

Homework #9

Solutions

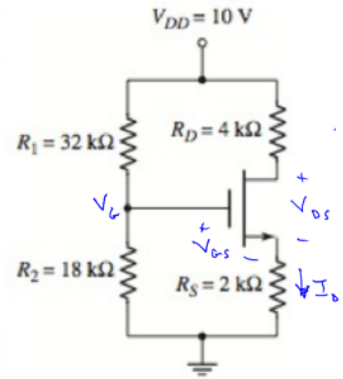
MOSFET Circuits: DC Biasing and Common Source Amplifier – *100 points*

DUE @ Beginning of Class: Thursday, November 16

- 1) E-Book, problem 3.26 (*10 points*)
- 2) E-Book, problem D3.28 (find R_1 and R_2) (*10 points*)
- 3) E-Book, problem 3.29 (*20 points*)
- 4) E-Book, problem 3.40 (*10 points*)
- 5) E-Book, problem 4.8 (*10 points*)
- 6) E-Book, problem 4.15 (*12 points*)
- 7) E-Book, problem 4.18 (*10 points*)
- 8) E-Book, problem D4.26 (*18 points*)

1) E-Book, problem 3.26 (10 points)

3.26 In the circuit in Figure P3.26, the transistor parameters are $V_{TN} = 0.8 \text{ V}$ and $K_n = 0.5 \text{ mA/V}^2$. Calculate V_{GS} , I_D , and V_{DS} .



$$V_G = \left(\frac{R_2}{R_1 + R_2} \right) V_{DD} = \left(\frac{18 \text{ k}\Omega}{18 \text{ k}\Omega + 32 \text{ k}\Omega} \right) (10 \text{ V}) = 3.6 \text{ V}$$

→ assume biased in sat.

$$I_D = \frac{V_S}{R_S} = \frac{V_G - V_{GS}}{R_S} = K_n (V_{GS} - V_{TN})^2$$

$$V_G - V_{GS} = R_S K_n (V_{GS} - V_{TN})^2$$

$$3.6 \text{ V} - V_{GS} = (2 \text{ k}\Omega) (0.5 \text{ mA/V}^2) (V_{GS} - 0.8 \text{ V})^2 \quad \text{Figure P3.26}$$

$$V_{GS}^2 - 0.6 V_{GS} - 2.96 = 0$$

Solve quadratic: $V_{GS} = 2.046 \text{ V}$ 3

$$I_D = \frac{V_G - V_{GS}}{R_S} = \frac{3.6 \text{ V} - 2.046 \text{ V}}{2 \text{ k}\Omega} = 0.777 \text{ mA} \quad 3$$

KVL gives:

$$V_{DS} = V_{DD} - I_D (R_D + R_S) = 10 \text{ V} - (0.777 \text{ mA}) (4 \text{ k}\Omega + 2 \text{ k}\Omega) = 5.34 \text{ V} \quad 2$$

→ is $V_{DS} > V_{DS}(\text{sat}) = V_{GS} - V_{TN} = 2.046 \text{ V} - 0.8 \text{ V}$? YES ✓

2) E-Book, problem D3.28 (find R_1 and R_2) (10 points)

D3.28 The transistor in Figure P3.28 has parameters $V_{TN} = 0.4 \text{ V}$, $k'_n = 120 \mu\text{A/V}^2$, and $W/L = 80$. Design the circuit such that $I_Q = 0.8 \text{ mA}$ and $R_{in} = 200 \text{ k}\Omega$.

assuming operation in saturation:

$$I_a = \frac{k'_n}{2} \left(\frac{W}{L} \right) (V_{GS} - V_{TN})^2$$

$$0.8 \text{ mA} = \frac{0.12 \text{ mA/V}^2}{2} (80) (V_{GS} - 0.4 \text{ V})^2$$

$$\Rightarrow V_{GS} = 0.808 \text{ V}$$

voltage divider:

$$V_{GS} = \frac{R_2}{R_1 + R_2} V_{DD} = \frac{1}{R_1} R_{in} V_{DD}$$

$$0.808 \text{ V} = \frac{1}{R_1} (200 \text{ k}\Omega) (1.8 \text{ V}) \Rightarrow R_1 = 445 \text{ k}\Omega$$

$$R_{in} = R_1 \parallel R_2 = 200 \text{ k}\Omega = \frac{(445 \text{ k}\Omega) R_2}{445 \text{ k}\Omega + R_2} \Rightarrow R_2 = 363 \text{ k}\Omega$$

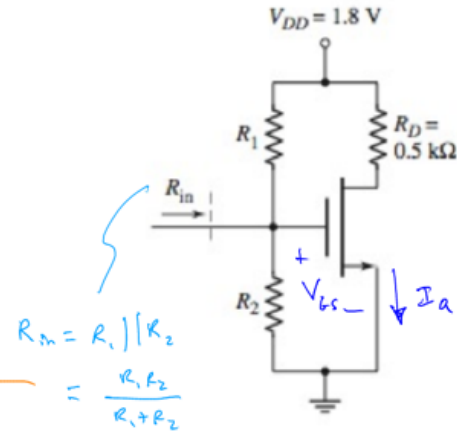


Figure P3.28

3) E-Book, problem 3.29 (20 points)

3.29 The transistor in the circuit in Figure P3.29 has parameters $V_{TP} = -0.8 \text{ V}$ and $K_p = 0.20 \text{ mA/V}^2$. Sketch the load line and plot the Q -point for (a) $V_{DD} = 3.5 \text{ V}$, $R_D = 1.2 \text{ k}\Omega$ and (b) $V_{DD} = 5 \text{ V}$, $R_D = 4 \text{ k}\Omega$. What is the operating bias region for each condition?

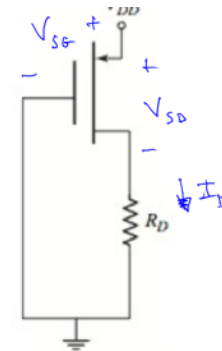
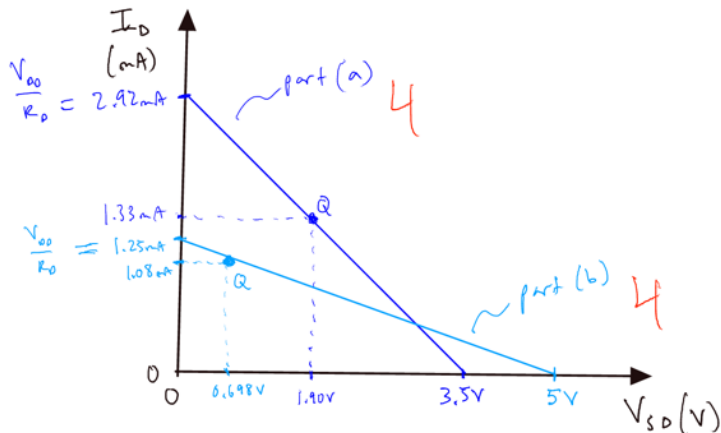


Figure P3.29

a) $V_{SG} = V_{DD} = 3.5 \text{ V}$, $V_{SD}(\text{sat}) = V_{SG} + V_{TP} = 3.5 \text{ V} - 0.8 \text{ V} = 2.7 \text{ V}$

If biased in sat: $I_D = K_p (V_{SG} + V_{TP})^2 = (0.2 \text{ mA/V}^2)(2.7 \text{ V})^2 = 1.46 \text{ mA}$

$V_{SD} = V_{DD} - I_D R_D = 3.5 \text{ V} - (1.46 \text{ mA})(1.2 \text{ k}\Omega) = 1.75 \text{ V} < V_{SD}(\text{sat})$

\Rightarrow Not in sat.

Non-sat:

$V_{DD} = V_{SD} + I_D R_D = V_{SD} + K_p R_D [2(V_{SG} + V_{TP})V_{SD} - V_{SD}^2]$

$3.5 \text{ V} = V_{SD} + 1.296 V_{SD} - 0.24 V_{SD}^2$

Solve quadratic: $V_{SD} = 1.90 \text{ V}$

$I_D = \frac{V_{DD} - V_{SD}}{R_D} = \frac{3.5 \text{ V} - 1.90 \text{ V}}{1.2 \text{ k}\Omega} = 1.33 \text{ mA}$

operating point 2

Linear or non-sat. region

2

b) $V_{SG} = V_{DD} = 5 \text{ V}$, $V_{SD}(\text{sat}) = 5 \text{ V} - 0.8 \text{ V} = 4.2 \text{ V}$

assume sat: $I_D = (0.2) [4.2 \text{ V}]^2 = 3.53 \text{ mA}$ would result in $V_{SD} < 0 \Rightarrow$ non-sat. region

non-sat:

$V_{DD} = V_{SD} + I_D R_D = V_{SD} + K_p R_D [2(V_{SG} + V_{TP})V_{SD} - V_{SD}^2]$

and

$I_D = \frac{V_{DD} - V_{SD}}{R_D}$

Same approach as in part a) gives:

$V_{SD} = 0.698 \text{ V}$

$I_D = 1.08 \text{ mA}$

operating point 2

2

4) E-Book, problem 3.40 (10 points)

3.40 The PMOS transistor in Figure P3.40 has parameters $\tilde{V}_{TP} = -0.7\text{ V}$, $k'_p = 50\text{ }\mu\text{A/V}^2$, $L = 0.8\text{ }\mu\text{m}$, and $\lambda = 0$. Determine the values of W and R such that $I_D = 0.1\text{ mA}$ and $V_{SD} = 2.5\text{ V}$.

$$I_o = 0.1\text{ mA} = \frac{V_{DD} - V_{SD}}{R} = \frac{9\text{ V} - 2.5\text{ V}}{R}$$

$$\Rightarrow R = 65\text{ k}\Omega \quad 2$$

assume sat.

$$I_o = \frac{k'_p}{2} \left(\frac{W}{L} \right) (V_{SG} + V_{TP})^2$$

$$0.1\text{ mA} = \frac{0.05\text{ mA/V}^2}{2} \left(\frac{W}{L} \right) (2.5\text{ V} - 0.7\text{ V})^2$$

$$\Rightarrow \left(\frac{W}{L} \right) = 1.235 = \frac{W}{0.8\text{ }\mu\text{m}} \Rightarrow W = 0.988\text{ }\mu\text{m} \quad 6$$

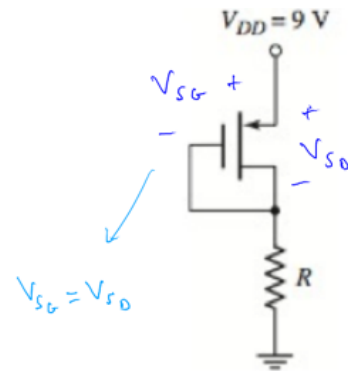


Figure P3.40

5) E-Book, problem 4.8 (10 points)

4.8 The parameters of the circuit in Figure 4.1 are $V_{DD} = 3.3\text{ V}$ and $R_D = 5\text{ k}\Omega$. The transistor parameters are $k'_n = 100\text{ }\mu\text{A/V}^2$, $W/L = 40$, $V_{TN} = 0.4\text{ V}$, and $\lambda = 0.025\text{ V}^{-1}$. (a) Find I_{DQ} and V_{GSQ} such that $V_{DSQ} = 1.5\text{ V}$. (b) Determine the small-signal voltage gain.

a) $V_{DD} = I_{DQ} R_D + V_{DSQ}$ (voltage loop)

$$3.3\text{ V} = I_{DQ} (5\text{ k}\Omega) + 1.5\text{ V} \Rightarrow I_{DQ} = 0.36\text{ mA}$$

$$I_{DQ} = \frac{k'_n}{2} \left(\frac{W}{L} \right) (V_{GSQ} - V_{TN})^2$$

$$0.36\text{ mA} = \frac{0.1\text{ mA/V}^2}{2} (40) (V_{GSQ} - 0.4\text{ V})^2 \Rightarrow V_{GSQ} = 0.824\text{ V}$$

b) $g_m = 2 \sqrt{K_n I_{DQ}} = 2 \sqrt{\frac{k'_n}{2} \left(\frac{W}{L} \right) I_{DQ}} = 2 \sqrt{\frac{0.1\text{ mA/V}^2}{2} (40) (0.36\text{ mA})} = 1.697\text{ mA/V}$

$$r_o = \frac{1}{\lambda I_{DQ}} = \frac{1}{(0.025\text{ V}^{-1})(0.36\text{ mA})} = 111\text{ k}\Omega$$

$$A_v = -g_m (r_o \parallel R_D) = - (1.697\text{ mA/V}) (111\text{ k}\Omega \parallel 5\text{ k}\Omega) = -8.12$$

6) E-Book, problem 4.15 (12 points)

4.15 For the NMOS common-source amplifier in Figure P4.15, the transistor parameters are: $V_{TN} = 0.8 \text{ V}$, $K_n = 1 \text{ mA/V}^2$, and $\lambda = 0$. The circuit parameters are $V_{DD} = 5 \text{ V}$, $R_S = 1 \text{ k}\Omega$, $R_D = 4 \text{ k}\Omega$, $R_1 = 225 \text{ k}\Omega$, and $R_2 = 175 \text{ k}\Omega$. (a) Calculate the quiescent values I_{DQ} and V_{DSQ} . (b) Determine the small-signal voltage gain for $R_L = \infty$. (c) Determine the value of R_L that will reduce the small-signal voltage gain to 75 percent of the value found in part (b).

a) Voltage divider:

$$V_G = \left(\frac{R_2}{R_1 + R_2} \right) V_{DD} = \left(\frac{175 \text{ k}\Omega}{175 \text{ k}\Omega + 225 \text{ k}\Omega} \right) (5 \text{ V}) = 2.19 \text{ V}$$

$$V_G = V_{GS} + I_D R_S = V_{GS} + K_n R_S (V_{GS} - V_{TN})^2$$

$$2.19 \text{ V} = V_{GS} + (1 \text{ mA/V}^2)(1 \text{ k}\Omega)(V_{GS} - 0.8 \text{ V})^2$$

$$\Rightarrow V_{GS} = 1.58 \text{ V}$$

$$I_{DQ} = K_n (V_{GS} - V_{TN})^2 = (1 \text{ mA/V}^2)(1.58 \text{ V} - 0.8 \text{ V})^2 = 0.608 \text{ mA} \quad 2$$

$$V_{DSQ} = V_{DD} - I_{DQ}(R_S + R_D) = 5 \text{ V} - (0.608 \text{ mA})(1 \text{ k}\Omega + 4 \text{ k}\Omega) = 1.96 \text{ V} \quad 2$$

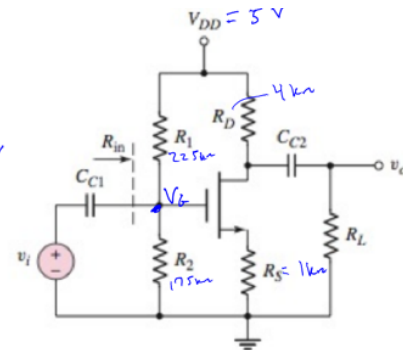


Figure P4.15

b) with $R_L = \infty$, then: $A_v = \frac{-g_m R_D}{1 + g_m R_S}$ (from ps-605, Ex. 4.5)

$$g_m = 2 \sqrt{K_n I_{DQ}} = 2 \sqrt{(1 \text{ mA/V}^2)(0.608 \text{ mA})} = 1.56 \text{ mA/V}$$

$$A_v = \frac{-(1.56 \text{ mA/V})(4 \text{ k}\Omega)}{1 + (1.56 \text{ mA/V})(1 \text{ k}\Omega)} = -2.44 \quad 4$$

c) If $R_L \neq \infty$, then $A_v = A_{v0} = \frac{-g_m R_D || R_L}{1 + g_m R_S} = \frac{-(1.56 \text{ mA/V}) R_D || R_L}{1 + (1.56 \text{ mA/V})(1 \text{ k}\Omega)} = -0.609(R_D || R_L)$

$$75\% \text{ of } -2.44: -(0.75)(2.44) = -0.609 R_D || R_L$$

$$\Rightarrow R_L = 12 \text{ k}\Omega \quad 4$$

7) E-Book, problem 4.18 (10 points)

4.18 The ac equivalent circuit of a common-source amplifier is shown in Figure P4.18. The small-signal parameters of the transistor are $g_m = 2 \text{ mA/V}$ and $r_o = \infty$. (a) The voltage gain is found to be $A_v = V_o/V_i = -15$ with $R_S = 0$. What is the value of R_D ? (b) A source resistor R_S is inserted. Assuming the transistor parameters do not change, what is the value of R_S if the voltage gain is reduced to $A_v = -5$.

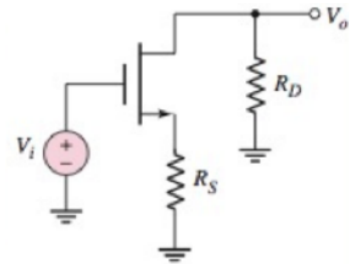


Figure P4.18

$$\begin{aligned} \text{a) } A_v &= -g_m R_D \\ -15 &= -(2 \text{ mA/V}) R_D \\ \Rightarrow R_D &= 7.5 \text{ k}\Omega \quad 2 \end{aligned}$$

$$\begin{aligned} \text{b) with } R_S: \\ A_v &= \frac{-g_m R_D}{1 + g_m R_S} \\ -5 &= \frac{-(2 \text{ mA/V})(7.5 \text{ k}\Omega)}{1 + (2 \text{ mA/V}) R_S} \Rightarrow R_S = 1 \text{ k}\Omega \quad 4 \end{aligned}$$

8) E-Book, problem D4.26 (18 points)

*D4.26 Design the common-source circuit in Figure P4.26 using an n-channel MOSFET with $\lambda = 0$. The quiescent values are to be $I_{DQ} = 6 \text{ mA}$, $V_{GSQ} = 2.8 \text{ V}$, and $V_{DSQ} = 10 \text{ V}$. The transconductance is $g_m = 2.2 \text{ mA/V}$. Let $R_L = 1 \text{ k}\Omega$, $A_v = -1$, and $R_{in} = 100 \text{ k}\Omega$. Find R_1 , R_2 , R_S , R_D , K_n , and V_{TN} .

$$I_{DQ} = K_n (V_{GSQ} - V_{TN})^2$$

$$g_m = 2 \sqrt{K_n I_{DQ}}$$

$$2.2 \text{ mA/V} = 2 \sqrt{K_n (6 \text{ mA})} \Rightarrow K_n = 0.202 \text{ mA/V}^2$$

$$6 \text{ mA} = (0.202 \text{ mA/V}^2) (2.8 \text{ V} - V_{TN})^2 \Rightarrow V_{TN} = -2.65 \text{ V}$$

$$V_{DSQ} = V_{DD} - I_{DQ} (R_S + R_D)$$

$$\hookrightarrow R_S + R_D = \frac{18 \text{ V} - 10 \text{ V}}{6 \text{ mA}} = 1.33 \text{ k}\Omega \Rightarrow R_S = 1.33 \text{ k}\Omega - R_D$$

$$A_v = \frac{g_m (R_D \parallel R_L)}{1 + g_m R_S} \rightarrow -1 = \frac{-(2.2 \text{ mA/V}) \left(\frac{R_D (1 \text{ k}\Omega)}{R_D + 1 \text{ k}\Omega} \right)}{1 + (2.2 \text{ mA/V}) (1.33 \text{ k}\Omega - R_D)} \Rightarrow R_D = 1.23 \text{ k}\Omega$$

$$R_S = 0.10 \text{ k}\Omega$$

$$V_G = V_{GS} + V_S = 2.8 \text{ V} + (6 \text{ mA}) (0.10 \text{ k}\Omega) = 3.4 \text{ V}$$

$$V_G = \left(\frac{R_2}{R_1 + R_2} \right) V_{DD} = \frac{1}{R_1} R_{in} V_{DD} = \frac{1}{R_1} (100 \text{ k}\Omega) (18 \text{ V}) = 3.4 \text{ V} \Rightarrow R_1 = 529 \text{ k}\Omega$$

$$R_{in} = 100 \text{ k}\Omega = R_1 \parallel R_2 = (529 \text{ k}\Omega) \parallel R_2 \Rightarrow R_2 = 123 \text{ k}\Omega$$

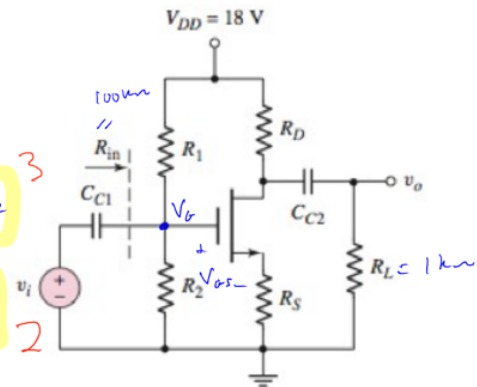


Figure P4.26