

# Approximate Model Inversion Based Model Reference Adaptive Control (AMI-MRAC)

## RECENT ADVANCES IN MODEL REFERENCE ADAPTIVE CONTROL: THEORY AND APPLICATIONS

### ORGANIZERS

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# Approximate Model Inversion (AMI) Based MRAC

## Plant

$$\ddot{x} = f(x, \dot{x}, u),$$

- $x \in \Re^n$  : system states
- $u \in \Re^m$  : control inputs (**multiple input**), controllable
- $f$  satisfies conditions for a unique solution, unknown

## Problem Statement: Model Reference Adaptive Control

Design a control law  $u(t)$  such that the plant tracks the reference model

$$\ddot{x}_{rm} = f_{rm}(x_{rm}, \dot{x}_{rm}, r)$$

- $x_{rm} \in \Re^n$  : system states
- $r \in \Re^l$  : Exogenous inputs
- $f_{rm}$  bounded input bounded output stable and continuously differentiable

# Approach

- Design a pseudo control  $\nu \in \Re^n$  such that  $x \rightarrow x_{rm}$
- If plant model were known and invertible, then we can simply set  $u = f^{-1}(x, \dot{x}, \nu)$ , in this case  $\nu = \ddot{x}_{desired}$
- However, this is usually not the case, so **choose** an inversion model  $\hat{f}$  and let  $u = \hat{f}^{-1}(x, \nu)$

## Assumption

The approximate inversion model  $\hat{f}: \Re^{n+l} \rightarrow \Re^n$  is continuous,  
The operator  $\hat{f}^{-1}: \Re^{2n} \rightarrow \Re^l$  exists and assigns a unique  $u \in \Re^l$  to every unique  $(x, \dot{x}, \nu) \in \Re^{2n}$

- So, we have  $\nu = \hat{f}(x, \dot{x}, u)$
- Realize that this usually means  $\dim(\ddot{x}) = \dim(u)$ . This is a matter of finding the right representation for most feedback linearizable systems
- E.g. in rotorcraft control, dim inputs 4, and 4 key directly affected states ( $p, q, r, a_z$ )

# AMI-MRAC

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- Alternative system descriptions that can be handled:

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= f(x_1, x_2, u)\end{aligned}$$

- As an example, consider systems affine in control

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= Gx_2 + B(\Theta(x_1, x_2) - u)\end{aligned}$$

- In this case, if the pair  $(G, B)$  is controllable, we can use  $v = Bu(t)$  is a valid choice for inversion model
  - The model error here is:  $\Delta(x_1, x_2) = Gx_2 + B\Theta(x_1, x_2)$
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# Control Action

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- Control task: Design a pseudo control  $v$  that achieves  
 $e = \begin{bmatrix} x_{rm} - x \\ \dot{x}_{rm} - \dot{x} \end{bmatrix} \rightarrow 0$
- The combined control action has the following three parts
- Linear feedback

$$v_{pd} = [K_p \quad K_d] \begin{bmatrix} x_{rm} - x \\ \dot{x}_{rm} - \dot{x} \end{bmatrix}$$

- Feedforward

$$v_{rm} = \ddot{x}_{rm}$$

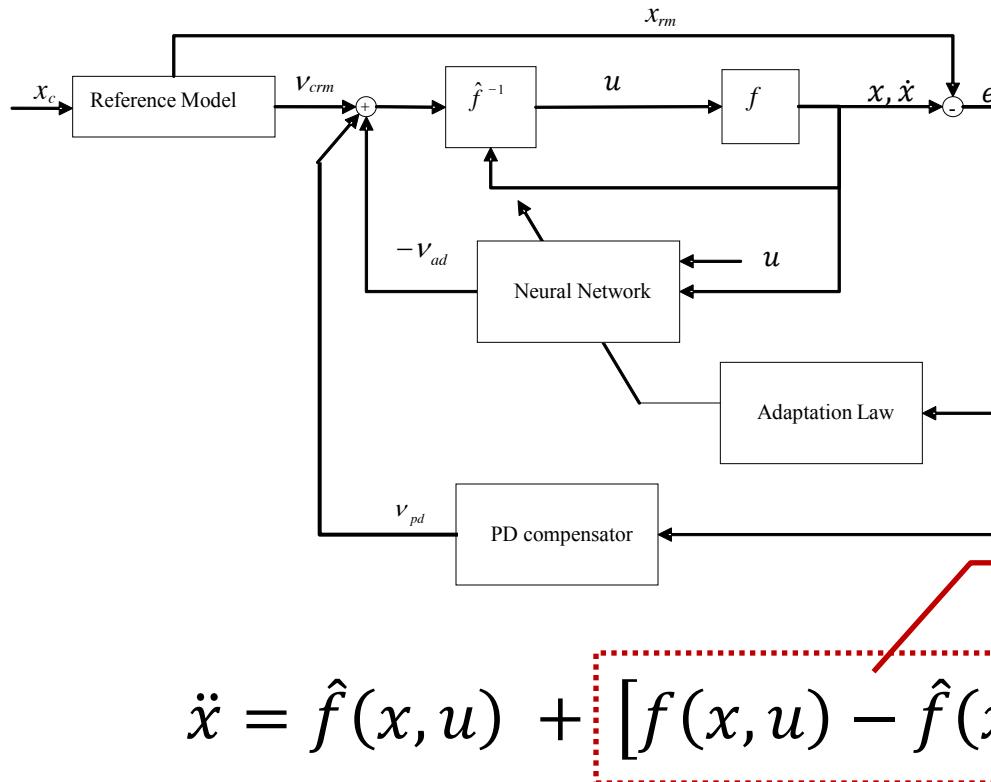
- Adaptive

$$v_{ad}$$

- Combined control action:

$$v = v_{pd} + v_{rm} - v_{ad}$$

# Tracking Error Dynamics



■ So,  $\ddot{x} = v + \Delta(x, u)$

# Tracking error dynamics

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■ Let's differentiate  $e$ ,

$$\dot{e} = \begin{bmatrix} \dot{x}_{rm} - \dot{x} \\ \ddot{x}_{rm} - \ddot{x} \end{bmatrix}$$

■ Now,  $\ddot{x} = \hat{f}(x, u) + [f(x, u) - \hat{f}(x, u)] = v + \Delta(x, u)$

$$\dot{e} = \begin{bmatrix} \dot{x}_{rm} - \dot{x} \\ v_{rm} - (v + \Delta) \end{bmatrix} = \begin{bmatrix} \dot{x}_{rm} - \dot{x} \\ v_{rm} - (v_{pd} + v_{rm} - v_{ad} + \Delta) \end{bmatrix}$$

Let  $A = \begin{bmatrix} 0 & I \\ K_{pd} & K_d \end{bmatrix}$ , and  $B = \begin{bmatrix} 0 \\ I \end{bmatrix}$

## Tracking error dynamics

$$\dot{e} = Ae + B(v_{ad} - \Delta)$$

# Choice of adaptive element

## Structured Uncertainty

Given that there exists a constant matrix  $W^*$  and known basis functions  $\Phi(x, u)$  such that

$$\Delta(x, u) = W^{*T} \Phi(x, u)$$

Then, choose adaptive element:

$$\nu_{ad} = W^T \Phi(x, u)$$

## Unstructured Uncertainty

Given  $\Delta(x, u)$  is continuous and defined over a compact set, then :

$$\Delta(x, u) = g(x, u, W) + \tilde{\epsilon}$$

where  $g$  is some universal function approximator parameterized by  $W$

# Adaptive law

- So,  $v = v_{pd} + v_{rm} - W^T(t)\Phi(x, u)$
- In traditional direct adaptive control, the aim is to create an adaptive law  $\dot{W}$  such that  $e \rightarrow 0$
- The key idea is going to be to update the weights such that some reward is maximized

## Instantaneous Error Minimization

Updates weights in the direction of maximum reduction of quadratic cost of the instantaneous tracking error

$$\dot{W}(t) \cong -\Gamma \frac{\partial(e(t)^T e(t))}{\partial W}$$

# MRAC with Instantaneous data

## Instantaneous Error Minimization

Updates weights in the direction of maximum reduction of quadratic cost of the instantaneous tracking error

$$\dot{W}(t) \cong -\Gamma \frac{\partial(e(t)^T e(t))}{\partial W}$$

- Letting  $P$  be the solution of the closed loop Lyapunov equation and  $\Gamma > 0$  the learning rate, this results in the following **rank -1** adaptive law:

$$\dot{W} = -\Gamma \Phi(x) e^T P B$$

- This adaptive law requires PE to ensure exponential stability of  $(e, \tilde{W} \equiv 0)$

# Derivation of adaptive law

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- Recall tracking error dynamics:

$$\dot{e} = Ae + B(\nu - \Delta)$$

- $\nu - \Delta = W^T(t)\Phi(x, u) - W^{*T}\Phi(x, u) = \tilde{W}^T\Phi(x, u)$

- Since  $A$  is Hurwitz by design, we have that for every positive definite  $Q$ , a positive definite matrix  $P$  exists such that:

$$AP + PA^T + Q = 0$$

- Let's start with a positive definite Lyapunov Candidate:  $V(e, \tilde{W}) = \frac{1}{2}e^T Pe + \frac{1}{2}\tilde{W}^T \Gamma^{-1} \tilde{W}$

# Derivation of adaptive law

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- Lie derivative of the Lyapunov candidate

$$\dot{V}(e, \tilde{W}) = -e^T Q e + e^T P B (\nu - \Delta) + \dot{W}^T \Gamma^{-1} \tilde{W}$$

$$\dot{V}(e, \tilde{W}) = -e^T Q e + e^T P B \tilde{W}^T \Phi(x, u) + \tilde{W}^T \Gamma^{-1} \dot{W}$$

- Notice that  $e^T P B$  is a scalar, so

$$\dot{V}(e, \tilde{W}) = -e^T Q e + \tilde{W}^T (\Gamma^{-1} \dot{W} + e^T P B \Phi(x, u))$$

- Set the term in the bracket to zero, so

$$\dot{W} = \Gamma e^T P B \Phi(x, u)$$

$$\dot{V}(e, \tilde{W}) \leq -\frac{1}{2} \lambda_{min}(Q) \|e\|^2$$

- From here use Barbalat's lemma to show that  $e \rightarrow 0$  asymptotically, and weights bounded (when no noise)
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# Entire closed loop system

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- The entire closed loop system has two coupled differential equations:

$$\begin{aligned}\dot{e} &= Ae + B\tilde{W}^T\Phi(x, u) \\ \dot{\tilde{W}} &= -\Gamma e^T PB\Phi(x, u)\end{aligned}$$

- Here we assumed  $\tilde{W}^*$  to be a constant
  - Notice no feedback from  $\tilde{W}$  in the second equation
  - This could lead to issues with boundedness of  $\tilde{W}$ , especially if there is noise in the system
  - When does  $\tilde{W} \rightarrow 0$ ? (Persistency of excitation)
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# Some relevant existing work

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- Baseline adaptive law only guarantee  $e(t) \rightarrow 0$  asymptotically, no performance guarantees
  - Classic modifications for weight boundedness:
    - $\sigma$ -mod (Ioannou 84),  $e$ -mod (Narendra 86), projection based adaptation
  - Intelligent excitation (Cao 07):
    - Excitation enforced as a function of tracking error
    - Increased control cost due to added excitation
  - $L_1$  adaptive control (Cao, Hovakimyan 08)
  - $Q$ -modification (Volyanksyy 09)
  - Direct Recursive Least Squares Adaptation (Nguyen 2006)
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# Example: Inverted pendulum

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- A nonlinear system which resembles an inverted pendulum

$$\ddot{x} = \delta + \sin(x) - |\dot{x}| \dot{x} + 0.5 e^{x \dot{x}}$$

- Approximate inversion model:  $v = \delta$

- Model error  $\Delta = [1 \quad -1 \quad 0.5] \begin{bmatrix} \sin(x) \\ |\dot{x}| \dot{x} \\ e^{x \dot{x}} \end{bmatrix}$

- Second order reference model
  - Simulation file: invpendu\_dmrac
-

# Wing Rock dynamics simulation

- Highly swept-back aircraft are susceptible to Wing Rock: lightly damped oscillations
- $\phi$ : roll angle,  $p$  roll rate,  $\delta_a$  aileron

## A model for Wing Rock dynamics (Monahemi 96)

$$\begin{aligned}\dot{\phi} &= p \\ \dot{p} &= \delta_a + \Delta(\phi, p)\end{aligned}$$

- Inversion model:  $v = \delta$
- Task: track roll commands in presence of wing rock dynamics:

$$\Delta(\phi, p) = 0.8 + 0.23\phi + 0.69p - 0.62|\phi| + 0.01|p|p + 0.02p^3$$

- Second order reference model used
- Simulation file: wingrock\_dmrac\_simple

# Issues

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- Boundedness of  $\tilde{W}$  in presence of noise etc
- Transient response
- Actuator saturation
- Imperfect selection of basis

# Neuroadaptive Control

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AIAA Guidance Navigation and Control Conference

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# Introduction

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- Neural Networks are universal function approximators
  - That means, given any continuous function on a compact domain, we have a tool to form a good approximation without having to know more
  - Single Hidden Layer, and Radial Basis Function NN have been widely used as adaptive elements
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# Model Reference Adaptive Control

## Plant

$$\dot{x}(t) = Ax(t) + B(u(t) + \Delta(x(t))),$$

- $x \in \Re^n$ : system states,  $u \in \Re$ : control inputs,  $\Delta(x(t))$ : uncertainty
- $A \in \Re^{n \times n}$ ,  $B = [0, \dots, 1]^T$ , easily generalizes to multi-input cases

## Problem Statement: Model Reference Adaptive Control

Design a control law  $u(t)$  such that the plant tracks the reference model

$$\dot{x}_{rm}(t) = A_{rm}x_{rm}(t) + B_{rm}r(t),$$

- $x_{rm}(t) \in \Re^n$ : system states,  $r(t) \in \Re$ : Exogenous inputs
- Assumed bounded input bounded output stable
- Chosen to characterize the desired response

# Control Action

- The tracking control law has the following three parts:

- Linear feedback

$$u_{pd} = K(x_{rm} - x)$$

- Linear feedforward:

$$u_{rm} = K_r[x_{rm}, r]$$

- Adaptive part

$$u_{ad}$$

## Tracking control law:

$$u = u_{pd} + u_{rm} - u_{ad}$$

- Tracking error dynamics, ( $e = x_{rm} - x$ )

$$\dot{e} = (A - BK)e + B(u_{ad} - \Delta)$$

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# Approach

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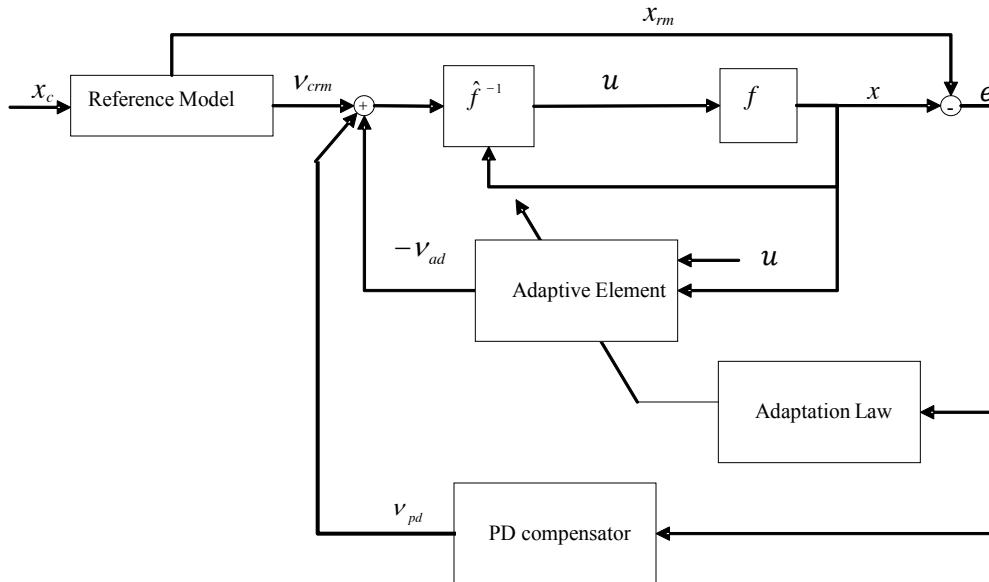
- Design a pseudo control  $\nu \in \Re^n$  such that  $x \rightarrow x_{rm}$
- If plant model were known and invertible, then we can simply set  $u = f^{-1}(x, \nu)$
- However, this is usually not the case, so **choose** an inversion model  $\hat{f}$  and let  $u = \hat{f}^{-1}(x, \nu)$

## Assumption

The approximate inversion model is continuous, and invertible w.r.t. u.  
I.e. the operator  $\hat{f}^{-1}: \Re^{2n} \rightarrow \Re^m$  exists and assigns for every unique  $(x, \nu) \in \Re^{2n}$  a unique  $u \in \Re^m$

- Combined control action:  $\nu = -Ke + \dot{x}_{rm} - \nu_{ad}$
-

# Tracking Error Dynamics



$$\nu = \nu_{pd} + \nu_{rm} - \nu_{ad}$$

■ Tracking error dynamics:

$$\dot{e} = Ae + B(\nu_{ad} - \Delta)$$

# Choice of adaptive element

## Structured Uncertainty

Given that there exists a constant matrix  $W^*$  and known basis functions  $\Phi(x, u)$  such that

$$\Delta(x, u) = W^{*T} \Phi(x, u)$$

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Given  $\Delta(x, u)$  is continuous and defined over a compact set, then :

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# Single Hidden Layer Neural Network

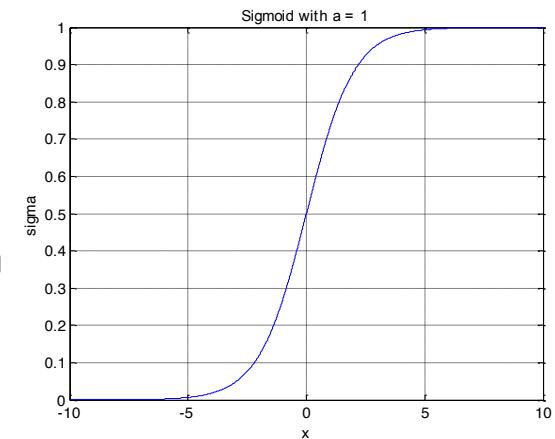
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- Single Hidden Layer (SHL) feedforward NN are universal approximators

$$v_{ad} = W^T(t)\sigma(V^T \bar{x})$$

- $\bar{x} = [b_a \ x]$ , where  $b_a$  is the input bias (constant)

$$\sigma = \begin{bmatrix} b_w \\ 1 \\ \frac{1}{1+e^{a_1 z_1}} \\ \vdots \\ 1 \\ \frac{1}{1+e^{a_{n_2} z_{n_2}}} \end{bmatrix} \in \Re^{n_2+1}, \text{ sigmoidal activation function}$$



$$V = \begin{bmatrix} \theta_{1,1} & \dots & \theta_{1,n_2} \\ v_{1,1} & \dots & \theta_{1,n_2} \\ \vdots & \ddots & \vdots \\ v_{n_1,1} & \dots & \theta_{n_1,n_2} \end{bmatrix} \in \Re^{(n_1+1) \times n_2} \quad W = \begin{bmatrix} \theta_{1,1} & \dots & \theta_{1,n_2} \\ w_{1,1} & \dots & w_{1,n_2} \\ \vdots & \ddots & \vdots \\ w_{n_2,1} & \dots & w_{n_2,n_3} \end{bmatrix} \in \Re^{(n_2+1) \times n_3}$$


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# Universal approximation property

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- Given sufficient number of hidden layer neurons ( $n_2$ ), and a corresponding set of ideal weights ( $W^*, V^*$ ) there exists  $\bar{\epsilon}$  such that

$$\bar{\epsilon} = \sup_{\bar{x} \in D} ||W^{*T} \sigma(V^{*T} \bar{x}) - \Delta(z)||$$

- Ideally we would like to update  $W, V$  such that they approach a compact neighborhood of  $W^*, V^*$
  - Direct adaptive control is happy with just updating  $W, V$  such that tracking error  $e$  stays bounded
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# NN training law

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- The “Classical” Error backpropagation based learning Law:

$$\dot{W} = -(\sigma - \sigma' V^T \bar{x}) r^T \Gamma_w$$

$$\dot{V} = -\Gamma_V \bar{x} r W^T \sigma'$$

where  $r^T = e^T P B$

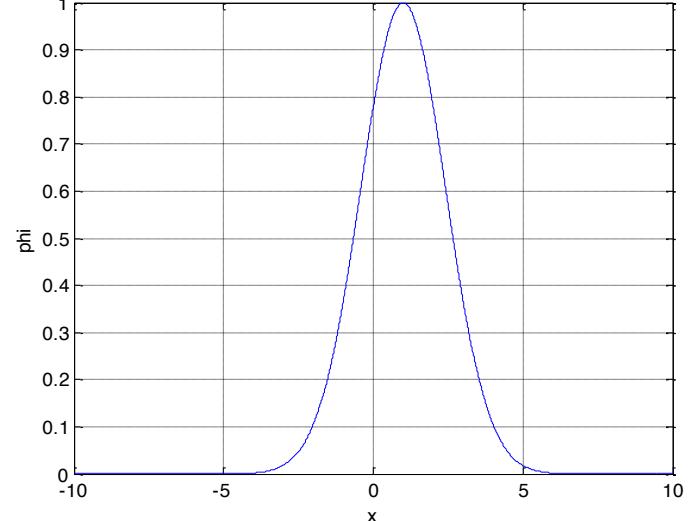
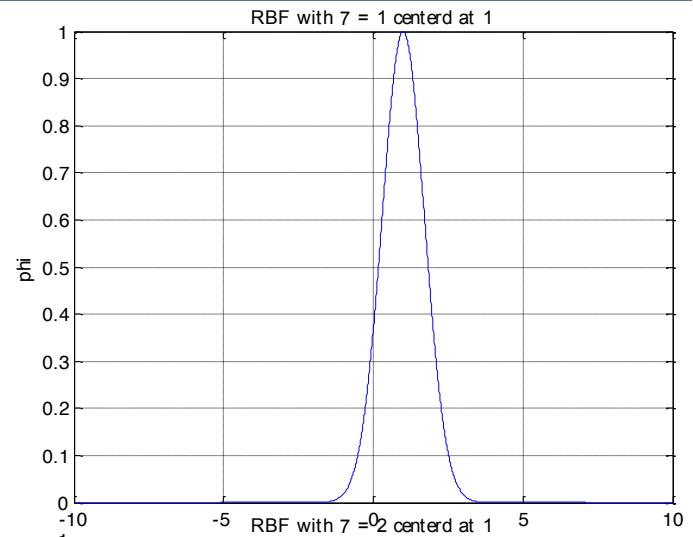
$$\sigma' = diag \left( \sigma(V^T \bar{x}) \left( I - diag \left( \sigma(V^T \bar{x}) \right) \right) \right)$$

- This adaptive law guarantees uniform ultimate boundedness of  $(e, \tilde{W})$  (Lewis et al.)
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# Radial Basis Function NN

- Radial Basis Functions (RBFs) are Gaussian Kernels
- Select  $n_2$  centers  $x_{c_j}$
- Select a width parameter
- Add a bias term, then  $\Phi(\bar{x}) \in \Re^{n_2+1}$

$$\Phi(\bar{x}) = \begin{bmatrix} b_w \\ e^{\frac{-||x_{c_1} - \bar{x}||}{\mu}} \\ \vdots \\ e^{\frac{-||x_{c_{n_2}} - \bar{x}||}{\mu}} \end{bmatrix}$$



# Universal Approximation with RBFs

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- Given fixed number of RBFs with a fixed width  $\mu$  there exists an ideal set of weights  $W^*$  such that

$$\bar{\epsilon} = \sup_{\bar{x} \in D} ||W^{*T} \Phi(\bar{x}) - \Delta(z)||$$

- $\bar{\epsilon}$  can be made arbitrarily small given sufficient number of RBFs
  - RBF NN  $v_{ad} = W^T(t) \Phi(\bar{x})$
  - Ideally, we would like  $W(t) \rightarrow W^*$
  - Traditionally, adaptive control is happy with keeping  $e$  bounded
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# RBF adaptive law

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- The following adaptive law guarantees that the tracking error stays bounded in a compact neighborhood

$$\dot{W} = -\Gamma\Phi(\bar{x})e^T PB$$

- Can use  $\sigma$  – mod, or  $e$  – mod to guarantee boundedness in presence of noise:

$$\dot{W} = -\Gamma\Phi(\bar{x})e^T PB - \kappa W$$

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# Which NN to choose?

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## ■ Benefits of SHL NN:

- Don't need to select centers
- More general parameterization

## ■ Issues:

- Nonlinearly parameterized, which makes analysis hard
- Rank-1 updates do not leverage the power of this NN

## ■ Benefits of RBF NN

- Linearly parameterized, relatively straight forward to analyze
- Lends to the theory of Gaussian Kernels and Reproducing Kernel Hilbert Spaces

## ■ Issues:

- How to select the centers (see Concurrent Learning Talk)
  - How many RBFs to use?
  - Can run into issues with bias estimation if the centers are far away
-

# Example: Inverted pendulum (SHL NN)

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- A nonlinear system which resembles an inverted pendulum

$$\ddot{x} = \delta + \sin(x) - |\dot{x}| \dot{x} + 0.5 e^{x \dot{x}}$$

- Approximate inversion model:  $v = \delta$

- Model error  $\Delta = [1 \quad -1 \quad 0.5] \begin{bmatrix} \sin(x) \\ |\dot{x}| \dot{x} \\ e^{x \dot{x}} \end{bmatrix}$

- Second order reference model
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# Example Inverted Pendulum

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Software:NN\_InvertedPendulum\_simple

Try the following

■ Control without NN: set

- gammaW=0; (line 61)
- gammaV=0; (line 62)

# Wing Rock dynamics(RBF NN)

- Highly swept-back aircraft are susceptible to Wing Rock: lightly damped oscillations
- $\phi$ : roll angle,  $p$  roll rate,  $\delta_a$  aileron

## A model for Wing Rock dynamics (Monahemi 96)

$$\begin{aligned}\dot{\phi} &= p \\ p &= \delta_a + \Delta(\phi, p)\end{aligned}$$

- Inversion model:  $v = \delta$
- Task: track roll commands in presence of wing rock dynamics:

$$\Delta(\phi, p) = 0.8 + 0.23\phi + 0.69p - 0.62|\phi| + 0.01|p|p + 0.02p^3$$

- Second order reference model used

# Example wingrock with RBF

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Software: wingrock\_rbf\_simple

Things to try

- Turn off adaptive control by setting gammaW=0
  - Add sigma mod: by setting kappa=0.1
  - Add e-mod by setting zeta=0.1
  - What effect does the bias term ( $W^*(1)$ ) have  
(this simulates trim)
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# Issues

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- Boundedness of  $\tilde{W}$  in presence of noise etc
  - Transient response
  - Actuator saturation
  - In case of RBFs, how do we distribute the centers?
    - See paper “*A Reproducing Kernel Hilbert Space Approach to Adaptive Control*”, Kingravi, Chowdhary, Vela, Johnson, *CDC 2011*
  - In general, traditional adaptive laws don’t guarantee that the weights approach their ideal values (as dictated by the universal approximation property)
  - Persistency of excitation is needed to guarantee this
-