



$$\cdot a_1 x a_2), \alpha - \frac{1}{\sqrt{a}} \overset{0}{\overbrace{m_1 \alpha \cdot a_1 x a_2}}$$

We denote the tangential surface tension tensor  $t^{ij}$ , the tangential bending moment density tensor in the surface  $m^{ij}$  and its related tensor  $\bar{m}^{ij} = -m^{\alpha\beta}e_{\alpha}^ie_{\beta}^j$ . We assume that no external force or torque density act on a surface element, and consider configurations of mechanical equilibrium with no flow. The tangential and normal force balance equations can then be written [8]

$$\nabla_i t^{ij} + C_i^{\alpha}\nabla_{\alpha}m^{ij} = 0 \quad , \tag{21}$$

$$\nabla_i(\nabla_j\bar{m}^{ij} - C_j^{\alpha}t^{\alpha i}) = 0 \quad . \tag{22}$$

We consider the following constitutive equations for the tension and bending moment density tensors

$$t_{ij} = K\frac{\partial}{\partial\epsilon}\epsilon_{ij} \quad , \tag{23}$$

$$m_{ij} = (\kappa C_i^{\alpha}C_j^{\beta} + \zeta_i)\delta_{ij} \quad , \tag{24}$$



With the constitutive equations [\(23\)-\(24\)](#) the tangential and normal force balance equations can be rewritten

$$K\partial_t\left(\frac{\sigma-\alpha_0}{\alpha_0}\right)+C_i^j\partial_j(\alpha C_1^k+\zeta)=0\quad , \tag{25}$$

$$\Delta(\alpha C_1^k+\zeta)-K\frac{\sigma-\alpha_0}{\alpha_0}C_1^k=0\quad , \tag{26}$$

where we have introduced the Laplace-Beltrami operator,  $\Delta=\frac{1}{\sqrt{g}}\partial_i(\sqrt{g}g^{ij}\partial_jf)$ .

