

ECE 68000: MODERN AUTOMATIC CONTROL

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Linear Quadratic Regulator (LQR)

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- The plant

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}, \quad \mathbf{x}(0) = \mathbf{x}_0$$

and the associated performance index

$$J = \int_0^{\infty} (\mathbf{x}^{\top} \mathbf{Q} \mathbf{x} + \mathbf{u}^{\top} \mathbf{R} \mathbf{u}) dt$$

where $\mathbf{Q} = \mathbf{Q}^{\top} \succeq 0$ and $\mathbf{R} = \mathbf{R}^{\top} \succ 0$

- Objective: construct a stabilizing linear state-feedback controller,

$$\mathbf{u} = -\mathbf{K}\mathbf{x}$$

that minimizes the performance index J

- Denote such a linear control law by \mathbf{u}^*

LQR development

- Assume that a linear state-feedback optimal controller exists such that the optimal closed-loop system

$$\dot{\mathbf{x}} = (\mathbf{A} - \mathbf{BK})\mathbf{x}$$

is asymptotically stable

- Hence there is a Lyapunov function $V = \mathbf{x}^\top \mathbf{P} \mathbf{x}$ for the closed-loop system, that is, for some $\mathbf{P} = \mathbf{P}^\top \succ 0$ the Lyapunov derivative dV/dt is negative definite

Theorem

If the state-feedback controller $\mathbf{u}^ = -\mathbf{K}\mathbf{x}$ is such that*

$$\min_{\mathbf{u}} \left(\frac{dV}{dt} + \mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^\top \mathbf{R} \mathbf{u} \right) = 0,$$

for some $V = \mathbf{x}^\top \mathbf{P} \mathbf{x}$, then the controller is optimal

Proof of the LQR theorem

- Rewrite the condition of the theorem as

$$\left. \frac{dV}{dt} \right|_{\mathbf{u}=\mathbf{u}^*} + \mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^{*\top} \mathbf{R} \mathbf{u}^* = 0$$

- Hence,

$$\left. \frac{dV}{dt} \right|_{\mathbf{u}=\mathbf{u}^*} = -\mathbf{x}^\top \mathbf{Q} \mathbf{x} - \mathbf{u}^{*\top} \mathbf{R} \mathbf{u}^*$$

- Integrate both sides of the resulting equation with respect to time from 0 to ∞

$$V(\mathbf{x}(\infty)) - V(\mathbf{x}(0)) = - \int_0^\infty (\mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^{*\top} \mathbf{R} \mathbf{u}^*) dt$$

Proof of the LQR theorem—contd.

- Since the closed-loop system is asymptotically stable, $\mathbf{x}(\infty) = \mathbf{0}$, and

$$V(\mathbf{x}(0)) = \mathbf{x}_0^\top \mathbf{P} \mathbf{x}_0 = \int_0^\infty (\mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^{*\top} \mathbf{R} \mathbf{u}^*) dt$$

- Thus, we showed that if a linear state-feedback controller satisfies the assumption of the theorem, then the value of the performance index for such a controller is

$$J(\mathbf{u}^*) = \mathbf{x}_0^\top \mathbf{P} \mathbf{x}_0$$

- To show that such a controller is indeed optimal, use a proof by contradiction
- Assume that \mathbf{u}^* is not optimal
- Suppose that $\tilde{\mathbf{u}}$ yields a smaller value of J , that is,

$$J(\tilde{\mathbf{u}}) < J(\mathbf{u}^*)$$

Proof of the LQR theorem—by contradiction

- Hence

$$\left. \frac{dV}{dt} \right|_{\mathbf{u}=\tilde{\mathbf{u}}} + \mathbf{x}^\top \mathbf{Q} \mathbf{x} + \tilde{\mathbf{u}}^\top \mathbf{R} \tilde{\mathbf{u}} \geq 0$$

that is,

$$\left. \frac{dV}{dt} \right|_{\mathbf{u}=\tilde{\mathbf{u}}} \geq -\mathbf{x}^\top \mathbf{Q} \mathbf{x} - \tilde{\mathbf{u}}^\top \mathbf{R} \tilde{\mathbf{u}}$$

- Integrating the above with respect to time from 0 to ∞ yields

$$V(\mathbf{x}(0)) \leq \int_0^\infty \left(\mathbf{x}^\top \mathbf{Q} \mathbf{x} + \tilde{\mathbf{u}}^\top \mathbf{R} \tilde{\mathbf{u}} \right) dt$$

implying that

$$J(\mathbf{u}^*) \leq J(\tilde{\mathbf{u}})$$

which is a contradiction, and the proof is complete.

Finding \mathbf{P}

- It follows from the above theorem that the synthesis of the optimal control law involves finding an appropriate Lyapunov function, or equivalently, the matrix \mathbf{P}
- The appropriate \mathbf{P} is found by minimizing

$$f(\mathbf{u}) = \frac{dV}{dt} + \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^\top \mathbf{R}\mathbf{u}$$

- Apply the necessary condition for unconstrained minimization

$$\left. \frac{\partial}{\partial \mathbf{u}} \left(\frac{dV}{dt} + \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^\top \mathbf{R}\mathbf{u} \right) \right|_{\mathbf{u}=\mathbf{u}^*} = \mathbf{0}^\top$$

Finding P —manipulations

- Differentiating yields

$$\begin{aligned}& \frac{\partial}{\partial \mathbf{u}} \left(\frac{dV}{dt} + \mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^\top \mathbf{R} \mathbf{u} \right) \\&= \frac{\partial}{\partial \mathbf{u}} (2\mathbf{x}^\top \mathbf{P} \dot{\mathbf{x}} + \mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^\top \mathbf{R} \mathbf{u}) \\&= \frac{\partial}{\partial \mathbf{u}} (2\mathbf{x}^\top \mathbf{P} \mathbf{A} \mathbf{x} + 2\mathbf{x}^\top \mathbf{P} \mathbf{B} \mathbf{u} + \mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^\top \mathbf{R} \mathbf{u}) \\&= 2\mathbf{x}^\top \mathbf{P} \mathbf{B} + 2\mathbf{u}^\top \mathbf{R} \\&= \mathbf{0}^\top\end{aligned}$$

Optimal control law

- Candidate for an optimal control law

$$\mathbf{u}^* = -\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P}\mathbf{x} = -\mathbf{K}\mathbf{x},$$

where $\mathbf{K} = \mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P}$

- Note that

$$\begin{aligned} & \frac{\partial^2}{\partial \mathbf{u}^2} \left(\frac{dV}{dt} + \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^\top \mathbf{R}\mathbf{u} \right) \\ &= \frac{\partial^2}{\partial \mathbf{u}^2} (2\mathbf{x}^\top \mathbf{P}\mathbf{A}\mathbf{x} + 2\mathbf{x}^\top \mathbf{P}\mathbf{B}\mathbf{u} + \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^\top \mathbf{R}\mathbf{u}) \\ &= \frac{\partial}{\partial \mathbf{u}} (2\mathbf{x}^\top \mathbf{P}\mathbf{B} + 2\mathbf{u}^\top \mathbf{R}) \\ &= 2\mathbf{R} \\ &\succ 0. \end{aligned}$$

- The second order sufficiency condition for \mathbf{u}^* to be optimal, that is, to minimize J satisfied

Closed-loop system driven by \mathbf{u}^*

- How to find appropriate \mathbf{P} ?
- The optimal closed-loop system

$$\dot{\mathbf{x}} = (\mathbf{A} - \mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P}) \mathbf{x}, \quad \mathbf{x}(0) = \mathbf{x}_0$$

- The optimal controller satisfies

$$\left. \frac{dV}{dt} \right|_{\mathbf{u}=\mathbf{u}^*} + \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^{*\top} \mathbf{R}\mathbf{u}^* = 0$$

that is,

$$2\mathbf{x}^\top \mathbf{P}\mathbf{A}\mathbf{x} + 2\mathbf{x}^\top \mathbf{P}\mathbf{B}\mathbf{u}^* + \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{u}^{*\top} \mathbf{R}\mathbf{u}^* = 0$$

Algebraic Riccati equation (ARE)

- Substitute the expression for \mathbf{u}^* into the above equation and represent it as

$$\begin{aligned} & \mathbf{x}^\top (\mathbf{A}^\top \mathbf{P} + \mathbf{P}\mathbf{A}) \mathbf{x} - 2\mathbf{x}^\top \mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P}\mathbf{x} \\ & + \mathbf{x}^\top \mathbf{Q}\mathbf{x} + \mathbf{x}^\top \mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P}\mathbf{x} \\ & = 0 \end{aligned}$$

- Factoring out \mathbf{x} yields

$$\mathbf{x}^\top (\mathbf{A}^\top \mathbf{P} + \mathbf{P}\mathbf{A} + \mathbf{Q} - \mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P}) \mathbf{x} = 0$$

- The above equation should hold for any \mathbf{x}
- For this to be true we have to have

$$\boxed{\mathbf{A}^\top \mathbf{P} + \mathbf{P}\mathbf{A} + \mathbf{Q} - \mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P} = \mathbf{O}}$$

CARE

- The equation

$$\boxed{\mathbf{A}^\top \mathbf{P} + \mathbf{P} \mathbf{A} + \mathbf{Q} - \mathbf{P} \mathbf{B} \mathbf{R}^{-1} \mathbf{B}^\top \mathbf{P} = \mathbf{O}}$$

is the *algebraic Riccati equation* (ARE) or *continuous-time algebraic Riccati equation* (CARE)

- In sum, the synthesis of the optimal linear state feedback controller minimizing the performance index

$$J = \int_0^\infty (\mathbf{x}^\top \mathbf{Q} \mathbf{x} + \mathbf{u}^\top \mathbf{R} \mathbf{u}) dt$$

subject to

$$\dot{\mathbf{x}} = \mathbf{A} \mathbf{x} + \mathbf{B} \mathbf{u}, \quad \mathbf{x}(0) = \mathbf{x}_0$$

requires solving the ARE

Example

- The plant:

$$\dot{x} = 2u_1 + 2u_2, \quad x(0) = 3,$$

and the associated performance index

$$J = \int_0^\infty (x^2 + ru_1^2 + ru_2^2) dt,$$

where $r > 0$ is a parameter

- Find the solution to the ARE, where

$$\mathbf{A} = 0, \quad \mathbf{B} = \begin{bmatrix} 2 & 2 \end{bmatrix}, \quad \mathbf{Q} = 1, \quad \mathbf{R} = r\mathbf{I}_2$$

- The ARE for this problem is

$$\mathbf{O} = \mathbf{A}^\top \mathbf{P} + \mathbf{P}\mathbf{A} + \mathbf{Q} - \mathbf{P}\mathbf{B}\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P} = 1 - \frac{8}{r}p^2,$$

whose solution is

$$p = \sqrt{\frac{r}{8}}$$

Example—contd.

- Write the equation of the closed-loop system driven by the optimal controller,

$$\mathbf{u} = -\mathbf{R}^{-1}\mathbf{B}^\top \mathbf{P}\mathbf{x} = -\frac{1}{\sqrt{2r}} \begin{bmatrix} 1 \\ 1 \end{bmatrix} x$$

- The closed-loop optimal system is described by

$$\dot{x} = \begin{bmatrix} 2 & 2 \end{bmatrix} \mathbf{u} = -\frac{4}{\sqrt{2r}}x$$

- Find the value of J for the optimal closed-loop system
- We have

$$J = \mathbf{x}(0)^\top \mathbf{P}\mathbf{x}(0) = \frac{9}{2}\sqrt{\frac{r}{2}}$$

Example—verification

- Verify that $J = \frac{9}{2}\sqrt{\frac{r}{2}}$ as follows:

$$\begin{aligned}\min J &= \min \int_0^\infty (x^2 + ru_1^2 + ru_2^2) dt \\ &= \int_0^\infty 9 \exp\left(-\frac{8t}{\sqrt{2r}}\right) (1 + 1) dt = 9 \frac{\sqrt{2r}}{4} = \frac{9}{2}\sqrt{\frac{r}{2}}\end{aligned}$$