

# Software Requirements Specification for CVT Simulator: subtitle describing software

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October 7, 2024

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## Revision History

Date	Version	Notes
Date 1	1.0	Notes
Date 2	1.1	Notes

# 1 Reference Material

This section records information for easy reference.

## 1.1 Table of Units

Throughout this document SI (Système International d’Unités) is employed as the unit system. In addition to the basic units, several derived units are used as described below. For each unit, the symbol is given followed by a description of the unit and the SI name.

symbol	unit	SI
m	length	metre
kg	mass	kilogram
s	time	second
°C	temperature	centigrade
J	energy	joule
W	power	watt ( $W = J s^{-1}$ )
N	force	newtons ( $N = kg m s^{-2}$ )
Nm	torque	newton metre ( $Nm = kg m^2 s^{-2}$ )
rad	angle	radian

[Only include the units that your SRS actually uses. —TPLT]

[Derived units, like newtons, pascal, etc, should show their derivation (the units they are derived from) if their constituent units are in the table of units (that is, if the units they are derived from are used in the document). For instance, the derivation of pascals as  $Pa = N m^{-2}$  is shown if newtons and m are both in the table. The derivations of newtons would not be shown if kg and s are not both in the table. —TPLT]

[The symbol for units named after people use capital letters, but the name of the unit itself uses lower case. For instance, pascals use the symbol Pa, watts use the symbol W, teslas use the symbol T, newtons use the symbol N, etc. The one exception to this is degree Celsius. Details on writing metric units can be found on the [NIST web-page](#). —TPLT]

## 1.2 Table of Symbols

The table that follows summarizes the symbols used in this document along with their units. The choice of symbols was made to be consistent with the heat transfer literature and with existing documentation for solar water heating systems. The symbols are listed in alphabetical order.

symbol	unit	description
--------	------	-------------

$A_C$	$\text{m}^2$	coil surface area
$A_{\text{in}}$	$\text{m}^2$	surface area over which heat is transferred in

---

[Use your problems actual symbols. The si package is a good idea to use for units.  
—TPLT]

### 1.3 Abbreviations and Acronyms

symbol	description
A	Assumption
DD	Data Definition
GD	General Definition
GS	Goal Statement
IM	Instance Model
LC	Likely Change
PS	Physical System Description
R	Requirement
SRS	Software Requirements Specification
TM	Theoretical Model
RPM	Revolutions Per Minute
CVT	Continuous Variable Transmission
SEC	Secondary
PRIM	Primary

---

### 1.4 Mathematical Notation

N/A

[This SRS template is based on [Smith and Lai \(2005\)](#); [Smith et al. \(2007\)](#); [Smith and Koothoor \(2016\)](#). It will get you started. You should not modify the section headings, without first discussing the change with the course instructor. Modification means you are not following the template, which loses some of the advantage of a template, especially standardization. Although the bits shown below do not include type information, you may need to add this information for your problem. If you are unsure, please can ask the instructor. —TPLT]

[Feel free to change the appearance of the report by modifying the LaTeX commands. —TPLT]

[This template document assumes that a single program is being documented. If you are documenting a family of models, you should start with a commonality analysis. A separate template is provided for this. For program families you should look at [Smith \(2006\)](#); [Smith et al. \(2017\)](#). Single family member programs are often programs based on a single physical model. General purpose tools are usually documented as a family. Families of physical models also come up. —TPLT]

[The SRS is not generally written, or read, sequentially. The SRS is a reference document. It is generally read in an ad hoc order, as the need arises. For writing an SRS, and for reading one for the first time, the suggested order of sections is:

- Goal Statement
- Instance Models
- Requirements
- Introduction
- Specific System Description

—TPLT]

[Guiding principles for the SRS document:

- Do not repeat the same information at the same abstraction level. If information is repeated, the repetition should be at a different abstraction level. For instance, there will be overlap between the scope section and the assumptions, but the scope section will not go into as much detail as the assumptions section.

—TPLT]

[The template description comments should be disabled before submitting this document for grading. —TPLT]

[You can borrow any wording from the text given in the template. It is part of the template, and not considered an instance of academic integrity. Of course, you need to cite the source of the template. —TPLT]

[When the documentation is done, it should be possible to trace back to the source of every piece of information. Some information will come from external sources, like terminology. Other information will be derived, like General Definitions. —TPLT]

[An SRS document should have the following qualities: unambiguous, consistent, complete, validatable, abstract and traceable. —TPLT]

[The overall goal of the SRS is that someone that meets the Characteristics of the Intended Reader (Section 2.3) can learn, understand and verify the captured domain knowledge. They should not have to trust the authors of the SRS on any statements. They should be able to independently verify/derive every statement made. —TPLT]

## 2 Introduction

The McMaster Baja engineering team is facing challenges in tuning their Continuous Variable Transmission (CVT). The current process of tuning the CVT is extensive, time consuming and requires testing of multiple physical components leading to possible inconsistencies due to weather and wear. These inconsistencies then complicate the tuning process of the CVT's torque transfer directly affecting the performance of the Baja vehicles. To address these issues, our team aims to develop a CVT simulation tool that uses mathematical models, a rendering engine and a user-friendly interface. Our solution aims to streamline the optimization process allowing Baja members to simulate real-world factors and virtually test various tuning parameters. Our simulation tool will be validated against data collected by the McMaster Baja Data Acquisition team to ensure reliability and accuracy.

This introduction will outline the key objectives of this document to provide a structured guide for the development of the CVT tool and outline of the system's requirements. Additionally, the scope will explore technical and functional assumptions and will intend to streamline the complex tuning process of a CVT. A detailed overview of this document will provide guidance to the reader regarding the structure and flow of the document.

### 2.1 Purpose of Document

The purpose of this Software Requirements Specification (SRS) is to provide an outline of the system requirements given for the development of a CVT simulation tool. This ensures that all stakeholders including members of the Baja team, Dr. Smith and the developers understand the project's objectives and constraints. This document will serve as a communication tool to align expectations, provide guidance during the design of this tool and aid in the development and testing phases of this project. This SRS will be referenced throughout the development of the system to ensure the tool is within the scope and meets the outlined requirements.

### 2.2 Scope of Requirements

[Modelling the real world requires simplification. The full complexity of the actual physics, chemistry, biology is too much for existing models, and for existing computational solution techniques. Rather than say what is in the scope, it is usually easier to say what is not. You



can think of it as the scope is initially everything, and then it is constrained to create the actual scope. For instance, the problem can be restricted to 2 dimensions, or it can ignore the effect of temperature (or pressure) on the material properties, etc. —TPLT]

[The scope section is related to the assumptions section (Section 4.2.4). However, the scope and the assumptions are not at the same level of abstraction. The scope is at a high level. The focus is on the “big picture” assumptions. The assumptions section lists, and describes, all of the assumptions. —TPLT]

[The scope section is relevant for later determining typical values of inputs. The scope should make it clear what inputs are reasonable to expect. This is a distinction between scope and context (context is a later section). Scope affects the inputs while context affects how the software will be used. —TPLT]

This model will simulate as a closed system and will not consider environmental factors such as temperature, humidity, and wind. It also will not consider any unintended damage, forces or effects on the components of the CVT system. The system will not account for any relative displacement between the components of the CVT system due to driver input or external forces.

## 2.3 Characteristics of Intended Reader

Readers or reviewers of this SRS document should have a solid understanding of the principles of physics and calculus. Knowledge of the components in a Continuous Variable Transmission (CVT) and a basic understanding of how these parts work together will also be beneficial. Proficiency in these areas will be enough to comprehend the material in this document.

## 2.4 Organization of Document

This document is structured as follows:

- Section 3 discusses the general context and description of the system
- Section 4 details the specific system description, goals, and definitions
- Section 5 covers the system requirements
- Section 6 outlines the likely changes for the system
- Section 7 discusses the unlikely changes for the system
- Section 8 covers the traceability of the requirements

## 3 General System Description

This section provides general information about the system. It identifies the interfaces between the system and its environment, describes the user characteristics and lists the system constraints.

### 3.1 System Context

- User Responsibilities:
  - Provide the necessary input data in a correct format.
- CVT Simulator Responsibilities:
  - Accept user input data to simulate the CVT system.
  - Display the results of the simulation.

### 3.2 User Characteristics

The expected user of this application is someone who is very familiar with drivetrains and CVTs but not necessarily familiar with software. The software expects the user to know all of the components of a CVT and how they can be modified or adjusted. The user should also have enough of an understanding of undergraduate physics and calculus to be able to make sense of the outputs of the software. On the software side, the user should be able to navigate a GUI and know how to input data into the software.

### 3.3 System Constraints

The system should be able to run on any machine that supports Python 3.9 or later and Unity projects.

## 4 Specific System Description

This section first presents the problem description, which gives a high-level view of the problem to be solved. This is followed by the solution characteristics specification, which presents the assumptions, theories, definitions and finally the instance models.

### 4.1 Problem Description

The CVT simulator is intended to address the challenges faced by the McMaster Baja racing team when they tune their CVT. The current tuning process is time-consuming and requires physical testing of multiple components and configurations. This leads to inconsistencies in the tuning process due to weather and wear. The CVT simulator will allow the Baja team to virtually test different tuning parameters and simulate real-world factors that affect the CVT's performance.

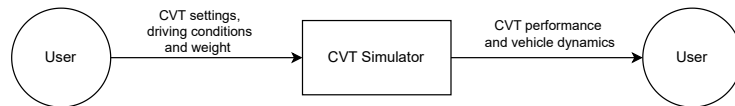


Figure 1: System Context

#### 4.1.1 Terminology and Definitions

[This section is expressed in words, not with equations. It provide the meaning of the different words and phrases used in the domain of the problem. The terminology is used to introduce concepts from the world outside of the mathematical model The terminology provides a real world connection to give the mathematical model meaning. —TPLT]

This subsection provides a list of terms that are used in the subsequent sections and their meaning, with the purpose of reducing ambiguity and making it easier to correctly understand the requirements:

- rpm
- CVT
- torque
- Primary RPM
- Secondary RPM
- Belt
- Ramp
- Fly Weight
- 

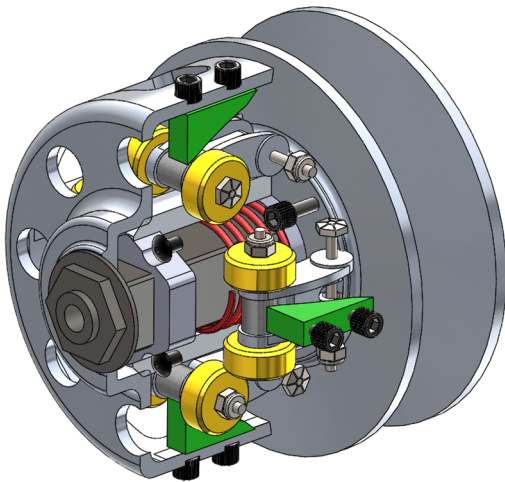


Figure 2: Primary CVT

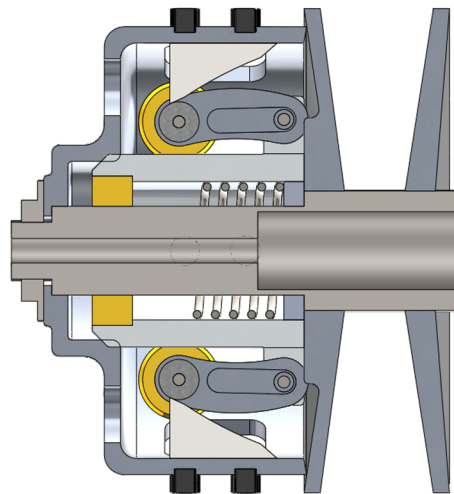


Figure 3: Primary CVT Side View

Note: The CVT that the McMaster Baja Team uses is slightly different from these figures but its mechanics are the same.

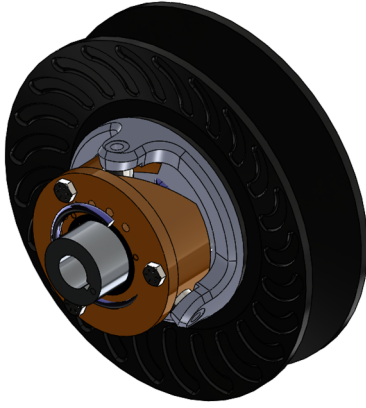


Figure 4: Secondary CVT

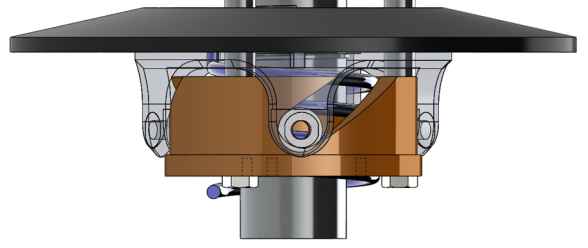


Figure 5: Secondary CVT Side View

#### 4.1.2 Physical System Description

The physical system of CVT Simulator, as shown in Figures 2-5, includes the following elements:

PS1: Fly weights

PS1a: mass ( $m_{\text{fly}}$ ) in kg.

PS1b: initial radius ( $r_{\text{fly\_init}}$ ) in m.

PS1c: final radius ( $r_{\text{fly\_final}}$ ) in m. Might not be needed, just a limit

PS2: Primary spring

PS2a: spring constant ( $k_{\text{prim}}$ ) in N/m.

PS2b: pretension ( $d_{\text{prim}}$ ) in m.

PS3: Primary ramp geometry function ( $f_{\text{prim\_angle}}$ )

PS3a: input distance ( $d_{\text{prim\_in}}$ ) in m.

PS3b: output angle ( $\theta_{\text{prim\_out}}$ ) in radians.

PS3: Primary ramp height function ( $f_{\text{prim\_height}}$ )

PS3a: input distance ( $d_{\text{prim\_in}}$ ) in m.

PS3c: output height ( $h_{\text{prim\_out}}$ ) in m.

PS4: Secondary spring

PS4a: compression spring constant ( $k_{\text{sec\_comp}}$ ) in N/m.

PS4b: torsional spring rate ( $k_{\text{sec\_tor}}$ ) in Nm/rad.

PS4c: pretension ( $d_{\text{sec}}$ ) in m.

PS5: Secondary ramp geometry function ( $f_{\text{sec}}$ )

PS5a: input distance ( $d_{\text{sec\_in}}$ ) in m.

PS5b: output angle ( $\theta_{\text{sec\_out}}$ ) in radians.

PS6: Weight

PS6a: driver weight ( $m_{\text{driver}}$ ) in kg.

PS6b: car weight ( $m_{\text{car}}$ ) in kg.

PS7: Engine torque function ( $f_{\text{engine}}$ )

PS7a: input angular velocity ( $\omega_{\text{engine}}$ ) in rad/s.

PS7b: output torque ( $T_{\text{engine}}$ ) in Nm.

PS8: Belt

PS8a: angle with sheave ( $\theta_{\text{belt}}$ ). I think this does not need to exist, it matches the sheave angle?

PS8b: friction coefficient ( $\mu_{\text{belt}}$ ), unitless.

PS9: Total reduction

PS9a: gearbox reduction ratio ( $r_{\text{gearbox}}$ ), unitless.

PS9b: wheel radius ( $r_{\text{wheel}}$ ) in m.

PS10: Coefficient of air resistance ( $\mu_{\text{air}}$ ), unitless.

PS11: Center to Center distance ( $d_{\text{center}}$ ) in m.

PS12: Angle on Incline ( $\theta_{\text{incline}}$ ) in radians.

PS13: Secondary Ramp Radius ( $r_{\text{sec\_ramp}}$ ) in m.

PS14: Traction ( $\mu_{\text{traction}}$ ), unitless.

We might also want belt length, belt width, belt weight?, other properties

### 4.1.3 Goal Statements

GS1: Simulates the kinematics of the vehicle

GS2: Simulates the output of the engine

GS3: Simulates the CVT system over time

## 4.2 Solution Characteristics Specification

[This section specifies the information in the solution domain of the system to be developed. This section is intended to express what is required in such a way that analysts and stakeholders get a clear picture, and the latter will accept it. The purpose of this section is to reduce the problem into one expressed in mathematical terms. Mathematical expertise is used to extract the essentials from the underlying physical description of the problem, and to collect and substantiate all physical data pertinent to the problem. —TPLT]

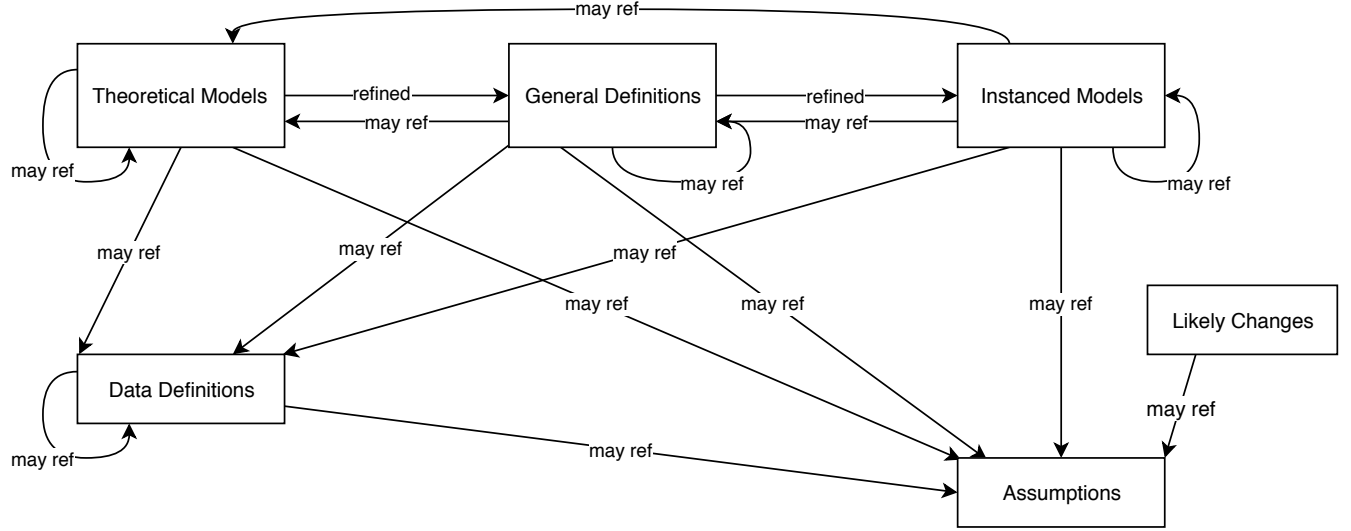
[This section presents the solution characteristics by successively refining models. It starts with the abstract/general Theoretical Models (TMs) and refines them to the concrete/specific Instance Models (IMs). If necessary there are intermediate refinements to General Definitions (GDs). All of these refinements can potentially use Assumptions (A) and Data Definitions (DD). TMs are refined to create new models, that are called GMs or IMs. DDs are not refined; they are just used. GDs and IMs are derived, or refined, from other models. DDs are not derived; they are just given. TMs are also just given, but they are refined, not used. If a potential DD includes a derivation, then that means it is refining other models, which would make it a GD or an IM. —TPLT]

[The above makes a distinction between “refined” and “used.” A model is refined to another model if it is changed by the refinement. When we change a general 3D equation to a 2D equation, we are making a refinement, by applying the assumption that the third dimension does not matter. If we use a definition, like the definition of density, we aren’t refining, or changing that definition, we are just using it. —TPLT]

[The same information can be a TM in one problem and a DD in another. It is about how the information is used. In one problem the definition of acceleration can be a TM, in another it would be a DD. —TPLT]

[There is repetition between the information given in the different chunks (TM, GDs etc) with other information in the document. For instance, the meaning of the symbols, the units etc are repeated. This is so that the chunks can stand on their own when being read by a reviewer/user. It also facilitates reuse of the models in a different context. —TPLT]

[The relationships between the parts of the document are show in the following figure. In this diagram “may ref” has the same role as “uses” above. The figure adds “Likely Changes,” which are able to reference (use) Assumptions. —TPLT]



The instance models that govern CVT Simulator are presented in Subsection 4.2.9. The information to understand the meaning of the instance models and their derivation is also presented, so that the instance models can be verified.

#### 4.2.1 Types

N/A

#### 4.2.2 Scope Decisions

N/A

#### 4.2.3 Modelling Decisions

N/A

#### 4.2.4 Assumptions

- A1: **Temperature variations** Ignore the effect of temperature on the material properties, excluding the belt.
- A2: **negligible Gravitational Influence:** The orientation of the CVT system and gravitational effects are considered negligible due to the high rotational speeds involved in the system's operation.
- A3: **Elasticity of Belts:** Elasticity of belts are assumed negligible, and the components are considered ideally rigid under normal operating conditions.



- A4: **Vibrational Effects:** Vibrational effects from the vehicle or external environment are assumed to be minimal and are not factored into the transmission’s operation in this model.
- A5: **Wear and Tear:** Component wear over time, including belt/chain wear and pulley degradation, is assumed negligible in the short-term operational model.
- A6: **Frictional Losses in Non-critical Components:** Frictional losses in non-critical components (e.g., bearings, shafts) are assumed negligible, focusing only on friction relevant to the CVT system’s core mechanics.
- A7: **Engine Behavior Assumption:** The engine is modeled to operate at full throttle with consistent power curves and peak performance, maintaining a uniform response throughout the analysis. Load feedback will be integrated to adjust RPM and power output as necessary.

#### 4.2.5 Theoretical Models

[Theoretical models are sets of abstract mathematical equations or axioms for solving the problem described in Section “Physical System Description” (Section 4.1.2). Examples of theoretical models are physical laws, constitutive equations, relevant conversion factors, etc. —TPLT]

[Optionally the theory section could be divided into subsections to provide more structure and improve understandability and reusability. Potential subsections include the following: Context theories, background theories, helper theories, generic theories, problem specific theories, final theories and rationale theories. —TPLT]

This section focuses on the general equations and laws that CVT Simulator is based on. [Modify the examples below for your problem, and add additional models as appropriate. —TPLT]

#### General Theories

This portion will specify the existing theories that are used in the development of the CVT simulation tool.

---

**RefName:** TM:HL

**Label:** Hookes Law

---

**Equation:**  $F = k\Delta x$

**Description:** F is the force (N)  
k is the spring constant (N/m)  
 $\Delta x$  is the displacement (m)

**Notes:** In the context of this project Hookes law is used in both a torsional and linear way.

**Source:** <https://www.britannica.com/science/Hookes-law>

**Ref. By:**

**Preconditions for TM:HL:** None

**Derivation for TM:HL:** Not Applicable

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---

**RefName:** TM:CF

**Label:** Centrifugal Force

---

**Equation:**  $F_c = m\omega^2 r$

**Description:** F is the force (N)

m is the mass (kg)

$\omega$  is the angular velocity (rad/s)

r is the radius (m)

**Notes:** None.

**Source:** <https://www.omnicalculator.com/physics/centrifugal-force>

**Ref. By:**

**Preconditions for TM:CF:** None

**Derivation for TM:CF:** Not Applicable

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---

**RefName:** TM:AR

**Label:** Air Resistance

---

**Equation:**  $F_d = \frac{1}{2}\rho v^2 C_d A$

**Description:** F is the force (N)  
 $\rho$  is the density of the fluid (kg/m<sup>3</sup>)  
v is the velocity of the object (m/s)  
 $C_d$  is the drag coefficient  
A is the cross-sectional area of the object (m<sup>2</sup>)

**Notes:** None.

**Source:** [https://softschools.com/formulas/physics/air\\_resistance\\_formula/85/](https://softschools.com/formulas/physics/air_resistance_formula/85/)

**Ref. By:**

**Preconditions for TM:AR:** None

**Derivation for TM:AR:** Not Applicable

---

---

**RefName:** TM:ET

**Label:** Engine Torque

---

**Equation:**  $\tau = \frac{P}{\omega}$

**Description:**  $\tau$  is the torque (N-m)  
P is the power (W)  
 $\omega$  is the angular velocity (rad/s)

**Notes:** None.

**Source:** <https://powertestdyno.com/how-to-calculate-horsepower/>

**Ref. By:**

**Preconditions for TM:ET:** None

**Derivation for TM:ET:** Not Applicable

---

---

**RefName:**    **TM:GR**

**Label:**    Secondary Torque

---

**Equation:**     $\tau_{\text{output}} = \tau_{\text{input}} \times \text{gear reduction}$

**Description:**     $\tau_{\text{output}}$  is the output torque (N-m)  
 $\tau_{\text{input}}$  is the input torque (N-m)

**Notes:**    None.

**Source:**

**Ref. By:**

**Preconditions for [TM:GR](#):**    None

**Derivation for [TM:GR](#):**    Not Applicable

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---

**RefName:**    **TM:FR**

**Label:**    Friction Formula

---

**Equation:**     $F_f = \mu F_n$

**Description:**     $\mu_{\text{effective}}$  is the effective coefficient of friction  
 $\mu_{\text{nominal}}$  is the nominal coefficient of friction  
 $\phi$  is the angle of wrap of the belt (radians)

**Notes:**    None.

**Source:**

**Ref. By:**

**Preconditions for [TM:FR](#):**    None

**Derivation for [TM:FR](#):**    Not Applicable

---

---

**RefName:** TM:DE

**Label:** Density

---

**Equation:**  $\rho = \frac{m}{V}$

**Description:**  $\rho$  is the density (kg/m<sup>3</sup>)  
m is the mass (kg)  
V is the volume (m<sup>3</sup>)

**Notes:** None.

**Source:** <https://www.britannica.com/science/density-physics>

**Ref. By:**

**Preconditions for TM:DE:** None

**Derivation for TM:DE:** Not Applicable

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---

**RefName:** TM:CE

**Label:** Capstan Equation

---

**Equation:**  $T_1 = T_2 e^{\mu\theta}$

**Description:**  $T_1$  is the tension on the first side of the belt (N)

$T_2$  is the tension on the second side of the belt (N)

$\mu$  is the coefficient of friction

$\theta$  is the angle of wrap of the belt (radians)

**Notes:** None.

**Source:** <https://hackaday.com/2021/01/26/cable-mechanism-maths-designing-against-the-capstan-equation/>

**Ref. By:**

**Preconditions for TM:CE:** None

**Derivation for TM:CE:** Not Applicable

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---

**RefName:** TM:N2

**Label:** Newtons 2nd Law

---

**Equation:**  $F = ma$

**Description:** F is the force (N)

m is the mass (kg)

a is the acceleration ( $\text{m/s}^2$ )

**Notes:** Newtons 2nd law is used repeatedly in several Instance models

**Source:** <https://www.physicsclassroom.com/class/newtlaws/lesson-3/newton-s-second-law>

**Ref. By:**

**Preconditions for TM:N2:** None

**Derivation for TM:N2:** Not Applicable

---

## Helper Theories

This portion will define auxiliary theories to aid in further derivation below.

Add here stuff like: - in: shift distance, out: radius of pulley - in: shift distance, out: angle of ramp - in: shift distance, out: angle of helix

[“Ref. By” is used repeatedly with the different types of information. This stands for Referenced By. It means that the models, definitions and assumptions listed reference the current model, definition or assumption. This information is given for traceability. Ref. By provides a pointer in the opposite direction to what we commonly do. You still need to have a reference in the other direction pointing to the current model, definition or assumption. As an example, if TM1 is referenced by GD2, that means that GD2 will explicitly include a reference to TM1. —TPLT]

### 4.2.6 General Definitions

We do not have any general definitions at this time.

### 4.2.7 Data Definitions

[The Data Definitions are definitions of symbols and equations that are given for the problem. They are not derived; they are simply used by other models. For instance, if a problem depends on density, there may be a data definition for the equation defining density. The DDs are given information that you can use in your other modules. —TPLT]

[All Data Definitions should be used (referenced) by at least one other model. —TPLT]

This section collects and defines all the data needed to build the instance models. The dimension of each quantity is also given. [Modify the examples below for your problem, and add additional definitions as appropriate. —TPLT]

data definitions so far, more to be added later

- velocity
- acceleration
- torque
- friction
- rpm

Number	DD1
Label	<b>Heat flux out of coil</b>
Symbol	$q_C$
SI Units	$\text{W m}^{-2}$
Equation	$q_C(t) = h_C(T_C - T_W(t))$ , over area $A_C$
Description	$T_C$ is the temperature of the coil ( $^{\circ}\text{C}$ ). $T_W$ is the temperature of the water ( $^{\circ}\text{C}$ ). The heat flux out of the coil, $q_C$ ( $\text{W m}^{-2}$ ), is found by assuming that Newton's Law of Cooling applies (A??). This law (GD??) is used on the surface of the coil, which has area $A_C$ ( $\text{m}^2$ ) and heat transfer coefficient $h_C$ ( $\text{W m}^{-2} ^{\circ}\text{C}^{-1}$ ). This equation assumes that the temperature of the coil is constant over time (A??) and that it does not vary along the length of the coil (A??).
Sources	Citation here
Ref. By	IM??

#### 4.2.8 Data Types

N/A

#### 4.2.9 Instance Models

This section transforms the problem defined in Section 4.1 into one which is expressed in mathematical terms. It uses concrete symbols defined in Section 4.2.7 to replace the abstract symbols in the models identified in Sections 4.2.5 and 4.2.6.

The goal statment GS1 are solved by Instance Models 1, 2 and 3

The goal statment GS3 are solved by Instance Models 4 and 5

Number	IM1
Label	<b>Acceleration</b>
Input	$r_{\text{gear}}, r_{\text{wheel}}, \rho, C_D, A, \theta, T_{\text{CVT}}, C_{\text{rr}}, m_v, m_d$
Equation	$a = \frac{\left(\frac{T_{\text{CVT}}}{r_{\text{gear}} + r_{\text{wheel}}}\right) - (C_{\text{rr}} F_g \sin(\theta)) - \left(\frac{1}{2} \rho v^2 C_D A\right) - (F_g \cos(\theta))}{m_v + m_d}$
Output	acceleration a
Description	$r_{\text{gear}}$ is the radius of the gear (m) $r_{\text{wheel}}$ is the radius of the wheel (m) $\rho$ is the density of the fluid (kg/m <sup>3</sup> ) $C_D$ is the drag coefficient $A$ is the cross-sectional area of the object (m <sup>2</sup> ) $\theta$ is the angle of incline ( $\theta$ ) $T_{\text{CVT}}$ is the torque transferred to the wheel (N-m) $C_{\text{rr}}$ is the coefficient of rolling resistance $m_v$ is the mass of the vehicle (kg) $m_d$ is the mass of the driver(kg)
Sources	-
Ref. By	

## Derivation of acceleration

The acceleration of the vehicle is derived as such:

$$T_W - R_r - F_D - F_g \cos(\theta) = ma$$

Where  $T_W$  is the torque of the wheel,  $R_r$  is the rolling resistance,  $F_D$  is the drag force,  $F_g$  is the gravitational force, and  $m$  is the mass of the vehicle.

$$T_W = \frac{T_{CVT}}{r_{\text{gear}} + r_{\text{wheel}}}$$

$$R_r = C_{rr} F_g \sin(\theta)$$

$$F_D = \frac{1}{2} \rho v^2 C_D A$$

$$m = m_v + m_d$$

Substitute the above equations into the original equation to get the final equation for acceleration.

$$a = \frac{\left( \frac{T_{CVT}}{r_{\text{gear}} + r_{\text{wheel}}} \right) - (C_{rr} F_g \sin(\theta)) - \left( \frac{1}{2} \rho v^2 C_D A \right) - (F_g \cos(\theta))}{m_v + m_d}$$

Number	IM2
Label	<b>Velocity</b>
Input	$a(t)$
Equation	$v(t) = \int a(t) dt$
Output	$v(t)$
Description	$a(t)$ is the function of acceleration over time
Sources	-
Ref. By	

Number	IM3
Label	<b>Distance</b>
Input	$v(t)$
Equation	$d(t) = \int v(t) dt$
Output	$d(t)$
Description	$v(t)$ is the function of velocity over time
Sources	-
Ref. By	

Number	IM4
Label	<b>Primary Clamping Force</b>
Input	$m, r_{\text{flyi}}, h_{\text{prim}}, F_{\text{prim}}(d_{\text{shift}}), K_{\text{prim}}, d_{\text{prc}}, d_{\text{shift}}$
Equation	$F_{FW} - F_S = m(r_{\text{flyi}} + F_{\text{primHeight}}(d_{\text{shift}})) \cdot \tan(F_{\text{prim}}(d_{\text{shift}})) + K_{\text{prim}}(d_{\text{prc}} + d_{\text{shift}})$
Output	$F_{FW} - F_S$ where $F_{FW}$ is the flywheel force and $F_S$ is the spring force, representing the total primary clamping force.
Description	<p><math>m</math>: Mass of the system.</p> <p><math>r_{\text{flyi}}</math>: Radius related to the flywheel.</p> <p><math>F_{\text{primHeight}}(d_{\text{shift}})</math>: Function that represents the height of the primary system.</p> <p><math>F_{\text{prim}}(d_{\text{shift}})</math>: Primary function that represents the force dependent on the shifting distance.</p> <p><math>K_{\text{prim}}</math>: Stiffness or coefficient related to the primary system.</p> <p><math>d_{\text{prc}}</math>: Pre-compression or pre-load distance.</p> <p><math>d_{\text{shift}}</math>: Displacement or shift in the system.</p>
Sources	
Ref. By	-

### Derivation of Primary Clamping Force

The flywheel force is derived as such:

$$F_{FW} = mr\omega^2 \cdot \tan(F_{\text{prim}}(d_{\text{shift}}))$$

Where  $r\omega^2$  can be represented by  $r_{\text{flyi}} + h_{\text{prim}}$

Then  $F_{FW}$  becomes  $m(r_{\text{flyi}} + h_{\text{prim}}) \cdot \tan(F_{\text{prim}}(d_{\text{shift}}))$

The spring force is derived as such:

$$-F_S = +K_{\text{prim}}(d_{\text{prc}} + d_{\text{shift}})$$

Combine those two forces to get the total primary clamping force.

$$F_{FW} - F_S = m(r_{\text{flyi}} + h_{\text{prim}}) \cdot \tan(F_{\text{prim}}(d_{\text{shift}})) + K_{\text{prim}}(d_{\text{prc}} + d_{\text{shift}})$$

Number	IM5
Label	<b>Secondary Clamping Force</b>
Input	$K_e, \theta_{\text{sec}}, \theta_{\text{shift}}, r_{\text{secramp}}, f_{\text{sec}}(d_{\text{shift}}), K_c, \delta_{\text{sec}}, d_{\text{shift}}$
Equation	$F_S + F_H = \frac{K_e(\theta_{\text{sec}} + \theta_{\text{shift}}) + T_{\text{eng}} CVT_{\text{ratio}}}{2 \cdot r_{\text{secramp}} \cdot \tan(f_{\text{sec}}(d_{\text{shift}}))} + K_c(\delta_{\text{sec}} + d_{\text{shift}})$
Output	$F_s + F_H$ where $F_S$ is spring clamping force and $F_H$ is the helix clamping force added together are the total the secondary clamping force
Description	<p><math>K_e</math>: Stiffness or spring constant related to elastic deformation.</p> <p><math>\theta_{\text{sec}}</math>: Secondary angle or rotational position.</p> <p><math>\theta_{\text{shift}}</math>: Shift in the secondary angle.</p> <p><math>r_{\text{secramp}}</math>: Radius or ramp characteristic related to the secondary system.</p> <p><math>f_{\text{sec}}(d_{\text{shift}})</math>: Function representing the force as a function of the secondary displacement or shift.</p> <p><math>K_c</math>: Stiffness or coefficient related to a damping or correction factor.</p> <p><math>\delta_{\text{sec}}</math>: Secondary deflection or displacement variable.</p> <p><math>d_{\text{shift}}</math>: Displacement or shift in the system.</p> <p><math>T_{\text{eng}}</math>: Torque of the engine.</p> <p><math>CVT_{\text{ratio}}</math>: Ratio of the CVT system.</p>
Sources	
Ref. By	-

## Derivation of Secondary Clamping Force

The spring force is derived as such:

$$F_S = \frac{K_e(\theta_{\text{sec}} + \theta_{\text{shift}})}{2 \cdot r_{\text{secramp}} \cdot \tan(f_{\text{sec}}(d_{\text{shift}}))} + K_c(\delta_{\text{sec}} + d_{\text{shift}})$$

The helix force is derived as such:

$$F_H = \frac{T_{\text{eng}} CVT_{\text{ratio}}}{2 \cdot r_{\text{secramp}} \cdot \tan(f_{\text{sec}}(d_{\text{shift}}))}$$

Combine those two forces to get the total secondary clamping force.

$$F_S + F_H = \frac{K_e(\theta_{\text{sec}} + \theta_{\text{shift}}) + T_{\text{eng}} CVT_{\text{ratio}}}{2 \cdot r_{\text{secramp}} \cdot \tan(f_{\text{sec}}(d_{\text{shift}}))} + K_c(\delta_{\text{sec}} + d_{\text{shift}})$$

Number	IM6
Label	<b>CVT Ratio</b>
Input	
Equation	
Output	
Description	
Sources	
Ref. By	-

Number	IM7
Label	<b>Torque Transferred</b>
Input	
Equation	
Output	
Description	
Sources	
Ref. By	-

Number	IM8
Label	<b>RPM and Torque of Engine</b>
Input	
Equation	
Output	
Description	
Sources	
Ref. By	-



#### 4.2.10 Input Data Constraints

Table 2 shows the data constraints on the input output variables. The column for physical constraints gives the physical limitations on the range of values that can be taken by the variable. The column for software constraints restricts the range of inputs to reasonable values. The software constraints will be helpful in the design stage for picking suitable algorithms. The constraints are conservative, to give the user of the model the flexibility to experiment with unusual situations. The column of typical values is intended to provide a feel for a common scenario. The uncertainty column provides an estimate of the confidence with which the physical quantities can be measured. This information would be part of the input if one were performing an uncertainty quantification exercise.

The specification parameters in Table 2 are listed in Table 4.

Table 2: Input Variables

Var	Physical Constraints	Software Constraints	Typical Value	Uncertainty
$L$	$L > 0$	$L_{\min} \leq L \leq L_{\max}$	1.5 m	10%
$m_{fly}$	$0 \leq m_{fly}$	$m_{fly} \leq 1$	0.2 kg	
$\omega_{engine}$	$0 \leq \omega_{engine}$	$\omega_{engine} \leq \omega_{\max}$	400 rad/s	
$d_{shift}$	$0 \leq d_{shift} \leq w_{belt}$		0.1 m	
$\theta_{prim\_out}$	$0 \leq \theta_{prim\_out} \leq \frac{\pi}{2}$		$\frac{\pi}{4}$ rad	
$d_{prim}$	$0 \leq d_{prim} \leq d_{\max\_prim\_pre}$		0.1 m	
$d_{sec}$	$0 \leq d_{sec} \leq d_{\max\_sec\_pre}$		0.1 rad	
$m_{driver}$	$0 \leq m_{driver}$	$m_{driver} \leq m_{\max\_human}$	75 kg	
$m_{car}$	$0 \leq m_{car}$	$m_{car} \leq m_{\max\_car}$	225 kg	
$k_{prim}$	$0 \leq k_{prim}$	$k_{prim} \leq k_{\max\_comp\_spring}$	100 N/m	
$k_{sec\_comp}$	$0 \leq k_{sec\_comp}$	$k_{sec\_comp} \leq k_{\max\_comp\_spring}$	100 N/m	
$k_{sec\_tor}$	$0 \leq k_{sec\_tor}$	$k_{sec\_tor} \leq k_{\max\_tor\_spring}$	50 Nm/rad	

(\*) [you might need to add some notes or clarifications —TPLT]

#### 4.2.11 Properties of a Correct Solution

A correct solution must exhibit [fill in the details —TPLT]. [These properties are in addition to the stated requirements. There is no need to repeat the requirements here. These additional properties may not exist for every problem. Examples include conservation laws (like conservation of energy or mass) and known constraints on outputs, which are usually summarized in tabular form. A sample table is shown in Table 6 —TPLT]

Table 4: Specification Parameter Values

Var	Value
$L_{\min}$	0.1 m
$\omega_{\max}$	600 rad/s
$w_{\text{belt}}$	UNKNOWN, see belt spec m
$d_{\text{max\_prim\_pre}}$	UNKNOWN, see CAD m
$d_{\text{max\_sec\_pre}}$	UNKNOWN, see CAD rad
$m_{\text{max\_human}}$	200 kg
$m_{\text{max\_car}}$	350 kg
$k_{\text{max\_comp\_spring}}$	1000 N/m
$k_{\text{max\_tor\_spring}}$	750 Nm/rad
$v_{\max}$	UNKNOWN, do gear calcs m/s
$f_{\text{belt\_max}}$	UNKNOWN, see belt spec N

Table 6: Output Variables

Var	Physical Constraints	unit
$T_W$	$T_{\text{init}} \leq T_W \leq T_C$ (by A??)	unitless
$v(t)$	$0 \leq v(t) \leq v_{\max}$	m/s
Sum of clamping forces	$\text{Clamp} \leq f_{\text{belt\_max}}$	N

[This section is not for test cases or techniques for verification and validation. Those topics will be addressed in the Verification and Validation plan. —TPLT]

## 5 Requirements

This section provides the functional requirements, the business tasks that the software is expected to complete, and the nonfunctional requirements, the qualities that the software is expected to exhibit.

### 5.1 Functional Requirements

- R1: The system shall simulate the behavior of the McMaster Baja Team's Continuous Variable Transmission(CVT) using mathematical models.
- R2: The system shall allow users to adjust the following CVT tuning parameters: primary weight, primary ramp geometry, primary spring rate, primary spring Pretension, secondary helix geometry, secondary spring rate, secondary spring pretension.
- R3: The system shall allow users to adjust vehicle and driver weight, traction and angle of incline in addition to the CVT tuning parameters.
- R4: The system shall provide users with an interface to input tuning parameters.
- R5: The system shall display graphs of simulation output based on the user inputted tuning parameters.
- R6: The system shall allow users to compare results of simulations with different CVT tuning parameters.
- R7: The system shall calculate the CVT ratio, clamping force, RPM, torque and belt slippage as functions of time. Combined with engine input, the system shall calculate distance, speed and acceleration as functions of time.
- R8: The system shall allow users to export outputted simulated graphical data.
- R9: The system shall allow users to access the application through the use of a personal computer or laptop.
- R10: The system shall be compatible with Windows, MacOS and Linux.

## 5.2 Nonfunctional Requirements

- NFR1: **Accuracy** The system shall achieve an accuracy of at least 95 % in correctly predicting CVT outputs.
- NFR2: **Usability** 85 % of a representative user group shall be able to successively input CVT parameters and receive CVT outputs on their first use.
- NFR3: **Maintainability** If a likely change is made to the finished software, it will take at most 10 % of the original development time, assuming the same development resources are available.
- NFR4: **Verifiability** The system shall output the resulting tuned CVT outputs which must be able to be cross-verified against data available through the McMaster Baja Team with a consistency rate of 95 %.

- NFR5: **Understandability** The system shall be understood by at least 90 % of a representative user group with no more than 15 minutes of initial training, as measured by assessing ability to generate and export tuned CVT output where users must score at least 90 %
- NFR6: **Reusability** The system's components shall be designed for reuse in the case the McMaster Baja team acquires a new CVT. These modifications should be made with minimal modifications, defined as requiring modification to less than 30 % of the code to configure these changes.

### 5.3 Rationale

The assumptions made for the CVT (Continuously Variable Transmission) system model aim to simplify its dynamics, making it easier to analyze and develop a solution. A key assumption is the exclusion of temperature effects on material properties, aside from the belt, which allows for a more straightforward focus on the mechanics of the interactions (A1). The negligible influence of gravitational forces, further simplifies the problem by removing the need to eliminating the need to consider variations in position. Additionally, the elasticity of belts is considered insignificant, treating components as ideally rigid, allowing the development of a model without accounting for material deformations (A3). Vibrational effects from external sources are also assumed to be minimal, avoiding the complexity of vibration-induced disturbances in the transmission behavior (A4). Wear and tear of components, including the belt and pulley are disregarded for short-term operational modeling, allowing for an idealized performance assumption (A5). Frictional losses in non-critical components, are deemed negligible, allowing the focus to frictional effects that directly impact the CVT's core mechanics (A6). Finally, the engine is assumed to operate at full throttle with consistent power delivery, simplifying the model by maintaining uniform engine behavior (A4). These simplifications affect the process of formulating equations governing velocity, distance, primary clamping force, secondary clamping force, CVT Ratio, Torque transfer and RPM and Torque of the Engine(IM1-IM8)

## 6 Likely Changes

- LC1: The effect of temperature on material properties might be included in the future, (A1)
- LC2: The elasticity of the belt might be considered in the future, (A3)
- LC3: Frictional losses in non-critical components might be considered in the future, (A6)
- LC4: Some of the math models will most likely change as the design is refined.

## 7 Unlikely Changes

None

## 8 Traceability Matrices and Graphs

The purpose of the traceability matrices is to provide easy references on what has to be additionally modified if a certain component is changed. Every time a component is changed, the items in the column of that component that are marked with an “X” may have to be modified as well. Table 8 shows the dependencies of theoretical models, general definitions, data definitions, and instance models with each other. Table 9 shows the dependencies of instance models, requirements, and data constraints on each other. Table 10 shows the dependencies of theoretical models, general definitions, data definitions, instance models, and likely changes on the assumptions.

[You will have to modify these tables for your problem. —TPLT]

[The traceability matrix is not generally symmetric. If GD1 uses A1, that means that GD1’s derivation or presentation requires invocation of A1. A1 does not use GD1. A1 is “used by” GD1. —TPLT]

[The traceability matrix is challenging to maintain manually. Please do your best. In the future tools (like Drasil) will make this much easier. —TPLT]

	TM??	TM??	TM??	GD??	GD??	DD1	DD??	DD??	DD??	IM??	IM??	IM??
TM??												
TM??			X									
TM??												
GD??												
GD??	X											
DD1				X								
DD??				X								
DD??												
DD??								X				
IM??					X	X	X				X	
IM??					X		X		X	X		
IM??		X										
IM??		X	X				X	X	X		X	

Table 8: Traceability Matrix Showing the Connections Between Items of Different Sections

The purpose of the traceability graphs is also to provide easy references on what has to be additionally modified if a certain component is changed. The arrows in the graphs represent

	IM??	IM??	IM??	IM??	<a href="#">4.2.10</a>	R??	R??
IM??		X				X	X
IM??	X			X		X	X
IM??						X	X
IM??		X				X	X
R??							
R??						X	
R??					X		
R??	X	X				X	X
R??	X						
R??		X					
R??			X				
R??				X			
R??			X	X			
R??		X					
R??		X					

Table 9: Traceability Matrix Showing the Connections Between Requirements and Instance Models

	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??	A??
TM??	X																		
TM??																			
TM??																			
GD??		X																	
GD??			X	X	X	X													
DD1							X	X	X										
DD??			X	X						X									
DD??																			
DD??																			
IM??											X	X		X	X	X			X
IM??												X	X			X	X	X	
IM??														X					X
IM??													X					X	
LC??				X															
LC??								X											
LC??									X										
LC??											X								
LC??												X							
LC??															X				

Table 10: Traceability Matrix Showing the Connections Between Assumptions and Other Items

dependencies. The component at the tail of an arrow is depended on by the component at the head of that arrow. Therefore, if a component is changed, the components that it points to should also be changed. Figure ?? shows the dependencies of theoretical models, general definitions, data definitions, instance models, likely changes, and assumptions on each other. Figure ?? shows the dependencies of instance models, requirements, and data constraints on each other.

## 9 Development Plan

[This section is optional. It is used to explain the plan for developing the software. In particular, this section gives a list of the order in which the requirements will be implemented. In the context of a course this is where you can indicate which requirements will be implemented as part of the course, and which will be “faked” as future work. This section can be organized as a prioritized list of requirements, or it could should the requirements that will be implemented for “phase 1”, “phase 2”, etc. —TPLT]

## 10 Values of Auxiliary Constants

[Show the values of the symbolic parameters introduced in the report. —TPLT]

[The definition of the requirements will likely call for SYMBOLIC\_CONSTANTS. Their values are defined in this section for easy maintenance. —TPLT]

[The value of FRACTION, for the Maintainability NFR would be given here. —TPLT]



## References

- W. Spencer Smith. Systematic development of requirements documentation for general purpose scientific computing software. In *Proceedings of the 14th IEEE International Requirements Engineering Conference, RE 2006*, pages 209–218, Minneapolis / St. Paul, Minnesota, 2006. URL <http://www.ifi.unizh.ch/req/events/RE06/>.
- W. Spencer Smith and Nirmitha Koothoor. A document-driven method for certifying scientific computing software for use in nuclear safety analysis. *Nuclear Engineering and Technology*, 48(2):404–418, April 2016. ISSN 1738-5733. doi: <http://dx.doi.org/10.1016/j.net.2015.11.008>. URL <http://www.sciencedirect.com/science/article/pii/S1738573315002582>.
- W. Spencer Smith and Lei Lai. A new requirements template for scientific computing. In J. Ralyté, P. Ågerfalk, and N. Kraiem, editors, *Proceedings of the First International Workshop on Situational Requirements Engineering Processes – Methods, Techniques and Tools to Support Situation-Specific Requirements Engineering Processes, SREP’05*, pages 107–121, Paris, France, 2005. In conjunction with 13th IEEE International Requirements Engineering Conference.
- W. Spencer Smith, Lei Lai, and Ridha Khedri. Requirements analysis for engineering computation: A systematic approach for improving software reliability. *Reliable Computing, Special Issue on Reliable Engineering Computation*, 13(1):83–107, February 2007.
- W. Spencer Smith, John McCutchan, and Jacques Carette. Commonality analysis for a family of material models. Technical Report CAS-17-01-SS, McMaster University, Department of Computing and Software, 2017.

[The following is not part of the template, just some things to consider when filing in the template. —TPLT]

[Grammar, flow and L<sup>A</sup>T<sub>E</sub>X advice:

- For Mac users \*.DS\_Store should be in .gitignore
- L<sup>A</sup>T<sub>E</sub>X and formatting rules
  - Variables are italic, everything else not, includes subscripts ([link to document](#))
    - \* [Conventions](#)
    - \* Watch out for implied multiplication
  - Use BibTeX
  - Use cross-referencing
- Grammar and writing rules
  - Acronyms expanded on first usage (not just in table of acronyms)
  - “In order to” should be “to”

—TPLT]

[Advice on using the template:

- Difference between physical and software constraints
- Properties of a correct solution means *additional* properties, not a restating of the requirements (may be “not applicable” for your problem). If you have a table of output constraints, then these are properties of a correct solution.
- Assumptions have to be invoked somewhere
- “Referenced by” implies that there is an explicit reference
- Think of traceability matrix, list of assumption invocations and list of reference by fields as automatically generatable
- If you say the format of the output (plot, table etc), then your requirement could be more abstract

—TPLT]

## Appendix — Reflection

[Not required for CAS 741 —SS]

The information in this section will be used to evaluate the team members on the graduate attribute of Lifelong Learning.

The purpose of reflection questions is to give you a chance to assess your own learning and that of your group as a whole, and to find ways to improve in the future. Reflection is an important part of the learning process. Reflection is also an essential component of a successful software development process.

Reflections are most interesting and useful when they're honest, even if the stories they tell are imperfect. You will be marked based on your depth of thought and analysis, and not based on the content of the reflections themselves. Thus, for full marks we encourage you to answer openly and honestly and to avoid simply writing “what you think the evaluator wants to hear.”

Please answer the following questions. Some questions can be answered on the team level, but where appropriate, each team member should write their own response:

1. What went well while writing this deliverable?
2. What pain points did you experience during this deliverable, and how did you resolve them?
3. How many of your requirements were inspired by speaking to your client(s) or their proxies (e.g. your peers, stakeholders, potential users)?
4. Which of the courses you have taken, or are currently taking, will help your team to be successful with your capstone project.
5. What knowledge and skills will the team collectively need to acquire to successfully complete this capstone project? Examples of possible knowledge to acquire include domain specific knowledge from the domain of your application, or software engineering knowledge, mechatronics knowledge or computer science knowledge. Skills may be related to technology, or writing, or presentation, or team management, etc. You should look to identify at least one item for each team member.
6. For each of the knowledge areas and skills identified in the previous question, what are at least two approaches to acquiring the knowledge or mastering the skill? Of the identified approaches, which will each team member pursue, and why did they make this choice?