

Experiment 1: Transfer Characteristics of a CS Amplifier

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Objective

- To obtain the transfer characteristics of a NMOS CS amplifier when (i) $R_D = 2.43 \text{ k}\Omega$, (ii) $R_D = 4.58 \text{ k}\Omega$ and (iii) Coupled NMOS with $R_D = 4.58 \text{ k}\Omega$.
- To plot the derivative (gain) in MATLAB and obtain the maximum gain and V_{\max} i.e. the input voltage V_{IN} at which the maximum gain occurs.
- To use the techniques of polynomial fitting and fast fourier transform to find the frequency spectrum of amplitude of V_{out} and thus determine the Total Harmonic Distortion (THD).
- To check the THD value for a given input signal when we cascade multiple amplifier stages together. Also, to see whether we get any difference in THD in case we change the order of the amplifiers (high gain first vs low gain first).
- To check the THD degradation as the output bias point is skewed away from the mid value of $V_{DD}/2$.
- To check the THD value for increasing signal magnitude and different gain values.

Components

- MOSFET
- Breadboard
- Resistors
- Potentiometers
- Connecting wires

Circuit Diagram

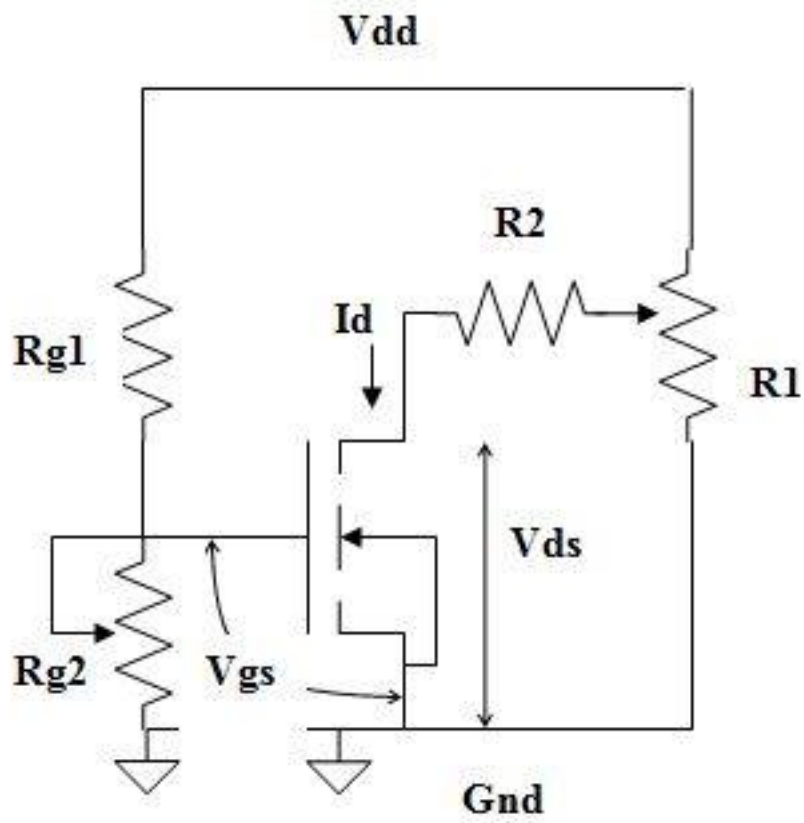


Fig. 2.a

Circuit diagram

Observation Table

0.1 V_{out} vs V_{in} for $R_D=2.54k\Omega$

| $V_{out}(V)$ | $V_{in}(V)$ |
|--------------|-------------|
| 1.53 | 12.02 |
| 1.78 | 12.01 |
| 1.97 | 11.83 |
| 2.14 | 11.54 |
| 2.24 | 11.29 |
| 2.31 | 11.05 |
| 2.36 | 10.88 |
| 2.45 | 10.54 |
| 2.55 | 10.13 |
| 2.63 | 9.78 |
| 2.7 | 9.38 |
| 2.77 | 9.04 |
| 2.81 | 8.86 |
| 2.87 | 8.57 |
| 2.91 | 8.19 |
| 2.98 | 7.81 |
| 3 | 7.67 |
| 3.06 | 7.27 |
| 3.11 | 6.98 |
| 3.17 | 6.55 |
| 3.22 | 6.14 |
| 3.3 | 5.64 |
| 3.4 | 4.99 |
| 3.43 | 4.57 |
| 3.51 | 4.11 |
| 3.61 | 3.83 |
| 3.59 | 3.46 |
| 3.64 | 2.94 |
| 3.69 | 2.6 |
| 3.74 | 2.08 |
| 3.78 | 1.7 |
| 3.85 | 1.22 |
| 3.94 | 0.99 |
| 4.1 | 0.8 |
| 4.88 | 0.54 |
| 5.86 | 0.41 |
| 6.3 | 0.38 |

0.2 V_{out} vs V_{in} for $R_D=4.9k\Omega$

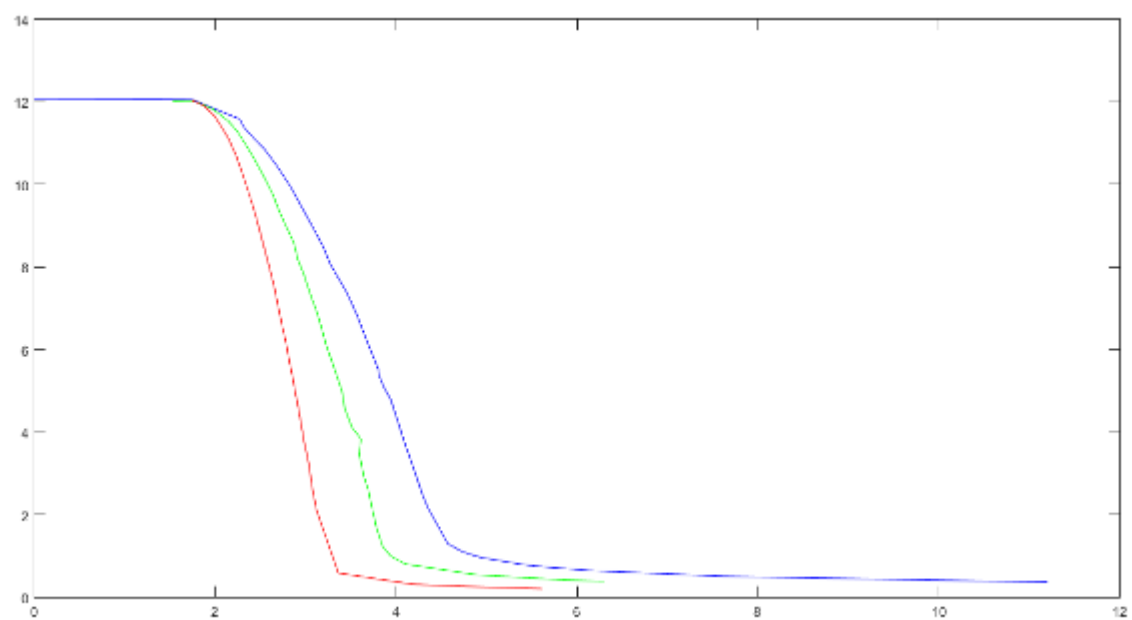
| $V_{out}(V)$ | $V_{in}(V)$ |
|--------------|-------------|
| 0.0 | 12.06 |
| 1.33 | 12.07 |
| 1.74 | 12.06 |
| 2.27 | 11.58 |
| 2.31 | 11.4 |
| 2.42 | 11.13 |
| 2.54 | 10.86 |
| 2.67 | 10.48 |
| 2.83 | 9.95 |
| 3.03 | 9.15 |
| 3.19 | 8.5 |
| 3.27 | 8.07 |
| 3.45 | 7.39 |
| 3.56 | 6.86 |
| 3.68 | 6.18 |
| 3.8 | 5.53 |
| 3.81 | 5.37 |
| 3.86 | 5.1 |
| 3.94 | 4.78 |
| 4.07 | 3.89 |
| 4.11 | 3.63 |
| 4.19 | 3.13 |
| 4.29 | 2.48 |
| 4.35 | 2.16 |
| 4.57 | 1.29 |
| 4.73 | 1.1 |
| 4.93 | 0.96 |
| 5.42 | 0.78 |
| 5.69 | 0.72 |
| 6.15 | 0.64 |
| 7.63 | 0.5 |
| 10.14 | 0.4 |
| 11.2 | 0.36 |

0.3 V_{out} vs V_{in} for coupled NMOS

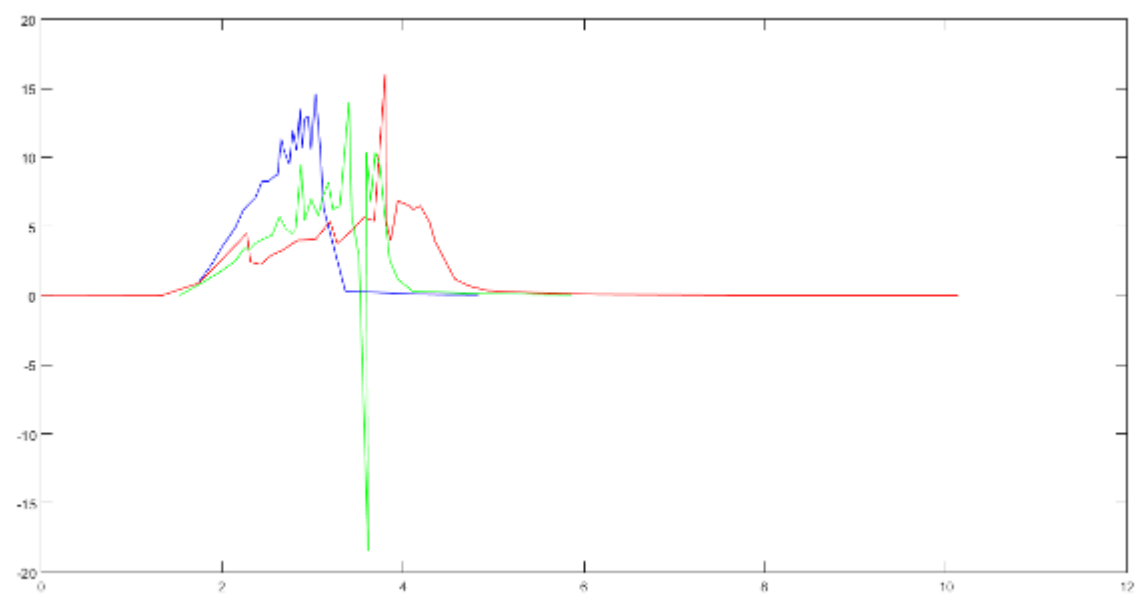
| $V_{out}(V)$ | $V_{in}(V)$ |
|--------------|-------------|
| 1.74 | 12.04 |
| 1.88 | 11.9 |
| 2.0 | 11.63 |
| 2.14 | 11.13 |
| 2.23 | 10.69 |
| 2.28 | 10.38 |
| 2.37 | 9.79 |
| 2.44 | 9.29 |
| 2.51 | 8.71 |
| 2.58 | 8.13 |
| 2.61 | 7.87 |
| 2.65 | 7.52 |
| 2.68 | 7.18 |
| 2.74 | 6.55 |
| 2.78 | 6.17 |
| 2.82 | 5.69 |
| 2.86 | 5.27 |
| 2.88 | 5.0 |
| 2.91 | 4.68 |
| 2.95 | 4.17 |
| 2.98 | 3.78 |
| 3.03 | 3.25 |
| 3.08 | 2.52 |
| 3.12 | 2.09 |
| 3.36 | 0.58 |
| 4.17 | 0.31 |
| 4.45 | 0.28 |
| 4.83 | 0.25 |
| 5.61 | 0.2 |

Plots

Plot of V_{out} vs V_{in}

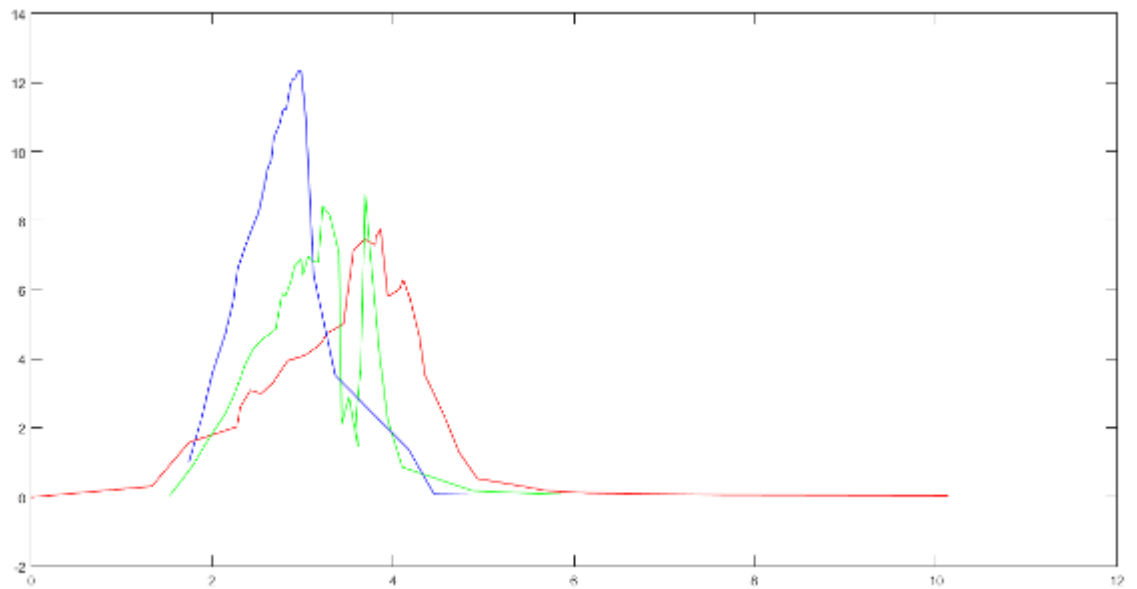


Gain versus V_{in}

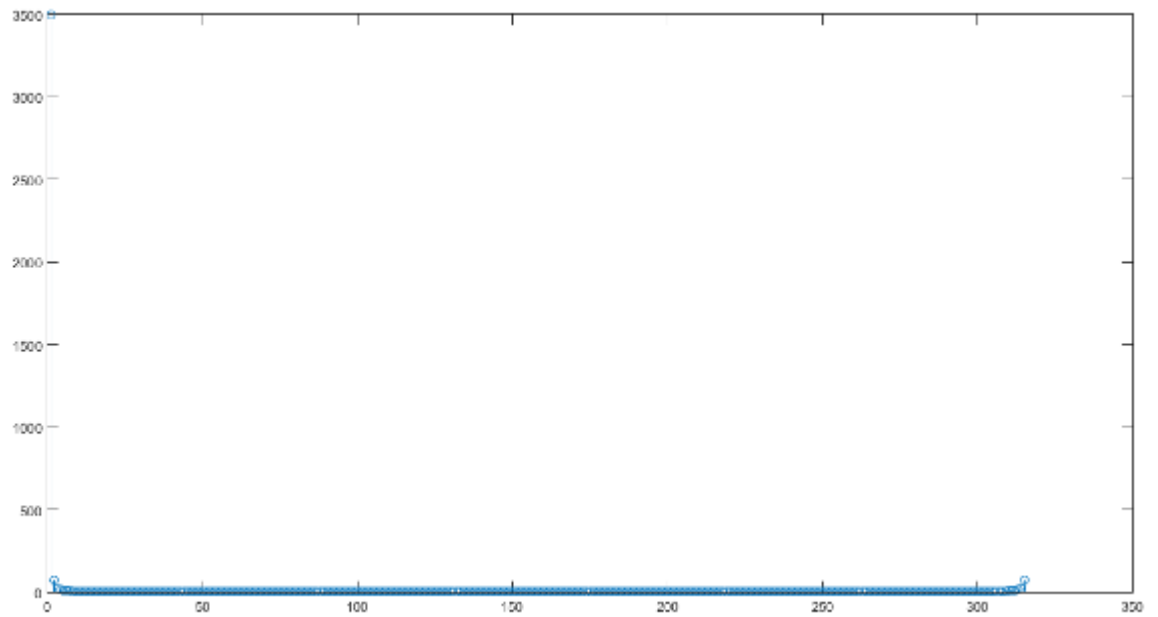


Gain versus V_{in} with moving average

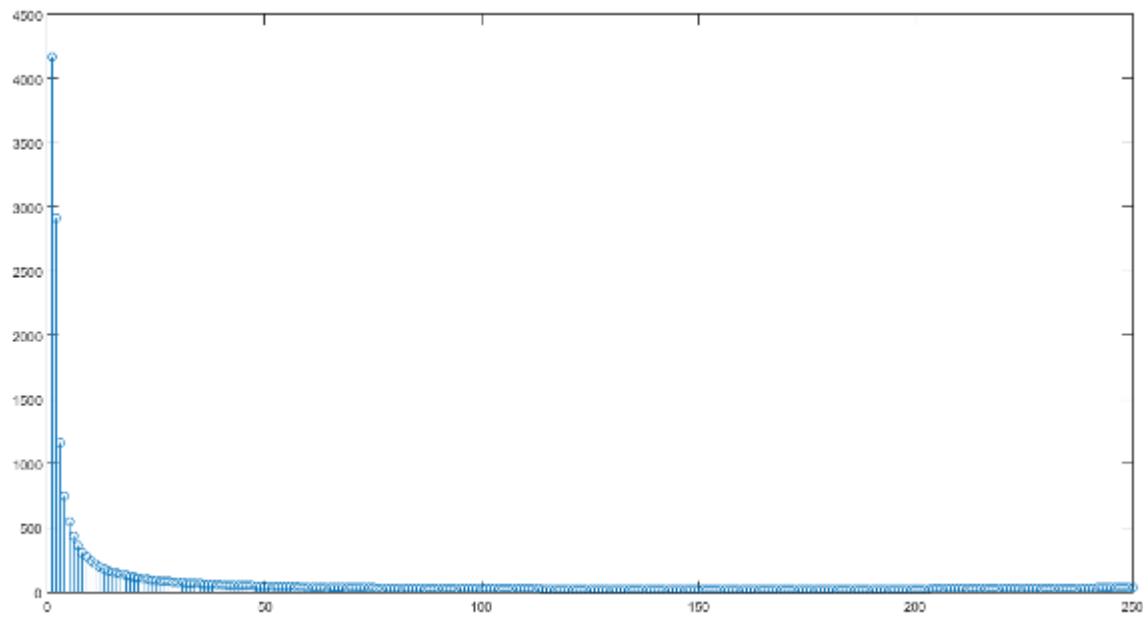
Then, we take a moving average smoothing filter (included in the MATLAB library as a built-in function) to smoothen it. Given below are the unsmoothed and smoothed plots respectively.



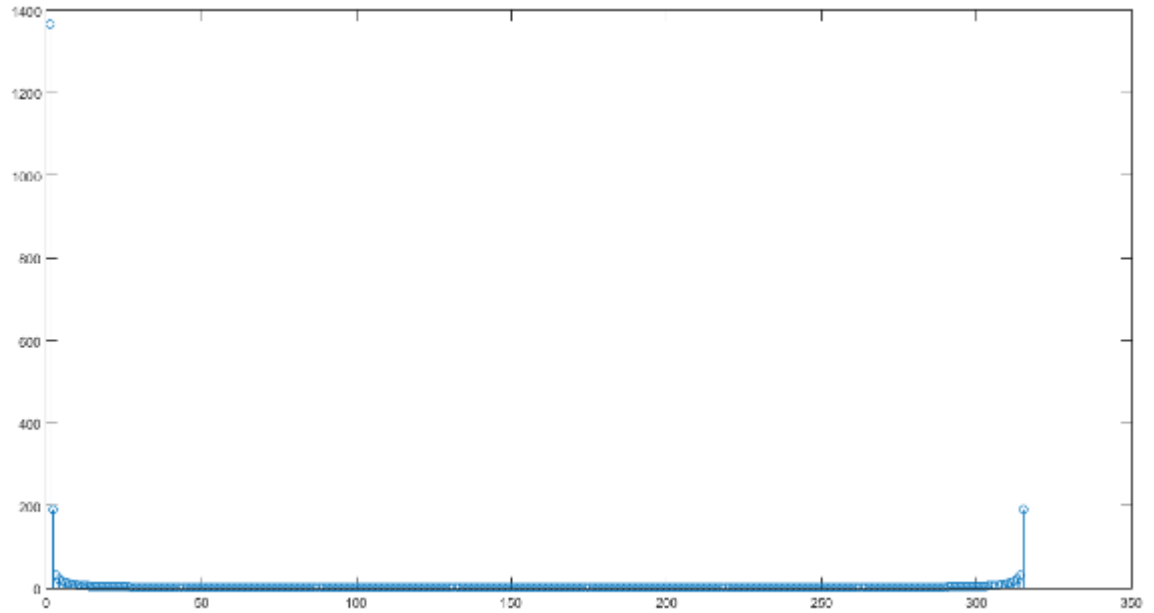
fft of amplifier response for $R_D=1.54k\Omega$



fft of amplifier response for $R_D=4.59k\Omega$



fft of amplifier response for coupled NMOS



Results

The bias point selected are as follows:

- i. $V_m = 3.726 \text{ V}$
- ii. $V_m = 3.120 \text{ V}$
- iii. $V_m = 2.717 \text{ V}$

From the plots, we infer that V_m value decreases and slope increases from case (i) to case (iii). This is the direct consequence of the formula $V_{out} = V_{DD} - K_n R_D (V_{in} - V_{tn})$. It is apparent that if either K_n or R_D increase, slope increases and V_m decreases.

SMALL SIGNAL OUTPUT CHARACTERISTICS (CALCULATION OF THD)

Now, we shift our origin to $(V_m, V_{DD}/2)$ and clip out the cut-off and triode parts and take only the region where the output is more or less linear. Following this, we use a degree 3 polynomial to fit the data (using inbuilt function `polyfit`), give a sinusoidal input array (`Sin(t)`) and then take the fast-Fourier transform (using inbuilt function `fft`) of the obtained output to study the

non-linearity of the amplifier. Following are the amplitude spectrum plots obtained: The given plots are for Case 1, Case 2 and Case 3 respectively.

Now, let us calculate the values of Total Harmonic Distortion for the three different gain values (the three different cases)

| THD ₁ | THD ₂ | THD ₃ |
|------------------|------------------|------------------|
| 7.43 | 8.39 | 14.31 |

ADDITIONAL LINEARITY TESTS

We calculate the Total Harmonic Distortion (THD) by taking inputs of different peak to peak values.

THD₁(for amplitude 0.5 V_{p-p}) = 7.43%

THD₁(for amplitude 1.0 V_{p-p}) = 11.7%

THD₁(for amplitude 2.0 V_{p-p}) = 20.61%

We can see that as input signal amplitude is increased, the total harmonic distortion increases. It is obvious because the input signal is affected by non-linear gain area due to change in curvature of fitted curve (In this case we used 6th degree polynomial) and hence gets distorted. Now, we check the degradation of THD as the bias point is skewed away from (V_m, VDD/2). It is expected that closer the bias point is to VDD/2 the lesser the THD, since the entire input signal we lie in the linear range.

We perform this check for again the first set of data. We take the bias point as 4.16V skewing away from 3.727V.

THD₁ = 16.94%

(skewed case)

Next we try to see the THD values when we cascade amplifiers of different gains. Then we try to observe the difference between the cases when low gain amplifier is kept at first stage versus when high gain amplifier is kept at second stage. Following are the amplitude spectrum plots for the two cases:

THD_{1→2}(low → high gain) = 24.27%

THD_{2→1}(high → low gain) = 7.92%

So, we see that when the high gain amplifier is taken as the first stage, we get a lesser value of THD. It is because the output of the first amplifier (high gain) is fed into the low gain amplifier. There is a fair chance that the signal may enter the non-linear region. But due to low gain the effect of non-linearity is quite suppressed as compared to the other case.

Discussion

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- We notice that there is a tradeoff between gain and linearity, as the gain increases, the linearity decreases which is reflected from the THD.
- As we fit the data with a better fitting function (DC transfer function) we see that the point where the maximum AC gain is obtained changes and the THD changes. We see that the Gaussian function is a better approximation than Fourier fit, and hence gives a better approximation of the DC bias point. As we move away from this point we notice that the THD increases.

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- When giving the input signal, it is important to ensure that the input span is within the linear region. For this purpose, input had to be scaled, especially when the gain is very high, as in the case of cascade amplifier configuration. For cascade amplifier, we have used input voltage of 0.1V_{p-p}.
- For completely linear output, THD=0% and the amplifier is said to be a linear amplifier.
- As bias point is skewed away from ($V_m, V_{DD}/2$), the new dc biasing is closer to the non-linear region and the same V_{p-p} causes more distortion. As a result, the THD obtained is higher.
- We get a higher value of THD for higher value of gain. This depicts the gain-linearity tradeoff.
- It is important to note that we do not consider the dc component of output signal while calculating the THD, as it is only because of the harmonics of the fundamental frequency.
- To find V_m , rather than using the discrete derivative curve or its smoothened counterpart (using moving average smoothing), we prefer taking the derivative of a Fourier or Gaussian fit as it is more exact and gives us a more accurate value of V_m . In our case we went on with Gaussian fit because it was observed to be more accurate of the two. It is worth noting that for the optimum performance of these fitting techniques the input needs to be equi-spaced or they tend to diverge at places where concentration of input is low.