**Vibration soil isolation using a 3-D frequency domain BEM: GPGPU implementation.**

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**Abstract.** This paper presents a Boundary Element formulation for dynamic response analysis … last text to write

**Keywords:** Boundary Element Method, GPGPU, High Performance Computing.

1. **INTRODUCTION**

The idea of mitigating vibrations transmitted by the ground in surrounding area of machine tools, trains or cars traffic and even mine blasting has long been studied. Vibration isolation may be accomplished by barriers which diffract the surface waves radiated from the vibration source and somehow reduce their amplitude. Among other possibilities, these barriers may be obtained by trenches (open or filled), subject addressed in this article.

As attested by (Beskos, Dasgupta, and Vardoulakis 1986), the analytical treatment of vibration isolation by wave barriers in the framework of linear elastodynamic is based on the theory of wave diffraction. (Barkan 1962) was the first to report some investigations for studying the effectiveness of wave barriers, however it was apparent that the analytical treatment of 3D elastic wave diffraction problems was confined to very simple geometries and idealized conditions and that realistic problems involving complex geometries, such as vibration isolation, could only be solved numerically.

This article reports a numerical investigation of vibration isolation from grounded transmitted waves generated by a soil load. The numerical code is written in Computer Unified Device Architecture (CUDA), for NVidia Graphics Processing Units (GPUs). The proposed methodology employs the frequency domain Direct version of the Boundary Element Method (DBEM) for the solution of vibration isolation problems by trenches in a 3D context and can deal with trenches of any arbitrary shape, but it is applied here to rectangular ones.

A comparative study for the case of vibration isolation by an open trench was presented by (Klein, Antes, and Le Houédec 1997) where a numerical simulation based on 3D DBEM was compared to an analytical solution and posteriorly to measured data constructed for full-scale testing and an important conclusion was the trench depth normalized with respect to the Rayleigh wave length.

Analyses developed by (Andersen and Nielsen 2005) on the study about reduction of ground vibration by means of barriers or soil improvement along a railway track indicated that open trenches are more efficient than infilled trenches or soil stiffening even at low frequencies noticing that the direction of the load is of primordial importance.. They coupled, in the frequency domain, a finite element-boundary element model of the track and subsoil, adopting a formulation in the moving frame of reference following the vehicle.

From the point of view of ground vibrations induced by the machine tools operation, (Alzawi and Hesham El Naggar 2011) proposed an innovative approach to construct GeoFoam trench as a wave barrier. Authors conducted A full-scale field experimental study to investigate the protective performance of both open and in-filled trench as well as to examine the influences of wall geometry and location from the vibratory source on the isolation efficiency. It was shown that both open and GeoFoam barriers can effectively reduce the transmitted waves.

Inserting a ground model as a fully saturated poroelastic half-space governed by Biot’s dynamic poroelastic theory, (Cao et al. 2012) proposed a semi-analytical study to investigate the screening efficiency of trenches to moving-load induced ground vibrations. Comparing two models of half-space, saturated poroelastic and a single-phase elastic, to the moving load-induced ground vibration, it was found that the discrepancy of the screening efficiencies between both models becomes significant when the load speed approaches to the Rayleigh wave speed of the ground surface.

Considering several fixed observation points, (Zoccali, Cantisani, and Loprencipe 2015) studied the mutual influence between trenches length and in-filled material type to mitigate ground-vibrations induced by trains. The analysis was performed using a finite element model, both in time and frequency domain, which was calibrated through comparison with in-situ measurements.

In view of Graphics Processing Units (GPUs), (Labaki, Ferreira, and Mesquita 2011) implemented the Direct version of the Boundary Element Method (DBEM) on a complementary GPU-CPU system adopting constant elements for the solution of 2D potential problems in which the efficiency of the implemented strategies was investigated. In this paper three important steps of BEM were evaluated, and it was observed that the point from which the GPU outperforms the CPU is function of the arithmetic intensity of each problem. In all three cases, however, the graphics hardware has shown to be more numerically efficient than the CPU as increasing number of elements and internal points.

Combining BEM with the fast multipole method (FMM), the fast multipole BEM (FMBEM), (Wang et al. 2013) proposed an adaptive scheme to solve large scale problems. Since Multipole Expansions (ME), Moment- to-Local (M2L) translation, Local Expansions (LE), and the Near Field Direct Computation (NFDC) are level independent, they are suitable for parallel computing. Authors showed that in some examples they reached speedup of 16.2. Based on the idea of rigid body motion method (RBMM) for the FMBEM, (Wang et al. 2015), once more achieved reasonable speedup for 3D elasticity problems.

On the analysis of GPU´s performance, (Carrion, Mesquita, and Ansoni 2015) developed a strategy to evaluate the dynamic response of frame-foundation-soil system. In this article, authors presented a DBEM to synthesize the 3D dynamic compliance matrix of a rigid and massless foundation interacting with unbounded soil profiles. The foundation compliance matrix was coupled to a frame, modeled by the Finite Element Method (FEM) leading to the dynamic response of a coupled frame-foundation-soil system. The performance analysis was done by comparing two codes: one was exclusively developed in C language and the other one in CUDA C (Compute Unified Device Architecture). The level of speedup was achieved by implementing some functions in the frame model, i.e., on the FEM based code.

Developing a simple strategy, (Vater, Betcke, and Dilba 2017) demonstrated how GPU-accelerated BEM routines can be used to accelerate fast boundary element formulations based on Hierarchical Matrices (H -Matrices) with ACA (Adaptive Cross Approximation). Have computed the scattered high-frequency sound field of a submarine to demonstrate the increase in overall application performance from moving to a GPU-based ACA assembly, authors based their methodology on offloading the CPU assembly of elements during the ACA assembly onto a GPU device and to use threading strategies across ACA blocks to create sufficient workload for the GPU. The proposed GPU strategy was designed such that it can be implemented in existing code with minimal changes to the surrounding application structure.

1. **Boundary Element formulation**

The frequency domain equations of motion for a 3D linear elastic, homogeneous and isotropic continuum body, known as Navier equations, can be expressed in terms of the displacement components as:

(1)

where *λ* and *μ* are Lamè constants, *ρ* is the mass density, *ω* is the circular frequency, are the components of body force and ; the point *x* has Cartesian coordinates *x*, *y* and *z*.

The auxiliary state used in the BE standard formulation is assumed to be the Full-Space Green’s Functions or Fundamental Solution with displacement and traction kernels given by and respectively. Thus, the differential Eq. (1) can be transformed into the integral Eq. (2) (Eringen and Suhubi 1975).

(2)

Equation (2) considers zero body forces; and represent displacements and tractions respectively of problem being solved. The collocation point is *ξ* and the field point is *x*. The elements of tensor are called integration free terms.

The solution of Eq. (2) is accomplished numerically. For this purpose, the boundary *S* of the body is discretized into a series of boundary elements over which displacements and tractions are assumed to be constant. Thus, a system of linear algebraic equations is obtained and can be written in matrix form as:

(3)

where and are square influence matrices consisting of elemental surface integrals with integrands the tensors and respectively.

After the boundary conditions are applied, the system can be solved to obtain all the unknown boundary values and consequently an approximate solution to the boundary value problem is obtained. Once the solutions at the boundary are obtained, Eq. (2) can be used to find interior displacements. The interior stresses can be obtained as in (Brebbia and Dominguez, 1989):

(4)

where the kernels and are listed in (Gaul and Fiedler 1993).

1. **Numerical Implemetation**

When , these integrals are regulars and integration is accomplished by using standard Gauss Quadrature. However, when , these integrals become singular due to the and singularities of the tensors and respectively and their integration are discussed below.

For kernel, which presents weak singularity, a particular treatment is applied to become possible the use of standard Gauss Quadrature (Dominguez 1993). The idea is to divide the quadrilateral element in triangular sub-elements. Then, each triangular sub-element is treated as a quadrilateral one with two corners collapsed at the collocation point. With this methodology the Jacobian of the transformation presents the order at the collocation point. This fact cancels the singularity at the mentioned point, which has the order . This approach has been introduced by (Lachat 1975) and has been further developed by (Telles 1987).

About kernel, an alternative to evaluate its integration is based on the rigid body motion. Nevertheless, this argument is only applicable to static problems and bounded domains. Below are described the way to apply this concept in dynamic problems and unbounded domains.

* 1. **Regularization of the Dynamic Kernel**

As the dynamic and static kernels present the same order of singularity, it is possible to regularize the singular integral by subtracting and adding the static kernel from the dynamic one. This strategy can be represented as follow.

Assuming the convention for the indexes:

*sta* = static problem

*dyn* = dynamic problem

Subtracting and adding the 3D static kernel to Eq. (2) results:

(5)

Integrals in Eq. (5) containing the difference between the dynamic and static kernels are no longer singular and can be evaluated by standard Gauss Quadrature. The integration of the static singular kernel is evaluated based on the rigid body motion concept.

* 1. **Treatment of Unbounded Domains**

Now this rigid body argument is extended to deal with unbounded half-space problems with the so-called Enclosing Elements. As the half-space discretization surface must be truncated at some point, a bounded body is created by adding a fictitious enclosing boundary which is discretized by the enclosing elements. Thus, it is possible to use the rigid body motion and determine all singular elements of the original half-space.

This idea has been used by (Ahmad and Banerjee 1988) and has been extended by (Araújo, Nishikava and Mansur 1997). (Carrion 2002) has also studied the enclosing elements in his Ph.D. thesis.

* 1. **GPGPU**

We used CUDA in order to access resources provided by NVidia GPUs with the objective to increase the software performance. CUDA is an extension to the C++ programming language that allows General Purpose computations in NVidia GPUs. CUDA uses the concept of kernels, which are functions to be called from the host (CPU) to be executed by the device (GPU).

CUDA kernels are organized into a set of blocks composed by a set of threads that cooperates with each other (Patterson and Hennessy 2007). CUDA memory hierarchy also reflects this structure, where Global memory is accessible by all threads; Local memory is private to a thread; and Shared memory is accessible by all threads in the same block (Patterson and Hennessy 2007).

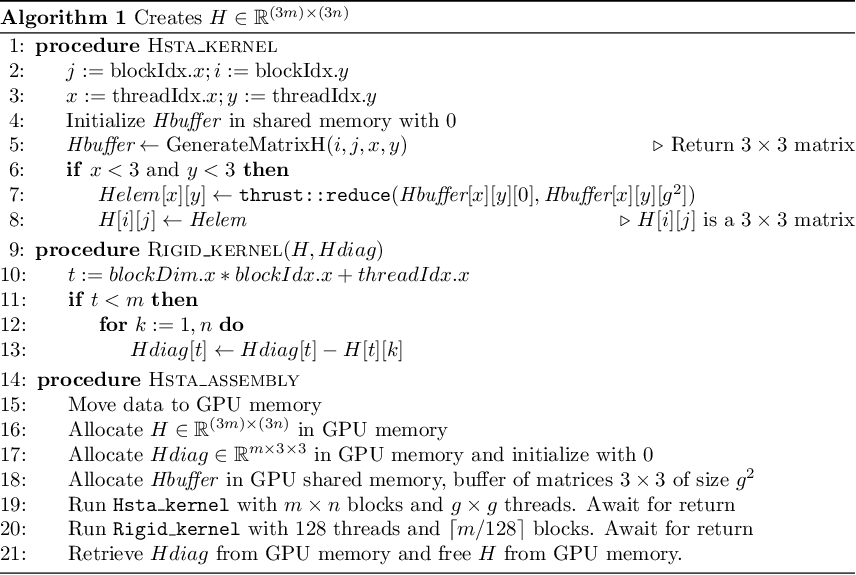
* + 1. **[H]sta Assembly**

[H]sta is assembled by computing the integrals described in equation (???) and later by considering the rigid body motion. Algorithm 1 shows a pseudocode for [H]sta creation in CUDA, where:

* *m* is the number of boundary elements
* *n* is the number of mesh elements
* *g* is the number of Gaussian Quadrature points
* GenerateMatrixH illustrates the evaluation of a single Gaussian point (*x, y*) of row *i* and column *j* of [H]sta
* Rigid\_kernel is a CUDA kernel responsible for evaluating the rigid body moviment.
* Thrust::reduce is a function provided by Thrust library for reductions.

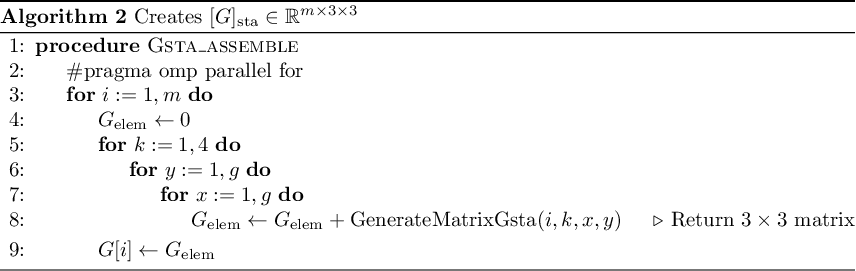
Althrough a sigle call to GenerateMatrixH is O(1), it does a considerable amount of floating point operations, justifying parallel calls to this procedure. Since it can be computed without branch divergence, we assigned each call to a CUDA thread and stored the results in a buffer located in CUDA shared memory. Then we assigned a block to compute all calls to GenerateMatrixH associated with the row i and column j of [H]est, allowing us to use the low latency CUDA shared memory for the reduction. Finally, we used the function reduce from thrust library in each matrix entry for efficiently computing the reduction at line 7. Launching this kernel with m×n blocks will generate the entire [H]sta.

For the rigid body movement routine, we had to implement our own reduction because how the data is structured. This routine did not require many improvements because it consumed little time when compared with the [H]sta assembly, and it only had to be faster than transferring [H]sta from the GPU to CPU. We used (fazer testes) CUDA threads because it yielded best results. Finally, we retrieved the Hdiag from the Device.



* + 1. **[G]sta Assembly**

[G]­sta is assembled by computing the integrals described in equation (???), as illustrated by Algorithm 2. The parameters *m*, *n* and *g* is the same as described in [H]sta assembly. Since [G]sta have no dependency relation with [H]sta, and its creation complexity is O(*g² m*), which is significantly lower than O(*g² mn*) from [H]est creation, we opted to compute [G]est entirely in the CPU in parallel to [H]est creation in the GPU. For better usage of multicore CPUs, we used OpenMP *parallel for* clause to compute each iteration of the loop at line 3 of Algorithm 2.

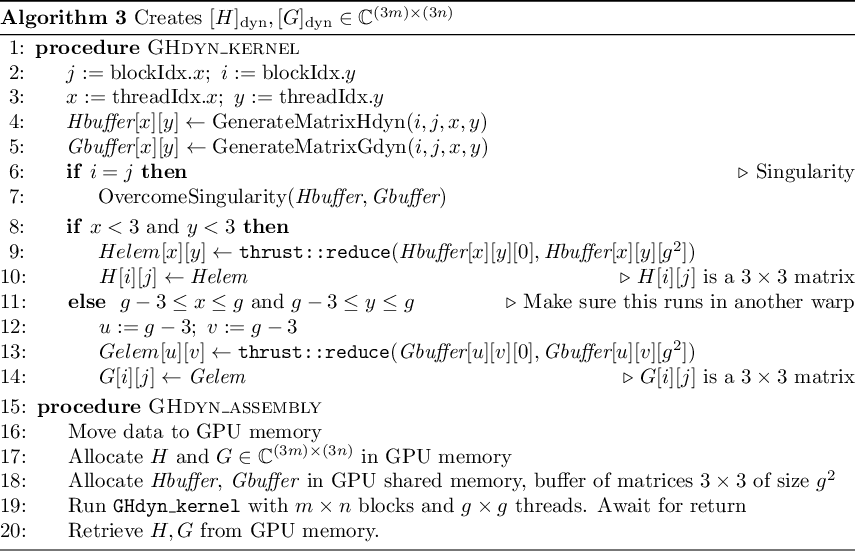


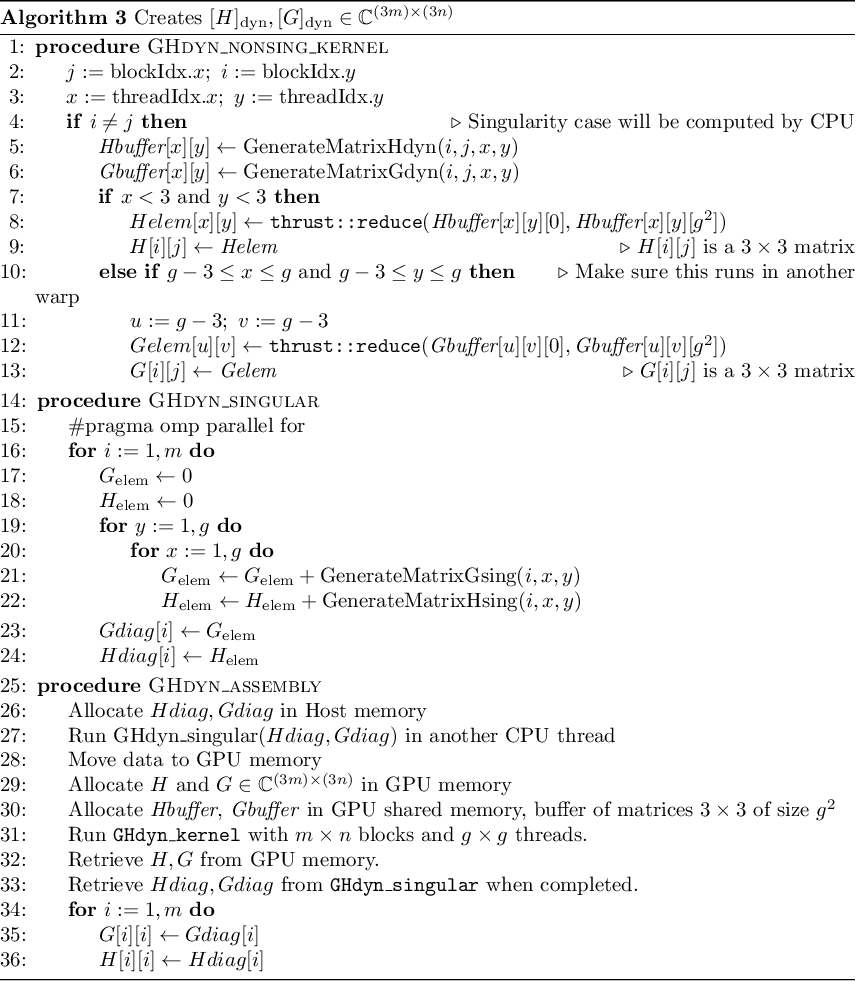
* + 1. **[H]dyn & [G]dyn Assembly**

[H]dyn and [G]dyn creation are one of the most floating point intensive parts of the software, requiring computations of several functions in the complex field. Some of these computations are shared between both [H]dyn and [G]dyn, leading us to develop a single CUDA kernel to assemble both these matrices. At first, we developed the kernel described in Algorithm 3 that computed the singular part of both [H]dyn and [G]dyn in the GPU, but this implementation resulted in errors caused by floating point imprecision. This result led us to develop another version that computed both [H]dyn and [G]dyn singular parts in the CPU while leaving the rest in the GPU. This reduced the magnitude of errors while maintaining performance.

As for implementation as a CUDA kernel, we follow the same approach described in [H]sta assembly. The differences are: We assigned one thread to compute one call to both GenerateMatrixHdyn and GenerateMatrixGdyn, and we made sure that reducing the buffer designed for the H matrices were done in parallel than the reduction of the G matrices.

Although the best performance can be archived by avoiding memory transferences between the Host and Device, for a very large grid it is not possible to maintain both [H]dyn and [G]dyn in the Device simply because the Device does not have enough memory. In order to run such large grids, we devised a memory swap logic that transfers the memory back to the Host when there isn't sufficient memory, freeing Device memory to proceed with the computation.

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* + 1. **Dense Linear System solving**

Next step is solving the system [H]dyn{u} = [G]dyn{t}. For multiplying [G]dyn{t}, we used the function CGEMV provided by OpenBLAS library. This function is heavly optimized and takes advantage of various CPU cores available.

For indeed solving the system of equation, we used a function **magma\_cgesv\_gpu** from library named MAGMA. This function solves a linear system by deploying the LU Decomposition with partial pivoting. It implements this algorithm using GPU acceleration.

* + 1. **Internal Points**

Code flowchart

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| --- |
|  |

Input data reading Static purposes: function INPUTECE

[H]sta assembly: functions GHMATECE, NONSINGE, SINGGE and SOLFUNE

Input data reading Dynamic purposes: function INPUTECD

[H]dyn and [G]dyn assembly: functions GHMATECD, NONSINGD, SING\_DE, SOLFUND and SOLFUNDIF

System of equation solver: function (from LAPACK package)

Internal points: function INTEREC

Output data writing: function SIGMAEC

1. **Numerical Examples**
2. **Conclusion**

**Acknowledgments:**

Alfredo, if you want, write the agency which funded Giuliano´s scholarship.

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