

Legame costitutivo

relazione lineare

materiali isotropi (acciaio, calcestruzzo)  
non il legno

$$\underline{\underline{T}} \leftrightarrow \underline{\underline{E}}$$

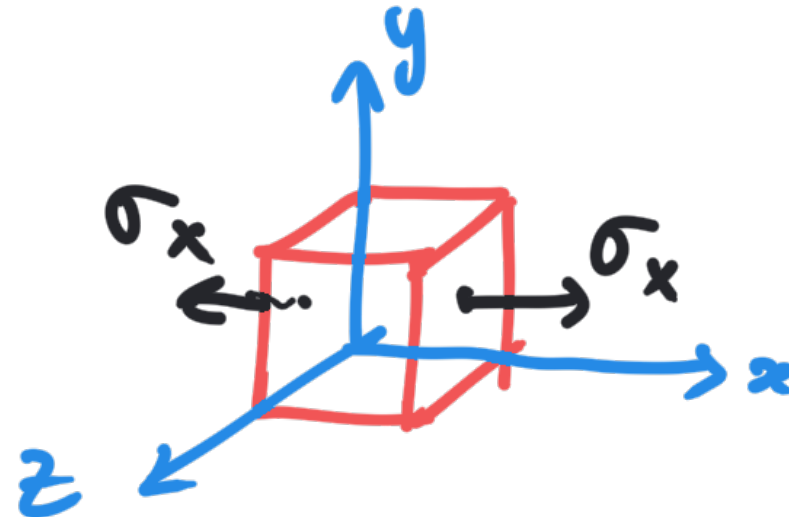
RIF:

15.2 e 15.3

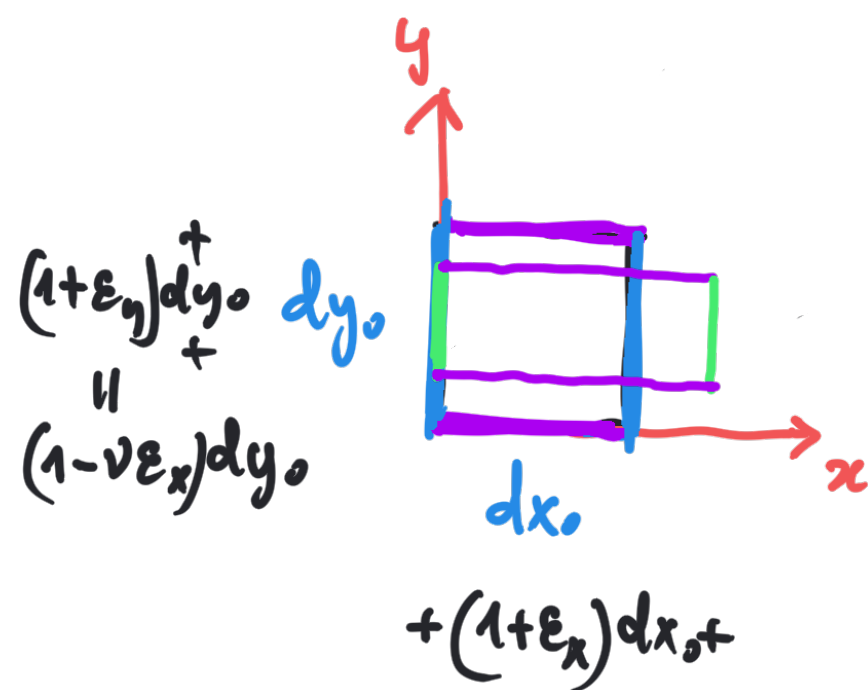
3 costanti:  $E$  modulo di Young  $[E] = FL^{-2}$   
 $\nu$  coeff. di Poisson  $[\nu] = 1$   
 $G$  modulo di scorrimento  $[G] = FL^{-2}$

NB:  $G = \frac{E}{2(1+\nu)}$

$$\underline{\underline{T}} = \begin{bmatrix} \sigma_x & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$



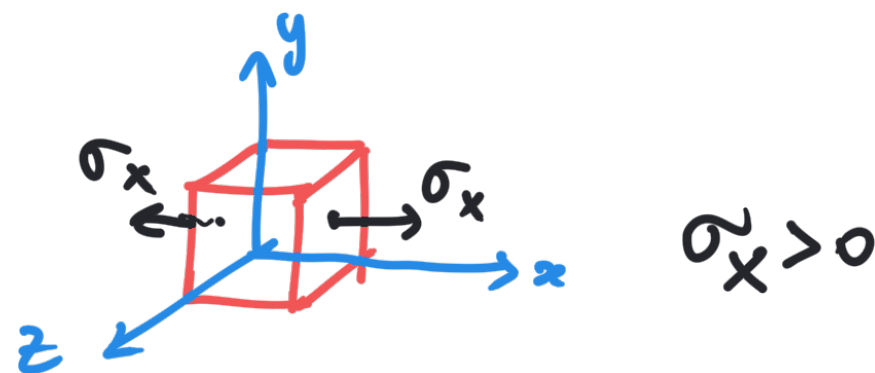
$$\underline{\underline{\epsilon}} = \begin{bmatrix} \epsilon_x & 0 & 0 \\ 0 & \epsilon_y & 0 \\ 0 & 0 & \epsilon_z \end{bmatrix}$$



$$\underline{\underline{\sigma}} = \begin{bmatrix} \sigma_x & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\epsilon_x = \frac{\sigma_x}{E} > 0$$

$$\epsilon_y = \epsilon_z = -\nu \frac{\sigma_x}{E} = -\nu \epsilon_x < 0$$



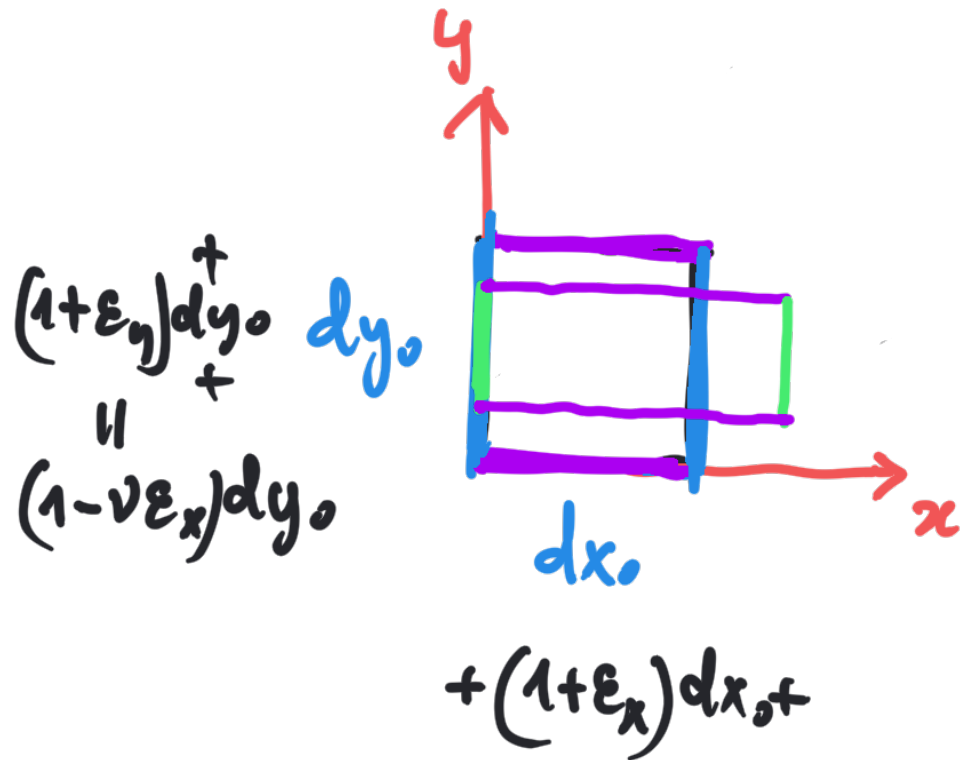
$$\underline{\underline{\epsilon}} = \begin{bmatrix} \epsilon_x & 0 & 0 \\ 0 & \epsilon_y & 0 \\ 0 & 0 & \epsilon_z \end{bmatrix}$$

$$\epsilon_y = \frac{a - a_0}{a} = -\nu \epsilon_x$$

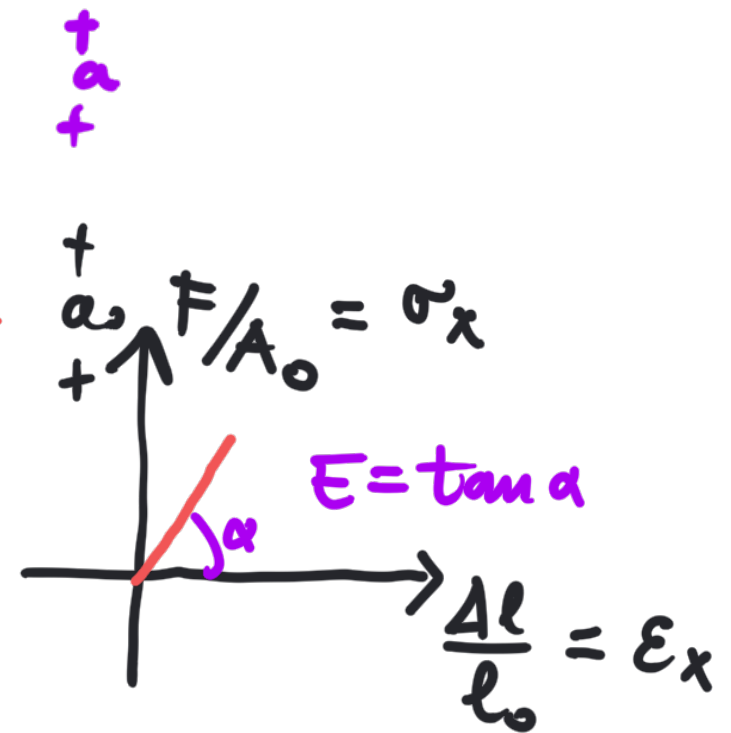
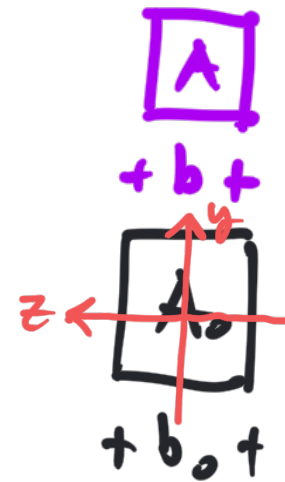
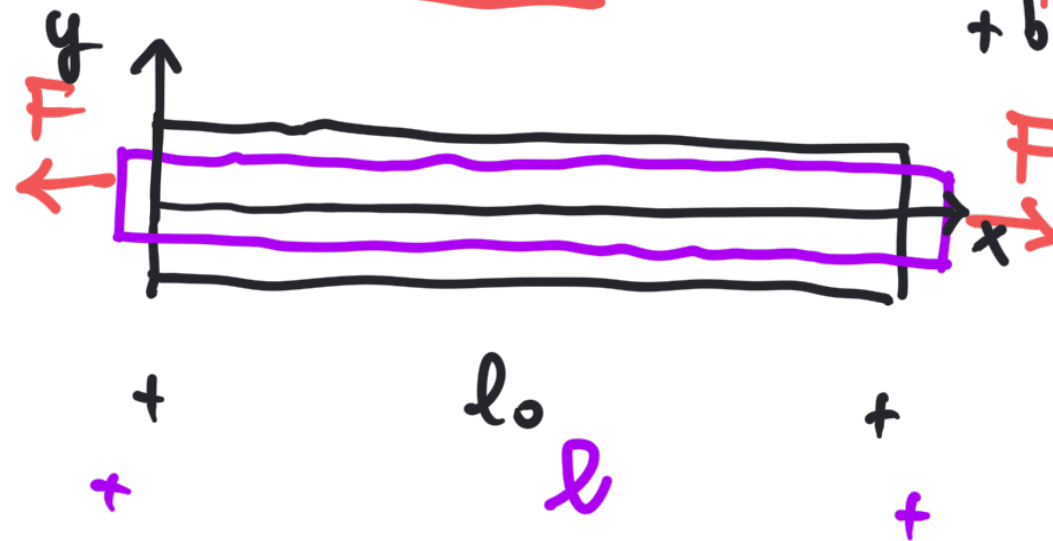
$$\epsilon_z = \frac{b - b_0}{b_0} = -\nu \epsilon_x$$

$$\epsilon_x = \frac{\sigma_x}{E}$$

$$\sigma_x = E \epsilon_x$$

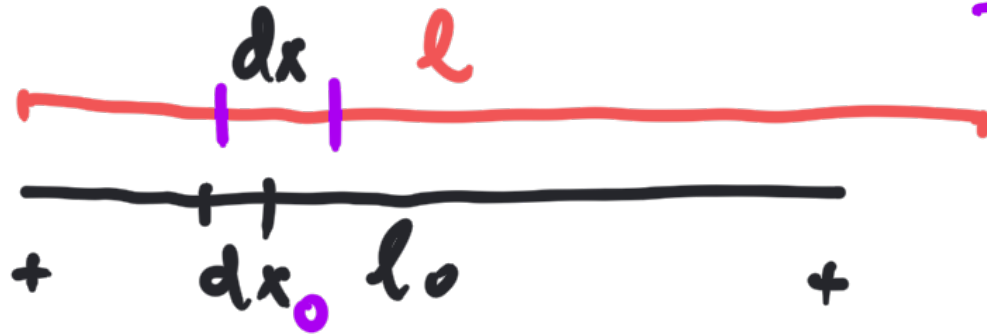


Misura sperimentale  
Prova uniassiale



I cost. E cost.

$$\sigma_x = F/A_0 \quad \epsilon_x = \frac{\Delta l}{l_0}$$



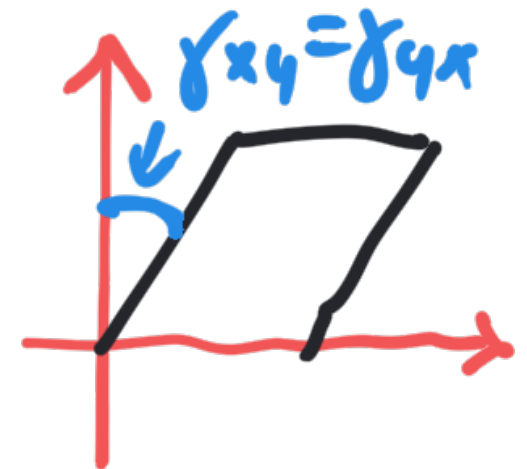
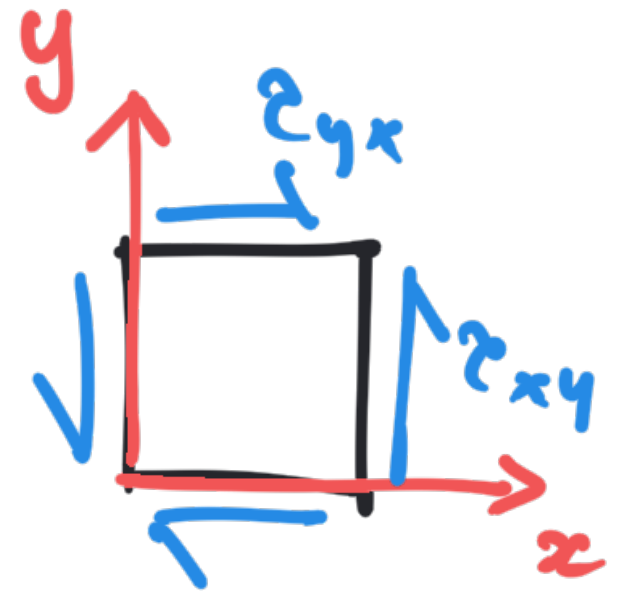
Risultato indipendente da  $l_0$  e dall'area della sezione trasversale del provino.  
Solo dal materiale

$$\frac{dx}{dx_0} - 1 = \frac{l}{l_0} - 1 \Rightarrow \frac{dx - dx_0}{dx_0} = \frac{l - l_0}{l_0} = \epsilon_x$$

Modulo di scorrimento  $G$

$$\underline{\underline{\tau}} = \begin{bmatrix} 0 & \tau_{yx} & 0 \\ \tau_{xy} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad (\text{taglio puro})$$

$$\underline{\underline{E}} = \begin{bmatrix} 0 & \frac{\gamma_{yx}}{2} & 0 \\ \gamma_{xy}/2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad \gamma_{xy} = \frac{\tau_{xy}}{G}$$



Prova di torsione



Caso generale

$$\underline{I} = \begin{bmatrix} \sigma_x & \tau_{yx} & \tau_{zx} \\ \tau_{xy} & \sigma_y & \tau_{zy} \\ \tau_{xz} & \tau_{yz} & \sigma_z \end{bmatrix} \equiv \text{sovrapposizione di} \\ \text{3 stati uniaxiali} \\ \text{e 3 stati di taglio puro}$$

$$\begin{bmatrix} \sigma_x & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad \begin{bmatrix} 0 & 0 & 0 \\ 0 & \sigma_y & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \sigma_z \end{bmatrix}$$

$$\begin{bmatrix} 0 & \tau_{xy} & 0 \\ \tau_{xy} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad \begin{bmatrix} 0 & 0 & \tau_{xz} \\ 0 & 0 & 0 \\ \tau_{xz} & 0 & 0 \end{bmatrix} \quad \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & \tau_{yz} \\ 0 & \tau_{yz} & 0 \end{bmatrix}$$

$$(15.16) \quad \begin{aligned} \varepsilon_x &= \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)] & \varepsilon_z &= \frac{1}{E} (\sigma_z - \nu(\sigma_x + \sigma_y)) \\ \varepsilon_y &= \frac{1}{E} [\sigma_y - \nu(\sigma_x + \sigma_z)] \end{aligned}$$

## Caso generale

$$\underline{I} = \begin{bmatrix} \sigma_x & \tau_{yx} & \tau_{zx} \\ \tau_{xy} & \sigma_y & \tau_{zy} \\ \tau_{xz} & \tau_{yz} & \sigma_z \end{bmatrix} \equiv \text{sovrapposizione di} \\ \text{3 stati uniascuali} \\ \text{e 3 stati di taglio puro}$$

(15.16)

$$\varepsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)]$$

$$\varepsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_x + \sigma_z)]$$

$$\varepsilon_z = \frac{1}{E} (\sigma_z - \nu(\sigma_x + \sigma_y))$$

$$\gamma_{xy} = \frac{\tau_{xy}}{G}$$

$$\gamma_{xz} = \frac{\tau_{xz}}{G}$$

$$\gamma_{yz} = \frac{\tau_{yz}}{G}$$