

## Springs and Dampers - Motivation

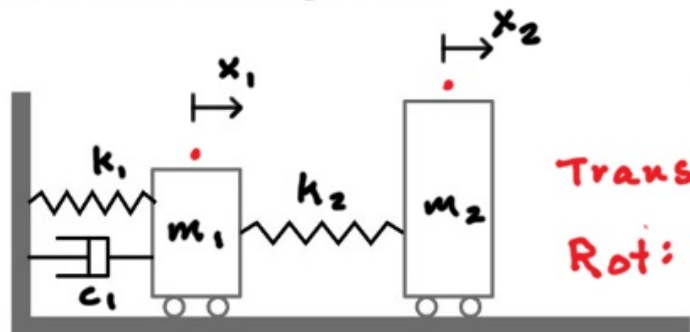
1. Dynamic systems that have spring behavior, but no physical springs, can be modeled with springs.
2. Systems with multiple bodies that are connected with a compliant joint, can also be modeled with springs, sometimes in series or in parallel
3. All dynamic systems lose energy over time. Introducing a damping is one way to capture this effect, even if there are no physical dampers.



## **Skills**

1. Given a lumped system with several springs or dampers in series or parallel, create a single equivalent spring or damper
2. Be able to correctly define the variables of motion for a lumped parameter system with springs and dampers

## Notation and Symbols

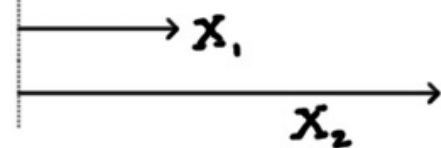
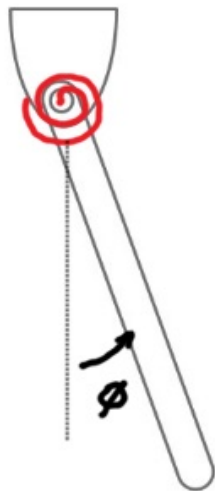


Units

Trans:  $k \left( \frac{N}{m} \right), c \left( \frac{N}{m/s} \right)$

Rot:  $K \left( \frac{N \cdot m}{rad} \right), c \left( \frac{N \cdot m}{rad/s} \right)$

Torsional  
Spring/Damper



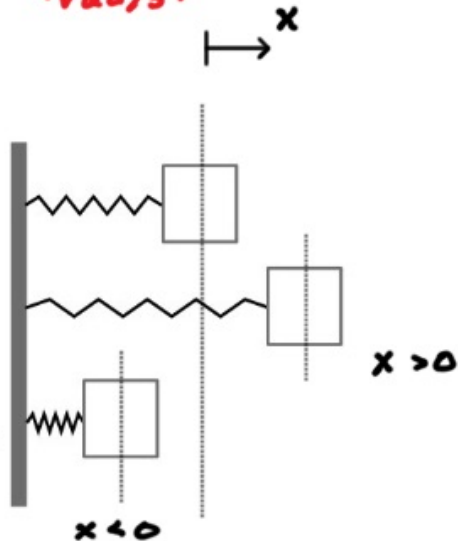
$$X_1 = x_{1,us} + x_1$$

$$X_2 = (x_{1,us} + x_{2,us}) + x_2$$

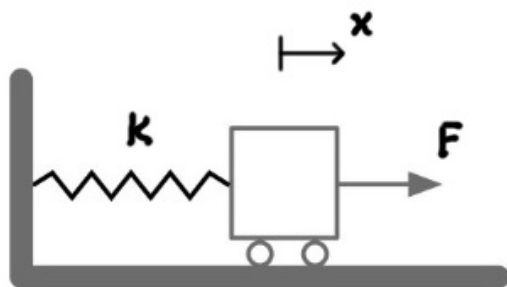
unstretched

tension

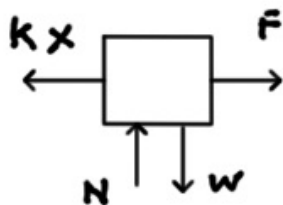
compression



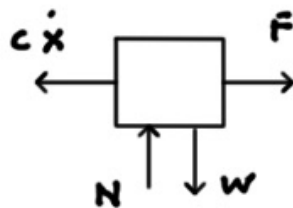
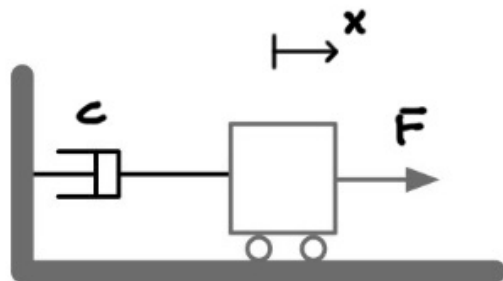
## Sign Convention



FBD



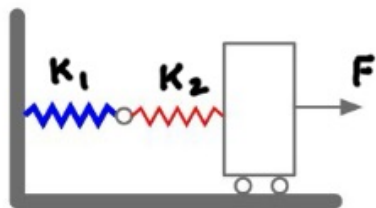
$$F_s = -kx$$



$$F_{\text{damp}} = -c\dot{x}$$

## Springs (Dampers) in Series and Parallel

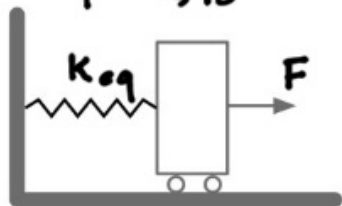
Series



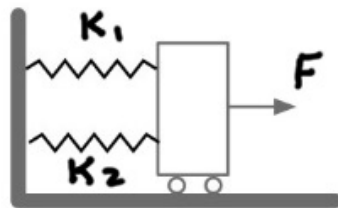
$$\frac{1}{K_{eq}} = \frac{1}{K_1} + \frac{1}{K_2} = \frac{K_1 K_2}{K_1 + K_2}$$

E.g.  $K_1 = 500 \frac{N}{m}$   $K_2 = 10 \frac{N}{m}$

$$K_{eq} = \frac{5000}{510} \approx 9.8 \frac{N}{m}$$

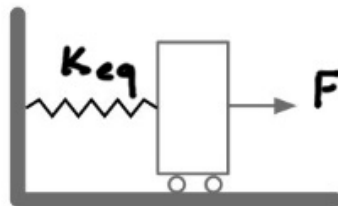


Parallel



$$K_{eq} = K_1 + K_2$$

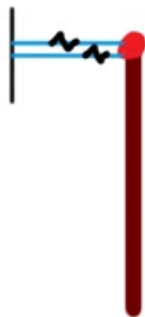
E.g.  $K_{eq} = 510 \frac{N}{m}$



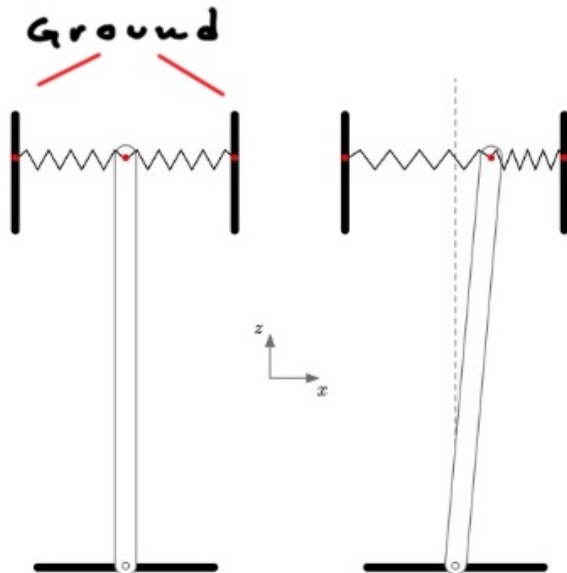
## Example 1

Calculate the equivalent spring constant and sketch the new system.

Same as:

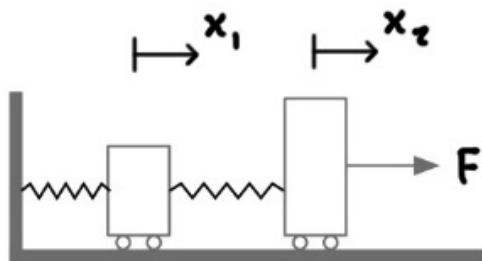


Parallel  
 $K_{eq} = 2K$



## FBDs - Variables of Motion

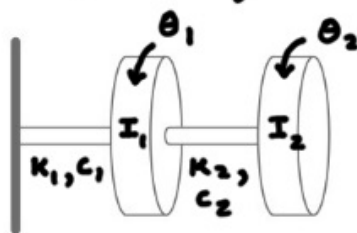
You can always use a single, inertial reference to define motions, but for systems with springs, we almost always define motion variables as deviations from the equilibrium configuration.



More  
Notation...

$x_1$  &  $x_2$  have different,  
but fixed (inertial)  
references.

Torsional stiffness,  
damping in shafts

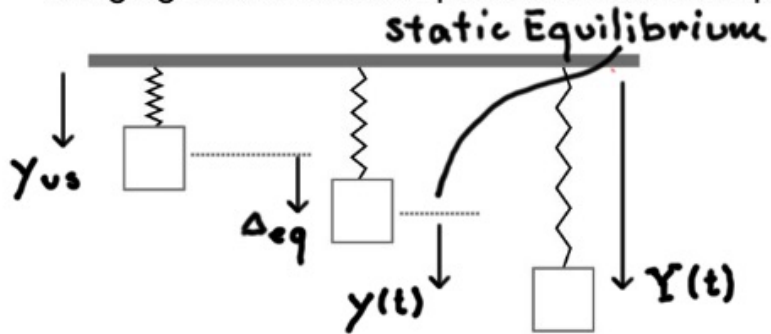


End View



## FBDs - Variables of Motion - Hanging Bodies

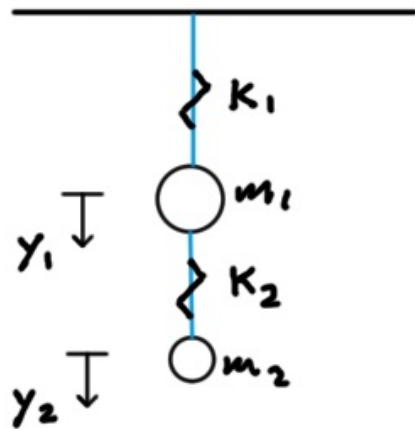
The common practice of defining motion relative to static equilibrium is the same, however, for hanging bodies static equilibrium doesn't equate to unstretched as it does for translating bodies.



$$Y = y_{us} + \Delta_{eq} + y$$

relative  
to  
static  
equil.

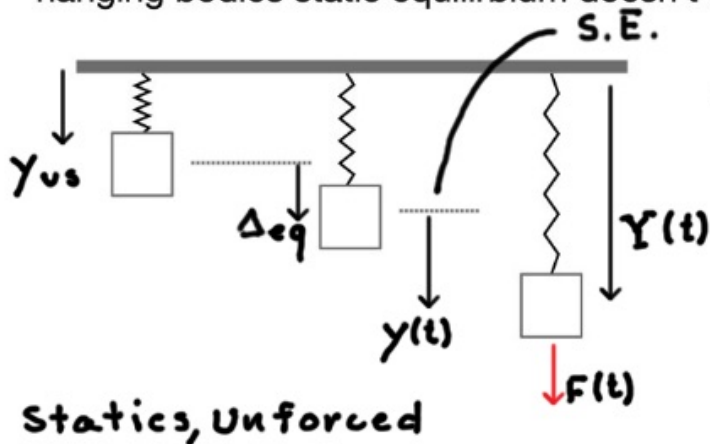
2 mass example





## FBDs - Variables of Motion - Hanging Bodies

The common practice of defining motion relative to static equilibrium is the same, however, for hanging bodies static equilibrium doesn't equate to unstretched as it does for translating bodies.



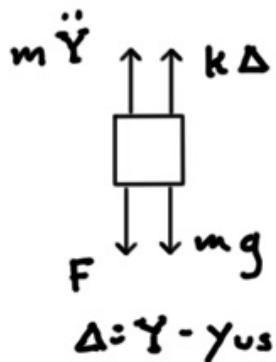
$$-m\ddot{Y} - k(Y - y_{us}) + F + mg = 0 \quad (1)$$

$$Y(t) = y_{us} + \Delta_{eq} + y(t) \quad (2)$$

Sub (2) into (1)

$$-m\ddot{y} - k(\Delta_{eq} + y) + F + mg = 0$$

$$m\ddot{y} + k(\Delta_{eq} + y) = F + mg \quad (4)$$



Sub (3) into (4)

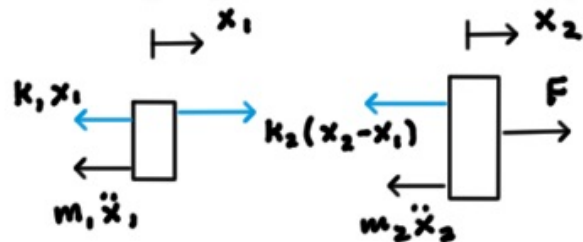
$$m\ddot{y} + Ky = F$$

Defining  $y$  rel. to  $\Delta_{eq}$  removes  $g$  from DEQ model

## FBDs - Spring and Damper Forces of Connected Bodies

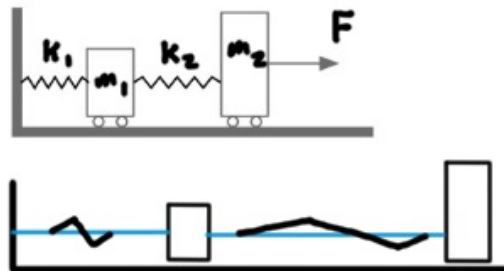
Assuming you've started the FBD process and now it's time to annotate them with spring or damper forces...

1. Virtually, apply a different positive displacement to each body
2. For each spring in the displaced configuration, create an expression for the force (or moment) magnitude and direction it exerts on the body it is attached to. If it's attached to two bodies, then apply the same force (or moment) expression, but in the opposite direction.



DEQ Model

$$\begin{aligned} m_1 \ddot{x}_1 + k_1 x_1 - k_2 (x_2 - x_1) &= 0 \\ m_2 \ddot{x}_2 + k_2 (x_2 - x_1) &= F \end{aligned}$$



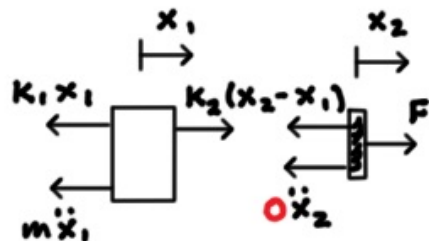
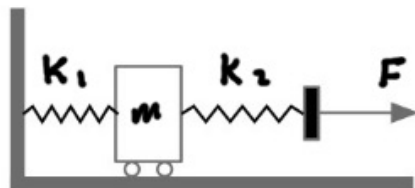
Sanity Check

← All  $x_1$  terms +

← All  $x_2$  terms +

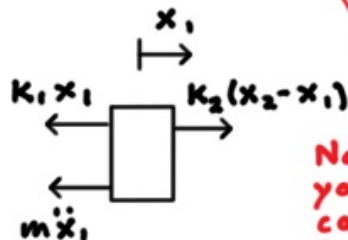
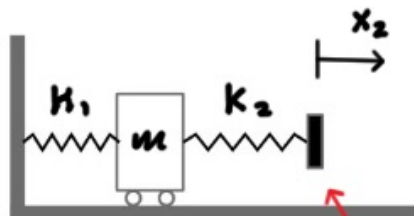
## FBDs - Massless Bodies and Imposed Motion

Sometimes motion is enforced on the system, or a force (moment) is applied directly to the spring or damper. The notation takes practice. Treat the massless object like any other FBD and the equations will develop nicely.



$$m\ddot{x}_1 + K_1 x_1 - K_2(x_2 - x_1) = 0$$

$$K_2(x_2 - x_1) = F \quad \text{So,} \quad m\ddot{x}_1 + K_1 x_1 = F$$



$$m\ddot{x}_1 + K_1 x_1 - K_2(x_2 - x_1) = 0$$

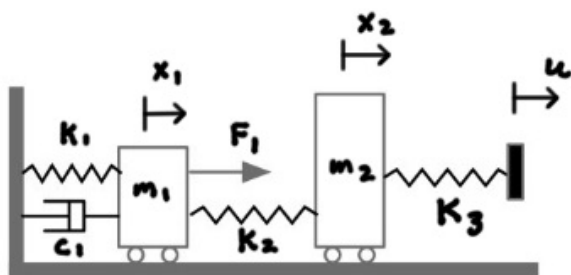
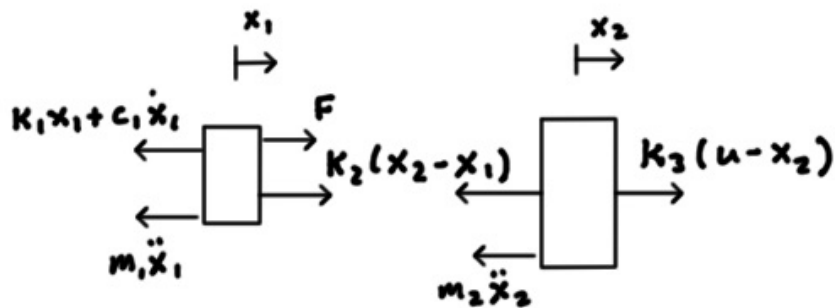
$$m\ddot{x}_1 + (K_1 + K_2)x_1 = K_2 x_2$$

$x_2$  is an imposed motion, an input.

No FBD, unless you need to calc  $F$  req'd to cause the motion...

## Example 2

Develop the FBDs for the system at right.



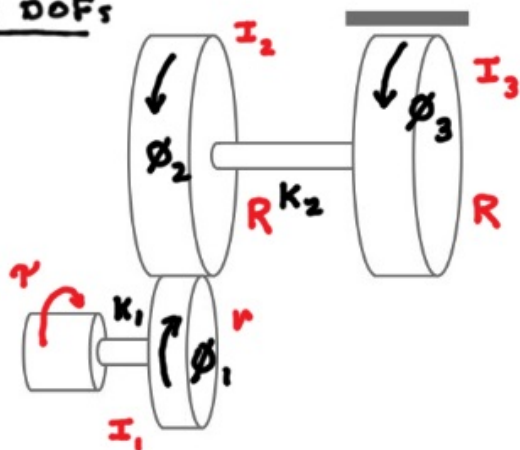
$$m_1 \ddot{x}_1 + k_1 x_1 + c_1 \dot{x}_1 - k_2 (x_2 - x_1) = F$$

$$m_2 \ddot{x}_2 + K_2 (x_2 - x_1) - k_3 (u - x_2) = 0$$

### Example 3

3 motion vars:  $\phi_1, \phi_2, \phi_3$  } 2 DOFs  
 1 constraint:  $r\phi_1 = R\phi_2$

Develop the FBDs for the system at right.



$$\begin{aligned} -I_1 \ddot{\phi}_1 - Fr + \tau &= 0 \quad 1. \rightarrow F = \frac{1}{r} (-I_1 \ddot{\phi}_1 + \tau), \ddot{\phi}_1 = \frac{R}{r} \ddot{\phi}_2 \\ -I_2 \ddot{\phi}_2 + K_1(\phi_3 - \phi_2) + FR &= 0 \quad 2. \\ -I_3 \ddot{\phi}_3 - K_2(\phi_3 - \phi_2) &= 0 \quad 3. \\ -I_2 \ddot{\phi}_2 + K_2(\phi_3 - \phi_2) + \frac{R}{r} (-I_1 \frac{R}{r} \ddot{\phi}_2 + \tau) &= 0 \end{aligned}$$

$$\begin{aligned} [I_2 + (\frac{R}{r})^2 I_1] \ddot{\phi}_2 + K_2(\phi_2 - \phi_3) &= \frac{R}{r} \tau \\ I_3 \ddot{\phi}_3 + K_2(\phi_3 - \phi_2) &= 0 \end{aligned}$$

## Summary

You are now a spring/damper ninja and can create FBDs of just about any translational, rotational dynamic system with springs and dampers.

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