

## Assignment - 5

Q. 2

1. (a) ideal gas law model.

$$PV = RT$$

$$\Rightarrow P = \frac{RT}{V}$$

$$\therefore \underline{W} = - \int P dV \quad \left[ \underline{W} \text{ is work done per mole} \right]$$

$$= - \int \frac{RT}{V} dV$$

$$= - RT \ln \frac{V_2}{V_1}$$

$$= - (8.314) (1000) \ln \left( \frac{1}{10} \right)$$

$$= 8.314 \times 1000 \times \ln 10$$

$$= 19143.69 \text{ J/mole.}$$

$$\therefore \text{Total workdone} = n \underline{W} = 2 \times 19143.69$$

$$= \boxed{38287.38 \text{ J}} \quad \text{or, } \boxed{38.287 \text{ KJ}}$$

(b) R-K equation:

$$P = \frac{RT}{V-b} - \frac{a}{T^{1/2} V(V+b)}$$

$$a = 14.24 \frac{\text{J K}^{1/2} \text{m}^3}{\text{mol}^2}$$

$$b = 2.11 \times 10^{-5} \frac{\text{m}^3}{\text{mol}}$$

$$V_{\text{initial}} = \frac{10}{2} = 5 \frac{\text{Litre}}{\text{mol}} = 0.005 \frac{\text{m}^3}{\text{mol}}$$

$$V_{\text{final}} = \frac{1}{2} = 0.5 \frac{\text{Litre}}{\text{mol}} = 0.0005 \frac{\text{m}^3}{\text{mol}}$$

$$\begin{aligned}
 \underline{W} &= - \int_{V_{\text{initial}}}^{V_{\text{final}}} P dV \\
 &= - \int_{V_{\text{initial}}}^{V_{\text{final}}} \frac{RT}{V-b} dV + \int_{V_{\text{initial}}}^{V_{\text{final}}} \frac{a}{T^{1/2} V(V+b)} dV \\
 &= -RT \ln \left| \frac{V_{\text{final}} - b}{V_{\text{initial}} - b} \right| + \frac{a}{T^{1/2} b} \int_{V_{\text{initial}}}^{V_{\text{final}}} \frac{(V+b) - V}{V(V+b)} dV \\
 &= RT \ln \left| \frac{0.005 - 2.11 \times 10^{-5}}{0.0005 - 2.11 \times 10^{-5}} \right| + \frac{a}{T^{1/2} b} \int_{V_{\text{initial}}}^{V_{\text{final}}} \frac{dV}{V} - \frac{a}{T^{1/2} b} \int_{V_{\text{initial}}}^{V_{\text{final}}} \frac{dV}{V+b} \\
 &= 19467.002 + \frac{14.24}{(1000)^{1/2} (2.11 \times 10^{-5})} \ln \frac{0.0005}{0.005} \\
 &\quad - \frac{14.24}{(1000)^{1/2} (2.11 \times 10^{-5})} \ln \left| \frac{0.0005 + 2.11 \times 10^{-5}}{0.005 + 2.11 \times 10^{-5}} \right| \\
 &= 19467.002 - 21341.63 \ln 10 + 21341.63 (2.26546) \\
 &= 18674.74 \text{ J/mol}
 \end{aligned}$$

$\therefore$  Total work done =  $2 \underline{W} = 2 \times 18674.74$

$$= \boxed{37349.484 \text{ J}} \text{ or } \boxed{37.349 \text{ kJ}}$$

(c) From first law of Thermodynamics,  $\Delta U = Q + W$

$$W = \Delta U - Q.$$

$$W = \Delta U = T \Delta S \quad (\text{since, Process is reversible})$$

$$W_{12} = (U_2 - U_1) - T(S_2 - S_1)$$

To use steam tables, we need to know initial and final Pressure.

Let it's calculated using Redlich-Kwong equation of state.

$$\therefore P_{\text{initial}} = \frac{RT}{v_{\text{initial}} - b} - \frac{a}{T^{1/2} v_{\text{in}}(v_{\text{in}} + b)}$$

$$= \frac{(8.314)(1000)}{0.005 - 2.11 \times 10^{-5}} - \frac{14.24}{(1000)^{1/2} (0.005)(0.005 + 2.11 \times 10^{-5})}$$

$$\begin{aligned} &= 1669846.75 - 17936.64 \\ &= 1651910.11 \text{ Pa.} \\ &= 1.65 \text{ MPa} \end{aligned}$$

Similarly  $P_{\text{final}}$  can also be calculated using RK EOS by putting

$$v = v_{\text{final}} = 0.0005$$

$$P_{\text{final}} = 15.6 \text{ MPa.}$$

From steam table at  $P = 1.65 \text{ MPa}$  and  $T = 1000 \text{ K}$ ,

$$\underline{u}_1 = 3522.6 \text{ kJ/kg} \quad \underline{s}_1 = 8.101 \frac{\text{kJ}}{\text{kg K}}$$

at  $P = 15.6 \text{ MPa}$  and  $T = 1000 \text{ K}$ .

$$\underline{u}_2 = 3462.2 \frac{\text{kJ}}{\text{kg}} \quad \underline{s}_2 = 7 \frac{\text{kJ}}{\text{kg K}}$$

$$\begin{aligned} \therefore \underline{w}_{12} &= (3462.2 - 3522.6) - 1000(7 - 8.101) \\ &= -60.4 + 1101 \\ &= 1040.6 \text{ kJ/kg} \end{aligned}$$

$$\therefore 2 \text{ mol water} = 0.036 \text{ kg}$$

$$\therefore \text{Total work done} = 0.036 * 1040.6$$

$$= \boxed{37.462 \text{ kJ}}$$

Part (a) has significant difference from Part (b) and (c).

Hence, Redlich-Kwong EOS or steam table is much accurate to calculate work done. Compared to ideal gas law.

2. For oxygen Van der Waal constants are as follows:

$$a = 0.138 \text{ Pa} \cdot \frac{\text{m}^6}{\text{mol}^2}$$

$$b = 32.6 \times 10^{-6} \text{ m}^3/\text{mol}$$

$$\text{where, } P = \frac{RT}{V-b} - \frac{a}{V^2}$$

$$\text{For } T_r = 0.95, \quad V_{r,L} = 0.68 \quad \text{and} \quad V_{r,g} = 1.7$$

(From figure 9.15)

$$\text{where, } T_r = \frac{T}{T_c}; \quad V_{r,L} = \frac{V^L}{V_{cr}}; \quad V_{r,g} = \frac{V^g}{V_{cr}}$$

$$\text{For Van der Waal, } V_{cr} = 3b$$

$$\therefore V^L = (0.68)(3 \times 32.6 \times 10^{-6}) = \cancel{65.28 \times 10^{-6} \text{ m}^3} \quad 66.504 \times 10^{-6} \text{ m}^3/\text{mol}$$

$$V^g = (1.7)(3 \times 32.6 \times 10^{-6}) = 166.26 \times 10^{-6} \text{ m}^3/\text{mol}$$

$$V = 200 \text{ cm}^3$$

$$= \frac{200 \times 10^{-6} \text{ m}^3}{2 \text{ mol}} = 10^{-4} \text{ m}^3/\text{mol}$$

$$\therefore x = \frac{V - V^L}{V^g - V^L} = \frac{10^{-4} - 66.504 \times 10^{-6}}{(166.26 - 66.504) \times 10^{-6}}$$

$$= 0.336$$

$$n_g = \text{mole number in Vapour Phase} = 2 \times 0.336 = \boxed{0.672 \text{ mole}}$$

$$n_L = \text{mole " " Liquid Phase} = 2 \times (1 - 0.336) = \boxed{1.328 \text{ mole}}$$

$$V_g = \text{volume " " Gas Phase} = 0.672 \times 166.26 = \boxed{111.73 \text{ cm}^3}$$

$$\therefore V_L = (200 - 111.73) = \boxed{88.27 \text{ cm}^3}$$



3. At triple Point all three Phases Coexist.

$$\therefore 24.38 - \frac{3063}{T_{tp}} = 27.92 - \frac{3754}{T_{tp}}$$

$$\Rightarrow \frac{3754 - 3063}{T_{tp}} = 27.92 - 24.38$$

$$\Rightarrow \frac{691}{T_{tp}} = 3.54$$

$$\Rightarrow \boxed{T_{tp} = 195.2 \text{ K}}$$

$$\therefore \ln p_{tp} = 24.38 - \frac{3063}{195.2} = 9$$

$$\Rightarrow P_{tp} = 5933.69 \text{ Pa} \approx \boxed{5.4 \text{ kPa}}$$

Latent heat of Sublimation,  $\Delta H_{sg} = 3754 R = (3754)(8.314)$

$$= \boxed{31210.756 \text{ J/mol}}$$

- latent heat of vapourization,  $\Delta H_{lg} = 3063 R = (3063)(8.314)$

$$= \boxed{25465.782 \text{ J/mol}}$$

[4] Van der Waals Eos is given as

$$P = \frac{RT}{V-b} - \frac{a}{V^2}, \quad N=1$$

→ One of the physical consequence of thermal stability is

$$k_T > 0$$

As we know;

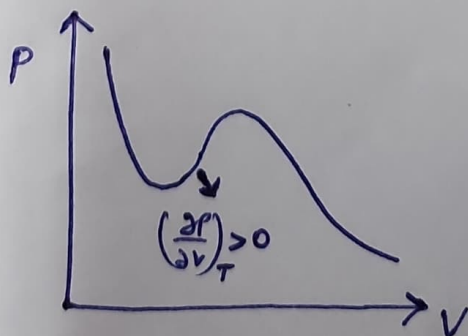
$$k_T = -\frac{1}{V} \left( \frac{\partial P}{\partial V} \right)_T \quad \text{--- (1)}$$

For Van der Waals Eos;

$$k_T = \left( -\frac{1}{V} \right) \left[ -\frac{RT}{(V-b)^2} + \frac{2a}{V^3} \right]$$

$$k_T = \frac{RT}{V(V-b)^2} + \frac{2a}{V^4}$$

→ Now, when  $\left( \frac{\partial P}{\partial V} \right)_T > 0 \Rightarrow k_T < 0 \Rightarrow$  This refers to instability



### Van der Waals EOS

$$5. \quad P = \frac{RT}{V-b} - \frac{a}{V^2}$$

$$\Rightarrow \frac{PV}{RT} = \frac{V}{V-b} - \frac{a}{RTV} = \frac{1}{1 - \frac{b}{V}} - \frac{a}{RTV}$$

We know,

$$\frac{1}{1-x} = 1 + x + x^2 + x^3 + \dots$$

$$\frac{1}{1 - \frac{b}{V}} = 1 + \frac{b}{V} + \left(\frac{b}{V}\right)^2 + \left(\frac{b}{V}\right)^3 + \dots$$

$$\therefore \frac{PV}{RT} = 1 + \frac{b - \frac{a}{RT}}{V} + \left(\frac{b}{V}\right)^2 + \left(\frac{b}{V}\right)^3 + \dots$$

$$= 1 + \frac{B}{V} + \frac{C}{V^2} + \dots$$

$\therefore$  Second virial coefficient,  $B = b - \frac{a}{RT}$

Third virial coefficient,  $C = b^2$

### Redlich-Kwong EOS

$$P = \frac{RT}{V-b} - \frac{a}{T^{1/2} V(V+b)}$$

$$\Rightarrow \frac{PV}{RT} = \frac{V}{V-b} - \frac{a}{RT^{3/2} V(V+b)} = \frac{1}{1 - \frac{b}{V}} - \frac{a/RT^{3/2}}{V+b}$$

$$\frac{1}{1-x} = 1 + x + x^2 + \dots$$

$$1 - \frac{b}{V} = 1 + \frac{b}{V} + \left(\frac{b}{V}\right)^2 + \dots$$



Second term :

$$\frac{a/pT^{3/2}}{v + b}$$

$$= \frac{a}{RT^{3/2}} \cdot \frac{v}{v(v+b)}$$

$$= \frac{a}{RT^{3/2}} \cdot \frac{1}{v} \cdot \frac{1}{\left(1 + \frac{b}{v}\right)}$$

$$= \frac{a}{RT^{3/2}} \cdot \frac{1}{v} \cdot \frac{1}{\left\{1 - \left(-\frac{b}{v}\right)\right\}}$$

$$\therefore \frac{1}{1 + \frac{b}{v}} = 1 - \frac{b}{v} + \left(\frac{b}{v}\right)^2 - \dots$$

$$\therefore \text{Second term} = \frac{a}{RT^{3/2}} \cdot \frac{1}{v} \left\{ 1 - \frac{b}{v} + \left(\frac{b}{v}\right)^2 - \dots \right\}$$

$$= \frac{a}{RT^{3/2} v} - \frac{ab}{RT^{3/2} v^2} + \frac{ab^2}{RT^{3/2} v^3} - \dots$$

$$\therefore \frac{Pv}{RT} = 1 + \frac{b}{v} + \left(\frac{b}{v}\right)^2 + \left(\frac{b}{v}\right)^3 - \frac{a}{RT^{3/2} v} + \frac{ab}{RT^{3/2} v^2} - \frac{ab^2}{RT^{3/2} v^3} + \dots$$

$$= 1 + \frac{b - \frac{a}{RT^{3/2}}}{v} + \frac{b^2 - \frac{ab}{RT^{3/2}}}{v^2} + \dots$$

Second virial Coefficient,  $B = b - \frac{a}{RT^{3/2}}$

$$C = b^2 - \frac{ab}{RT^{3/2}}$$

$$6. \quad T = -30^\circ\text{C} = 243.15 \text{ K},$$

$$P = 10.6 \text{ bar} = 1.06 \times 10^6 \text{ Pa}.$$

Critical Properties of ethane:

$$T_c = 305.4 \text{ K} \quad P_c = 48.84 \text{ bar} \quad \omega = 0.099$$

$$= 48.84 \times 10^5 \text{ Pa}.$$

$$P = \frac{RT}{\underline{v} - b} - \frac{a \alpha(T)}{\underline{v}(\underline{v} + b) + b(\underline{v} - b)}$$

$$\alpha(T) = \left[ 1 + \kappa(1 - \sqrt{T_r}) \right]^2 \quad T_r = \frac{T}{T_c} = \frac{243.15}{305.4} = 0.796.$$

$$\kappa = 0.37464 + 1.54226(0.099) - 0.26992(0.099)^2$$

$$= 0.52468$$

$$\alpha = \left[ 1 + 0.52468(1 - \sqrt{0.796}) \right]^2 = 1.116.$$

$$a = \frac{0.45724 (RT_c)^2}{P_c} = 0.6036 \text{ J} \cdot \frac{\text{m}^3}{\text{mol}}$$

$$b = \frac{0.0778 RT_c}{P_c} = 4.045 \times 10^{-5} \text{ m}^3/\text{mol}$$

$$P = \frac{RT}{\underline{v} - 4.045 \times 10^{-5}} - \frac{(0.6036)(1.116)}{\underline{v}(\underline{v} + 4.045 \times 10^{-5}) + 4.045 \times 10^{-5}(\underline{v} - b)}$$

$$= \frac{2021.549}{\underline{v} - b} - \frac{0.6736}{\underline{v}^2 + 2b\underline{v} - b^2}$$

$$\Rightarrow P = \frac{2021.549 (V^2 + 2.6V - b^2) - 0.6736 (V - b)}{(V - b) (V^2 + 2.6V - b^2)}$$

$$\Rightarrow P = \frac{2021.549 V^2 + 0.1635 V - 3.31 \times 10^{-6} - 0.6736 V + 2.724 \times 10^{-5}}{(V - b) (V^2 + 2.6V - b^2)}$$

$$\Rightarrow P \{ V^3 + 2.6V^2 - b^2V - bV^2 - 2b^2V + b^3 \}$$

$$= 2021.549 V^2 - 0.5101V + 2.394 \times 10^{-5}$$

$$\Rightarrow 1.06 \times 10^6 V^3 + 42.877 V^2 - 5.23 \times 10^{-3} V + 7.015 \times 10^{-8}$$

$$= 2021.549 V^2 - 0.5101 V + 2.394 \times 10^{-5}$$

$$\Rightarrow 1.06 \times 10^6 V^3 - 1978.672 V^2 + 0.5049 V - 2.387 \times 10^{-5} = 0$$

Using Cubic equation solver,

$$V = \begin{cases} 6.02 \times 10^{-5} \\ 0.00023 \\ 0.00157 \end{cases}$$

Among these three, the lowest value corresponds to the molar volume of saturated ethane liquid & highest value corresponds to molar volume of saturated ethane vapour.

$$\therefore V^L = 6.02 \times 10^{-5} \text{ m}^3/\text{mol} \quad V^g = 0.00157 \text{ m}^3/\text{mol}$$

M.W. of ethane = 30 g/mol.

$$\rho^{liq} = \frac{1}{V_L} \times \text{M.W. ethane} \left( \frac{\text{g}}{\text{mol}} \right) \cdot \left( \frac{\text{mol}}{\text{m}^3} \right)$$

$$= \frac{1}{6.02 \times 10^{-5}} \times 30 \frac{\text{g}}{\text{mol}} \times \frac{1}{10^6} \frac{\text{mol}}{\text{cm}^3}$$

$$= 0.498 \text{ g/cm}^3$$

$$\rho^{vap} = \frac{\text{M.W. ethane}}{V_g}$$

$$= \frac{30}{0.00157} \times \frac{1}{10^6}$$

$$= 0.019 \text{ g/cm}^3$$

→ The reported values are:  $\rho^{liq} = 0.468 \text{ g/cm}^3$

$$\rho^{vap} = 0.0193 \text{ g/cm}^3$$

using Peng-Robinson equation  $\rho^{liq}$  value is 6.4% higher than the reported value, and  $\rho^{vap}$  value is ~1% lower than the reported value.

7. M.W. of Propane. =  $44 \times 10^{-3} \frac{\text{kg}}{\text{mol}}$

$\therefore$  No. of moles of Propane present,  $n = \frac{50}{44 \times 10^{-3}}$   
 $= 1136 \text{ mol}$

(a) ideal gas law

$$V = \frac{nRT}{P}$$

here,  $T = 50^\circ\text{C} = 323.15 \text{ K}$ ,  $P = 35 \text{ bar} = 35 \times 10^5 \text{ Pa}$

$$V = \frac{1136 \times 8.314 \times 323.15}{35 \times 10^5} = \boxed{0.872 \text{ m}^3}$$

(b) Redlich Kwong EOS :-

$$P = \frac{RT}{v-b} - \frac{a}{T^{1/2} v(v+b)}$$

$$a = \frac{0.42748 R^2 T_c^{2.5}}{P_c}$$

$$b = \frac{0.08664 RT_c}{P_c}$$

Critical Properties of Propane:

$T_c = 370 \text{ K}$ ;  $P_c = 42.44 \text{ bar}$ ,  $\omega = 0.152$

$= 42.44 \times 10^5 \text{ Pa}$



Putting the values of  $T_c$  &  $P_c$

$$a = 18.33 \frac{\text{J} \cdot \text{m}^3 \text{K}^{1/2}}{\text{mol}^2}$$

$$b = 6.28 \times 10^{-5} \frac{\text{m}^3}{\text{mol}}$$

Now,  $\underline{v}$  is calculated using excel solver.

Initially, guessed value of  $\underline{v} = 0.001$   
After solving,

$$\underline{v} = 0.0001095 \text{ m}^3/\text{mol}$$

$$\therefore v = (1136)(0.0001095) = \boxed{0.1244 \text{ m}^3}$$

© Peng Robinson EOS:

$$P = \frac{RT}{\underline{v}-b} - \frac{a\alpha(T)}{\underline{v}(\underline{v}+b) + b(\underline{v}-b)}$$

$$\alpha = \left[ 1 + K(1 - \sqrt{T_r}) \right]^2$$

$$T_r = \frac{T}{T_c} = \frac{323.15}{370} = 0.8734$$

$$\text{where, } K = 0.37464 + 1.54226 \omega - 0.26992 \omega^2.$$

$$= 0.37464 + 1.54226(0.152) - 0.26992(0.152)^2$$

$$= 0.6028$$

$$\alpha = \left[ 1 + 0.6028(1 - \sqrt{0.8734}) \right]^2 = 1.081$$

$$a = \frac{0.45724 (RT_c)^2}{P_c} = 1.02 \frac{\text{J} \cdot \text{m}^3}{\text{mol}}$$

$$b = \frac{0.0778 RT_c}{P_c} = 5.64 \times 10^{-5} \frac{\text{m}^3}{\text{mol}}$$

After solving using excel-solver,

$$\underline{V} = 9.421 \times 10^{-5} \cdot \text{m}^3/\text{mol}.$$

$$\therefore V = 1136 \underline{V} = 1136 \times 9.421 \times 10^{-5} = \boxed{0.107 \text{ m}^3}$$

④ Compressibility Chart

$$P_r = \frac{P}{P_c} = \frac{35 \times 10^5}{42.44 \times 10^5} = 0.8247, \quad T_r = 0.8734$$

From Compressibility chart at  $P_r \approx 0.8247$  and  $T_r \approx 0.875$ ;

$$Z_c \approx 0.13$$

$$\therefore V = \frac{Z_c \cdot n RT}{P} = \frac{0.13 \times 1136 \times 8.314 \times 320.15}{35 \times 10^5} = \boxed{0.113 \text{ m}^3}$$