

RESONANCE COMPENSATION STUDIES AT THE FNAL RECYCLER RING

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A DISSERTATION

Submitted to  
Michigan State University  
in partial fulfillment of the requirements  
for the degree of

Physics—Doctor of Philosophy

2024

## ABSTRACT

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## **ACKNOWLEDGEMENTS**

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## **LIST OF ABBREVIATIONS**

<b>MSU</b>	Michigan State University
<b>FNAL</b>	Fermilab National Accelerator Laboratory
<b>RR</b>	Recycler Ring
<b>MI</b>	Main Injector
<b>RDTs</b>	Resonance Driving Terms
<b>NuMI</b>	Neutrinos at the Main Injector
<b>PSB</b>	CERN Proton Synchrotron Booster

# CHAPTER 1

## INTRODUCTION

Particle accelerators are the workhorses for modern scientific discoveries.

### 1.1 Circular Accelerators and Storage Rings

### 1.2 Fermilab

### 1.3 Outline

The following thesis will explore the compensation of third-order resonances in the Fermilab Recycler Ring. This first chapter introduces the motivation behind this thesis work. The second chapter summarizes single particle dynamics with the help of exponential Lie operators and moves forward to introduce a relevant concept of collective beam dynamics: the space charge tune shift. This theoretical overview gives segue into the third chapter of this thesis, where the Recycler Ring is introduced and described in detail. Motivation for the compensation of third order resonances is given in this chapter under the framework of current and future operation of the RR. With the basic physics concepts and the description of the machine put in place, the fourth chapter describes in full detail the scheme and experiments developed in order to compensate third order resonances at low intensities. Before moving to explore the Recycler Ring at high intensities, chapter five provides an interlude in order to show a series of experiments done at the CERN PS Booster. These experiments explore the use of advanced optimization algorithms in the aid of compensating multiple resonance lines simultaneously. Coming back to Fermilab, chapter six showcases the studies and experiments done at high intensities in the RR in order to understand the interplay between the compensation of resonance lines and space charge effects. Finally, chapter seven brings down the curtain by providing some general conclusions and future work stemming from this thesis.



## CHAPTER 2

### BEAM DYNAMICS IN RINGS

#### 2.1 Lie Maps in Accelerator Physics

The most basic element of a particle accelerator can be thought of as a black box. This black box takes some single charged particle with initial transverse coordinates  $(x_0, x'_0, y_0, y'_0)$ , as defined in a Frenet-Serret coordinate system, and maps them to some final coordinates  $(x_f, x'_f, y_f, y'_f)$ . For simplicity, any longitudinal effect will not be taken into account for this analysis, but can be easily incorporated. By gathering the initial coordinates into a vector, i.e.  $\vec{X}_0 = (x_0, x'_0, y_0, y'_0)$ , and doing the same for the final coordinates, i.e.,  $\vec{X}_f = (x_f, x'_f, y_f, y'_f)$ , one can define the mapping  $\mathcal{M}$  that relates both vectors, such that:

$$\vec{X}_f = \mathcal{M}\vec{X}_0. \quad (2.1)$$

For a charged particle inside some accelerator element that can be described using Hamiltonian dynamics, the mapping  $\mathcal{M}$  can be understood in terms of Poisson brackets and exponential Lie operators [1–4].

Let  $\vec{X} = (q_1, p_1, \dots, q_n, p_n)$  be a  $2n$  dimensional vector, made from  $n$  pairs of canonical coordinates  $(q_i, p_i)$  that make up the  $2n$  dimensional phase space. And let two arbitrary functions  $f(\vec{X}; s)$  and  $g(\vec{X}; s)$  be functions of  $\vec{X}$  and  $s$ , where  $s$  plays the role of the independent "time" coordinate. The Poisson brackets  $[\bullet, \bullet]$  can be defined as:

$$[f, g] = \sum_{i=1}^n \frac{\partial f}{\partial q_i} \frac{\partial g}{\partial p_i} - \frac{\partial f}{\partial p_i} \frac{\partial g}{\partial q_i}. \quad (2.2)$$

Using this definition, one can explicitly write out the Poisson bracket definition for a 4 dimensional phase space described by state vector  $\vec{X} = (x, x', y, y')$ . This reads:

$$[f, g] = \frac{\partial f}{\partial x} \frac{\partial g}{\partial x'} - \frac{\partial f}{\partial x'} \frac{\partial g}{\partial x} + \frac{\partial f}{\partial y} \frac{\partial g}{\partial y'} - \frac{\partial f}{\partial y'} \frac{\partial g}{\partial y}. \quad (2.3)$$

The Lie operator  $: f :$  acts on some function  $g$  and is the adjoint operator of the Poisson bracket operator. Its definition reads:

$$: f : g = [f, g]. \quad (2.4)$$

This specific  $: \bullet :$  notation allows for a compact notation in order to define the exponential Lie operator. The exponential Lie operator of an arbitrary function  $f$  is defined as

$$e^{:f:\bullet} = \sum_{k=0}^{\infty} \frac{1}{k!} (:f:)^k \bullet. \quad (2.5)$$

It turns out that for a Hamiltonian system, the mapping of coordinates from  $\vec{X}_0$  to  $\vec{X}_f$  follows the expression:

$$\vec{X}_f = e^{-\ell:H:\vec{X}} \Big|_{\vec{X}=\vec{X}_0}, \quad (2.6)$$

which is known as a Lie Map [2]. In this case,  $\ell$  corresponds to the integration length of the independent coordinate. For example, for a particle traversing a magnet which has length  $L$ , the integration length is  $\ell = L$ . When looking at the one-turn map, the integration length corresponds to the circumference  $C$  of the accelerator over an effective Hamiltonian  $H_{eff}$ . Furthermore, if working with action-angle variables, the integration length  $\ell$  would just be the phase advance  $\mu$ .

## 2.2 One-turn Map and Normal Form

The one-turn map  $\mathcal{M}_1$  of a circular accelerator is the composition ( $\circ$ ) of mappings from every element in the ring. Choosing an arbitrary initial point at  $s = 0$  and going around the ring, the one-turn map describes the transformation of coordinates after one turn, i.e.,  $\vec{X}_{N+1} = \mathcal{M}_1 \vec{X}_0$ . This map composition reads:

$$\mathcal{M}_1 = M_{N+1} \circ e^{:h_N:} \circ \dots \circ e^{:h_2:} \circ M_2 \circ e^{:h_1:} \circ M_1 = M_{N+1} e^{:h_N:} \dots e^{:h_2:} M_2 e^{:h_1:} M_1, \quad (2.7)$$

where  $M_i$  is the matrix representation of a linear mapping, that does not couple  $x - y$  plane, e.g., drift space mapping, quadrupole mapping. On the other hand, the map  $e^{:h_i:}$  represents any linear or non-linear mapping that can be found around the machine and can be considered a perturbation to the ideal lattice including coupling elements, e.g., skew quadrupoles, higher order multipole elements. Figure 2.1 illustrates the procedure to build the one-turn map for a circular accelerator.

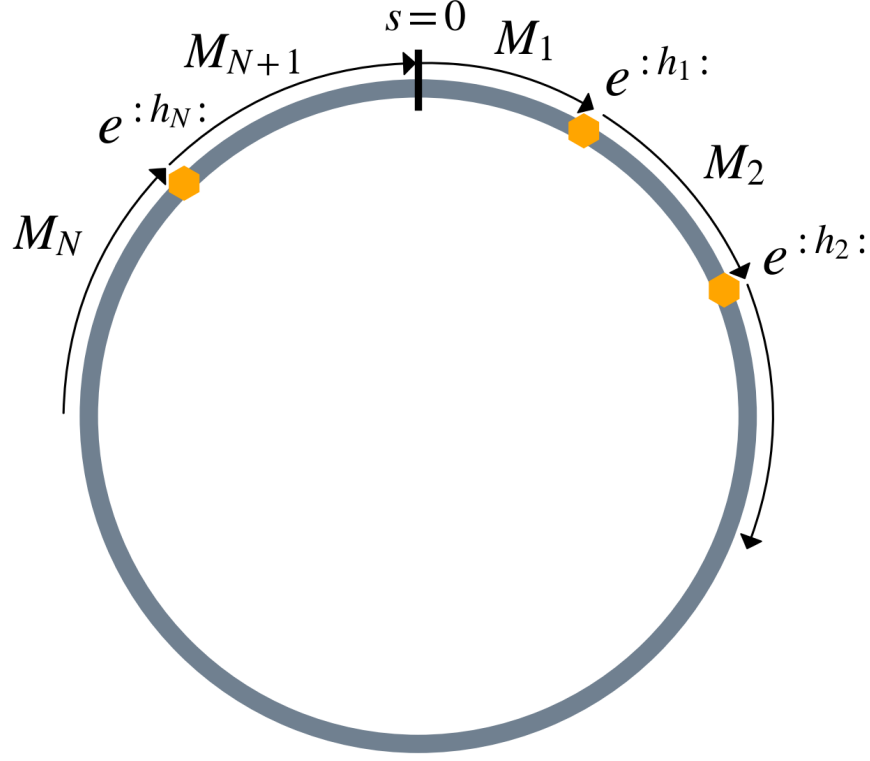


Figure 2.1 Diagram of an arbitrary circular accelerator in order to illustrate the one-turn map.

Through the use of the Baker-Campbell-Hausdorff formula , Eq. 2.7 can be collapsed to the expression

$$\mathcal{M}_1 = e^{-C:H_{eff}:}, \quad (2.8)$$

where  $C$  is the circumference of the ring and  $H_{eff}$  is the effective Hamiltonian of the machine over one turn. As mentioned earlier, for most cases, it is of interest to look at the perturbations to the linear uncoupled dynamics of the design lattice. With this in mind, Eq. 2.8 can be rewritten as:

$$\mathcal{M}_1 = e^{:h:} R, \quad (2.9)$$

where  $R$  is a rotation matrix encoding the linear uncoupled dynamics of the ideal lattice. On the other hand, the term  $e^{:h:}$  encodes the perturbations to this ideal situation. It is worth pointing out that for the case  $h = 0$ , the traditional Courant-Snyder variables are recovered.

The Courant-Snyder variables  $(\hat{x}, \hat{p}_x, \hat{y}, \hat{p}_y)$  or normalized phase space coordinates can be written for a linear uncoupled case as:

$$\hat{u} = \sqrt{2J_u} \cos(\phi_u + \phi_{u_0}); \quad (2.10)$$

$$\hat{p}_u = -\sqrt{2J_u} \sin(\phi_u + \phi_{u_0}), \quad (2.11)$$

where  $u$  can stand either for the  $x$  or  $y$  coordinate,  $J_u$  and  $\phi_u$  correspond to the action-angle variables and  $\phi_{u_0}$  corresponds to the initial phase. For the case where perturbations exist, i.e.,  $h \neq 0$ , the action  $J_u$  is not constant anymore and will be a function of  $\phi_u$ .

The Normal Form formalism is introduced at this point in order to find amplitude-independent coordinates  $I_u$  and  $\psi_u$ , such that the motion just depends on  $\psi_u$  at a constant  $I_u$ , with some initial phase  $\psi_{u_0}$ . These are known as non-linear action-angle variables. The variables  $I_u$  and  $\psi_u$  are calculated from the transformation  $e^{-iF}$  acting on  $J_u$  and  $\phi_u$ . Without loss of generality, the generating function  $F$  can be written as a Fourier expansion over the objective space  $(I_x, \psi_x, I_y, \psi_y)$  such that:

$$F = \sum_{jklm} f_{jklm} (2I_x)^{\frac{j+k}{2}} (2I_y)^{\frac{l+m}{2}} e^{i[(j-k)(\psi_x+\psi_{x0})+(l-m)(\psi_y+\psi_{y0})]}. \quad (2.12)$$

In a similar fashion, the argument of the Lie operator  $e^{ih}$  from Eq. 2.9 can be expanded as:

$$h = \sum_{jklm} h_{jklm} (2J_x)^{\frac{j+k}{2}} (2J_y)^{\frac{l+m}{2}} e^{i[(j-k)(\phi_x+\phi_{x0})+(l-m)(\phi_y+\phi_{y0})]}. \quad (2.13)$$

For Eqs. 2.12 and 2.13, the integer indices  $j, k, l, m$  run from 0 to infinity, and correspond to the four degrees of freedom for transverse phase space.

The terms  $f_{jklm}$  are known as generating function coefficients. The terms  $h_{jklm}$  are known as Hamiltonian coefficients or resonance driving terms (RDTs). Section 2.4 will take a closer look into how RDTs can be used to characterize the non-linear dynamics of accelerators. The generating function coefficients  $f_{jklm}$  can be related to the Hamiltonian resonance driving terms  $h_{jklm}$  through the following relation [3, 5]:

$$f_{jklm} = \frac{h_{jklm}}{1 - e^{2\pi i[(j-k)Q_x + (l-m)Q_y]}}, \quad (2.14)$$

where  $Q_x$  and  $Q_y$  represent the transverse uncoupled and unperturbed tunes of the accelerator. The transverse tunes of a circular accelerator are defined as the phase advances in each plane over one turn, in units of  $2\pi$ , i.e.,  $Q_u = \phi_u(s = C)/2\pi$ .

### 2.3 Resonances in Circular Accelerators

Equation 2.14 diverges for when the denominator goes to zero. Specifically, this happens when the following condition is met:

$$(j - k) Q_x + (l - m) Q_y = p, \quad (2.15)$$

where  $p$  can be any integer. Equation 2.15 defines resonance lines in tune space of order  $n = j + k + l + m$ . If the accelerator is tuned to operate on top of these resonances, the perturbations will add up coherently turn to turn and kick the resonant particles out of their original trajectory. In general, operating close or on top of a resonance line is harmful as particles will be lost. This is specially true for lower order resonances, i.e., for  $n < 4$ . In general, the higher order of a resonance, the weaker it is [6]. This thesis work focuses on third order resonances, i.e.,  $n = 3$ , and how to mitigate their deleterious effect.

Figure 2.2 shows the tune diagram with resonance lines, as defined by Eq. 2.15, drawn up to fifth order. The integer part of both tunes are chosen to include the actual area of operation of the Recycler Ring. The operation and tune diagram for the Recycler Ring are described in more detail in Ch. 3. Normally, the operation point of a circular accelerator is chosen to be clear of any resonance line and far away as possible from integer ( $n = 1$ ) and half integer ( $n = 2$ ) resonances. Nevertheless, in reality there are two concepts that complicate things. The first one relates to the fact that resonance lines are not infinitely thin and have some stop band width. The second one, concerns the fact that at high intensities particles will not have localized tunes, but rather a distribution of tunes with some tune spread, i.e., a tune footprint. Section 2.5 takes a closer look at this effect known as space charge tune shift. Ultimately, choosing the operation point on Fig. 2.2 is a matter of localizing a resonance-free region where the intensity-dependent tune footprint can be placed.

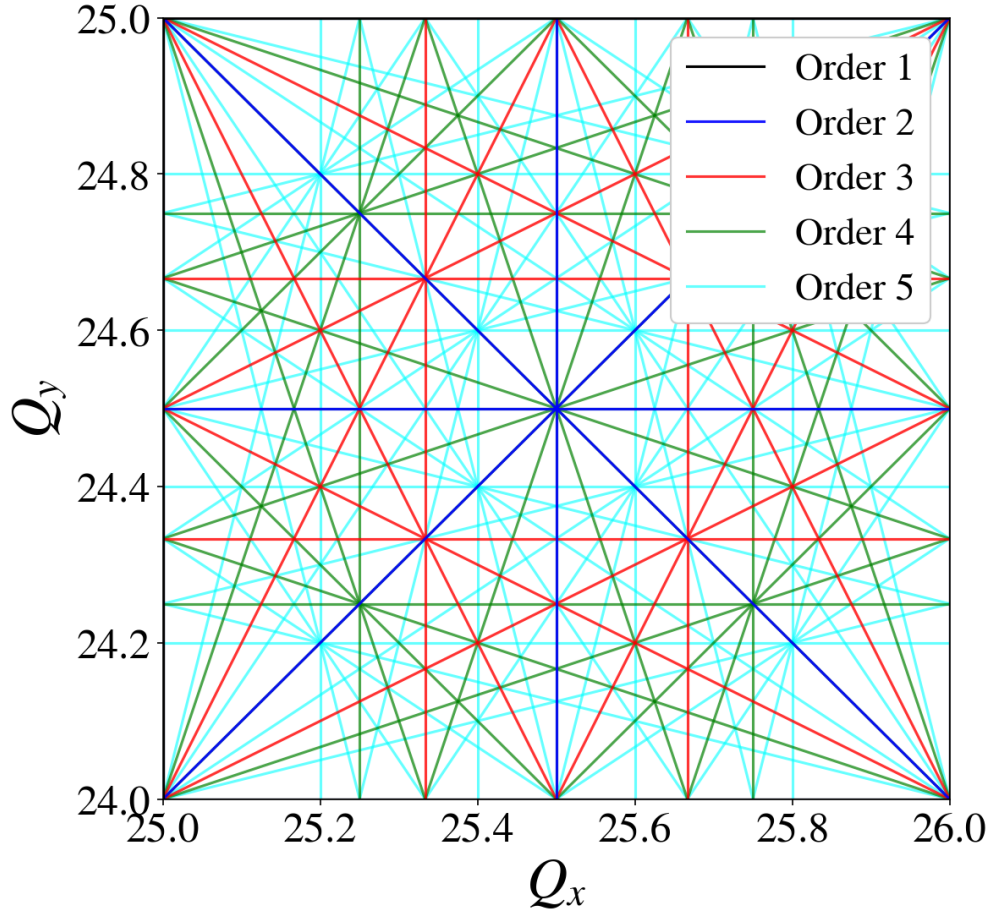


Figure 2.2 Tune diagram with resonance lines up to fifth order, enclosing the operation point of the Recycler Ring.

It is worth stopping here and asking what is the driving force behind each of these resonance lines. Classic accelerator references such as Refs. [1, 6, 7] will derive Eq. 2.15 by perturbing Hill's equation with different magnetic multipole orders. A closer look into each

Figure 2.3 zooms into the region of interest for the Recycler Ring operation in the tune diagram, as shown in Fig. 2.2. As mentioned before, the operation point

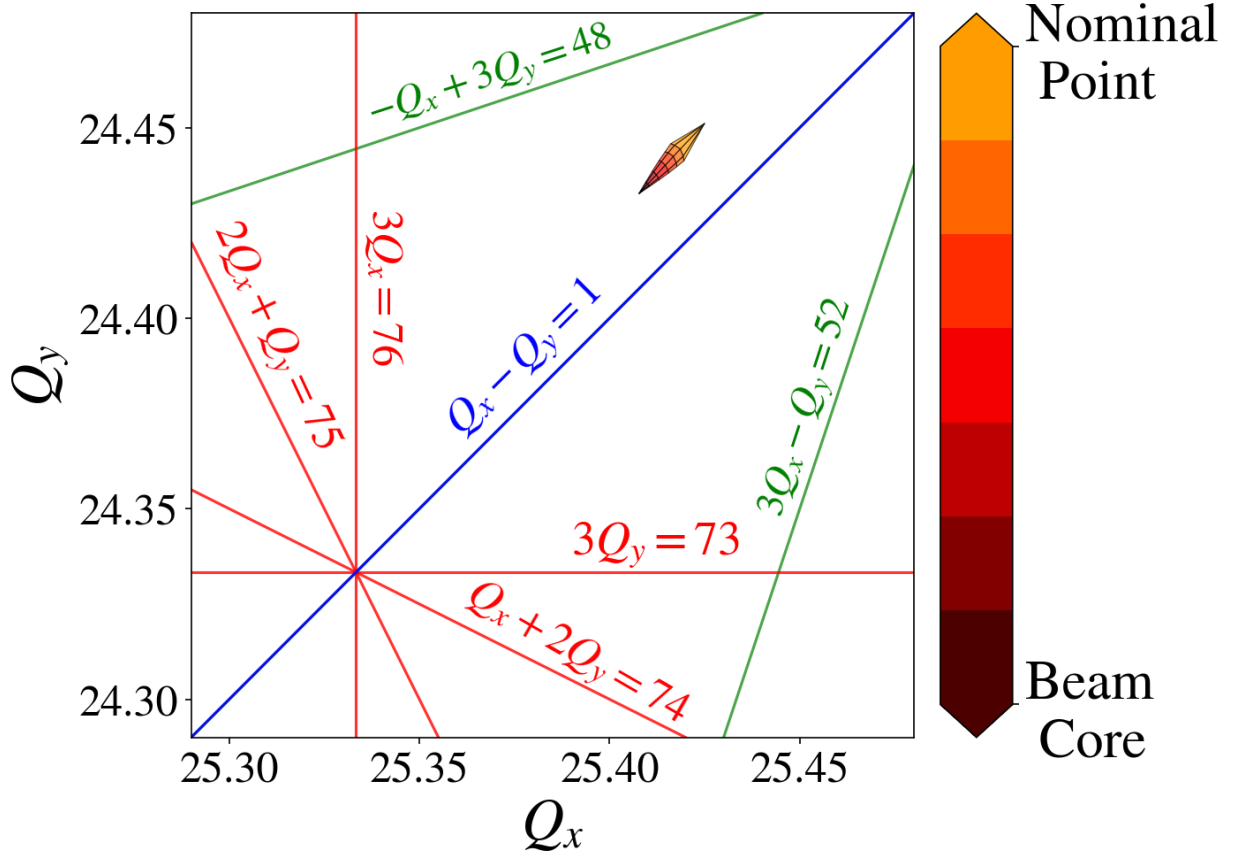


Figure 2.3 Approximate operational tune footprint at low intensities, i.e.,  $1e10$  particles per bunch.

## 2.4 Resonance Driving Terms

As it turns out, the RDTs  $h_{jklm}$  are related to the strength

The resonance basis can be built by getting the quantity  $h_u^\pm = \hat{u} \pm \hat{p}_u$  in terms of the number of turns  $N$ . Specifically, for  $h_x^-$  this reads:

$$h_x^-(N) = \sqrt{2I_x} e^{i(2\pi Q_x N + \psi_{x_0})} - 2i \sum_{jklm} j f_{jklm} (2I_x)^{\frac{j+k-1}{2}} (2I_y)^{\frac{l+m}{2}} e^{i[(1-j+k)(2\pi Q_x N + \psi_{x_0}) + (m-l)(2\pi Q_y N + \psi_{y_0})]}, \quad (2.16)$$

where  $Q_x$  and  $Q_y$  are the horizontal and vertical tune [3].

In general, RDTs are defined by the order in which they enter the one-turn normal form Hamiltonian [5]. The general expression to define RDTs reads:

$$h_{jklm} = \Xi_{jklm} \sum_i L_i \beta_{xi}^{\frac{j+k}{2}} \beta_{yi}^{\frac{l+m}{2}} V_{ni} e^{i[(j-k)\phi_{xi} + (l-m)\phi_{yi}]}, \quad (2.17)$$

where  $\Xi_{jklm}$  is just a constant defined as:

$$\Xi_{jklm} = -\frac{q}{p_0} \frac{1}{2^n} \frac{1}{n} \binom{n}{l+m} \binom{j+k}{j} \binom{l+m}{l}. \quad (2.18)$$

For Eqs. 2.17 and 2.18,  $n = j + k + l + m$  represents the order of the resonance. The sum over  $i$  is done over all multipoles of order  $n$  and length  $L_i$  that either have a normal component  $V_{ni} = B_{ni}$  if  $l + m$  is even, or a skew component  $V_{ni} = A_{ni}$  if  $l + m$  is odd. The symbols for  $\beta_{xi}$ ,  $\beta_{yi}$ ,  $\phi_{xi}$  and  $\phi_{yi}$  represent the beta functions and phase advances in each plane, respectively.

## 2.5 Space Charge Tune Shift



## CHAPTER 3

### THE FNAL RECYCLER RING

The Fermilab Recycler Ring (RR) is one of the circular accelerators located in the Fermilab Accelerator Complex. It was originally designed to store and accumulate antiprotons that remained from a Tevatron event [8]. The recycling of antiprotons was deemed ineffective and was never operationally implemented [9]. Since 2011, the RR has been repurposed to act as a pre-injector to the Main Injector (MI) by storing and accumulating protons [10]. It is worth pointing out, that the MI and the RR share the same tunnel, which has a circumference of 3.319 km (2.062 mi).

The MI/RR complex is fed protons by the Proton Source, which by itself consists of the Pre-Accelerator, the Linear Accelerator (Linac), and the Booster. The Pre-Accelerator systems provide  $H^-$  ions to the Linac, where they are accelerated to an energy of 400 MeV. After this, the beam is injected into the Booster, which is a rapid-cycling synchrotron operating at a 15 Hz repetition rate. During this injection process, the  $H^-$  beam passes through a carbon stripping foil, and it incorporates to the circulating proton beam. The Booster ramps the energy up from 400 MeV to 8 GeV. This 8 GeV proton beam can either go to the Booster Neutrino Experiments or get injected into the Recycler Ring. Once in RR the beam has two possible destinations: 1) high energy neutrino experiments through MI or 2) Muon Campus. For the latter, proton beam gets rebunched from 53 MHz to 2.5 MHz and transported to Muon Campus. For high energy neutrino experiments, the proton beam gets slip-stacked, hence doubling the intensity that gets injected into Main Injector. Once in MI, the beam is accelerated to 120 GeV and sent to the NuMI (Neutrinos at the Main Injector) beam facility [9–11]. A description of the accelerator complex is shown in figure 3.1, including the experimental beamlines which feed neutrino, muon and fixed target experiments.

The work done for this thesis focuses on the Recycler Ring. The following chapter starts by giving a general description for the operation and physics of the Recycler Ring. The next sections introduce and motivate the compensation of third order resonances for high intensity operation.

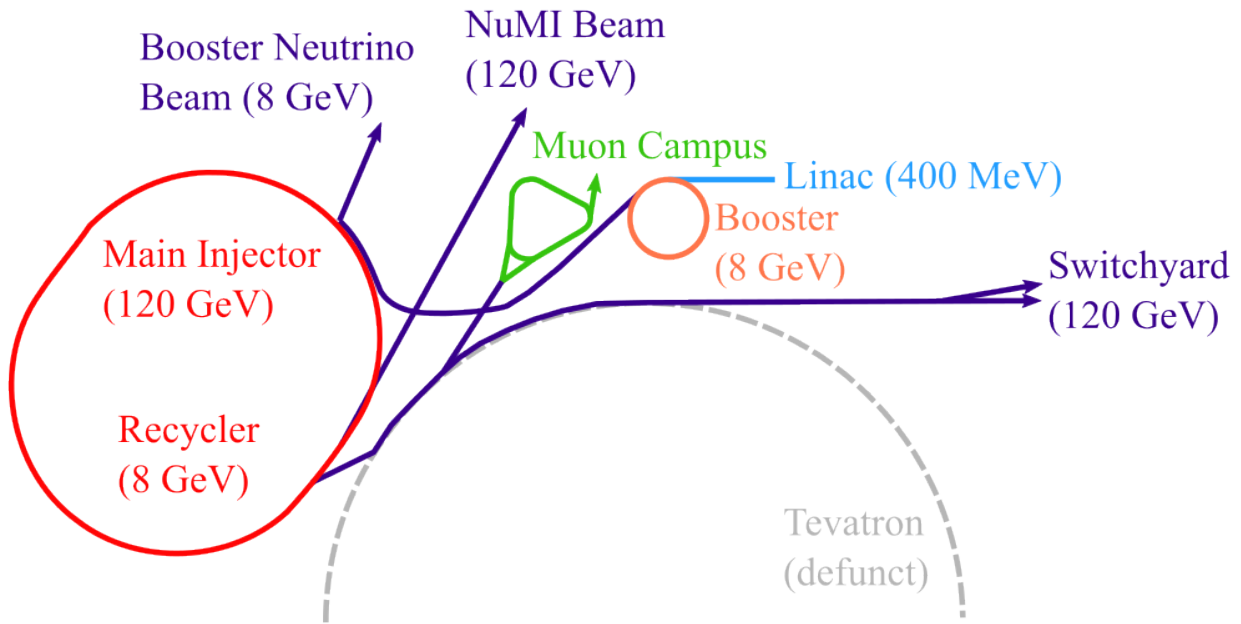


Figure 3.1 The past (Tevatron), present and future (PIP-II and LBNF) of the FNAL Accelerator Complex, taken from [3].

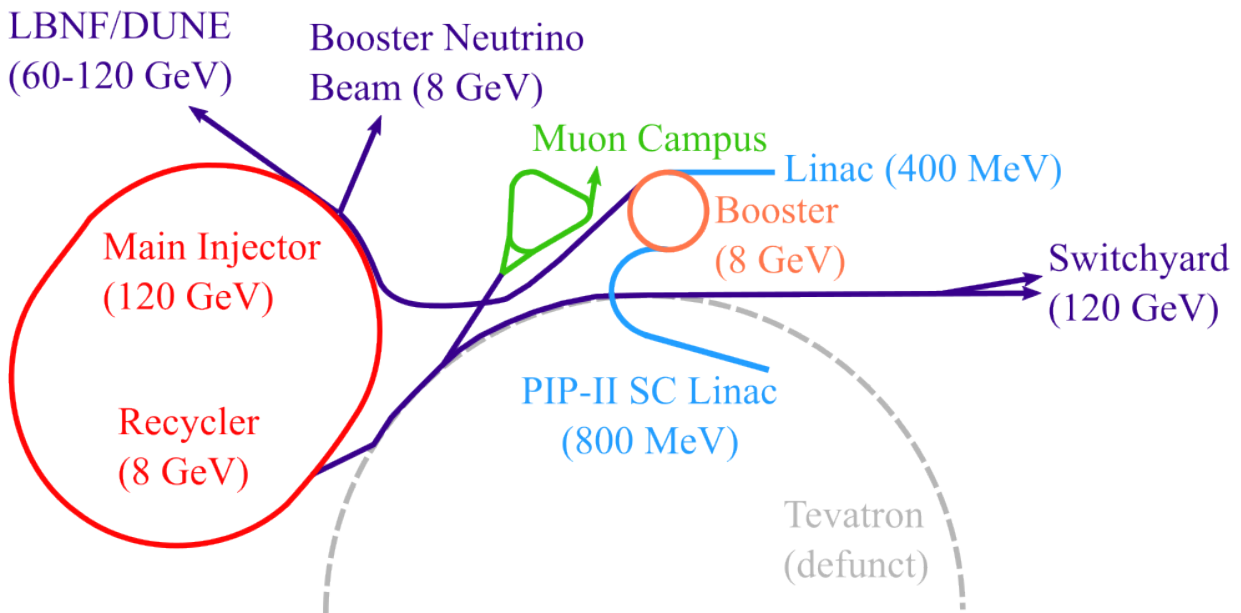


Figure 3.2 The past (Tevatron), present and future (PIP-II and LBNF) of the FNAL Accelerator Complex, taken from [3].

### 3.1 General Specifications

The RR is a permanent magnet storage ring operating at a fixed momentum of 8.835 GeV/c.

[12] [13]

Table 3.1 Typical Recycler Ring properties for beam sent to NuMI

Parameter	Value	Unit
Circumference	3319	m
Momentum	8.835	GeV/c
RF Frequency	52.8	MHz
RF Voltage	80	kV
Harmonic Number	588	
Synchrotron Tune	0.0028	
Slip Factor	$-8.6 \times 10^{-3}$	
Superperiodicity	2	
Horizontal Tune	25.43	
Vertical Tune	24.445	
Horizontal Chromaticity	-6	
Vertical Chromaticity	-7	
95% Normalized Emittance	15	$\pi$ mm mrad
95% Longitudinal Emittance	0.08	eV s
Intensity	$5 \times 10^{10}$	ppb
	$8 \times 10^{10}$ (PIP-II)	ppb
MI Ramp Time	1.2	s
	1.133	s
	1.067	s
Booster Frequency	15	Hz
	20 (PIP-II)	Hz

### 3.2 Tune Diagram and Resonances

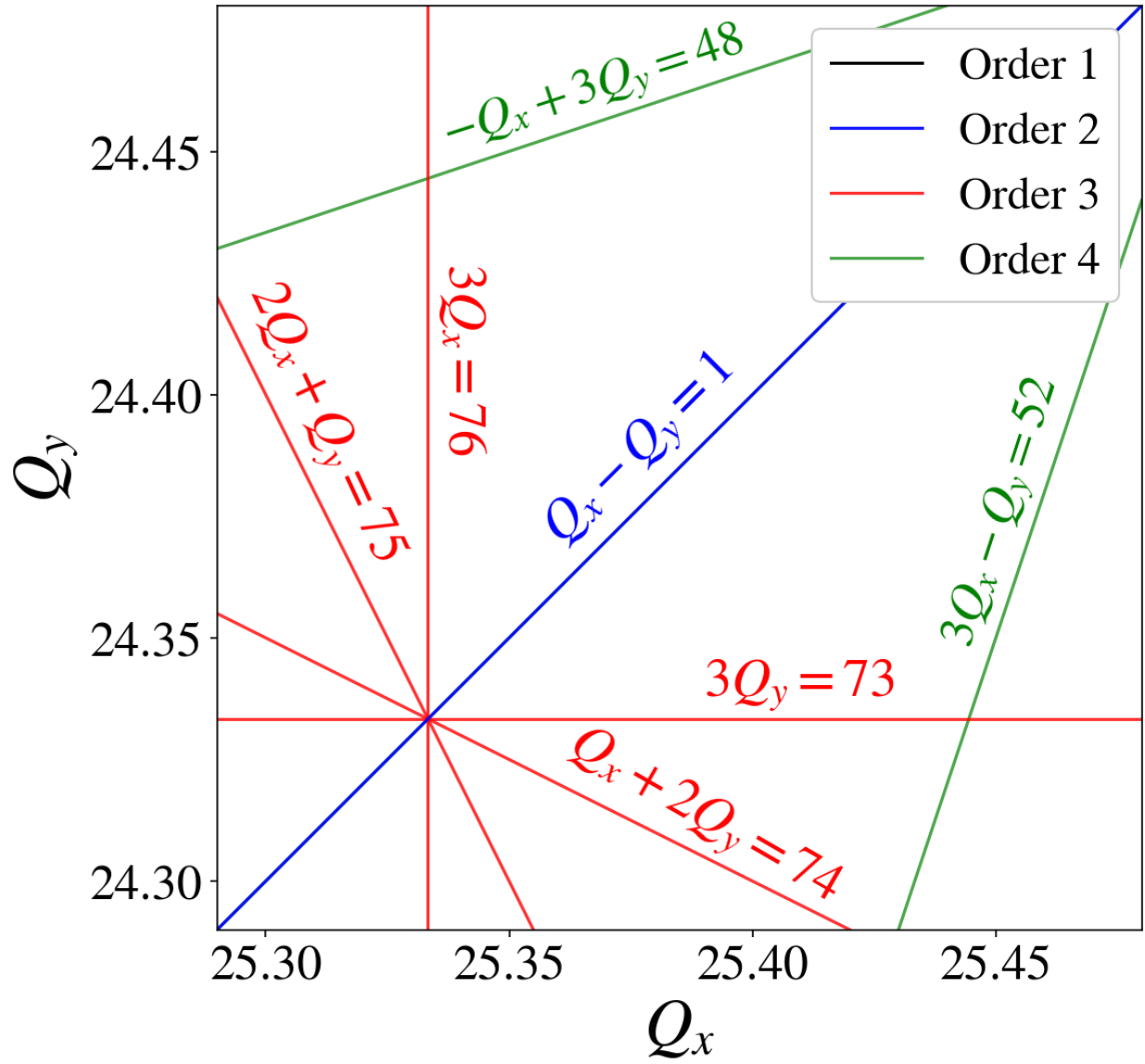


Figure 3.3 Portion of the tune diagram enclosing the operational tunes of the Recycler Ring.

### 3.3 High Intensity and Tune Footprint

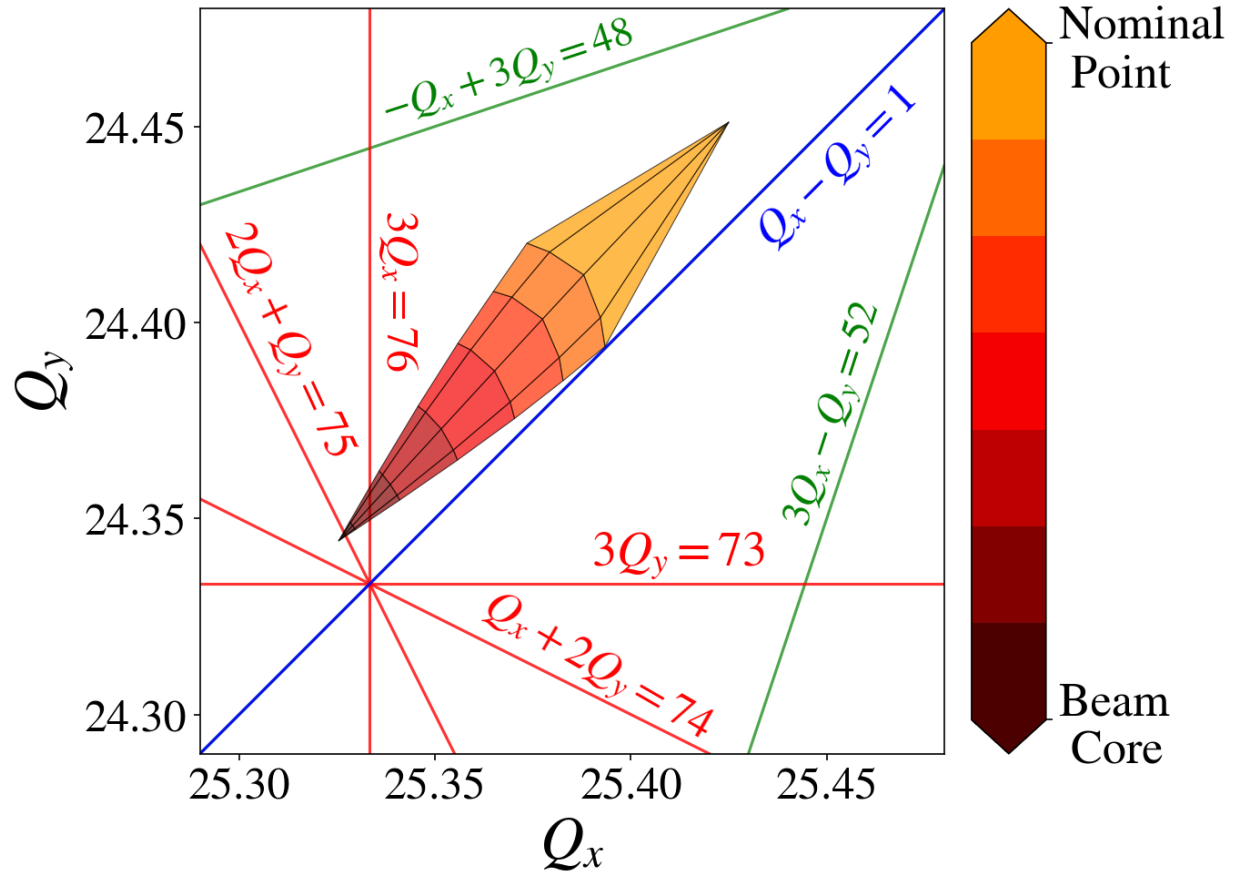


Figure 3.4 Approximate operational tune footprint at high intensities, i.e.,  $1e11$  particles per bunch.

## **CHAPTER 4**

### **COMPENSATION OF THIRD-ORDER RESONANCES AT LOW INTENSITIES**

#### **4.1 Global RDTs and Lattice Model**

#### **4.2 Measurement of Third Order RDTs**

#### **4.3 Compensation of RDTs**

#### **4.4 Optimization of Compensation Currents**

#### **4.5 Experimental Verification of Compensation**

##### **4.5.1 Dynamic Loss Map**

##### **4.5.2 Static Tune Scans**

## **CHAPTER 5**

### **RESONANCE COMPENSATION STUDIES AT THE CERN PROTON SYNCHROTRON BOOSTER**

#### **5.1 General specifications**

#### **5.2 Tune Diagram and Operation**

#### **5.3 Optimization Algorithms for Resonance Compensation**

#### **5.4 Experimental Verification of Compensation**

## **CHAPTER 6**

### **HIGH INTENSITY STUDIES**

#### **6.1 Global RDTs and Intensity-Dependent Effects**

[14]

#### **6.2 Space Charge Tune Shift**

#### **6.3 Measurement of Tune Shift**

#### **6.4 Static Tune Scans at Different Intensities**



## **CHAPTER 7**

### **CONCLUSIONS AND FUTURE WORK**

[15] [16]

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**APPENDIX**  
**YOUR APPENDIX**