week14-springs

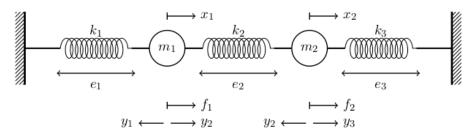
April 23, 2024

- George McNinch Math 87 Spring 2024
- 2 Week 13
- Spring networks
- Modeling spring networks

Examples of "Structural modeling" that will ultimately involve least squares approximation.

One-dimensional models 4.1

Let's consider a linear network of 3 springs and 2 masses:



Here are the variables:

- $f_j=$ applied load or force to mass (in N = Newtons), for j=1,2• $k_i=$ spring constant (in N/m = Newtons per meter), for i=1,2,3
- $e_i = \text{elongation of spring } i \text{ from equilibrium (in } m = meters)$
- $x_j = \text{displasement of mass } j \text{ from equilibrium (in } \mathbf{m} = \mathbf{meters})$
- $y_i = \text{restoring force on spring } i \text{ (in N} = \text{Newtons)}$

The "inputs" are the applied forces f_i which cause the masses to move, resulting in elongation of springs.

We'll take "movement to the right" to be *positive*, and a stretch as *positive* elongation.

Thus we have the equations:

$$e_1 = x_1, \quad e_2 = x_2 - x_1, \quad e_3 = -x_2.$$

(This third equation reflects the fact that spring 3 compresses when m_2 moves to the right.)

Let's put this in matrix form:

$$\mathbf{e} = \begin{bmatrix} e_1 \\ e_2 \\ e_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -1 & 1 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = B\mathbf{x}.$$

Now, let's recall that according to Hooke's Law, the elongation of the spring causes a restoring force on the mass, determined by the *spring constant* $k_i > 0$. Thus we get equations

$$y_j = k_j e_j$$
 for $j = 1, 2, 3$.

In matrix form, these equations read:

$$\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \\ y_3 \end{bmatrix} = \begin{bmatrix} k_1 & 0 & 0 \\ 0 & k_2 & 0 \\ 0 & 0 & k_3 \end{bmatrix} \begin{bmatrix} e_1 \\ e_2 \\ e_3 \end{bmatrix} = K\mathbf{e}.$$

Combining these equations gives

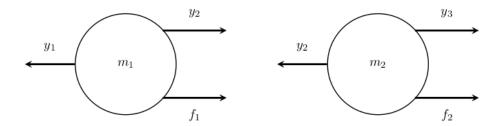
array([[1, 0],

[-1, 1], [0, -1]]))

$$y = Ke = KBx$$
.

```
[15]: import numpy as np
      import numpy.linalg as la
      import sympy as sp
      def sbv(i,n):
          return np.array([1 if j == i else 0 for j in range(n)])
      def makeK(kar):
          n = len(kar)
          return np.array([kar[i]*sbv(i,n) for i in range(n)])
      def makeB(m,n):
          return np.array([(-1)*sbv(i-1,m) + sbv(i,m) for i in range(n)])
      k1, k2, k3 = sp.symbols('k1 k2 k3')
      K = makeK([k1,k2,k3])
      B = makeB(2,3)
      (K,B)
[15]: (array([[k1, 0, 0],
              [0, k2, 0],
              [0, 0, k3]], dtype=object),
```

Next, we assume that the system is at rest after the loads are applied (i.e. the forces f_i).



Looking at the diagram, we see that the following equations must hold:

(The first diagram gives:)

$$\begin{array}{c} y_1 = y_2 + f_1 \implies \\ y_1 - y_2 = f_1 \end{array}$$

(The second diagram gives:)

$$\begin{array}{c} y_2 = y_3 + f_2 \implies \\ y_2 - y_3 = f_2 \end{array}$$

In matrix form this reads

$$\begin{bmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \\ y_3 \end{bmatrix} = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix},$$

i.e.

$$B^T \mathbf{y} = \mathbf{f}$$

Combined with our earlier equation

$$y = Ke = KBx$$

we now see

$$B^T K B \mathbf{x} = \mathbf{f}.$$

Thus we have

$$A=B^TKB=\begin{bmatrix}k_1+k_2 & -k_2 \\ -k_2 & k_2+k_3\end{bmatrix}.$$

```
[16]: def findDisplacements(kar,far):
    # kar = array of spring constants
    # far = array of initial forces.
    m = len(far)
    n = len(kar)
    B = makeB(m,n)
    K = makeK(kar)
    A = B.transpose() @ K @ B
    f = np.array(far)
    return la.solve(A,f)

# Let's find the displacements for spring constants `k = [1,1,1]`
# and forces `f = [3,-3]`

findDisplacements([1,1,1],[3,-3])
```

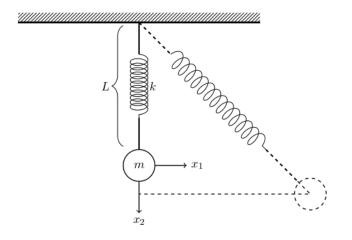
[16]: array([1., -1.])

```
[4]: findDisplacements([1,1,1],[3,-2])
```

[4]: array([1.33333333, -0.33333333])

4.2 Two dimensional models

Now let's allow the mass to move in two dimensions:



L - resting length of spring

k - spring constant

 x_1 - displacement to the right

 x_2 - displacement downward

e - elongation.

We see in this case that the elongation e satisfies

$$e = \sqrt{x_1^2 + (L + x_2)^2} - L$$

Since this does not express a linear relationship between e and the displacements x_1, x_2 , we can't express this relationship using a matrix.

But we can linearize. Recall that the linearization (first-order Taylor polynomial) about t=0 of

the function $y = \sqrt{1+t}$ is given by

(4)
$$\sqrt{1+t} \approx 1 + \frac{t}{2} + O(t^2)$$
.

Let's use this linearization to rewrite the expression for e given above.

We first rewrite

$$\begin{split} x_1^2 + (L + x_2)^2 &= x_1^2 + L^2 + 2Lx_2 + x_2^2 \\ &= L^2 \left(\frac{x_1^2}{L^2} + 1 + \frac{2x_2}{L} + \frac{x_2^2}{L^2} \right) \\ &= L^2 \left(1 + \frac{2x_2}{L} + \frac{x_1^2}{L^2} + \frac{x_2^2}{L^2} \right) \end{split}$$

so that

$$\begin{split} e &= \sqrt{x_1^2 + (L + x_2)^2} - L \\ &= \sqrt{L^2 \left(1 + \frac{2x_2}{L} + \frac{x_1^2}{L^2} + \frac{x_2^2}{L^2} \right)} - L \\ &= L \sqrt{1 + \frac{2x_2}{L} + \frac{x_1^2}{L^2} + \frac{x_2^2}{L^2}} - L \end{split}$$

Now taking $t = \frac{2x_2}{L} + \frac{x_1^2}{L^2} + \frac{x_2^2}{L^2}$ the approximation (4) gives

$$\begin{split} e &\approx L \left(1 + \frac{1}{2}t \right) - L \\ &= L \left(1 + \frac{1}{2} \frac{2x_2}{L} + \frac{x_1^2}{L^2} + \frac{x_2^2}{L^2} \right) - L \\ &= x_2 + \frac{x_1^2 + x_2^2}{2L} \end{split}$$

Now, this is of course still not a linear relationship between e and x_1, x_2 . Note that the approximation (\clubsuit) depends on the assumption that $t = \frac{2x_2}{L} + \frac{x_1^2}{L^2} + \frac{x_2^2}{L^2} \approx 0$.

If we suppose that the displacements x_1, x_2 are small compared to the resting length L of the spring, then $x_1^2 + x_2^2$ is even smaller compared to L, so making one more approximation, we eliminate the quadratic term and so we get

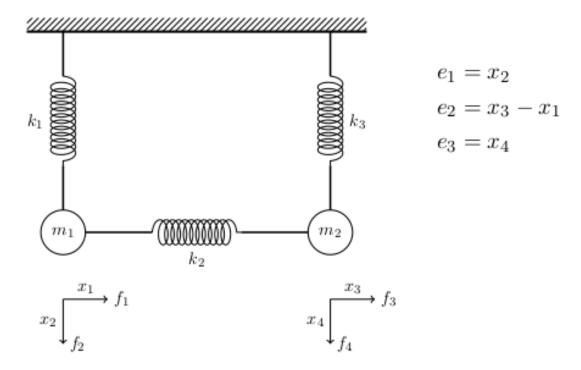
$$e \approx x_2$$
.

Remark The approximation $e \approx x_2$ is equivalent to a small-angle approximation. It essentially says that the horizontal displacements are negligible in the elongation, but vertical displacements are important.

Remark This assumption is of course "wrong", but can still be useful. Especially, it is now linear

4.3 Spring networks

Let's consider a network of springs in the two-dimensional setting.



The *linearization* discussed in the previous section says that the elongation is determined by the displacement in the "1 dimensional direction of the spring".

We get the matrix equation

$$\mathbf{e} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = B\mathbf{x}.$$

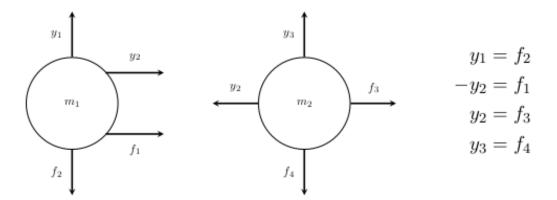
i.e.

$$B = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

As before, Hooke's Law gives

$$\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \\ y_3 \end{bmatrix} = \begin{bmatrix} k_1 & 0 & 0 \\ 0 & k_2 & 0 \\ 0 & 0 & k_3 \end{bmatrix} \begin{bmatrix} e_1 \\ e_2 \\ e_3 \end{bmatrix} = K\mathbf{e}.$$

We see again that the equations to balance the forces come from the transposed matrix B^T :



This gives

$$\begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \mathbf{y} = B^T \mathbf{y} = \mathbf{f}.$$

Thus

$$B^T K B \mathbf{x} = \mathbf{f}.$$

the matrix $B^T K B =$

is singular

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- 5 so we just need to find a non-zero vector in the null space
- 6 now, the Null space of A can be obtained from the *singular* value decomposition of A.
- 7 la.svd(A) returns a tuple (U , S, Vh)
- 8 where e.g. U is a unitary matrix

U,S,Vh = la.svd(A)

9 notice that the last column of U is in the null space:

A@U

```
[75]: nullA = U[:,3]
A @ nullA
```

[75]: array([0., 0., 0., 0.])

[76]: (array([0., 1., 0., 1.]), array([0.70710678, 0. , 0.70710678, 0.]))

Thus we see that the general solution to

$$A\mathbf{x} = \mathbf{f}$$

is given by

$$x = \begin{bmatrix} 0 \\ 1 \\ 0 \\ 1 \end{bmatrix} + t \begin{bmatrix} 1 \\ 0 \\ 1 \\ 0 \end{bmatrix} = \begin{bmatrix} t \\ 1 \\ t \\ 1 \end{bmatrix}.$$

What is the physical meaning of the solutions given by the null space of A? i.e. the solutions

$$t\mathbf{x}_n = t \begin{bmatrix} 1\\0\\1\\0 \end{bmatrix}$$

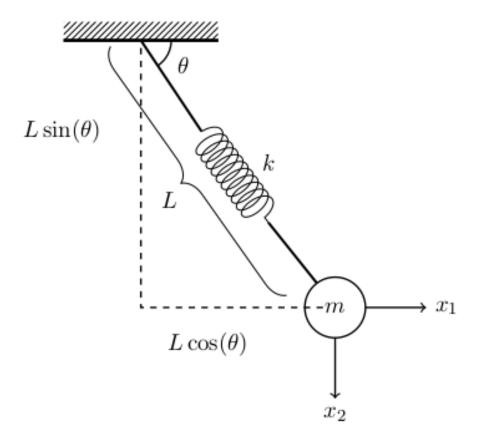
Well, since $A\mathbf{x}_n = \mathbf{0}$, we see that a non-zero displacement can result from application of zero force (!).

This is clearly "wrong", and is a consequence of our linearization, **but** these displacement are referred to as *unstable modes*, and they do correspond to some real physical phenomena –

see e.g. Tacoma bridge collapse (1940)

10 Stabilizing the unstable modes

One way to try to stabilize the unstable modes is to add a diagonal spring:



For the indicate angle θ , the elongation is given by

$$e = \sqrt{(L\cos(\theta) + x_1)^2 + (L\sin(\theta) + x_2)^2}$$

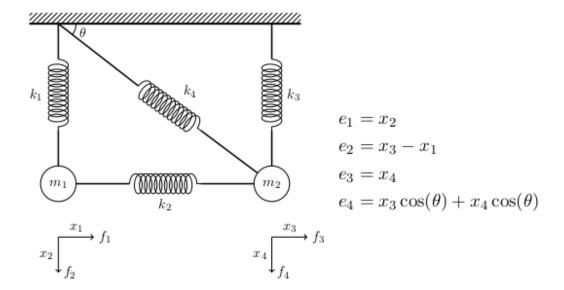
Now our linearization assumption gives

$$e \approx x_1 \cos(\theta) + x_2 \sin(\theta)$$
.

Observe that under the linearization, the elongation is again in the "spring direction".

Note e.g. if
$$\theta=0$$
 then $e=x_1$ and if $\theta=\frac{\pi}{2}$ then $e=x_2$ (as before).

Now return to our unstable network, and add a diagonal spring:

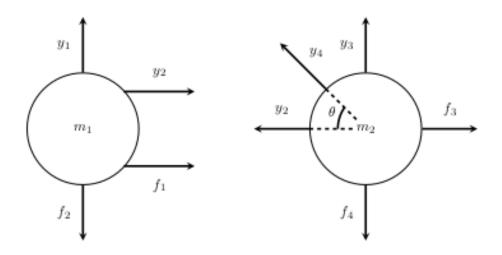


The new parameter here is the elongation $e_4.$

Now we see that $\mathbf{e} = B\mathbf{x}$ where

$$B = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & \cos(\theta) & \sin(\theta) \end{bmatrix}.$$

Let's inspect the force balancing conditions:



As before, we see that

$$B^T\mathbf{y} = \mathbf{f}$$

so that

$$B^T K B \mathbf{x} = \mathbf{f}.$$

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So there are no *unstable modes* for this system. Non-zero displacements \mathbf{x} are only determined by non-zero force vectors \mathbf{f} .

[]: