Chromosome segregation model - detailed description

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Introduction

This is a more detailed version of the kinetochore segregation model to be published in the JCB article, which should be referred to for all the experimental, biological and non-technical aspects of this work.

1 Definitions

1.1 State vector

The mitotic spindle is described by the speeds and position along the x axis of two spindle pole bodies, N chromosomes with two centromeres and M_k attachment sites per centromere.

Positions are noted as follow:

- $\bullet\,$ The left and right spindle pole bodies (SPBs), x_s^L and x_s^R
- The N centromeres, $x_n^A,\,x_n^B,n\in\{1,\cdots,N\}$
- The M_k attachment sites of each centromere, $x_{nm}^A, x_{nm}^B, n \in \{1, \dots, N\}, m \in \{1, \dots, M_k\}$

The speeds are noted with a dot: $dx/dt = \dot{x}$.

As all the interactions are assumed to be parallel to the spindle axis, only the positions along this axis are considered, in a coordinate system with its origin at the center of the spindle, which means that $x_s^L(t) = -x_s^R(t) \, \forall t$.

1.2 Random variables for the attachment

We define ρ_{nm}^A and λ_{nm}^A , two random variables that govern the attachment state of the site x_{nm}^A , such that:

$$\lambda_{nm}^{A} = \begin{cases} 1 & \text{if the site is attached to the left SPB} \\ 0 & \text{otherwise} \end{cases}$$
 (1)

$$\rho_{nm}^{A} = \begin{cases} 1 & \text{if the site is attached to the right SPB} \\ 0 & \text{otherwise} \end{cases}$$
 (2)

Note that ρ^A_{nm} and λ^A_{nm} are not independent, as an attachment site can't be attached to both poles. To take this into account, we can define the variable $\pi^A_{nm} = \rho^A_{nm} - \lambda^A_{nm}$ such that:

$$\pi_{nm}^{A} = \begin{cases} -1 & \text{if the site is attached to the left SPB} \\ 0 & \text{if the site is not attached} \\ 1 & \text{if the site is attached to the right SPB} \end{cases}$$
 (3)

We have:

$$\lambda_{nm}^A = \pi_{nm}^A \left(\pi_{nm}^A - 1 \right) / 2 \tag{4}$$

$$\rho_{nm}^{A} = \pi_{nm}^{A} \left(\pi_{nm}^{A} + 1 \right) / 2 \tag{5}$$

We also define N_n^{AL} and N_n^{AR} as the number of ktMTs of centromere A attached to the left and right SPBs, respectively:

$$N_n^{AL} = \sum_{m=1}^{M_k} \lambda_{nm}^A \text{ and } N_n^{AR} = \sum_{m=1}^{M_k} \rho_{nm}^A$$
 (6)

Note that $N_n^{AL} + N_n^{AR} \leqslant M_k \, \forall \, \pi_{nm}$ The same definitions apply for the centromere B and left SPB.

2 Mechanical system

2.1 Forces

The following force balances are considered:

2.1.1 Forces at the left SPB:

Because of the reference frame definition, $\dot{x_s}^R = -\dot{x_s}^L \, \forall t$. Here we substituted x_s^L with $-x_s^R$

- Friction forces (viscous drag): $F_f^L = \mu_s \dot{x_s}^R$
- Midzone force generators:

$$F_{mid}^{L} = -F_z \left(1 - 2\dot{x}_s^R / V_z \right)$$

• Total kinetochore microtubules force generators:

$$F_{kMT}^{T} = \sum_{n=1}^{N} \sum_{m=1}^{M_k} -\lambda_{nm}^{A} F_k \left(1 + (\dot{x}_{nm}^{A} + \dot{x}_{s}^{R})/V_k \right) -\lambda_{nm}^{B} F_k \left(1 + (\dot{x}_{nm}^{B} + \dot{x}_{s}^{R})/V_k \right)$$

2.1.2 Forces at the right SPB:

- Friction forces (viscous drag): $F_f^R = -\mu_s \dot{x_s}^R$
- Midzone force generators:

$$F_{mid} = F_z \left(1 - (\dot{x}_s^R - \dot{x}_s^L) / V_z \right) = F_z \left(1 - 2\dot{x}_s^R / V_z \right)$$

• Total kinetochore microtubules force generators:

$$F_{kMT}^{T} = \sum_{n=1}^{N} \sum_{m=1}^{M_k} -\rho_{nm}^{A} F_k \left(1 - (\dot{x}_{nm}^{A} - \dot{x}_{s}^{R})/V_k\right) - \rho_{nm}^{B} F_k \left(1 - (\dot{x}_{nm}^{B} - \dot{x}_{s}^{R})/V_k\right)$$

2.1.3 Forces at centromere An

- Drag: $F_c^f = -\mu_c \dot{x_n}^A$
- Cohesin bond (Hook spring) restoring force exerted by centromere¹:

$$F_{BA} = \begin{cases} \kappa_c(x_n^B - x_n^A - d_0) & \text{if} \quad x_n^A \leqslant x_n^B\\ \kappa_c(x_n^B - x_n^A + d_0) & \text{if} \quad x_n^A > x_n^B \end{cases}$$
(7)

With $F_{AB} = -F_{BA}$.

• Total visco-elastic bond between the centromere A and the attachment sites:

$$F_v^T = \sum_{m=1}^{M_k} -\kappa_k (x_n^A - x_{nm}^A) - \mu_k (\dot{x}_n^A - \dot{x}_{nm}^A)$$

2.1.4 Forces at attachment site Anm

• Visco-elastic bond between the centromere A and the attachment sites:

$$F_v = \kappa_k (x_n^A - x_{nm}^A) + \mu_k (\dot{x}_n^A - \dot{x}_{nm}^A)$$

• Kinetochore microtubules force generators:

$$F_{kMT}^{A} = F_{kMT}^{RA} + F_{kMT}^{LA}$$

$$F_{kMT}^{RA} = \rho_{nm}^{A} F_{k} \left(1 - \frac{\dot{x}_{nm}^{A} - \dot{x}_{s}^{R}}{V_{k}} \right)$$

$$F_{kMT}^{LA} = \lambda_{nm}^{A} F_{k} \left(-1 - \frac{\dot{x}_{nm}^{A} - \dot{x}_{s}^{L}}{V_{k}} \right)$$
(8)

With $F_k = 1$ and $V_k = 1$ (for now on, we are taking F_k as unit force and V_k as unit speed), this gives:

$$F_{kMT}^{A} = \rho_{nm}^{A} \left(\dot{x}_{s}^{R} - \dot{x}_{nm}^{A} + 1 \right) - \lambda_{nm}^{A} \left(\dot{x}_{s}^{R} + \dot{x}_{nm}^{A} + 1 \right) \tag{9}$$

Eventually, substituting $\lambda^A_{nm}-\rho^A_{nm}$ with π^A_{nm} and $\lambda^A_{nm}+\rho^A_{nm}$ with $|\pi^A_{nm}|$:

$$F_{kMT}^{A} = \pi_{nm}^{A}(\dot{x}_{s}^{R} + 1) - |\pi_{nm}^{A}|\dot{x}_{nm}^{A}$$
(10)

2.2 Set of coupled first order differential equations

In the viscous nucleoplasm, inertia is negligible. Newton first principle thus reduces to: $\sum F = 0$. This force balance equation can be written for each elements of the spindle. To simplify further, the equations for the right and left SPBs can be combined:

$$-\mu_{s}\dot{x}_{s}^{R} + F_{z}\left(1 - 2\dot{x}_{s}^{R}/V_{z}\right) + \sum_{n,m} -\rho_{nm}^{A}\left(\dot{x}_{s}^{R} - \dot{x}_{nm}^{A} + 1\right) = 0 \text{ for the right SPB}$$

$$\mu_{s}\dot{x}_{s}^{R} - F_{z}\left(1 - 2\dot{x}_{s}^{R}/V_{z}\right) + \sum_{n,m} \lambda_{nm}^{A}\left(\dot{x}_{s}^{R} + \dot{x}_{nm}^{A} + 1\right) = 0 \text{ for the left SPB}$$
(11)

The difference of those two expressions gives, with the same substitutions as before:

¹We want the centromeres to be able to cross each over. In one dimension, this introduces a discontinuity. In the previous version, the 'swap' mechanism was solving this directly (as x_A and x_B are exchanged). This is not possible any more, as the 'swap' mechanism is now irrelevant, as there is no preferred side for a given centromere.

$$-2\mu_s \dot{x}_s^R + 2F_z \left(1 - 2\dot{x}_s^R/V_z\right) + \sum_{n,m} -(|\pi_{nm}^A| + |\pi_{nm}^B|)(\dot{x}_s^R + 1) + \pi_{nm}^A \dot{x}_{nm}^A + \pi_{nm}^B \dot{x}_{nm}^B = 0$$
 (12)

All the equations are gathered together in the system of equations:

$$\mathbf{A}\dot{X} + \mathbf{B}X + C = 0$$

The vector X has $1 + 2N(M_k + 1)$ elements and is defined as follow²:

$$X=\{x_s^R,\{x_n^A,\{x_{nm}^A\},x_n^B,\{x_{nm}^B\}\}\}$$
 with $n\in 1\cdots N$ and $m\in 1\cdots M_k$

In matrix form, we have:

As is actually done in the python implementation, A can be decomposed into a time invariant part A_0 and a variable part A_t with:

(13)

²Note that the left SPB is omitted in X.

For the sake of clarity, B can be decomposed in a kinetochore and a cohesin part, $B = B_c + B_k$:

3 Attachment instability

3.1 Attachment rate

For a detached site ($\pi_{nm}=0$), the probability to attach to a new microtubule in the time interval dt is given by: $P_a=1-\exp(k_a\,dt)$. If an attachment event occurs, it can be to the left SPB with a probability P_L such that:

$$P_L = 1/2 + \beta \frac{N_n^{AL} - N_n^{BL}}{2(N_n^{AL} + N_n^{BL})}$$
 (16)

3.2 Detachment rate

The detachment rate k_d depends on the position of the attachment site with respect to the centromere³:

$$k_d = k_d^0 \frac{d_\alpha}{|(x_{nm}^A + x_{nm}^B)/2 - x_n^A|}$$
(17)

The following expression diverges when $x_{nm}^A = x_n^A$, but this is only means the probability tends to 1. In the simulation code, a cut off value for k_d is given.