

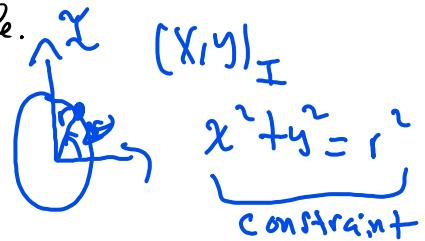
Ch 3 in KFDP Particle Dynamics

Constraints and Degrees of freedom (DOF)

Collection of particles: The number of DOF is the number of independent coordinates needed to describe the position of every particle.

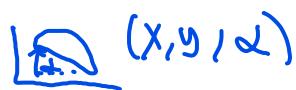
$$2\text{-D}: 2N - K = M$$

↓ ↑ ↗
 Particle Constraints DOF



$$3\text{-D}: M = 3N - K$$

Collection of rigid bodies: The number of DOF is the number of coordinates needed to describe the position and orientation of every body.



$$2\text{-D}: M = 3N - K$$

$$3\text{-D}: M = 6N - K$$

A constraint force reduces the number of DOF

and often acts orthogonal to direction of motion. In which case it is called a normal force.

Constraints can often be expressed algebraically.

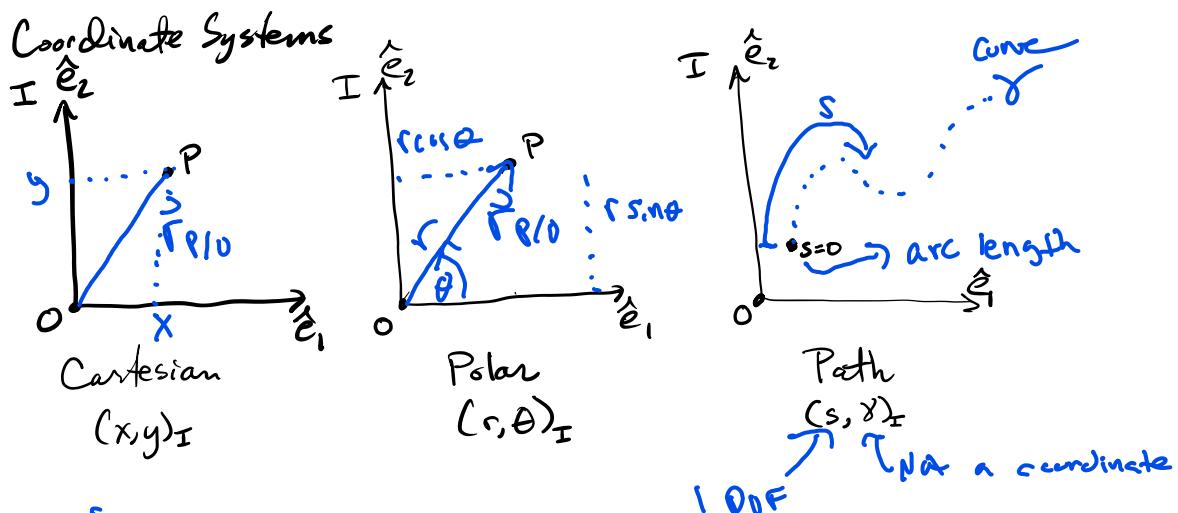
Ex. Particle on sphere

A diagram showing a particle on a sphere of radius R . The position vector is r_{pos} .

$$\| \vec{r}_{pos} \| = \sqrt{x^2 + y^2 + z^2} = R$$

We will re-visit constraints later in the course.

Inertial Particle Kinematics in the Plane



Description of systems motion based on geometry in reference frames only

Solving for the Kinematics of a particle (or rigid body) involves calculating the velocity and acceleration by differentiating the position vector w.r.t. time.

Cartesian coord:

$$\begin{aligned}\vec{r}_{P/I} &= x \hat{\mathbf{e}}_1 + y \hat{\mathbf{e}}_2 \\ \vec{v}_{P/I} &= \frac{d}{dt}(\vec{r}_{P/I}) = \dot{x} \hat{\mathbf{e}}_1 + \dot{y} \hat{\mathbf{e}}_2 \\ \vec{a}_{P/I} &= \frac{d}{dt}(\vec{v}_{P/I}) = \ddot{x} \hat{\mathbf{e}}_1 + \ddot{y} \hat{\mathbf{e}}_2\end{aligned}$$

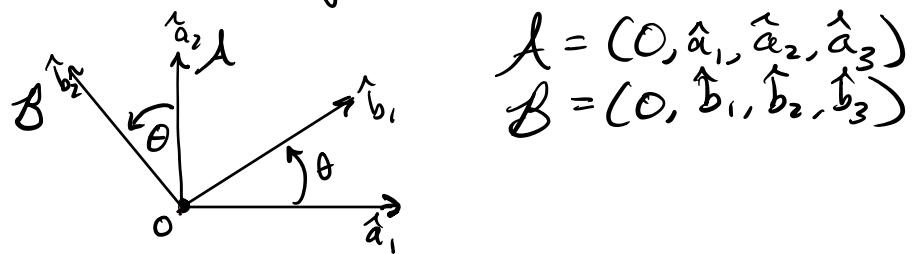
$$\text{Polar Coord.: } \vec{r}_{P/I} = r \cos \theta \hat{\mathbf{e}}_1 + r \sin \theta \hat{\mathbf{e}}_2$$

$$\vec{v}_{P/I} = \frac{d}{dt}(\vec{r}_{P/I}) = (\dot{r} \cos \theta - \dot{\theta} r \sin \theta) \hat{\mathbf{e}}_1 + (r \dot{\sin} \theta + \dot{\theta} r \cos \theta) \hat{\mathbf{e}}_2$$

$$\vec{a}_{P/I} = \frac{d}{dt}(\vec{v}_{P/I}) = (\ddot{r} \cos \theta - \dot{r} \dot{\theta} \sin \theta - \dot{r} \dot{\theta} \sin \theta - r \dot{\theta}^2 \cos \theta) \hat{\mathbf{e}}_1 + (\dot{r} \dot{\sin} \theta + 2\dot{r} \dot{\theta} \cos \theta + \ddot{r} \cos \theta - r \dot{\theta}^2 \sin \theta) \hat{\mathbf{e}}_2$$

Sometimes problems are easily solved when making use of different types of reference frames. Including moving & non-inertial frames.

Transforming between reference frames



$$\begin{aligned} A &= (O, \hat{a}_1, \hat{a}_2, \hat{a}_3) \\ B &= (O, \hat{b}_1, \hat{b}_2, \hat{b}_3) \end{aligned}$$

Transformation Table

	\hat{b}_1	\hat{b}_2
\hat{a}_1	$\langle \hat{a}_1, \hat{b}_1 \rangle$	$\langle \hat{a}_1, \hat{b}_2 \rangle$
\hat{a}_2	$\langle \hat{a}_2, \hat{b}_1 \rangle$	$\langle \hat{a}_2, \hat{b}_2 \rangle$

The (i, j) th entry represents the dot product between the i th row and j th column

	\hat{b}_1	\hat{b}_2
\hat{a}_1	$\cos\theta$	$-\sin\theta$
\hat{a}_2	$\sin\theta$	$\cos\theta$

$\stackrel{\text{TO}}{\downarrow} \quad \stackrel{\text{From}}{\swarrow}$

$${}^A C {}^B = \begin{bmatrix} \cos\theta & -\sin\theta \\ \sin\theta & \cos\theta \end{bmatrix}$$

$\stackrel{\text{From}}{\uparrow} \quad \stackrel{\text{To}}{\swarrow}$

$B \rightarrow A$

$$[\vec{f}_{AB}]_A = {}^A C {}^B [\vec{f}_{AB}]_B$$

This transformation table process results in
Transformation matrices.

Often, but not always, these transformation matrices are also rotation matrices. (If there is a reflection involved, the resulting matrix will not be a rotation matrix.)

An important property for rotation matrices:

$$({}^B C {}^A)^T = ({}^B C {}^A)^{-1} \quad \text{orthogonal matrices}$$

Now, if I know the ${}^A C {}^B$ is a rotation matrix,
I can find ${}^B C {}^A$ easily: $\det = +1$

$$[\vec{r}_{P/O}]_A = {}^A C {}^B [\vec{r}_{P/O}]_B$$

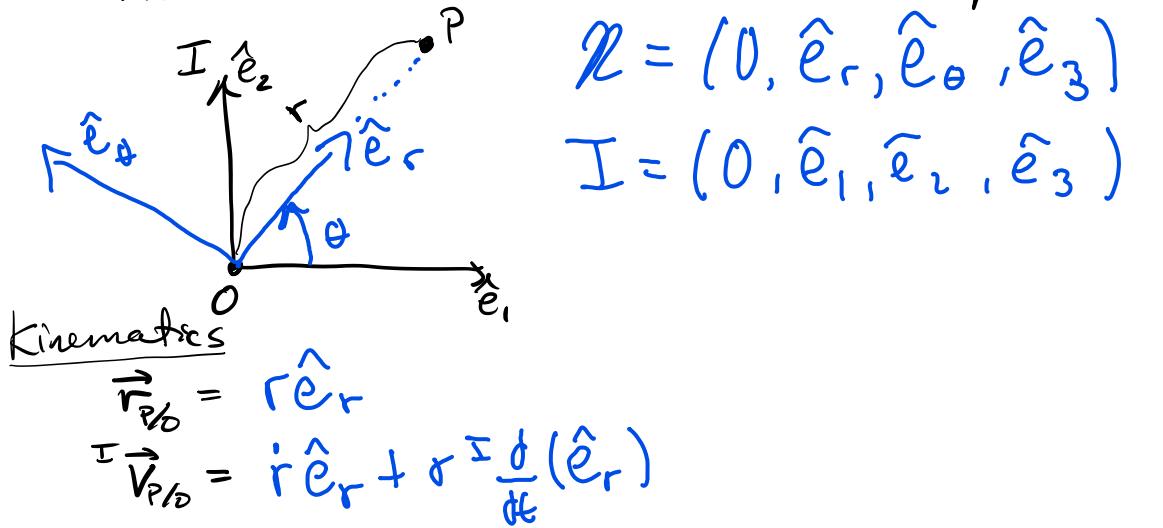
$$({}^A C {}^B)^{-1} [\vec{r}_{P/O}]_A = [\vec{r}_{P/O}]_B$$

or $[\vec{r}_{P/O}]_B = ({}^A C {}^B)^{-1} [\vec{r}_{P/O}]_A = \underbrace{({}^A C {}^B)^T}_{B C {}^A} [\vec{r}_{P/O}]_A$

$$B C {}^A$$

Polar Frame

↳ Reference frame that rotates to follow a point



$$\mathcal{R} = (0, \hat{e}_r, \hat{e}_\theta, \hat{e}_3)$$

$$I = (0, \hat{e}_1, \hat{e}_2, \hat{e}_3)$$

Option #1
Convert all
basis vectors
to I frame,
differentiate

Substitute $\vec{r}_{P/O} = r \hat{e}_r$
back

Transformation Table

	\hat{e}_r	\hat{e}_θ
\hat{e}_1	$\cos\theta$	$-\sin\theta$
\hat{e}_2	$\sin\theta$	$\cos\theta$

$$= {}^I C^R$$

$${}^I \vec{v}_{P/O} = \dot{r} \cos\theta \hat{e}_1 - r \sin\theta \dot{\theta} \hat{e}_1 + \dot{r} \sin\theta \hat{e}_2 + r \cos\theta \dot{\theta} \hat{e}_2$$

$${}^I \vec{a}_{P/O} = \ddot{r} (\cos\theta \hat{e}_1 + \sin\theta \hat{e}_2) + r \dot{\theta} (-\sin\theta \hat{e}_1 + \cos\theta \hat{e}_2)$$

$$= \dot{r} \hat{e}_r + r \dot{\theta} \hat{e}_\theta$$

Compare to

$$= \dot{r} \hat{e}_r + r \frac{d}{dt} (\hat{e}_r)$$

$${}^I \frac{d}{dt} (\hat{e}_r) = \dot{\theta} \hat{e}_\theta$$

Option #2: Differentiate unit vectors using the angular velocity vector

Angular velocity of R wrt I

$${}^I \vec{\omega} = \dot{\theta} \hat{e}_3$$

$$\begin{aligned} {}^I \frac{d}{dt}(\hat{e}_r) &= {}^I \frac{d}{dt}(\cos\theta \hat{e}_1 + \sin\theta \hat{e}_2) = \\ &= \dot{\theta} \underbrace{(-\sin\theta \hat{e}_1 + \cos\theta \hat{e}_2)}_{\hat{e}_\theta} = \dot{\theta} \hat{e}_\theta = \underbrace{\dot{\theta} (\hat{e}_3 \times \hat{e}_r)}_{{}^I \vec{\omega}} \end{aligned}$$

$${}^I \frac{d}{dt}(\hat{e}_r) = {}^I \vec{\omega} \times \hat{e}_r = \dot{\theta} \hat{e}_\theta$$

$${}^I \frac{d}{dt}(\hat{e}_\theta) = {}^I \vec{\omega} \times \hat{e}_\theta = -\dot{\theta} \hat{e}_r$$

Inertial kinematics of point P in the Polar Frame

$$\vec{r}_{P/O} = r \hat{e}_r$$

$${}^I \vec{v}_{P/O} = \dot{r} \hat{e}_r + r \dot{\theta} \hat{e}_\theta$$

$${}^I \vec{a}_{P/O} = \ddot{r} \hat{e}_r + 2\dot{r}\dot{\theta} \hat{e}_\theta + r\ddot{\theta} \hat{e}_\theta - r\dot{\theta}^2 \hat{e}_r$$

$${}^I \vec{a}_{P/O} = (\ddot{r} - r\dot{\theta}^2) \hat{e}_r + (2\dot{r}\dot{\theta} + r\ddot{\theta}) \hat{e}_\theta$$

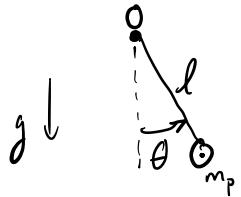
$$\vec{F}_P = m_P {}^I \vec{a}_{P/O}$$

$$\text{DOF: } M = 2N - n$$

$$2(1) - 1$$

$$r = l$$

Ex. Pendulum



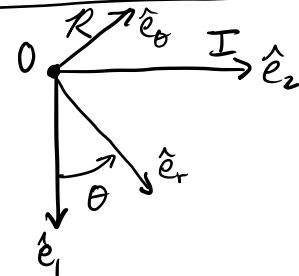
Kinematics:

$$\vec{r}_{P/O} = l \hat{e}_r$$

$$\vec{v}_{P/O} = l \dot{\theta} \hat{e}_\theta$$

$$\vec{a}_{P/O} = l \ddot{\theta} \hat{e}_\theta + l \dot{\theta}^2 \hat{e}_r$$

Reference Frames



FBD

$$\vec{T} = T \hat{e}_r$$

$$\vec{W} = mg \hat{e}_i$$

N2L:

$$\vec{F}_P = m_p \vec{a}_{P/O}$$

$$-T \hat{e}_r + m_p g \hat{e}_i = m_p (l \dot{\theta} \hat{e}_\theta - l \dot{\theta}^2 \hat{e}_r)$$

To get the scalar eqn of motion, we will try to stay in the polar \vec{R} frame; Let's convert the \hat{e}_i vector

$$-T \hat{e}_r + mg (\cos \theta \hat{e}_r - \sin \theta \hat{e}_\theta) = m_p (l \dot{\theta} \hat{e}_\theta - l \dot{\theta}^2 \hat{e}_r)$$

Equate coefficients

$$\hat{e}_r: -T + mg \cos \theta = -m_p l \dot{\theta}^2 \quad (\text{constraint force})$$

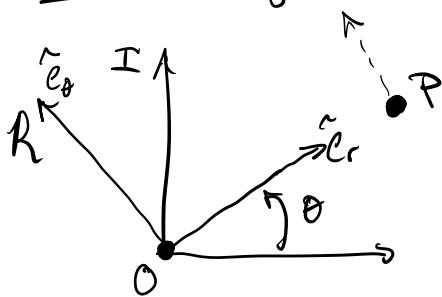
$$\hat{e}_\theta: mg \sin \theta = m_p l \ddot{\theta}$$

E.O.M

$$\ddot{\theta} = -\frac{g}{l} \sin\theta$$

1 DOF

Ex. Straight line motion using a polar frame



$$\overset{I}{\vec{a}}_{P/O} = (\ddot{r} - r\dot{\theta}^2)\hat{e}_r + (r\ddot{\theta} + 2\dot{r}\dot{\theta})\hat{e}_\theta$$

Centrifugal acceleration Coriolis acceleration

$$\vec{F}_P = m_p \overset{I}{\vec{a}}_{P/O}$$

$$0 = m_p ((\ddot{r} - r\dot{\theta}^2)\hat{e}_r + (r\ddot{\theta} + 2\dot{r}\dot{\theta})\hat{e}_\theta)$$

$$\Rightarrow \begin{aligned} \hat{e}_r : \ddot{r} &= r\dot{\theta}^2 \\ \hat{e}_\theta : \ddot{\theta} &= -\frac{2\dot{r}\dot{\theta}}{r} \end{aligned} \quad \left. \begin{array}{l} \text{Arise due} \\ \text{to rotating} \\ \text{frame effects} \end{array} \right\}$$