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INTRODUCTION

- Magnetism plays an integral part in almost every electrical device used today in industry, research, or the home.
- ☐ Generators, motors, transformers, circuit breakers, televisions, computers, tape recorders, and telephones all employ magnetic effects to perform a variety of important tasks.

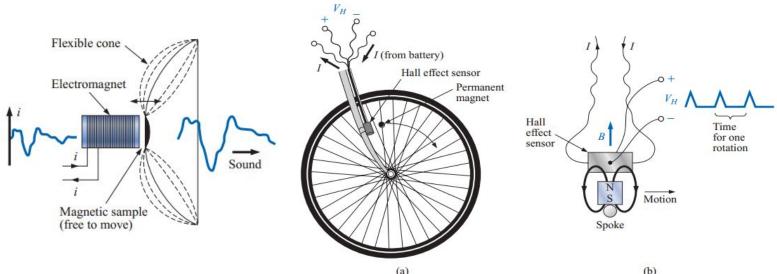


Fig: Speaker

Fig:Obtaining a speed indication for a bicycle using a Hall effect sensor: (a) mounting the components; (b) Hall effect response.

For the first time it was demonstrated that electricity and magnetism were related, and the French physicist André-Marie Ampère performed experiments in this area and developed what is presently known as **Ampère's circuital law.**

- ☐ In the region surrounding a permanent magnet there exists a magnetic field, which can be represented by **magnetic flux lines**
- \square Magnetic flux lines, do not have origins or terminating points. The symbol for magnetic flux is the Greek letter φ (phi).

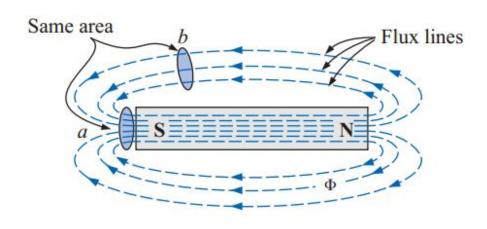


Fig. Flux distribution for a permanent magnet.

☐ When the nonmagnetic material (glass or copper), and magnetic material (soft iron) are placed in the flux paths surrounding a permanent magnet,

there will be an almost unnoticeable change in the flux distribution in non magnetic materials as seen in Fig.

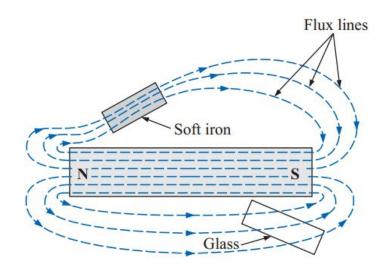
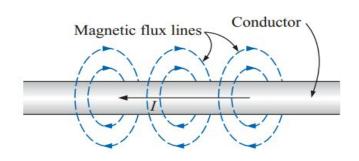
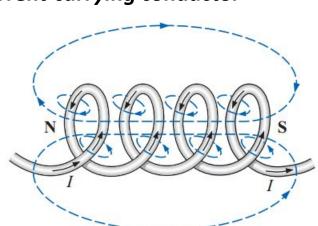


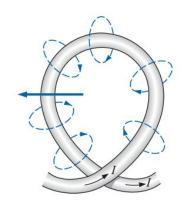
Fig: Effect of a ferromagnetic sample on the flux distribution of a permanent magnet.



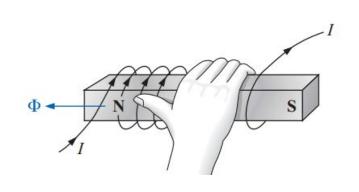
(a) Magnetic flux lines around a current-carrying conductor



(c) Flux distribution of a current-carrying coil.



(b) Flux distribution of a single-turn coil.

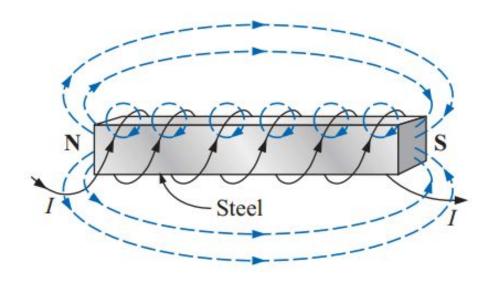


Right-hand rule

The direction of the magnetic flux lines can be found simply by placing the thumb of the *right* hand in the direction of *conventional* current flow and noting the direction of the fingers.

Electromagnet

Electromagnet has all the properties of a permanent magnet, also has a field strength that can be varied by changing one of the component values (current, turns, and so on).



FLUX DENSITY

☐ The number of flux lines per unit area is called the **flux density**, is denoted by the capital letter *B*.

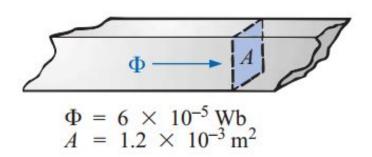
$$B = \frac{\Phi}{A}$$

$$B = \text{teslas (T)}$$

$$\Phi = \text{webers (Wb)}$$

$$A = \text{square meters (m}^2)$$

EXAMPLE.1: For the core of Fig, determine the flux density *B* in teslas.



PERMEABILITY

The permeability (μ) is a measure of the ease with which magnetic flux lines can be established in the material

☐ It is similar in many respects to conductivity in electric circuits.

☐ The ratio of the permeability of a material to that of free space is called its **relative permeability**

$$\mu_r = \frac{\mu}{\mu_o}$$

Permeability of free space $\mu_o = 4\pi \times 10^{-7}$

RELUCTANCE

The resistance of a material to the flow of charge (current) is determined for electric circuits by the equation

$$R = \rho \frac{l}{A}$$
 (ohms, Ω)

☐ The **reluctance** of a material to the setting up of magnetic flux lines in the material is determined by the following equation

$$\Re = \frac{l}{\mu A}$$
 (rels, or At/Wb)

Where I is the length of the magnetic path, and A is the cross-sectional area

OHM'S LAW FOR MAGNETIC CIRCUITS

$$\Phi = \frac{\mathscr{F}}{\Re}$$

The magnetomotive force \mathcal{F} is proportional to the product of the number of turns around the core (in which the flux is to be established) and the current through the turns of wire

$$\mathcal{F} = NI$$
 (ampere-turns, At)

The magnetomotive force per unit length is called the **magnetizing force** (*H*).

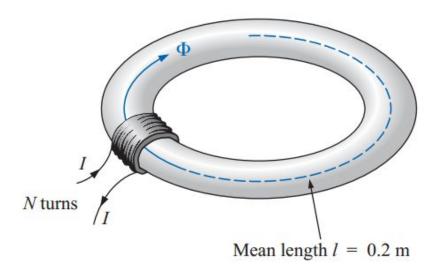
$$H = \frac{\mathcal{F}}{l} \qquad (At/m)$$

Substituting for the magnetomotive force will result in

$$H = \frac{NI}{l}$$
 (At/m)

EXAMPLE.2:

For the magnetic circuit of Fig, if NI = 40 At and length I=0.2 m, then H=?



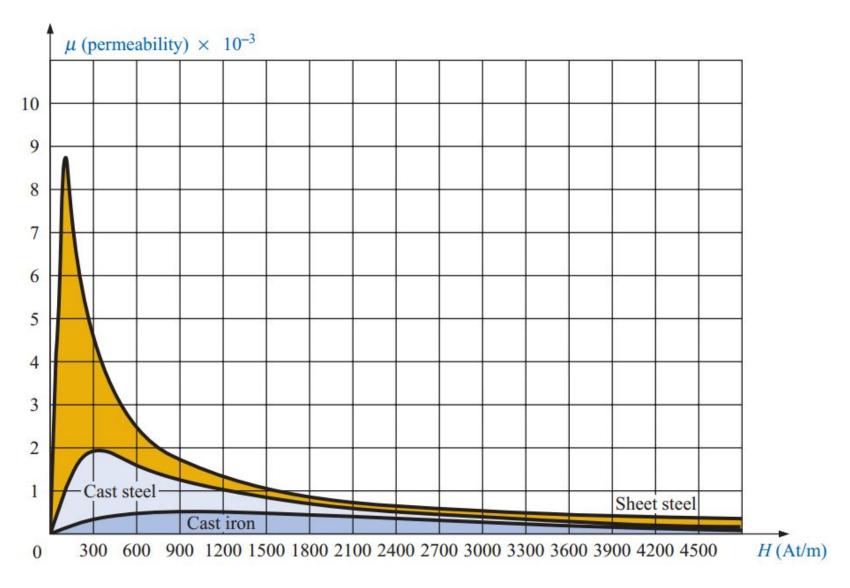
The magnetizing force is independent of the type of core material. It is determined solely by the number of turns, the current, and the length of the core.

☐ The relation between the flux density and the magnetizing force is

$$B = \mu H$$

☐ The applied magnetizing force has a pronounced effect on the resulting permeability of a magnetic material.

As the magnetizing force increases, the permeability rises to a maximum and then drops to a minimum



Magnetizing force (H) vs Permeability

 \Box A curve of the flux density B versus the magnetizing force H of a material is of particular importance to the engineer.

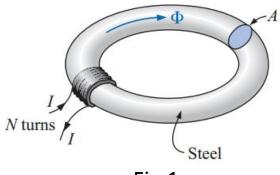


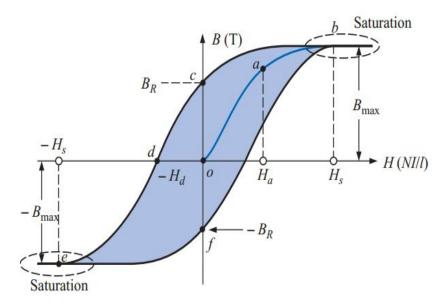
Fig.1

☐ The core is initially unmagnetized and **the current** *I* **= 0**. If the current I is increased to some value above zero, the **magnetizing force H** will increase to a value determined by

$$H \uparrow = \frac{NI \uparrow}{l}$$

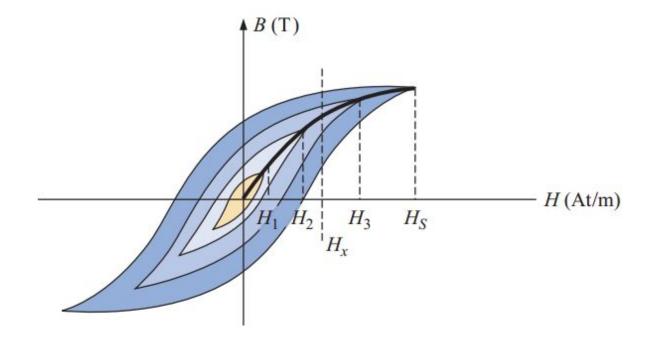
 The flux and the flux density will also increase with the current I (or H)

☐ When saturation occurs, any further increase in current through the coil increasing H will result in a very small increase in flux density B.



- \Box The flux density B_R , which remains when the magnetizing force is zero, is called the *residual flux density*.
- \Box The magnetizing force $-H_d$ required to "coerce" the flux density to reduce its level to zero is called the *coercive force*, a measure of the coercivity of the magnetic sample.

☐ Three hysteresis loops for the same material for maximum values of *H*, less than the saturation value are shown in Fig.



 \square Note from the various curves that for a particular value of H_x , say, H_x , the value of B can vary widely, as determined by the history of the core.

 \square A comparison of Figs. (A) and (B) shows that for the same value of H, the value of B is higher in Fig. (B) for the materials with the higher μ in fig. (A).

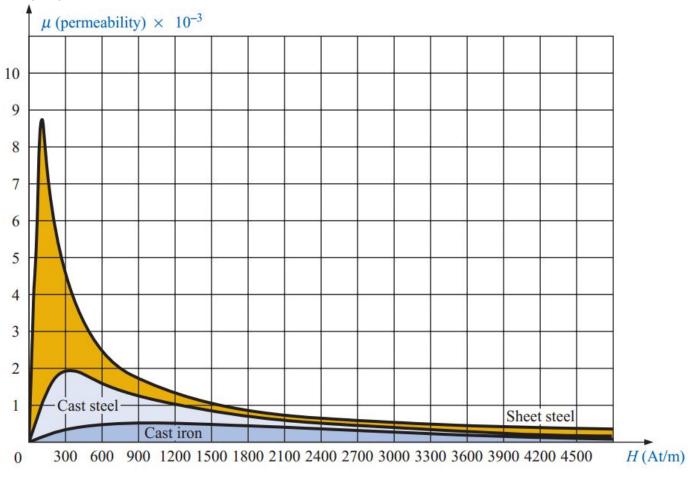


Fig. (A).

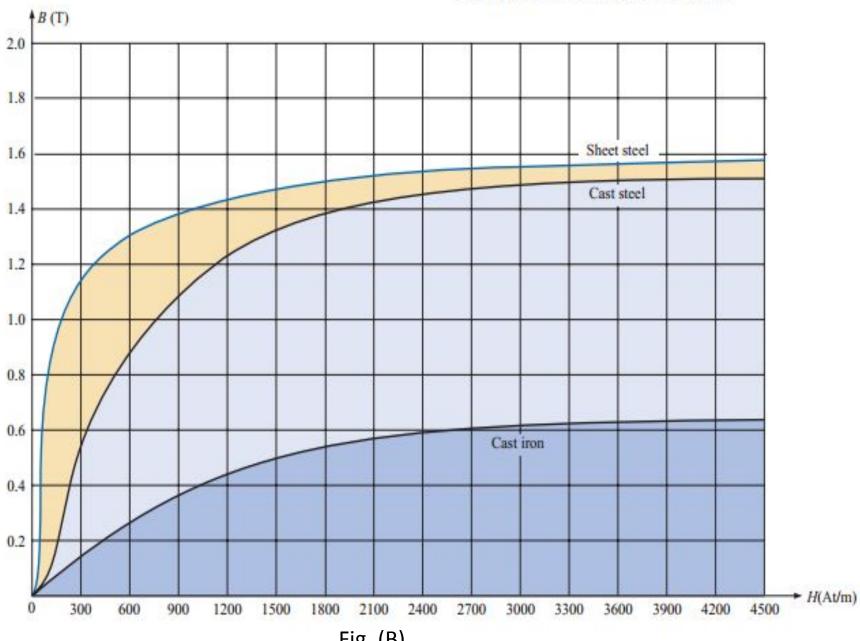


Fig. (B)

There is a broad similarity between the analyses of electric and magnetic circuits

	Electric Circuits	Magnetic Circuits
Cause	E	${\mathcal F}$
Effect	I	Φ
Opposition	R	R

Kirchhoff's voltage law:

The algebraic sum of the rises and drops of the mmf around a closed loop of a magnetic circuit is equal to zero; that is, the sum of the rises in mmf equals the sum of the drops in mmf around a closed loop.

$$\Sigma_{\mathcal{C}} \mathcal{F} = 0$$
 (for magnetic circuits)

$$\Sigma_{\mathbb{C}} \mathcal{F} = 0$$
 (for magnetic circuits)

This equation is referred to as Ampère's circuital law

When it is applied to magnetic circuits,

☐ The sources of mmf are expressed by the equation is

$$\mathcal{F} = NI$$
 (At)

The drop mmf across a portion of a magnetic circuit is expressed by the equation

$$\mathcal{F} = \Phi \mathcal{R}$$
 (At) or $\mathcal{F} = Hl$ (At)

EXAMPLE.3:

consider the magnetic circuit appearing in Fig. constructed of three different ferromagnetic materials.

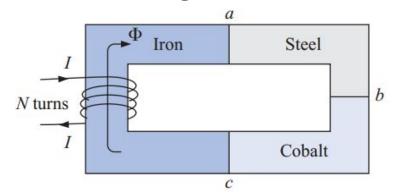


FIG. Series magnetic circuit of three different materials.

☐ Applying Ampère's circuital law, we have

$$\Sigma_{\mathbb{C}} \mathcal{F} = 0$$

$$\underbrace{+NI}_{\text{Rise}} - \underbrace{H_{ab}l_{ab}}_{\text{Drop}} - \underbrace{H_{bc}l_{bc}}_{\text{Drop}} - \underbrace{H_{ca}l_{ca}}_{\text{Drop}} = 0$$

$$\underbrace{NI}_{\text{Impressed}} = \underbrace{H_{ab}l_{ab} + H_{bc}l_{bc} + H_{ca}l_{ca}}_{\text{mmf drops}}$$

Kirchhoff's current law:

The sum of the fluxes entering a junction is equal to the sum of the fluxes leaving a junction

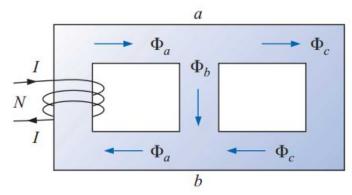


FIG. Flux distribution of a series-parallel magnetic network

$$\Phi_a = \Phi_b + \Phi_c \qquad \text{(at junction } a\text{)}$$

$$\Phi_b + \Phi_c = \Phi_a \qquad \text{(at junction } b\text{)}$$

Both of which are equivalent.

Series magnetic circuits in which the flux ϕ is the same throughout

An approach frequently employed in the analysis of magnetic circuits is the table method.
Before a problem is analyzed in detail, a table is prepared listing in the extreme left-hand column the various sections of the magnetic circuit.
The columns on the right are reserved for the quantities to be found for each section.
Now we will see some of the series magnetic circuits and find the magnitude of the magnetomotive force of magnetic circuit.

EXAMPLE.4:

For the series magnetic circuit of Fig. (i):

- a. Find the value of I required to develop a magnetic flux of $\emptyset = 4 \times 10^{-4}$ Wb.
- b. Determine μ and μ_r for the material under these conditions.

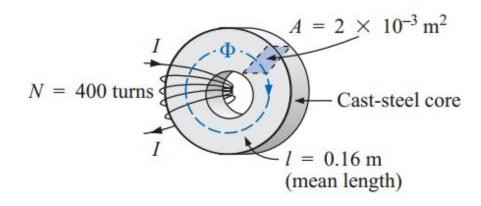


Fig. (i)

Solution:

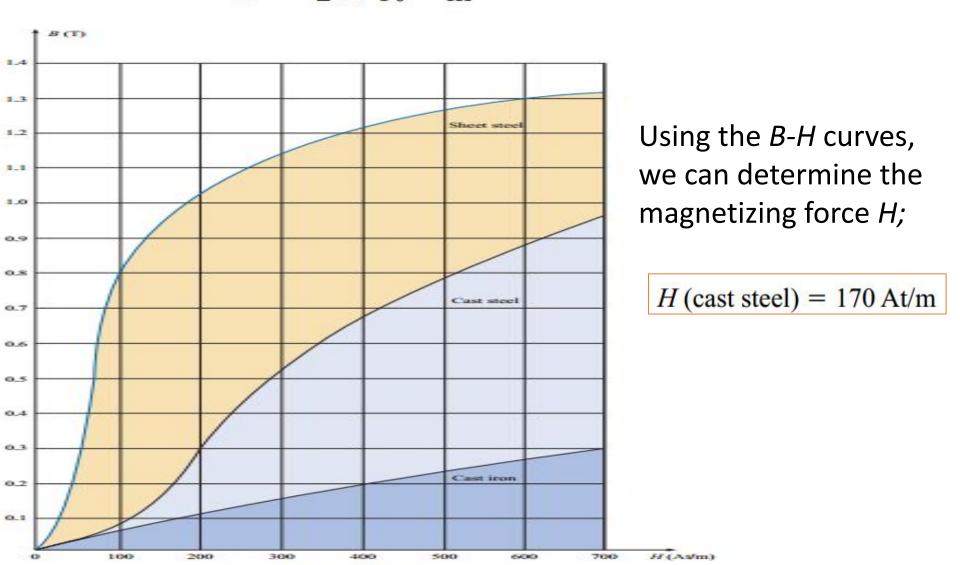


Fig:(a) Magnetic circuit equivalent and (b) electric circuit analogy.

Section	Φ (Wb)	$A (m^2)$	B (T)	H (At/m)	<i>l</i> (m)	Hl (At)
One continuous section	4 × 10 ⁻⁴	2×10^{-3}			0.16	

(a) The flux density B is

$$B = \frac{\Phi}{A} = \frac{4 \times 10^{-4} \text{ Wb}}{2 \times 10^{-3} \text{ m}^2} = 2 \times 10^{-1} \text{ T} = 0.2 \text{ T}$$



Applying Ampère's circuital law yields

$$NI = Hl$$

$$I = \frac{Hl}{N} = \frac{(170 \text{ At/m})(0.16 \text{ m})}{400 \text{ t}} = 68 \text{ mA}$$

(Recall that t represents turns.)

(b) The permeability of the material

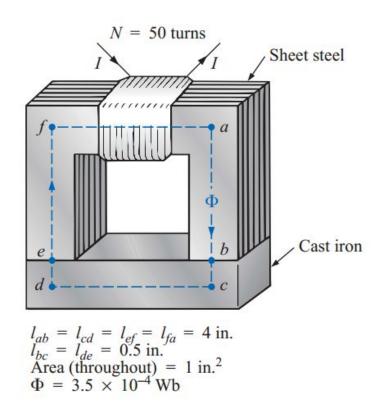
$$\mu = \frac{B}{H} = \frac{0.2 \text{ T}}{170 \text{ At/m}} = 1.176 \times 10^{-3} \text{ Wb/A} \cdot \text{m}$$

the relative permeability is

$$\mu_r = \frac{\mu}{\mu_o} = \frac{1.176 \times 10^{-3}}{4\pi \times 10^{-7}} = 935.83$$

PROBLEM.1:

The electromagnet of Fig. has picked up a section of cast iron. Determine the current *I* required to establish the indicated flux in the core.



To solve this problem, Use these B-H curve to get H values for corresponding B values

H (sheet steel, Fig. 11.24) \cong 70 At/m H (cast iron, Fig. |11.23) \cong 1600 At/m

- The spreading of the flux lines outside the common area of the core for the air gap in Fig. (a) is known as fringing.
- ☐ For our purposes, we shall neglect this effect and assume the flux distribution to be as in Fig.(b).

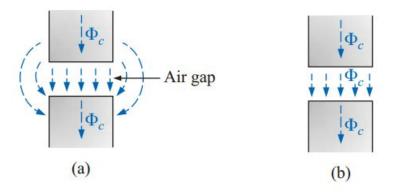


Fig. Air gaps: (a) with fringing; (b) ideal

☐ The average flux density in the air-gap is slightly less than the flux density in the core i.e., $(B_g)_{(av)} < B_c$.

$$B_g = \frac{\Phi_g}{A_g}$$

☐ The flux density of the air gap in Fig.(b) is given by

$$\Phi_g = \Phi_{\text{core}}$$

$$A_g = A_{\text{core}}$$

☐ For most practical applications, **the permeability of air** is taken to be equal to that of **free space**. The magnetizing force of the air gap is then determined by

$$H_g = \frac{B_g}{\mu_o}$$

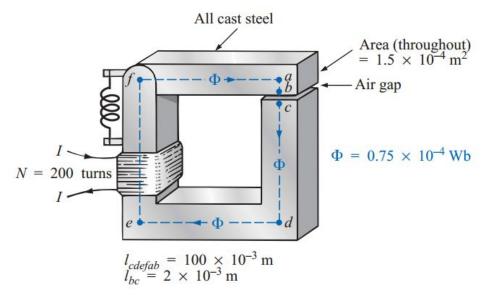
 \square The mmf drop across the air gap is equal to $H_g I_g$. An equation for H_a is as follows:

$$H_g = \frac{B_g}{\mu_o} = \frac{B_g}{4\pi \times 10^{-7}}$$

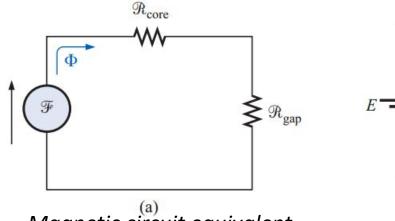
$$H_g = (7.96 \times 10^5) B_g$$
 (At/m)

EXAMPLE.5:

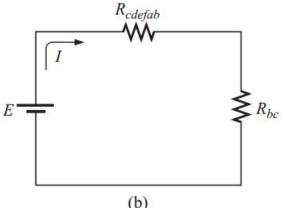
Find the value of I required to establish a magnetic flux of $\emptyset = 0.75 \times 10^{-6}$ 10^{-4} Wb in the series magnetic circuit of Fig.



Solution:



Magnetic circuit equivalent



Electric circuit analogy

The flux density for each section is $B = \frac{\Phi}{A} = \frac{0.75 \times 10^{-4} \text{ Wb}}{1.5 \times 10^{-4} \text{ m}^2} = 0.5 \text{ T}$

From the *B-H* curves, H (cast steel) $\cong 280 \text{ At/m}$

An equation for $H_q = (7.96 \times 10^5)B_g$ (At/m)

$$H_g = (7.96 \times 10^5)B_g = (7.96 \times 10^5)(0.5 \text{ T}) = 3.98 \times 10^5 \text{ At/m}$$

The mmf drops are

$$H_{\text{core}}l_{\text{core}} = (280 \text{ At/m})(100 \times 10^{-3} \text{ m}) = 28 \text{ At}$$

$$H_g l_g = (3.98 \times 10^5 \,\text{At/m})(2 \times 10^{-3} \,\text{m}) = 796 \,\text{At}$$

Applying Ampere's circuital law,

$$NI = H_{\text{core}}l_{\text{core}} + H_g l_g = 28 \text{ At} + 796 \text{ At}$$

$$(200 \text{ t})I = 824 \text{ At}$$

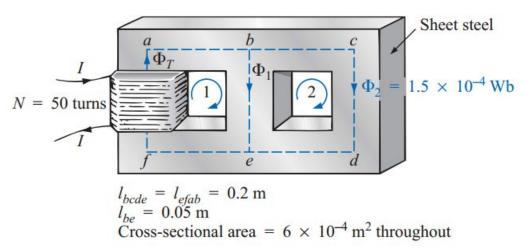
 $I = 4.12 \text{ A}$

Note from the above that the air gap requires the biggest share (by far) of the impressed NI due to the fact that air is nonmagnetic.

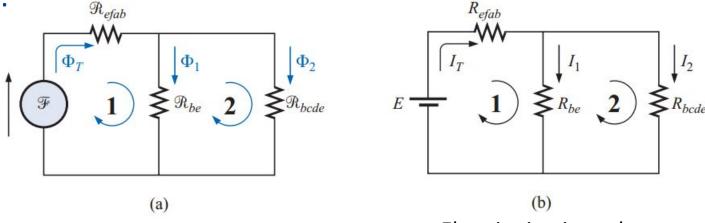
SERIES-PARALLEL MAGNETIC CIRCUITS

EXAMPLE.6:

Determine the current I required to establish a flux of $\emptyset = 1.5 \times 10^{-4}$ Wb in the section of the core indicated in Fig.



Solution:



Magnetic circuit equivalent

Electric circuit analogy

$$B_2 = \frac{\Phi_2}{A} = \frac{1.5 \times 10^{-4} \text{ Wb}}{6 \times 10^{-4} \text{ m}^2} = 0.25 \text{ T}$$

Applying Ampère's circuital law around loop 2

$$\Sigma_{C} \mathcal{F} = 0$$

$$H_{be}l_{be} - H_{bcde}l_{bcde} = 0$$

$$H_{be}(0.05 \text{ m}) - (40 \text{ At/m})(0.2 \text{ m}) = 0$$

$$H_{be} = \frac{8 \text{ At}}{0.05 \text{ m}} = 160 \text{ At/m}$$

From BH Curve:

$$B_1 \cong 0.97 \text{ T}$$

$$\Phi_1 = B_1 A = (0.97 \text{ T})(6 \times 10^{-4} \text{ m}^2) = 5.82 \times 10^{-4} \text{ Wb}$$

Table

Section	Φ (Wb)	$A (m^2)$	B (T)	H (At/m)	<i>l</i> (m)	Hl (At)
bcde be efab	$1.5 \times 10^{-4} \\ 5.82 \times 10^{-4}$	6×10^{-4} 6×10^{-4} 6×10^{-4}	0.25 0.97	40 160	0.2 0.05 0.2	8

The table reveals that we must now turn our attention to section *efab*:

$$\Phi_T = \Phi_1 + \Phi_2 = 5.82 \times 10^{-4} \text{ Wb} + 1.5 \times 10^{-4} \text{ Wb}$$

$$= 7.32 \times 10^{-4} \text{ Wb}$$

$$B = \frac{\Phi_T}{A} = \frac{7.32 \times 10^{-4} \text{ Wb}}{6 \times 10^{-4} \text{ m}^2}$$

$$= 1.22 \text{ T}$$

From B-H Graph $H_{efab}\cong 400~\mathrm{At}$

Applying Ampère's circuital law,

$$+NI - H_{efab}l_{efab} - H_{be}l_{be} = 0$$

 $NI = (400 \text{ At/m})(0.2 \text{ m}) + (160 \text{ At/m})(0.05 \text{ m})$
 $(50 \text{ t})I = 80 \text{ At} + 8 \text{ At}$
 $I = \frac{88 \text{ At}}{50 \text{ t}} = 1.76 \text{ A}$

To demonstrate that μ is sensitive to the magnetizing force H,

☐ The permeability of each section is determined as follows.

For section bcde,

$$\mu = \frac{B}{H} = \frac{0.25 \text{ T}}{40 \text{ At/m}} = 6.25 \times 10^{-3}$$

$$\mu = \frac{B}{H} = \frac{0.97 \text{ T}}{160 \text{ At/m}} = 6.06 \times 10^{-3}$$

$$\mu_r = \frac{\mu}{\mu_o} = \frac{6.25 \times 10^{-3}}{12.57 \times 10^{-7}} = 4972.2$$

$$\mu_r = \frac{\mu}{\mu_o} = \frac{6.06 \times 10^{-3}}{12.57 \times 10^{-7}} = 4821$$

For section efab,

$$\mu = \frac{B}{H} = \frac{1.22 \text{ T}}{400 \text{ At/m}} = 3.05 \times 10^{-3}$$

$$\mu_r = \frac{\mu}{\mu_o} = \frac{3.05 \times 10^{-3}}{12.57 \times 10^{-7}} = 2426.41$$

PROBLEMS.2&3:

Calculate the magnetic flux ϕ for the magnetic circuit of Fig. (a) and (b)

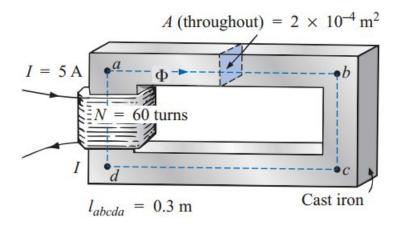


Fig.(a)

Cast iron

Air gap 0.001 m $N = 100 \text{ turns } l_{\text{core}} = 0.16 \text{ m}$

Fig.(b)

Use the B-H Curves to solve this problems