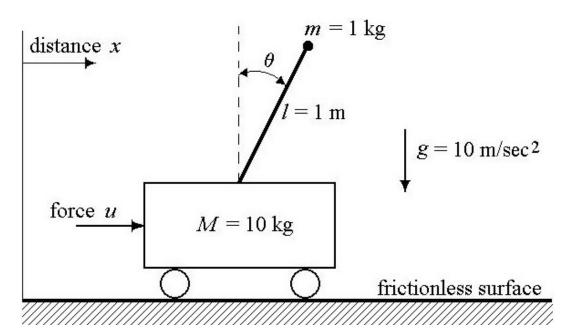
## **Case Study**

We will use the Lagrange equations of motion to derive a state-space model of a dynamical system consisting of a cart with an inverted pendulum (point mass on a mass-less shaft) attached to it as depicted in the figure below.



The kinetic energy K is  $K=K_1+K_2$ , where  $K_1$  is the kinetic energy of the cart, while  $K_2$  is the kinetic energy of pendulum. The kinetic energy of the cart,  $K_1$ , is due to its translational velocity  $\dot{x}$ . Hence,

$$K_1=rac{1}{2}M\dot{x}^2.$$

The kinetic energy of the pendulum is the sum of the translational and rotational energies,

$$K_2 = rac{1}{2} m \|v\|^2 + rac{1}{2} I_{cm} \dot{ heta}^2,$$

where  $I_{cm}$  is the rotational inertia with respect to the center of mass. In our example,  $I_{cm}=0$ . Hence, the kinetic energy of this pendulum is

$$K_2 = rac{1}{2} m \|v\|^2 = rac{1}{2} m (\dot{x}_m^2 + \dot{y}_m^2),$$

where the horizontal position of the bob is  $x_m=x+l\sin\theta$ , and its vertical position is  $y_m=l\cos\theta$ . Therefore, the magnitude squared velocity of the bob is

$$egin{split} \left(rac{d}{dt}\left(x+l\sin heta
ight)
ight)^2 + \left(rac{d}{dt}\left(l\cos heta
ight)
ight)^2 &= \left(\dot{x}+l\dot{ heta}\cos heta
ight)^2 + \left(-l\dot{ heta}\sin heta
ight)^2 \ &= \dot{x}^2 + 2l\dot{x}\dot{ heta}\cos heta + l^2\dot{ heta}^2\left(\cos^2 heta + \sin^2 heta
ight) \ &= \dot{x}^2 + 2l\dot{x}\dot{ heta}\cos heta + l^2\dot{ heta}^2. \end{split}$$

So the kinetic energy of the pendulum is

$$K_2 = rac{1}{2} m \left( \dot{x}^2 + 2 l \dot{x} \dot{ heta} \cos heta + l^2 \dot{ heta}^2 
ight).$$

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The total kinetic energy of the system is

$$K=K_1+K_2=rac{1}{2}M\dot{x}^2+rac{1}{2}m\left(\dot{x}^2+2l\dot{x}\dot{ heta}\cos heta+l^2\dot{ heta}^2
ight).$$

The potential energy of the system U is due only to the point mass m and is equal to

$$U = mgl\cos\theta.$$

Hence, the Lagrangian L is

$$L=K-U=rac{1}{2}M\dot{x}^2+rac{1}{2}m\left(\dot{x}^2+2l\dot{x}\dot{ heta}\cos heta+l^2\dot{ heta}^2
ight)-mgl\cos heta.$$

We can now determine the equations that model the system using Lagrange's equations. The first Lagrange equation is

$$rac{d}{dt}\left(rac{\partial L}{\partial \dot{x}}
ight)-rac{\partial L}{\partial x}=u.$$

We note that

$$rac{\partial L}{\partial \dot{x}} = M \dot{x} + m (\dot{x} + l \dot{ heta} \cos heta),$$

and hence

$$rac{d}{dt}\left(rac{\partial L}{\partial \dot{x}}
ight) = M\ddot{x} + m\ddot{x} + ml\ddot{ heta}\cos heta - ml\dot{ heta}^2\sin heta.$$

Because  $rac{\partial L}{\partial x}=0$  , we obtain

$$egin{aligned} rac{d}{dt} \left( rac{\partial L}{\partial \dot{x}} 
ight) - rac{\partial L}{\partial x} &= M \ddot{x} + m \ddot{x} + m l \ddot{ heta} \cos heta - m l \dot{ heta}^2 \sin heta \ &= u. \end{aligned}$$

We now write the second Lagrange equation,

$$\frac{d}{dt}\left(\frac{\partial L}{\partial \dot{\theta}}\right) - \frac{\partial L}{\partial \theta} = 0.$$

Note that

$$rac{\partial L}{\partial \dot{ heta}} = m(l\dot{x}\cos{ heta} + l^2\dot{ heta}),$$

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and thus

$$rac{d}{dt}\left(rac{\partial L}{\partial \dot{ heta}}
ight) = ml\left(\ddot{x}\cos heta - \dot{x}\dot{ heta}\sin heta
ight) + ml^2\ddot{ heta}.$$

We also have,

$$rac{\partial L}{\partial heta} = -m l \dot{x} \dot{ heta} \sin heta + m g l \sin heta.$$

The second Lagrange equation is

$$\begin{split} \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{\theta}} \right) - \frac{\partial L}{\partial \theta} &= ml \left( \ddot{x} \cos \theta - \dot{x} \dot{\theta} \sin \theta \right) + ml^2 \ddot{\theta} + ml \dot{x} \dot{\theta} \sin \theta - mgl \sin \theta \\ &= ml \ddot{x} \cos \theta + ml^2 \ddot{\theta} - mgl \sin \theta \\ &= \ddot{x} \cos \theta + l \ddot{\theta} - g \sin \theta \\ &= 0. \end{split}$$

We represent the obtained Lagrange equations in matrix form

$$egin{bmatrix} M+m & ml\cos heta \ \cos heta & l \end{bmatrix} egin{bmatrix} \ddot{x} \ \ddot{ heta} \end{bmatrix} = egin{bmatrix} ml\dot{ heta}^2\sin heta + u \ g\sin heta \end{bmatrix}.$$

The above representation is convenient from the calculation point of view. Indeed, we can use, the following MATLAB commands to calculate the vector  $\begin{bmatrix} \ddot{x} & \ddot{\theta} \end{bmatrix}^\top$ :

syms M m theta I u thetadot g
D=[M+m m\*I\*cos(theta);cos(theta) I];
v=[u+m\*I\*thetadot^2\*sin(theta);g\*sin(theta)];
D\_inv=inv(D);

g=D\_inv\*v;

simplify(g);

protty/opo

pretty(ans)

to obtain the desired result. Let

$$\Delta = M + m - m\cos^2\theta.$$

Then, we have

$$egin{aligned} egin{aligned} \ddot{x} \ \ddot{ heta} \end{aligned} &= rac{1}{\Delta} egin{bmatrix} u + ml\dot{ heta}^2\sin heta - mg\cos heta\sin heta \ rac{1}{l}(-u\cos heta - ml\dot{ heta}^2\cos heta\sin heta + gM\sin heta + gm\sin heta) \end{bmatrix}. \end{aligned}$$

We define the following state variables:

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$$x_1=x,\quad x_2=\dot x,\quad x_3= heta,\quad x_4=\dot heta.$$

Then, we represent the above two second-order differential modeling equations in state-space format,

$$egin{array}{lcl} \dot{x}_1 &=& x_2 \ \dot{x}_2 &=& rac{mlx_4^2\sin x_3 - mg\cos x_3\sin x_3 + u}{M + m - m\cos^2 x_3} \ \dot{x}_3 &=& x_4 \ \dot{x}_4 &=& rac{-mlx_4^2\cos x_3\sin x_3 + gM\sin x_3 + gm\sin x_3 - \cos x_3 u}{l(M + m - m\cos^2 x_3)} \end{array}$$



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