

# **ECE 68000: MODERN AUTOMATIC CONTROL**

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Observer-Based Feedback Control Design:  
Further Analysis

# Observer-Based Feedback Control Design—Further Analysis

- **Objective:** Construct **Combined Observer-Controller Compensator** to control linear continuous-time (CT) or discrete-time (DT) system using only input-output info
- We consider linear time-varying (LTI) systems

$$\begin{aligned}\dot{\mathbf{x}}(t) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) \\ \mathbf{y}(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{D}\mathbf{u}(t)\end{aligned}$$

or

$$\begin{aligned}\mathbf{x}[k+1] &= \mathbf{A}\mathbf{x}[k] + \mathbf{B}\mathbf{u}[k] \\ \mathbf{y}[k] &= \mathbf{C}\mathbf{x}[k] + \mathbf{D}\mathbf{u}[k]\end{aligned}$$

- Assumption: the systems are reachable and observable

# Combined Observer-Controller Compensator

- The observer,

$$\dot{\tilde{\mathbf{x}}}(t) = \mathbf{A}\tilde{\mathbf{x}}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{L}(\mathbf{y}(t) - \tilde{\mathbf{y}}(t)),$$

- In our analysis of the closed-loop system driven by the combined observer-controller compensator, take into account that  $\tilde{\mathbf{y}}(t) = \mathbf{C}\tilde{\mathbf{x}}(t) + \mathbf{D}\mathbf{u}(t)$
- Substituting the above expressions for  $\tilde{\mathbf{y}}(t)$  gives

$$\begin{aligned}\dot{\tilde{\mathbf{x}}}(t) &= \mathbf{A}\tilde{\mathbf{x}}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{L}(\mathbf{y}(t) - \tilde{\mathbf{y}}(t)) \\ &= (\mathbf{A} - \mathbf{L}\mathbf{C})\tilde{\mathbf{x}}(t) + \mathbf{L}\mathbf{y}(t) + (\mathbf{B} - \mathbf{L}\mathbf{D})\mathbf{u}(t)\end{aligned}$$

# Combined Observer-Controller Compensator Analysis

- Taking into account that  $\mathbf{y}(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}\mathbf{u}(t)$  and  $\tilde{\mathbf{y}}(t) = \mathbf{C}\tilde{\mathbf{x}}(t) + \mathbf{D}\mathbf{u}(t)$ , we obtain

$$\begin{aligned}\dot{\tilde{\mathbf{x}}}(t) &= \mathbf{A}\tilde{\mathbf{x}}(t) + \mathbf{B}\mathbf{u}(t) + \mathbf{L}(\mathbf{y}(t) - \tilde{\mathbf{y}}(t)) \\ &= (\mathbf{A} - \mathbf{L}\mathbf{C})\tilde{\mathbf{x}}(t) + \mathbf{L}\mathbf{C}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)\end{aligned}$$

- Closed-loop system

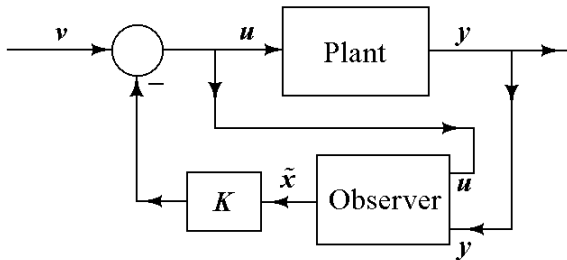
$$\left. \begin{aligned} \begin{bmatrix} \dot{\mathbf{x}}(t) \\ \dot{\tilde{\mathbf{x}}}(t) \end{bmatrix} &= \begin{bmatrix} \mathbf{A} & \mathbf{O} \\ \mathbf{L}\mathbf{C} & \mathbf{A} - \mathbf{L}\mathbf{C} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \tilde{\mathbf{x}}(t) \end{bmatrix} + \begin{bmatrix} \mathbf{B} \\ \mathbf{B} \end{bmatrix} \mathbf{u}(t) \\ \mathbf{y}(t) &= \begin{bmatrix} \mathbf{C} & \mathbf{O} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \tilde{\mathbf{x}}(t) \end{bmatrix} + \mathbf{D}\mathbf{u}(t) \end{aligned} \right\}$$

# Controller implementation

- The control law

$$\mathbf{u}(t) = -\mathbf{K}\tilde{\mathbf{x}}(t) + \mathbf{v}(t)$$

instead of the actual state-feedback control law



# Closed-loop system

- Closing the loop

$$\left. \begin{aligned} \begin{bmatrix} \dot{\mathbf{x}}(t) \\ \dot{\tilde{\mathbf{x}}}(t) \end{bmatrix} &= \begin{bmatrix} \mathbf{A} & \mathbf{O} \\ \mathbf{LC} & \mathbf{A} - \mathbf{LC} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \tilde{\mathbf{x}}(t) \end{bmatrix} + \begin{bmatrix} \mathbf{B} \\ \mathbf{B} \end{bmatrix} (-\mathbf{K}\tilde{\mathbf{x}}(t) + \mathbf{v}(t)) \\ \mathbf{y}(t) &= \begin{bmatrix} \mathbf{C} & \mathbf{O} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \tilde{\mathbf{x}}(t) \end{bmatrix} + \mathbf{D}(-\mathbf{K}\tilde{\mathbf{x}}(t) + \mathbf{v}(t)) \end{aligned} \right\}$$

- Perform manipulations,

$$\begin{aligned} \begin{bmatrix} \dot{\mathbf{x}}(t) \\ \dot{\tilde{\mathbf{x}}}(t) \end{bmatrix} &= \begin{bmatrix} \mathbf{A} & -\mathbf{BK} \\ \mathbf{LC} & \mathbf{A} - \mathbf{LC} - \mathbf{BK} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \tilde{\mathbf{x}}(t) \end{bmatrix} + \begin{bmatrix} \mathbf{B} \\ \mathbf{B} \end{bmatrix} \mathbf{v}(t) \\ \mathbf{y}(t) &= \begin{bmatrix} \mathbf{C} & -\mathbf{DK} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \tilde{\mathbf{x}}(t) \end{bmatrix} + \mathbf{D}\mathbf{v}(t) \end{aligned}$$

- To analyze the above closed-loop system, it is convenient to perform a change of coordinates

# Closed-loop system analysis

- Use the transformation

$$\begin{bmatrix} \mathbf{x} \\ \mathbf{x} - \tilde{\mathbf{x}} \end{bmatrix} = \begin{bmatrix} \mathbf{I}_n & \mathbf{O} \\ \mathbf{I}_n & -\mathbf{I}_n \end{bmatrix} \begin{bmatrix} \mathbf{x} \\ \tilde{\mathbf{x}} \end{bmatrix}$$

- Note that

$$\begin{bmatrix} \mathbf{I}_n & \mathbf{O} \\ \mathbf{I}_n & -\mathbf{I}_n \end{bmatrix}^{-1} = \begin{bmatrix} \mathbf{I}_n & \mathbf{O} \\ \mathbf{I}_n & -\mathbf{I}_n \end{bmatrix}$$

# Closed-loop system in the new coordinates

- The closed-loop system in the new coordinates

$$\begin{aligned} \begin{bmatrix} \dot{\mathbf{x}}(t) \\ \dot{\mathbf{x}}(t) - \dot{\tilde{\mathbf{x}}}(t) \end{bmatrix} &= \begin{bmatrix} \mathbf{A} - \mathbf{BK} & \mathbf{BK} \\ \mathbf{O} & \mathbf{A} - \mathbf{LC} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \mathbf{x}(t) - \tilde{\mathbf{x}}(t) \end{bmatrix} \\ &\quad + \begin{bmatrix} \mathbf{B} \\ \mathbf{O} \end{bmatrix} \mathbf{v}(t) \\ \mathbf{y}(t) &= \begin{bmatrix} \mathbf{C} - \mathbf{DK} & \mathbf{DK} \end{bmatrix} \begin{bmatrix} \mathbf{x}(t) \\ \mathbf{x}(t) - \tilde{\mathbf{x}}(t) \end{bmatrix} + \mathbf{D}\mathbf{v}(t) \end{aligned}$$

- The transfer function matrix of the closed-loop system

$$\mathbf{Y}(s) = \left( (\mathbf{C} - \mathbf{DK}) (s\mathbf{I}_n - \mathbf{A} + \mathbf{BK})^{-1} \mathbf{B} + \mathbf{D} \right) \mathbf{V}(s)$$

- The closed-loop system driven by the combined observer-controller compensator has the same transfer function as the system driven by the state-feedback control law  $\mathbf{u}(t) = -\mathbf{K}\mathbf{x}(t) + \mathbf{v}(t)$



# Implementing the combined observer-controller compensator for nonlinear systems

- Non-linear system  $\dot{\mathbf{x}} = f(\mathbf{x}, \mathbf{u})$ ,  $\mathbf{y} = \mathbf{h}(\mathbf{x}, \mathbf{u})$  linearized about  $(\mathbf{x}_e, \mathbf{u}_e)$
- Linearized model

$$\begin{aligned}\frac{d}{dt}\delta\mathbf{x} &= \mathbf{A}\delta\mathbf{x} + \mathbf{B}\delta\mathbf{u} \\ \delta\mathbf{y} &= \mathbf{C}\delta\mathbf{x} + \mathbf{D}\delta\mathbf{u}\end{aligned}$$

where

$$\delta\mathbf{x} = \mathbf{x} - \mathbf{x}_e, \quad \delta\mathbf{u} = \mathbf{u} - \mathbf{u}_e, \quad \text{and} \quad \delta\mathbf{y} = \mathbf{y} - \mathbf{y}_e$$

- Control law designed for the linearized system

$$\delta\mathbf{u} = -\mathbf{K}\delta\mathbf{x} + \mathbf{v}$$

# Observer for nonlinear systems

- Observer constructed for the linearized model

$$\begin{aligned}\frac{d}{dt}\delta\mathbf{x} &= \mathbf{A}\delta\mathbf{x} + \mathbf{B}\delta\mathbf{u} \\ \delta\mathbf{y} &= \mathbf{C}\delta\mathbf{x} + \mathbf{D}\delta\mathbf{u}\end{aligned}$$

- Observer

$$\begin{aligned}\frac{d}{dt}\mathbf{z} &= \mathbf{A}\mathbf{z} + \mathbf{B}\delta\mathbf{u} + \mathbf{L}(\delta\mathbf{y} - \delta\tilde{\mathbf{y}}) \\ \delta\tilde{\mathbf{y}} &= \mathbf{C}\mathbf{z} + \mathbf{D}\delta\mathbf{u}\end{aligned}$$

- Note that, for simplicity, I used  $\mathbf{z}$  instead of  $\delta\tilde{\mathbf{x}}$
- Observer's estimate  $\mathbf{z}$  estimates  $\delta\mathbf{x}$ , that is,  $\mathbf{z} \rightarrow \delta\mathbf{x}$
- Control law,  $\delta\mathbf{u} = -\mathbf{K}\mathbf{z} + \mathbf{v}$ , designed for the linearized system

# Combined observer-controller compensator for nonlinear systems

- Observer constructed for the linearized model
- Observer's estimate  $\mathbf{z} = \delta\tilde{\mathbf{x}}$  estimates  $\delta\mathbf{x}$
- Control law,  $\delta\mathbf{u} = -\mathbf{K}\delta\mathbf{x} + \mathbf{v}$ , designed for the linearized system
- Use  $\mathbf{z} = \delta\tilde{\mathbf{x}}$  instead of  $\delta\mathbf{x}$

$$\begin{aligned}\delta\mathbf{u} &= \mathbf{u} - \mathbf{u}_e \\ &= -\mathbf{K}\delta\tilde{\mathbf{x}} + \mathbf{v} \\ &= -\mathbf{K}\mathbf{z} + \mathbf{v}\end{aligned}$$

- Controller applied to the nonlinear system

$$\mathbf{u} = -\mathbf{K}\mathbf{z} + \mathbf{u}_e + \mathbf{v}$$