



SAFARI

A Simulation of

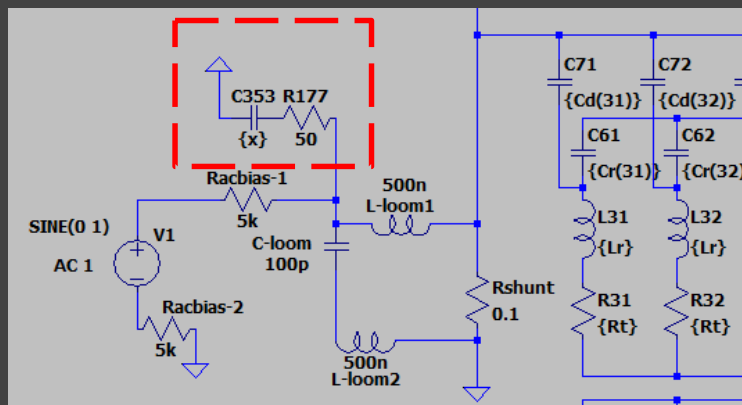
Out of Band Resonances (OBR) of the SAFARI FDM - Frequency Dependent(R,L) Twisted Pairs

SRON

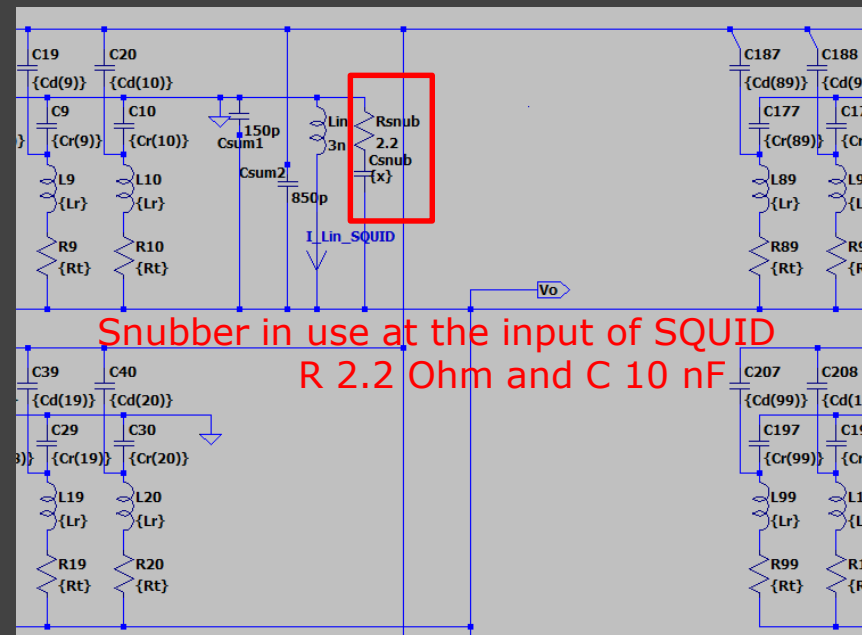
Amin Aminaei, 6 April 2020

REMINDER

Simulation of SAFARI FDM blocks up to the input of the 1st SQUID

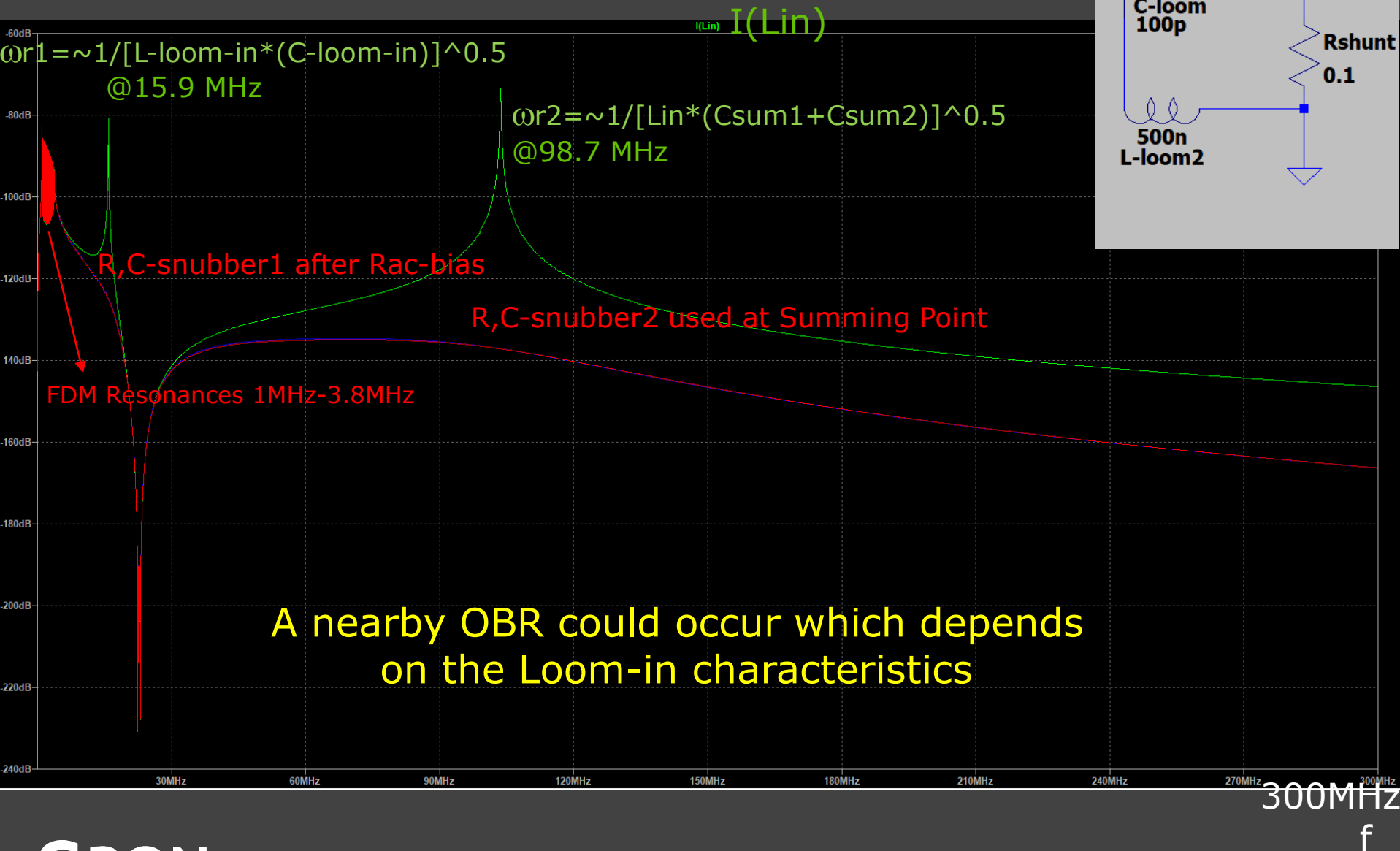


Snubber-1 (Theory) after Rac-bias
Optimal values, R 50 Ohm and C 10 nF

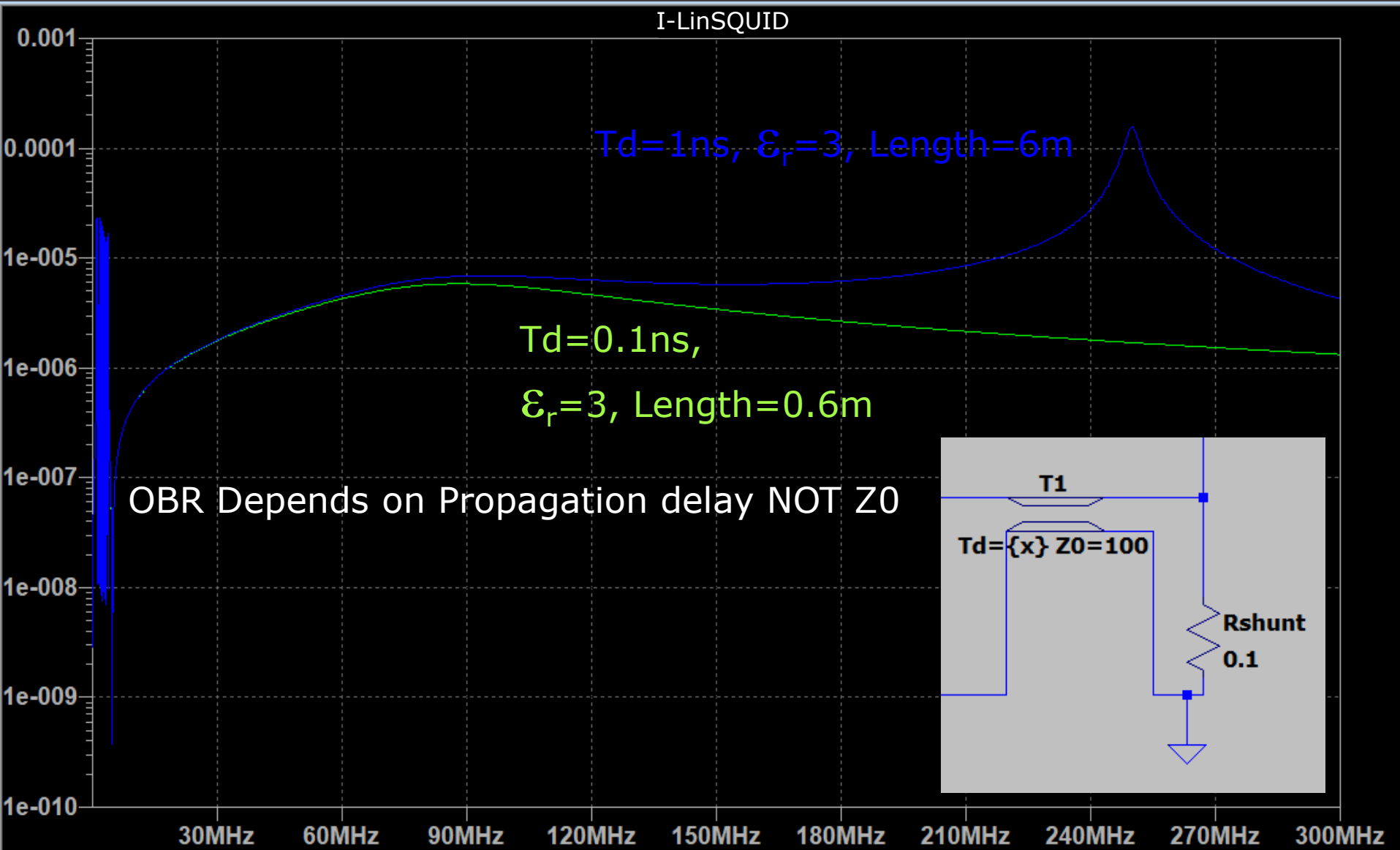


Snubber in use at the input of SQUID
R 2.2 Ohm and C 10 nF

Simulation of Input Loom with L,C

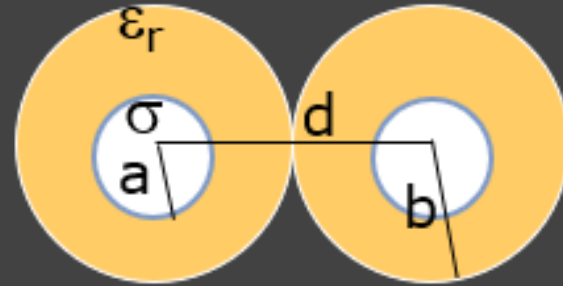


Simulation of Input Loom as a Lossless Transmission Line



Network model of twisted pairs, nominal values

SS Stainless Steel σ 1.45E6
diameter $2a=2 \times 100 \mu\text{m}$ ($a=50 \mu\text{m}$)
total wire = 300 μm
insulation 100.0 μm , each side
distance between cable centres, $d=300 \mu\text{m}$
permittivity of inner dielectric and outer dielectric permittivity(3)

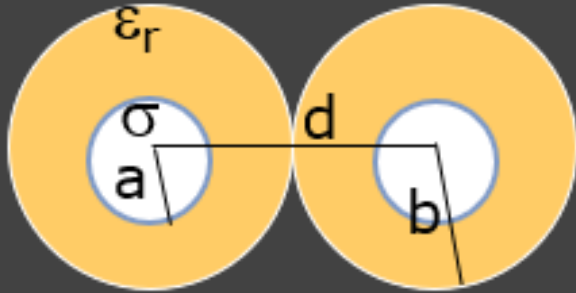


SAFARI2019_07_harness_EXCEL_v07-A.A..xlsx - Excel

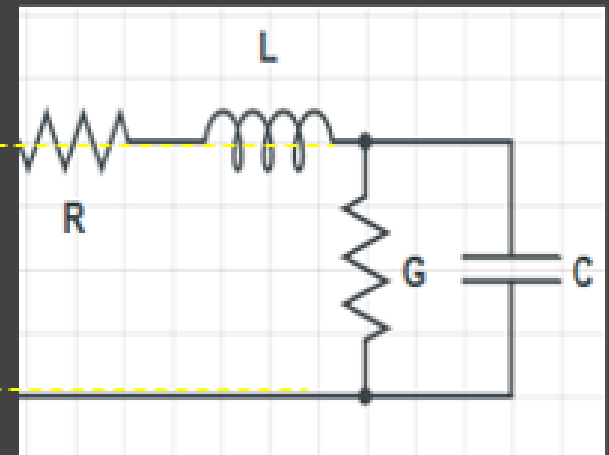
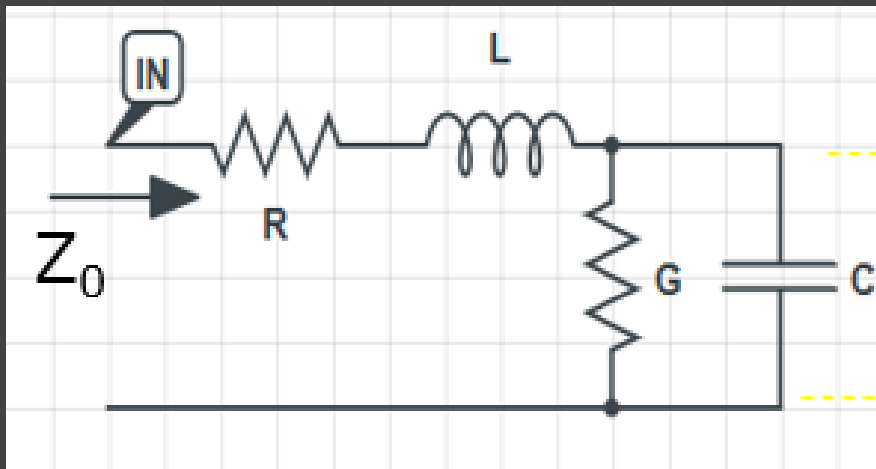
Name	Type	Shielded	Wires	Material	AWG	diameter
FE_SQUID_heater	Twisted pair	no	2	ss	38	100,70
AMP_SQUID_heater	Twisted pair	no	2	ss	38	100,70
AreaCond ss	insulation	wiretot	AreaIns	signal ID		
0,02	100,00	300,70	0,13	601,40		
0,02	100,00	300,70	0,13	601,40		

Model Schematics

--→ Calculated and Implemented in LT-Spice

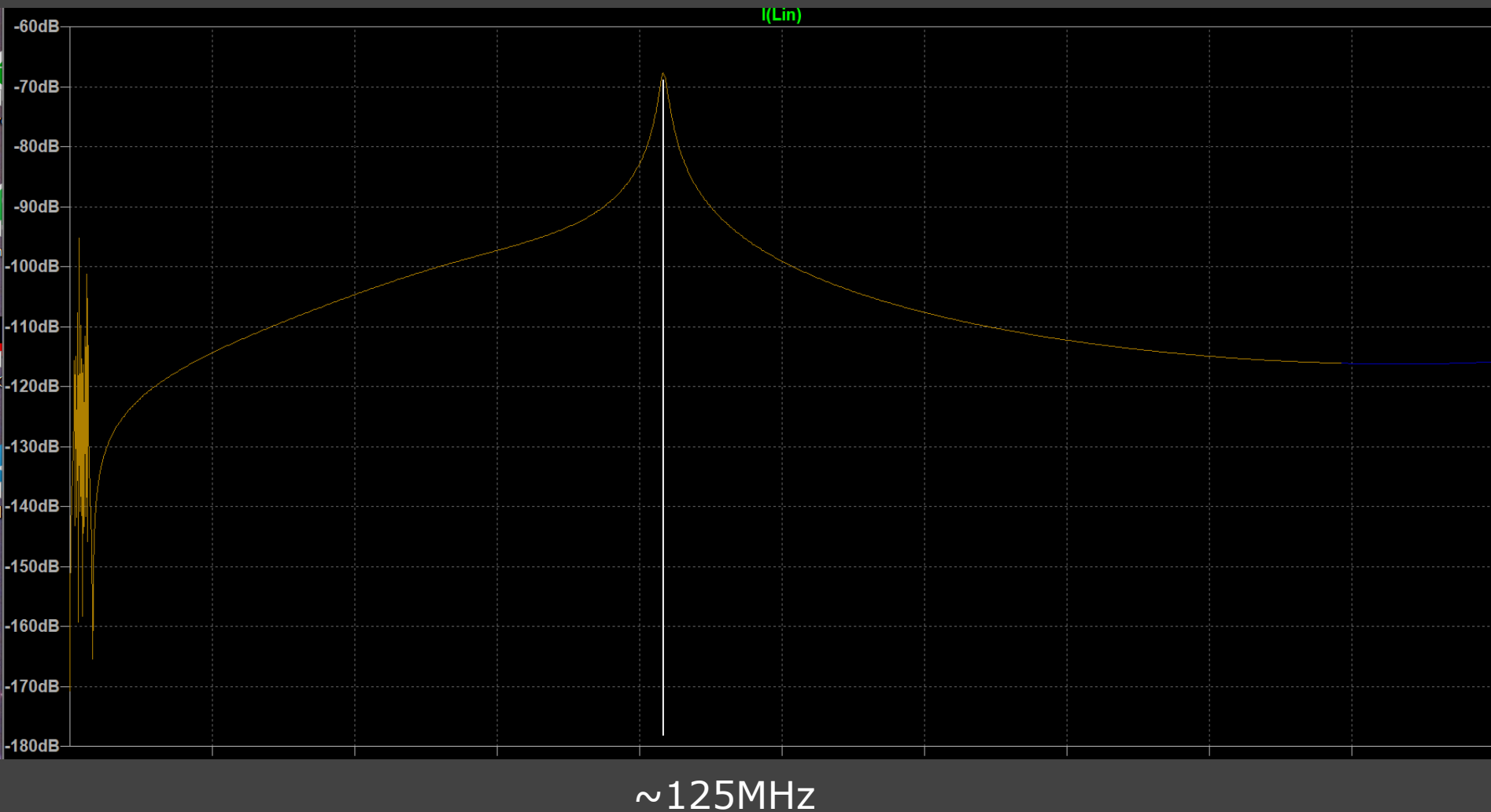


$$Z_0 = \sqrt{\frac{Z}{Y}} = \sqrt{\frac{R(\omega) + j\omega \cdot L(\omega)}{G(\omega) + j\omega \cdot C(\omega)}}$$



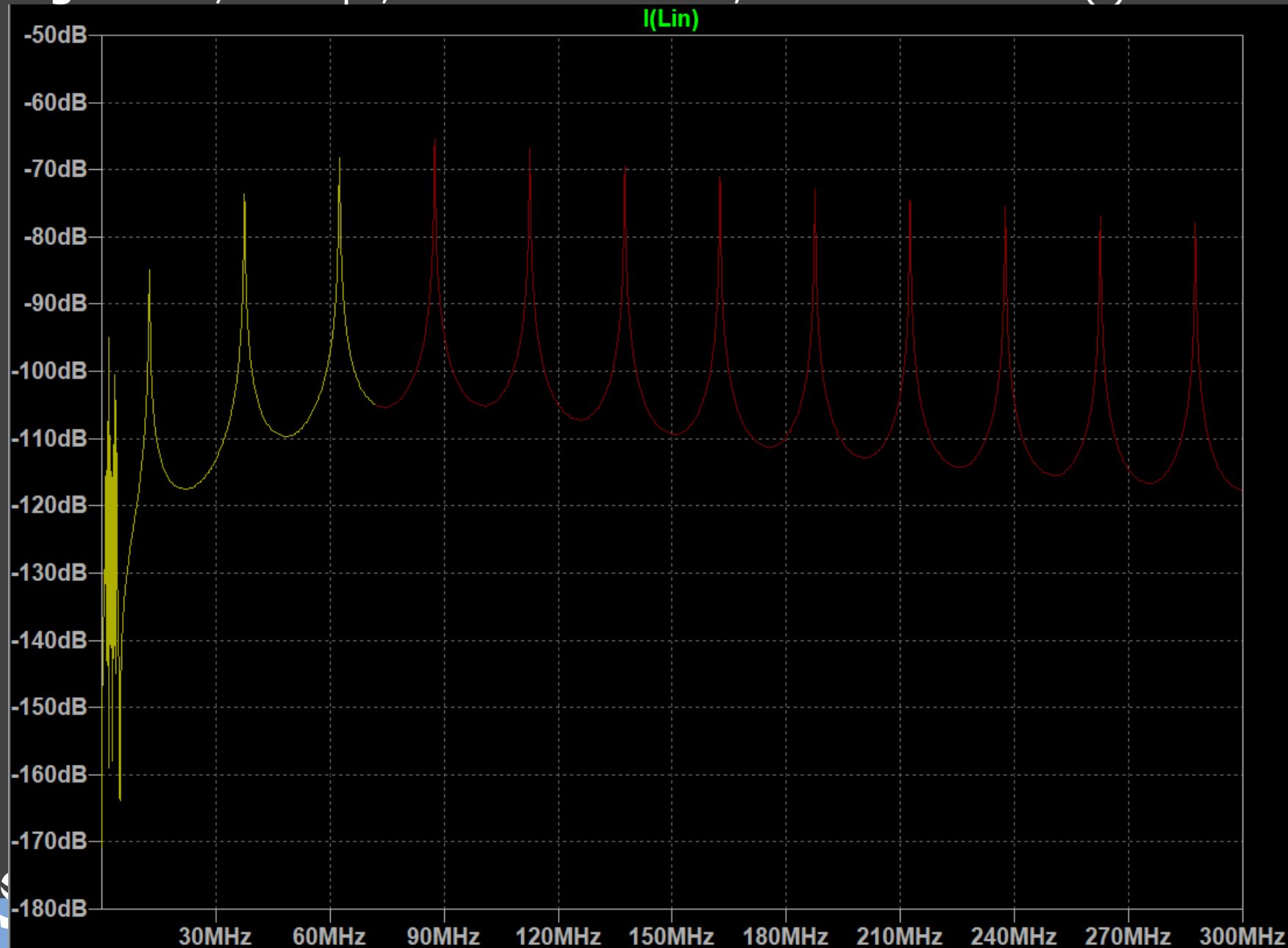
Typical frequency dependent micro-twisted pair, before R_{shunt}

Length=60cm, $C=34\text{pF}$, $R=0.0065$. $f^{0.5}$, $L=3.24 \cdot 10^{-7} + 0.001 \cdot (f)^{-0.5}$



Typical frequency dependent micro-twisted pair, before R_{shunt}

Length=6m, $C=34\text{pF}$, $R=0.0065$. $f^{0.5}$, $L=3.24\text{E-}7+.001.(f)^{-0.5}$



Typical frequency dependent micro-twisted pair, before R_{shunt}

Length=10cm, $C=34\text{pF}$, $R=0.0065$. $f^{0.5}$, $L=3.24\text{E-}7+.001.(f)^{-0.5}$

