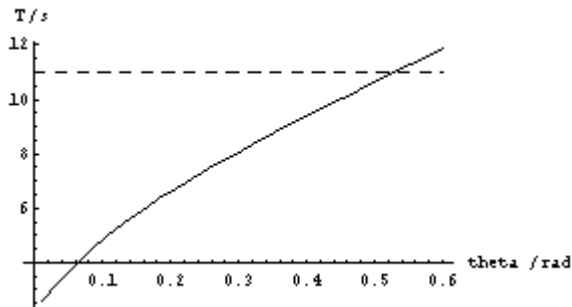
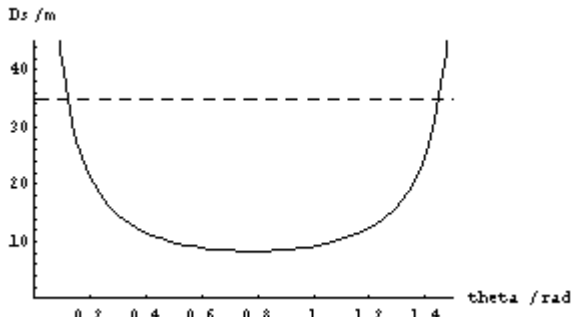


--	--	--

<p><u>Alternate Solution (Not taking induced emf into consideration):</u></p> <p>If induced emf is not taken into account, there is no induced current, so the net force acting on the combined mass of the young man and rod is</p> $F_N = BIL - mg \sin \theta .$ <p>And we have instead</p> $dv / dt = \alpha ,$ <p>where</p> $\alpha = BIL / m - g \sin \theta .$ $\therefore v(t) = \alpha t$ <p>and</p> $\therefore v_s = v(t_s) = \alpha t_s$ $t_f = \frac{2v_s \sin \theta}{g} = \frac{2\alpha t_s \sin \theta}{g} .$ <p>Therefore,</p> $w = (v_s \cos \theta) t_f = \frac{\alpha^2 t_s^2 \sin 2\theta}{g} ,$ <p>giving</p> $t_s = \frac{1}{\alpha} \sqrt{\frac{gw}{\sin 2\theta}}$ <p>and</p> $t_f = \sqrt{\frac{2w \tan \theta}{g}} .$ <p>Hence,</p> $T = t_s + t_f = \frac{1}{\alpha} \sqrt{\frac{gw}{\sin 2\theta}} + \sqrt{\frac{2w \tan \theta}{g}} = \frac{\sqrt{wg}}{\alpha} \left[1 + 2 \left(\frac{\alpha}{g} \right) \sin \theta \right] .$ <p>where $\alpha = BIL / m - g \sin \theta .$</p> <p>The values of the parameters are: B=10.0 T, I= 2424 A, L=2.00m, R=1.0 Ω, g=10 m/s², m=80 kg, and w=1000 m. Then,</p> $T = \frac{100}{\alpha} \frac{[1 + 0.20\alpha \sin \theta]}{\sqrt{\sin 2\theta}}$ <p>where $\alpha = 606 - 10 \sin \theta .$</p>	<p>0.2 BIL 0.2 mg sin θ</p> <p>0.1</p> <p>0.2</p> <p>0.5</p> <p>0.5</p> <p>0.3</p>	<p>2</p>
--	--	----------

 <p>For θ within the range ($\sim 0, 0.52$) radian the time T is within 11 s.</p>	<p>Labeling: 0.1 each axis</p> <p>Unit: 0.1 each axis</p> <p>Proper Range in θ: 0.1 lower limit (more than 0, less than 0.5), 0.2 upper limit (more than 0.52 and less than 0.8)</p> <p>Proper shape of curve: 0.2</p> <p>Accurate intersection at $\theta = 0.52$: 0.4</p>	<p>1.3</p>
<p>However, there is another constraint, i.e. the length of rail D. Let D_s be the distance travelled during the time interval t_s</p> $D_s = \frac{gw}{2\alpha \sin 2\theta} = \frac{5000}{\alpha \sin 2\theta}$ <p>which is plotted below</p>  <p>It is necessary that $D_s \leq D$, which means θ must range between 0.11 and 1.43 radians.</p> <p>In order to satisfy both conditions, θ must range between 0.11 & 0.52 radians.</p>	<p>Labeling: 0.1 each axis</p> <p>Unit: 0.1 each axis</p> <p>Proper Range in θ: 0.1 lower limit (more than 0.08, less than 0.11), 0.1 upper limit (more than 0.52 and less than 1.5)</p> <p>Proper shape of curve: 0.2</p> <p>Accurate intersection at $\theta = 0.11$: 0.4</p>	<p>1.2</p> <p>0.5</p>

Question 3 - Marking Scheme

(a) Since $W(v) = 4\pi \left(\frac{M}{2\pi R T} \right)^{3/2} v^2 e^{-M v^2 / (2RT)}$,

$$\bar{v} = \int_0^{\infty} v W(v) dv =$$

$$= \int_0^{\infty} v 4\pi \left(\frac{M}{2\pi R T} \right)^{3/2} v^2 e^{-M v^2 / (2RT)} dv$$

$$= \int_0^{\infty} 4\pi \left(\frac{M}{2\pi R T} \right)^{3/2} v^3 e^{-M v^2 / (2RT)} dv$$

$$= 4\pi \left(\frac{M}{2\pi R T} \right)^{3/2} \int_0^{\infty} v^3 e^{-M v^2 / (2RT)} dv$$

$$= 4\pi \left(\frac{M}{2\pi R T} \right)^{3/2} \frac{4 R^2 T^2}{2 M^2}$$

$$= \sqrt{\frac{8 R T}{\pi M}}$$

Marking Scheme:

Performing the integration correctly:

1 mark

Simplifying

0.5 marks

Subtotal for the section

1.5

marks

- (b) Assuming an ideal gas, $P V = N k T$, so that the concentration of the gas molecules, n , is given by

$$n = \frac{N}{V} = \frac{P}{k T}$$

the impingement rate is given by

$$\begin{aligned} J &= \frac{1}{4} n \bar{v} \\ &= \frac{1}{4} \frac{P}{k T} \sqrt{\frac{8 R T}{\pi M}} \\ &= P \sqrt{\frac{8 R T}{16 k^2 T^2 \pi M}} \\ &= P \sqrt{\frac{N_A k}{2 k^2 T \pi M}} \\ &= P \sqrt{\frac{1}{2 k T \pi m}} \\ &= \frac{P}{\sqrt{2 \pi m k T}} \end{aligned}$$

where we have note that $R = N_A k$ and $m = \frac{M}{N_A}$ (N_A being Avogadro number).

Marking Scheme:

Using ideal gas formula to estimate concentration of gas molecules:	0.7
marks	
Simplifying expression:	0.4
marks	
Using $R = N k$, and the formula for m ; (0.2 mark each)	0.4
marks	
<u>Subtotal for the section</u>	<u>1.5</u>
<u>marks</u>	

- (c) Assuming close packing, there are approximately 4 molecules in an area of $16 r^2$ m^2 . Thus, the number of molecules in 1 m^2 is given by

$$n_1 = \frac{4}{16 (3.6 \times 10^{-10})^2} = 1.9 \times 10^{18} \text{ m}^{-2}$$

However at $(273 + 300) \text{ K}$ and 133 Pa , the impingement rate for oxygen is

$$\begin{aligned} J &= \frac{P}{\sqrt{2 \pi m k T}} \\ &= \frac{133}{\sqrt{2 \pi \left(\frac{32 \times 10^{-3}}{6.02 \times 10^{23}} \right) (1.38 \times 10^{-23}) 573}} \\ &= 2.6 \times 10^{24} \text{ m}^{-2} \text{ s}^{-1} \end{aligned}$$

Therefore, the time needed for the deposition is $\frac{n_1}{J} = 0.7 \mu\text{s}$

The calculated time is too short compared with the actual processing.

Marking Scheme:

Estimation of number of molecules in 1 m^2 :	0.4 marks
Calculation the impingement rate:	0.6 marks
Taking note of temperature in Kelvin	0.3 marks
Calculating the time	0.4 marks
<u>Subtotal for the section</u>	<u>1.7</u>
<u>marks</u>	

- (d) With activation energy of 1 eV and letting the velocity of the oxygen molecule at this energy is v_1 , we have

$$\frac{1}{2} m v_1^2 = 1.6 \times 10^{-19} \text{ J}$$

$$\Rightarrow v_1 = 2453.57 \text{ ms}^{-1}$$

At a temperature of 573 K, the distribution of the gas molecules is

We can estimate the fraction of the molecules with speed greater than 2454 ms^{-1} using the trapezium rule (or any numerical techniques) with ordinates at 2453, $2453 + 500$, $2453 + 1000$. The values are as follows:

Velocity, v	Probability, $W(v)$
2453	1.373×10^{-10}
2953	2.256×10^{-14}
3453	6.518×10^{-19}

Using trapezium rule, the fraction of molecules with speed greater than 2453 ms^{-1} is given by

$$\text{fraction of molecules} = \frac{500}{2} \left[(1.373 \times 10^{-10}) + (2 \times 2.256 \times 10^{-14}) + (6.518 \times 10^{-19}) \right]$$

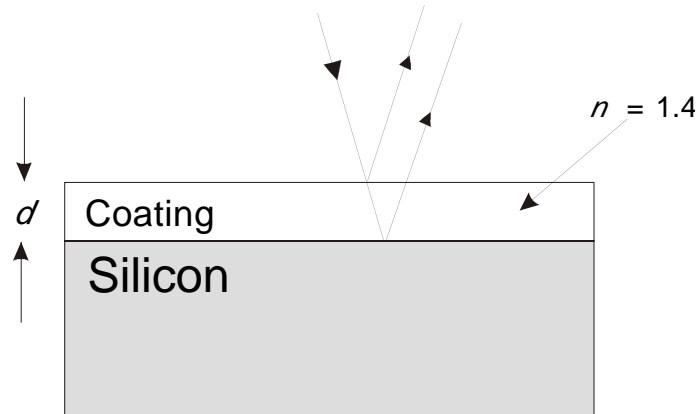
$$f = 3.43 \times 10^{-8}$$

Thus the time needed for the deposition is given by $0.7 \mu\text{s} / (3.43 \times 10^{-8})$ that is 20.4 s

Marking Scheme

Computing the value of the cut-off energy or velocity:	0.6
marks	
Estimating the fraction of molecules	1.2 marks
Correct method of final time	0.4 marks
Correct value of final time	0.6 marks
<u>Subtotal for the section</u>	<u>2.8</u>
<u>marks</u>	

- (e) For destructive interference, optical path difference = $2 d = \frac{\lambda'}{2}$ where $\lambda' = \frac{\lambda_{\text{air}}}{n}$ is the wavelength in the coating.



The relation is given by:

$$d = \frac{\lambda_{\text{air}}}{4 n}$$

Plugging in the given values, one gets $d = 105$ or 105.2 nm.

Derive equation:

Finding the optical path length 0.2 marks

Knowing that there is a phase change at the reflection 0.5 marks

Putting everything together to get the final expression 0.6 marks

Subtotal: 1.3 marks

Computation of d : 0.6 marks

Getting the correct number of significant figures: 0.6 marks

Subtotal: 1.2 marks

Subtotal for Section 2.5 marks

TOTAL 10 marks