

# Chromosome segregation model - detailed description

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## Introduction

This is a more detailed version of the kinetochore segregation model to be published in the JCB article, which should be referred to for all the experimental, biological and non-technical aspects of this work.

## 1 Definitions

### 1.1 State vector

The mitotic spindle is described by the speeds and position along the  $x$  axis of two spindle pole bodies,  $N$  chromosomes with two centromeres and  $M_k$  attachment sites per centromere.

Positions are noted as follow:

- The left and right spindle pole bodies ( SPBs ),  $x_s^L$  and  $x_s^R$
- The  $N$  centromeres,  $x_n^A, x_n^B, n \in \{1, \dots, N\}$
- The  $M_k$  attachment sites of each centromere,  $x_{nm}^A, x_{nm}^B, n \in \{1, \dots, N\}, m \in \{1, \dots, M_k\}$

The speeds are noted with a dot:  $dx/dt = \dot{x}$ .

As all the interactions are assumed to be parallel to the spindle axis, only the positions along this axis are considered, in a coordinate system with its origin at the center of the spindle, which means that  $x_s^L(t) = -x_s^R(t) \forall t$ .

The following force balances are considered:

#### 1.1.1 Forces at the right SPB :

- Friction forces (viscous drag):  $F_s^f = -\mu_s \dot{x}_s^R$
- Midzone force generators (applied at the right SPB):

$$F_{mid} = F_z (1 - (\dot{x}_s^R - \dot{x}_s^L)/V_z) = F_z (1 - 2\dot{x}_s^R/V_z)$$

- Total kinetochore microtubules force generators:

$$\begin{aligned} F_{kMT}^T = & \sum_{n=1}^N \sum_{m=1}^{M_k} -\rho_{nm}^A F_k (1 - (\dot{x}_{nm}^A - \dot{x}_s^R)/V_k) \\ & + \lambda_{nm}^A F_k (1 - (\dot{x}_{nm}^A + \dot{x}_s^R)/V_k) \\ & - \rho_{nm}^B F_k (1 - (\dot{x}_{nm}^B - \dot{x}_s^R)/V_k) \\ & + \lambda_{nm}^B F_k (1 - (\dot{x}_{nm}^B + \dot{x}_s^R)/V_k) \end{aligned}$$

### 1.1.2 Forces at centromere $An$

- Drag:  $F_c^f = -\mu_c \dot{x}_n^A$
- Cohesin bond (Hook spring) restoring force exerted by centromere B:

$$F_{BA} = -\kappa_c(x_n^A - x_n^B - d_0), \text{ with } F_{BA} = -F_{AB}$$

- Total visco-elastic bond between the centromere A and the attachment sites:

$$F_v^T = \sum_{m=1}^{M_k} -\kappa_k(x_n^A - x_{nm}^A) - \mu_k(\dot{x}_n^A - \dot{x}_{nm}^A)$$

### 1.1.3 Forces at attachment site $Anm$

- Visco-elastic bond between the centromere A and the attachment sites:

$$F_v = \kappa_k(x_n^A - x_{nm}^A) + \mu_k(\dot{x}_n^A - \dot{x}_{nm}^A)$$

- Kinetochore microtubules force generators:

$$F_{kMT}^A = \rho_{nm}^A F_k (1 - (\dot{x}_{nm}^A - \dot{x}_s^R)/V_k) - \lambda_{nm}^A F_k (1 - (\dot{x}_{nm}^A - \dot{x}_s^L)/V_k)$$

Here,  $\rho_{nm}^A$  and  $\lambda_{nm}^A$  are two random variables that govern the attachment state of the site  $x_{nm}^A$ , such that:

$$\rho_{nm}^A = \begin{cases} 1 & \text{if the site is attached to the right SPB} \\ 0 & \text{otherwise} \end{cases} \quad (1)$$

$$\lambda_{nm}^A = \begin{cases} 1 & \text{if the site is attached to the left SPB} \\ 0 & \text{otherwise} \end{cases} \quad (2)$$

Note that  $\rho_{nm}^A$  and  $\lambda_{nm}^A$  are not independent, as an attachment site can't be attached to both poles. To take this into account, we can define the variable  $p_{nm}^A = \rho_{nm}^A - \lambda_{nm}^A$  such that:

$$p_{nm}^A = \begin{cases} -1 & \text{if the site is attached to the left SPB} \\ 0 & \text{if the site is not attached} \\ 1 & \text{if the site is attached to the right SPB} \end{cases} \quad (3)$$

We have:

$$\lambda_{nm}^A = p_{nm}^A (p_{nm}^A - 1) / 2 \quad (4)$$

$$\rho_{nm}^A = p_{nm}^A (p_{nm}^A + 1) / 2 \quad (5)$$

We also define  $N_n^{AL}$  and  $N_n^{AR}$  as the number of ktMTs of centromere A attached to the left and right SPBs, respectively:

$$N_n^{AL} = \sum_{m=1}^{M_k} \lambda_{nm}^A \text{ and } N_n^{AR} = \sum_{m=1}^{M_k} \rho_{nm}^A \quad (6)$$

Note that  $N_n^{AL} + N_n^{AR} \leq M_k \forall p_{nm}$  The same definitions apply for the centromere B and left SPB.

## 1.2 Set of first order coupled equations

In the viscous nucleoplasm, inertia is negligible. Newton first principle thus reduces to:  $\sum F = 0$ , all the equations are gathered together in the system of equations:

$$\mathbf{A}\dot{X} + \mathbf{B}X + C = 0$$

The vector  $X$  has  $1 + 2N(M_k + 1)$  elements and is defined as follow:

$$X = \{x_s^R, \{x_n^A, \{x_{nm}^A\}, x_n^B, \{x_{nm}^B\}\}\} \text{ with } n \in 1 \cdots N \text{ and } m \in 1 \cdots M_k$$

With this order, the index of the  $n^{th}$  centromere A, noted  $i_n^A$  is given by  $i_n^A = 2n(M_k + 1) + 2$ . Similarly, we have:

$$\begin{aligned} i_n^B &= 2n(M_k + 1) + M_k + 3 \\ i_{nm}^A &= 2n(M_k + 1) + 3 + m \\ i_{nm}^B &= 2n(M_k + 1) + M_k + 4 + m \end{aligned}$$

To simplify the equations, we set  $F_k$  as unit force and  $V_k$  as unit speed, thus  $F_k/V_k = 1$ . From the above we have:

$$\begin{aligned} A &= \begin{pmatrix} a_{1,1} & \dots & a_{1,i_{nm}^A} & \dots & a_{1,i_{nm}^B} \\ \dots & a_{i_n^A,i_n^A} & a_{i_n^A,i_{nm}^A} & \dots & \\ a_{i_{nm}^A,1} & a_{i_{nm}^A,i_n^A} & a_{i_{nm}^A,i_{nm}^A} & \dots & \\ \dots & \dots & a_{i_n^B,i_n^B} & a_{i_n^B,i_{nm}^B} & \\ a_{i_{nm}^B,1} & \dots & a_{i_n^B,i_{nm}^B} & a_{i_{nm}^B,i_{nm}^B} & \end{pmatrix} \\ &= \begin{pmatrix} -\mu_s - F_z/V_z - \sum(p_{nm}^A + p_{nm}^B) & \dots & p_{nm}^A & \dots & p_{nm}^B \\ \dots & -\mu_c - M_k\mu_k & \mu_k & \dots & \\ p_{nm}^A & \mu_k & -\mu_k + p_{nm}^A & \dots & \\ \dots & \dots & -\mu_c - M_k\mu_k & \mu_k & \\ p_{nm}^B & \dots & \mu_k & -\mu_k + p_{nm}^B & \end{pmatrix}, \quad (7) \\ B &= \begin{pmatrix} 0 & \dots & \dots & \dots & \dots \\ \dots & -\kappa_c - M_k\kappa_k & \kappa_k & \kappa_c & \dots \\ \dots & \kappa_k & -\kappa_k & \dots & \dots \\ \dots & \kappa_c & \dots & -\kappa_c - M_k\kappa_k & \kappa_k \\ \dots & \dots & \kappa_k & -\kappa_k & \end{pmatrix} \quad \text{and} \quad C = \begin{pmatrix} 0 \\ 0 \\ d_0 \\ 0 \\ d_0 \\ 0 \end{pmatrix} \end{aligned}$$