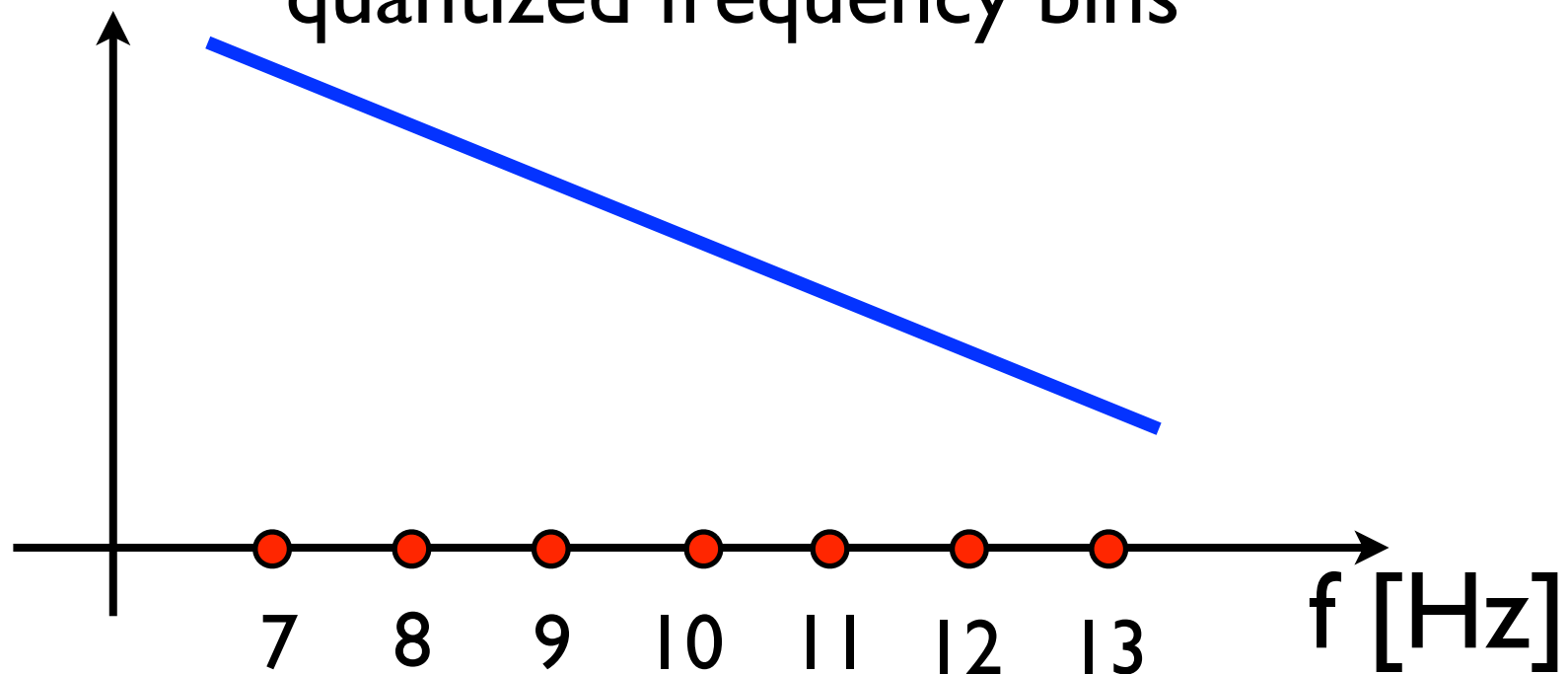
Even if we have better frequency resolution nothing changes



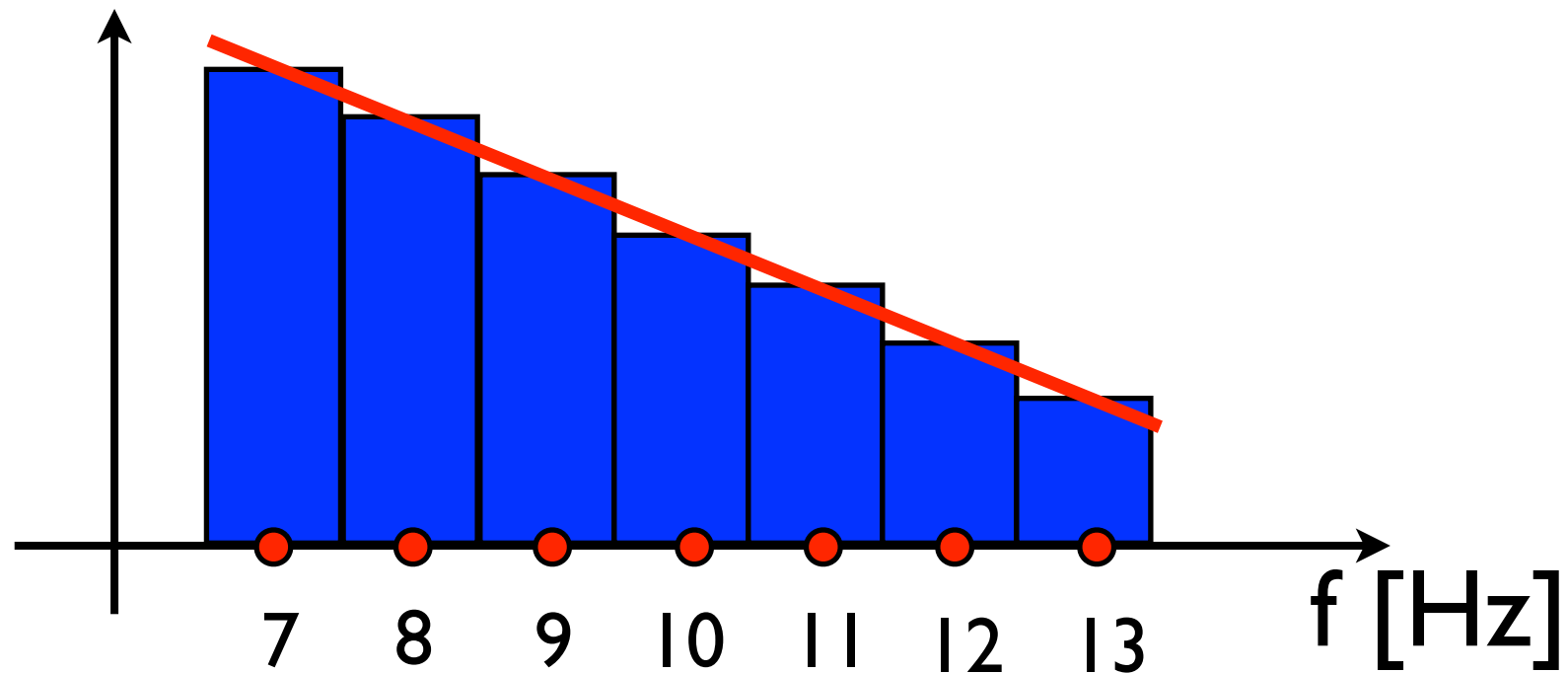
Other signals have a spectrum with continuous frequency components



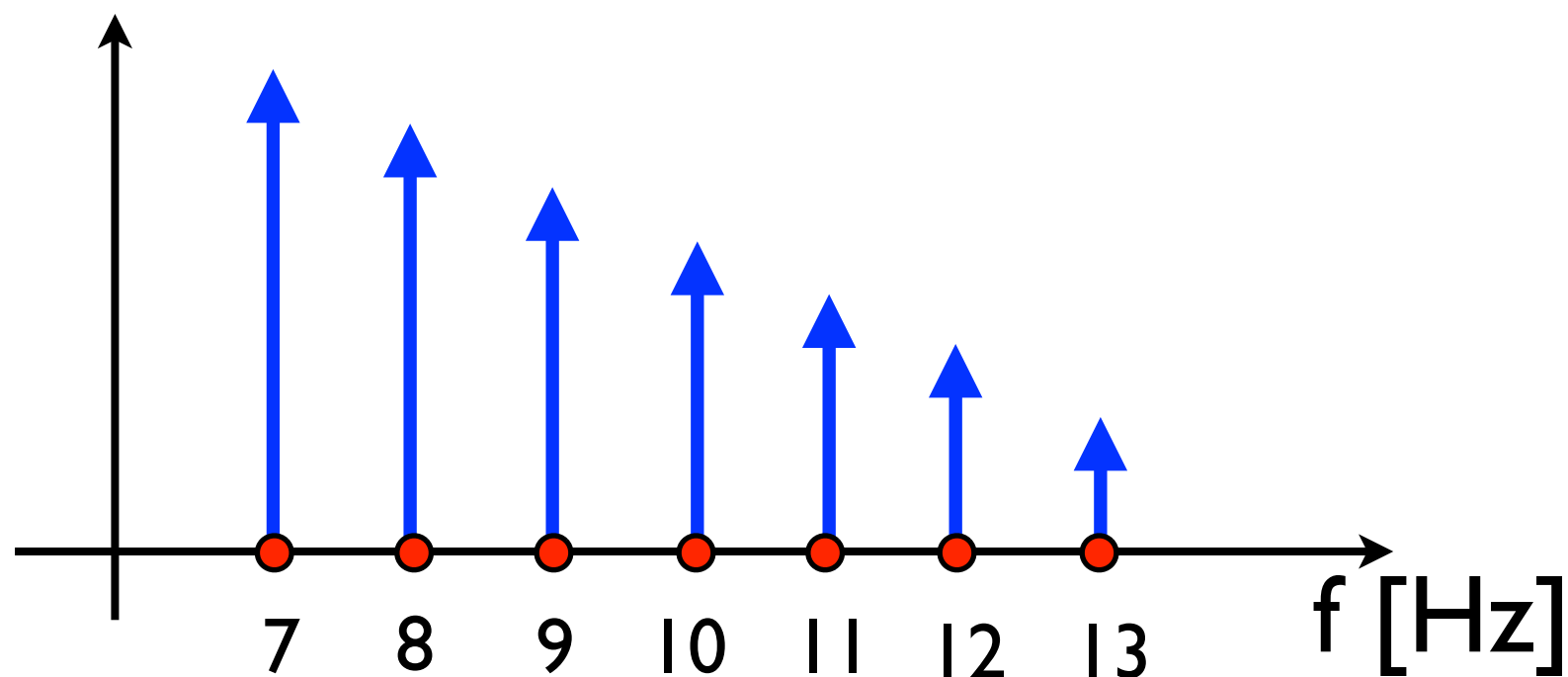
When you calculate the spectrum from the digitized data you have quantized frequency bins

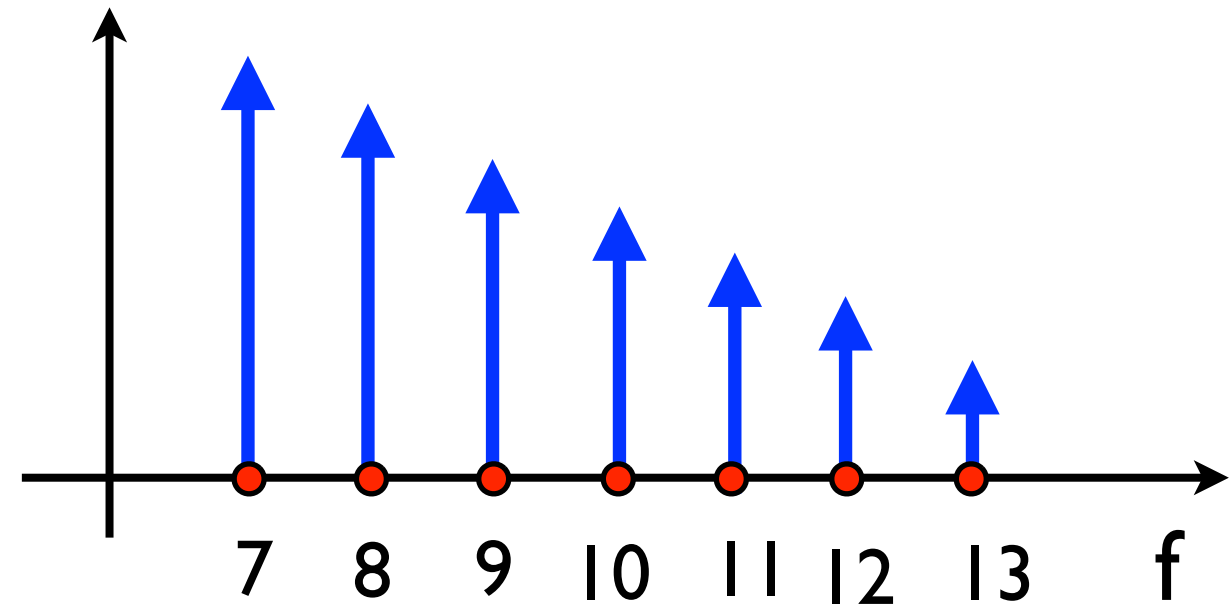
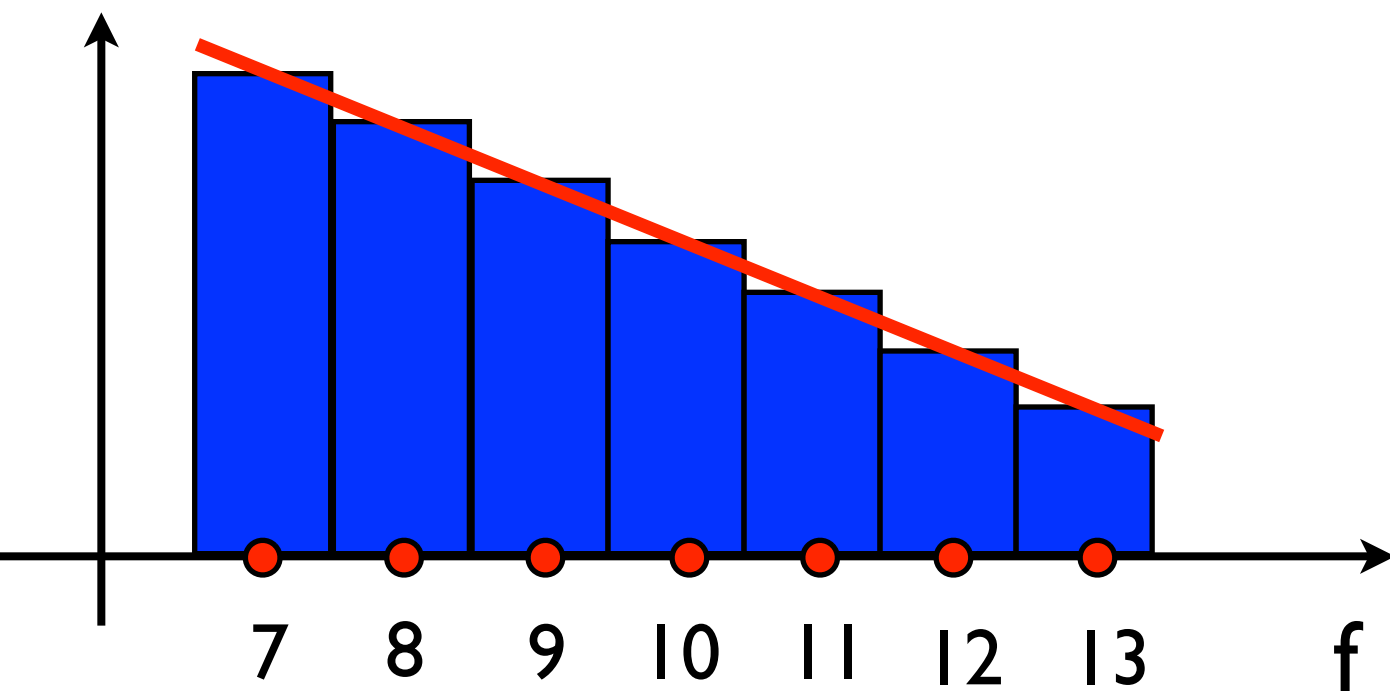




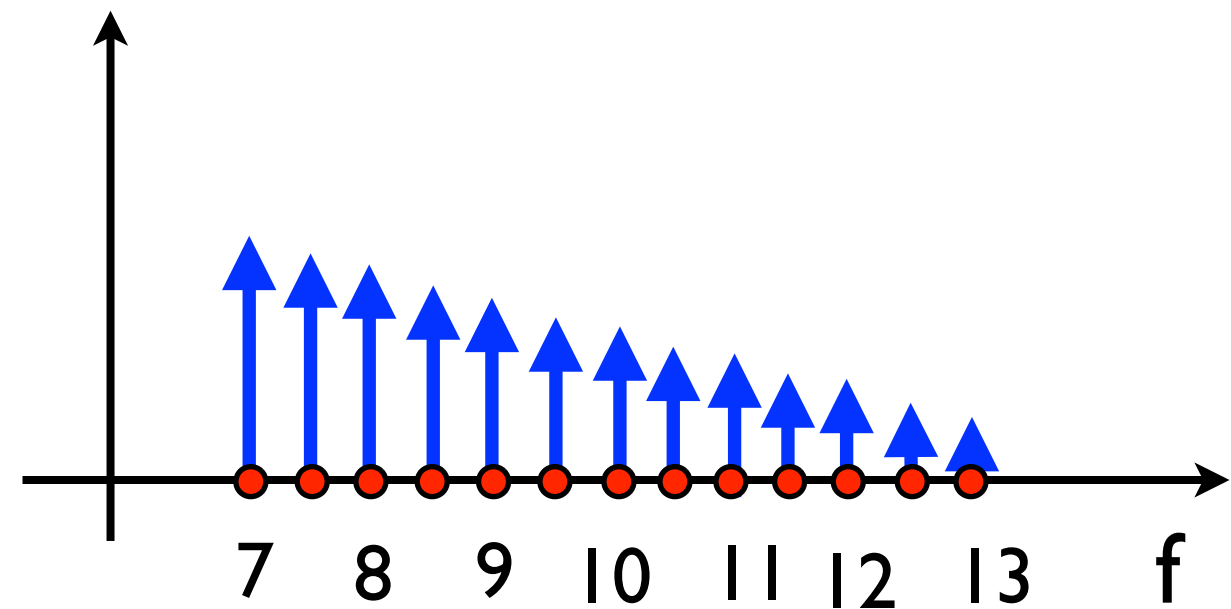
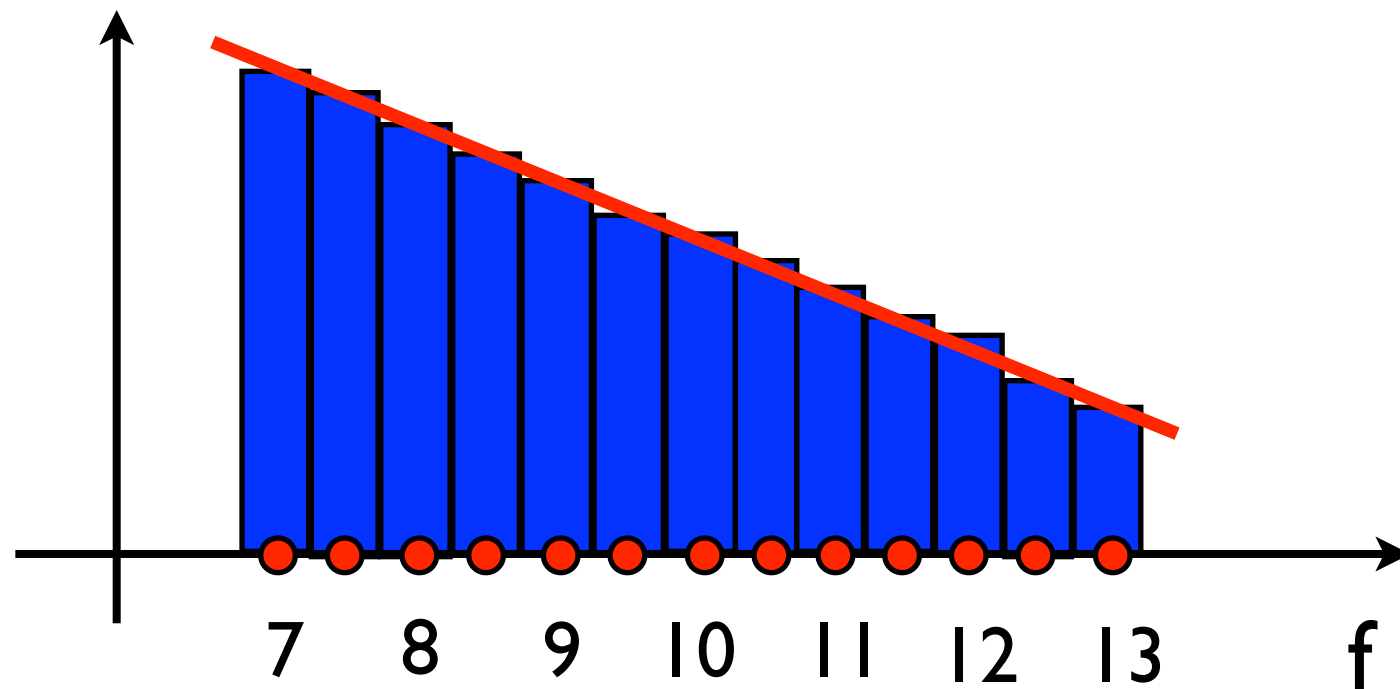


The computed spectrum will have discrete frequency lines, but each of them in fact represent a bin with a frequency width

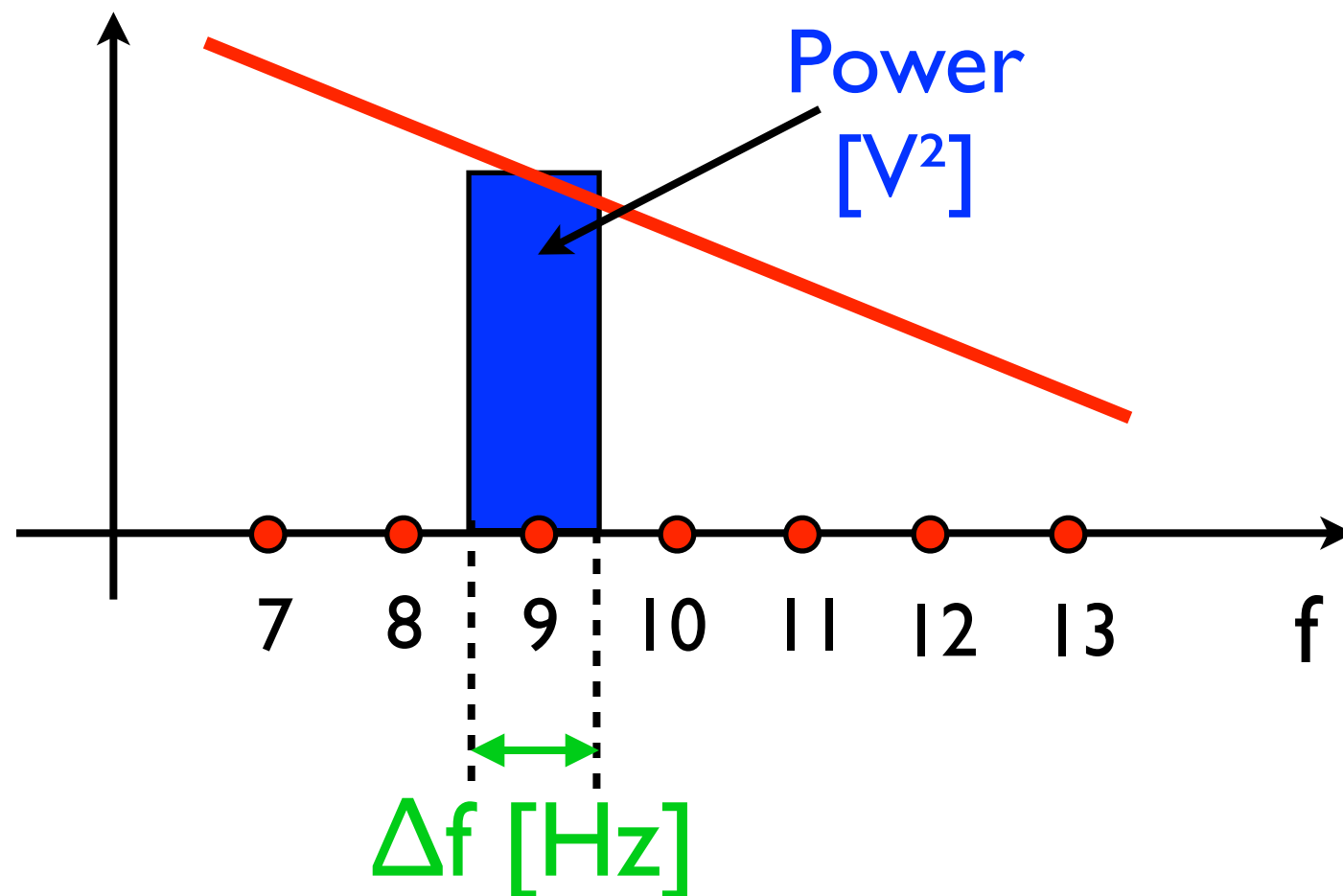




If you increase the frequency resolution you have a larger number of bins. Then, the area of each bin will be lower.



In this case you should set the spectrum analyzer to display  
**PSD (power spectral density)**



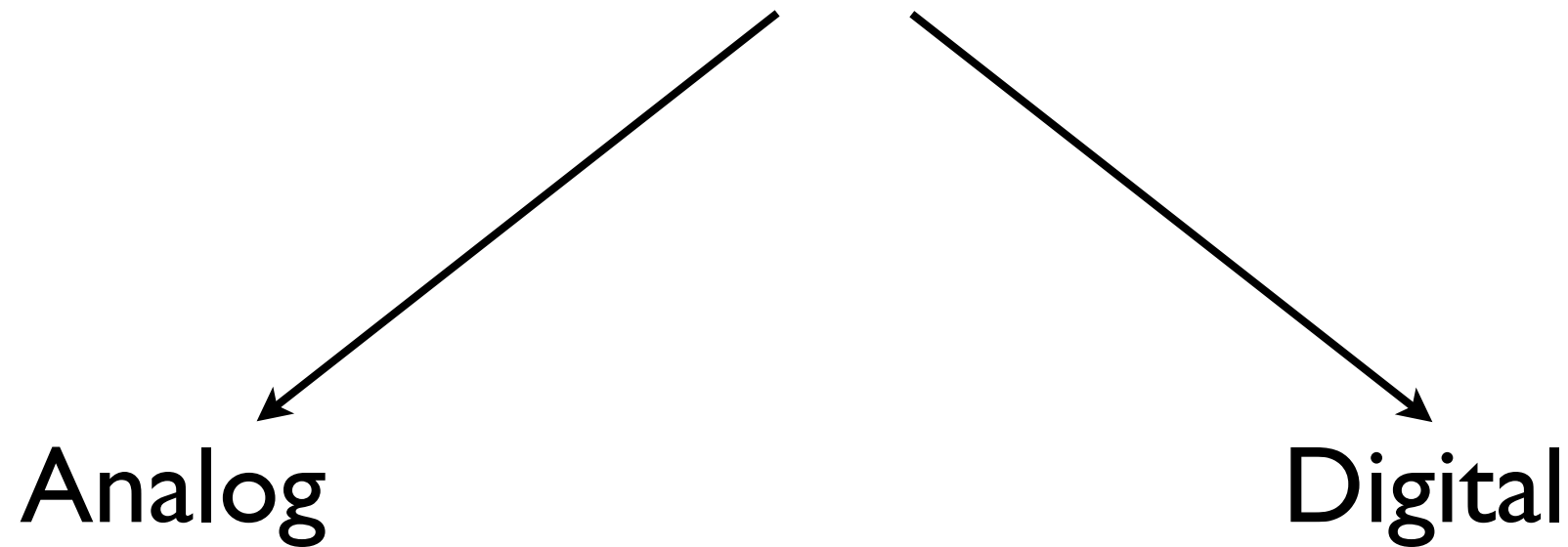
$$\text{PSD} = \text{Power} / \Delta f \\ = [\text{V}^2] / [\text{Hz}]$$

More typically it is  
shown in  $[\text{V}] / \sqrt{[\text{Hz}]}$

The PSD does **NOT** depend on the number of  
frequency bins!

The spectrum analyzer calculates it taking into  
account the width of the bins

# WAVEFORM GENERATORS



- Sinewave generators  
(based on RC or LC  
oscillators)

- Function generators

- Arbitrary waveform  
generators

# Arbitrary waveform generators

