

ELEC 221 Lecture 16

Time and frequency domain analysis II

Tuesday 1 November 2022

Announcements

- Midterms available for pickup at my office
- Quiz 7 today
- Assignment 5 released soon (last one before midterm 2)

Important:

- Nov. 8 class on Zoom
- Office hours this Friday and next Friday on Zoom (same time)

Links will be distributed on Canvas.

Last time

We formalized the magnitude-phase representation of spectra:

$$H(j\omega) = |H(j\omega)| e^{j\angle H(j\omega)}$$

where

- $|H(j\omega)|$ is the gain
- $\angle H(j\omega)$ is the phase shift

We used these to analyze how systems affect phase:

$$|Y(j\omega)| = |H(j\omega)| \cdot |X(j\omega)|$$

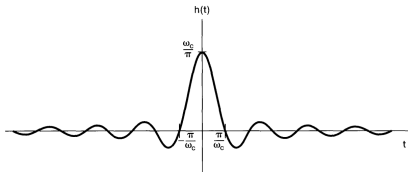
$$\angle Y(j\omega) = \angle H(j\omega) + \angle X(j\omega)$$

Last time

We saw how linear shifts in phase affect a system's behaviour:

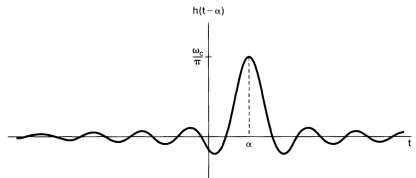
$$H(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$$

$$h(t) = \frac{\sin(\omega_c t)}{\pi t}$$



$$H(j\omega) = \begin{cases} e^{-j\alpha\omega} & |\omega| \leq \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$$

$$h(t) = \frac{\sin(\omega_c (t - \alpha))}{\pi (t - \alpha)}$$



We analyzed non-linear shifts by making an approximation that they are linear for small bands of frequencies:

$$\angle H(j\omega) \approx -\phi - \alpha\omega$$

We extended this to the idea of group delay:

$$\tau(\omega) = -\frac{d}{d\omega} \angle H(j\omega)$$

Illustrative example (Oppenheim Ex. 6.1): group delay

Suppose we have some system whose frequency response is

$$H(j\omega) = \prod_{i=1}^3 H_i(j\omega),$$

$$H_i(j\omega) = \frac{1 + (j\omega/\omega_i)^2 - 2j\zeta_i(\omega/\omega_i)}{1 + (j\omega/\omega_i)^2 + 2j\zeta_i(\omega/\omega_i)},$$

$$\begin{cases} \omega_1 = 315 \text{ rad/sec and } \zeta_1 = 0.066, \\ \omega_2 = 943 \text{ rad/sec and } \zeta_2 = 0.033, \\ \omega_3 = 1888 \text{ rad/sec and } \zeta_3 = 0.058. \end{cases}$$

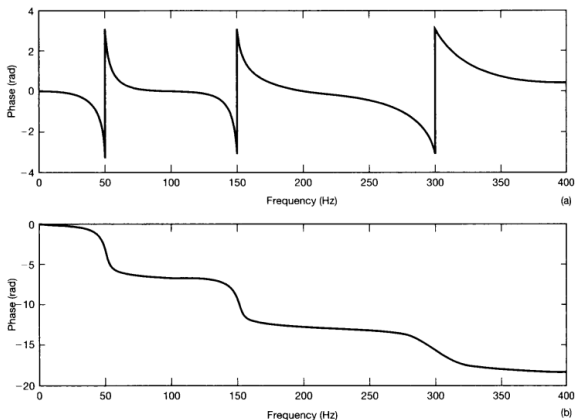
Actual frequencies: $f_1 \approx 50 \text{ Hz}$, $f_2 \approx 150 \text{ Hz}$, $f_3 = 300 \text{ Hz}$.

Image credit: Oppenheim 6.2

Illustrative example (Oppenheim Ex. 6.1): group delay

Can find that $|H(j\omega)| = 1$, and the phase component is

$$\angle H(j\omega) = -2 \sum_{i=1}^3 \tan^{-1} \left[\frac{2\zeta_i(\omega/\omega_i)}{1 - (\omega/\omega_i)^2} \right]$$



Illustrative example (Oppenheim Ex. 6.1): group delay

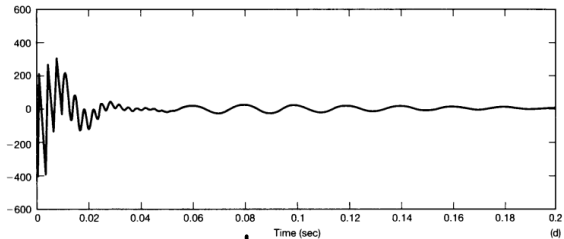
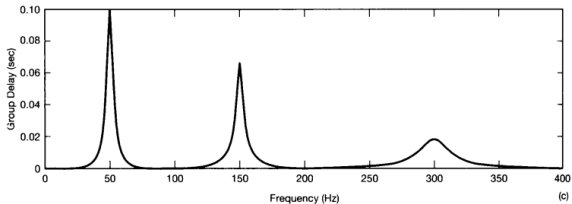


Image credit: Oppenheim 6.2

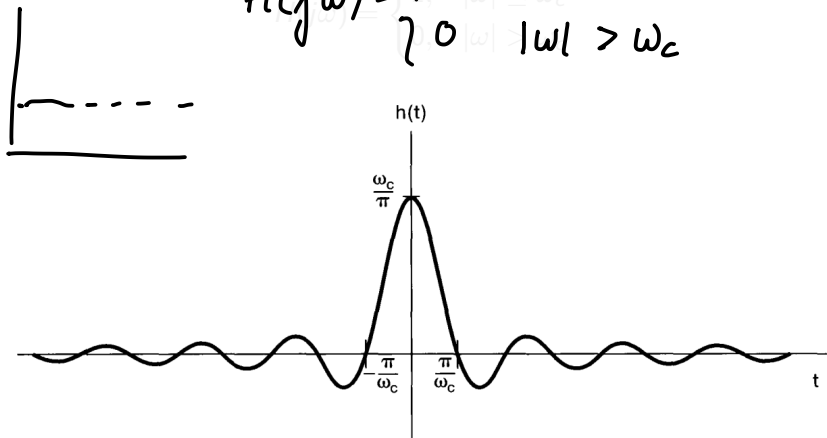
Learning outcomes:

- define and compute the unit step response of a system
- plot frequency response using a Bode plot
- characterize the oscillatory behaviour of CT systems described by second-order differential equations

We will continue to work in CT: you will get practice problems and assignment problems about the DT case (it is very similar).

Ideal filter step response

$$H(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$$



Ideal filter step response

It is also important to consider *step response* of filters.

Recall that

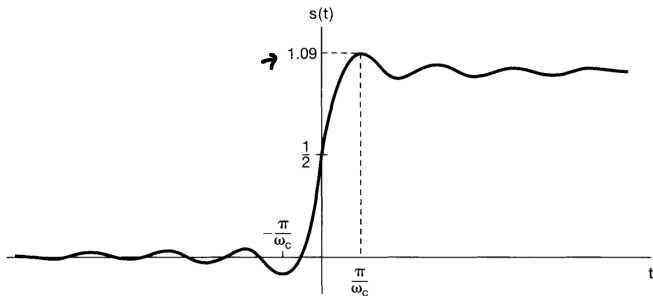
$$u(t) = \int_{-\infty}^t \delta(\tau) d\tau$$

By linearity, if we put this in a system, the result is

$$s(t) = \int_{-\infty}^t h(\tau) d\tau$$

Ideal filter step response

$$s(t) = \int_{-\infty}^t h(\tau) d\tau = h(t) = \frac{\sin(\omega_c t)}{\pi t}$$



An ideal filter leads to **ringing** in the step response.

Image credit: Oppenheim 6.3

Ideal filter step response

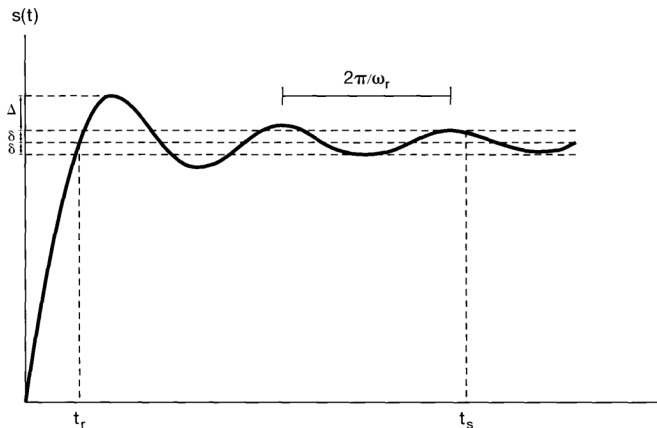
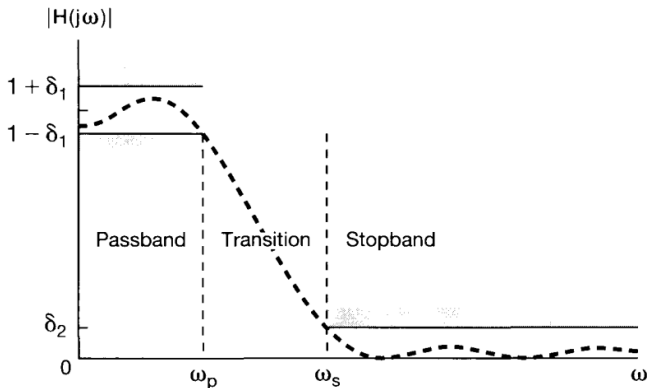


Figure 6.17 Step response of a continuous-time lowpass filter, indicating the rise time t_r , overshoot Δ , ringing frequency ω_r , and settling time t_s —i.e., the time at which the step response settles to within $\pm\delta$ of its final value.

Non-ideal filters

There are **tradeoffs** in filter design. Compromises in the frequency domain can lead to nicer behaviour in the time domain.



First-order systems

LTI system described by a first-order ODE:

$$\tau \frac{dy(t)}{dt} + y(t) = x(t)$$

Exercise: what is the frequency response $H(j\omega)$?

$$\frac{1}{1 + \tau j\omega}$$

First-order systems

Solution: recall the handy formula we derived from the convolution property. Given an arbitrary-order ODE,

$$\sum_{k=0}^N \alpha_k \frac{d^k y(t)}{dt^k} = \sum_{k=0}^M \beta_k \frac{d^k x(t)}{dt^k}$$

the frequency response is

$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{\sum_{k=0}^M \beta_k (j\omega)^k}{\sum_{k=0}^N \alpha_k (j\omega)^k}$$

So for our system,

$$H(j\omega) = \frac{1}{1 + j\omega\tau}$$

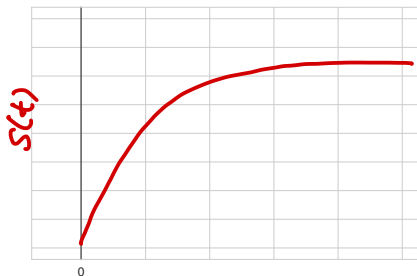
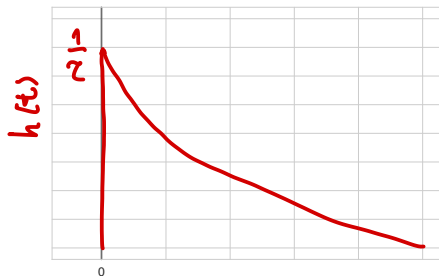
First-order systems

$$\tau \frac{dy(t)}{dt} + y(t) = x(t), \quad H(j\omega) = \frac{1}{1 + j\omega\tau}$$

The impulse and step response of the system are

$$h(t) = \frac{1}{\tau} e^{-t/\tau} u(t) \quad s(t) = (1 - e^{-t/\tau}) u(t)$$

τ is the **time constant** of the system.



First-order systems

$$\tau \frac{dy(t)}{dt} + y(t) = x(t), \quad H(j\omega) = \frac{1}{1 + j\omega\tau}$$

Let's view these in the magnitude-phase representation:

$$H(j\omega) = \frac{1}{1 + j\omega\tau} \frac{1 - j\omega\tau}{1 - j\omega\tau} = \frac{1}{(\omega\tau)^2 + 1} - j \frac{\omega\tau}{(\omega\tau)^2 + 1}$$

From this, we find

$$|H(j\omega)| = \frac{1}{\sqrt{(\omega\tau)^2 + 1}}$$

$$\angle H(j\omega) = \tan^{-1}(-\omega\tau)$$

Let's plot these in a new way...

Recall:

$$|Y(j\omega)| = |H(j\omega)| \cdot |X(j\omega)|$$
$$\angle Y(j\omega) = \angle H(j\omega) + \angle X(j\omega)$$

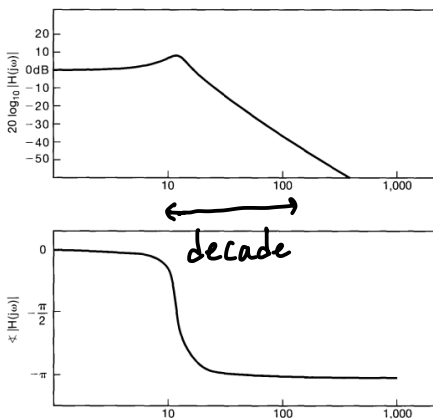
Magnitude is multiplicative and phase is additive... would be nicer if both were additive.

$$\log_{10} |Y(j\omega)| = \log_{10} |H(j\omega)| + \log_{10} |X(j\omega)|$$

Rather than making plots of $|H(j\omega)|$ and $\angle H(j\omega)$, it is common to make plots of $20 \log_{10} |H(j\omega)|$ and $\angle H(j\omega)$ against $\log_{10} \omega$.

Bode plots

These are called *Bode plots*:



The logarithmic scale also allows us to view the response over a much wider range of frequencies.

First-order systems

We have

$$|H(j\omega)| = \frac{1}{\sqrt{(\omega\tau)^2 + 1}}$$

$$\angle H(j\omega) = \tan^{-1}(-\omega\tau)$$

To make our Bode plot, compute

$$\begin{aligned} 20 \log_{10} |H(j\omega)| &= -10 \log_{10} ((\omega\tau)^2 + 1) \\ &= -20 \log_{10} ((\omega\tau)^2 + 1)^{1/2} \\ &= -10 \log_{10} ((\omega\tau)^2 + 1) \end{aligned}$$

$$20 \log_{10} |H(j\omega)| = -10 \log_{10} (\omega\tau^2 + 1)$$

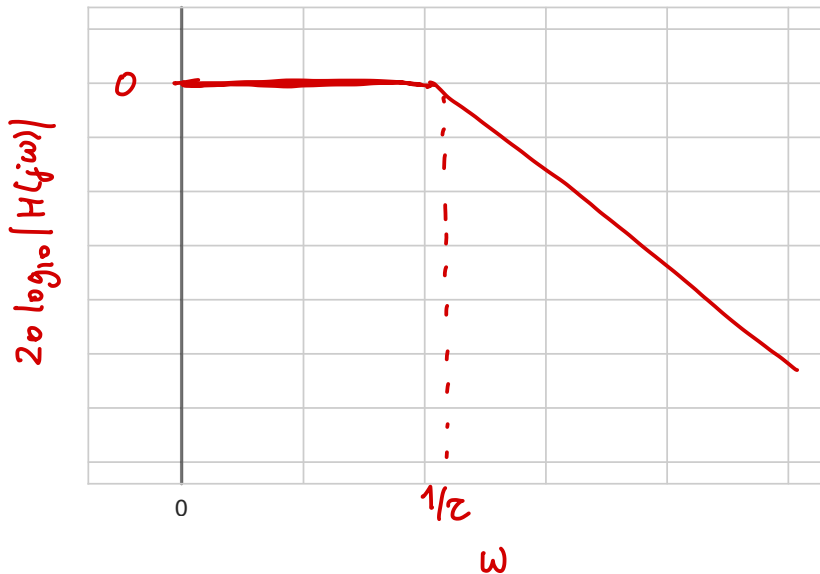
If $\omega \ll 1/\tau$,

$$20 \log_{10} |H(j\omega)| \approx 0$$

If $\omega \gg 1/\tau$, $\omega\tau \gg 1$

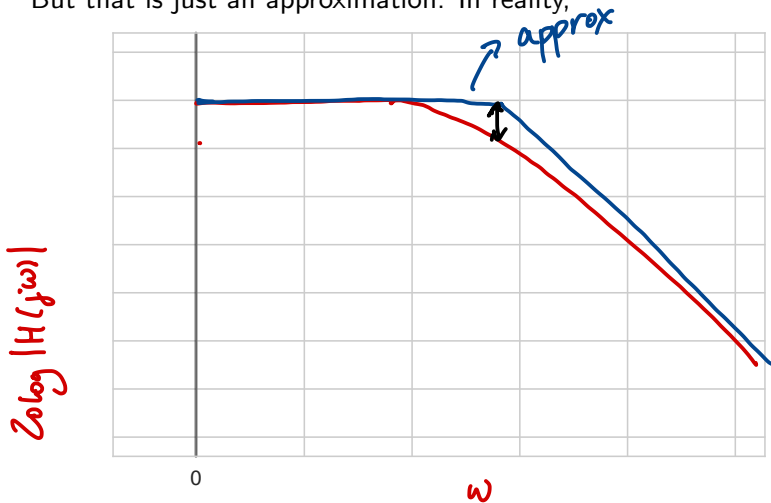
$$\begin{aligned} 20 \log_{10} |H(j\omega)| &\approx -10 \log_{10} (\omega\tau)^2 \\ &= -20 \log_{10} (\omega\tau) \\ &= -20 \log_{10}(\omega) - 20 \log_{10}(\tau) \end{aligned}$$

First-order systems



First-order systems

But that is just an approximation. In reality,



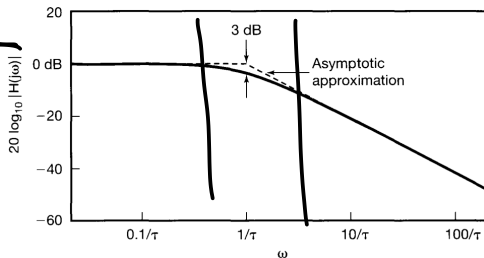
The case of $\omega = 1/\tau$ has a special name.

First-order systems

$$20 \log_{10} |H(j\omega)| = -10 \log_{10} ((\omega\tau)^2 + 1)$$

If $\omega = 1/\tau$,

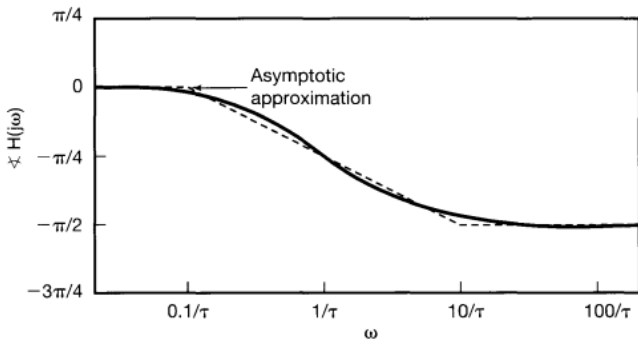
$$20 \log_{10} |H(j\omega)| = -10 \log_{10}(2) \\ \approx -3$$



First-order systems

Can make similar approximations to recover plot of the phase

$$H(j\omega) = \tan^{-1}(-\omega\tau)$$



Second-order systems

Consider a system described by the ODE

$$\frac{d^2 y(t)}{dt^2} + 2\zeta\omega_n \frac{dy(t)}{dt} + \omega_n^2 y(t) = \omega_n^2 x(t)$$

Exercise: what is the frequency response?

$$\begin{aligned} H(j\omega) &= \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2} \\ &= \frac{1}{(j\omega/\omega_n)^2 + 2\zeta(j\omega/\omega_n) + 1} \end{aligned}$$

Second-order systems

Let's explore this in a little more detail and compute the impulse and step response of this system.

$$\begin{aligned} H(j\omega) &= \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2} \\ &= \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)} \end{aligned}$$

where

$$c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Three cases to consider:

- $\zeta = 1$
- $\zeta > 1$
- $\zeta < 1$

$$\frac{1}{a + j\omega}$$

$$H(j\omega) = \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)}, \quad c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Case: $\zeta = 1$.

$$c_{\pm} = -\zeta\omega_n = -\omega_n$$

$$H(j\omega) = \frac{\omega_n^2}{(j\omega + \omega_n)^2}$$

Use handy table of Fourier transform pairs to find

$$h(t) = \omega_n^2 t e^{-\omega_n t} u(t)$$

Second-order systems

$$H(j\omega) = \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)}, \quad c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Case: $\zeta \neq 1$. Do a partial fraction expansion:

$$\begin{aligned} H(j\omega) &= \frac{A}{j\omega - c_+} + \frac{B}{j\omega - c_-} \\ &= \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \cdot \frac{1}{j\omega - c_+} - \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \cdot \frac{1}{j\omega - c_-} \end{aligned}$$

Use handy table of Fourier transform pairs to find

$$h(t) = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \left[e^{c_+ t} - e^{c_- t} \right] u(t)$$

Second-order systems

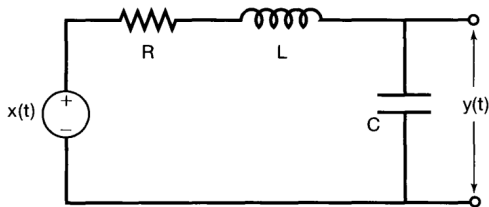
$$h(t) = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} (e^{c_+ t} - e^{c_- t}) u(t), \quad c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

The form of the exponential depends on whether $\zeta > 1$ or $\zeta < 1$

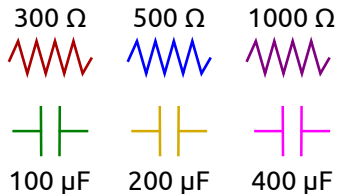
- $\zeta < 1$: c_{\pm} are imaginary; complex exponentials, so the response will oscillate!
- $\zeta > 1$: c_{\pm} real and negative; decaying exponentials

Let's go plot these.

Example: RLC circuit

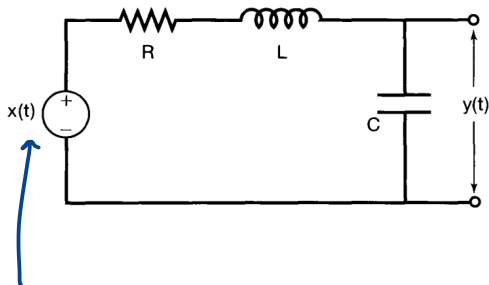


Suppose $L = 6$ H. We have a box of capacitors and resistors:



What is the best choice to ensure step response doesn't oscillate?

Example: RLC circuit



First, we need to set up the ODE for the system.

$$V_{\text{Total}} = V_R(t) + V_C(t) + V_L(t)$$

$$x(t) = LC \frac{d^2 y(t)}{dt^2} + RC \frac{dy(t)}{dt} + y(t)$$

Image credit: Oppenheim P6.19.

Example: RLC circuit

$$x(t) = LC \frac{d^2 y(t)}{dt^2} + RC \frac{dy(t)}{dt} + y(t)$$

Solution: compute the frequency response

$$\begin{aligned} H(j\omega) &= \frac{1}{LC(j\omega)^2 + RCj\omega + 1} \\ &= \frac{1}{(j\omega/(1/\sqrt{LC}))^2 + 2(R/2)\sqrt{C/L}j\omega + 1} \end{aligned}$$

Find that $\zeta = (R/2)\sqrt{C/L}$

Example: RLC circuit

If $\zeta = (R/2)\sqrt{C/L}$, and $L = 6$ H, we want

$$\begin{aligned}\frac{R}{2}\sqrt{\frac{C}{L}} &\geq 1 \\ R^2 C &\geq 4L = 24H\end{aligned}$$

Best choice is $R = 500\Omega$, and $C = 100\mu F$ ($R^2 C = 25$)

Learning outcomes:

- define and compute the unit step response of a system
- plot frequency response using a Bode plot
- characterize the oscillatory behaviour of CT systems described by second-order differential equations

Oppenheim practice problems:

- (DT) 6.35, 6.36, 6.41, 6.42, 6.65
- (CT) 6.15, 6.28 (choose a couple), 6.32, 6.33, 6.53

For next time

Content:

- The sampling theorem
- Basics of interpolation
- The Nyquist rate and aliasing

Action items:

1. Work through Oppenheim section 6.5-6.7
2. Assignment 5 coming soon
3. Midterm 2 in two weeks

Recommended reading:

- From this class: Oppenheim 6.4-6.8
- For next class: Oppenheim 7.1-7.3