# ELEC 221 Lecture 16 Time and frequency domain analysis II

Tuesday 1 November 2022

#### Announcements

- Midterms available for pickup at my office
- Quiz 7 today
- Assignment 5 released soon (last one before midterm 2)

#### Important:

- Nov. 8 class on Zoom
- Office hours this Friday and next Friday on Zoom (same time)

Links will be distributed on Canvas.

#### Last time

We formalized the magnitude-phase representation of spectra:

$$H(j\omega) = |H(j\omega)|e^{\not\subset H(j\omega)}$$

#### where

- $|H(j\omega)|$  is the gain
- $\not \subset H(j\omega)$  is the phase shift

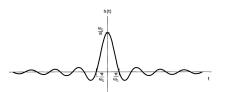
We used these to analyze how systems affect phase:

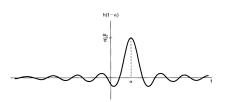
$$|Y(j\omega)| = |H(j\omega)||X(j\omega)|$$
  
 $\not < Y(j\omega) = \not < H(j\omega) + \not < X(j\omega)$ 

#### Last time

We saw how linear shifts in phase affect a system's behaviour:

$$H(j\omega) = \begin{cases} 1, & |\omega| \le \omega_c \\ 0, & |\omega| > \omega_c \end{cases} \qquad H(j\omega) = \begin{cases} e^{-\alpha\omega}, & |\omega| \le \omega_c \\ 0, & |\omega| > \omega_c \end{cases}$$
$$h(t) = \frac{\sin(\omega_c t)}{\pi t} \qquad h(t) = \frac{\sin(\omega_c (t - \alpha))}{\pi (t - \alpha)}$$





#### Last time

We analyzed non-linear shifts by making an approximation that they are linear for small bands of frequencies:

$$\not\subset H(j\omega) \approx -\phi - \alpha\omega$$

We extended this to the idea of group delay:

$$\tau(\omega) = -\frac{d}{d\omega}(\not \subset H(j\omega))$$

# Illustrative example (Oppenheim Ex. 6.1): group delay

Suppose we have some system whose frequency response is

$$H(j\omega) = \prod_{i=1}^{3} H_i(j\omega),$$

$$H_i(j\omega) = \frac{1 + (j\omega/\omega_i)^2 - 2j\zeta_i(\omega/\omega_i)}{1 + (j\omega/\omega_i)^2 + 2j\zeta_i(\omega/\omega_i)},$$

$$\begin{cases} \omega_1 = 315 \text{ rad/sec and } \zeta_1 = 0.066, \\ \omega_2 = 943 \text{ rad/sec and } \zeta_2 = 0.033, \\ \omega_3 = 1888 \text{ rad/sec and } \zeta_3 = 0.058. \end{cases}$$

Actual frequencies:  $f_1 \approx 50$  Hz,  $f_2 \approx 150$  Hz,  $f_3 = 300$  Hz.

Image credit: Oppenheim 6.2

# Illustrative example (Oppenheim Ex. 6.1): group delay

Can find that  $|H(j\omega)| = 1$ , and the phase component is

$$\langle H(j\omega) = -2 \sum_{i=1}^{3} \tan^{-1} \left[ \frac{2\zeta_i(\omega/\omega_i)}{1 - (\omega/\omega_i)^2} \right]$$

# Illustrative example (Oppenheim Ex. 6.1): group delay

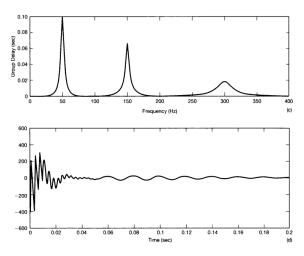


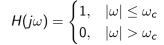
Image credit: Oppenheim 6.2

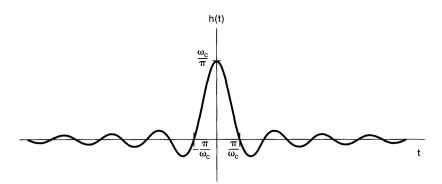
# Today

#### Learning outcomes:

- define and compute the unit step response of a system
- plot frequency response using a Bode plot
- characterize the oscillatory behaviour of CT systems described by second-order differential equations

We will continue to work in CT: you will get practice problems and assignment problems about the DT case (it is very similar).





It is also important to consider step response of filters.

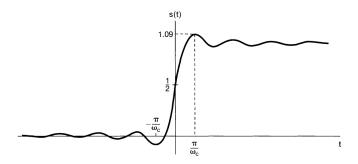
Recall that

$$u(t) = \int_{-\infty}^{t} \delta(\tau) d\tau$$

By linearity, if we put this in a system, the result is

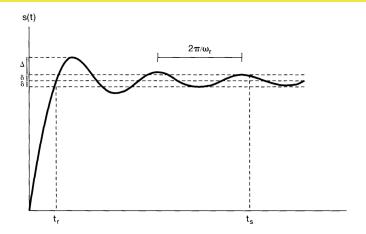
$$s(t) = \int_{-\infty}^{t} h(\tau) d\tau$$

$$s(t) = \int_{-\infty}^{t} h(\tau) d au, \quad h(t) = \frac{\sin(\omega_c t)}{\pi t}$$



An ideal filter leads to **ringing** in the step response.

Image credit: Oppenheim 6.3



**Figure 6.17** Step response of a continuous-time lowpass filter, indicating the rise time  $t_r$ , overshoot  $\Delta$ , ringing frequency  $\omega_r$ , and settling time  $t_s$ —i.e., the time at which the step response settles to within  $\pm \delta$  of its final value.

#### Non-ideal filters

There are **tradeoffs** in filter design. Compromises in the frequency domain can lead to nicer behaviour in the time domain.

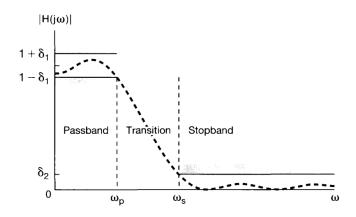


Image credit: Oppenheim 6.4

LTI system described by a first-order ODE:

$$\tau \frac{dy(t)}{dt} + y(t) = x(t)$$

Exercise: what is the frequency response  $H(j\omega)$ ?

Solution: recall the handy formula we derived from the convolution property. Given an arbitrary-order ODE,

$$\sum_{k=0}^{N} \alpha_k \frac{d^k y(t)}{dt^k} = \sum_{k=0}^{M} \beta_k \frac{d^k x(t)}{dt^k}$$

the frequency response is

$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)} = \frac{\sum_{k=0}^{M} \beta_k(j\omega)^k}{\sum_{k=0}^{N} \alpha_k(j\omega)^k}$$

So for our system,

$$H(j\omega) = \frac{1}{1 + j\omega\tau}$$

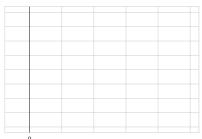
$$\tau \frac{dy(t)}{dt} + y(t) = x(t), \qquad H(j\omega) = \frac{1}{1 + j\omega\tau}$$

The impulse and step response of the system are

$$h(t) = \frac{1}{\tau} e^{-t/T} u(t), \qquad s(t) = (1 - e^{-t\tau}) u(t)$$

au is the **time constant** of the system.





$$au rac{dy(t)}{dt} + y(t) = x(t), \qquad H(j\omega) = rac{1}{1 + j\omega au}$$

Let's view these in the magnitude-phase representation:

$$H(j\omega) = \frac{1}{1+j\omega\tau} \cdot \frac{1-j\omega\tau}{1-j\omega\tau} = \frac{1}{(\omega\tau)^2+1} - j\frac{\omega\tau}{(\omega\tau)^2+1}$$

From this, we find

$$|H(j\omega)| = \frac{1}{\sqrt{(\omega\tau)^2 + 1}}$$
  
 $\not \prec H(j\omega) = \tan^{-1}(-\omega\tau)$ 

Let's plot these in a new way...

#### Bode plots

Recall:

$$|Y(j\omega)| = |H(j\omega)||X(j\omega)|$$
  
 $\not < Y(j\omega) = \not < H(j\omega) + \not < X(j\omega)$ 

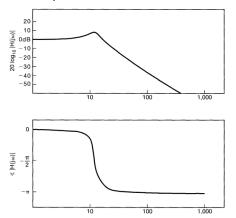
Magnitude is multiplicative and phase is additive... would be nicer if both were additive.

$$\log |Y(j\omega)| = \log |H(j\omega)| + \log |X(j\omega)|$$

Rather than making plots of  $|H(j\omega)|$  and  $\not\subset H(j\omega)$ , it is common to make plots of  $20\log_{10}|H(j\omega)|$  and  $\not\subset H(j\omega)$  against  $\log_{10}\omega$ .

## Bode plots

These are called Bode plots:



The logarithmic scale also allows us to view the response over a much wider range of frequencies.

Image credit: Oppenheim 6.2

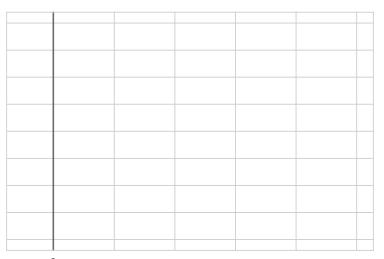
We have

$$|H(j\omega)| = \frac{1}{\sqrt{(\omega\tau)^2 + 1}}$$
  
 $\not \prec H(j\omega) = \tan^{-1}(-\omega\tau)$ 

To make our Bode plot, compute

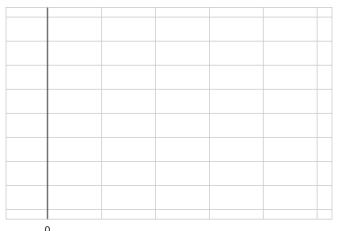
$$20 \log_{10} |H(j\omega)| = 20 \log_{10} \left( \frac{1}{\sqrt{(\omega\tau)^2 + 1}} \right)$$
$$= -20 \log_{10} \left( (\omega\tau)^2 + 1 \right)^{1/2}$$
$$= -10 \log_{10} ((\omega\tau)^2 + 1)$$

$$\begin{aligned} 20\log_{10}|H(j\omega)| &= -10\log_{10}((\omega\tau)^2 + 1) \\ \text{If } \omega &<< 1/\tau, \\ & 20\log_{10}|H(j\omega)| \approx 0 \\ \\ \text{If } \omega >> 1/\tau, \ \omega\tau >> 1 \\ & 20\log_{10}|H(j\omega)| \ \approx \ -10\log_{10}((\omega\tau)^2) \\ & = \ -20\log_{10}(\omega\tau)) \\ & = \ -20\log_{10}(\omega) - 20\log_{10}(\tau) \end{aligned}$$



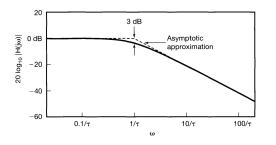
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But that is just an approximation. In reality,



The case of  $\omega = 1/\tau$  has a special name.

$$20 \log_{10}|H(j\omega)| = -10 \log_{10}((\omega \tau)^2 + 1)$$
  
If  $\omega = 1/\tau$ ,  
 $20 \log_{10}|H(j\omega)| = -10 \log_{10}(((1/\tau)\tau)^2 + 1)$   
 $= -10 \log_{10}(2)$   
 $\approx -3$ 



Can make similar approximations to recover plot of the phase

$$H(j\omega) = \tan^{-1}(-\omega\tau)$$

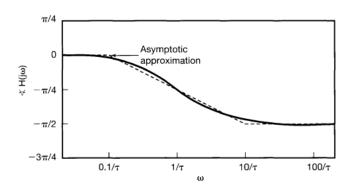


Image credit: Oppenheim 6.5

Consider a system described by the ODE

$$\frac{d^2y(t)}{dt^2} + 2\zeta\omega_n\frac{dy(t)}{dt} + \omega_n^2y(t) = \omega_n^2x(t)$$

Exercise: what is the frequency response?

Let's explore this in a little more detail and compute the impulse and step response of this system.

$$H(j\omega) = \frac{\omega_n^2}{(j\omega)^2 + 2\zeta\omega_n(j\omega) + \omega_n^2}$$
$$= \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)}$$

where

$$c_{\pm} = -\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

Three cases to consider:

- $\zeta = 1$
- $\zeta > 1$

$$H(j\omega) = \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)}, \quad c_{\pm} = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

Case:  $\zeta = 1$ .

$$c_{\pm} = -\zeta \omega_n = -\omega_n$$
 $H(j\omega) = \frac{\omega_n^2}{(j\omega + \omega_n)^2}$ 

Use handy table of Fourier transform pairs to find

$$h(t) = \omega_n^2 t e^{-\omega_n t} u(t)$$

$$H(j\omega) = \frac{\omega_n^2}{(j\omega - c_+)(j\omega - c_-)}, \quad c_{\pm} = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

Case:  $\zeta \neq 1$ . Do a partial fraction expansion:

$$H(j\omega) = \frac{A}{j\omega - c_{+}} + \frac{B}{j\omega - c_{-}}$$

$$= \frac{\omega_{n}}{2\sqrt{\zeta^{2} - 1}} \frac{1}{j\omega - c_{+}} - \frac{\omega_{n}}{2\sqrt{\zeta^{2} - 1}} \frac{1}{j\omega - c_{-}}$$

Use handy table of Fourier transform pairs to find

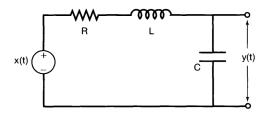
$$h(t) = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \left( e^{c_+ t} - e^{c_- t} \right) u(t)$$

$$h(t) = \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \left( e^{c_+ t} - e^{c_- t} \right) u(t), \qquad c_{\pm} = -\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

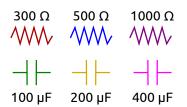
The form of the exponential depends on whether  $\zeta>1$  or  $\zeta<1$ 

- $\zeta < 1$ :  $c_{\pm}$  are imaginary; complex exponentials, so the response will oscillate!
- $\zeta > 1$ :  $c_{\pm}$  real and negative; decaying exponentials

Let's go plot these.

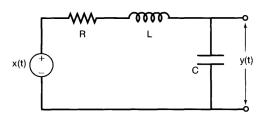


Suppose L = 6 H. We have a box of capacitors and resistors:



What is the best choice to ensure step response doesn't oscillate?

Image credit: Oppenheim P6.19.



First, we need to set up the ODE for the system.

$$V_{TOTAL} = V_R(t) + V_I(t) + V_L(t)$$
$$x(t) = LC \frac{d^2y(t)}{dt^2} + RC \frac{dy(t)}{dt} + y(t)$$

Image credit: Oppenheim P6.19.

$$x(t) = LC\frac{d^2y(t)}{dt^2} + RC\frac{dy(t)}{dt} + y(t)$$

# Today

#### Learning outcomes:

- define and compute the unit step response of a system
- plot frequency response using a Bode plot
- characterize the oscillatory behaviour of CT systems described by second-order differential equations

#### Oppenheim practice problems:

- (DT) 6.35, 6.36, 6.41, 6.42, 6.65
- (CT) 6.15, 6.28 (choose a couple), 6.32, 6.33, 6.53

#### For next time

#### Content:

- The sampling theorem
- Basics of interpolation
- The Nyquist rate and aliasing

#### Action items:

- 1. Work through Oppenheim section 6.5-6.7
- 2. Assignment 5 coming soon
- 3. Midterm 2 in two weeks

#### Recommended reading:

- From this class: Oppenheim 6.4-6.8
- For next class: Oppenheim 7.1-7.3