

$$\cdot \alpha_1 \times \alpha_2)_{,\alpha} - \frac{1}{\sqrt{a}} M_{1\alpha} \cdot \alpha_1 \times \alpha_2$$

We denote the tangential surface tension tensor ℓ^{ij} , the tangential bending moment density tensor in the surface m^{ij} and its related tensor $\bar{m}^{ij} = -m^{ik}\epsilon_{kl}^j$. We assume that no external force or torque density act on a surface element, and consider configurations of mechanical equilibrium with no flow. The tangential and normal force balance equations can then be written [3]

$$\nabla_i \ell^{ij} + C_l \nabla_k m^{kj} = 0 \quad , \quad (21)$$

$$\nabla_i \nabla_j \ell^{ij} - C_{kl} \ell^{kl} = 0 \quad . \quad (22)$$

We consider the following constitutive equations for the tension and bending moment density tensors

$$t_{ij} = K^{a-\alpha_0}_{\alpha_0} g_{ij} \quad , \quad \boxed{\text{SoftWPC}} \quad (23)$$

$$\bar{m}_{ij} = (\alpha C_k^k + \zeta) g_{ij} \quad . \quad (24)$$

With the constitutive equations [23][24] the tangential and normal force balance equations can be rewritten

$$K \partial_i \left(\frac{a - a_0}{a_0} \right) + C_l^i \partial_j (e C_k^k + \zeta_e) = 0 \quad , \quad (25)$$

$$\Delta (e C_k^k + \zeta_e) - K \frac{a - a_0}{a_0} C_k^k = 0 \quad , \quad (26)$$

where we have introduced the Laplace-Beltrami operator, $\Delta = \frac{1}{\sqrt{g}} \partial_i (\sqrt{g} g^{ij} \partial_j f)$.

