

ELEC 221 Lecture 14
**Analysis of CT systems based on first- and
second-order differential equations**

Thursday 24 October 2024

Announcements

- Tutorial assignment 3 due Monday 23:59
- Assignment 3 available, due Saturday 2 Nov 23:59
- Monday's tutorial will focus on problem solving
- MT2 information available next week

Erratum from last class:

$$z(t) = x(t)y(t) \Rightarrow Z(j\omega) = \frac{1}{2\pi} X(j\omega) * Y(j\omega)$$

Last time

We expressed systems in the magnitude phase representation

$$X(j\omega) = |X(j\omega)| e^{j\angle X(j\omega)}$$

For a signal $x(t)$ and system with frequency response $H(j\omega)$,

$$|Y(j\omega)| = |H(j\omega)| |X(j\omega)|$$

$$\angle Y(j\omega) = \angle H(j\omega) + \angle X(j\omega)$$

$|H(j\omega)|$ is the gain and $\angle H(j\omega)$ is the phase shift. We plotted these separately.

Last time

We derived the behaviour of the Fourier transform under differentiation and integration:

$$\begin{aligned}x(t) &\stackrel{\mathcal{F}}{\longleftrightarrow} X(j\omega) \\ \frac{dx(t)}{dt} &\stackrel{\mathcal{F}}{\longleftrightarrow} j\omega X(j\omega) \\ \int_{-\infty}^t x(\tau) d\tau &\stackrel{\mathcal{F}}{\longleftrightarrow} \frac{1}{j\omega} X(j\omega) + \pi X(0) \delta(\omega)\end{aligned}$$

From these, we determined

$$\begin{aligned}\delta(t) &\stackrel{\mathcal{F}}{\longleftrightarrow} \Delta(j\omega) = 1 \\ u(t) &\stackrel{\mathcal{F}}{\longleftrightarrow} U(j\omega) = \frac{1}{j\omega} + \pi \delta(\omega)\end{aligned}$$

Finally, we combined many properties to write an expression for the frequency responses of systems described by differential equations,

$$\sum_{k=0}^N \alpha_k \frac{dy^k(t)}{dt^k} = \sum_{k=0}^M \beta_k \frac{dx^k(t)}{dt^k}$$

$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{\sum_{k=0}^M \beta_k (j\omega)^k}{\sum_{k=0}^N \alpha_k (j\omega)^k}$$

Last time: exercise

What are the **impulse response** and **frequency response** of the system described by

$$\frac{d^3 y(t)}{dt^3} - 4 \frac{dy(t)}{dt} = 3 \frac{d^2 x(t)}{dt^2} + x(t)$$

We computed frequency response and began using partial fractions:

$$\begin{aligned} H(j\omega) &= \frac{3(j\omega)^2 + 1}{(j\omega)^3 - 4j\omega} \\ &= \frac{3(j\omega)^2 + 1}{j\omega((j\omega)^2 - 4)} \\ &= \frac{3(j\omega)^2 + 1}{j\omega(j\omega + 2)(j\omega - 2)} \\ &= \frac{A}{j\omega} + \frac{B}{j\omega + 2} + \frac{C}{j\omega - 2} \end{aligned}$$

Last time: exercise

Details are left as an exercise:

$$H(j\omega) = \frac{-1/4}{j\omega} + \frac{13/8}{j\omega+2} + \frac{13/8}{j\omega-2}$$

To get the impulse response, we can take the inverse Fourier transform, and leverage linearity:

$$h(t) = -\frac{1}{4} \mathcal{F}^{-1}\left(\frac{1}{j\omega}\right) + \frac{13}{8} \mathcal{F}^{-1}\left(\frac{1}{j\omega+2}\right) + \frac{13}{8} \mathcal{F}^{-1}\left(\frac{1}{j\omega-2}\right)$$

Last time: exercise

$$x(t)=1 \xleftrightarrow{\mathcal{F}} 2\pi\delta(\omega)$$

time reversed
←

$$h(t) = -\frac{1}{4}\mathcal{F}^{-1}\left(\frac{1}{j\omega}\right) + \frac{13}{8}\mathcal{F}^{-1}\left(\frac{1}{j\omega+2}\right) + \frac{13}{8}\mathcal{F}^{-1}\left(\frac{1}{j\omega-2}\right) - \frac{13}{8}\mathcal{F}^{-1}\left(\frac{1}{2-j\omega}\right)$$

Check Table 4.2 - two expressions to leverage:

$$\mathcal{F}\left[e^{-at}u(t)\right] = \frac{1}{a+j\omega} \quad \text{Re}(a) > 0$$

$$\mathcal{F}^{-1}\left(\frac{1}{j\omega}\right) = \mathcal{F}^{-1}\left(\frac{1}{j\omega} + \pi\delta(\omega) - \pi\delta(\omega)\right) = \underbrace{u(t)} - \underbrace{\frac{1}{2}}$$

So we have:

$$h(t) = -\frac{1}{4}u(t) + \frac{1}{8} + \frac{13}{8}e^{-2t}u(t) - \frac{13}{8}e^{2t}u(-t)$$

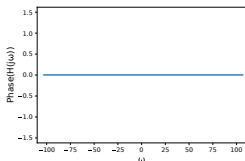
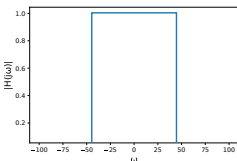
Learning outcomes:

- define and compute the unit step response of a system
- characterize the oscillatory behaviour of CT systems described by second-order differential equations
- read a Bode plot

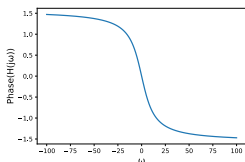
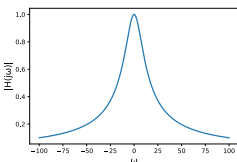
Lowpass filters

We've seen two versions of lowpass filters:

$$H(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$$



$$H(j\omega) = \frac{1}{1 + j\omega RC}$$



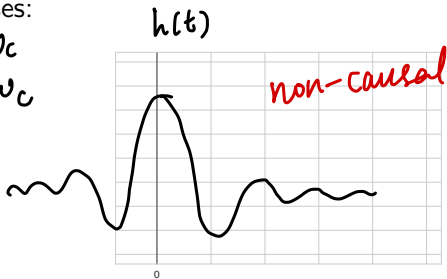
What's the difference?

Lowpass filters

Look at their impulse responses:

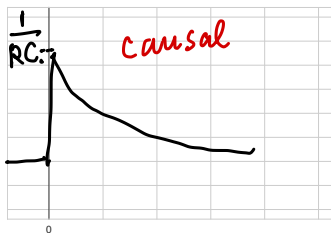
$$H(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$$

$$h(t) = \frac{\sin(\omega_c t)}{\pi t}$$



$$H(j\omega) = \frac{1}{1 + j\omega RC} = \frac{1}{RC(\frac{1}{RC} + j\omega)}$$

$$h(t) = \frac{1}{RC} e^{-t/RC} u(t)$$



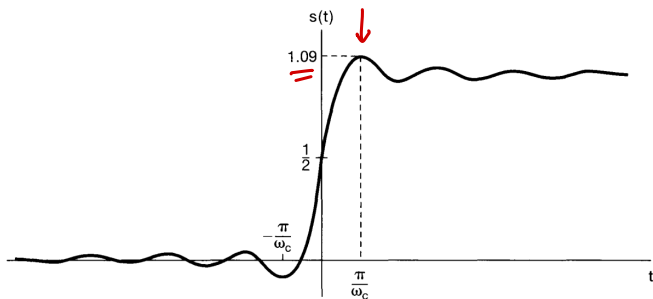
Step response

It is also important to consider the *step response* of filters:

$$\begin{aligned} s(t) &= h(t) * u(t) & t - \tau > 0 \\ &= \int_{-\infty}^{\infty} h(\tau) u(t - \tau) d\tau \\ &= \int_{-\infty}^t h(\tau) d\tau \end{aligned}$$

Ideal filter step response

$$h(t) = \frac{\sin(\omega_c t)}{\pi t} \quad s(t) = \int_{-\infty}^t h(\tau) d\tau$$



An ideal filter leads to **ringing** in the step response.

Ideal filter step response

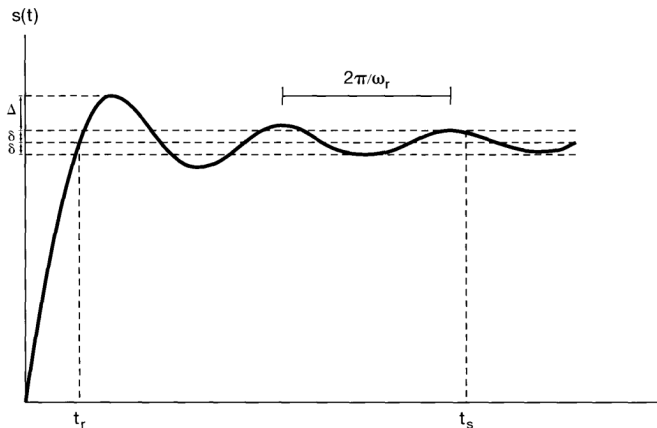
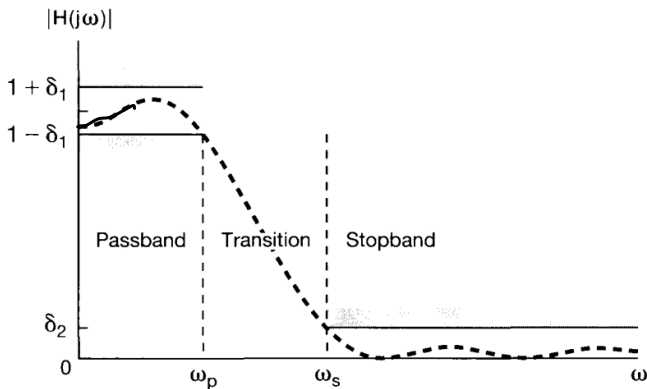


Figure 6.17 Step response of a continuous-time lowpass filter, indicating the rise time t_r , overshoot Δ , ringing frequency ω_r , and settling time t_s —i.e., the time at which the step response settles to within $\pm\delta$ of its final value.

Non-ideal filters

There are **tradeoffs** in filter design. Compromises in the frequency domain can lead to nicer behaviour in the time domain.



$$S(t) = \int_{-\infty}^t h(\tau) d\tau$$

Exercise: What is the step response of a system described by a first-order ODE?

$$T \frac{dy(t)}{dt} + y(t) = x(t)$$

$$H(j\omega) = \frac{1}{1 + j\omega T}$$

$$h(t) = \frac{1}{T} e^{-t/T} u(t)$$

$$s(t) = (1 - e^{-t/T}) u(t)$$

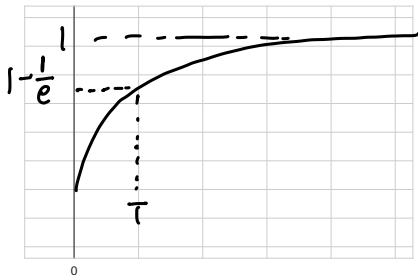
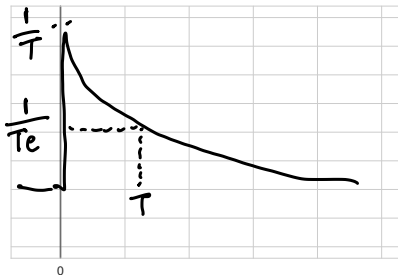
$$\begin{aligned} s(t) &= \int_{-\infty}^t h(\tau) d\tau \\ &= \frac{1}{T} \int_{-\infty}^t e^{-\tau/T} u(\tau) d\tau \\ &= \frac{1}{T} \int_0^t e^{-\tau/T} d\tau \\ &= (1 - e^{-t/T}) u(t) \end{aligned}$$

First-order systems

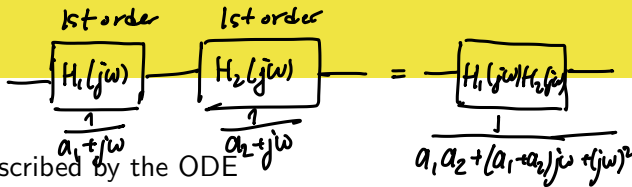
The impulse and step response of the system are

$$h(t) = \frac{1}{T} e^{-t/T} u(t) \quad s(t) = (1 - e^{-t/T}) u(t)$$

T is the **time constant** of the system.



Second-order systems



Consider a system described by the ODE

$$\frac{d^2y(t)}{dt^2} + 2\zeta\omega_n \frac{dy(t)}{dt} + \omega_n^2 y(t) = \omega_n^2 x(t)$$

Exercise: what is the frequency response?

$$\begin{aligned} H(j\omega) &= \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2} \\ &= \frac{1}{(j\omega/\omega_n)^2 + 2\zeta(j\omega/\omega_n) + 1} \end{aligned}$$

Second-order systems

Let's explore this in a little more detail and compute the impulse and step response of this system.

$$\begin{aligned} H(j\omega) &= \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2} \\ &= \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)} \end{aligned}$$

where

$$c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Three cases to consider:

- $\zeta = 1$
- $\zeta > 1$
- $\zeta < 1$

Second-order systems

$$H(j\omega) = \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)}, \quad c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Case: $\zeta = 1$.

$$c_{\pm} = -\zeta\omega_n = -\omega_n$$

$$H(j\omega) = \frac{\omega_n^2}{(j\omega + \omega_n)^2}$$

Use handy table of Fourier transform pairs to find

$$h(t) = \omega_n^2 t e^{-\omega_n t} u(t)$$

$$s(t) = (1 - e^{-\omega_n t} - \omega_n t e^{-\omega_n t}) u(t)$$

Second-order systems

$$H(j\omega) = \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)}, \quad c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Case: $\zeta \neq 1$. Do a partial fraction expansion:

$$\begin{aligned} H(j\omega) &= \frac{A}{j\omega - c_+} + \frac{B}{j\omega - c_-} \\ &= \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \left[\frac{1}{j\omega - c_+} - \frac{1}{j\omega - c_-} \right] \end{aligned}$$

Use table of Fourier transform pairs to find

$$h(t) = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \left(e^{c_+ t} - e^{c_- t} \right) u(t)$$

Second-order systems

$$h(t) = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} (e^{c_+ t} - e^{c_- t}) u(t), \quad c_{\pm} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Exercise: derive the step response,

$$s(t) = \left[1 + \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \left(\frac{e^{c_+ t}}{c_+} - \frac{e^{c_- t}}{c_-} \right) \right] u(t)$$

The form of the exponential depends whether $\zeta > 1$ or $\zeta < 1$

- $\zeta < 1$: c_{\pm} are imaginary; complex exponentials, so the response will oscillate!
- $\zeta > 1$: c_{\pm} real and negative; decaying exponentials

Let's go plot these.

Recall:

$$|Y(j\omega)| = |H(j\omega)| |X(j\omega)|$$
$$\angle Y(j\omega) = \angle H(j\omega) + \angle X(j\omega)$$

Magnitude is multiplicative and phase is additive... would be nicer if both were additive.

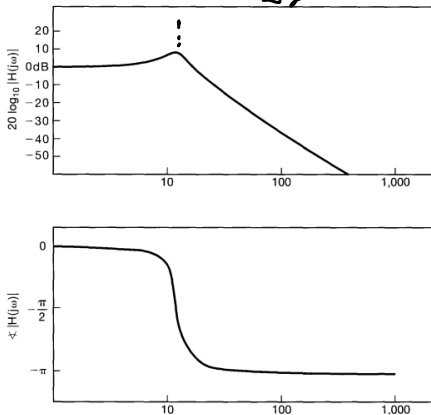
$$\log_{10} |Y(j\omega)| = \log_{10} |H(j\omega)| + \log_{10} |X(j\omega)|$$

Rather than plotting $|H(j\omega)|$ and $\angle H(j\omega)$, it is common to plot $20 \log_{10} |H(j\omega)|$ and $\angle H(j\omega)$ against $\log_{10} \omega$.

Bode plots

These are called *Bode plots*:

$$Q = \frac{1}{2\zeta}$$



The logarithmic scale also allows us to view the response over a much wider range of frequencies.

Bode plots: first-order systems ** We didn't cover this in lecture; just here for reference.*

$$T \frac{dy(t)}{dt} + y(t) = x(t), \quad H(j\omega) = \frac{1}{1 + j\omega T}$$

Let's view these in the magnitude-phase representation:

$$H(j\omega) = \frac{1}{1 + j\omega T} \cdot \frac{1 - j\omega T}{1 - j\omega T} = \frac{1}{(\omega T)^2 + 1} - j \frac{\omega T}{(\omega T)^2 + 1}$$

From this, we find

$$\begin{aligned} |H(j\omega)| &= \frac{1}{\sqrt{(\omega T)^2 + 1}} \\ \angle H(j\omega) &= \tan^{-1}(-\omega T) \end{aligned}$$

Bode plots: first-order systems

We have

$$\begin{aligned}|H(j\omega)| &= \frac{1}{\sqrt{(\omega T)^2 + 1}} \\ \angle H(j\omega) &= \tan^{-1}(-\omega T)\end{aligned}$$

To make our Bode plot, compute

$$\begin{aligned}20 \log_{10} |H(j\omega)| &= 20 \log_{10} \left(\frac{1}{\sqrt{(\omega T)^2 + 1}} \right) \\ &= -20 \log_{10} ((\omega T)^2 + 1)^{1/2} \\ &= -10 \log_{10} ((\omega T)^2 + 1)\end{aligned}$$

Bode plots: first-order systems

$$20 \log_{10} |H(j\omega)| = -10 \log_{10}((\omega T)^2 + 1)$$

If $\omega \ll 1/T$,

$$20 \log_{10} |H(j\omega)| \approx 0$$

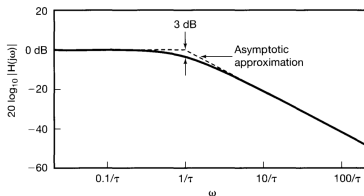
If $\omega \gg 1/T$, $\omega T \gg 1$

$$\begin{aligned} 20 \log_{10} |H(j\omega)| &\approx -10 \log_{10}((\omega T)^2) \\ &= -20 \log_{10}(\omega T) \\ &= -20 \log_{10}(\omega) - 20 \log_{10}(T) \end{aligned}$$

If $\omega = 1/T$,

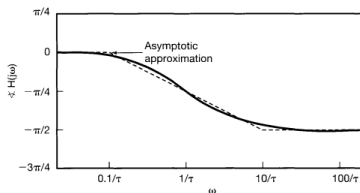
$$\begin{aligned} 20 \log_{10} |H(j\omega)| &= -10 \log_{10}(((1/T)T)^2 + 1) \\ &= -10 \log_{10}(2) \approx -3 \end{aligned}$$

Bode plots: first-order systems



Can make similar approximations to recover plot of phase

$$H(j\omega) = \tan^{-1}(-\omega T)$$



Let's replot the second-order system functions as Bode plots.

For next time

Content:

- Discrete-time Fourier transform

Action items:

1. Tutorial Assignment 3 due Monday 23:59
2. Assignment 3 due next Saturday 23:59

Recommended reading:

- From today's class: Oppenheim 6.1-6.5, 6.7
- Suggested problems: 6.1, 6.3a, 6.5, 6.9, 6.15, 6.21-6.23
- For next class: Oppenheim 5.0-5.7